Appendix S

Transportation Study



TRAFFIC IMPACT STUDY

OUR LADY OF MT. LEBANON PROJECT

City of Los Angeles, California April 16, 2019

Prepared for:

Sheppard, Mullin, Richter & Hampton LLP 333 S. Hope Street, 43rd Floor Los Angeles, California 90071

LLG Ref. 5-17-0315-1



Prepared by:

Jason A. Shender Transportation Planner II Under the Supervision of:

David S. Shender, P.E. Principal

Linscott, Law & Greenspan, Engineers

20931 Burbank Boulevard Suite C Woodland Hills, CA 91367

818.835.8648 T 818.835.8649 F

www.llgengineers.com

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TRAFFIC IMPACT STUDY

OUR LADY OF MT. LEBANON PROJECT

City of Los Angeles, California April 16, 2019

1.0 Introduction

This traffic analysis has been conducted to identify and evaluate the potential construction and operational traffic impacts of the proposed Our Lady of Mt. Lebanon Project (the "Project") located at 333 S. San Vicente Boulevard in the City of Los Angeles. The Project applicant seeks to construct 153 residential apartments units and 31,342 square feet of church floor area. The Project site is bounded by an existing alleyway to the north, Burton Way to the south, S. San Vicente Boulevard to the east, and Holt Avenue to the west. The Project site location and general vicinity are shown in *Figure 1–1*.

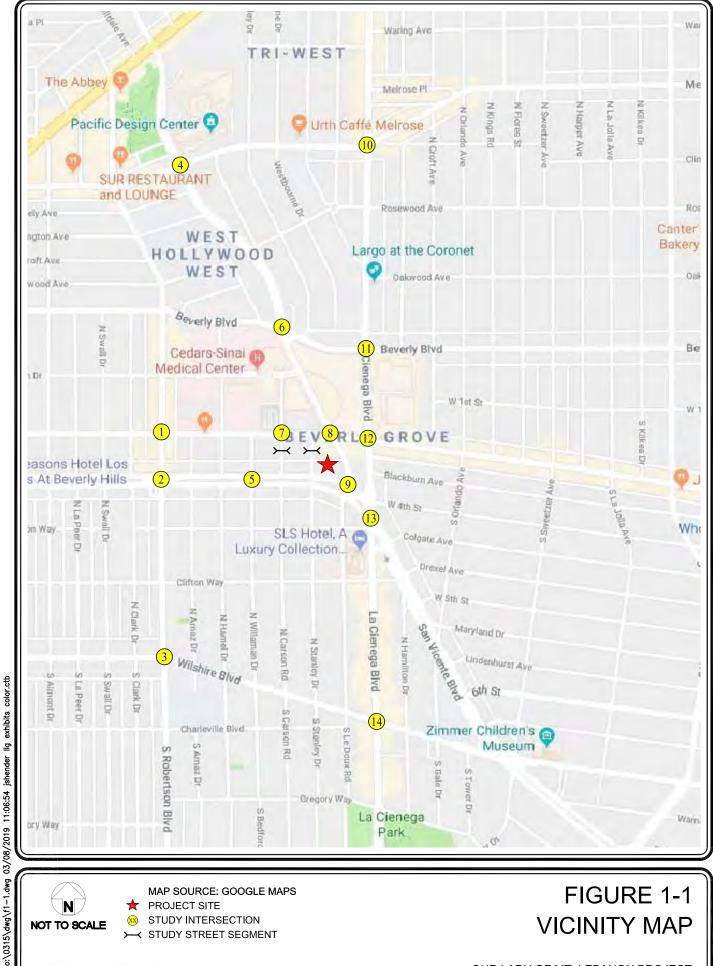
The traffic analysis follows City of Los Angeles traffic study guidelines¹ and is consistent with traffic impact assessment guidelines set forth in the Los Angeles County Congestion Management Program². This traffic analysis evaluates potential Project-related impacts at 14 key intersections in the vicinity of the Project site. The study intersections were determined in consultation with City of Los Angeles Department of Transportation (LADOT) staff. Critical Movement Analysis method was used to determine Volume-to-Capacity (v/c) ratios and corresponding Levels of Service (LOS) at the study intersections located within the City of Los Angeles. Additionally, a supplemental analysis utilizing the Intersection Capacity Utilization method was used to determine Volume-to-Capacity ratios and corresponding LOS for the study intersections located within or shared with the City of Beverly Hills. supplemental analysis utilizing the Highway Capacity Manual method was used to determine average control delays and corresponding LOS at the study intersections located within or shared with the City of West Hollywood. In addition, a review of potential impacts to local residential street segments was prepared for two residential street segments in the vicinity of the Project site. A review also was conducted of Los Angeles County Metropolitan Transportation Authority (Metro) freeway and intersection monitoring stations to determine if a Congestion Management Program transportation impact assessment analysis is required for the proposed Project. This traffic analysis also includes a screening of the proposed Project's potential impacts on freeway mainline segments and off-ramps. Finally, the traffic impacts associated with the construction of the Project were assessed.

This study (i) presents existing traffic volumes, (ii) includes existing traffic volumes with the forecast net new traffic volumes from the proposed Project, (iii) forecasts future cumulative baseline traffic volumes, (iv) forecasts future traffic volumes with the proposed Project, and (vi) determines future forecast with Project-related impacts.

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¹ Transportation Impact Study Guidelines, City of Los Angeles Department of Transportation, December 2016.

² 2010 Congestion Management Program for Los Angeles County, Los Angeles County Metropolitan Transportation Authority, 2010.





1.1 Study Area

Upon coordination with LADOT staff, 14 study intersections have been identified for evaluation during the weekday morning and afternoon peak hours. The study intersections were evaluated from 7:00 AM to 10:00 AM and 3:00 PM to 6:00 PM on Thursday, May 17, 2018 to determine the respective peak commuter hours. The 14 study intersections provide local access to the study area and define the extent of the boundaries for this traffic impact analysis. Further discussion of the existing street system and study area is provided in Section 3.0.

The general location of the Project in relation to the study locations and surrounding street system is presented in $Figure \ 1-1$. The traffic analysis study area is generally comprised of those locations which have the greatest potential to experience significant traffic impacts due to the proposed Project as defined by the Lead Agency. In the traffic engineering practice, the study area generally includes those intersections that are:

- a. Immediately adjacent or in close proximity to the Project site;
- b. In the vicinity of the Project site that are documented to have current or projected future adverse operational issues; and
- c. In the vicinity of the Project site that are forecast to experience a relatively greater percentage of Project-related vehicular turning movements (e.g., at freeway ramp intersections).

The locations selected for analysis were based on the above criteria, the peak-hour vehicle trip generation associated with the proposed Project, the anticipated distribution of Project vehicular trips, and existing intersection/corridor operations.

2.0 PROJECT DESCRIPTION

2.1 Site Location

The Project site is located at 333 S. San Vicente Boulevard in the City of Los Angeles. The Project site is bounded by an existing alleyway to the north, Burton Way to the south, San Vicente Boulevard to the east, and Holt Avenue to the west. The Project site location and general vicinity are shown in *Figure 1–1*.

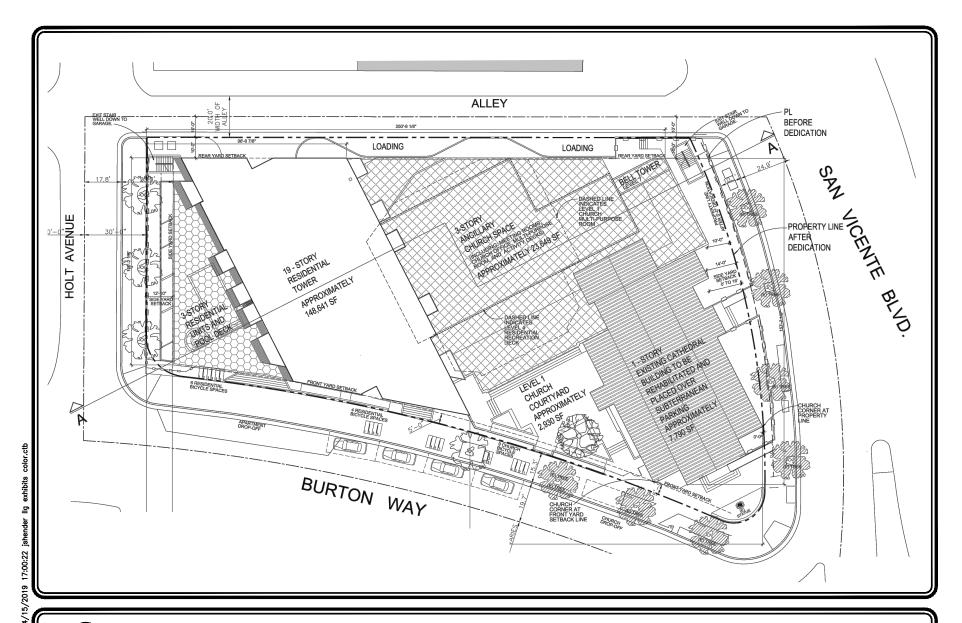
2.2 Existing Project Site

The Project site is currently owned by Our Lady of Mt. Lebanon – St. Peter Cathedral and is presently occupied by four buildings and a surface parking lot, the latter of which covers approximately half of the Project site. The four buildings include the cathedral building, a rectory, social hall, and chancery. Vehicular access to the Project site is currently provided via the adjacent alleyway located north of the Project site. In addition, two driveways are provided along the existing Project site's Burton Way frontage.

2.3 Project Description

The Project includes 153 residential apartments units and 31,342 square feet of church floor area. Construction and occupancy of the proposed Project is planned to be completed by the year 2024. The existing cathedral building will be retained and modified to increase the floor area from 6,848 square feet to 7,790 square feet. The other three existing buildings will be removed to accommodate development of the Project. The site plan for the Project is illustrated in *Figure* 2–1.

Vehicular access to the Project site following development of the Project will be provided via the adjacent alleyway located north of the Project site. Further discussion of the Project site access and circulation schemes is provided in Section 3.0.





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MAP SOURCE: NADEL ARCHITECTURE + PLANNING

FIGURE 2-1 PROJECT SITE PLAN

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3.0 SITE ACCESS AND CIRCULATION

The proposed site access scheme for the Project is displayed in Figure 2-1. A description of the proposed site access and circulation scheme is provided in the following subsections.

3.1 Existing Vehicular Site Access

Existing vehicular access to the Project site is provided via one driveway along the south side of adjacent alley located on the northerly frontage of the Project site. In addition, two driveways are provided along the existing Project site's Burton Way frontage.

3.2 Vehicular Project Site Access

Vehicular access to the Project site will be provided via one point of access along the south side of adjacent alley located along the north edge of the Project site. The Project's alley access will provide vehicular access to the subterranean levels of the on-site parking garage. The alley access is proposed to accommodate left-turn and right-turn ingress and egress turning movements.

The existing curb cuts on Burton Way serving the parking area on the existing Project site will be closed in conjunction with the Project. The Project will accommodate passenger loading/unloading along the Project's Burton Way frontage.

4.0 Existing Street System

4.1 Regional Highway System

Primary regional access to the Project Site is provided by the I-10 (Santa Monica) Freeway. A brief description of the I-10 Freeway is provided in the following paragraph.

I-10 (Santa Monica) Freeway is an east-west freeway that extends across Southern California. In the project vicinity, four mixed-free flow freeway lanes are provided on the I-10 Freeway. Eastbound and westbound ramps on the I-10 Freeway are provided at Robertson Boulevard and La Cienega Boulevard in the Project vicinity, and are located approximately three miles south of the Project site.

4.2 Local Roadway System

The study intersections were selected in consultation with LADOT staff. The following intersections were analyzed for potential traffic impacts due to the proposed Project:

- 1. Robertson Boulevard / 3rd Street (City of Los Angeles)
- 2. Robertson Boulevard / Burton Way (City of Los Angeles / City of Beverly Hills)
- 3. Robertson Boulevard / Wilshire Boulevard (City of Beverly Hills)
- 4. San Vicente Boulevard / Melrose Avenue (City of West Hollywood)
- 5. Willaman Drive / Burton Way (City of Los Angeles)
- 6. San Vicente Boulevard / Beverly Boulevard (City of Los Angeles / City of West Hollywood)
- 7. Sherbourne Drive / 3rd Street (City of Los Angeles)
- 8. San Vicente Boulevard / 3rd Street (City of Los Angeles)
- 9. San Vicente Boulevard Le Doux Road / Burton Way (City of Los Angeles)
- 10. La Cienega Boulevard / Melrose Avenue (City of West Hollywood)
- 11. La Cienega Boulevard / Beverly Boulevard (City of Los Angeles)
- 12. La Cienega Boulevard / 3rd Street (City of Los Angeles)
- 13. La Cienega Boulevard / San Vicente Boulevard (City of Los Angeles / City of Beverly Hills)
- 14. La Cienega Boulevard / Wilshire Boulevard (City of Beverly Hills)

As noted above, Intersections No. 2, 3, 13, and 14 are located within or shared with the City of Beverly Hills, and Intersections No. 4, 6, and 10 are located within or shared with the City of West Hollywood. The 14 intersections selected for analysis are all presently controlled by traffic signals. The existing lane configurations at the study intersections are displayed in *Figure 4–1*.

4.3 Roadway Descriptions

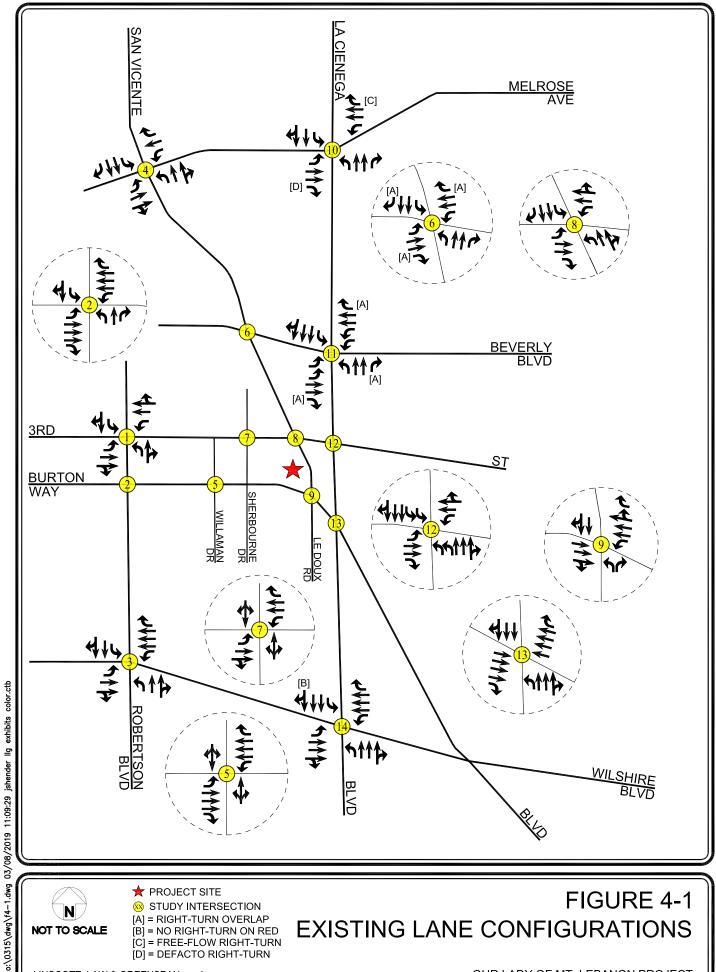
A brief description of the roadways in the Project vicinity is provided in the following paragraphs.

Robertson Boulevard is a north-south oriented roadway located west of the Project site. Within the Project study area, Robertson Boulevard is designated as an Avenue II by the City of Los Angeles and as a Minor Arterial by the City of Beverly Hills. One through travel lane is provided in each direction on Robertson Boulevard north of Burton Way within the Project study area. Two through travel lanes are provided in each direction on Robertson Boulevard south of Burton Way within the Project study area. Separate exclusive left-turn lanes are provided on Robertson Boulevard at major intersections. North of Burton Way, Robertson Boulevard is posted for a speed limit of 30 miles per hour. South of Burton Way, Robertson Boulevard is posted for a speed limit of 25 miles per hour.

San Vicente Boulevard is a north-south oriented roadway that borders the Project site to the east. Within the Project study area, San Vicente Boulevard is designated as a Boulevard II by the City of Los Angeles, as a Principal Arterial by the City of Beverly Hills, and as an Arterial by the City of West Hollywood. North of Burton Way, two through travel lanes are provided in each direction on San Vicente Boulevard within the Project study area. South of Burton Way, three through travel lanes are provided in each direction on San Vicente Boulevard within the Project study area. Separate exclusive left-turn lanes are provided on San Vicente Boulevard at major intersections. San Vicente Boulevard is posted for a speed limit of 35 miles per hour within the Project study area.

Willaman Drive is a north-south oriented roadway located west of the Project site. Within the Project study area, Willaman Drive is designated as a Local Street by the City of Los Angeles. One through travel lane is provided in each direction on Willaman Drive within the Project study area. There is no speed limit posted on Willaman Drive within the Project study area, thus a prima facie speed limit of 25 miles per hour is assumed, consistent with the State of California Vehicle Code.

Sherbourne Drive is a north-south oriented roadway located west of the Project site. Within the Project study area, Sherbourne Drive is designated as a Local Street by the City of Los Angeles. One through travel lane is provided in each direction on Sherbourne Drive within the Project study area. There is no speed limit posted on Sherbourne Drive within the Project study area, thus a prima facie speed limit of 25 miles per hour is assumed, consistent with the State of California Vehicle Code.



N NOT TO SCALE

★ PROJECT SITE

STUDY INTERSECTION

[A] = RIGHT-TURN OVERLAP

[B] = NO RIGHT-TURN ON RED [C] = FREE-FLOW RIGHT-TURN [D] = DEFACTO RIGHT-TURN

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FIGURE 4-1 **EXISTING LANE CONFIGURATIONS**

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Holt Avenue is a north-south oriented roadway that borders the Project site to the west. Within the Project study area, Holt Avenue is designated as a Local Street by the City of Los Angeles. One through travel lane is provided in each direction on Holt Avenue within the Project study area. There is no speed limit posted on Holt Avenue within the Project study area, thus a prima facie speed limit of 25 miles per hour is assumed, consistent with the State of California Vehicle Code.

Le Doux Road is a north-south oriented roadway located south of the Project site. Within the Project study area, Le Doux Road is designated as a Local Street by the City of Los Angeles. One through travel lane is provided in each direction on Le Doux Road within the Project study area. There is no speed limit posted on Le Doux Road within the Project study area, thus a prima facie speed limit of 25 miles per hour is assumed, consistent with the State of California Vehicle Code.

La Cienega Boulevard is a north-south oriented roadway located east of the Project site. Within the Project study area, La Cienega Boulevard is designated as an Avenue I by the City of Los Angeles and as a Principal Arterial by the City of Beverly Hills. North of Melrose Avenue, La Cienega Boulevard is designated as a Collector by the City of West Hollywood within the Project study area. South of Melrose Avenue, La Cienega Boulevard is designated as an Arterial by the City of West Hollywood within the Project study area. North of Melrose Avenue, two through travel lanes are provided on La Cienega Boulevard in each direction. South of Melrose Avenue, three through travel lanes are provided in each direction. Separate exclusive left-turn lanes are provided on La Cienega Boulevard at major intersections. La Cienega Boulevard is posted for a speed limit of 35 miles per hour within the Project area.

3rd Street is an east-west oriented roadway located north of the Project site. Within the Project study area, 3rd Street is designated as an Avenue II by the City of Los Angeles. Two through travel lanes are provided in each direction on 3rd Street within the Project study area. Separate exclusive left-turn lanes are provided on 3rd Street at major intersections. 3rd Street is posted for a speed limit of 35 miles per hour within the Project study area.

Burton Way is an east-west oriented roadway that borders the Project site to the south. Within the Project study area, Burton Way is designated as an Avenue II by the City of Los Angeles and as a Principal Arterial by the City of Beverly Hills. Three through travel lanes are provided in each direction on Burton Way within the Project study area. Separate exclusive left-turn lanes are provided on Burton Way at major intersections. Burton Way is posted for a speed limit of 35 miles per hour within the Project study area.

Wilshire Boulevard is an east-west oriented roadway located south of the Project site. Within the Project study area, Wilshire Boulevard is designated as an Avenue I by the City of Los Angeles and as a Principal Arterial by the City of Beverly Hills. Three though travel lanes are provided in each direction on Wilshire Boulevard within the Project study area. Separate exclusive left-turn lanes are provided on Wilshire Boulevard at major intersections. Wilshire Boulevard is posted for a speed limit of 35 miles per hour within the Project study area.

Melrose Avenue is an east-west oriented roadway located north of the Project site. Within the project study area, Melrose Avenue is designated as an Avenue II by the City of Los Angeles and as a Collector by the City of West Hollywood. East of San Vicente Boulevard, two through travel lanes are provided in both directions on Melrose Avenue. West of San Vicente Boulevard, two through travel lanes are provided in the eastbound direction on Melrose Avenue, and one through travel lane is provided in the westbound direction on Melrose Avenue. Separate exclusive left-turn lanes are provided on Melrose Avenue at the major intersections. Melrose Avenue is posted for a speed limit of 35 miles within the Project study area.

Beverly Boulevard is an east-west oriented roadway located north of the Project site. Within the Project study area, Beverly Boulevard is designated as an Avenue I by the City of Los Angeles and as an Arterial by the City of West Hollywood. Two through travel lanes are generally provided in both directions on Beverly Boulevard within the Project study area. Separate exclusive left-turn lanes are provided on Beverly Boulevard at major intersections. Beverly Boulevard is posted for a speed limit of 35 miles per hour within the Project study area.

4.4 Public Transit Services

Public transit service within the Project study area is currently provided by the Los Angeles County Metropolitan Transit Authority (Metro), the City of Los Angeles Department of Transportation (LADOT), the City of West Hollywood (CityLine), and the Antelope Valley Transit Authority. A summary of the existing transit service, including the transit route, destinations and peak hour headways is presented in *Table 4–1*. The existing public transit routes in the Project site vicinity are illustrated in *Figure 4–2*.

Table 4-1
EXISTING PUBLIC TRANSIT ROUTES [1]

08-Mar-19

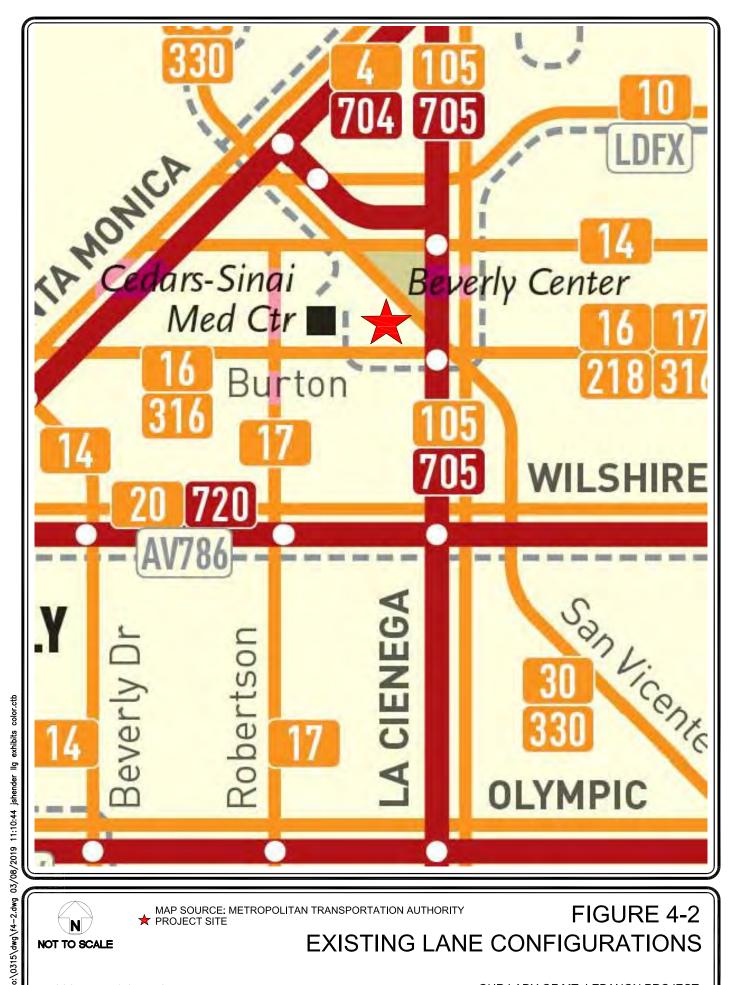
		ROADWAY(S)		NO. OF BUSES/TRAIN DURING PEAK HOUL			
ROUTE	DESTINATIONS	NEAR SITE	DIR	AM	PM		
Metro 10	Downtown Los Angeles to West Hollywood (via Temple Street & Melrose Avenue)	Melrose Avenue	EB WB	12 18	8 14		
Metro 14	Downtown Los Angeles to Beverly Hills (via Beverly Boulevard)	Beverly Boulevard	EB WB	14 23	26 22		
Metro 16/17/316	Downtown Los Angeles to Century City/Culver City Expo Station (via 3rd Street & Robertson Boulevard)	3rd Street	EB WB	33 35	35 35		
Metro 20	Downtown Los Angeles to Santa Monica (via Wilshire Boulevard)	Wilshire Boulevard	EB WB	16 17	17 17		
Metro 30/330	East Los Angeles to West Hollywood (via San Vicente Boulevard, Pico Boulevard & East 1st Street)	San Vicente Boulevard	EB WB	5 6	5 5		
Metro 105	Vernon to West Hollywood (via La Cienega Boulevard & Vernon Avenue)	La Cienega Boulevard	NB SB	11 9	11 11		
Metro 218	Studio City to Beverly Hills (via Laurel Canyon Boulevard)	3rd Street	NB SB	6 5	5 5		
Metro Rapid 705	West Hollywood to Vernon (via La Cienega Boulevard & Vernon Avenue)	La Cienega Boulevard	NB SB	15 6	11 12		

Table 4-1 (Continued) EXISTING PUBLIC TRANSIT ROUTES [1]

		ROADWAY(S)		OF BUSES/TI ING PEAK H	
ROUTE	DESTINATIONS	NEAR SITE	DIR	AM	PM
Metro Rapid 720	Commerce to Santa Monica (via Wilshire Boulevard & Whittier Boulevard)	Wilshire Boulevard	EB WB	19 55	48 20
DASH Fairfax	Cedars-Sinai Medical Center to Park La Brea (via La Cienega Boulevard, Melrose Avenue, & Wilshire Boulevard)	La Cienega Boulevard	EB WB	7 6	7 6
West Hollywood CityLine	Cedars-Sinai Medical Center to La Brea (via San Vicente Boulevard & Santa Monica Boulevard)	San Vicente Boulevard	EB WB	3 1	4 6
West Hollywood CityLine X	Cedars-Sinai Medical Center to La Brea (via San Vicente Boulevard & Santa Monica Boulevard)	San Vicente Boulevard	EB WB	7 6	1 0
AVTA 786	Century City/West Los Angeles to Lancaster (via Santa Monica Boulevard & Wilshire Boulevard)	Wilshire Boulevard	NB SB	0 3	3 0
			Total	338	334

[1] Sources: Los Angeles County Metropolitan Transportation Authority (Metro) website, 2018.

Los Angeles Department of Transportation (DASH) website, 2018. West Hollywood Transit Services (CityLine) website, 2018. Antelope Valley Transit Authority (AVTA) website, 2018.





MAP SOURCE: METROPOLITAN TRANSPORTATION AUTHORITY
★ PROJECT SITE

FIGURE 4-2

EXISTING LANE CONFIGURATIONS

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5.0 TRAFFIC COUNTS

Manual traffic counts of vehicular turning movements were conducted on Thursday, May 17, 2018 at each of the study intersections during the weekday morning and afternoon commuter periods to determine the peak hour traffic volumes. The manual traffic counts at the study intersections were conducted from 7:00 AM to 10:00 AM and 3:00 PM to 6:00 PM to determine the respective peak commuter hours.

The weekday AM and PM peak period manual counts of vehicle movements at the study intersections are summarized in *Table 5–1*. The existing traffic volumes at the study intersections during the weekday AM and PM peak hours are shown in *Figures 5–1* and 5–2, respectively. Summary data worksheets of the manual traffic counts at the study intersections are contained in *Appendix A*.

Table 5-1
EXISTING TRAFFIC VOLUMES [1]

08-Mar-19

				AM PE	AK HOUR	PM PE	08-Mar-19 AK HOUR
NO.	INTERSECTION	DATE	DIR	BEGAN	VOLUME	BEGAN	VOLUME
1	Robertson Boulevard / 3rd Street	05/17/2018	NB SB EB WB	8:00	671 457 429 905	4:45	705 477 482 660
2	Robertson Boulevard / Burton Way	05/17/2018	NB SB EB WB	8:30	596 536 946 1,629	5:00	661 616 1,683 1,083
3	Robertson Boulevard / Wilshire Boulevard	05/17/2018	NB SB EB WB	8:00	949 776 980 1,847	4:30	774 778 1,694 1,031
4	San Vicente Boulevard / Melrose Ave	05/17/2018	NB SB EB WB	8:15	740 557 618 1,165	5:00	912 687 786 774
5	Willaman Drive / Burton Way	05/17/2018	NB SB EB WB	8:15	290 130 787 1,622	4:45	210 325 1,809 1,010
6	San Vicente Boulevard / Beverly Boulevard	05/17/2018	NB SB EB WB	8:45	883 760 807 1,393	5:00	1,245 823 971 985
7	Sherbourne Drive / 3rd Street	05/17/2018	NB SB EB WB	8:00	114 81 695 1,371	3:45	84 391 773 696
8	San Vicente Boulevard / 3rd Street	05/17/2018	NB SB EB WB	8:15	687 655 633 1,462	3:30	533 1,045 863 692
9	San Vicente Boulevard-Le Doux Road / Burton Way	05/17/2018	NB SB EB WB	8:15	53 561 676 2,353	5:00	105 475 1,888 1,392
10	La Cienega Boulevard / Melrose Avenue	05/17/2018	NB SB EB WB	7:30	798 1,053 464 1,434	5:00	1,376 981 1,044 933
11	La Cienega Boulevard / Beverly Boulevard	05/17/2018	NB SB EB WB	8:45	1,009 1,286 803 1,535	5:00	1,550 1,189 1,450 1,207
12	La Cienega Boulevard / 3rd Street	05/17/2018	NB SB EB WB	8:15	1,130 1,482 603 1,410	5:00	1,402 1,282 1,090 827

Table 5-1 (Continued) EXISTING TRAFFIC VOLUMES [1]

08-Mar-19

				AM PE	AK HOUR	PM PE	AK HOUR
NO.	INTERSECTION	DATE	DIR	BEGAN	VOLUME	BEGAN	VOLUME
13	La Cienega Boulevard / San Vicente Boulevard	05/17/2018	NB SB EB WB	8:15	871 1,514 1,126 2,229	5:00	1,386 1,317 2,308 1,427
14	La Cienega Boulevard / Wilshire Boulevard	05/17/2018	NB SB EB WB	8:00	922 1,115 624 1,161	5:00	1,162 1,115 852 854

[1] National Data & Surveying Services

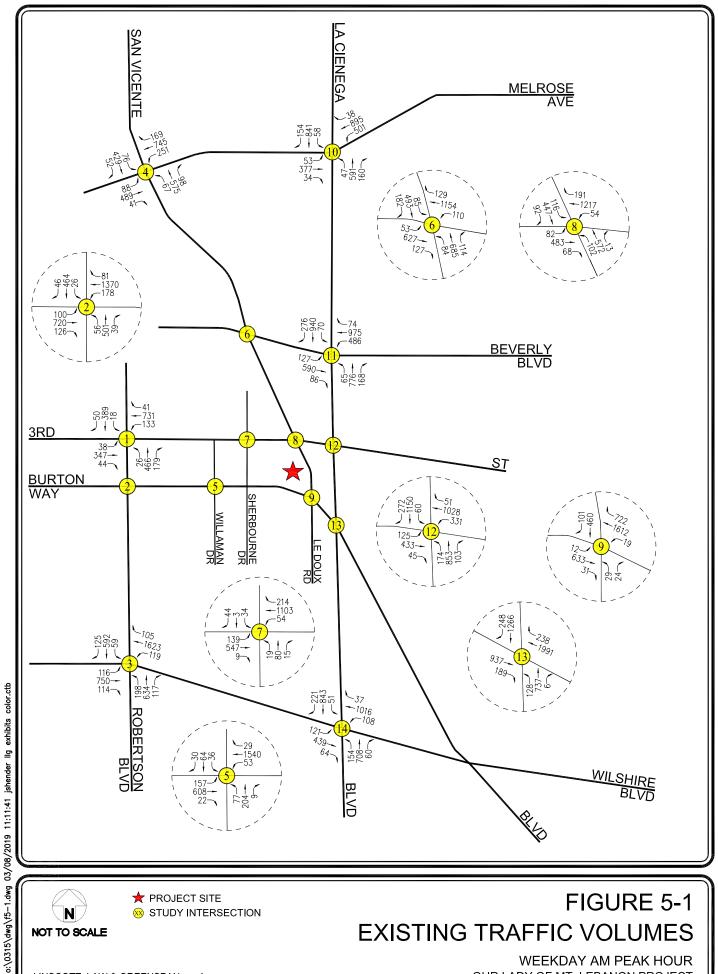
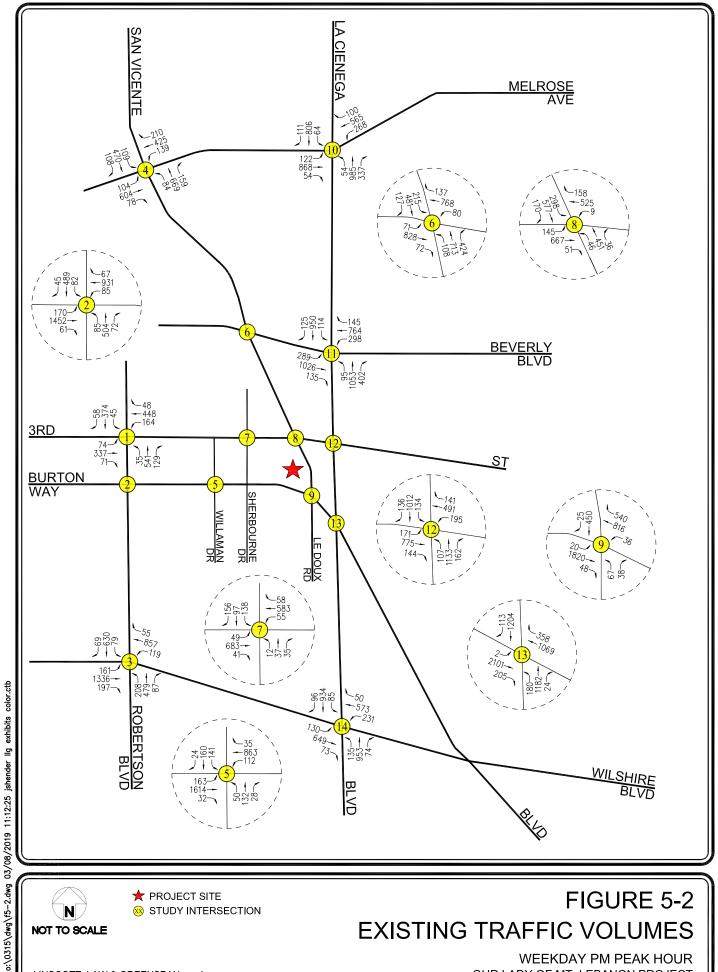




FIGURE 5-1 **EXISTING TRAFFIC VOLUMES**

WEEKDAY AM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT

LINSCOTT, LAW & GREENSPAN, engineers



★ PROJECT SITE M STUDY INTERSECTION NOT TO SCALE

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FIGURE 5-2 **EXISTING TRAFFIC VOLUMES**

WEEKDAY PM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT

6.0 CUMULATIVE DEVELOPMENT PROJECTS

The forecast of future pre-Project conditions was prepared in accordance to procedures outlined in Section 15130 of the CEQA Guidelines. Specifically, the CEQA Guidelines provide two options for developing the future traffic volume forecast:

- "(A) A list of past, present, and probable future projects producing related or cumulative impacts, including, if necessary, those projects outside the control of the [lead] agency, or
- (B) A summary of projections contained in an adopted local, regional or statewide plan, or related planning document, that describes or evaluates conditions contributing to the cumulative effect. Such plans may include: a general plan, regional transportation plan, or plans for the reduction of greenhouse gas emissions. A summary of projections may also be contained in an adopted or certified prior environmental document for such a plan. Such projections may be supplemented with additional information such as a regional modeling program. Any such document shall be referenced and made available to the public at a location specified by the lead agency."

Accordingly, the traffic analysis provides a highly conservative estimate of future pre-Project traffic volumes as it incorporates both the "A" and "B" options outlined in CEQA Guidelines for purposes of developing the forecast.

6.1 Related Projects

A forecast of on-street traffic conditions prior to occupancy of the proposed Project was prepared by incorporating the potential trips associated with other known development projects (related projects) in the area. With this information, the potential impact of the proposed Project can be evaluated within the context of the cumulative impact of all ongoing development. The related projects research was based on information on file at LADOT, the City of Los Angeles Department of Planning, the City of Beverly Hills Community Development Department, and the City of West Hollywood Community Development Department. The list of related projects in the Project site area is presented in *Table 6–1*. The location of the related projects is shown in *Figure 6–1*.

Traffic volumes expected to be generated by the related projects were calculated using rates provided in the Institute of Transportation Engineers' (ITE) *Trip Generation Manual*³. The related projects' respective traffic generation for the weekday AM and PM peak hours, as well as on a daily basis for a typical weekday, is summarized in *Table 6–1*. The distribution of the related projects traffic volumes to the study intersections during the weekday AM and PM peak hours are displayed in *Figures 6–2* and *6–3*, respectively.

-

³ Institute of Transportation Engineers *Trip Generation Manual*, 10th Edition, Washington, D.C., 2017.

Table 6-1
RELATED PROJECTS LIST AND TRIP GENERATION [1]

08-Mar-19

MAP	PROJECT NAME/	PROJECT	ADDRESS/	LAND USI	E DATA	PROJECT DATA	DAILY TRIP ENDS [2]		M PEAK H			M PEAK H VOLUMES	
NO.	PROJECT NUMBER	STATUS	LOCATION	LAND-USE	SIZE	SOURCE	VOLUMES	IN	OUT	TOTAL	IN	OUT	TOTAL
				City of I	os Angeles								
LA1	Four Seasons Residences	Under Construction	300 S. Wetherly Drive	Condominiums	140 DU		270	3	17	20	16	6	22
LA2	Cedars-Sinai Medical Center Project West Tower	Proposed	8723 W. Alden Drive	Hospital	100 Beds		1,181	79	34	113	47	83	130
LA3	S. La Cienega Boulevard Eldercare Facility	Proposed	1022 S. La Cienega Boulevard	Assisted Living Skilled Nursing Apartments	183 Beds 22 DU (36) DU		242	14	(6)	8	6	16	22
LA4	6535 Wilshire Boulevard Mixed-Use Project	Proposed	6535 Wilshire Boulevard	Office Apartments Retail	62,000 GSF 22 DU 5,603 GSF		786	61	17	78	20	63	86
LA5	Beverly & Fairfax Mixed-Use Project	Approved	7901 W. Beverly Boulevard	Apartments Retail	71 DU 11,454 GSF		493	7	29	36	30	16	46
LA6	333 La Cienega Boulevard Project	Under Construction	333 S. La Cienega Boulevard	Apartments Supermarket Restaurant	145 DU 27,685 GSF 3,370 GSF	[3]	2,020	35	71	106	114	77	191
LA7	6399 W. Wilshire Boulevard Mixed-Use Hotel	Under Construction	6399 W. Wilshire Boulevard	Hotel Restaurant Lounge	176 Rooms 871 GSF 860 GSF		377	(64)	19	(45)	26	(48)	(22)
LA8	Unified Elder Care Facility/ Mixed-Use	Proposed	8052 W. Beverly Boulevard	Synagogue Apartments Medical Office Retail	5,000 GSF 102 DU 15,000 GSF 1,000 GSF		725	19	26	45	21	49	70
LA9	8000 W. Beverly Boulevard Mixed-Use Project	Proposed	8000 W. Beverly Boulevard	Apartments Retail	48 DU 7,400 GSF		774	21	36	57	42	17	59
LA10	Edin Park	Proposed	8001 W. Beverly Boulevard	Restaurant Office	22,600 GSF 11,358 GSF		3,248	142	118	260	157	106	263
LA11	488 S. San Vicente Boulevard Mixed-Use Project	Proposed	488 S. San Vicente Boulevard	Apartments Retail	53 DU 6,585 GSF		281	1	20	21	18	9	27
LA12	Solstice	Proposed	431 N. La Cienega Boulevard	Apartments Car Wash Retail	72 DU (7,373) GSF (5,310) GSF	[4]	(409)	(9)	10	1	(12)	(22)	(34)

Table 6-1 (Continued) RELATED PROJECTS LIST AND TRIP GENERATION [1]

MAP	PROJECT NAME/	PROJECT	ADDRESS/	LAND US	E DATA	PROJECT DATA	DAILY TRIP ENDS [2]		A PEAK HO			M PEAK H VOLUMES	
NO.	PROJECT NUMBER	STATUS	LOCATION	LAND-USE	SIZE	SOURCE	VOLUMES	IN	OUT	TOTAL	IN	OUT	TOTAL
LA13	Third Street Mixed-Use Project	Proposed	8000 W. 3rd Street	Apartments Affordable Housing Retail	45 DU 5 DU 7,251 GSF		428	9	17	26	23	13	36
LA14	7951 W. Beverly Boulevard Mixed-Use Project	Proposed	7951 W. Beverly Boulevard	Apartments Affordable Housing Retail Restaurant	51 DU 6 DU 1,142 GSF 6,294 GSF		782	30	32	62	40	26	66
				City of B	everly Hills							<u>I</u>	
BH1	Beverly Hills Media Center Project	Proposed	100 N. Crescent Drive	Office Restaurant Office	156,825 GSF 4,330 GSF (106,085) GSF	[5] [6] [5]	1,527 486 (1,033)	157 24 (106)	25 19 (17)	182 43 (123)	29 26 (20)	151 16 (102)	180 42 (122)
ВН2	55 N. La Cienega Boulevard Mixed-Use Hotel Project	Proposed	55 N. La Cienega Boulevard	Hotel Retail Restaurant Restaurant	200 Rooms 10,222 GSF 3,346 GSF (13,500) GSF	[7] [8] [6] [6]	1,672 386 375 (1,514)	55 6 18 (74)	39 4 15 (60)	94 10 33 (134)	61 19 20 (82)	59 20 13 (50)	120 39 33 (132)
ВН3	168 N. La Peer Drive Residential Project	Under Construction	154-168 N. La Peer Drive	Condominiums Condominiums	16 DU (6) DU	[9] [9]	117 (44)	2 (1)	5 (2)	7 (3)	6 (2)	3 (1)	9 (3)
BH4	457 N. Oakhurst Drive Residential Project	Proposed	457 N. Oakhurst Drive	Condominiums Condominiums	8 DU (2) DU	[9] [9]	59 (15)	1 0	3 (1)	4 (1)	3 (1)	1 0	4 (1)
ВН5	425 N. Palm Drive Residential Project	Proposed	425 N. Palm Drive	Condominiums Condominiums	20 DU (18) DU	[9] [9]	146 (132)	2 (2)	7 (6)	9 (8)	7 (6)	4 (4)	11 (10)
ВН6	Gardenhouse Mixed-Use Project	Under Construction	8600 Wilshire Boulevard	Apartments Retail	18 DU 6,355 GSF	[9] [8]	132 240	2 4	6 2	8 6	6 12	4 12	10 24
ВН7	9000 Wilshire Boulevard Office Project	Approved	9000 Wilshire Boulevard	Retail Office	(4,820) GSF 31,702 GSF	[8] [5]	(182) 309	(3) 32	(2) 5	(5) 37	(9) 6	(9) 30	(18) 36
ВН8	9145 Wilshire Boulevard Project	Proposed	9145 Wilshire Boulevard	Religious Facility	8,269 GSF	[10]	240	13	7	20	14	10	24
ВН9	9200 Wilshire Boulevard Mixed-Use Project	Approved	9200 Wilshire Boulevard	Apartments Retail	54 DU 14,000 GSF	[9] [8]	395 529	6 8	19 5	25 13	19 25	11 28	30 53
				City of We	st Hollywood	1							
WH1	8816 Beverly Boulevard Mixed-Use Project	Proposed	8816 Beverly Boulevard	Apartments Retail Restaurant Office	10 DU 19,493 GSF 1,860 GSF 25,575 GSF	[11]	959	47	18	65	31	54	85

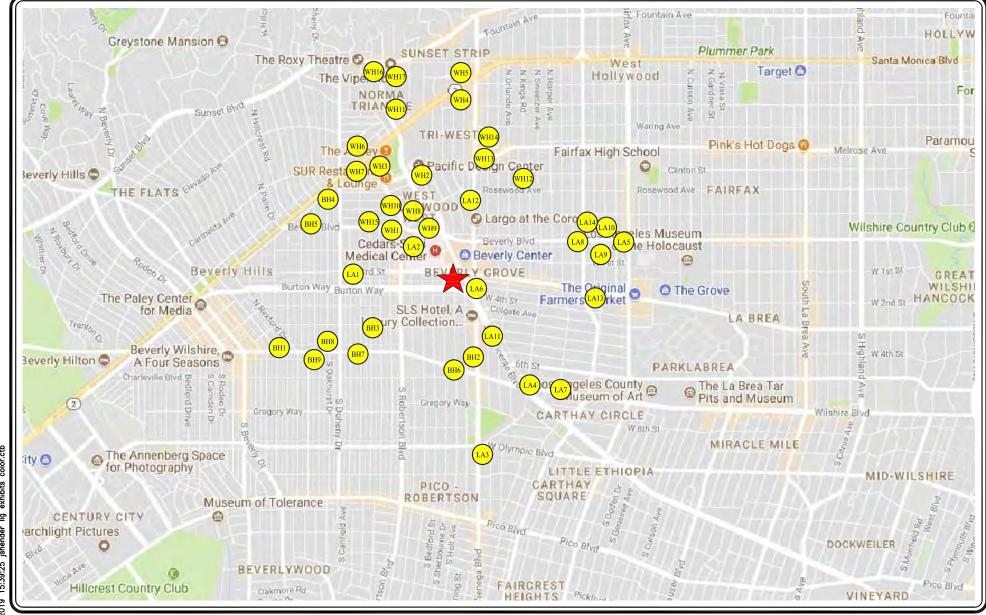
Table 6-1 (Continued)
RELATED PROJECTS LIST AND TRIP GENERATION [1]

MAP	PROJECT NAME/	PROJECT	ADDRESS/	LAND USE	DATA	PROJECT DATA	DAILY TRIP ENDS [2]		I PEAK HO		PM PEAK HOUR VOLUMES [2]			
NO.	PROJECT NUMBER	STATUS	LOCATION	LAND-USE	SIZE	SOURCE	VOLUMES	IN	OUT	TOTAL	IN	OUT	TOTAL	
WH2	8650 Melrose Avenue Mixed-Use Project	Proposed	8650 Melrose Avenue	Apartments Retail	7 DU 14,571 GSF	[9] [8]	51 550	1 9	2 5	3 14	3 27	1 29	4 56	
WH3	Robertson Lane Hotel	Approved	645-681 Roberston Boulevard & 648-668 La Peer Drive	Hotel Restaurant Specialtay Retail Design Showroom Nightclub	241 Rooms 22,615 GSF 18,130 GSF 10,325 GSF 3,780 GSF	[12]	2,390	77	51	128	80	77	157	
WH4	Sprouts - 8550 Santa Monica Boulevard Project	Under Construction	8550 Santa Monica Boulevard	Grocery Store Restaurant Office Health/Fitness Club Specialty Retail	25,000 GSF 1,319 GSF 3,998 GSF 8,000 GSF 4,000 GSF	[13]	1,989	48	29	77	92	89	181	
WH5	8555 Santa Monica Boulevard Mixed-Use Project	Proposed	8555 Santa Monica Boulevard	Apartments Live-Work Condominiums Office Specialty Retail Restaurant	97 DU 12 DU 6,080 GSF 19,400 GSF 2,820 GSF	[14]	809	11	40	51	42	24	66	
WH6	9001 Santa Monica Boulevard Mixed-Use Project	Proposed	9001 Santa Monica Boulevard	Condominiums Retail Restaurant	42 DU 9,850 GSF 9,800 GSF	[12]	829	16	(8)	8	31	16	47	
WH7	Melrose Triangle	Under Construction	9040-9048 Santa Monica Boulevard	General Retail Art Gallery Design Showroom Restaurant Apartments General Office	45,112 GSF 16,404 GSF 12,303 GSF 8,202 GSF 76 DU 137,064 GSF	[15]	3,578	193	67	260	123	180	303	
WH8	8763 Rosewood Avenue Mixed-Use Project	Proposed	8763 Rosewood Avenue	Retail	4,945 GSF	[8]	187	3	2	5	9	10	19	
WH9	8713 Beverly Boulevard Mixed-Use Project	Proposed	8713 Beverly Boulevard	Apartments Office Retail Gallery	30 DU 3,416 GSF 5,475 GSF 500 GSF	[11]	303	9	15	24	22	20	42	
WH10	417 Robertson Boulevard Showroom Project	Proposed	417 Robertson Boulevard	Retail	7,558 GSF	[8]	285	4	3	7	14	15	29	
WH11	829 Larrabee Street Residential Project	Proposed	829 Larrabee Street	Apartments	13 DU	[9]	95	1	5	6	4	3	7	

Table 6-1 (Continued) RELATED PROJECTS LIST AND TRIP GENERATION [1]

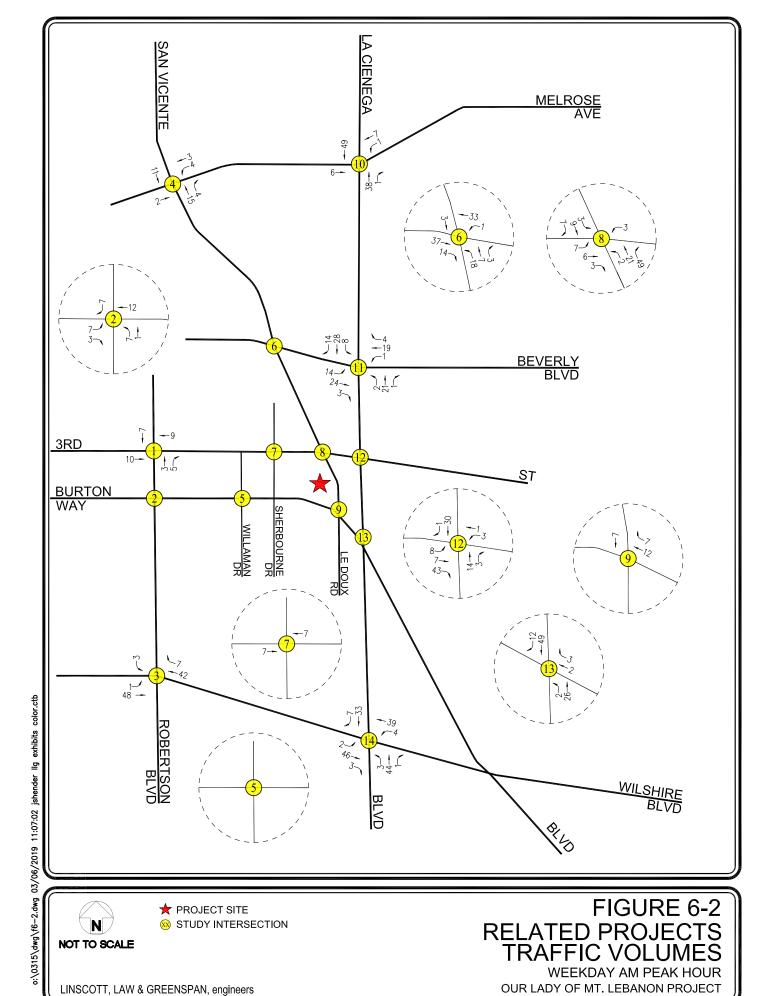
						PROJECT DATA	DAILY		M PEAK H			M PEAK H			
MAP	PROJECT NAME/	PROJECT	ADDRESS/				LAND USE DATA		TRIP ENDS [2]		OLUMES			VOLUMES	
NO.	PROJECT NUMBER	STATUS	LOCATION	LAND-USE	SIZE	SOURCE	VOLUMES	IN	OUT	TOTAL	IN	OUT	TOTAL		
WH12	511 N. Flores Street Residential Project	Proposed	511 N. Flores Street	Apartments	10 DU	[9]	73	1	4	5	4	2	6		
WH13	600 N. La Cienega Boulevard Mixed-Use Project	Proposed	600 N. La Cienega Boulevard	Apartments Showroom Mechanical Retail Restaurant	5 DU 15,727 GSF 2,776 GSF 5,355 GSF 7,094 GSF	[9] [8] [8] [8]	37 594 105 202 796	0 9 2 3 39	2 6 1 2 32	2 15 3 5 71	2 29 5 10 43	1 31 6 10 26	3 60 11 20 69		
WH14	624 N. La Cienega Boulevard Mixed-Use Project	Proposed	624 N. La Cienega Boulevard	Apartments Retail	6 DU 54,209 GSF	[9] [8]	44 2,046	1 32	2 19	3 51	2 99	1 108	3 207		
WH15	8899 Beverly Boulevard Mixed-Use Project	Approved	8899 Beverly Boulevard	Apartments Condominiums Townhomes Office Retail Restaurant	12 DU 56 DU 13 DU 10,562 GSF 19,875 GSF 4,394 GSF	[16]	(129)	(69)	21	(48)	17	(54)	(37)		
WH16	8950 Sunset Boulevard Hotel Project	Proposed	8950 Sunset Boulevard	Hotel Apartments Specialty Dining Restaurant Whiskey Bar Day Spa 3-Meal Restaurant Lounge	165 Rooms 4 DU 7,697 GSF 5,578 GSF 2,002 GSF 9,230 GSF 2,505 GSF 3,685 GSF	[17]	2,539	63	49	112	121	89	210		
WH17	The Arts Club	Proposed	8920 Sunset Boulevard	Private Club Museum Office Specialty Retail	7,000 Members 2,192 GSF 46,009 GSF 11,933 GSF	[18]	1,961	103	19	122	68	91	159		
TOTAL	L	•					35,184	1,095	899	1,994	1,559	1,436	2,995		

- [1] Source: City of Los Angeles Department of Transportation Related Projects List, City of Beverly Hills Community Development Department Related Project List, and City of West Hollywood Community Development Department Polects List.
- [2] Trips are one-way traffic movements, entering or leaving.
- [3] Source: 333 La Cienega Boulevard Traffic Study, prepared by The Mobility Group, March 2015.
- [4] Source: Traffic Analysis Addendum Proposed Residential Project at 431 N. La Cienega Boulevard, prepared by Linscott, Law & Greenspan, Engineers, May 2018
- [5] ITE Land Use Code 710 (General Office Building) trip generation average rates.
- [6] ITE Land Use Code 932 (High-Turnover [Sit-Down] Restaurant) trip generation average rates.
- [7] ITE Land Use Code 310 (Hotel) trip generation average rates.
- [8] ITE Land Use Code 820 (Shopping Center) trip generation average rates.
- [9] ITE Land Use Code 220 (Multifamily Housing [Low-Rise]) trip generation average rates.
- [10] ITE Land Use Code 561 (Synagogue) trip generation average rates.
- [11] Source: Draft Transportation Study for the 8713 Beverly Boulevard Mixed-Use Project, prepared by Fehr & Peers, January 2016.
- [12] Source: Traffic Impact Study for Robertson Lane Hotel Project, prepared by KOA Corporation, January 2017.
- [13] Source: Transportation Study for the Sprouts 8550 Santa Monica Boulevard Project, prepared by Fehr & Peers, June 2014.
- [14] Source: Transportation Analysis Report for the 8555 Santa Monica Boulevard Mixed-Use Project, prepared by Fehr & Peers, January 2018.
- [15] Source: Revised Traffic Impact Analysis for the Melrose Triangle Project, prepared by LSA Associates, Inc., December 2013.
- [16] Source: Draft Transportation Study for the 8899 Beverly Boulevard Project, prepared by Gibson Transportation Consulting, Inc., November 2013.
- [17] Source: Traffic Impact Assessment for the 8950 Sunset Boulevard Hotel Project, prepared by Linscott, Law & Greenspan, Engineers, September 2014.
- [18] Source: Transportation Study for The Arts Club West Hollywood Project, prepared by Gibson Transportation Consulting, Inc., September 2017.

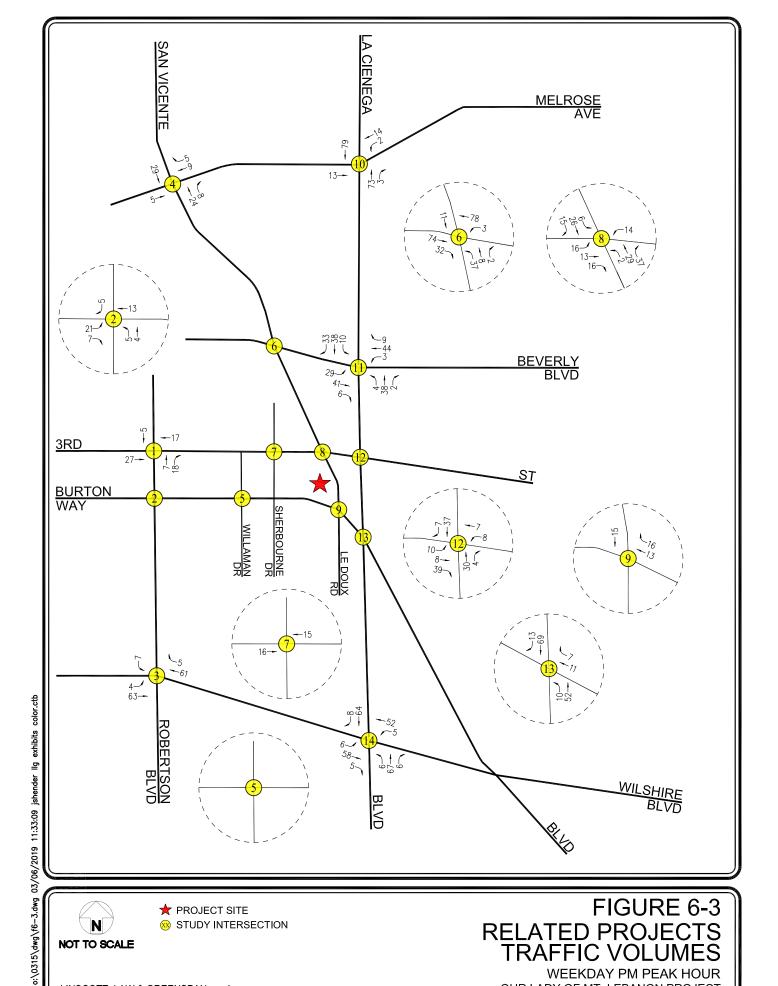




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6.2 Ambient Traffic Growth Factor

In order to account for unknown related projects not included in this analysis, the existing traffic volumes were increased at an annual rate of 1.0 percent (1.0%) per year to and including the year 2024 (i.e., the anticipated year of Project build-out). The ambient growth factor was based on general traffic growth factors provided in the 2010 Congestion Management Program for Los Angeles County ("CMP manual") and determined in consultation with LADOT staff. It is noted that based on review of the general traffic growth factors provided in the CMP manual for the West/Central Los Angeles area, it is anticipated that the existing traffic volumes are expected to increase at an annual rate of less than 0.17% per year between the years 2015 and 2024. Thus, application of an annual growth factor of 1.0% annual growth provides a very conservative, worst-case forecast of future traffic volumes in the area as it substantially exceeds the annual traffic growth rate published in the CMP manual. Further, it is noted that the CMP manual's traffic growth rate is intended to anticipate future traffic generated by development projects in the Project vicinity. Thus, the inclusion in this traffic analysis of both a forecast of traffic generated by known related projects plus the use of an ambient growth traffic factor based on CMP traffic model data results in an extremely conservative estimate of future traffic volumes at the study intersections.

7.0 Traffic Forecasting Methodology

In order to estimate the traffic impact characteristics of the proposed Project, a multi-step process has been utilized. The first step is trip generation, which estimates the total arriving and departing traffic volumes on a peak hour and daily basis. The traffic generation potential is forecast by applying the appropriate vehicle trip generation equations or rates to the Project development tabulation.

The second step of the forecasting process is trip distribution, which identifies the origins and destinations of inbound and outbound Project traffic volumes. These origins and destinations are typically based on demographics and existing/anticipated travel patterns in the study area.

The third step is traffic assignment, which involves the allocation of Project traffic to study area streets and intersections. Traffic assignment is typically based on minimization of travel time, which may or may not involve the shortest route, depending on prevailing operating conditions and travel speeds. Traffic distribution patterns are indicated by general percentage orientation, while traffic assignment allocates specific volume forecasts to individual roadway links and intersection turning movements throughout the study area.

With the forecasting process complete and Project traffic assignments developed, the impact of the proposed Project is isolated by comparing operational (i.e., Levels of Service) conditions at the selected key intersections using existing and expected future traffic volumes without and with forecast Project traffic. The need for site-specific and/or cumulative local area traffic improvements can then be evaluated and the significance of the Project's impacts identified.

7.1 Project Traffic Generation

Traffic volumes expected to be generated by the proposed Project during the weekday AM and PM peak hours, as well as on a daily basis, were estimated using rates published in the ITE *Trip Generation Manual*. The following trip generation rates were used to forecast the traffic volumes expected to be generated by the Project land use components:

- Apartments: ITE Land Use Code 222 (Multifamily Residential [High-Rise]) trip generation average rates were used to forecast the traffic volumes expected to be generated by the residential component of the Project.
- Church: ITE Land Use Code 560 (Church) trip generation average rates were used to forecast the traffic volumes expected to be generated by the church component of the Project.

In addition to the trip generation forecasts for the Project's land use components (which are essentially an estimate of the number of vehicles that could be expected to enter and exit the Project site access points), an adjustment was made to reduce the overall trip generation forecast based on the existing church use. The Project includes the removal of three of the existing church buildings and the retention and rehabilitation of the cathedral building. The three existing buildings that will be removed include 12,370 square feet of floor area. The floor area of the

existing cathedral building is 6,848 square feet. This results in an aggregate of 19,218 square feet of existing church floor area. ITE Land Use Code 560 (Church) trip generation average rates were used to estimate the trips generated by the existing church buildings.

Furthermore, a forecast was also made of transit trips. The transit reduction is based on the Project site's proximity to the various bus lines, as well as the land use characteristics of the Project. As shown in *Table 4–1* and *Figure 4–2*, the Project site is well served by public transit. Specifically, the Project site is located within a quarter-mile walking distance to the Metro Rapid stop at the La Cienega Boulevard / 3rd Street intersection. Thus, as stipulated in the LADOT *Transportation Impact Study Guidelines*, a transit adjustment of 15% has been utilized based on the Project site's proximity to the Metro Rapid stop.

It is also noted that one of Metro's priority projects, the Purple Line Extension, is currently under construction in the Project area. From the current terminus at the Wilshire / Western station, the Purple Line Extension will extend westward for about nine miles and add seven new stations, providing easier access to the Westside, the region's second-largest job center. Travel time between downtown Los Angeles and Westwood is expected to be about 25 minutes. The project is being built in three sections. The first section between the Wilshire / Western station and the Wilshire / La Cienega station is currently under construction and is scheduled for completion in 2023. The Wilshire / La Cienega station will be located approximately 0.6 miles south of the Project site and will enhance transit options for Project residents and church officials, parishioners and guests. The Purple Line Extension will enhance the Project study area's transit areas, thus further justifying the 15% transit adjustment.

The trip generation forecast for the proposed Project was submitted for review and approval by LADOT staff. As presented in *Table 7–1*, the proposed Project is expected to generate 43 net new vehicle trips (increase in 11 inbound trips and 32 outbound trips) during the AM peak hour. During the PM peak hour, the proposed Project is expected to generate 53 net new vehicle trips (increase in 32 inbound trips and 21 outbound trips). Over a 24-hour period, the proposed Project is forecast to generate 650 daily trips ends (approximately 325 inbound trips and 325 outbound trips) during a typical weekday.

Table 7-1 PROJECT TRIP GENERATION [1]

02-Apr-19

		DAILY TRIP ENDS [2]		PEAK HO			PEAK HO	
LAND USE	SIZE	VOLUMES	IN	OUT	TOTAL	IN	OUT	TOTAL
Proposed Project								
Apartments [3]	153 DU	681	11	36	47	34	21	55
Church [4]	31,342 GSF	218	<u>6</u>	4	<u>10</u>	<u>7</u>	<u>8</u>	<u>15</u>
Subtotal	,	899	17	40	57	41	29	70
Transit Trips [5]								
Apartments (15%)		(102)	(2)	(5)	(7)	(5)	(3)	(8)
Church (15%)		(33)	(1)	(1)	(2)	(1)	(1)	(2)
Subtotal		(135)	(3)	(6)	(9)	(6)	(4)	(10)
Subtotal Project Driveway Trips		764	14	34	48	35	25	60
Existing Site								
Church [4]	(19,218) GSF	(134)	(4)	(2)	(6)	(4)	(5)	(9)
Transit Trips [5]								
Church (15%)		20	1	0	1	1	1	2
Subtotal Existing Driveway Trips		(114)	(3)	(2)	(5)	(3)	(4)	(7)
NET INCREASE DRIVEWAY TRIPS		650	11	32	43	32	21	53

- [1] Source: ITE "Trip Generation Manual", 10th Edition, 2017.
- [2] Trips are one-way traffic movements, entering or leaving.
- [3] ITE Land Use Code 222 (Multifamily Housing [High-Rise]) trip generation average rates.
 - Daily Trip Rate: 4.45 trips/dwelling unit; 50% inbound/50% outbound
 - AM Peak Hour Trip Rate: 0.31 trips/dwelling unit; 24% inbound/76% outbound
 - PM Peak Hour Trip Rate: 0.36 trips/dwelling unit; 61% inbound/39% outbound
- [4] TTE Land Use Code 560 (Church) trip generation average rates.

 Daily Trip Rate: 6.95 trips/1,000 SF of floor area; 50% inbound/50% outbound

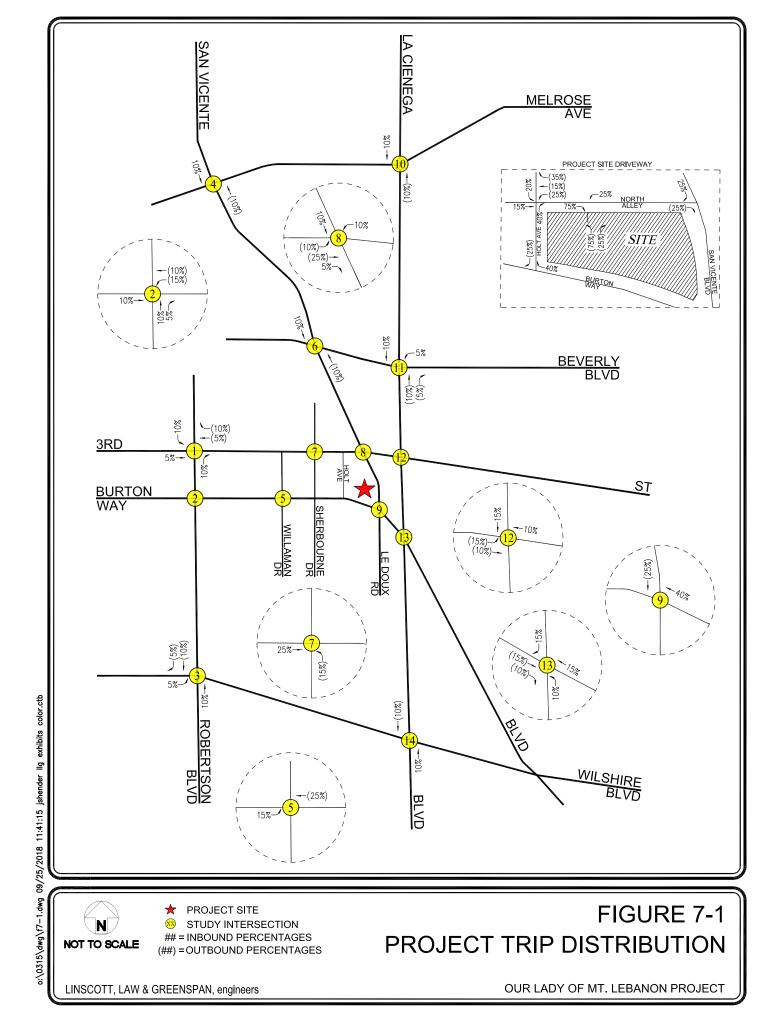
 AM Peak Hour Trip Rate: 0.33 trips/1,000 SF of floor area; 60% inbound/40% outbound
 - PM Peak Hour Trip Rate: 0.49 trips/1,000 SF of floor area; 45% inbound/55% outbound
- [5] The Project site is located within 1/4 mile of a Metro Rapid bus stop. The trip reduction for transit trips has been applied to all components of the project based on the "LADOT Transportation Impact Study Guidelines", December 2016 for developments within a 1/4 mile walking distance of a transit station or a RapidBus stop.

7.2 Project Traffic Distribution and Assignment

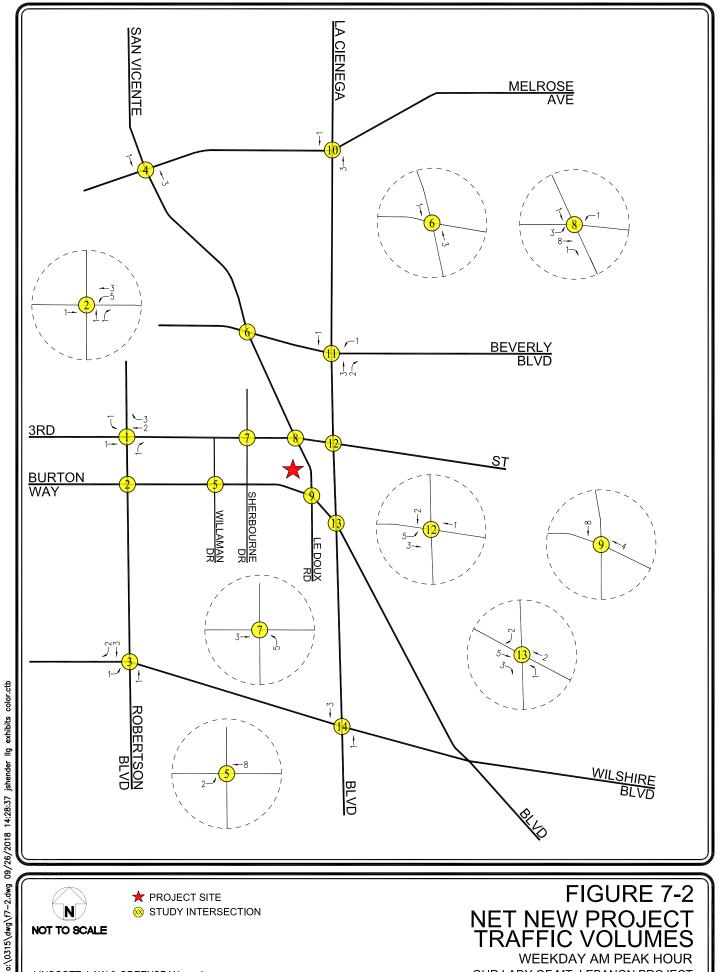
Project traffic volumes that will enter and exit the Project site have been distributed and assigned to the adjacent street system based on the following considerations:

- The site's proximity to major traffic corridors (i.e., San Vicente Boulevard, Burton Way, La Cienega Boulevard, etc.);
- Expected localized traffic flow patterns based on adjacent roadway channelization and presence of traffic signals;
- Existing intersection traffic volumes;
- Ingress/egress availability at the Project site assuming the site access and circulation scheme described in Section 3.0;
- The location of existing and proposed parking areas;
- Nearby population and employment centers as well as adjacent residential neighborhoods; and
- Input from LADOT staff.

The general, directional traffic distribution patterns for the proposed Project are presented in *Figure 7–1*. The forecast net new weekday AM and PM peak hour Project traffic volumes at the study intersections associated with the proposed Project are presented in *Figures 7–2* and *7–3*, respectively. The traffic volume assignments presented in *Figures 7–2* and *7–3* reflect the traffic distribution characteristics shown in *Figure 7–1* and the Project traffic generation forecast presented in *Table 7–1*.



-34-

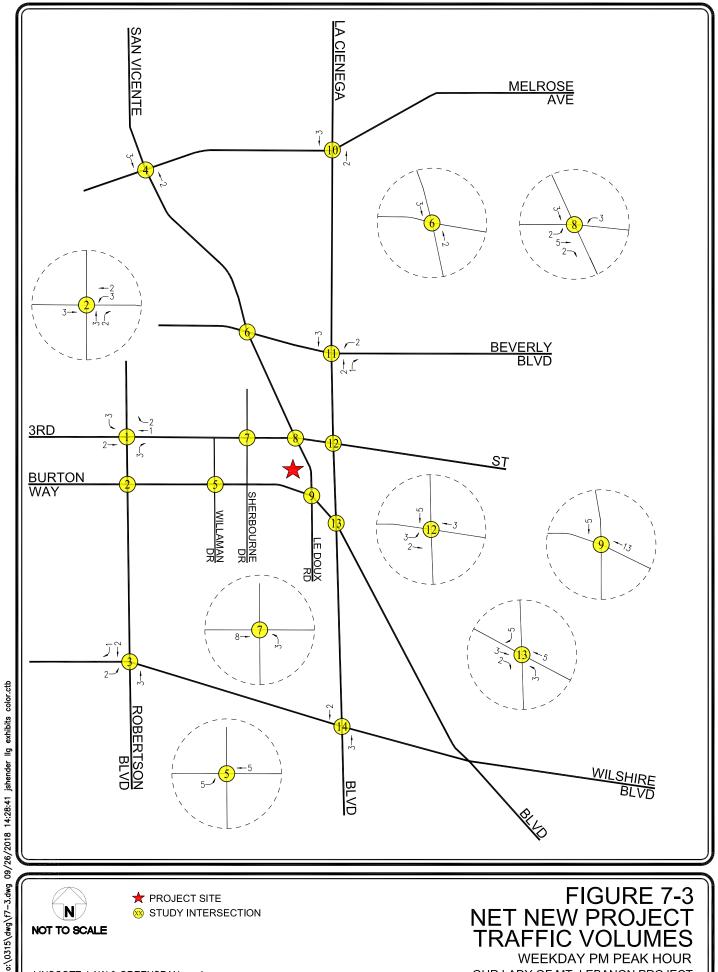


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NOT TO SCALE

NET NEW PROJECT TRAFFIC VOLUMES

WEEKDAY AM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT



STUDY INTERSECTION NOT TO SCALE LINSCOTT, LAW & GREENSPAN, engineers

FIGURE 7-3 NET NEW PROJECT TRAFFIC VOLUMES

WEEKDAY PM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT

8.0 Traffic Impact Analysis Methodology

Ten of the 14 study intersections are located within or shared with the City of Los Angeles, and therefore were evaluated using LADOT's Critical Movement Analysis (CMA) method of analysis that determines v/c ratios based on a critical lane basis.

A supplemental traffic analysis was prepared using the Intersection Capacity Utilization (ICU) method for the four study intersections located within or shared with the City of Beverly Hills. Specifically, the ICU method was used to determine v/c ratios and corresponding Levels of Service at the two study intersections as the ICU method is used for traffic analysis purposes in the City of Beverly Hills. The ICU calculations use a lane capacity of 1,600 vehicles per hour (vph) for left-turn, through, and right-turn lanes, and dual left-turn capacity of 2,880 vph. A clearance adjustment factor of 0.10 was added to each CMA and ICU Level of Service calculation.

Additionally, a supplemental traffic analysis was prepared using the Highway Capacity Manual (HCM 2010) method for the three study intersections located within or shared with the City of West Hollywood, as the HCM 2010 methodology is used for traffic analysis purposes in the City of West Hollywood.

For the CMA, ICU, and HCM 2010 methodologies, the overall intersection v/c ratio is subsequently assigned a LOS value to describe intersection operations. Level of Service varies from LOS A (free flow) to LOS F (jammed condition). A description of the CMA, ICU, and HCM 2010 methods and corresponding Levels of Service are provided in *Appendix B*, *C*, and *D*, respectively.

8.1 Impact Criteria and Thresholds

The relative impact of the added Project traffic volumes to be generated by the proposed Project during the AM and PM peak hours was evaluated based on analysis of future operating conditions at the study intersections, without and with the proposed Project. The previously discussed capacity analysis procedures were utilized to evaluate the future v/c relationships and service level characteristics at each study intersection.

The significance of the potential impacts of Project-generated traffic was identified using the traffic impact criteria set forth in LADOT's *Transportation Impact Study Guidelines*, December 2016. According to the respective published guidelines, a traffic impact is considered significant if the Project-related increase in the v/c ratio is equal to or exceeds the thresholds presented in *Table 8–1* for intersections located within the City of Los Angeles.

Table 8-1								
	CITY OF LOS ANGELES							
INTER	SECTION IMPACT THRESHOI	LD CRITERIA						
Final v/c	Final v/c Level of Service Project Related Increase in v/c							
> 0.701 - 0.800	С	equal to or greater than 0.040						
> 0.801 - 0.900	equal to or greater than 0.020							
> 0.901	E or F	equal to or greater than 0.010						

For the study intersections located partially or completely within the Cities of Beverly Hills and West Hollywood, the relative traffic impacts were assessed based on the thresholds of significance adopted by these cities for intersections located within their respective jurisdictions. *Tables 8–2* and *8–3* provide the thresholds of significance related to potential traffic impacts for intersections located within the Cities of Beverly Hills and West Hollywood, respectively.

Table 8-2								
	CITY OF BEVERLY HILLS							
SIGNALIZED	SIGNALIZED INTERSECTION IMPACT THRESHOLD CRITERIA							
Final v/c	Level of Service	Project Related Increase in v/c						
> 0.800 - 0.900	D	equal to or greater than 0.030						
> 0.900	E or F	equal to or greater than 0.020						

	Table 8-3					
CITY OF WEST HOLLYWOOD						
INTER	RSECTION IMPACT THRESHOLD CRITERIA					
Project Increase in Delay Level of Service						
Level of Service	Commercial Corridor Intersection					
D	12 seconds					
Е	8 seconds					
F	8 seconds					

As required by the City of Los Angeles, City of Beverly Hills, and City of West Hollywood, mitigation of Project traffic impacts are required whenever traffic generated by the proposed development causes an increase of the analyzed intersection v/c ratio by an amount equal to or greater than the values shown above.

8.2 LADOT ATSAC/ATCS

The City of Los Angeles Automated Traffic Surveillance and Control (ATSAC) and Adaptive Traffic Control System (ATCS) provides computer control of traffic signals allowing automatic adjustment of signal timing plans to reflect changing traffic conditions, identification of unusual traffic conditions caused by accidents, the ability to centrally implement special purpose short term traffic timing changes in response to incidents, and the ability to quickly identify signal equipment malfunctions. ATCS provides real time control of traffic signals and includes additional loop detectors, closed-circuit television, an upgrade in the communications links and a new generation of traffic control software. LADOT estimates that the ATSAC system reduces the critical v/c ratios by seven percent (0.07). An ATCS system upgrade further reduces the critical v/c ratios by three percent (0.03) for a total of 10 percent (0.10). ATSAC system upgrades for the study intersections have been implemented as part of the LADOT ATSAC/ATCS system. Accordingly, for intersections located within the City of Los Angeles, the Level of Service calculations reflect a 0.10 adjustment for all analysis scenarios evaluated.

8.3 Traffic Impact Analysis Scenarios

8.3.1 City of Los Angeles Transportation Impact Analysis Scenarios

Pursuant to LADOT traffic study guidelines, LOS calculations have been prepared for the following scenarios for the 10 study intersections located within or shared with the City of Los Angeles:

- (a) Existing (2018) conditions.
- (b) Condition (a) with completion and occupancy of the Project.
- (c) Condition (b) with implementation of Project mitigation measures where necessary.
- (d) Condition (a) plus one percent (1.0%) annual ambient traffic growth through year 2024 and with completion and occupancy of the related projects (i.e., future cumulative baseline).
- (e) Condition (d) with completion and occupancy of the Project.
- (f) Condition (e) with implementation of Project mitigation measures where necessary.

The traffic volumes for each new condition were added to the volumes in the prior condition to determine the change in capacity utilization at the study intersections.

8.3.2 City of Beverly Hills Transportation Impact Analysis Scenarios

Pursuant to City of Beverly Hills' traffic impact analysis guidelines, Level of Service calculations have been prepared for the following scenarios for the four study intersections located within or shared with the City of Beverly Hills:

- (a) Existing (2018) conditions.
- (b) Condition (a) with completion and occupancy of the Project.
- (c) Condition (b) with implementation of Project mitigation measures, where necessary.
- (d) Condition (a) plus one percent (1.0%) annual ambient traffic growth through year 2024 and with completion and occupancy of the related projects (i.e., future cumulative baseline).
- (e) Condition (d) with completion and occupancy of the Project.
- (f) Condition (e) with implementation of Project mitigation measures where necessary.

The traffic volumes for each new condition were added to the volumes in the prior condition to determine the change in capacity utilization at the study intersections.

8.3.3 City of West Hollywood Traffic Impact Analysis Scenarios

Pursuant to the City of West Hollywood's traffic study guidelines, Level of Service calculations have been prepared for the following scenarios for the three study intersections located within or shared with the City of West Hollywood:

- (a) Existing (2018) conditions.
- (b) Condition (a) with completion and occupancy of the Project.
- (c) Condition (b) with implementation of Project mitigation measures where necessary.
- (d) Condition (a) plus one percent (1.0%) annual ambient traffic growth through year 2024 and with completion and occupancy of the related projects (i.e., future cumulative baseline).
- (e) Condition (d) with completion and occupancy of the Project.
- (f) Condition (e) with implementation of Project mitigation measures where necessary.

The traffic volumes for each new condition were added to the volumes in the prior condition to determine the change in capacity utilization at the study intersections.

9.0 CITY OF LOS ANGELES TRAFFIC ANALYSIS

The traffic impact analysis prepared for the 10 study intersections located within or shared with the City of Los Angeles using the CMA methodology and application of the City of Los Angeles significant traffic impact criteria is summarized in *Table 9–1*. The CMA data worksheets for the analyzed intersections are contained in *Appendix B*.

9.1 Existing Conditions

9.1.1 Existing Conditions

As indicated in column [1] of *Table 9–1*, the 10 study intersections located within or shared with the City of Los Angeles are presently operating at LOS D or better during the weekday AM and PM peak hours under existing conditions. The existing traffic volumes at the study intersections during the weekday AM and PM peak hours are displayed in *Figures 5–1* and 5–2, respectively.

9.1.2 Existing With Project Conditions

As shown in column [2] of *Table 9–1*, application of the City's threshold criteria to the "Existing With Project" scenario indicates that the Project would not result in a significant impact at any of the 10 study intersections. Incremental, but not significant, impacts are noted at the study intersections. Therefore, no mitigation measures are required or recommended with respect to these intersections under the "Existing With Project" conditions. The existing with Project traffic volumes at the study intersections during the weekday AM and PM peak hours are illustrated in *Figures 9–1* and *9–2*, respectively.

9.2 Future Conditions

9.2.1 Future Cumulative Baseline Conditions

The future cumulative baseline conditions were forecast based on the addition of traffic generated by the completion and occupancy of related projects, as well as the growth in traffic due to the combined effects of continuing development, intensification of existing developments and other factors (i.e., ambient growth). The v/c ratios at all of the study intersections are incrementally increased with the addition of ambient traffic and traffic generated by the related projects listed in *Table 6–1*.

As presented in column [3] of *Table 9–1*, nine of the 10 study intersections located within or shared with the City of Los Angeles are expected to operate at LOS D or better during the weekday AM and PM peak hours with the addition of growth in ambient traffic and related project traffic under the future cumulative baseline conditions. The following intersection is expected to operate at LOS E during the peak hours shown below under the future cumulative baseline conditions:

 Int. No. 11: La Cienega Boulevard / Beverly Boulevard PM Peak Hour: v/c = 0.954, LOS E

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Table 9-1 SUMMARY OF VOLUME TO CAPACITY RATIOS AND LEVELS OF SERVICE CITY OF LOS ANGELES INTERSECTIONS

08-Mar-19

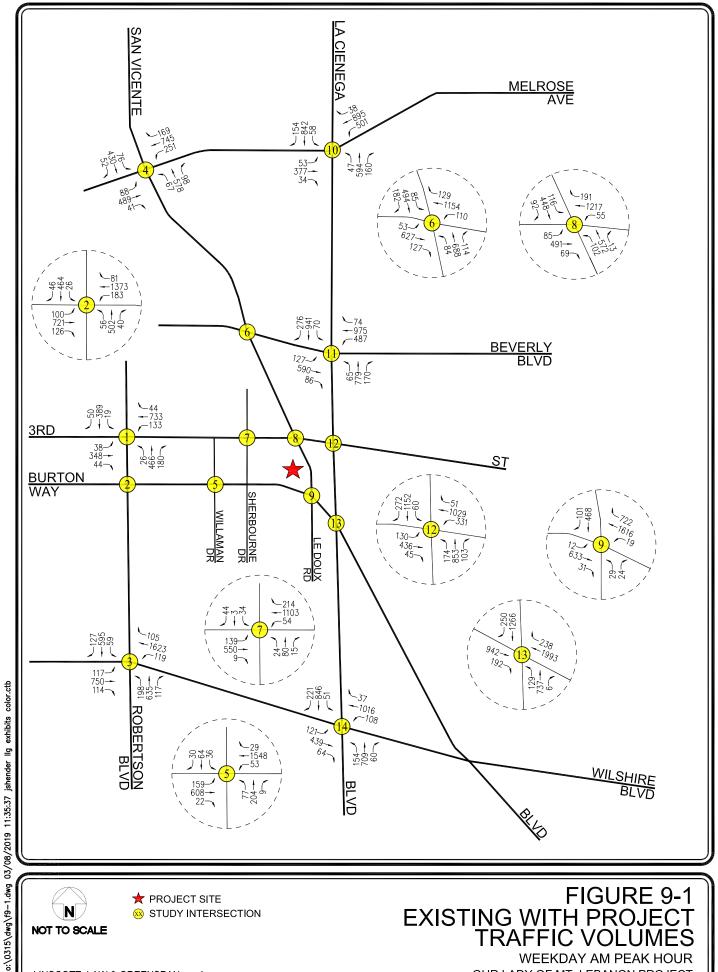
			[1]			[2]			[3]		[4]			
					YEAR	2018			YEAR	2024	YEAR	2024		
			YEAR	2018	EXIST	ING	CHANGE	SIGNIF.	FUTURE	E PRE-	FUTU	RE	CHANGE	SIGNIF.
		PEAK	EXIST	ING	W/ PRO	JECT	V/C	IMPACT	PROJI	ECT	W/ PRO	JECT	V/C	IMPACT
NO.	INTERSECTION	HOUR	V/C	LOS	V/C	LOS	[(2)-(1)]	[a]	V/C	LOS	V/C	LOS	[(4)-(3)]	[a]
1	Robertson Boulevard /	AM	0.625	B	0.628	B	0.003	NO	0.678	B	0.681	B	0.003	NO
	3rd Street	PM	0.622	B	0.627	B	0.005	NO	0.692	B	0.697	B	0.005	NO
2	Robertson Boulevard /	AM	0.688	B	0.689	B	0.001	NO	0.754	C	0.755	C	0.001	NO
	Burton Way	PM	0.734	C	0.736	C	0.002	NO	0.792	C	0.795	C	0.003	NO
5	Willaman Drive /	AM	0.599	A	0.602	B	0.003	NO	0.643	B	0.647	B	0.004	NO
	Burton Way	PM	0.619	B	0.619	B	0.000	NO	0.664	B	0.664	B	0.000	NO
6	San Vicente Boulevard /	AM	0.669	B	0.670	B	0.001	NO	0.731	C	0.732	C	0.001	NO
	Beverly Boulevard	PM	0.695	B	0.695	B	0.000	NO	0.773	C	0.773	C	0.000	NO
7	Sherbourne Drive /	AM	0.459	A	0.463	A	0.004	NO	0.496	A	0.499	A	0.003	NO
	3rd Street	PM	0.447	A	0.451	A	0.004	NO	0.486	A	0.491	A	0.005	NO
8	San Vicente Boulevard /	AM	0.697	B	0.699	B	0.002	NO	0.776	C	0.778	C	0.002	NO
	3rd Street	PM	0.586	A	0.587	A	0.001	NO	0.665	B	0.666	B	0.001	NO

Table 9-1 (Continued) SUMMARY OF VOLUME TO CAPACITY RATIOS AND LEVELS OF SERVICE CITY OF LOS ANGELES INTERSECTIONS

			[1]				[2]		[3]				[4]	
					YEAR 2018		YEAR 2024		YEAR 2024					
			YEAR 2	2018	EXIST	ING	CHANGE	SIGNIF.	FUTURE	PRE-	FUTU	RE	CHANGE	SIGNIF.
		PEAK	EXIST	ING	W/ PRO	JECT	V/C	IMPACT	PROJI	ECT	W/ PRO	JECT	V/C	IMPACT
NO.	INTERSECTION	HOUR	V/C	LOS	V/C	LOS	[(2)-(1)]	[a]	V/C	LOS	V/C	LOS	[(4)-(3)]	[a]
9	San Vicente Boulevard-Le Doux Road /	AM	0.527	A	0.531	Α	0.004	NO	0.571	A	0.574	Α	0.003	NO
	Burton Way	PM	0.576	A	0.578	A	0.002	NO	0.623	В	0.625	В	0.002	NO
	1 C: D 1 1/	43.6	0.651	D	0.650	ъ	0.001	NO	0.717		0.710	-	0.002	NO
11	La Cienega Boulevard /	AM	0.651	В	0.652	В	0.001	NO	0.717	C	0.719	C	0.002	NO
	Beverly Boulevard	PM	0.859	D	0.860	D	0.001	NO	0.954	Е	0.956	E	0.002	NO
12	La Cienega Boulevard /	AM	0.798	С	0.803	D	0.005	NO	0.867	D	0.872	D	0.005	NO
	3rd Street	PM	0.692	В	0.693	В	0.001	NO	0.757	C	0.758	C	0.001	NO
13	La Cienega Boulevard /	AM	0.654	В	0.655	В	0.001	NO	0.715	C	0.717	C	0.002	NO
	San Vicente Boulevard	PM	0.663	В	0.667	В	0.004	NO	0.735	C	0.738	C	0.003	NO

[a] According to LADOT's "Transportation Impact Study Guidelines", December 2016, a transportation impact on an intersection shall be deemed significant in accordance with the following table:

Final v/c	LOS	Project Related Increase in v/c
0.701 - 0.800	C	equal to or greater than 0.040
0.801 - 0.900	D	equal to or greater than 0.020
> 0.901	E, F	equal to or greater than 0.010

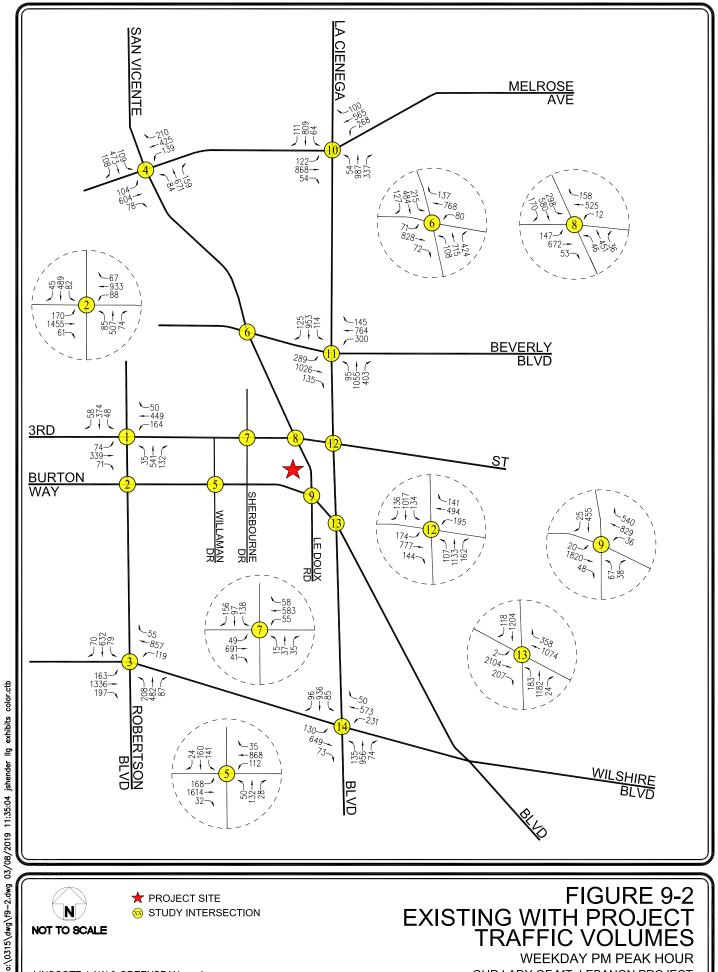




LINSCOTT, LAW & GREENSPAN, engineers

FIGURE 9-1 EXISTING WITH PROJECT TRAFFIC VOLUMES

WEEKDAY AM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT



★ PROJECT SITE **STUDY INTERSECTION** NOT TO SCALE

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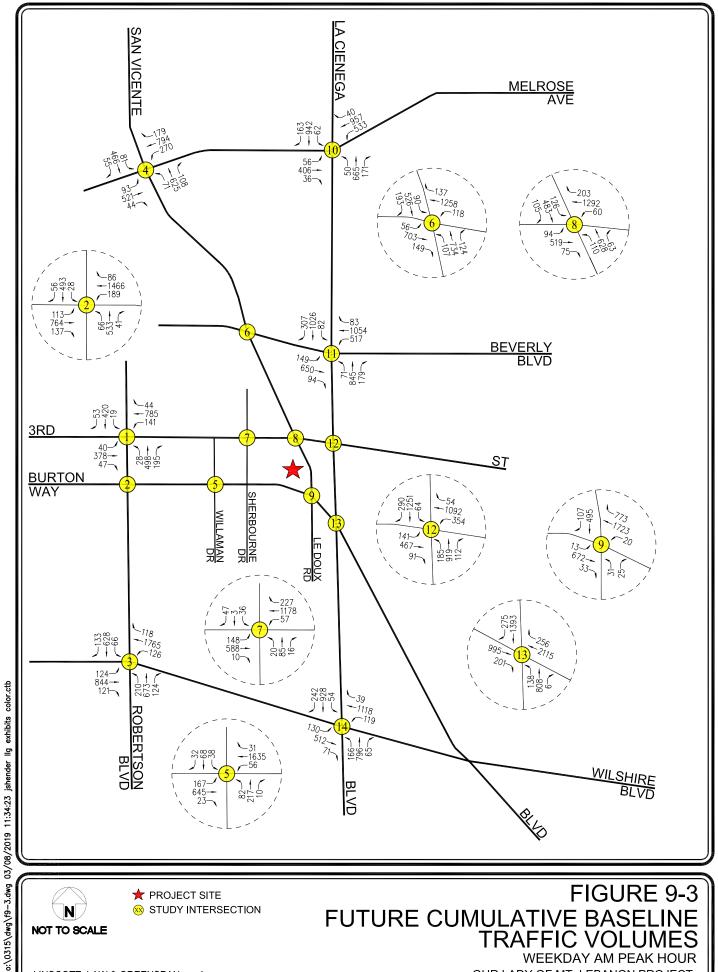
FIGURE 9-2 EXISTING WITH PROJECT TRAFFIC VOLUMES

WEEKDAY PM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT

The future cumulative baseline (existing, ambient growth and related Projects) traffic volumes at the study intersections during the weekday AM and PM peak hours are presented in *Figures 9–3* and *9–4*, respectively.

9.2.2 Future Cumulative With Project Conditions

The future cumulative with Project conditions were forecast based on the addition of traffic generated by the Project plus completion and occupancy of related projects. As shown in column [4] of *Table 9–1*, application of the City's threshold criteria to the "Future With Project" scenario indicates that the proposed Project would not result in a significant impact at any of the 10 study intersections. Incremental, but not significant impacts are noted at the study intersections. Therefore, no mitigation measures are required or recommended with respect to these intersections under the "Future Cumulative With Project" conditions. The future cumulative with Project (existing, ambient growth, related projects, and Project) traffic volumes at the study intersections during the weekday AM and PM peak hours are illustrated in *Figures 9–5* and *9–6*, respectively.

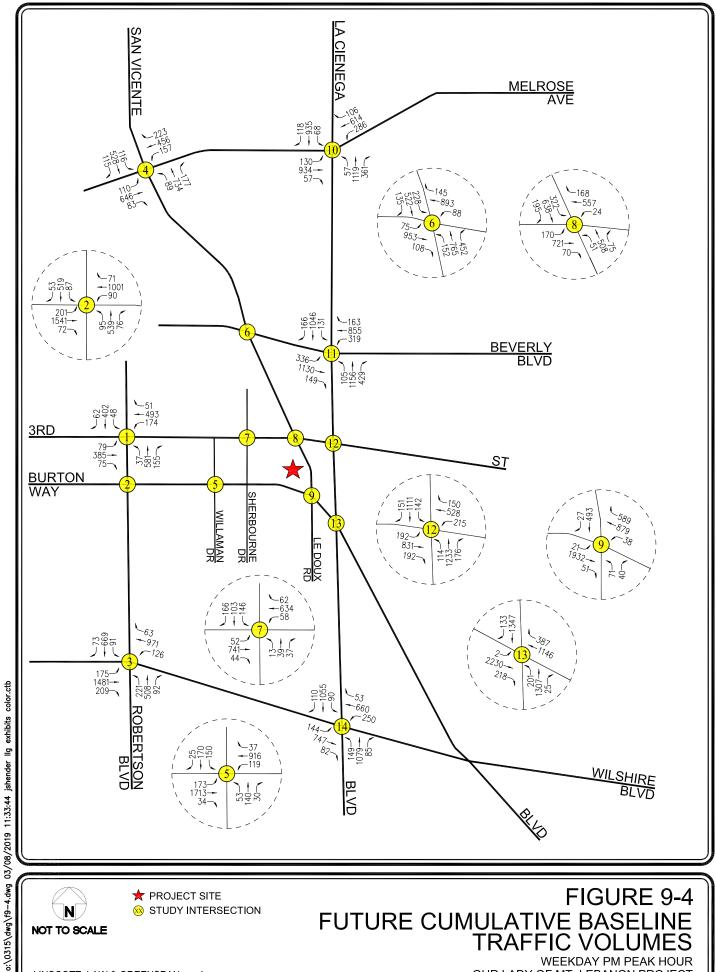


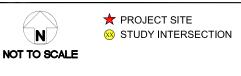
★ PROJECT SITE STUDY INTERSECTION NOT TO SCALE

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FUTURE CUMULATIVE BASELINE TRAFFIC VOLUMES

WEEKDAY AM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT

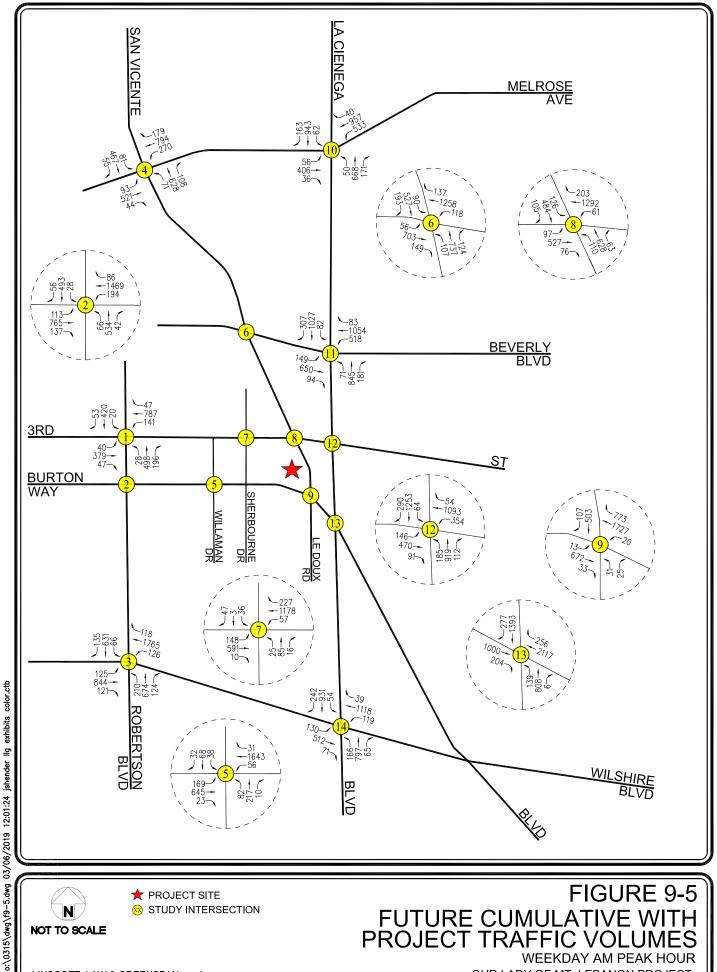




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FIGURE 9-4 FUTURE CUMULATIVE BASELINE TRAFFIC VOLUMES

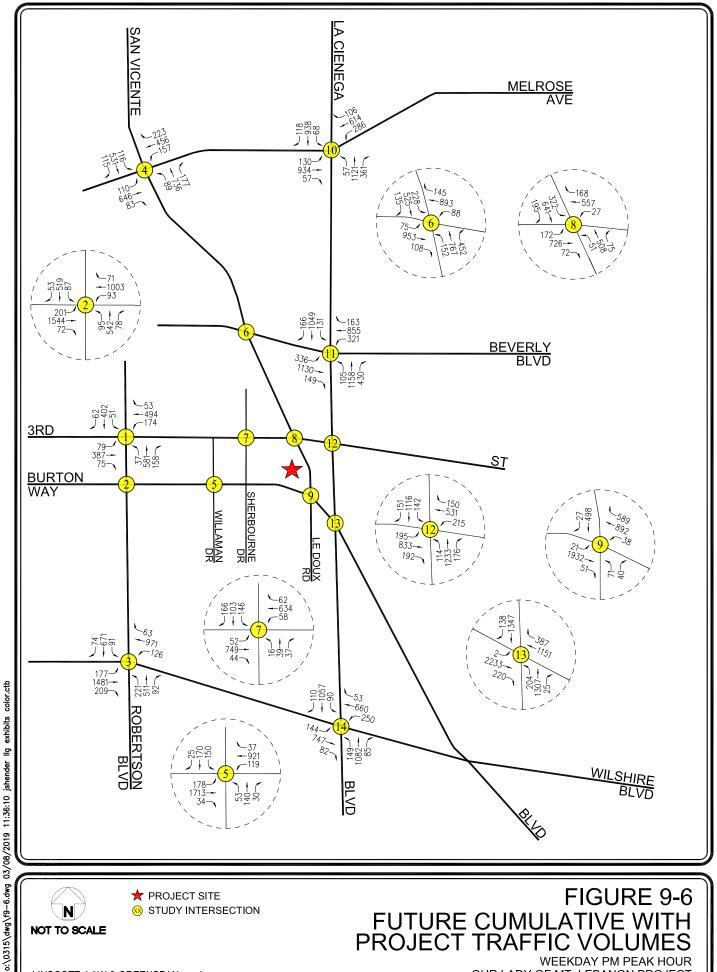
WEEKDAY PM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT



★ PROJECT SITE STUDY INTERSECTION NOT TO SCALE LINSCOTT, LAW & GREENSPAN, engineers

FUTURE CUMULATIVE WITH PROJECT TRAFFIC VOLUMES

WEEKDAY AM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT



★ PROJECT SITE STUDY INTERSECTION NOT TO SCALE

LINSCOTT, LAW & GREENSPAN, engineers

FIGURE 9-6 FUTURE CUMULATIVE WITH PROJECT TRAFFIC VOLUMES

WEEKDAY PM PEAK HOUR OUR LADY OF MT. LEBANON PROJECT

10.0 CITY OF BEVERLY HILLS TRAFFIC ANALYSIS

The traffic impact analysis prepared for the four study intersections located within or shared with the City of Beverly Hills using the ICU methodology and application of the City of Beverly Hills significant traffic impact criteria is summarized in *Table 10–1*. The ICU data worksheets for the analyzed intersections are contained in *Appendix C*.

10.1 Existing Conditions

10.1.1 Existing Conditions

As indicated in column [1] of *Table 10–1*, the four study intersections located within or shared with the City of Beverly Hills are presently operating at LOS D or better during the weekday AM and PM peak hours under existing conditions. The existing traffic volumes at the study intersections during the weekday AM and PM peak hours are displayed in *Figures 5–1* and *5–2*, respectively.

10.1.2 Existing With Project Conditions

As shown in column [2] of *Table 10–1*, application of the City's threshold criteria to the "Existing With Project" scenario indicates that the Project would not result in a significant impact at any of the four study intersections. Incremental, but not significant, impacts are noted at the study intersections. Therefore, no mitigation measures are required or recommended with respect to these intersections under the "Existing With Project" conditions. The existing with Project traffic volumes at the study intersections during the weekday AM and PM peak hours are illustrated in *Figures 9–1* and *9–2*, respectively.

10.2 Future Conditions

10.2.1 Future Cumulative Baseline Conditions

The future cumulative baseline conditions were forecast based on the addition of traffic generated by the Project plus completion and occupancy of related projects, as well as the growth in traffic due to the combined effects of continuing development, intensification of existing developments and other factors (i.e., ambient growth). The v/c ratios at all of the study intersections are incrementally increased with the addition of ambient traffic and traffic generated by the related projects listed in *Table 6–1*.

As presented in column [3] of *Table 10–1*, three of the four study intersections located within or shared with the City of Beverly Hills are expected to operate at LOS D or better during the weekday AM and PM peak hours with the addition of growth in ambient traffic and related project traffic under the future cumulative baseline conditions. The following intersection is expected to operate at LOS E during the peak hours shown below under the future cumulative baseline conditions:

 Int. No. 3: Robertson Boulevard / Wilshire Boulevard AM Peak Hour: v/c = 0.914, LOS E PM Peak Hour: v/c = 0.901, LOS E

Table 10-1 SUMMARY OF VOLUME TO CAPACITY RATIOS AND LEVELS OF SERVICE AM AND PM PEAK HOURS CITY OF BEVERLY HILLS INTERSECTIONS

02-Apr-19

			[1]				[2]						[4]	4]	
			YEAR 2	2018	YEAR :	2018	CHANGE		YEAR 2024		YEAR	2024	CHANGE		
			EXIST	ING	EXIST	ING	IN		FUTURE	PRE-	FUTU	IRE	IN		
					W/ PRO	JECT	DELAY	SIGNIF.	PROJE	ECT	W/ PRO	JECT	DELAY	SIGNIF.	
		PEAK	DELAY		DELAY		OR V/C	IMPACT	DELAY		DELAY		OR V/C	IMPACT	
NO.	INTERSECTION	HOUR	OR V/C	LOS	OR V/C	LOS	[(2)-(1)]	[a]	OR V/C	LOS	OR V/C	LOS	[(4)-(3)]	[a]	
2	Robertson Boulevard /	AM	0.802	D	0.802	D	0.000	NO	0.860	D	0.861	D	0.001	NO	
	Burton Way	PM	0.843	D	0.845	D	0.002	NO	0.894	D	0.897	D	0.003	NO	
3	Robertson Boulevard /	AM	0.858	D	0.861	D	0.003	NO	0.914	E	0.916	E	0.002	NO	
	Wilshire Boulevard	PM	0.842	D	0.843	D	0.001	NO	0.901	E	0.902	E	0.001	NO	
13	La Cienega Boulevard /	AM	0.807	D	0.808	D	0.001	NO	0.864	D	0.865	D	0.001	NO	
	San Vicente Boulevard	PM	0.815	D	0.819	D	0.004	NO	0.883	D	0.886	D	0.003	NO	
				_		_				_		_			
14	La Cienega Boulevard /	AM	0.713	C	0.714	C	0.001	NO	0.770	C	0.771	C	0.001	NO	
	Wilshire Boulevard	PM	0.694	В	0.694	В	0.000	NO	0.765	C	0.765	C	0.000	NO	

[a] According to the City of Beverly Hills' "Traffic Thresholds of Significance", Adopted October 2010, an impact is considered significant if the final volume-to-capacity ratio (v/c) equals or exceeds the thresholds shown below:

 $\begin{array}{c|cccc} \underline{Level \ of \ Service} & \underline{Final \ V/C} & \underline{Project\text{-}Related \ Increase \ in \ V/C} \\ D & > 0.800 - 0.900 & equal \ to \ or \ greater \ than \ 0.030 \\ E/F & > 0.900 & equal \ to \ or \ greater \ than \ 0.020 \\ \end{array}$

The future cumulative baseline (existing, ambient growth and related Projects) traffic volumes at the study intersections during the weekday AM and PM peak hours are presented in *Figures 9–3* and *9–4*, respectively.

10.2.2 Future Cumulative With Project Conditions

The future cumulative with Project conditions were forecast based on the addition of traffic generated by the Project plus completion and occupancy of related projects. As shown in column [4] of *Table 10–1*, application of the City's threshold criteria to the "Future With Project" scenario indicates that the proposed Project would not result in a significant impact at any of the four study intersections. As indicated in *Table 10–1*, no significant impacts would occur at the four study intersections. Therefore, no mitigation measures are required or recommended with respect to these intersections under the "Future Cumulative With Project" conditions. The future cumulative with Project (existing, ambient growth, related projects, and Project) traffic volumes at the study intersections during the weekday AM and PM peak hours are illustrated in *Figures 9–5 and 9–6*, respectively.

11.0 CITY OF WEST HOLLYWOOD TRAFFIC ANALYSIS

The traffic impact analysis prepared for the three study intersections located within or shared with the City of West Hollywood using the HCM 2010 methodology and application of the City of West Hollywood significant traffic impact criteria is summarized in *Table 11–1*. The HCM 2010 data worksheets for the analyzed intersections are contained in *Appendix D*.

11.1 Existing Conditions

11.1.1 Existing Conditions

As indicated in column [1] of *Table 11–1*, the three study intersections located within or shared with the City of West Hollywood are presently operating at LOS C or better during the weekday AM and PM peak hours under existing conditions. The existing traffic volumes at the study intersections during the weekday AM and PM peak hours are displayed in *Figures 5–1* and *5–2*, respectively.

11.1.2 Existing With Project Conditions

As shown in column [2] of *Table 11–1*, application of the City's threshold criteria to the "Existing With Project" scenario indicates that the Project would not result in a significant impact at any of the three study intersections. Incremental, but not significant, impacts are noted at the study intersections. Therefore, no mitigation measures are required or recommended with respect to these intersections under the "Existing With Project" conditions. The existing with Project traffic volumes at the study intersections during the weekday AM and PM peak hours are illustrated in *Figures 9–1* and *9–2*, respectively.

11.2 Future Conditions

11.2.1 Future Cumulative Baseline Conditions

The future cumulative baseline conditions were forecast based on the addition of traffic generated by the Project plus completion and occupancy of related projects, as well as the growth in traffic due to the combined effects of continuing development, intensification of existing developments and other factors (i.e., ambient growth). The delay value at all of the study intersections are incrementally increased with the addition of ambient traffic and traffic generated by the related projects listed in Table 6-1.

As presented in column [3] of *Table 11–1*, the three study intersections located within or shared with the City of West Hollywood are expected to operate at LOS C or better during the weekday AM and PM peak hours with the addition of growth in ambient traffic and related project traffic under the future cumulative baseline conditions. The future cumulative baseline (existing, ambient growth and related Projects) traffic volumes at the study intersections during the weekday AM and PM peak hours are presented in *Figures 9–3* and *9–4*, respectively.

Table 11-1 SUMMARY OF DELAY VALUES AND LEVELS OF SERVICE [A] AM AND PM PEAK HOURS CITY OF WEST HOLLYWOOD INTERSECTIONS

11-Mar-19

				[1]			[2]			[3]		[4]			
						YEAR	YEAR 2018				YEAR 2024				
				YEAR	2018	EXISTIN	G PLUS	CHANGE	SIGNIF.	YEAR	2024	FUTURE	PLUS	CHANGE	SIGNIF.
		INTERSECTION	PEAK	EXIST	ING	PROPOSED	PROJECT	DELAY	IMPACT	FUTU	RE	PROPOSED	PROJECT	DELAY	IMPACT
NO.	INTERSECTION	TYPE	HOUR	DELAY [B]	LOS [C]	DELAY	LOS	[(2)-(1)]	[D]	DELAY [B]	LOS [C]	DELAY	LOS	[(4)-(3)]	[D]
4	San Vicente Boulevard /	Commercial	AM	18.6	В	18.6	В	0.0	NO	19.6	В	19.6	В	0.0	NO
	Melrose Avenue	Corridor	PM	18.4	В	18.4	В	0.0	NO	19.0	В	19.0	В	0.0	NO
6	San Vicente Boulevard /	Commercial	AM	24.0	C	24.0	C	0.0	NO	25.3	C	25.3	C	0.0	NO
	Beverly Boulevard	Corridor	PM	26.5	C	26.5	C	0.0	NO	31.4	C	31.4	C	0.0	NO
10	La Cienega Boulevard /	Commercial	AM	20.4	C	20.4	C	0.0	NO	22.0	C	22.0	C	0.0	NO
	Melrose Avenue	Corridor	PM	21.7	C	21.7	C	0.0	NO	23.8	C	23.9	C	0.1	NO

- [A] Intersection analysis based on the Highway Capacity Manual 2010 operational analysis methodologies, per the City of West Hollywood.
- [B] Control delay reported in seconds per vehicle.
- [C] Signalized Intersection Levels of Service were based on the following criteria:

Control Delay (s/veh)	LC
<= 10	Α
> 10-20	В
> 20-35	C
> 35-55	D
> 55-80	E
> 80	F

[D] According to the City of West Hollywood, a transportation impact on an intersection shall be deemed significant in accordance with the following criteria:

Project Related Increase in Delay

LOS	Commercial Corridor	Signalized	Two-Way Stop
D	12 seconds	8 seconds	5 seconds
E	8 seconds	5 seconds	5 seconds
F	8 seconds	5 seconds	5 seconds

11.2.2 Future Cumulative With Project Conditions

The future cumulative with Project conditions were forecast based on the addition of traffic generated by the Project plus completion and occupancy of related projects. As shown in column [4] of *Table 11–1*, application of the City's threshold criteria to the "Future With Project" scenario indicates that the proposed Project would not result in a significant impact at any of the three study intersections. As indicated in *Table 11–1*, no significant impacts would occur at the three study intersections. Therefore, no mitigation measures are required or recommended with respect to these intersections under the "Future Cumulative With Project" conditions. The future cumulative with Project (existing, ambient growth, related projects, and Project) traffic volumes at the study intersections during the weekday AM and PM peak hours are illustrated in *Figures 9–5 and 9–6*, respectively.

12.0 RESIDENTIAL STREET SEGMENT ANALYSIS

A residential street segment analysis was prepared to evaluate Project-related traffic using local streets to access the Project site. Two residential street segments located near the Project site have been analyzed for potential impacts:

- Sherbourne Drive, south of 3rd Street; and
- Holt Avenue, south of 3rd Street.

The potential impacts of Project-generated traffic at the study street segments were identified using criteria set forth in LADOT's *Transportation Impact Study Guidelines*, December 2016. According to the City's published traffic study guidelines, a transportation impact on a local residential street shall be deemed significant based on an increase in the Project "Average Daily Traffic (ADT) volumes" as shown in *Table 12–1*.

Table 12-1							
CITY OF LOS ANGELES							
LOCAL RESIDENTIAL STREET SEGMENT IMPACT THRESHOLD CRITERIA							
Projected Average Daily Traffic With Project (Final ADT)	Project Related Increase in ADT						
0 to 999	120 or more						
1,000 to 1,999	12 percent or more of final ADT						
2,000 or 2,999	10 percent or more of final ADT						
3,000 or more	8 percent or more of final ADT						

Automatic 24-hour machine traffic counts were conducted on Thursday, May 17, 2018 for the analyzed street segments. Copies of the 24-hour machine counts are contained in *Appendix A*.

The forecast traffic conditions at the analyzed street segments for existing, existing with Project, future cumulative baseline, and future cumulative with Project scenarios are summarized in *Table 12–2*. As presented in column [1] of *Table 12–2*, the actual 24-hour count data was utilized to evaluate existing conditions on the roadway. Additionally, as shown in column [1] of *Table 12–2*, a 1.0 percent (1.0%) annual ambient growth rate through the year 2024 was conservatively added to the existing ADT volume in order to estimate the future cumulative baseline traffic volumes.

As presented in column [4] of *Table 12–2*, the Project daily trips would increase traffic volumes on Sherbourne Drive, south of 3rd Street by 2.2% and 2.1%, under existing with Project and future cumulative with Project conditions, respectively. The Project daily trips would increase traffic volumes on Holt Avenue, south of 3rd Street by 9.0% and 8.5%, under existing with Project and future cumulative with Project conditions, respectively. Therefore, based on the applicable 10% significance threshold presented in *Table 12–1*, and as indicated in *Table 12–2*, no significant impact would occur on either of the two analyzed street segments.

Table 12-2 RESIDENTIAL STREET SEGMENT ANALYSIS SUMMARY

08-Mar-19

			[1]	[2] PROPOSED		[3] DAILY	PROJECTED ADT		
			24-HOUR VOLUME	PROJECT DISTRIBUTION [b]		PROJECT BUILD-OUT	WITH PROJECT (FINAL ADT)	ADT % INCREASE	SEGMENT
NO.	STREET SEGMENT	SCENARIO [a]	W/O PROJECT	IN	OUT	TRIP ENDS [c]	[(1)+(3)]	WITH PROJECT	IMPACT [d]
1	Sherbourne Drive south of 3rd Street (west of Project Site)	Existing 2018 Future 2024	2,239 2,373	0.0%	15.0% 15.0%	49 49	2,288 2,422	2.2%	NO
2	Holt Avenue south of 3rd Street (west of Project Site)	Existing 2018 Future 2024	1,979 2,098	20.0% 20.0%	35.0% 35.0%	179 179	2,158 2,277	9.0% 8.5%	NO NO

- [a] Future 2024 traffic volumes estimated by applying a 1% annual growth factor to Existing 2018 traffic volumes.
- [b] See Figure 7-1, Project Trip Distribution for the forecast assignment of Project trips to Sherbourne Drive and Holt Avenue south of 3rd Street.
- [c] Forecast daily trips (325 inbound trips, 325 outbound trips) per Table 7-1 applied to forecast assignment of trips on street segment in Column [2].
- [d] According to LADOT's "Transportation Impact Study Guidelines, "December 2016, page 9: "A local residential street shall be deemed significantly impacted based on an increase in the projected average daily traffic (ADT) volumes."

Projected ADT with Project-Related
Project (Final ADT) Increase in ADT
0 to 999 120 or more

1,000 to 1,999
12 percent or more of final ADT
2,000 to 2,999
10 percent or more of final ADT
3,000 or more
8 percent or more of final ADT

13.0 CONGESTION MANAGEMENT PROGRAM TRAFFIC IMPACT ASSESSMENT

The Congestion Management Program (CMP) is a state-mandated program that was enacted by the California State Legislature with the passage of Proposition 111 in 1990. The program is intended to address the impact of local growth on the regional transportation system.

As required by the 2010 Congestion Management Program for Los Angeles County, a Traffic Impact Assessment (TIA) has been prepared to determine the potential impacts on designated monitoring locations on the CMP highway system. The analysis has been prepared in accordance with procedures outlined in the 2010 Congestion Management Program for Los Angeles County, County of Los Angeles Metropolitan Transportation Authority, 2010.

According to Section D.9.1 (Appendix D, page D-6) of the 2010 CMP manual, the criteria for determining a significant transportation impact is listed below:

"A significant transportation impact occurs when the proposed Project increases traffic demand on a CMP facility by 2% of capacity (V/C \geq 0.02), causing or worsening LOS F (V/C > 1.00)."

The CMP impact criteria apply for analysis of both intersection and freeway monitoring locations.

13.1 Intersections

The following CMP intersection monitoring locations in the Project vicinity have been identified:

•	CMP Station	Intersection
	No. 5	Santa Monica Boulevard / Wilshire Boulevard (2.0 miles west of Project Site)
	No. 6	La Cienega Boulevard / Wilshire Boulevard (Study Int. No. 14) (0.6 miles south of Project Site)
	No. 160	Doheny Drive / Santa Monica Boulevard (1.1 miles northwest of Project Site)
	No. 160	La Cienega Boulevard / Santa Monica Boulevard (1.1 miles north of Project Site)

The CMP TIA guidelines require that intersection monitoring locations must be examined if the proposed Project will add 50 or more trips during either the AM or PM weekday peak hours. Based on extrapolations of the traffic volume forecasts provided in *Figure 7–2* and *Figure 7–3*, the proposed Project would not add 50 or more trips during the AM or PM peak hours at any of the CMP monitoring locations. Specifically, the proposed Project is forecast to add the following peak hour traffic volumes to the CMP intersection monitoring locations:

- Santa Monica Boulevard / Wilshire Boulevard:
 - o 3 AM peak hour trips, 4 PM peak hour trips
- La Cienega Boulevard / Wilshire Boulevard
 - o 7 AM peak hour trips, 8 PM peak hour trips
- Doheny Drive / Santa Monica Boulevard
 - o 3 AM peak hour trips, 4 PM peak hour trips
- La Cienega Boulevard / Santa Monica Boulevard
 - o 7 AM peak hour trips, 8 PM peak hour trips

Therefore, no further review of potential impacts to intersection monitoring locations that are part of the CMP highway system is required.

13.2 Freeways

The following CMP freeway monitoring locations have been identified in the Project vicinity:

•	CMP Station	Location
	No. 1011	I-10 Freeway east of Overland Avenue
	No. 1012	I-10 Freeway east of La Brea Avenue

The CMP TIA guidelines require that freeway monitoring locations must be examined if the proposed Project will add 150 or more trips (in either direction) during either the AM or PM weekday peak periods. The proposed Project will not add 150 or more trips (in either direction) during either the AM or PM weekday peak hours to the CMP freeway monitoring locations, which number of trips is the threshold for preparing a traffic impact assessment, as stated in the CMP manual. Specifically, the proposed Project would add the following peak hour traffic volumes to the CMP freeway monitoring locations⁴:

- I-10 Freeway east of Overland Avenue
 - o 5 AM peak hour trips, 6 PM peak hour trips
- I-10 Freeway east of La Brea Avenue
 - o 6 AM peak hour trips, 5 PM peak hour trips

-

⁴ See Exhibit A contained within Appendix E for the detailed forecast assignment of Project trips to I-10.

Therefore, no further review of potential impacts to freeway monitoring locations that are part of the CMP highway system is required.

13.3 Transit Impact Review

A review has been made of the potential impacts of the Project on transit service based on the procedures outlined in the 2010 Congestion Management Program for Los Angeles County. As discussed in Section 4.4 herein, existing transit service is provided in the vicinity of the proposed Project.

The Project trip generation, as shown in *Table 7–1*, was adjusted by values set forth in the CMP (i.e., a person trip equals 1.4 times vehicle trips, and transit trips equal 3.5 percent of the total person trips) to estimate transit trip generation. Pursuant to the CMP guidelines, the proposed Project is forecast to generate demand for 2 transit trips during the AM peak hour and 3 transit trips during the PM peak hour. Over a 24-hour period, the proposed Project is forecast to generate demand for 32 daily transit trips. Therefore, the calculations are as follows:

- AM Peak Hour = $43 \times 1.4 \times 0.035 = 2$ Transit Trips
- PM Peak Hour = $53 \times 1.4 \times 0.035 = 3$ Transit Trips
- Daily Trips = $650 \times 1.4 \times 0.035 = 32$ Transit Trips

As shown in *Table 4–1*, 13 bus transit lines and routes are provided adjacent to or in close proximity the Project site. As outlined in *Table 4–1*, under the "No. of Buses/Trains During Peak Hour" column, these 13 public transit lines provide services for an average of (i.e., average of the directional number of buses/trains during the peak hours) 338 buses during the AM peak hour and 334 buses during the PM peak hour. Therefore, based on the above calculated AM and PM peak hour trips, this would correspond to an insignificant number of additional Project-generated transit trips per bus. It is anticipated that the existing transit service in the Project area will adequately accommodate the increase of Project-generated transit trips.

14.0 CONSTRUCTION IMPACT ASSESSMENT

14.1 Construction Assumptions

There are two phases related to construction of the Project, each with separate trip generation characteristics. First is the shoring/excavation phase, which generally results in the highest number of truck trips per day as compared to other phases of project construction. Second is the building construction phase, which typically generates the highest number of construction workers on site as compared to other phases of construction.

Shoring/Excavation

The shoring/excavation phase of the Project would result in the need to export approximately 110,000 cubic yards of material from the Project site. During this phase, hauling of material from the Project site would occur on weekdays between 7:00 AM and 4:00 PM (i.e., a 9-hour period), and on Saturdays between 8:00 AM and 3:00 PM (i.e., a 7-hour period). A total of 63 truck round-trips per day (i.e., 63 inbound and 63 outbound) carrying approximately 14 cubic yards of material per truck are expected on weekdays (i.e., 7 trucks per hour). Similarly, a total of 49 truck round-trips per day (i.e., 49 inbound and 49 outbound) carrying approximately 14 cubic yards of material per truck are expected based on Saturdays (i.e., 7 trucks per hour). Based on the estimated removal of 882 cubic yards of material on each weekday, and 686 cubic yards of material on each Saturday, it is expected that the materials would be removed from the Project site over a period of approximately 129 work days.

The precise route of haul trucks arriving to and departing from the Project site will be determined by the City's Advisory Agency in connection with this consideration of the proposed vesting tentative map for the Project. It is reasonable to assume, however, that the primary route to be used by haul trucks traveling to and from the Project site will include S. La Cienega Boulevard to and from the I-10 (Santa Monica) Freeway.

In addition to the trips by hauling trucks, approximately 60 round-trips per day by construction workers (30 inbound and 30 outbound) are expected related to the shoring/excavation phase during peak activity.

Building Construction

Building construction is estimated to occur over an approximate 28-month period. During peak construction activity, it is estimated that approximately 175 construction worker round-trips per day would be generated (175 inbound and 175 outbound), as well as 32 round-trips by miscellaneous delivery trucks (32 inbound and 32 outbound). Building construction is permitted in the City of Los Angeles on weekdays between 7:00 AM and 9:00 PM, as well as on Saturdays from 8:00 AM to 6:00 PM.

Construction Worker Parking and Roadway/Sidewalk Closures

Parking for construction workers will be provided in a lot in proximity to the Project site. Street parking by construction workers will not be permitted.

The construction of the Project would not require the closure of any vehicle travel lanes. This is due primarily to the availability of parking "lanes" adjacent to the Project site on San Vicente Boulevard, Burton Way and Holt Avenue, so that the use of the adjacent travel lanes should not be required. The street parking spaces adjacent to the Project site on Burton Way and/or Holt Avenue may be reserved for use by construction vehicles for the duration of construction. As these street parking spaces are likely associated with the existing uses on the Project site (which will be removed as part of the Project), the temporary unavailability of these street parking spaces is not expected to cause any adverse effect.

Temporary closures of the sidewalks adjacent to the Project site on San Vicente Boulevard, Burton Way, and Holt Avenue may be required during portions of the construction period, and the sidewalk along Burton Way could be closed for the duration of the Project construction. However, signs would be posted advising pedestrians of temporary sidewalk closures and providing alternative routes (e.g., if the sidewalk on the west side of San Vicente Boulevard adjacent to the Project site is temporarily closed, a sign or signs would direct pedestrians to use the sidewalk on the east side of San Vicente Boulevard as an alternative route). The Project applicant would prepare and submit a work site traffic control plan to LADOT prior to the start of construction. That plan would show the location of any temporary street parking or sidewalk closures, warning signs and access to abutting properties.

14.2 Vehicle Trip Generation

The potential traffic impacts of the Project at build-out and occupancy are assessed in Sections 9.0, 10.0 and 11.0 herein based on the evaluation of operations at local intersections during the weekday morning (AM) and afternoon (PM) commuter peak hours. Set forth below is a similar forecast of trip generation related to Project construction, which is provided for the AM and PM peak hours for comparison purposes to the Project at build-out. Also provided for informational purposes is a forecast of the weekday daily (24-hour) trip generation related to construction of the Project.

In addition to the construction assumptions outlined in the prior section, the following additional assumptions are made relative to vehicular trip generation during the construction period:

• Typically, most construction workers arrive and depart the worksite outside of the commuter peak hours. For this analysis, it has been conservatively assumed that 10% of the inbound daily trips would arrive at the Project site during the AM peak hour and that 10% of the outbound daily trips would depart the Project site during the PM peak hour.

• Trucks utilize more of the physical roadway as compared to passenger cars and small trucks. Thus, for trips generated by trucks, a passenger car equivalency (PCE) factor of 2.0 has been assumed based on factors provided in the *Highway Capacity Manual* published by the Transportation Research Board.

Table 14–1 provides the trip generation forecast related to construction of the Project. As shown in *Table 14–1*, and based on the preceding assumptions, the forecast trip generation by phase of construction is as follows:

Shoring/Excavation

- o 312 daily trips (156 inbound / 156 outbound)
- o 34 AM peak hour trips (20 inbound / 14 outbound)
- o 14 PM peak hour trips (30 inbound / 20 outbound)

• Building Construction

- o 478 daily trips (239 inbound / 239 outbound)
- o 63 AM peak hour trips (49 inbound/ 14 outbound)
- o 63 PM peak hour trips (14 inbound / 49 outbound)

14.3 Traffic Assessment

Table 7–1 provides the trip generation forecast for the Project at build-out. As shown in *Table 7–1*, the Project is forecast to generate 650 net new trips during a typical weekday, including 43 net new AM peak hour trips and 53 net new PM peak hour trips. By comparison, the shoring/excavation phase is estimated to generate 312 daily trips, 34 AM peak hour trips and 34 PM peak hour trips while the building construction phase is estimated to generate 478 daily trips, 63 AM peak hour trips and 63 PM peak hour trips. Thus, construction activity at the Project site during the shoring/excavation phase would generate fewer trips than the operation of the Project following its completion. Activity at the Project site during the building construction phase would generate fewer daily trips, 20 more AM peak hour trips, and 10 more PM peak hour trips than the operation of the Project following its completion.

Tables 9–1, 10–1 and 11–1 show that following construction, the Project's operational traffic impacts would be less than significant at all of the study intersections based on the City of Los Angeles thresholds of significance (and City of Beverly Hills and City of West Hollywood thresholds of significance for the four study intersections and three study intersections located therein, respectively). Accordingly, it is reasonable to conclude that construction activity at the Project site during the shoring/excavation phase of the Project would also result in traffic impacts that are less than significant. As shown in Table 14–1, the building construction phase is expected to generate 10 more trips during the AM peak hour and 20 more trips during the PM peak hour as compared to the operation of the Project following its completion. However, as shown on Tables 9–1, 10–1, and 11–1, the operation of the Project would not come close to causing a significant impact at any of the study intersections. Therefore, the addition on 10 more AM peak hour trips and 20 more PM peak hour trips would not result in a significant impact at any of the study intersections. Moreover, the construction traffic impact is temporary and would

Table 14-1 CONSTRUCTION TRIP GENERATION [1]

01-Apr-19

	DAILY	AM PEAK HOUR			PM PEAK HOUR		
	TRIP ENDS	VOLUMES			VOLUMES		
PHASE	VOLUMES	IN	OUT	TOTAL	IN	OUT	TOTAL
Shoring / Excavation Construction Workers Trucks PCE (2.0) Adjusted [2]	60	6	0	6	0	6	6
	126	7	7	14	7	7	14
	252	14	14	28	14	14	28
Phase Subtotal (PCE Adjusted)	312	20	14	34	14	20	34
Building Construction Construction Workers Trucks PCE (2.0) Adjusted [2]	350	35	0	35	0	35	35
	64	7	7	14	7	7	14
	128	14	14	28	14	14	28
Phase Subtotal (PCE Adjusted)	478	49	14	63	14	49	63

^[1] Source: KPFF

^[2] A Passenger Car Equivalent (PCE) factor of 2.0 was applied to all trucks based on standard traffic engineering practice to conservatively estimate the equivalent number of vehicles associated with the trucks.

and at the completion of construction. There relating to the construction of the Project is required.	efore, no a ired.	additional	analysis o	of traffic	impacts

15.0 CONCLUSIONS

This traffic impact analysis has been prepared to evaluate the potential impacts to the local street system resulting from the development of the proposed Our Lady of Mt. Lebanon Project. Fourteen intersections were identified and analyzed in order to determine changes in operations following construction and occupancy of the proposed Project. Application of the impact threshold criteria from the City of Los Angeles, City of Beverly Hills, and the City of West Hollywood indicate that none of the 14 study intersections would be significantly impacted by the forecast Project traffic. Incremental, but not significant, impacts are noted at the 14 study intersections evaluated in this analysis. As the Project is not expected to result in any significant traffic impacts, no traffic mitigation measures are required or recommended.

Additionally, a residential street segment analysis has been prepared to evaluate Project-related traffic using local streets to access the Project site. Two residential street segments were identified and analyzed in order to determine increases in Average Daily Traffic volumes following construction and occupancy of the Project. Application of the residential street segment impact threshold criteria from the City of Los Angeles indicate that neither of the analyzed street segments would be significantly impacted by the forecast Project traffic.

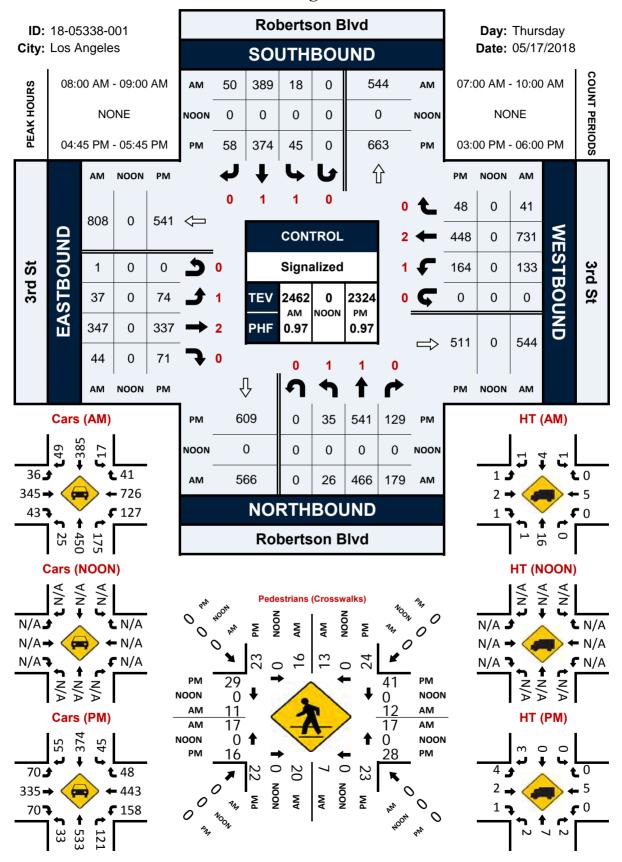
Furthermore, a Traffic Impact Assessment (TIA) has been prepared to determine the potential impacts on designated monitoring locations on the Congestion Management Program (CMP) highway system based on the procedures outlined in the 2010 CMP for Los Angeles County. Application of the impact threshold criteria outlined in the CMP manual indicate that none of the intersection and freeway monitoring locations within the Project's vicinity would be significantly impacted by the forecast Project traffic. In addition, a review of the potential impacts of the Project on transit service indicates that an insignificant number of additional transit trips per bus would be generated by the Project. It is anticipated that the existing transit service in the Project area would adequately accommodate the increase of Project-generated transit trips.

Finally, a Construction Impact Assessment has been prepared to determine the potential impacts of construction-related traffic to the local street system. It has been determined that trips generated during the shoring/excavation phase of the Project's construction would be fewer than the operation of the Project following its completion. The building construction phase is expected to generate slightly more AM and PM peak hour trips as compared to the operation of the Project following its completion. However, as the Project would not come close to causing a significant operational traffic impact on any of the 14 analyzed study intersections, the trips related to the building construction phase of the Project, which is temporary in duration, would not have a significant impact on any of the study intersections.

	APPENDIX A
Μανιιαι	TRAFFIC COUNT DATA

STREET: North/South	Robertson Blvd						
East/West	3rd St						
Day:	Thursday Date:	05/17/20	018 Weather:	SUNNY			
Hours:		C	hekrs: NDS				
School Day:	Yes		I/S COI	DE			
	N/B	S/B	E/B		W/B		
DUAL- WHEELED	66	47	29	_	34		
BIKES BUSES	9 34	7 0	14 1		13 35		
	N/B TIME	S/B TIME	E/B	TIME	W/B TIME		
AM PK 15 MIN	184 9.15	130 8.00	119	9.15	253 7.30		
PM PK 15 MIN	191 17.15	128 15.15	129	16.30	189 17.00		
AM PK HOUR	687 7.30	492 7.15	445	8.30	905 8.00		
PM PK HOUR	723 17.00	489 16.30	490	16.30	677 16.15		
NORTHBOUND A	proach	SOUTHB	OUND Approach		TOTAL	XING S/L	XING N/L
8-9 2 9-10 2 15-16 3 16-17 3	Th Rt Total 17 415 186 62 16 466 179 67 19 499 150 67 10 483 135 64 10 461 125 61 18 557 128 72	1 8-9 8 9-10 8 15-16 6 16-17	Lt Th 21 421 18 389 17 372 48 395 48 384 42 382	Rt Total 40 482 50 457 41 430 40 483 46 478 52 476	N-S 1110 1128 1108 1131 1094 1199	Ped Sch 10 1 25 2 18 0 55 2 36 0 40 0	Ped Sch 21 0 29 0 35 0 57 5 54 1 46 7
TOTAL 18	903 396	4 TOTAL	194 2343	269 2806	6770	184 5	242 13
EASTBOUND Appr	oach	WESTBO	OUND Approach		TOTAL	XING W/L	XING E/L
8-9 3 9-10 3 15-16 7 16-17 7	Th Rt Total 88 260 26 31 88 347 44 42 88 322 52 41 0 285 69 44 4 316 76 46 9 335 76 49 77 1865 343 253	9 8-9 2 9-10 4 15-16 6 16-17 0 17-18	Lt Th 145 624 133 731 102 548 133 415 169 440 156 413	Rt Total 48 817 41 905 61 711 75 623 45 654 48 617 318 4327	E-W 1131 1334 1123 1047 1120 1107	Ped Sch 22 1 28 0 14 0 48 0 40 1 52 2	Ped Sch 26 0 28 1 36 2 57 8 66 1 66 2
1011E 32	1005 545 255	IOIAL	030 3171	310 4327	0002	204 4	217 14

Robertson Blvd & 3rd St



Intersection Turning Movement Count

Location: Robertson Blvd & 3rd St City: Los Angeles Control: Signalized

Project ID: 18-05338-001 Date: 5/17/2018

Total

NS/EW Streets:		Robertso	on Blvd			Robertso	n Blvd			3rd	St			3rd	St		
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	BOUND		
AM	1	1	0	0	1	1	0	0	1	2	0	0	1	2	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	7	82	45	0	5	111	4	0	5	50	4	0	31	115	9	0	468
7:15 AM	8	93	48	0	7	103	10	0	10	69	12	0	40	152	17	0	569
7:30 AM	6	122	45	0	2	109	12	0	6	64	3	0	37	203	13	0	622
7:45 AM	6	118	48	0	7	98	14	0	7	77	7	0	37	154	9	0	582
8:00 AM	9	129	43	0	5	114	11	0	/	83	/.	0	24	170	3	0	605
8:15 AM 8:30 AM	4	110 105	42 47	0	3 6	91 100	15	0	13 8	86 81	16 9	0	38 38	186 178	10 14	0	619 603
8:45 AM	4	105	47	0	4	84	12 12	0	9	97	12	0	33	178	14	0	635
9:00 AM	7	109	33	0	2	89	10	0	12	87	10	0	24	150	15	0	548
9:15 AM	7	137	40	0	5	100	14	0	13	94	12	0	24	146	12	0	604
9:30 AM	9	119	38	0	4	98	8	0	7	79	13	0	22	119	19	0	535
9:45 AM	6	134	39	0	6	85	9	0	6	62	17	0	32	133	15	0	544
7.43 AW	U	134	37	U		03	,	U	U	02	- 17	U	32	133	13	U	344
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	82	1380	515	0	56	1182	131	0	103	929	122	1	380	1903	150	0	6934
APPROACH %'s:	4.15%	69.80%	26.05%	0.00%	4.09%	86.34%	9.57%	0.00%	8.92%	80.43%	10.56%	0.09%	15.62%	78.22%	6.17%	0.00%	
PEAK HR :	(08:00 AM -	09:00 AM														TOTAL
PEAK HR VOL :	26	466	179	0	18	389	50	0	37	347	44	1	133	731	41	0	2462
PEAK HR FACTOR:	0.722	0.903	0.952	0.000	0.750	0.853	0.833	0.000	0.712	0.894	0.688	0.250	0.875	0.928	0.732	0.000	0.969
		0.9	27			0.8	79			0.90	ງ9			0.92	77		0.707
		0.7				0.0											
																<u> </u>	
DM		NORTH	BOUND			SOUTH	BOUND	_		EASTB	OUND		_	WESTE	BOUND		
PM	1	NORTH 1	BOUND 0	0	1	SOUTH 1	BOUND 0	0	1	EASTB 2	OUND 0	0	1	WESTE 2	BOUND 0	0	TOTAL
	NL	NORTH 1 NT	BOUND 0 NR	NU	SL	SOUTH 1 ST	BOUND 0 SR	SU	EL	EASTB 2 ET	OUND 0 ER	EU	WL	WESTE 2 WT	BOUND 0 WR	WU	TOTAL
3:00 PM	NL 7	NORTH 1 NT 122	BOUND 0 NR 37	NU 0	SL 12	SOUTH 1 ST 103	BOUND 0 SR 9	SU 0	EL 13	EASTB 2 ET 78	OUND 0 ER 17	EU 0	WL 35	WESTE 2 WT 103	BOUND 0 WR 20	WU 0	556
3:00 PM 3:15 PM	NL 7 6	NORTH 1 NT 122 110	BOUND 0 NR 37 41	0 0	SL 12 14	SOUTH 1 ST 103 104	BOUND 0 SR 9 10	SU 0 0	EL 13 14	EASTB 2 ET 78 63	OUND 0 ER 17 14	0 0	WL 35 26	WESTE 2 WT 103 104	80UND 0 WR 20 20	0 0	556 526
3:00 PM 3:15 PM 3:30 PM	NL 7 6 9	NORTH 1 NT 122 110 123	BOUND 0 NR 37 41 27	0 0 0	SL 12 14 12	SOUTH 1 ST 103 104 99	BOUND 0 SR 9 10	0 0 0	13 14 21	EASTB 2 ET 78 63 71	OUND 0 ER 17 14	0 0 0	WL 35 26 34	WESTE 2 WT 103 104 96	80UND 0 WR 20 20 16	0 0 0	556 526 535
3:00 PM 3:15 PM 3:30 PM 3:45 PM	NL 7 6 9 8	NORTH 1 NT 122 110 123 128	BOUND 0 NR 37 41 27 30	NU 0 0 0	SL 12 14 12 10	SOUTH 1 ST 103 104 99 89	BOUND 0 SR 9 10 10 11	SU 0 0	EL 13 14 21 22	EASTB 2 ET 78 63 71 73	OUND 0 ER 17 14 17 21	0 0	WL 35 26 34 38	WESTE 2 WT 103 104 96 112	80UND 0 WR 20 20 16 19	WU 0 0 0 0	556 526 535 561
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM	NL 7 6 9	NORTH 1 NT 122 110 123	BOUND 0 NR 37 41 27	0 0 0	SL 12 14 12	SOUTH 1 ST 103 104 99	BOUND 0 SR 9 10 10 11	SU 0 0 0	13 14 21	EASTB 2 ET 78 63 71	OUND 0 ER 17 14	0 0 0 0	WL 35 26 34	WESTE 2 WT 103 104 96	80UND 0 WR 20 20 16	0 0 0	556 526 535
3:00 PM 3:15 PM 3:30 PM 3:45 PM	NL 7 6 9 8	NORTH 1 NT 122 110 123 128 118	BOUND 0 NR 37 41 27 30 35	NU 0 0 0 0	SL 12 14 12 10	SOUTH 1 ST 103 104 99 89	BOUND 0 SR 9 10 10 11	SU 0 0 0 0	EL 13 14 21 22 20	EASTB 2 ET	OUND 0 ER 17 14 17 21 21	EU 0 0 0 0	WL 35 26 34 38 51	WESTE 2 WT 103 104 96 112 102	80UND 0 WR 20 20 16 19	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM	NL 7 6 9 8 10 6	NORTH 1 NT 122 110 123 128 118 116	BOUND 0 NR 37 41 27 30 35 25	NU 0 0 0 0 0	SL 12 14 12 10 19 6	SOUTH 1 ST 103 104 99 89 97 78	BOUND 0 SR 9 10 10 11 10 18	SU 0 0 0 0 0	EL 13 14 21 22 20 14	EASTB 2 ET 78 63 71 73 68 76	OUND 0 ER 17 14 17 21 21 27	EU 0 0 0 0 0	WL 35 26 34 38 51 40	WESTE 2 WT 103 104 96 112 102 109	80UND 0 WR 20 20 16 19 13	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 7 6 9 8 10 6 9	NORTH 1 NT 122 110 123 128 118 116 113	BOUND 0 NR 37 41 27 30 35 25 25	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10	SOUTHI 1 ST 103 104 99 89 97 78 111	BOUND 0 SR 9 10 10 11 10 18 3 15 14	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17	EASTB 2 ET 78 63 71 73 68 76 87	OUND 0 ER 17 14 17 21 21 27 20	EU 0 0 0 0 0	WL 35 26 34 38 51 40 37	WESTE 2 WT 103 104 96 112 102 109 104	80UND 0 WR 20 20 16 19 13 11 7	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM	NL 7 6 9 8 10 6 9 5	NORTH 1 NT 122 110 123 128 118 116 113 114	BOUND 0 NR 37 41 27 30 35 25 25 40 31 28	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 9 16	SOUTHI 1 ST 103 104 99 89 97 78 111 98 93 92	BOUND 0 SR 9 10 10 11 10 18 3 15 14 15	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21	EASTB 2 ET 78 63 71 73 68 76 87 85 90 83	OUND 0 ER 17 14 17 21 21 27 20 8 21 18	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41	WESTE 2 WT 103 104 96 112 102 109 104 125 130 102	80UND 0 WR 20 20 16 19 13 11 7 14 14	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583
3:00 PM 3:15 PM 3:30 PM 3:35 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM	NL 7 6 9 8 10 6 9 5 3 15 12	NORTH 1 NT 122 110 123 128 118 116 113 114 131 148	BOUND 0 NR 37 41 27 30 35 25 25 40 31 28 30	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 9 16 10	SOUTH 1 ST 103 104 99 89 97 78 111 98 93 92 91	BOUND 0 SR 9 10 10 11 10 18 3 15 14	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21 18	EASTB 2 ET 78 63 71 73 68 76 87 85 90 83 79	OUND 0 ER 17 14 17 21 27 20 8 21 18 24	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41 45 35 43	WESTE 2 WT 103 104 96 112 102 109 104 125 130 102 91	80UND 0 WR 20 20 16 19 13 11 7 14 14 10 10	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583 570
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM	NL 7 6 9 8 10 6 9 5 3 15	NORTH 1 NT 122 110 123 128 118 116 113 114 131 148	BOUND 0 NR 37 41 27 30 35 25 25 40 31 28	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 9 16	SOUTHI 1 ST 103 104 99 89 97 78 111 98 93 92	BOUND 0 SR 9 10 10 11 10 18 3 15 14 15	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21	EASTB 2 ET 78 63 71 73 68 76 87 85 90 83	OUND 0 ER 17 14 17 21 21 27 20 8 21 18	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41 45 35	WESTE 2 WT 103 104 96 112 102 109 104 125 130 102	80UND 0 WR 20 20 16 19 13 11 7 14 14	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583
3:00 PM 3:15 PM 3:30 PM 3:345 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM	NL 7 6 9 8 10 6 9 5 3 15 12 8	NORTH 1 122 110 123 118 116 113 114 131 148 148 130	BOUND 0 NR 37 41 27 30 35 25 25 40 31 28 30 39	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 9 16 10 7	SOUTH 1 ST 103 104 99 97 78 111 98 93 92 91 106	BOUND 0 SR 9 10 10 11 10 18 3 15 14 15 14 9	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21 18 23	EASTB 2 ET 78 63 71 73 68 76 85 90 83 79 83	OUND 0 ER 17 14 17 21 21 27 20 8 21 18 24 13	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41 45 35 43 33	WESTE 2 WT 103 104 96 112 102 109 104 125 130 102 91 90	SOUND 0 WR 20 20 20 16 19 13 11 7 14 14 10 10	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583 570 555
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:10 PM 5:15 PM 5:30 PM 5:45 PM	NL 7 6 9 8 10 6 9 5 3 15 12 8 NL	NORTH 1 NT 122 110 123 128 118 116 113 114 131 148 148 130 NT	BOUND 0 NR 37 411 27 30 35 25 25 40 31 28 30 39 NR	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 9 16 10 7	SOUTH 1 1 ST 103 104 99 89 97 77 8 111 98 93 92 91 106 ST	BOUND 0 SR 9 10 110 11 10 18 3 15 14 19 SR	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21 18 23 EL	EASTB 2 ET 78 63 71 73 68 76 87 85 90 83 79 83	OUND 0 ER 17 14 17 21 21 27 20 8 21 18 24 13 ER	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41 45 35 43 33	WESTE 2 WT 103 104 96 112 109 109 104 125 130 102 91 90 WT	SOUND 0 WR 20 20 116 119 13 11 7 14 14 10 10 14 WR	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583 570 555
3:00 PM 3:15 PM 3:30 PM 3:345 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	NL 7 6 9 8 10 6 9 5 3 15 12 8 NL 98	NORTH 1 NT 122 110 123 128 118 116 113 114 131 148 130 NT 1501	BOUND 0 NR 37 41 27 30 35 25 25 40 31 28 30 9 NR 388	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 9 16 10 7	SOUTH 1 1 ST 103 104 99 89 97 78 8111 98 93 92 91 106 ST 1161	BOUND 0 SR 9 10 10 11 11 10 18 3 15 14 15 14 9	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21 18 23 EL 223	EASTB 2 ET 78 63 71 73 68 76 87 78 85 90 83 79 83 ET 936	OUND 0 ER 17 14 17 21 27 20 8 21 18 24 13 ER 221	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41 45 35 43 33 WL 458	WESTE 2 WT 103 104 96 112 102 109 104 125 130 102 91 90 WT 1268	OUND 0 WR 20 20 16 19 13 11 14 14 10 10 14 WR 168	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583 570 555
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:35 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	NL 7 6 9 8 10 6 9 5 3 15 12 8 NL 98 4.93%	NORTH 1 NT 122 110 123 128 118 116 113 114 131 148 148 130 NT 1501 75.54%	BOUND 0 NR 37 41 27 30 35 25 25 40 31 38 30 39 NR 388 19.53%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 9 16 10 7	SOUTH 1 1 ST 103 104 99 89 97 77 8 111 98 93 92 91 106 ST	BOUND 0 SR 9 10 110 11 10 18 3 15 14 19 SR	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21 18 23 EL	EASTB 2 ET 78 63 71 73 68 76 87 85 90 83 79 83	OUND 0 ER 17 14 17 21 21 27 20 8 21 18 24 13 ER	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41 45 35 43 33	WESTE 2 WT 103 104 96 112 109 109 104 125 130 102 91 90 WT	SOUND 0 WR 20 20 116 119 13 11 7 14 14 10 10 14 WR	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583 570 555 TOTAL 6698
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:00 PM 4:15 PM 4:30 PM 5:15 PM 5:10 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	NL 7 6 9 8 10 6 9 5 3 15 12 8 NL 98 4.93%	NORTH 1 NT 122 110 123 128 118 116 113 114 131 148 130 NT 1501 75.54%	BOUND 0 NR 37 41 27 30 35 25 25 40 31 28 30 39 NR 388 19.53% 05:45 PM	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 9 16 10 7 SL 138 9,60%	SOUTHI 1 ST 103 104 99 89 97 78 111 98 93 92 91 106 ST 1161 80.79%	BOUND 0 SR 9 10 10 110 118 3 15 14 15 14 9 SR 138 9.60%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21 18 23 EL 223 16.16%	EASTB 2 ET 78 63 71 73 76 87 86 87 90 83 ET 936 67.83%	OUND 0 ER 17 14 17 21 27 20 8 21 18 24 13 ER 221 16.01%	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41 45 35 43 33 WL 458 24.18%	WESTE 2 WT 103 104 96 112 1009 1009 1004 125 130 1009 1009 1009 1009 1009 1009 1009	OUND 0 WR 20 20 16 19 13 11 7 7 14 14 10 10 14 WR 168 8.87%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583 570 555 TOTAL 6698
3:00 PM 3:15 PM 3:30 PM 3:345 PM 4:00 PM 4:15 PM 4:30 PM 4:44 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR: VOL:	NL 7 6 9 8 10 6 9 5 3 15 12 8 NL 98 4.93%	NORTH 1 NT 122 110 123 128 118 116 113 114 131 148 148 149 150 NT 1501 75.54% 04:45 PM - 541	BOUND 0 NR 37 41 27 30 35 25 40 31 28 30 39 39 NR 388 19.53% 05:45 PM 129	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 10 7 SL 138 9.60%	SOUTHI 1 ST 103 104 99 89 97 78 111 98 93 92 91 106 ST 1161 80.79%	BOUND 0 SR 9 10 10 11 10 18 3 15 14 15 14 9 SR 138 9.60%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21 18 23 EL 223 16.16%	EASTB 2 ET 78 63 71 73 68 76 87 76 87 90 83 ET 936 67.83%	OUND 0 ER 17 14 17 21 21 27 20 8 21 18 24 13 ER 221 16.01%	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41 45 35 43 33 WL 458 24.18%	WESTE 2 WT 103 104 96 112 109 104 125 130 102 91 109 WT 1268 66.95%	SOUND 0 WR 20 20 16 19 13 11 7 7 14 14 10 10 14 WR 168 8.87%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583 570 555 TOTAL 6698
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:00 PM 4:15 PM 4:30 PM 5:15 PM 5:10 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	NL 7 6 9 8 10 6 9 5 3 15 12 8 NL 98 4.93%	NORTH 1 NT 122 110 123 128 118 116 113 114 131 148 130 NT 1501 75.54%	BOUND 0 NR 37 41 27 30 35 25 40 31 28 30 39 NR 388 19.53% 05:45 PM 129 0.806	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 12 14 12 10 19 6 13 10 9 16 10 7 SL 138 9,60%	SOUTHI 1 ST 103 104 99 89 97 78 111 98 93 92 91 106 ST 1161 80.79%	BOUND 0 SR 9 10 10 11 11 10 18 3 15 14 15 14 9 SR 138 9.60% 58 0.967	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 13 14 21 22 20 14 22 18 17 21 18 23 EL 223 16.16%	EASTB 2 ET 78 63 71 73 76 87 86 87 90 83 ET 936 67.83%	OUND 0 ER 17 14 17 21 27 20 8 21 18 24 13 ER 221 16.01%	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 35 26 34 38 51 40 37 41 45 35 43 33 WL 458 24.18%	WESTE 2 WT 103 104 96 112 1009 1009 1004 125 130 1009 1009 1009 1009 1009 1009 1009	OUND 0 WR 20 16 19 13 11 7 14 14 10 10 14 WR 168 8.87% 48 0.857	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	556 526 535 561 564 526 551 573 598 583 570 555 TOTAL 6698

766 5631 616 7013

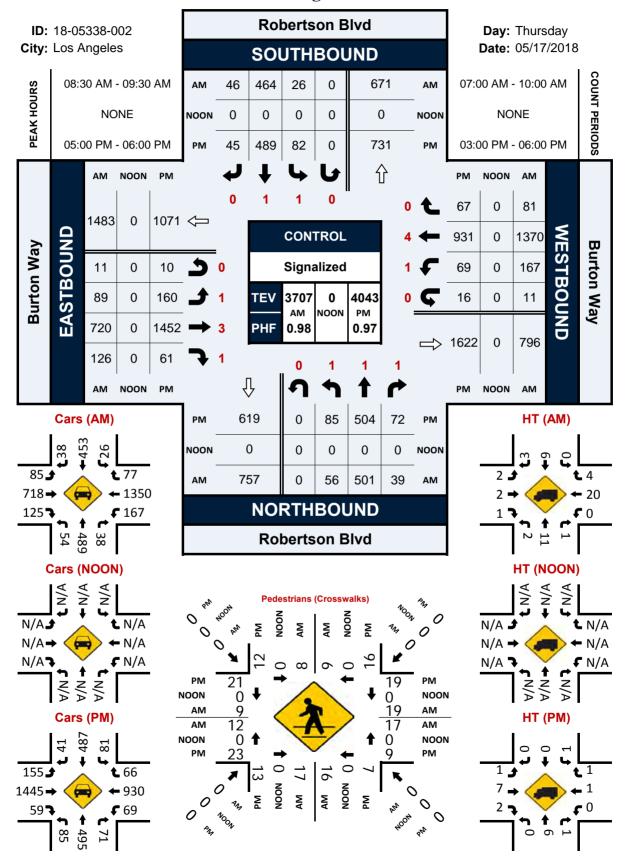
TOTAL

STREET: North/South		Robertson	n Blvd											
East/West		Burton W	ay											
Day:		Thursday		Date:		05/17/2	018	Weather:		SUNNY				
Hours:						(Chekrs:	NDS		-				
School Day:			Yes		·=			I/S CO	DE					
DULL		N/B		_	S/B			E/B		_	W/B			
DUAL- WHEELED BIKES BUSES		58 14 13			49 5 35			51 26 22			82 20 1			
		N/B	TIME	_	S/B	TIME		E/B	TIME		W/B	TIME		
AM PK 15 MIN	V	160	7.30		156	7.15		261	9.15		440	8.30		
PM PK 15 MIN	V	192	17.30		174	16.30		437	17.15		288	17.15		
AM PK HOUR		622	7.30		596	7.15		966	9.00		1630	8.00		
PM PK HOUR		662	16.45		631	16.00		1683	17.00		1083	17.00		
NORTHBOU	ND App	roach				SOUTHI	BOUND Ap	proach				TOTAL	XING S/L	XING N/L
Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 59 67 43 77 79 85	Th 479 502 499 447 441 504	Rt 37 43 42 46 71 72	575 612 584 570 591 661		Hours 7-8 8-9 9-10 15-16 16-17 17-18	3	Th 21 515 35 491 34 446 76 469 05 497 32 489	Rt 51 53 46 59 29 45	Total 587 579 526 604 631 616		N-S 1162 1191 1110 1174 1222 1277	Ped Sch 8 0 30 0 19 1 20 0 19 0 20 0	Ped Sch 5 0 17 0 10 1 13 0 20 0 28 0
TOTAL	410	2872	311	3593		TOTAL	35	53 2907	283	3543	[7136	116 1	93 1
EASTBOUND	Appro	ach				WESTBO	OUND App	roach				TOTAL	XING W/L	XING E/L
Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 82 95 113 152 154 170	618 704 1179 1334	Rt 93 113 149 109 91 61	519 826 966 1440 1579 1683		Hours 7-8 8-9 9-10 15-16 16-17 17-18		32 1363 55 1188	85 95 66 56	Total 1324 1630 1448 994 918 1083		E-W 1843 2456 2414 2434 2497 2766	Ped Sch 8 1 21 0 9 2 36 1 36 0 43 1	Ped Sch 22 1 35 1 30 7 39 0 33 0 28 0

804 6165 428 7397

14410 153 5 187 9

Robertson Blvd & Burton Way



Intersection Turning Movement Count

City: Los Angeles
Control: Signalized Project ID: 18-05338-002 Date: 5/17/2018

<u></u>								To	tal								
NS/EW Streets:		Robertso	on Blvd			Robertso	n Blvd			Burton	Way			Burton	Way		
		NORTHI	BOUND			SOUTH	BOUND			EASTB	OUND			WESTB	OUND		
AM	1	1	1	0	1	1	0	0	1	3	1	0	1	4	0	0	
7.00 414	NL 14	NT 100	NR 10	NU	SL	ST	SR 13	SU 0	EL	ET	ER	EU 1	WL	WT	WR	WU	TOTAL
7:00 AM 7:15 AM	14 19	116	10 6	0	2 7	122 135	13	0	23 16	61 71	11 22	1	20 41	231 258	12 15	1 1	621 722
7:30 AM	17	133	10	0	3	132	15	0	21	99	27	1	56	336	15	2	867
7:45 AM	9	130	11	0	9	126	9	Ö	18	113	33	i	39	279	17	ī	795
8:00 AM	16	131	13	0	11	122	13	0	24	132	24	0	43	336	33	3	901
8:15 AM	17	121	14	0	10	122	14	0	24	154	28	0	40	330	16	3	893
8:30 AM	15	119	11	0	4	128	14	0	18	157	39	1	44	374	21	1	946
8:45 AM 9:00 AM	19 10	131 118	5 16	0	10 3	119 103	12 12	0	27 21	175 198	22 26	0	45 44	323 334	15 17	2	907 904
9:00 AM 9:15 AM	12	133	7	0	9	114	8	0	23	198	26 39	9	34	334	28	5	950
9:30 AM	8	120	13	0	14	118	10	0	22	153	46	3	36	272	30	4	849
9:45 AM	13	128	6	0	8	111	16	0	32	163	38	3	36	243	20	4	821
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	169	1480	122	0	90	1452	150	0	269	1666	355	21	478	3655	239	30	10176
APPROACH %'s:	9.54%	83.57%	6.89%	0.00%	5.32%	85.82%	8.87%	0.00%	11.64%	72.09%	15.36%	0.91%	10.86%	83.03%	5.43%	0.68%	
PEAK HR :		8:30 AM -								700			4.77	4070			TOTAL
PEAK HR VOL : PEAK HR FACTOR :	56 0.737	501 0.942	39 0.609	0.000	26 0.650	464 0.906	46 0.821	0 0.000	89 0.824	720 0.909	126 0.808	11 0.306	167 0.928	1370 0.916	81 0.723	11 0.550	3707
PEAK HR FACTOR :	0.737	0.942		0.000	0.030	0.900		0.000	0.024	0.909		0.300	0.920	0.910		0.550	0.976
PM	1	NORTHI 1	BOUND 1	0	1	SOUTHI 1	0 O	0	1	EASTB 3	OUND 1	0	1	WESTB 4	OUND	0	
FIVI	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
3:00 PM	21											LU					916
3:15 PM		114	15	0	20	115	16	0	32	271	28	6	28	225	20	5	
	17	114 116	15 14	0	20 21	115 119	16 14	0		271 293	28 33	6 0	28 16	225 195	20 8		892
3:30 PM	17 23	116 102	14 8	0	21 21	119 116	14 18	0	32 36 33	293 312	33 29		16 23	195 199	8 21	5 10 5	892 912
3:30 PM 3:45 PM	23 16	116 102 115	14 8 9	0 0 0	21 21 14	119 116 119	14 18 11	0 0 0	32 36 33 40	293 312 303	33 29 19	0 2 3	16 23 22	195 199 197	8 21 17	5 10 5 3	892 912 888
3:30 PM 3:45 PM 4:00 PM	23 16 16	116 102 115 117	14 8 9	0 0 0	21 21 14 23	119 116 119 144	14 18 11 6	0 0 0	32 36 33 40 34	293 312 303 329	33 29 19 21	0 2 3	16 23 22 23	195 199 197 183	8 21 17 12	5 10 5 3	892 912 888 929
3:30 PM 3:45 PM 4:00 PM 4:15 PM	23 16 16 27	116 102 115 117 101	14 8 9 16 16	0 0 0	21 21 14 23 25	119 116 119 144 107	14 18 11 6 5	0 0 0 0	32 36 33 40 34 40	293 312 303 329 325	33 29 19 21 29	0 2 3 3	16 23 22 23 23	195 199 197 183 192	8 21 17 12 11	5 10 5 3 2 2	892 912 888 929 903
3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM	23 16 16 27 21	116 102 115 117 101 109	14 8 9 16 16 16	0 0 0	21 21 14 23 25 31	119 116 119 144 107 133	14 18 11 6 5	0 0 0	32 36 33 40 34 40 30	293 312 303 329 325 330	33 29 19 21 29 22	0 2 3	16 23 22 23 23 20	195 199 197 183 192 199	8 21 17 12 11 17	5 10 5 3	892 912 888 929 903 945
3:30 PM 3:45 PM 4:00 PM 4:15 PM	23 16 16 27	116 102 115 117 101	14 8 9 16 16	0 0 0 0	21 21 14 23 25	119 116 119 144 107	14 18 11 6 5	0 0 0 0 0	32 36 33 40 34 40	293 312 303 329 325	33 29 19 21 29	0 2 3 3 0 3	16 23 22 23 23	195 199 197 183 192	8 21 17 12 11	5 10 5 3 2 2 4	892 912 888 929 903
3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	23 16 16 27 21 15	116 102 115 117 101 109 114 120 142	14 8 9 16 16 16 23 10	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	21 21 14 23 25 31 26 24	119 116 119 144 107 133 113 129 126	14 18 11 6 5 10 8 6	0 0 0 0 0 0	32 36 33 40 34 40 30 43 38 40	293 312 303 329 325 330 350 362 382	33 29 19 21 29 22 19 18 14	0 2 3 3 0 3 1	16 23 22 23 23 20 23 22 12	195 199 197 183 192 199 189	8 21 17 12 11 17 16 9	5 10 5 3 2 2 4	892 912 888 929 903 945 942 997 1043
3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	23 16 16 27 21 15 18 16 25	116 102 115 117 101 109 114 120 142 138	14 8 9 16 16 16 23 10 12 29	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	21 21 14 23 25 31 26 24 12 29	119 116 119 144 107 133 113 129 126 109	14 18 11 6 5 10 8 6 10	0 0 0 0 0 0 0	32 36 33 40 34 40 30 43 38 40 29	293 312 303 329 325 330 350 362 382 359	33 29 19 21 29 22 19 18 14 9	0 2 3 3 0 3 1 2 1 6	16 23 22 23 23 20 23 22 12 19	195 199 197 183 192 199 189 235 249 210	8 21 17 12 11 17 16 9 19	5 10 5 3 2 2 4 2 4 8 4	892 912 888 929 903 945 942 997 1043 1000
3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	23 16 16 27 21 15 18 16	116 102 115 117 101 109 114 120 142	14 8 9 16 16 16 23 10	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	21 21 14 23 25 31 26 24	119 116 119 144 107 133 113 129 126	14 18 11 6 5 10 8 6	0 0 0 0 0 0 0	32 36 33 40 34 40 30 43 38 40	293 312 303 329 325 330 350 362 382	33 29 19 21 29 22 19 18 14	0 2 3 3 0 3 1 2	16 23 22 23 23 20 23 22 12	195 199 197 183 192 199 189 235 249	8 21 17 12 11 17 16 9	5 10 5 3 2 2 4 2 4 8	892 912 888 929 903 945 942 997 1043
3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:35 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	23 16 16 27 21 15 18 16 25 26	116 102 115 117 101 109 114 120 142 138 104	14 8 9 16 16 16 23 10 12 29 21	0 0 0 0 0 0 0 0	21 21 14 23 25 31 26 24 12 29 17	119 116 119 144 107 133 113 129 126 109 125	14 18 11 6 5 10 8 6 10 15 14	0 0 0 0 0 0 0 0 0	32 36 33 40 34 40 30 43 38 40 29 53	293 312 303 329 325 330 350 362 382 359 349	33 29 19 21 29 22 19 18 14 9 20	0 2 3 3 0 3 1 2 1 6 1	16 23 22 23 23 20 23 20 23 21 19 16	195 199 197 183 192 199 189 235 249 210 237	8 21 17 12 11 17 16 9 19 19 20	5 10 5 3 2 2 4 2 4 8 4 0	892 912 888 929 903 945 942 997 1043 1000 1003
3:30 PM 3:45 PM 4:10 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:30 PM 5:30 PM 5:45 PM	23 16 16 27 21 15 18 16 25 26 NL 241	116 102 115 117 101 109 114 120 142 138 104 NT 1392	14 8 9 16 16 16 16 23 10 12 29 21 NR 189	0 0 0 0 0 0 0 0 0	21 21 14 23 25 31 26 24 12 29 17	119 116 119 144 107 133 113 129 126 109 125 ST 1455	14 18 11 6 5 10 8 6 10 15 14 SR 133	0 0 0 0 0 0 0 0 0 0	32 36 33 40 34 40 30 43 38 40 29 53	293 312 303 329 325 330 350 362 382 359 349 ET 3965	33 29 19 21 29 22 19 18 14 9 20 ER 261	0 2 3 3 0 3 1 2 1 6 1	16 23 22 23 23 20 23 20 21 19 16 WL 247	195 199 197 183 192 199 189 235 249 210 237 WT 2510	8 21 17 12 11 17 16 9 19 19 20 WR 189	5 10 5 3 2 2 4 4 2 4 8 4 0	892 912 888 929 903 945 942 997 1043 1000 1003
3:30 PM 3:45 PM 4:100 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	23 16 16 27 21 15 18 16 25 26 NL 241 13.23%	116 102 115 117 101 109 114 120 142 138 104 NT 1392 76.40%	14 8 9 16 16 16 23 10 12 29 21 NR 189 10.37%	0 0 0 0 0 0 0 0	21 21 14 23 25 31 26 24 12 29 17	119 116 119 144 107 133 113 129 126 109 125	14 18 11 6 5 10 8 6 10 15 14	0 0 0 0 0 0 0 0 0	32 36 33 40 34 40 30 43 38 40 29 53	293 312 303 329 325 330 350 362 382 359 349	33 29 19 21 29 22 19 18 14 9 20	0 2 3 3 0 3 1 2 1 6 1	16 23 22 23 23 20 23 20 23 21 19 16	195 199 197 183 192 199 189 235 249 210 237	8 21 17 12 11 17 16 9 19 19 20	5 10 5 3 2 2 4 2 4 8 4 0	892 912 888 929 903 945 942 997 1043 1000 1003 TOTAL 11370
3:30 PM 3:45 PM 4:10 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:39 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	23 16 16 27 21 15 18 16 25 26 NL 241 13.23%	116 102 115 117 101 109 114 120 142 138 104 NT 1392 76.40%	14 8 9 16 16 16 16 23 10 12 29 21 NR 189 10.37%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	21 21 14 23 25 31 26 24 12 29 17 SL 263 14.21%	119 116 119 144 107 133 113 129 126 109 125 ST 1455 78.61%	14 18 11 6 5 10 8 6 10 15 14 SR 133 7.19%	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	32 36 33 40 34 40 30 43 38 40 29 53 EL 448 9.53%	293 312 303 329 325 330 350 362 382 359 349 ET 3965 84.33%	33 29 19 21 29 22 19 18 14 9 20 ER 261 5.55%	0 2 3 3 0 3 1 2 1 6 1 EU 28 0.60%	16 23 22 23 23 20 23 22 12 19 16 WL 247 8.25%	195 199 197 183 192 199 189 235 249 210 237 WT 2510 83.81%	8 21 17 12 11 17 16 9 19 19 20 WR 189 6.31%	5 10 5 3 2 2 4 4 2 4 8 4 0 WU 49 1.64%	892 912 888 929 903 945 942 997 1043 1000 1003 TOTAL 11370
3:30 PM 3:45 PM 4:100 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	23 16 16 27 21 15 18 16 25 26 NL 241 13.23%	116 102 115 117 101 109 114 120 142 138 104 NT 1392 76.40%	14 8 9 16 16 16 23 10 12 29 21 NR 189 10.37%	0 0 0 0 0 0 0 0 0	21 21 14 23 25 31 26 24 12 29 17	119 116 119 144 107 133 113 129 126 109 125 ST 1455	14 18 11 6 5 10 8 6 10 15 14 SR 133	0 0 0 0 0 0 0 0 0 0	32 36 33 40 34 40 30 43 38 40 29 53	293 312 303 329 325 330 350 362 382 359 349 ET 3965	33 29 19 21 29 22 19 18 14 9 20 ER 261	0 2 3 3 0 3 1 2 1 6 1	16 23 22 23 23 20 23 20 21 19 16 WL 247	195 199 197 183 192 199 189 235 249 210 237 WT 2510	8 21 17 12 11 17 16 9 19 19 20 WR 189	5 10 5 3 2 2 4 4 2 4 8 4 0	892 912 888 929 903 945 942 997 1043 1000 1003 TOTAL 11370

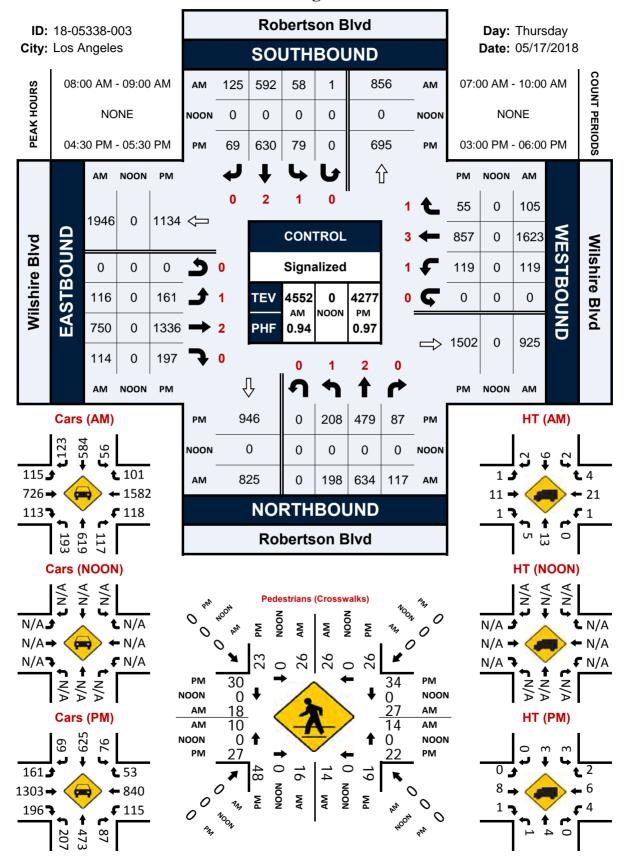
					'		011							
STREET: North/South	Ro	obertson	Blvd											
East/West	W	ilshire I	Blvd											
Day:	Th	ursday		Date:		05/17/	2018		Weather:		SUNNY			
Hours:							Chekrs	8:	NDS		-			
School Day:	_		Yes		-				I/S CC	DE				
	_	N/B			S/B				E/B		_	W/B		
DUAL- WHEELED BIKES BUSES		65 15 13			49 17 12				81 31 100			102 29 109		
	_	N/B	TIME	_	S/B	TIME			E/B	TIME		W/B	TIME	
AM PK 15 MIN	V	255	9.30		216	9.30			285	8.15		525	8.45	
PM PK 15 MIN	V	217	15.15		212	16.00			468	16.00		277	17.15	
AM PK HOUR		985	8.45		785	7.45			980	8.00		1847	8.00	
PM PK HOUR		834	15.00		791	16.00			1744	17.00		1031	16.30	
NORTHBOU	ND Approa	ich				SOUTH	BOUN	D Аррі	oach				TOTAL	XING S/L
Hours 7-8 8-9 9-10	Lt 196 198 194	Th 608 634 652	Rt 7 93 117 112	otal 897 949 958		Hours 7-8 8-9 9-10		Lt 52 59 62	592 580	Rt 109 125 112	776 754		N-S 1616 1725 1712	Ped Sch 24 0 30 0 35 0

Hours	Lt	Th	Rt	Total	Hours	Lt	Th	Rt	Total	_	N-S	Ped	Sch	Pe	d Sch	1
7-8	196	608	93	897	7-8	52	558	109	719		1616	24	0	4	9 2	J
8-9	198	634	117	949	8-9	59	592	125	776		1725	30	0	4	9 3	
9-10	194	652	112	958	9-10	62	580	112	754		1712	35	0	4	8 0	Ī
15-16	212	528	94	834	15-16	79	586	98	763		1597	53	8	4	3 3	1
16-17	202	453	91	746	16-17	80	637	74	791		1537	56	1	4	5 2	.]
17-18	205	518	78	801	17-18	70	579	65	714		1515	68	2	5	3 0	Ī
										_						_
TOTAL	1207	3393	585	5185	TOTAL	402	3532	583	4517		9702	266	11	28	7 10	Ī.
																-

XING N/L

EASTBOUN	D Approa	ch			WESTBOUN	D Approa	ch			TOTAL	XING	W/L	XING	E/L
Hours	Lt	Th	Rt	Total	Hours	Lt	Th	Rt	Total	E-W	Ped	Sch	Ped	Sch
7-8	76	597	83	756	7-8	104	1283	73	1460	2216	28	0	30	3
8-9	116	750	114	980	8-9	119	1623	105	1847	2827	26	2	34	7
9-10	88	720	145	953	9-10	132	1282	111	1525	2478	26	0	36	0
15-16	111	1153	185	1449	15-16	137	710	87	934	2383	37	13	57	13
16-17	149	1364	194	1707	16-17	124	801	57	982	2689	39	1	51	0
17-18	184	1337	223	1744	17-18	117	844	38	999	2743	60	0	49	1
		•												
TOTAL	724	5921	944	7589	TOTAL	733	6543	471	7747	15336	216	16	257	24

Robertson Blvd & Wilshire Blvd



Location: Robertson Blvd & Wilshire Blvd
City: Los Angeles
Control: Signalized Project ID: 18-05338-003 Date: 5/17/2018

NS/EW Streets: Robertson Blvd Robertson Blvd Wilshire Blvd Wilshire Blvd Wilshire Blvd Wilshire Blvd Wilshire Blvd Wilshire Blvd AM	TOTAL 749 927 1035 1121 1066 1157 1115 1214 1021
AVI 1 2 0 0 1 1 2 0 0 0 1 2 0 0 1 1 2 0 0 0 1 3 1 0 0 1 1 2 0 0 0 1 3 1 0 0 1 1 0 1 1 1 1 1 1 1 1 1	749 927 1035 1121 1066 1157 1115 1214
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU 7:00 AM 52 138 17 0 111 115 22 0 14 117 16 0 22 212 13 0 7:15 AM 53 145 22 0 8 147 31 0 16 127 20 0 21 323 14 0 7:30 AM 44 161 21 0 10 135 31 0 26 157 23 0 35 368 24 0 7:45 AM 47 164 33 0 23 161 25 0 20 196 24 0 26 380 22 0 8:00 AM 39 154 31 0 14 131 38 1 22 183 23 0 26 377 27 0 8:15 AM 55 159 35 0 16 146 29 0 36 219 30 0 20 389 23 0 8:30 AM 51 171 18 0 16 158 27 0 23 157 34 0 30 406 24 0 8:45 AM 53 150 33 0 12 157 31 0 35 191 27 0 43 451 31 0 9:00 AM 53 172 21 0 21 130 31 0 22 163 29 0 20 324 35 0 9:15 AM 48 171 29 0 14 141 25 0 30 189 39 0 38 346 28 0 9:30 AM 48 176 31 0 15 173 28 0 20 187 35 0 40 340 20 0	749 927 1035 1121 1066 1157 1115 1214
7:00 AM 52 138 17 0 111 115 22 0 144 117 16 0 22 212 13 0 7:15 AM 53 145 22 0 8 147 31 0 16 127 20 0 21 323 14 0 7:30 AM 44 161 21 0 10 135 31 0 26 157 23 0 35 368 24 0 7:45 AM 47 164 33 0 23 161 25 0 20 196 24 0 26 380 22 0 8:00 AM 39 154 31 0 14 131 38 1 22 183 23 0 26 37 27 0 8:15 AM 55 159 35 0 16 146 29 0 36 219 30 0 20 389 23 0 8:30 AM 51 171 18 0 16 158 27 0 23 157 34 0 30 406 24 0 8:30 AM 53 150 33 0 12 157 31 0 35 191 27 0 43 451 31 0 9:00 AM 53 172 21 0 21 130 31 0 22 163 29 0 20 324 35 0 9:15 AM 48 171 29 0 14 141 25 0 30 189 39 0 38 346 28 0 9:30 AM 48 176 31 0 15 173 28 0 20 187 35 0 40 340 20 0	749 927 1035 1121 1066 1157 1115 1214
7:15 AM 53 145 22 0 8 147 31 0 16 127 20 0 21 323 14 0 7:30 AM 44 161 21 0 10 135 31 0 26 157 23 0 35 368 24 0 7:45 AM 47 164 33 0 23 161 25 0 20 196 24 0 26 380 22 0 8:00 AM 39 154 31 0 14 131 38 1 22 183 23 0 26 377 27 0 8:15 AM 55 159 35 0 16 146 29 0 36 219 30 0 20 389 23 0 8:30 AM 51 171 18 0 16 158 27 0 23 157 34 0 30 406 24 0 36 28:45 AM 53 150 33 0 12 157 31 0 35 191 27 0 43 451 31 0 9:15 AM 48 171 29 0 14 141 25 0 30 189 39 0 38 346 28 0 9:30 AM 48 176 31 0 15 173 28 0 20 187 35 0 40 340 20 0	927 1035 1121 1066 1157 1115 1214
7:30 AM	1035 1121 1066 1157 1115 1214
7:45 AM 47 164 33 0 23 161 25 0 20 196 24 0 26 380 22 0 8:00 AM 39 154 31 0 14 131 38 1 22 183 23 0 26 377 27 0 8:15 AM 55 159 35 0 16 146 29 0 36 219 30 0 20 389 23 0 8:30 AM 51 171 18 0 16 158 27 0 23 157 34 0 30 406 24 0 8:45 AM 53 150 33 0 12 157 31 0 35 191 27 0 43 451 34 0 34 406 24 0 39 9 32 32 0 22 163 29<	1121 1066 1157 1115 1214 1021
8:00 AM	1066 1157 1115 1214 1021
8:15 AM 55 159 35 0 16 146 29 0 36 219 30 0 20 389 23 0 8:30 AM 51 171 18 0 16 158 27 0 23 157 34 0 30 406 24 0 16 158 27 0 23 157 34 0 30 406 24 0 17 18 18 150 33 0 12 157 31 0 35 191 27 0 43 451 31 0 18 150 31 17 17 18 18 17 18 18 18 18 18 18 18 18 18 18 18 18 18	1157 1115 1214 1021
8:30 AM 51 171 18 0 16 158 27 0 23 157 34 0 30 406 24 0 8:45 AM 53 150 33 0 12 157 31 0 35 191 27 0 43 451 31 0 9:00 AM 53 172 21 0 21 130 31 0 22 163 29 0 20 324 35 0 9:15 AM 48 171 29 0 14 141 25 0 30 189 39 0 38 346 28 0 9:30 AM 48 176 31 0 15 173 28 0 20 187 35 0 40 340 20 0	1115 1214 1021
8:45 AM 53 150 33 0 12 157 31 0 35 191 27 0 43 451 31 0 9:00 AM 53 172 21 0 21 130 31 0 22 163 29 0 20 324 35 0 9:15 AM 48 171 29 0 14 141 25 0 30 189 39 0 38 346 28 0 9:30 AM 48 176 31 0 15 173 28 0 20 187 35 0 40 340 20 0	1214 1021
9:00 AM 53 172 21 0 21 130 31 0 22 163 29 0 20 324 35 0 9:15 AM 48 171 29 0 14 141 25 0 30 189 39 0 38 346 28 0 9:30 AM 48 176 31 0 15 173 28 0 20 187 35 0 40 340 20 0	1021
9:15 AM 48 171 29 0 14 141 25 0 30 189 39 0 38 346 28 0 9:30 AM 48 176 31 0 15 173 28 0 20 187 35 0 40 340 20 0	
9:30 AM 48 176 31 0 15 173 28 0 20 187 35 0 40 340 20 0	1098
	1113
9.43 AW 43 133 31 0 12 130 26 0 10 101 42 0 34 2/2 20 0	958
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU	TOTAL
TOTAL VOLUMES: 588 1894 322 0 172 1730 346 1 280 2067 342 0 355 4188 289 0	12574
APPROACH %'s: 20.97% 67.55% 11.48% 0.00% 7.65% 76.92% 15.38% 0.04% 10.41% 76.87% 12.72% 0.00% 7.35% 86.67% 5.98% 0.00%	
PEAK HR: 08:00 AM - 09:00 AM	TOTAL
PEAK HR VOL : 198 634 117 0 58 592 125 1 116 750 114 0 119 1623 105 0	4552
PEAK HR FACTOR: 0.900 0.927 0.836 0.000 0.906 0.937 0.822 0.250 0.806 0.856 0.838 0.000 0.692 0.900 0.847 0.000 0.953 0.965 0.860 0.860 0.860	0.937
0.953 0.965 0.860 0.880	
NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND	
PM 1 2 0 0 1 2 0 0 1 2 0 0 1 3 1 0	
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU	TOTAL
3:00 PM 55 114 24 0 25 147 32 0 24 285 46 0 30 187 19 0	988
3:15 PM 53 143 21 0 21 133 32 0 39 264 46 0 36 175 27 0	990
3:30 PM 51 139 23 0 13 161 18 0 26 314 46 0 42 172 20 0	1025
3:45 PM 53 132 26 0 20 145 16 0 22 290 47 0 29 176 21 0	977
4:00 PM 52 115 19 0 23 174 15 0 33 383 52 0 25 200 14 0	1105
4:15 PM 51 122 27 0 19 139 21 0 32 311 49 0 40 190 12 1 4:30 PM 45 106 24 0 24 169 18 0 33 334 44 0 28 204 17 0	1014
	1046 1061
4:45 PM 54 110 21 0 14 155 20 0 51 336 49 0 30 207 14 0 5:00 PM 57 130 22 0 19 157 19 0 34 318 59 0 31 209 14 0	1069
5.00 rm 57 150 22 0 17 131 17 0 34 316 37 0 31 207 14 0 5.15 rm 52 133 20 0 22 149 12 0 43 348 45 0 30 237 10 0	1101
5:30 PM 55 120 16 0 14 136 11 0 56 338 57 0 33 194 9 0	1039
5:45 PM 41 135 20 0 15 137 23 0 51 333 62 0 23 204 5 0	1049
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU	TOTAL
	TOTAL 12464
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU	
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU TOTAL VOLUMES: 619 1499 263 0 229 1802 237 0 444 3854 602 0 377 2355 182 1 APPROACH %'s: 26.00% 62.96% 11.05% 0.00% 10.10% 79.45% 10.45% 0.00% 9.06% 78.65% 12.29% 0.00% 12.93% 80.79% 6.24% 0.03% PEAK HR: 04:30 PM - 05:30 PM	
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU	12464
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU TOTAL VOLUMES: 619 1499 263 0 229 1802 237 0 444 3854 602 0 377 2355 182 1 APPROACH %'s: 26.00% 62.96% 11.05% 0.00% 10.10% 79.45% 10.45% 0.00% 9.06% 78.65% 12.29% 0.00% 12.93% 80.79% 6.24% 0.03% PEAK HR: 04:30 PM - 05:30 PM	12464 TOTAL

TOTAL

532 2911 349 3792

TOTAL

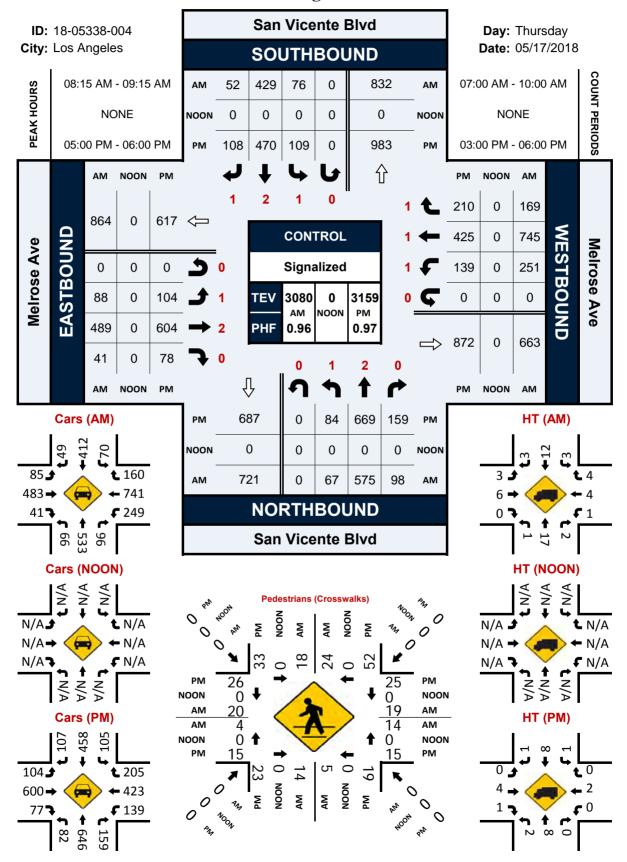
STREET: North/South	San Vice	nte Blvd										
East/West	Melrose A	Ave										
Day:	Thursday	г	Date:	05/17/2	2018	Weather:		SUNNY				
Hours:					Chekrs:	NDS						
School Day:		Yes				I/S CO	DE					
	N/B		S/I	3		E/B		_	W/B			
DUAL- WHEELED BIKES BUSES	84 27 90		8° 2:	5		53 15 1			50 29 28			
	N/B	TIME	S/I	TIME		E/B	TIME	_	W/B	TIME		
AM PK 15 MIN	211	8.45	163	8.15		182	9.15		319	8.15		
PM PK 15 MIN	244	17.00	240	15.00		211	17.45		203	17.30		
AM PK HOUR	802	8.45	578	9.00		678	9.00		1227	7.45		
PM PK HOUR	912	17.00	799	15.00		786	17.00		774	17.00		
NORTHBOUND Ap	proach			SOUTH	BOUND Appr	oach			,	TOTAL	XING S/L	XING N/L
Hours Lt 7-8 5 8-9 5 9-10 7 15-16 6 16-17 5 17-18 8	6 569 4 615 2 558 1 625 4 669	Rt 7 49 101 102 141 113 159	70tal 537 726 791 761 789 912	Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 54 85 71 119 117 109	Th 247 419 444 608 528 470	Rt 78 58 63 72 88 108	Total 379 562 578 799 733 687	- - - -	N-S 916 1288 1369 1560 1522 1599	Ped Sch 17 0 22 0 18 0 69 6 48 2 38 4	Ped Sch 28 3 40 3 44 4 72 2 85 3 83 2 352 17
EASTBOUND Appr	oach		<u></u>	WESTB	OUND Appro	ach			,	TOTAL	XING W/L	XING E/L
Hours Lt 7-8 4 8-9 7 9-10 11 15-16 7 16-17 11 17-18 10	7 471 7 493 8 581 0 534	Rt 7 23 35 68 68 77 78	297 583 678 727 721 786	Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 155 283 185 120 125 139	Th 816 753 664 424 354 425	Rt 147 170 173 181 208 210	Total 1118 1206 1022 725 687 774	- - -	E-W 1415 1789 1700 1452 1408 1560	Ped Sch 22 0 29 0 31 0 73 1 49 0 37 4	Ped Sch 11 1 24 0 31 0 45 1 23 1 37 3

1007 3436 1089 5532

9324

241 5 171 6

San Vicente Blvd & Melrose Ave



Intersection Turning Movement Count

Location: San Vicente Blvd & Melrose City: Los Angeles Control: Signalized Project ID: 18-05338-004 Date: 5/17/2018

								10	tal								
NS/EW Streets:		San Vice	nte Blvd			San Vicer	nte Blvd			Melrose	e Ave			Melros	e Ave		
		NORTH	IBOUND			SOUTH	BOUND			EASTB	OUND			WESTE	BOUND		
AM	1	2	0	0	1	2	1	0	1	2	0	0	1	1	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	10	98	9	0	11	48	20	0	9	29	4	0	25	211	25	0	499
7:15 AM	18	80	13	0	14	56	22	0	10	52	4	0	30	210	42	0	551
7:30 AM	10	96	11	0	12	68	15	0	12	71	6	0	45	195	32	0	573
7:45 AM	12	164	16	0	17	75	21	0	15	76	9	0	55	200	48	0	708
8:00 AM	7	152	24	0	22	101	21	0	22	94	6	0	86	177	41	0	753
8:15 AM 8:30 AM	18	115 136	24 29	0	31 18	121	11 14	0	12 26	139 110	12 8	0	79 66	200 187	40 48	0	802
8:30 AM 8:45 AM	10 21	166	29	0	18	108 89	12	0	26 17	128	9	0	52	187	48 41	0	760 762
9:00 AM	18	158	21	0	13	111	15	0	33	112	12	0	54	169	40	0	756
9:15 AM	20	162	27	0	24	112	13	0	31	136	15	0	46	160	44	0	790
9:30 AM	18	141	26	0	16	114	18	0	34	111	17	0	47	170	51	0	763
9:45 AM	18	154	28	0	18	107	17	0	19	134	24	0	38	165	38	0	760
7.10744								ŭ				ŭ	00	100	00	ŭ	700
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	180	1622	252	0	210	1110	199	0	240	1192	126	0	623	2233	490	0	8477
APPROACH %'s:	8.76%	78.97%	12.27%	0.00%	13.82%	73.07%	13.10%	0.00%	15.40%	76.51%	8.09%	0.00%	18.62%	66.74%	14.64%	0.00%	
PEAK HR:		08:15 AM -															TOTAL
PEAK HR VOL :	67	575	98	0	76	429	52	0	88	489	41	0	251	745	169	0	3080
PEAK HR FACTOR :	0.798	0.866	0.845	0.000	0.613	0.886	0.867	0.000	0.667	0.879	0.854	0.000	0.794	0.931	0.880	0.000	0.960
		0.8	77			0.8	54			0.94	18			0.9	13		
PM	1	NORTH	IBOUND	0	1	SOUTH	BOUND	0	1	EASTB	OUND	0	1	WESTE	BOUND	0	
PM	1 NI	NORTH 2	IBOUND 0	O NIII	1	SOUTH 2	BOUND 1	0	1 FI	EASTB 2	OUND 0	0	1 WI	WESTE	BOUND 1	0 WII	TOTAL
	NL	NORTH 2 NT	IBOUND 0 NR	NU	SL	SOUTH 2 ST	BOUND 1 SR	SU	EL	EASTB 2 ET	OUND 0 ER	EU	WL	WESTE 1 WT	BOUND 1 WR	WU	TOTAL
3:00 PM		NORTH 2	IBOUND 0 NR 46		SL 38	SOUTH 2	BOUND 1 SR 15			EASTB 2	OUND 0 ER 13			WESTE	BOUND 1 WR 37		TOTAL 792 759
	NL 16	NORTH 2 NT 136	IBOUND 0 NR	NU 0	SL	SOUTH 2 ST 187	BOUND 1 SR	SU 0	EL 28	EASTB 2 ET 138	OUND 0 ER	EU 0	WL 28	WESTE 1 WT 110	BOUND 1 WR	WU 0	792
3:00 PM 3:15 PM	NL 16 15	NORTH 2 NT 136 127	0 NR 46 31 22 42	0 0	SL 38 24 25 32	SOUTH 2 ST 187 150 138 133	BOUND 1 SR 15 23 15 19	SU 0 0	28 11 23 16	EASTB 2 ET 138 155	OUND 0 ER 13 23 17 15	0 0	WL 28 30	WESTE 1 WT 110 114	BOUND 1 WR 37 56 44 44	0 0	792 759
3:00 PM 3:15 PM 3:30 PM	NL 16 15 14	NORTH 2 NT 136 127 144	BOUND 0 NR 46 31 22 42 24	0 0 0	SL 38 24 25 32 29	SOUTH 2 ST 187 150 138	BOUND 1 SR 15 23 15	0 0 0	28 11 23	EASTB 2 ET 138 155 112	OUND 0 ER 13 23 17	0 0 0	WL 28 30 33	WESTE 1 WT 110 114 100	37 56 44	0 0 0	792 759 687
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM	NL 16 15 14 17 13	NORTH 2 NT 136 127 144 151 170 141	BOUND 0 NR 46 31 22 42 24 36	NU 0 0 0 0 0	SL 38 24 25 32 29 35	SOUTHI 2 ST 187 150 138 133 159 135	BOUND 1 SR 15 23 15 19 18 24	SU 0 0 0 0	EL 28 11 23 16 29 19	EASTB 2 ET 138 155 112 176 148 126	OUND 0 ER 13 23 17 15 24 21	EU 0 0 0 0 0	WL 28 30 33 29 30 32	WESTE 1 WT 110 114 100 100 90 89	37 56 44 44 45 56	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM	NL 16 15 14 17 13 12 18	NORTH 2 NT 136 127 144 151 170 141 155	BOUND 0 NR 46 31 22 42 24 36 26	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30	SOUTHI 2 ST 187 150 138 133 159 135 131	BOUND 1 SR 15 23 15 19 18 24 23	SU 0 0 0 0 0	EL 28 11 23 16 29 19 30	EASTB 2 ET 138 155 112 176 148 126 131	OUND 0 ER 13 23 17 15 24 21 17	EU 0 0 0 0 0	WL 28 30 33 29 30 32 33	WESTE 1 WT 110 114 100 100 90 89 79	37 56 44 45 56 58	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 16 15 14 17 13 12 18 8	NORTH 2 NT 136 127 144 151 170 141 155 159	BOUND 0 NR 46 31 22 42 24 36 26 27	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23	SOUTH 2 ST 187 150 138 133 159 135 131	BOUND 1 SR 15 23 15 19 18 24 23 23	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32	EASTB 2 ET 138 155 112 176 148 126 131 129	OUND 0 ER 13 23 17 15 24 21 17 15	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30	WESTE 1 WT 110 114 100 100 90 89 79 96	37 56 44 44 45 56 58 49	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 16 15 14 17 13 12 18 8 22	NORTH 2 NT 136 127 144 151 170 141 155 159 172	BOUND 0 NR 46 31 22 42 24 36 26 27 50	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23	SOUTH 2 ST 187 150 138 133 159 135 131 103	BOUND 1 SR 15 23 15 19 18 24 23 23 31	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27	EASTB 2 ET 138 155 112 176 148 126 131 129 143	OUND 0 ER 13 23 17 15 24 21 17 15 25	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31	WESTE 1 WT 110 114 100 100 90 89 79 96 104	37 56 44 44 45 56 58 49 60	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM	NL 16 15 14 17 13 12 18 8 22 26	NORTH 2 NT 136 127 144 151 170 141 155 159 172 179	BOUND 0 NR 46 31 22 42 24 36 26 27 50 35	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26	SOUTH 2 ST 187 150 138 133 159 135 131 103 123 141	BOUND 1 SR 15 23 15 19 18 24 23 23 31 22	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129	OUND 0 ER 13 23 17 15 24 21 17 15 25 19	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37	WESTE 1 WT 110 114 100 100 90 89 79 96 104 102	37 56 44 44 45 56 58 49 60 57	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813
3:00 PM 3:15 PM 3:30 PM 3:345 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 16 15 14 17 13 12 18 8 22 26 16	NORTH 2 NT 136 127 144 151 170 141 155 159 172 179 164	BOUND 0 NR 46 31 22 42 24 36 26 27 50 35 39	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26 30	SOUTH 2 ST 187 150 138 133 159 135 131 103 123 141 95	BOUND 1 SR 15 23 15 19 18 24 23 23 31 22 30	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40 24	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129 150	OUND 0 ER 13 23 17 15 24 21 17 15 25 19 18	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37 38	WESTE 1 WT 110 114 100 100 90 89 79 96 104 102 113	37 56 44 44 45 56 58 49 60 57 52	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813 769
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM	NL 16 15 14 17 13 12 18 8 22 26	NORTH 2 NT 136 127 144 151 170 141 155 159 172 179	BOUND 0 NR 46 31 22 42 24 36 26 27 50 35	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26	SOUTH 2 ST 187 150 138 133 159 135 131 103 123 141	BOUND 1 SR 15 23 15 19 18 24 23 23 31 22	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129	OUND 0 ER 13 23 17 15 24 21 17 15 25 19	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37	WESTE 1 WT 110 114 100 100 90 89 79 96 104 102	37 56 44 44 45 56 58 49 60 57	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813
3:00 PM 3:15 PM 3:30 PM 3:345 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 16 15 14 17 13 12 18 8 22 26 16 20	NORTH 2 NT 136 127 144 151 170 141 155 159 172 179 164 154	BOUND 0 NR 46 31 22 42 24 36 26 27 50 35 39 35	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26 30 24	SOUTH 2 ST 187 150 138 133 159 135 131 103 123 141 95 111	BOUND 1 SR 15 23 15 19 18 24 23 31 22 30 25	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40 24 13	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129 150 182	OUND 0 ER 13 23 17 15 24 21 17 15 25 19 18 16	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37 38 33	WESTE 1 110 1110 1114 1000 90 89 79 96 104 102 113 106	30UND 1 WR 37 56 44 45 56 58 49 60 57 52 41	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813 769 760
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 16 15 14 17 13 12 18 8 22 26 16 20 NL	NORTH 2 NT 136 127 144 151 170 141 155 159 172 179 164 154 NT	BOUND 0 NR 46 31 22 42 24 36 26 27 50 35 39 35	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26 30 24	SOUTH 2 2 ST 187 150 138 133 159 135 131 103 123 141 95 111	BOUND 1 SR 15 15 19 18 24 23 23 31 31 22 30 25 SR	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40 24 13	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129 150 182 ET	OUND 0 ER 13 23 17 15 24 21 17 15 25 19 18 16 ER	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37 38 33 WL	WESTE 1 10 110 110 100 100 90 89 79 96 104 102 113 106 WT	30UND 1 WR 37 56 44 44 45 56 58 49 60 57 52 41	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813 769 760
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:30 PM 5:15 PM 5:30 PM 5:45 PM	NL 16 15 14 17 13 12 18 8 22 26 16 20	NORTH 2 NT 136 127 144 151 170 141 155 159 172 179 164 154	BOUND 0 NR 46 31 22 42 24 26 26 26 27 50 35 38 NR 413	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26 30 24	SOUTH 2 ST 187 150 138 133 159 135 131 103 123 141 95 111	BOUND 1 SR 15 23 15 19 18 24 23 31 22 30 25	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40 24 13	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129 150 182 ET 1719	OUND 0 ER 13 23 17 15 24 21 17 15 25 19 18 16	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37 38 33	WESTE 1 110 1110 1114 1000 90 89 79 96 104 102 113 106	30UND 1 WR 37 56 44 45 56 58 49 60 57 52 41	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813 769 760
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 16 15 14 17 13 12 18 8 22 26 16 20 NL 197 8.00%	NORTH 2 NT 136 127 144 151 170 141 155 179 179 164 154 NT 1852	BOUND 0 NR 46 31 22 42 42 36 26 27 50 35 39 35 NR 413 16.77%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26 30 24 SL 345	SOUTH 2 ST 187 150 138 133 159 135 131 103 123 141 95 111 ST 1606	BOUND 1 SR 15 23 15 19 18 24 23 23 31 22 5 SR 268	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40 24 13 EL 292	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129 150 182 ET	OUND 0 ER 13 23 17 15 24 21 17 15 25 19 18 16 ER 223	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37 38 33 WL 384	WESTE 1 110 1114 1000 1000 900 899 96 1004 1002 1113 1006 WT 1203	30UND 1 WR 37 56 44 44 45 56 58 49 60 57 52 41 WR 599	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813 769 760
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:15 PM 4:30 PM 4:345 PM 5:00 PM 5:30 PM 5:30 PM 5:45 PM	NL 16 15 14 17 13 12 18 8 22 26 16 20 NL 197 8.00%	NORTH 2 NT 136 127 144 151 170 141 155 159 172 179 164 154 NT 1852 75.22%	BOUND 0 NR 46 31 22 42 42 36 26 27 50 35 39 35 NR 413 16.77%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26 30 24 SL 345	SOUTH 2 ST 187 150 138 133 159 135 131 103 123 141 95 111 ST 1606	BOUND 1 SR 15 23 15 19 18 24 23 23 31 22 5 SR 268	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40 24 13 EL 292	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129 150 182 ET 1719	OUND 0 ER 13 23 17 15 24 21 17 15 25 19 18 16 ER 223	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37 38 33 WL 384	WESTE 1 110 1114 1000 1000 900 899 96 1004 1002 1113 1006 WT 1203	30UND 1 WR 37 56 44 44 45 56 58 49 60 57 52 41 WR 599	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813 769 760 TOTAL 9101
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	NL 16 15 14 17 13 12 18 8 22 26 16 20 NL 197 8.00%	NORTH 2 NT 136 127 144 151 170 141 155 159 172 179 164 154 NT 1852 75.22% 05:00 PM -	BOUND 0 NR 46 46 31 22 42 42 36 26 27 50 35 NR 413 16.77% 06:00 PM	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26 30 24 SL 345 15.55%	SOUTHI 2 ST 187 150 138 133 159 135 131 103 123 141 95 111 ST 1606 72.37%	BOUND 1 SR 15 23 15 19 18 24 23 31 22 23 30 25 SR 268 12.08%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40 24 13 EL 292 13.07%	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129 150 182 ET 1719 76.95%	OUND 0 ER 13 23 17 15 24 21 17 15 25 19 18 16 ER 223 9.98%	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37 38 33 WL 384 17.57%	WESTE 1 WT 110 114 100 100 90 89 79 96 104 102 113 106 WT 1203 55.03%	30UND 1 WR 37 56 44 44 45 56 58 49 60 57 52 41 WR 599 27.40%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813 769 760 TOTAL 9101
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR: SPEAK HR: SPEAK HR VOL:	NL 16 15 14 17 13 12 18 8 22 26 16 20 NL 197 8.00%	NORTH 2 NT 136 127 144 151 170 141 155 159 172 179 164 154 NT 1852 75.22% 05:00 PM -669	BOUND 0 NR 46 31 22 42 42 24 36 26 27 50 35 NR 413 16,77% 06:00 PM 159 0.795	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 38 24 25 32 29 35 30 23 29 26 30 24 SL 345 15.55%	SOUTHI 2 ST 187 150 138 133 159 135 131 103 123 141 95 111 ST 1606 72.37%	BOUND 1 SR 15 123 15 19 18 24 23 31 22 30 25 SR 268 12.08%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 28 11 23 16 29 19 30 32 27 40 41 13 EL 292 13.07%	EASTB 2 ET 138 155 112 176 148 126 131 129 143 129 150 182 ET 1719 76.95%	OUND 0 ER 13 23 23 17 15 24 21 17 15 25 19 18 16 ER 223 9.98% 78 0.780	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 28 30 33 29 30 32 33 30 31 37 37 38 33 WL 384 17.57%	WESTE 1 WT 110 1114 100 100 90 89 79 96 104 102 113 106 WT 1203 55.03%	SOUND 1 WR 37 56 44 44 45 56 58 49 60 57 52 41 WR 599 27.40% 210 0.875	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	792 759 687 774 779 726 731 694 817 813 769 760 TOTAL 9101

TOTAL

903 5709 154 6766

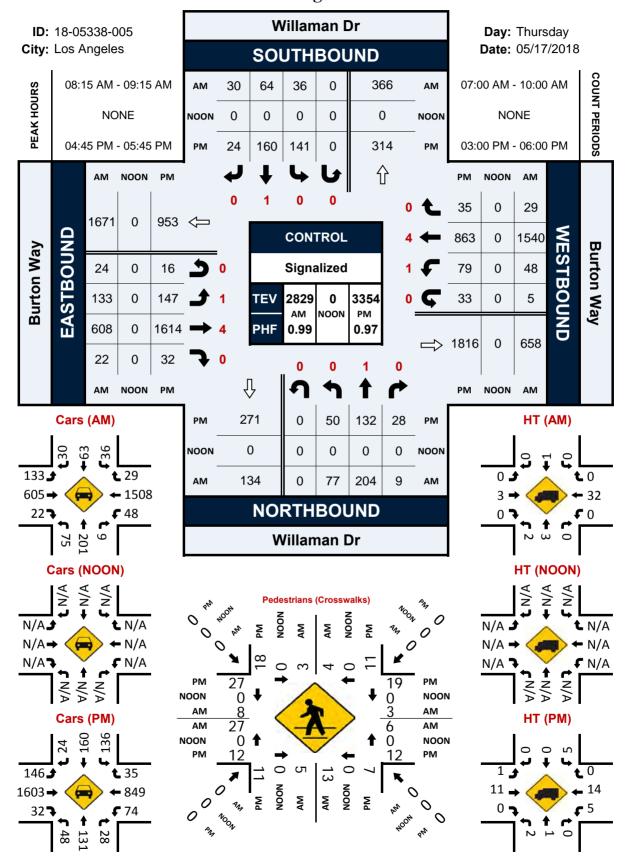
TOTAL

STREET: North/South	Willaman	n Dr											
East/West	Burton W	/ay											
Day:	Thursday	Е	ate:		05/17/2	018	Weather:		SUNNY				
Hours:					(Chekrs:	NDS		-				
School Day:		Yes		-			I/S CO	DE					
	N/B		_	S/B			E/B		_	W/B			
DUAL- WHEELED BIKES	28 29			21 5			55 29			160 27			
BUSES	0			0			0			1			
	N/B	TIME		S/B	TIME		E/B	TIME	_	W/B	TIME		
AM PK 15 MIN	76	8.15		42	8.30		214	8.45		420	8.30		
PM PK 15 MIN	67	16.00		93	17.15		464	17.30		278	17.30		
AM PK HOUR	290	7.45		142	8.30		826	8.45		1622	8.15		
PM PK HOUR	244	15.30		343	16.30		1809	16.45		1018	17.00		
NORTHBOUND A	Approach			5	SOUTHE	OUND Appr	oach			•	TOTAL	XING S/L	XING N/L
Hours L	t Th	Rt T	otal 189		Hours 7-8	Lt 17	Th 37	Rt 31	Total 85	Г	N-S 274	Ped Sch	Ped Sch
8-9 9-10	80 197 65 179	8 14	285 258	ě	8-9 9-10	33 27	62 69	39 31	134 127		419 385	19 0 5 0	7 1 2 0
15-16	61 136	16	213		15-16	89	112	43	244		457	20 0	20 0
16-17 17-18	46 153 52 133	20 35	219 220		16-17 17-18	129 114	140 167	24 33	293 314		512 534	18 1 17 0	30 0 28 1
TOTAL	352 933	99	1384		ГОТАL	409	587	201	1197	Ī	2581	93 1	97 3
EASTBOUND Ap	proach			,	WESTBO	OUND Appro	ach			,	TOTAL	XING W/L	XING E/L
Hours L	t Th	Rt T	otal 427		Hours 7-8	Lt 30	Th 1284	Rt	Total 1332	Г	E-W 1759	Ped Sch	Ped Sch
8-9	140 578	24	742	ě	8-9	51	1520	30	1601		2343	38 2	10 1
	164 612 179 1174	27 40	803 1393		9-10 15-16	50 90	1306 825	21 44	1377 959	}	2180 2352	14 0 43 1	1 0 16 0
	167 1428 159 1595	16 36	1611 1790		16-17 17-18	114 98	725 889	27 31	866 1018		2477 2808	35 2 37 2	29 2 27 3

433 6549 171 7153

13919 188 8 92 7

Willaman Dr & Burton Way



Intersection Turning Movement Count

Location: Willaman Dr & Burton Way City: Los Angeles Control: Signalized

Project ID: 18-05338-005 Date: 5/17/2018

Total NS/EW Streets: Willaman Dr Willaman Dr Burton Way Burton Way NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND **AM** TOTAL NU SU EU WL WU WT 387 466 588 592 644 705 707 706 7:30 AM 7:45 AM 8:00 AM 24 31 28 8:15 AM 8:30 AM 8:45 AM 389 394 372 9:00 AM 9:15 AM 9:30 AM 149 151 161 151 12 13 10 8 45 41 31 23 19 20 14 16 0 5 6 293 0 11 12 9:45 AM NT 511 69.81% NU 0 0.00 SU 0 0.00 EL 334 16.949 TOTAL 7360 SL 77 TOTAL VOLUMES : APPROACH %'s : PEAK HR : PEAK HR VOL : 101 29.19% 4110 95.36% TOTAL 2829 133 PEAK HR FACTOR 0.000 0.739 0.802 0.879 0.563 0.000 0.818 0.727 0.750 0.916 0.611 0.600 0.923 0.977 0.725 0.417 0.995

		NORTH	DOUND			300111	BOUND			EASID	DOUND			WESTE	OUND		
PM	0	1	0	0	0	1	0	0	1	4	0	0	1	4	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
3:00 PM	14	33	4	0	19	22	11	1	36	261	10	2	17	240	11	2	683
3:15 PM	9	31	5	0	14	21	13	0	42	291	7	6	22	192	4	6	663
3:30 PM	23	37	2	0	30	27	8	0	40	310	9	7	7	200	15	9	724
3:45 PM	15	35	5	0	25	42	11	0	39	312	14	7	22	193	14	5	739
4:00 PM	12	49	6	0	24	35	6	0	37	338	3	5	27	169	4	9	724
4:15 PM	13	40	7	0	23	41	6	0	44	326	2	5	16	173	5	5	706
4:30 PM	10	36	5	0	37	34	9	0	34	379	8	7	18	198	10	7	792
4:45 PM	11	28	2	0	45	30	3	0	32	385	3	3	25	185	8	7	767
5:00 PM	13	30	10	0	35	47	10	0	36	413	6	5	21	222	9	9	866
5:15 PM	16	37	10	0	42	45	6	0	39	407	11	5	16	216	9	5	864
5:30 PM	10	37	6	0	19	38	5	0	40	409	12	3	17	240	9	12	857
5:45 PM	13	29	9	0	18	37	12	0	29	366	7	2	10	211	4	8	755
<u> </u>																	
i	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	159	422	71	0	331	419	100	1	448	4197	92	57	218	2439	102	84	9140
APPROACH %'s:	24.39%	64.72%	10.89%	0.00%	38.90%	49.24%	11.75%	0.12%	9.35%	87.55%	1.92%	1.19%	7.67%	85.79%	3.59%	2.95%	
PEAK HR :)4:45 PM -															TOTAL
PEAK HR VOL :	50	132	28	0	141	160	24	0	147	1614	32	16	79	863	35	33	3354
PEAK HR FACTOR :	0.781	0.892	0.700	0.000	0.783	0.851	0.600	0.000	0.919	0.977	0.667	0.800	0.790	0.899	0.972	0.688	0.968
		0.8	33			0.8	74			0.9	75			0.90)8		200

TOTAL

332 4383 627 5342

TOTAL

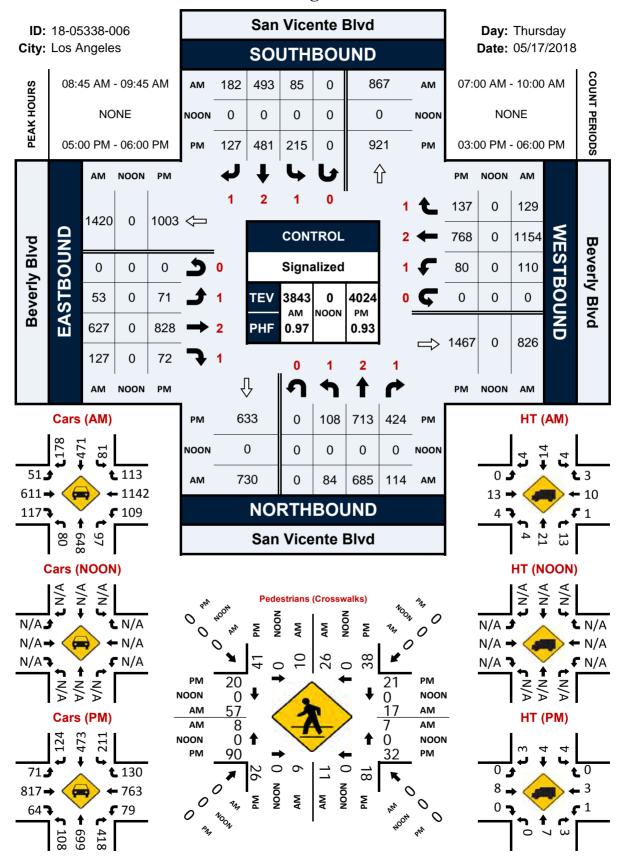
558 5762 770 **7090**

12432

631 23 171 2

STREET: North/South	San Vicente Blvd					
East/West	Beverly Blvd					
Day:	Thursday Date:	05/17/2018	Weather: SUNNY			
Hours:		Chekrs:	NDS			
School Day:	Yes		I/S CODE			
DUAL-	N/B	S/B	E/B	W/B		
WHEELED BIKES BUSES	126 31 78	78 24 38	86 14 63	76 25 59		
	N/B TIME	S/B TIME	E/B TIME	W/B TIME		
AM PK 15 MIN	228 9.15	209 8.30	245 7.45	382 7.30		
PM PK 15 MIN	341 17.15	246 15.15	297 15.00	277 16.00		
AM PK HOUR	883 8.45	789 9.00	870 7.45	1459 7.15		
PM PK HOUR	1245 17.00	913 15.00	1082 15.00	1027 15.15		
NORTHBOUND A _I	pproach	SOUTHBOUND App	proach	TOTAL	XING S/L	XING N/L
8-9 9-10 15-16	95 666 363 1124		4 647 102 913 4 569 107 850	N-S 1170 1589 1666 1845 1974 2068	Ped Sch 31 0 27 1 14 0 42 1 75 0 44 0	Ped Sch 33 2 42 3 26 1 38 3 59 2 72 7
TOTAL 55	54 3711 1378 5643	TOTAL 79	3 3060 816 4669	10312	233 2	270 18
EASTBOUND Appr	roach	WESTBOUND Appr	roach	TOTAL	XING W/L	XING E/L
8-9 9-10 15-16 16-17	Th Rt Total 29 510 102 641 50 681 112 843 17 638 128 813 66 887 119 1082 59 839 94 992 71 828 72 971	9-10 10 15-16 8 16-17 6	1 1119 144 1354	E-W 2060 2197 2170 2090 1959	Ped Sch 106 2 108 5 54 3 109 0 154 3 100 10	Ped Sch 24 0 38 0 23 0 19 0 14 2 53 0

San Vicente Blvd & Beverly Blvd



Intersection Turning Movement Count

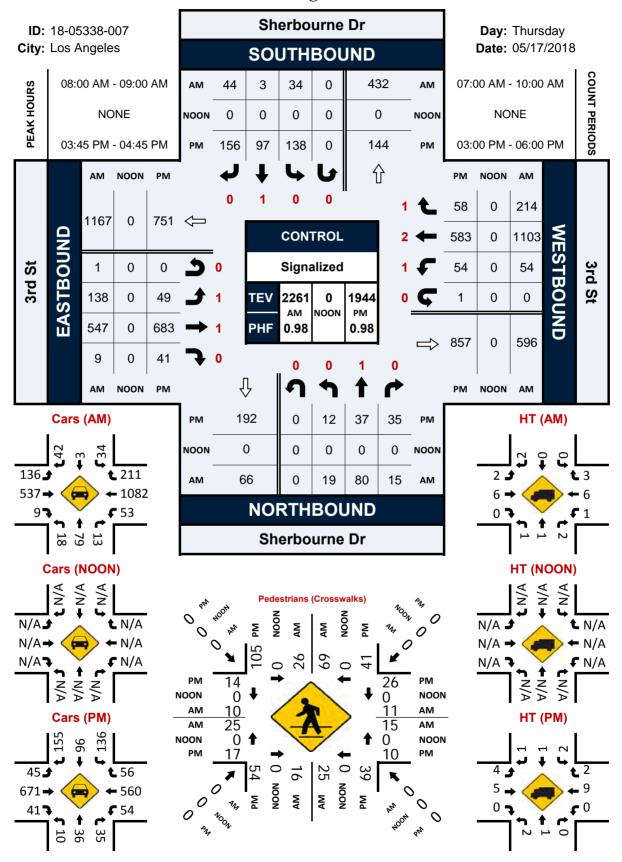
City: Los Angeles
Control: Signalized Project ID: 18-05338-006 Date: 5/17/2018

	Signalized							To	tal					Date.	5/17/2018		
NS/EW Streets:		San Vicer	ata Dhud			San Vicer	nto Divid	10	lai	Beverly	Divid			Beverly	Dhad		
NS/EW Streets:														,			
0.04		NORTH				SOUTH				EASTB				WESTE			
AM	1	2	1	0	1	2	1	0	1	2	1	0	1	2	.1	0	
7:00 AM	NL 20	NT 105	NR 16	NU 0	SL 8	ST 69	SR 30	SU 0	EL	67	ER 20	EU 0	WL 25	WT 258	WR 24	WU 0	TOTAL 647
7:00 AM 7:15 AM	20 16	105	16	0	8 10	69	30 29	0	5 8	93	20 15	0	25 41	258 325	24 15	0	739
7:30 AM	17	107	29	0	15	87	36	0	2	155	31	0	29	325	28	0	857
7:45 AM	12	165	38	Ö	19	108	51	Ö	14	195	36	0	36	285	28	0	987
8:00 AM	24	156	35	0	29	120	41	0	9	170	25	0	19	284	44	0	956
8:15 AM	27	134	34	0	20	141	40	0	11	191	27	0	19	264	27	0	935
8:30 AM	21	155	26	0	17	151	41	0	12	155	25	0	23	274	38	0	938
8:45 AM	17	171	26	0	14	112	37	0	18	165	35	0	30	297	35	0	957
9:00 AM	23	174	28	0	27	110	53	0	14	146	33	0	25	284	31	0	948
9:15 AM 9:30 AM	24 20	171 169	33 27	0	21 23	137 134	48 44	0	12 9	162 154	27 32	0	32 23	295 278	28 35	0	990 948
9:30 AM 9:45 AM	20 25	158	25	0	23 37	125	30	0	12	176	36	0	23	267	36	0	948
7.43 AW	23	130	23	U	37	123	30	U	12	170	30	U	23	207	30	U	730
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	246	1768	328	0	240	1363	480	0	126	1829	342	0	325	3436	369	0	10852
APPROACH %'s :	10.50%	75.49%	14.01%	0.00%	11.52%	65.43%	23.04%	0.00%	5.49%	79.63%	14.89%	0.00%	7.87%	83.20%	8.93%	0.00%	
PEAK HR :		08:45 AM -															TOTAL
PEAK HR VOL :	84	685	114	0	85	493	182	0	53	627	127	0	110	1154	129	0	3843
PEAK HR FACTOR :	0.875	0.984	0.864	0.000	0.787	0.900	0.858	0.000	0.736	0.950	0.907	0.000	0.859	0.971	0.921	0.000	0.970
		0.96	58			0.92	22			0.92	25			0.96	02		
		NORTH	ROLIND			SOUTH	ROLIND			FASTR	OUND			WESTE	OUND		
PM	1	NORTH 2	BOUND 1	0	1	SOUTH 2	BOUND 1	0	1	EASTB 2	OUND 1	0	1	WESTE 2	OUND 1	0	
PM	1 NL	NORTH 2 NT		0 NU	1 SL	SOUTH 2 ST		0 SU	1 EL	EASTB 2 ET		0 EU	1 WL	WESTE 2 WT		0 WU	TOTAL
3:00 PM		2	1		SL 46	2 ST 170	1 SR 19		22	2	1 ER 38			2	1		994
3:00 PM 3:15 PM	NL 31 21	2 NT 132 116	1 NR 41 64	NU 0 0	SL 46 37	2 ST 170 177	1 SR 19 32	SU 0 0	22 20	2 ET 237 214	1 ER 38 32	0 0	WL 23 15	2 WT 203 206	1 WR 32 30	0 0	994 964
3:00 PM 3:15 PM 3:30 PM	NL 31 21 31	2 NT 132 116 141	1 NR 41 64 86	0 0 0	SL 46 37 41	2 ST 170 177 149	1 SR 19 32 22	0 0 0	22 20 12	2 ET 237 214 229	1 ER 38 32 24	0 0 0	23 15 24	2 WT 203 206 194	1 WR 32 30 30	0 0 0	994 964 983
3:00 PM 3:15 PM 3:30 PM 3:45 PM	NL 31 21 31 22	2 NT 132 116 141 175	1 NR 41 64 86 72	NU 0 0 0	SL 46 37 41 40	2 ST 170 177 149 151	1 SR 19 32 22 29	SU 0 0 0	22 20 12 22	2 ET 237 214 229 207	1 ER 38 32 24 25	0 0 0 0	WL 23 15 24 24	2 WT 203 206 194 185	1 WR 32 30 30 42	0 0 0 0	994 964 983 994
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM	NL 31 21 31 22 30	2 NT 132 116 141 175 158	1 NR 41 64 86 72 97	NU 0 0 0 0	SL 46 37 41 40 39	2 ST 170 177 149 151	1 SR 19 32 22 29 28	SU 0 0 0 0	22 20 12 22 14	2 ET 237 214 229 207 221	1 ER 38 32 24 25 28	0 0 0 0 0	WL 23 15 24 24 21	2 WT 203 206 194 185 227	1 WR 32 30 30 42 29	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM	NL 31 21 31 22 30 19	2 NT 132 116 141 175 158 170	1 NR 41 64 86 72 97 85	NU 0 0 0 0 0	SL 46 37 41 40 39 39	2 ST 170 177 149 151 152 149	1 SR 19 32 22 29 28 27	SU 0 0 0 0	22 20 12 22 14 21	2 ET 237 214 229 207 221 188	1 ER 38 32 24 25 28 20	EU 0 0 0 0 0	WL 23 15 24 24 21 19	2 WT 203 206 194 185 227 182	1 WR 32 30 30 42 29 31	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM	NL 31 21 31 22 30	2 NT 132 116 141 175 158	1 NR 41 64 86 72 97	NU 0 0 0 0	SL 46 37 41 40 39 39 51	2 ST 170 177 149 151 152 149 149	1 SR 19 32 22 29 28 27 25	SU 0 0 0 0	22 20 12 22 14	2 ET 237 214 229 207 221	1 ER 38 32 24 25 28 20 21	0 0 0 0 0	WL 23 15 24 24 21	2 WT 203 206 194 185 227	1 WR 32 30 30 42 29	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM	NL 31 21 31 22 30 19 29	2 NT 132 116 141 175 158 170 161	1 NR 41 64 86 72 97 85 100	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 46 37 41 40 39 39	2 ST 170 177 149 151 152 149	1 SR 19 32 22 29 28 27	SU 0 0 0 0 0	22 20 12 22 14 21 8	2 ET 237 214 229 207 221 188 193	1 ER 38 32 24 25 28 20	EU 0 0 0 0 0	WL 23 15 24 24 21 19 15	2 WT 203 206 194 185 227 182 179	1 WR 32 30 30 42 29 31 33	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950 964
3:00 PM 3:15 PM 3:30 PM 3:35 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 31 21 31 22 30 19 29 17 31 25	2 NT 132 116 141 175 158 170 161 177 180 201	1 NR 41 64 86 72 97 85 100 81 102 115	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 46 37 41 40 39 39 51 45 66 62	2 ST 170 177 149 151 152 149 149 119 130 134	1 SR 19 32 22 29 28 27 25 27 27 27 39	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22 20 12 22 14 21 8 16 20	2 ET 237 214 229 207 221 188 193 237 191 207	1 ER 38 32 24 25 28 20 21 25 24 13	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 23 15 24 24 21 19 15 12 16 19	2 WT 203 206 194 185 227 182 179 182 173 208	1 WR 32 30 30 42 29 31 33 37 38 42	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950 964 975 998 1083
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 31 21 31 22 30 19 29 17 31 25 22	2 NT 132 116 141 175 158 170 161 177 180 201 157	1 NR 41 64 86 72 97 85 100 81 102 115 100	NU 0 0 0 0 0 0 0 0	SL 46 37 41 40 39 39 51 45 66 62 44	2 ST 170 177 149 151 152 149 149 119 130 134 108	1 SR 19 32 22 29 28 27 25 27 27 27 39 29	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22 20 12 22 14 21 8 16 20 18	2 ET 237 214 229 207 221 188 193 237 191 207 207	1 ER 38 32 24 25 28 20 21 25 24 13 19	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 23 15 24 24 21 19 15 12 16 19 22	2 WT 203 206 194 185 227 182 179 182 173 208 191	1 WR 32 30 30 42 29 31 33 37 38 42 35	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950 964 975 998 1083 950
3:00 PM 3:15 PM 3:30 PM 3:35 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 31 21 31 22 30 19 29 17 31 25	2 NT 132 116 141 175 158 170 161 177 180 201	1 NR 41 64 86 72 97 85 100 81 102 115	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 46 37 41 40 39 39 51 45 66 62	2 ST 170 177 149 151 152 149 149 119 130 134	1 SR 19 32 22 29 28 27 25 27 27 27 39	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22 20 12 22 14 21 8 16 20	2 ET 237 214 229 207 221 188 193 237 191 207	1 ER 38 32 24 25 28 20 21 25 24 13	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 23 15 24 24 21 19 15 12 16 19	2 WT 203 206 194 185 227 182 179 182 173 208	1 WR 32 30 30 42 29 31 33 37 38 42	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950 964 975 998 1083
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 31 21 31 22 30 19 29 17 31 25 22 30	2 NT 132 116 141 175 158 170 161 177 180 201 157 175	1 NR 41 64 86 72 97 85 100 81 102 115 100 107	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 46 37 41 40 39 39 51 45 66 62 44 43	2 ST 170 177 149 151 152 149 119 130 134 108 109	1 SR 19 32 22 29 28 27 25 27 27 27 39 29 32	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22 20 12 22 14 21 8 16 20 18 16	2 ET 237 214 229 207 221 188 193 237 191 207 207 223	1 ER 38 32 24 25 28 20 21 25 24 13 19	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 23 15 24 24 21 19 15 12 16 19 22 23	2 WT 203 206 194 185 227 182 179 182 173 208 191 196	1 WR 32 30 30 42 29 31 33 37 38 42 35 22	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950 964 975 998 1083 950 993
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	NL 31 21 31 22 30 19 29 17 31 25 22 30 NL	2 NT 132 116 141 175 158 170 161 177 180 201 157 175	1 NR 41 64 86 72 97 85 100 81 102 115 100 107	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 46 37 41 40 39 39 51 45 66 62 44 43 SL	2 ST 170 177 149 151 152 149 149 119 130 134 108 109	1 SR 19 32 22 29 28 27 25 27 27 27 39 29 32	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22 20 12 22 14 21 8 16 20 18 16 17	2 ET 237 214 229 207 221 188 193 237 191 207 207 223	1 ER 38 32 24 25 28 20 21 25 24 13 19 16	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 23 15 24 24 21 19 15 12 16 19 22 23 WL	2 WT 203 206 194 185 227 182 179 182 173 208 191 196	1 WR 32 30 30 42 29 31 33 37 38 42 35 22	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950 964 975 998 1083 950 993
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	NL 31 21 31 22 30 19 29 17 31 25 22 30 NL 308	2 NT 132 116 141 175 158 170 161 177 180 201 157 175	1 NR 41 64 86 72 97 85 100 81 102 115 100 107 NR 1050	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 46 37 41 40 39 51 45 66 62 44 43 SL 553	2 ST 170 177 149 151 152 149 149 119 130 134 108 109	1 SR 19 32 22 29 28 27 25 27 27 27 39 29 32 SR 336	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22 20 12 22 14 21 8 16 20 18 16 17	2 ET 237 214 229 207 221 188 193 237 191 207 207 223 ET 2554	1 ER 38 32 24 25 28 20 21 25 24 13 19 16 ER 285	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 23 15 24 24 21 19 15 12 16 19 22 23 WL 233	2 WT 203 206 194 185 227 182 179 182 173 208 191 196	1 WR 32 30 30 30 42 29 31 33 37 38 42 35 22 WR 401	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950 964 975 998 1083 950 993
3:00 PM 3:15 PM 3:30 PM 3:34 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:30 PM 5:30 PM 5:45 PM	NL 31 21 31 22 30 19 17 31 25 22 30 NL 308 9.33%	2 NT 132 116 141 175 158 170 161 177 180 201 157 175 NT 1943 58.86%	1 NR 41 64 86 72 97 85 100 81 102 115 100 107 NR 1050 31.81%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 46 37 41 40 39 39 51 45 66 62 44 43 SL	2 ST 170 177 149 151 152 149 149 119 130 134 108 109	1 SR 19 32 22 29 28 27 25 27 27 27 39 29 32	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22 20 12 22 14 21 8 16 20 18 16 17	2 ET 237 214 229 207 221 188 193 237 191 207 207 223	1 ER 38 32 24 25 28 20 21 25 24 13 19 16	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 23 15 24 24 21 19 15 12 16 19 22 23 WL	2 WT 203 206 194 185 227 182 179 182 173 208 191 196	1 WR 32 30 30 42 29 31 33 37 38 42 35 22	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950 964 975 998 1083 950 993 TOTAL 11892
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	NL 31 21 31 22 30 19 17 31 25 22 30 NL 308 9.33%	2 NT 132 116 141 175 158 170 161 177 180 201 157 175 NT 1943 58.86%	1 NR 41 64 86 72 97 85 100 81 102 115 100 107 NR 1050	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 46 37 41 40 39 51 45 66 62 44 43 SL 553	2 ST 170 177 149 151 152 149 149 119 130 134 108 109	1 SR 19 32 22 29 28 27 25 27 27 27 39 29 32 SR 336	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22 20 12 22 14 21 8 16 20 18 16 17	2 ET 237 214 229 207 221 188 193 237 191 207 207 223 ET 2554	1 ER 38 32 24 25 28 20 21 25 24 13 19 16 ER 285	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 23 15 24 24 21 19 15 12 16 19 22 23 WL 233	2 WT 203 206 194 185 227 182 179 182 173 208 191 196	1 WR 32 30 30 30 42 29 31 33 37 38 42 35 22 WR 401	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	994 964 983 994 1044 950 964 975 998 1083 950 993

STREET: North/South	Sherbour	ne Dr										
East/West	3rd St											
Day:	Thursday		Date:		05/17/2	.018 Weath	er:	SUNNY				
Hours:					(Chekrs: NDS		_				
School Day:		Yes		-		I/S	CODE	-				
	N/B		_	S/B		E	В	_	W/B			
DUAL- WHEELED BIKES BUSES	16 9 0			26 6 0		2	6 3 3		82 12 94			
	N/B	TIME	_	S/B	TIME	E	в тімі	<u> </u>	W/B	TIME		
AM PK 15 MIN	39	8.15		36	9.45	20	4 9.3	0	365	7.30		
PM PK 15 MIN	23	15.45		130	17.00	20	3 16.3	0	205	15.45		
AM PK HOUR	132	7.30		119	9.00	73	0 8.4	5	1371	8.00		
PM PK HOUR	84	15.45		432	16.30	77	3 15.4	5	726	15.00		
NORTHBOUND Ap	proach				SOUTHI	BOUND Approach				TOTAL	XING S/L	XING N/L
8-9 1 9-10 15-16 1 16-17 1	Th 3 86 9 80 9 54 11 27 10 29 8 18	Rt 15 15 21 27 34 37	104 114 84 65 73 63		Hours 7-8 8-9 9-10 15-16 16-17 17-18	34 34 104	Rt 4 4 4 7 6 6 11 4 16 1 15	4 81 8 119 8 278 6 398	-	N-S 169 195 203 343 471 450	Ped Sch 15 3 40 1 58 4 87 4 78 7 97 2	Ped Sch 39 5 90 5 112 8 121 12 118 16 120 11
TOTAL 6	50 294	149	503		TOTAL	451 28	5 59	2 1328	1	1831	375 21	600 57
EASTBOUND Appr	roach				WESTBO	OUND Approach				TOTAL	XING W/L	XING E/L
16-17 4	547	Rt 6 9 35 32 38 24	Total 565 695 725 738 771 736		Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt Th 30 94 54 110 42 90 58 55 52 50 60 50	3 21- 11 16- 2 7- 5 4	4 1371 3 1106 6 726 8 665	-	E-W 1769 2066 1831 1464 1436 1411	Ped Sch 23 5 34 1 34 2 52 0 35 3 53 2	Ped Sch 12 2 24 2 36 0 41 1 28 1 45 2

TOTAL 568 3518 144 4230 TOTAL 296 4669 782 5747 9977 231 13 186 8

Sherbourne Dr & 3rd St



Intersection Turning Movement Count

Location: Sherbourne Dr & 3rd St City: Los Angeles Control: Signalized

Project ID: 18-05338-007 Date: 5/17/2018

Total

NS/EW Streets:		Sherbou	ırne Dr		Sherbourne Dr SOUTHBOUND					3rd	St			3rd	St		
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	BOUND		
AM	0	1	0	0	0	1	0	0	1	1	0	0	1	2	1	0	
7.00.444	NL 1	NT 15	NR 5	NU 0	SL 2	ST 0	SR 2	SU	EL 25	71	ER 0	EU 0	WL	WT 205	WR	WU 0	TOTAL
7:00 AM 7:15 AM	0	15	2	0	3	0	9	0	25 37	80	2	0	8	205	48 62	0	378 440
7:30 AM	1	25	3	0	8	2	18	0	27	138	2	0	11	293	61	0	589
7:45 AM	i	32	5	ő	8	2	11	0	43	138	2	Ö	7	225	57	0	531
8:00 AM	2	22	2	0	7	0	8	0	33	136	1	0	14	269	61	0	555
8:15 AM	6	26	7	0	7	1	10	0	41	133	6	1	11	264	56	0	569
8:30 AM	1	16	3	0	10	1	10	0	26	149	0	0	15	297	50	0	578
8:45 AM	10	16	3	0	10	1	16	0	38	129	2	0	14	273	47	0	559
9:00 AM 9:15 AM	1 3	17 16	5 7	0	9	0 8	10 17	0	31 38	139 134	3 11	0	9 15	279 221	45 37	0	548 514
9:30 AM	2	11	3	0	9	6	18	0	26	166	12	0	11	191	46	1	502
9:45 AM	3	10	6	0	10	3	23	0	29	124	9	2	6	210	35	0	470
7. 10 7			· ·				20				•	-	•	2.0	00	ŭ	.,,
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	31	220	51	0	89	24	152	0	394	1537	50	4	125	2950	605	1	6233
APPROACH %'s:	10.26%	72.85%	16.89%	0.00%	33.58%	9.06%	57.36%	0.00%	19.85%	77.43%	2.52%	0.20%	3.40%	80.14%	16.44%	0.03%	
PEAK HR :		- MA 00:80							400					4400			TOTAL
PEAK HR VOL :	19 0.475	80 0.769	15 0.536	0.000	34 0.850	3 0.750	44 0.688	0.000	138 0.841	547 0.918	9 0.375	1 0.250	54 0.900	1103 0.928	214 0.877	0.000	2261
PEAK HR FACTOR :	0.475	0.769		0.000	0.850	0.750		0.000	0.841	0.918		0.250	0.900	0.928		0.000	0.978
		0.7	31			0.7.	50			0.70	50			0.75	+/		
		NORTH				SOUTH				EASTB				WESTE			
PM	0	NORTH 1	BOUND 0	0	0	SOUTH 1	BOUND 0	0	1	EASTB 1	OUND 0	0	1	WESTE 2	BOUND 1	0	
	0 NL	NORTH 1 NT	BOUND 0 NR	NU	SL	SOUTH 1 ST	BOUND 0 SR	SU	EL	EASTB 1 ET	OUND	EU	WL	WESTE 2 WT	BOUND 1 WR	WU	TOTAL
3:00 PM	NL 1	NORTH 1 NT 3	BOUND 0 NR 11	NU 0	SL 24	SOUTH 1 ST 10	BOUND 0 SR 38	SU 0	EL 15	EASTB 1 ET 162	OUND 0 ER 7	EU 2	WL 10	WESTE 2 WT 140	BOUND 1 WR 20	WU 0	443
3:00 PM 3:15 PM	NL 1 4	NORTH 1 NT 3 6	BOUND 0 NR 11 4	0 0	SL 24 23	SOUTH 1 ST 10 16	BOUND 0 SR 38 21	0 0	EL 15 14	EASTB 1 ET 162 168	OUND 0 ER 7 6	EU 2 0	WL 10 14	WESTE 2 WT 140 151	80UND 1 WR 20 15	0 0	443 442
3:00 PM 3:15 PM 3:30 PM	NL 1	NORTH 1 NT 3 6 4	BOUND 0 NR 11	NU 0	SL 24 23 32	SOUTH 1 ST 10 16 12	BOUND 0 SR 38 21 31	0 0 0	EL 15 14 18	EASTB 1 ET 162 168 152	OUND 0 ER 7	EU 2	WL 10 14 17	WESTE 2 WT 140 151 137	80UND 1 WR 20 15	0 0 0	443 442 439
3:00 PM 3:15 PM	NL 1 4 2	NORTH 1 NT 3 6	BOUND 0 NR 11 4 7	0 0 0	SL 24 23	SOUTH 1 ST 10 16	BOUND 0 SR 38 21	0 0	EL 15 14	EASTB 1 ET 162 168	OUND 0 ER 7 6	2 0 0	WL 10 14	WESTE 2 WT 140 151	80UND 1 WR 20 15	0 0	443 442
3:00 PM 3:15 PM 3:30 PM 3:45 PM	NL 1 4 2 4	NORTH 1 NT 3 6 4 14	BOUND 0 NR 11 4 7	NU 0 0 0	SL 24 23 32 25	SOUTH 1 ST 10 16 12 18	BOUND 0 SR 38 21 31 28	SU 0 0 0 0	EL 15 14 18 14	EASTB 1 ET 162 168 152 161	OUND 0 ER 7 6 10 9	EU 2 0 0	WL 10 14 17 17	WESTE 2 WT 140 151 137 164	8OUND 1 WR 20 15 17 24	0 0 0 0	443 442 439 483
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM	NL 1 4 2 4 6 0 2	NORTH 1 NT 3 6 4 14 7 13 3	BOUND 0 NR 11 4 7 5 8 10 12	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36	SOUTH 1 ST 10 16 12 18 27 23 29	BOUND 0 SR 38 21 31 28 45 34 49	SU 0 0 0 0 0	EL 15 14 18 14 15 11 9	EASTB 1 ET 162 168 152 161 165 173 184	OUND 0 ER 7 6 10 9 11 11	EU 2 0 0 0 0 0	WL 10 14 17 17 12 13 12	WESTE 2 WT 140 151 137 164 145 137 137	30UND 1 WR 20 15 17 24 10 13 11	WU 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 1 4 2 4 6 0 2 2	NORTH 1 NT 3 6 4 14 7 13 3 6	BOUND 0 NR 11 4 7 5 8 10 12 4	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25	SOUTHI 1 ST 10 16 12 18 27 23 29 15	BOUND 0 SR 38 21 31 28 45 34 49 38	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9	EASTB 1 ET 162 168 152 161 165 173 184 165	OUND 0 ER 7 6 10 9 11 11 10 6	EU 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 10 14 17 17 12 13 12 14	WESTE 2 WT 140 151 137 164 145 137 137 146	30UND 1 WR 20 15 17 24 10 13 11 14	WU 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM	NL 1 4 2 4 6 0 2 2 2	NORTH 1 NT 3 6 4 14 7 13 3 6 3	BOUND 0 NR 11 4 7 5 8 10 12 4 8	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42	SOUTH 1 ST 10 16 12 18 27 23 29 15	BOUND 0 SR 38 21 31 28 45 34 49 38 49	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 9	EASTB 1 ET 162 168 152 161 165 173 184 165	OUND 0 ER 7 6 10 9 11 11 10 6 7	2 0 0 0 0 0 0 0	WL 10 14 17 17 12 13 12 14 12	WESTE 2 WT 140 151 137 164 145 137 137 146	BOUND 1 WR 20 15 17 24 10 13 11 14	WU 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 1 4 2 4 6 0 2 2 2 4	NORTH 1 NT 3 6 4 14 7 13 3 6 3 5	BOUND 0 NR 11 4 7 5 8 10 12 4 8 13	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42 35	SOUTH 1 ST 10 16 12 18 27 23 29 15 39 29	BOUND 0 SR 38 21 31 28 45 34 49 38 49 46	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 9 14	EASTB 1 ET 162 168 152 161 165 173 184 165 177 154	OUND 0 ER 7 6 10 9 11 11 10 6 7 8	EU 2 0 0 0 0 0 0 0 0 0 1	WL 10 14 17 17 12 13 12 14 12 20	WESTE 2 WT 140 151 137 164 145 137 137 146 144 139	BOUND 1 WR 20 15 17 24 10 13 11 14 10 11	WU 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504 477
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM	NL 1 4 2 4 6 0 2 2 2 4 2	NORTH 1 NT 3 6 4 14 7 13 3 6 3 5 4	BOUND 0 NR 11 4 7 5 8 10 12 4 8 13 13	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42 35 26	SOUTH 1 ST 10 16 12 18 27 23 29 15 39 29 31	BOUND 0 SR 38 21 31 28 45 34 49 38 49 46 32	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 9 14 14	EASTB 1 ET 162 168 152 161 165 173 184 165 177 154	OUND 0 ER 7 6 10 9 11 11 10 6 7 8 3	EU 2 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0	WL 10 14 17 17 12 13 12 14 12 20 14	WESTE 2 WT 140 151 137 164 145 137 146 144 139 145	BOUND 1 WR 20 15 17 24 10 13 11 14 10 11 20	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504 477 462
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	NL 1 4 2 4 6 0 2 2 2 4	NORTH 1 NT 3 6 4 14 7 13 3 6 3 5	BOUND 0 NR 11 4 7 5 8 10 12 4 8 13	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42 35	SOUTH 1 ST 10 16 12 18 27 23 29 15 39 29	BOUND 0 SR 38 21 31 28 45 34 49 38 49 46	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 9 14	EASTB 1 ET 162 168 152 161 165 173 184 165 177 154	OUND 0 ER 7 6 10 9 11 11 10 6 7 8	EU 2 0 0 0 0 0 0 0 0 0 1	WL 10 14 17 17 12 13 12 14 12 20	WESTE 2 WT 140 151 137 164 145 137 137 146 144 139	BOUND 1 WR 20 15 17 24 10 13 11 14 10 11	WU 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504 477
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM	NL 1 4 2 4 6 0 2 2 2 4 2 0	NORTH 1 NT 3 6 4 14 7 13 3 6 3 5 4	BOUND 0 NR 11 4 7 5 8 10 12 4 8 13 13	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42 35 26	SOUTH 1 ST 10 16 12 18 27 23 29 15 39 29 31	BOUND 0 SR 38 21 31 28 45 34 49 38 49 46 32	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 9 14 14	EASTB 1 ET 162 168 152 161 165 173 184 165 177 154	OUND 0 ER 7 6 10 9 11 11 10 6 7 8 3	EU 2 0 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0	WL 10 14 17 17 12 13 12 14 12 20 14	WESTE 2 WT 140 151 137 164 145 137 146 144 139 145	BOUND 1 WR 20 15 17 24 10 13 11 14 10 11 20	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504 477 462
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM	NL 1 4 2 4 6 0 2 2 4 2 0 2	NORTH 1 NT 3 6 4 14 7 13 3 6 6 3 5 4 6 NT 74	BOUND 0 NR 111 4 7 7 5 8 10 112 4 8 113 113 113 113 113 113 113 115 115 115	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42 35 26 17 SL 362	SOUTHI 1 ST 10 16 12 27 23 29 15 39 29 31 12	BOUND 0 SR 38 21 31 28 45 34 49 46 32 29	SU 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 9 14 14 23	EASTB 1 ET 162 168 152 161 165 173 184 165 177 154 160 160	OUND 0 ER 7 6 10 9 11 11 10 6 7 8 3 6 6	EU 2 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0	WL 10 14 17 17 12 13 12 14 12 20 14	WESTE 2 WT 140 151 137 164 145 137 146 144 139 145 134	SOUND 1 WR 20 15 17 24 10 13 11 14 10 11 20 12	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504 477 462 418
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	NL 1 4 2 4 6 0 2 2 2 4 4 2 0 2 2 NL 29 14.43%	NORTH 1 NT 3 6 4 14 7 13 3 6 3 5 4 6 NT 74 36.82%	BOUND 0 NR 111 4 7 7 5 8 10 12 4 8 13 13 13 3 NR 98 48.76%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42 35 26 17 SL	SOUTH 1 1 10 110 110 110 110 110 110 110 110	BOUND 0 SR 38 21 31 28 45 34 49 38 49 46 32 29 SR	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 9 14 14 23	EASTB 1 ET 162 168 152 161 165 173 184 165 177 154 160 160 ET	OUND 0 ER 7 6 110 9 111 110 6 7 8 3 6 ER	EU 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 10 14 17 17 12 13 12 14 12 20 14 14 14 WL	WESTE 2 WT 140 151 137 164 145 137 146 144 139 145 134 WT	SOUND 1 WR 20 15 17 24 10 13 11 14 10 11 20 12 WR	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504 477 462 418 TOTAL 5575
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:00 PM 4:15 PM 4:30 PM 5:15 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	NL 1 4 2 4 6 0 2 2 4 2 0 2 NL 29 14.43%	NORTH 1 NT 3 6 4 14 17 13 3 6 3 5 4 6 NT 74 36.82% 03:45 PM -	BOUND 0 NR 111 4 7 7 5 8 10 12 4 4 8 13 13 3 NR 98 48.76% 04:45 PM	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42 35 26 17 SL 362 34.05%	SOUTHI 1 ST 10 16 12 18 27 23 29 15 39 29 29 31 12 ST 261 24.55%	BOUND 0 SR 38 21 31 28 45 34 49 38 49 46 32 29 SR 440 41.39%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 14 23 EL 167 7.44%	EASTB 1 ET 162 168 152 161 165 173 184 165 177 154 160 160 ET 1981 88.24%	OUND 0 ER 7 6 10 9 11 11 10 6 7 8 3 6 ER 94 4.19%	EU 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 10 14 17 17 12 13 12 14 12 20 14 14 14 WL 169 8.18%	WESTE 2 WT 140 151 137 164 145 137 146 144 139 145 134 WT 1719 83.20%	SOUND 1 WR 20 15 17 24 10 13 11 14 10 12 WR 177 8.57%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504 477 462 418 TOTAL 5575
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:10 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR: 3	NL 1 4 2 4 6 0 2 2 4 2 0 2 NL 29 14.43%	NORTH 1 NT 3 6 4 14 7 13 3 6 3 5 4 6 NT 74 36.82% 03:45 PM - 37	BOUND 0 NR 11 4 7 7 5 8 10 12 4 8 13 13 3 3 NR 98 48.76% O4:45 FM 35	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42 35 26 17 SL 362 34.05%	SOUTHI 1 ST 10 16 12 18 8 27 23 29 15 39 29 29 31 12 ST 261 24.55%	BOUND 0 SR 38 21 31 28 45 34 49 49 46 32 29 SR 440 41.39%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 19 14 23 EL 167 7.44%	EASTB 1 ET 162 168 152 161 165 173 184 165 177 154 160 ET 1981 88.24%	OUND 0 ER 7 6 10 9 11 11 10 6 7 8 3 6 ER 94 4.19%	EU 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 10 14 17 17 17 12 13 12 14 12 20 14 14 14 14 WL 169 8.18%	WESTE 2 WT 140 151 151 137 164 145 137 146 144 139 145 134 WT 1719 83.20%	SOUND 1 WR 20 15 17 24 10 13 11 14 10 11 20 12 WR 177 8.57%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504 477 462 418 TOTAL 5575
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:00 PM 4:15 PM 4:30 PM 5:15 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	NL 1 4 2 4 6 0 2 2 4 2 0 2 NL 29 14.43%	NORTH 1 NT 3 6 4 14 17 13 3 6 3 5 4 6 NT 74 36.82% 03:45 PM -	BOUND 0 NR 111 4 7 5 8 10 12 4 8 13 13 3 NR 98 48.76% 04:45 PM 35 0.729	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 24 23 32 25 37 40 36 25 42 35 26 17 SL 362 34.05%	SOUTHI 1 ST 10 16 12 18 27 23 29 15 39 29 29 31 12 ST 261 24.55%	BOUND 0 SR 38 21 31 28 45 34 49 46 32 29 SR 440 41.39%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 15 14 18 14 15 11 9 11 14 23 EL 167 7.44%	EASTB 1 ET 162 168 152 161 165 173 184 165 177 154 160 160 ET 1981 88.24%	OUND 0 ER 7 6 6 100 9 9 111 110 6 7 8 3 6 ER 94 4.19%	EU 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 10 14 17 17 12 13 12 14 12 20 14 14 14 WL 169 8.18%	WESTE 2 WT 140 151 137 164 145 137 146 144 139 145 134 WT 1719 83.20%	OUND 1 WR 20 15 17 24 10 13 11 14 10 11 20 12 WR 177 8.57% 58 0.604	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	443 442 439 483 488 479 494 446 504 477 462 418 TOTAL 5575

TOTAL

618 3343 362 4323

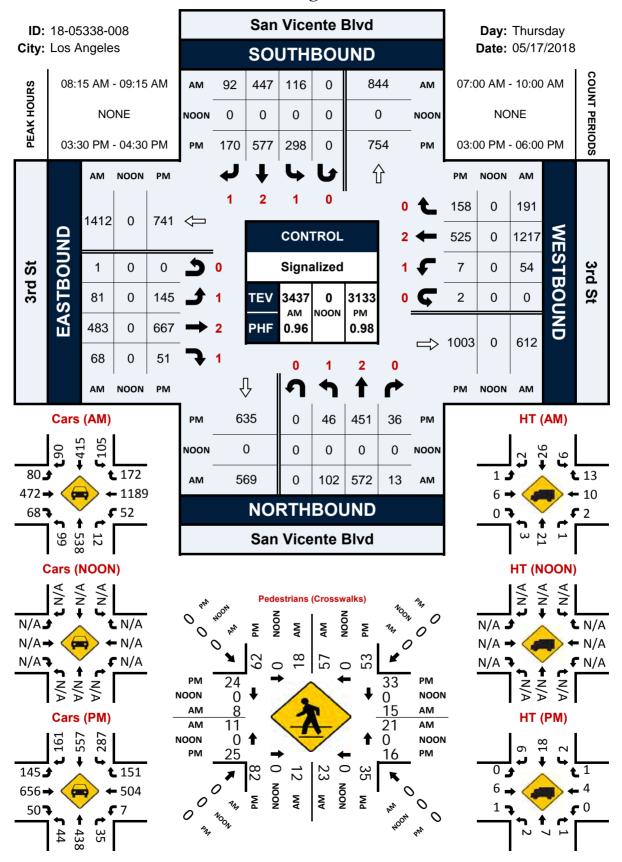
TOTAL

STREET: North/South	San Vice	nte Blvd										
East/West	3rd St											
Day:	Thursday	1	Date:	05/17/	2018	Weather:		SUNNY				
Hours:					Chekrs:	NDS		-				
School Day:		Yes				I/S CC	DE					
	N/B		S	В		E/B		_	W/B			
DUAL- WHEELED BIKES BUSES	90 17 51			57 18 79		41 26 33			87 25 117			
	N/B	TIME	S	B TIME	-	E/B	TIME		W/B	TIME		
AM PK 15 MIN	188	7.45	1	9.15		183	9.30		385	7.30		
PM PK 15 MIN	151	17.30	2	76 15.00		247	16.15		194	17.00		
AM PK HOUR	724	7.45	6	8.45		654	9.00		1462	8.15		
PM PK HOUR	579	17.00	10	15.00		919	16.15		720	17.00		
NORTHBOUND Ap	proach			SOUTH	BOUND App	oroach				TOTAL	XING S/L	XING N/L
8-9 10 9-10 9 15-16 5 16-17 4	602 66 440 41 415 63 489	Rt 5 15 9 34 37 37 137	70tal 572 717 708 530 493 579 3599	Hours 7-8 8-9 9-10 15-16 16-17 17-18	11. 13. 26. 30. 34.	3 444 1 449 4 615 2 497 2 401	Rt 66 92 105 169 145 126	Total 436 649 685 1048 944 869		N-S 1008 1366 1393 1578 1437 1448	Ped Sch 27 0 36 2 54 0 93 2 121 2 141 0	Ped Sch 50 1 61 1 58 0 116 3 82 2 86 1
EASTBOUND Appr	oach			WESTE	OUND Appr	oach				TOTAL	XING W/L	XING E/L
8-9 9	9 726	Rt 79 59 67 52 58 47	620 654 787 913 868	Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 33 35 55 11 22	9 1222 4 946 2 532 2 529	Rt 135 186 180 147 158 173	Total 1254 1447 1180 691 699 720		E-W 1735 2067 1834 1478 1612 1588	Ped Sch 27 0 18 2 27 0 47 0 40 0 56 1	Ped Sch 24 2 24 2 35 0 46 3 44 3 49 1

169 4843 979 5991

10314 215 3 222 11

San Vicente Blvd & 3rd St



Intersection Turning Movement Count

Location: San Vicente Blvd & 3rd St City: Los Angeles Control: Signalized

0.913

Project ID: 18-05338-008 Date: 5/17/2018

0.873

								To	tal								
NS/EW Streets:		San Vicer	nte Blvd			San Vicer	nte Blvd			3rd	St			3rd	St		
		NORTH	BOUND			SOUTH	BOUND			EASTE	OUND			WESTE	BOUND		
AM	1	2	0	0	1	2	1	0	1	2	1	0	1	2	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	21	112	1	0	22	47	12	0	7	60	15	0	2	230	27	0	556
7:15 AM	26	102	2	0	15	51	9	0	11	62	7	0	7	274	27	0	593
7:30 AM	22	98	0	0	27	85	18	0	18	114	29	0	9	334	42	0	796
7:45 AM	30	156	2	0	34	89	27	0	22	108	28	0	12	251	39	0	798
8:00 AM	30	155	3	0	26	91	19	0	29	99	15	1	10	302	48	0	828
8:15 AM	33	139	5	0	26	124	27	0	20	118	19	0	7	304	39	0	861
8:30 AM	24	145	2	0	22	116	27	0	22	133	14	1	12	328	45	0	891
8:45 AM	21	155	5	0	39	113	19	0	18	120	11	0	10	288	54	0	853
9:00 AM	24	133	1	0	29	94	19	0	21	112	24	0	25	297	53	0	832
9:15 AM	26	156	4	0	36	128	31	0	30	117	14	0	7	237	39	0	825
9:30 AM	20	163	2	0	34	116	30	0	19	149	15	0	13	202	49	0	812
9:45 AM	27	150	2	0	32	111	25	0	18	121	14	0	9	210	39	0	758
TOTAL WOLLINGS	NL 204	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU 2	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	304	1664	29	0	342	1165	263	0	235	1313	205	-	123	3257	501	0	9403
APPROACH %'s :	15.22%	83.32%	1.45%	0.00%	19.32%	65.82%	14.86%	0.00%	13.39%	74.81%	11.68%	0.11%	3.17%	83.92%	12.91%	0.00%	TOTAL
PEAK HR :	102	08:15 AM - 572	09:15 AM 13	^	44/	447	00		0.1	483			F.4	4047	101		TOTAL
PEAK HR VOL :	0.773	0.923	0.650	0.000	116 0.744	447 0.901	92 0.852	0.000	81 0.920	483 0.908	68 0.708	1 0.250	54 0.540	1217 0.928	191 0.884	0	3437
PEAK HR FACTOR :	0.773	0.923		0.000	0.744	0.901		0.000	0.920	0.908		0.250	0.540	0.928		0.000	0.964
		0.9	49			0.92	23			0.9	31			0.9	49		
		NORTH	BOUND			SOUTH	ROLIND			EASTE	NOLIND			WESTE	ROLIND		
PM	1	2	0	0	1	2	1	0	1	2	1	0	1	2	0	0	
1 101	NL.	NT	NR	NU	SL	ST	SR	SU	EL	ĒT	ER	EU	WL	WT	WR	wu	TOTAL
3:00 PM	14	108	11	0	55	195	25	1	22	144	24	0	6	139	42	1	787
3:15 PM	15	87	10	Ō	62	146	38	0	40	160	8	0	2	130	26	Ö	724
3:30 PM	11	120	8	Ō	70	150	48	0	43	151	11	0	1	131	38	1	783
3:45 PM	16	125	5	0	76	124	58	0	30	145	9	0	1	132	41	0	762
4:00 PM	9	107	16	0	76	141	42	0	37	180	10	0	1	123	49	1	792
4:15 PM	10	99	7	0	76	162	22	0	35	191	21	0	4	139	30	0	796
4:30 PM	13	109	4	0	64	121	34	0	26	186	16	0	4	132	36	0	745
4:45 PM	9	100	10	0	86	73	47	0	31	169	11	0	2	135	43	0	716
5:00 PM	12	117	10	0	85	77	36	0	32	185	16	0	4	131	57	2	764
5:15 PM								0	30	167	8	0	1	121	45	0	772
5:30 PM	17	118	10	0	92	121	42	-				_					
	17 15	118 127	9	0	100	85	36	0	25	171	7	0	7	140	26	2	750
5:45 PM								-				0	7 6				750 750
5:45 PM	15 9 NL	127 127 NT	9 8 NR	0 0 NU	100 65 SL	85 118 ST	36 12 SR	0 0 SU	25 30 EL	171 181 ET	7 16 ER	0 EU	6 WL	140 133 WT	26 45 WR	2 0 WU	750 TOTAL
5:45 PM TOTAL VOLUMES :	15 9 NL 150	127 127 NT 1344	9 8 NR 108	0 0 NU 0	100 65 SL 907	85 118 ST 1513	36 12 SR 440	0 0 SU 1	25 30 EL 381	171 181 ET 2030	7 16 ER 157	EU 0	6 WL 39	140 133 WT 1586	26 45 WR 478	2 0 WU 7	750
5:45 PM	15 9 NL 150 9.36%	127 127 NT 1344 83.90%	9 8 NR 108 6.74%	0 0 NU	100 65 SL	85 118 ST	36 12 SR	0 0 SU	25 30 EL	171 181 ET	7 16 ER	0 EU	6 WL	140 133 WT	26 45 WR	2 0 WU	750 TOTAL 9141
5:45 PM TOTAL VOLUMES : APPROACH %'s : PEAK HR :	15 9 NL 150 9.36%	127 127 NT 1344 83.90% D3:30 PM -	9 8 NR 108 6.74%	0 0 NU 0 0.00%	100 65 SL 907 31.70%	85 118 ST 1513 52.88%	36 12 SR 440 15.38%	0 0 SU 1	25 30 EL 381	171 181 ET 2030 79.05%	7 16 ER 157 6.11%	EU 0	6 WL 39	140 133 WT 1586 75.17%	26 45 WR 478 22.65%	2 0 WU 7 0.33%	750 TOTAL 9141 TOTAL
5:45 PM TOTAL VOLUMES : APPROACH %'s :	15 9 NL 150 9.36%	127 127 NT 1344 83.90%	9 8 NR 108 6.74%	0 0 NU 0	100 65 SL 907	85 118 ST 1513	36 12 SR 440	0 0 SU 1	25 30 EL 381	171 181 ET 2030	7 16 ER 157	EU 0	6 WL 39	140 133 WT 1586	26 45 WR 478	2 0 WU 7	750 TOTAL 9141

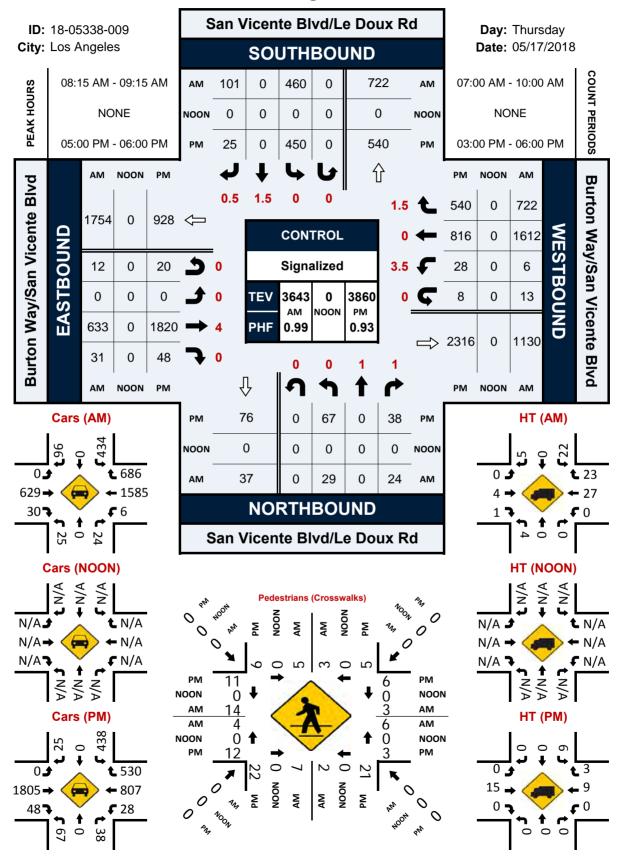
0.975

STREET: North/South	San Vicer	nte Blvd/Le Doux	κ Rd								
East/West	Burton W	ay/San Vicente I	Blvd								
Day:	Thursday	Date:		05/17/20	18	Weather:		SUNNY			
Hours:				C	hekrs:	NDS					
School Day:		Yes				I/S CO	DE				
DUAL-	N/B		S/B			E/B		=	W/B		
WHEELED	13		130			53			226		
BIKES BUSES	0		17 33			18 0			39 51		
	N/B	TIME	S/B	TIME		E/B	TIME		W/B	TIME	
AM PK 15 MIN	19	9.00	149	9.15		187	9.15		600	8.45	
PM PK 15 MIN	34	17.00	224	15.00		536	17.15		386	17.45	
AM PK HOUR	57	9.00	568	8.30		712	8.45		2353	8.15	
PM PK HOUR	105	17.00	681	15.00		1932	16.45		1392	17.00	
NORTHBOUND Ap	proach			SOUTHBO	OUND App	roach				TOTAL	XI
8-9 2	Th 5 0 3 0	Rt Total 11 26 17 40	i	Hours 7-8 8-9	Lt 29 43	6 0	Rt 75	Total 374 533		N-S 400 573	_1

NORTHBO	UND Appro	oacn			SOUTHBOU	ND Appro	oacn			IUIAL	AING	5/L	AING	N/L
Hours	Lt	Th	Rt	Total	Hours	Lt	Th	Rt	Total	N-S	Ped	Sch	Ped	Sch
7-8	15	0	11	26	7-8	299	0	75	374	400	9	0	3	0
8-9	23	0	17	40	8-9	436	0	97	533	573	6	0	7	0
9-10	36	0	21	57	9-10	465	0	101	566	623	31	2	9	0
15-16	62	0	36	98	15-16	619	0	62	681	779	26	1	15	0
16-17	58	0	31	89	16-17	542	0	33	575	664	40	2	8	0
17-18	67	0	38	105	17-18	450	0	25	475	580	41	2	10	1
TOTAL	261	0	154	415	TOTAL	2811	0	393	3204	3619	153	7	52	1

EASTBOUN	D Approa	ch			WESTBOUN	D Approa	ch			TOTAL	XING	W/L	XING	E/L
Hours	Lt	Th	Rt	Total	Hours	Lt	Th	Rt	Total	E-W	Ped	Sch	Ped	Sch
7-8	4	343	15	362	7-8	4	1360	562	1926	2288	11	0	0	0
8-9	9	613	26	648	8-9	14	1595	724	2333	2981	18	0	9	0
9-10	17	647	47	711	9-10	19	1278	727	2024	2735	25	1	9	0
15-16	21	1289	56	1366	15-16	32	786	496	1314	2680	12	0	15	0
16-17	16	1603	49	1668	16-17	31	659	471	1161	2829	29	0	9	0
17-18	20	1820	48	1888	17-18	36	816	540	1392	3280	22	1	9	0
							•							
TOTAL	87	6315	241	6643	TOTAL	136	6494	3520	10150	16793	117	2	51	0

San Vicente Blvd/Le Doux Rd & Burton Way/San Vicente Blvd



Intersection Turning Movement Count

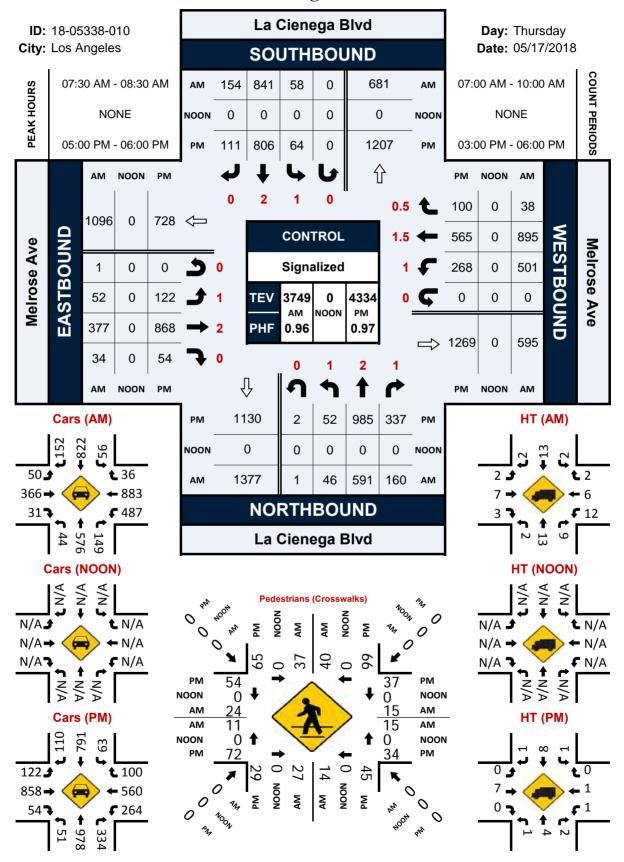
City: Los Angeles
Control: Signalized Project ID: 18-05338-009 Date: 5/17/2018

Control:	Signalized							То	tal					Date:	5/17/2018		
NS/EW Streets:	San	Vicente Blv	/d/Le Doux	Rd	San	Vicente Blv	d/Le Doux			on Way/Sai	n Vicente Bl	vd	Burt	on Way/Sar	n Vicente B	lvd	
				-						,				,			
AM	0 NL	NORTH 1 NT	1 NR	0 NU	0 SL	SOUTH 1.5 ST	0.5 SR	0 SU	<mark>0</mark> EL	EASTB 4 ET	0 ER	0 EU	3.5 WL	WESTE 0 WT	1.5 WR	0 WU	TOTAL
7:00 AM	3	0	2	0	58	0	11	0	0	63	4	0	1	336	114	0	592
7:15 AM	3	0	3	0	44	0	16	0	0	69	3	2	2	302	135	0	579
7:30 AM	6	0	3	0	96	0	23	0	0	94	3	1	0	369	130	0	725
7:45 AM	3	0	3	0	101	0	25	0	0	117	5	1	1	353	183	0	792
8:00 AM	4	0	2	0	99	0	21	0	0	134	4	2	0	367	180	1	814
8:15 AM	6	0	4 5	0	119	0	23	0	0	159	8 7	4	1	400	192	1	917
8:30 AM 8:45 AM	5 8	0	6	0	117 101	0	31 22	0	0	145 175	7	2	2	414 414	174 178	1 6	903 920
9:00 AM	10	0	9	0	123	0	25	0	0	154	9	5	1	384	178	5	920
9:15 AM	6	0	3	0	120	0	29	0	0	172	13	2	5	336	177	0	863
9:30 AM	9	0	5	0	122	0	21	0	0	164	9	1	1	286	190	4	812
9:45 AM	11	0	4	0	100	Ö	26	0	0	157	16	9	o o	272	182	3	780
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	74	0	49	0	1200	0	273	0	0	1603	88	30	16	4233	2013	21	9600
APPROACH %'s:	60.16%	0.00%	39.84%	0.00%	81.47%	0.00%	18.53%	0.00%	0.00%	93.14%	5.11%	1.74%	0.25%	67.37%	32.04%	0.33%	
PEAK HR :		08:15 AM -															TOTAL
PEAK HR VOL :	29	0	24	0	460	0	101	0	0	633	31	12	6	1612	722	13	3643
PEAK HR FACTOR :	0.725	0.000	0.667	0.000	0.935	0.000	0.815	0.000	0.000	0.904	0.861	0.600	0.750	0.973	0.940	0.542	0.990
		0.0	91			0.94	18			0.9.	23			0.90	30		
		NORTH	BOLIND			SOUTH	ROLIND			EASTB	OUND			WESTE	ROLIND	I	
PM	0	1	1	0	0	1.5	0.5	0	0	4	0	0	3.5	0	1.5	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
3:00 PM	18	0	12	0	196	0	28	0	0	276	8	2	9	210	101	2	862
3:15 PM	14	0	11	0	143	0	17	0	0	329	16	6	5	182	114	7	844
3:30 PM	11	0	8	0	163	0	14	0	0	328	18	3	3	181	128	0	857
3:45 PM	19	0	5	0	117	0	3	0	0	356	14	10	5	213	153	1	896
4:00 PM 4:15 PM	13	0	10 7	0	179	0	7 13	0	0	333 396	12	4	4 5	155	114	4	835 878
4:15 PM 4:30 PM	18 15	0	5	0	149 147	0	10	0	0	396 403	12 9	6	4	151 167	123 108	2	878 876
4:45 PM	12	0	9	0	67	0	3	0	0	471	16	5	7	186	126	2	904
5:00 PM	22	0	12	0	101	0	5	0	0	442	10	3	10	198	118	1	922
5:15 PM	15	Ö	5	Ö	114	Ö	5	Ö	Ö	519	11	6	8	200	149	4	1036
5:30 PM	13	0	13	0	101	0	2	0	0	429	16	4	4	194	117	3	896
5:45 PM	17	0	8	0	134	0	13	0	0	430	11	7	6	224	156	0	1006
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	187	0	105	0	1611	0	120	0	0	4712	153	57	70	2261	1507	29	10812
APPROACH %'s :	64.04%	0.00%	35.96%	0.00%	93.07%	0.00%	6.93%	0.00%	0.00%	95.73%	3.11%	1.16%	1.81%	58.47%	38.97%	0.75%	
PEAK HR :		05:00 PM -			150					4000					E 40		TOTAL
PEAK HR VOL : PEAK HR FACTOR :	67 0.761	0.000	38	0.000	450	0.000	25 0.481	0	0	1820	48	20	28	816	540	8	3860
		(1 (1()()	0.731	()()()	0.840	()()()	0.481	0.000	0.000	0.877	0.750	0.714	0.700	0.911	0.865	0.500	0.021

STREET: North/South	La Ciene	ga Blvd											
East/West	Melrose A	Ave											
Day:	Thursday		Date:		05/17/2	2018	Weather:		SUNNY				
Hours:						Chekrs:	NDS						
School Day:		Yes		ē			I/S CO	DE					
	N/B			S/B			E/B			W/B			
DUAL- WHEELED	106		_	81			54		_	60			
BIKES BUSES	19 32			16 43			20 28			21 40			
	N/B	TIME	-	S/B	TIME		E/B	TIME	-	W/B	TIME		
AM PK 15 MIN	247	9.00		296	8.00		158	8.15		403	7.15		
PM PK 15 MIN	398	16.30		291	17.00		293	16.15		252	17.15		
AM PK HOUR	945	9.00		1074	8.45		546	8.00		1545	7.00		
PM PK HOUR	1453	16.30		991	16.15		1049	16.15		933	17.00		
NORTHBOUND A	proach				SOUTH	BOUND Appr	oach				TOTAL	XING S/L	XING N/L
8-9 9-10 15-16 16-17	Th 68 463 66 639 15 709 71 924 66 977 64 985	Rt 111 190 191 313 374 337	Total 612 885 945 1308 1417 1376		Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 37 50 40 66 61 64	Th 826 877 858 778 796 806	Rt 139 139 143 82 90 111	Total 1002 1066 1041 926 947 981		N-S 1614 1951 1986 2234 2364 2357	Ped Sch 35 1 53 10 39 1 70 19 83 18 68 6	Ped Sch 67 0 69 2 66 2 95 14 106 14 160 4
TOTAL 33	4697	1516	6543		TOTAL	318	4941	704	5963	[12506	348 55	563 36
EASTBOUND Appr	oach				WESTB	OUND Appro	ach				TOTAL	XING W/L	XING E/L
8-9	1 860	Rt 31 42 63 52 62 54	Total 315 546 536 922 1033 1044		Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 514 465 416 226 238 268	Th 1001 705 734 550 457 565	Rt 30 39 70 89 75 100	Total 1545 1209 1220 865 770 933		E-W 1860 1755 1756 1787 1803 1977	Ped Sch 35 0 45 2 63 1 84 7 101 9 122 4	Ped Sch 25 0 35 1 35 0 78 16 64 8 62 9

TOTAL 559 3533 304 4396 TOTAL 2127 4012 403 6542 10938 450 23 299 34

La Cienega Blvd & Melrose Ave



Intersection Turning Movement Count

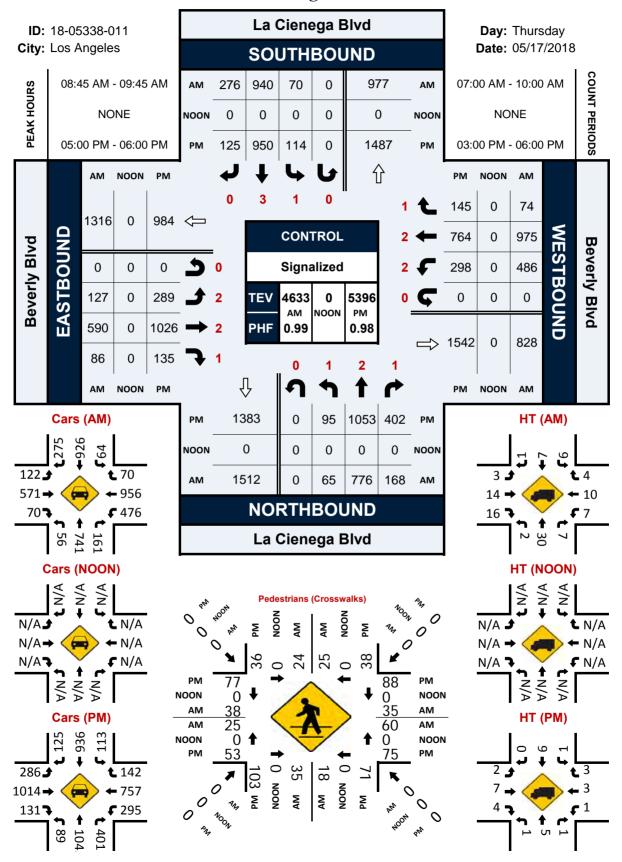
City: Los Angeles
Control: Signalized Project ID: 18-05338-010 Date: 5/17/2018

_								To	tal								
NS/EW Streets:		La Ciene	ga Blvd		La Cienega Blvd Melrose Ave Melrose Ave						e Ave						
		NORTH	BOUND			SOUTH	BOUND			EASTB	EASTBOUND				BOUND		
AM	1	2	1	0	1	2	0	0	1	2	0	0	1	1.5	0.5	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	8	99	28	0	4	217	30	0	4	44	5	0	103	245	5	1	793
7:15 AM	11	84	14	0	7	191	27	0	5	50	11	0	142	253	8	0	803
7:30 AM	6	159	32 37	0	16	233	41	0	18 7	67	7	1	144	247	9	0	980
7:45 AM 8:00 AM	13 16	121 175	36	1	10 20	185 229	41	0	13	88 89	<u>8</u> 8	0	124 113	256 200	8 10	0	898 957
8:00 AM 8:15 AM	11	136	55	0	12	194	25	0	14	133	11	0	120	192	11	0	914
8:30 AM	14	170	52	0	13	242	29	0	14	97	11	0	131	187	6	0	966
8:45 AM	13	158	47	1	5	212	38	0	26	118	12	0	101	126	12	0	869
9:00 AM	9	187	51	0	11	228	44	0	18	74	14	0	113	158	16	0	923
9:15 AM	12	160	56	0	6	202	34	0	20	115	16	0	117	184	17	0	939
9:30 AM	13	185	41	0	15	242	37	0	19	89	15	0	92	188	18	0	954
9:45 AM	11	177	43	0	8	186	28	0	28	110	18	0	94	204	19	0	926
			ND					011				F11	140		1115		TOTA:
TOTAL VOLUMES :	NL 137	NT 1811	NR 492	NU 2	SL 127	ST 2561	SR 421	SU 0	EL 186	ET 1074	ER 136	EU 1	WL 1394	WT 2440	WR 139	WU	TOTAL 10922
APPROACH %'s :	5.61%	74.16%	492 20.15%	0.08%	4.08%	82.37%	13.54%	0.00%	13.31%	76.88%	9.74%	0.07%	35.08%	2440 61.40%	3.50%	1 0.03%	10922
PEAK HR :		07:30 AM -		0.08%	4.08%	82.37%	13.54%	0.00%	13.31%	/0.88%	9.74%	0.07%	35.08%	01.40%	3.50%	0.03%	TOTAL
PEAK HR VOL :	46	591	160	1	58	841	154	0	52	377	34	1	501	895	38	0	3749
PEAK HR FACTOR :	0.719	0.844	0.727	0.250	0.725	0.902	0.819	0.000	0.722	0.709	0.773	0.250	0.870	0.874	0.864	0.000	
LAKTIK FACTOR:	0.717			0.230	0.723			0.000	0.722			0.230	0.070			0.000	0.956
LAK HK FACTOR :	0.717	0.8		0.230	0.723	0.8		0.000	0.722	0.73		0.230	0.070	0.89		0.000	0.956
	0.717		75	0.230	0.723		89	0.000	0.722		34	0.230	0.070		96	0.000	0.956
PM	1	0.8 NORTH 2	BOUND 1	0	1	SOUTH 2	BOUND 0	0	1	0.73 EASTB	OUND 0	0	1	0.89 WESTE 1.5	96 BOUND 0.5	0	
PM	1 NL	NORTH 2 NT	BOUND 1 NR	O NU	1 SL	SOUTH 2 ST	BOUND 0 SR	0 SU	1 EL	0.73 EASTB 2 ET	OUND 0 ER	0 EU	1 WL	0.89 WESTE 1.5 WT	BOUND 0.5 WR	0 WU	TOTAL
PM 3:00 PM	1 NL 16	0.8° NORTH 2 NT 236	75 BOUND 1 NR 95	0 NU 0	1 SL 20	0.88 SOUTH 2 ST 187	BOUND 0 SR 22	0 SU 0	1 EL 45	0.73 EASTB 2 ET 176	OUND 0 ER 13	0 EU 0	1 WL 51	0.89 WESTE 1.5 WT 130	96 BOUND 0.5 WR 19	0 WU 0	TOTAL 1010
PM 3:00 PM 3:15 PM	1 NL 16 23	0.8 NORTH 2 NT 236 228	BOUND 1 NR 95 80	0 NU 0 0	1 SL 20 13	0.88 SOUTH 2 ST 187 179	BOUND 0 SR 22 18	0 SU 0 0	1 EL 45 39	0.73 EASTB 2 ET 176 185	OUND 0 ER 13 11	0 EU 0 0	1 WL 51 58	0.89 WESTE 1.5 WT 130 165	96 BOUND 0.5 WR 19 27	0 WU 0 1	TOTAL 1010 1027
PM 3:00 PM 3:15 PM 3:30 PM	1 NL 16 23 15	0.8 NORTH 2 NT 236 228 247	75 BOUND 1 NR 95 80 65	0 NU 0 0	1 SL 20 13 16	0.8i SOUTH 2 ST 187 179 215	BOUND 0 SR 22 18 25	0 SU 0 0	1 EL 45 39 23	0.73 EASTB 2 ET 176 185 169	OUND 0 ER 13 11	0 EU 0 0	1 WL 51 58 59	0.86 WESTE 1.5 WT 130 165 129	80UND 0.5 WR 19 27 17	0 WU 0 1 1	TOTAL 1010 1027 995
PM 3:00 PM 3:15 PM 3:30 PM 3:45 PM	1 NL 16 23 15 17	0.8 NORTH 2 NT 236 228 247 213	75 BOUND 1 NR 95 80 65 73	0 NU 0 0	1 SL 20 13 16 17	0.88 SOUTH 2 ST 187 179 215 197	BOUND 0 SR 22 18 25 17	0 SU 0 0	1 EL 45 39 23 32	0.73 EASTB 2 ET 176 185 169 201	OUND 0 ER 13 11 14 14	0 EU 0 0 0	1 WL 51 58 59 55	0.89 WESTE 1.5 WT 130 165 129 126	96 BOUND 0.5 WR 19 27 17 26	0 WU 0 1 1	TOTAL 1010 1027 995 989
PIM 3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM	1 NL 16 23 15 17	0.8 NORTH 2 NT 236 228 247 213 245	75 BOUND 1 NR 95 80 65 73 94	0 NU 0 0 0	1 SL 20 13 16 17	0.8 SOUTH 2 ST 187 179 215 197 209	BOUND 0 SR 22 18 25 17 21	0 SU 0 0	1 EL 45 39 23 32 29	0.73 EASTB 2 ET 176 185 169 201 184	OUND 0 ER 13 11 14 14 18	0 EU 0 0 0	1 WL 51 58 59 55 62	0.86 WESTE 1.5 WT 130 165 129 126	80UND 0.5 WR 19 27 17 26 22	0 WU 0 1 1 1	TOTAL 1010 1027 995 989 1040
PM 3:00 PM 3:15 PM 3:30 PM 3:45 PM	1 NL 16 23 15 17	0.8 NORTH 2 NT 236 228 247 213	75 BOUND 1 NR 95 80 65 73	0 NU 0 0	1 SL 20 13 16 17	0.88 SOUTH 2 ST 187 179 215 197	BOUND 0 SR 22 18 25 17	0 SU 0 0 0	1 EL 45 39 23 32	0.73 EASTB 2 ET 176 185 169 201	OUND 0 ER 13 11 14 14	0 EU 0 0 0	1 WL 51 58 59 55	0.89 WESTE 1.5 WT 130 165 129 126	96 BOUND 0.5 WR 19 27 17 26	0 WU 0 1 1	TOTAL 1010 1027 995 989
PIM 3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM	1 NL 16 23 15 17 11 20	0.8 NORTH 2 NT 236 228 247 213 245 224	75 BOUND 1 NR 95 80 65 73 94 76	0 NU 0 0 0	1 SL 20 13 16 17 17	0.8 SOUTH 2 ST 187 179 215 197 209 206	BOUND 0 SR 22 18 25 17 21 24	0 SU 0 0 0 0	1 EL 45 39 23 32 29 29	0.73 EASTB 2 ET 176 185 169 201 184 251	OUND 0 ER 13 11 14 14 18 13	0 EU 0 0 0 0	1 WL 51 58 59 55 62 67	0.86 WESTE 1.5 WT 130 165 129 126 128 116	80UND 0.5 WR 19 27 17 26 22 20	0 WU 0 1 1 1 0 0	TOTAL 1010 1027 995 989 1040 1060
PIVI 3:00 PM 3:15 PM 3:30 PM 3:35 PM 4:00 PM 4:15 PM 4:30 PM	1 NL 16 23 15 17 11 20 20	0.8 NORTH 2 NT 236 228 247 213 245 224 269	75 BOUND 1 NR 95 80 65 73 94 76 109	0 NU 0 0 0 0	1 SL 20 13 16 17 17 14 17	0.88 SOUTH 2 ST 187 179 215 197 209 206 211	BOUND 0 SR 22 18 25 17 21 24 20	0 SU 0 0 0 0	1 EL 45 39 23 32 29 29 29	0.73 EASTB 2 ET 176 185 169 201 184 251 209	OUND 0 ER 13 11 14 14 18 13 13	0 EU 0 0 0 0	1 WL 51 58 59 55 62 67 55	0.86 WESTE 1.5 WT 130 165 129 126 128 116 104	96 BOUND 0.5 WR 19 27 17 26 22 20 17	0 WU 0 1 1 1 0 0	TOTAL 1010 1027 995 989 1040 1060 1070
PIVI 3:00 PM 3:15 PM 3:30 PM 3:35 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	1 NL 16 23 15 17 11 20 20 14	0.8° NORTH 2 NT 236 228 247 213 245 224 269 239 274 228	75 BOUND 1 NR 95 80 65 73 94 76 109 95 89 91	0 NU 0 0 0 0 0 0 0	1 SL 20 13 16 17 17 14 17 13 16 17	0.88 SOUTH 2 ST 187 179 215 197 209 206 211 170 242 180	BOUND 0 SR 22 18 25 17 21 24 20 25 33 26	0 SU 0 0 0 0 0 0	1 EL 45 39 23 32 29 29 26 27 27	0.73 EASTB 2 ET 176 185 169 201 184 251 209 216 207 211	OUND 0 ER 13 11 14 14 18 13 13 13 18 13 15	0 EU 0 0 0 0 0 0	1 WL 51 58 59 55 62 67 55 54 58 66	0.86 WESTE 1.5 WT 130 165 129 126 128 116 104 109 119 153	30UND 0.5 WR 19 27 17 26 22 20 17 16 25 33	0 WU 0 1 1 1 0 0 0 0	TOTAL 1010 1027 995 989 1040 1060 1070 997 1112 1074
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:30 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM	1 NL 16 23 15 17 11 20 20 14 8 15 16	0.8' NORTH 2 NT 236 228 247 213 245 224 269 239 274 228 268	75 BOUND 1 NR 95 80 65 73 94 76 109 95 89 91 83	0 NU 0 0 0 0 0 0 0 1	1 SL 20 13 16 17 17 14 17 13 16 17	0.8i SOUTH 2 ST 187 179 215 197 209 206 211 170 242 180 216	BOUND 0 SR 22 18 25 17 21 24 20 25 33 26 25	0 SU 0 0 0 0 0 0 0	1 EL 45 39 23 32 29 29 29 26 27 27 27 39 28	0.73 EASTB 2 ET 176 185 169 201 184 251 209 216 207 211 201	OUND 0 ER 13 11 14 14 18 13 13 18 15 14	0 EU 0 0 0 0 0 0 0 0	1 WL 51 58 59 55 62 67 55 54 58 66 69	0.86 WESTE 1.5 WT 130 165 129 126 128 116 104 109 119 153 150	30UND 0.5 WR 19 27 17 26 22 20 17 16 25 33 22	0 WU 0 1 1 1 0 0 0 0 0	TOTAL 1010 1027 995 989 1040 1060 1070 997 1112 1074 1110
PIVI 3:00 PM 3:15 PM 3:30 PM 3:35 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM	1 NL 16 23 15 17 11 20 20 14 8 15	0.8° NORTH 2 NT 236 228 247 213 245 224 269 239 274 228	75 BOUND 1 NR 95 80 65 73 94 76 109 95 89 91	0 NU 0 0 0 0 0 0 0	1 SL 20 13 16 17 17 14 17 13 16 17	0.88 SOUTH 2 ST 187 179 215 197 209 206 211 170 242 180	BOUND 0 SR 22 18 25 17 21 24 20 25 33 26	0 SU 0 0 0 0 0 0	1 EL 45 39 23 32 29 29 26 27 27	0.73 EASTB 2 ET 176 185 169 201 184 251 209 216 207 211	OUND 0 ER 13 11 14 14 18 13 13 13 18 13 15	0 EU 0 0 0 0 0 0	1 WL 51 58 59 55 62 67 55 54 58 66	0.86 WESTE 1.5 WT 130 165 129 126 128 116 104 109 119 153	30UND 0.5 WR 19 27 17 26 22 20 17 16 25 33	0 WU 0 1 1 1 0 0 0 0	TOTAL 1010 1027 995 989 1040 1060 1070 997 1112 1074
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:30 PM 4:30 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	1 NL 16 23 15 17 11 20 20 14 8 15 16 13	0.8' NORTH 2 NT 236 228 247 213 245 224 269 239 274 228 268 215 NT	75 BOUND 1 NR 95 80 65 73 94 76 109 95 89 91 83 74 NR	0 NU 0 0 0 0 0 0 0 1 1 1 0	1 SL 20 13 16 17 17 14 17 13 16 17 17 14 18 18 18 18 18 18 18 18 18 18 18 18 18	0.8i SOUTH 2 ST 187 179 215 197 209 206 211 170 242 180 216 168 ST	BOUND 0 SR 22 18 25 17 21 24 20 25 33 26 25 27 SR	0 SU 0 0 0 0 0 0 0 0 0	1 EL 45 39 23 32 29 29 26 27 27 39 28 28 EL	0.73 EASTB 2 ET 176 185 169 201 184 251 209 216 207 211 201 249 ET	OUND 0 ER 13 11 14 14 18 13 13 18 15 14 12 ER	0 EU 0 0 0 0 0 0 0 0 0 0	1 WL 51 58 59 55 62 67 55 54 58 66 69 75 WL	0.86 WESTE 1.5 WT 130 165 129 126 128 116 104 109 119 153 150 143	000 0.5 WR 19 27 17 26 22 20 17 16 25 20 WR	0 WU 0 1 1 1 0 0 0 0 0	TOTAL 1010 1027 995 989 1040 1060 1070 997 1112 1074 1110 1038
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM	1 NL 16 23 15 17 111 20 20 14 8 15 16 13 NL 188	0.8' NORTH 2 NT 236 228 247 213 245 224 269 239 274 228 268 215 NT 2886	75 BOUND 1 NR 95 80 65 73 74 76 109 95 89 91 83 74 NR 1024	0 NU 0 0 0 0 0 0 0 1 1 0 1 0	1 SL 20 13 16 17 17 17 14 17 13 16 17 17 17 17 18 18 19 19 19	0.8i SOUTH 2 ST 187 179 215 197 209 206 211 170 242 180 216 168 ST 2380	BOUND 0 SR 22 18 25 17 24 20 25 33 26 25 27 SR 283	0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 EL 45 39 23 32 29 29 26 27 27 39 28 28 EL 372	0.73 EASTB 2 ET 176 185 169 201 184 251 209 216 207 211 201 249 ET 2459	0UND 0 ER 13 11 14 14 18 13 13 15 14 12 ER 168	0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 51 58 59 55 62 67 67 55 54 66 69 75 WL 729	0.86 WESTE 1.5 WT 130 165 129 126 116 104 109 119 153 150 143 WT 1572	000 0.5 WR 19 27 17 26 22 20 17 16 25 33 22 20 WR 264	0 WU 0 1 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1010 1027 995 989 1040 1060 1070 997 1112 1074 1110 1038
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:30 PM 4:30 PM 5:00 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM	1 NL 16 23 15 17 11 20 20 14 8 15 16 13 NL 188 4.58%	0.8' NORTH 2 NT 236 228 247 213 245 224 269 239 274 228 268 215 NT 2886 70.37%	75 BOUND 1 NR 95 80 65 73 94 76 109 95 89 91 83 74 NR NR 1024 24,97%	0 NU 0 0 0 0 0 0 0 1 1 1 0	1 SL 20 13 16 17 17 14 17 13 16 17 17 14 18 18 18 18 18 18 18 18 18 18 18 18 18	0.8i SOUTH 2 ST 187 179 215 197 209 206 211 170 242 180 216 168 ST	BOUND 0 SR 22 18 25 17 21 24 20 25 33 26 25 27 SR	0 SU 0 0 0 0 0 0 0 0 0	1 EL 45 39 23 32 29 29 26 27 27 39 28 28 EL	0.73 EASTB 2 ET 176 185 169 201 184 251 209 216 207 211 201 249 ET	OUND 0 ER 13 11 14 14 18 13 13 18 15 14 12 ER	0 EU 0 0 0 0 0 0 0 0 0 0	1 WL 51 58 59 55 62 67 55 54 58 66 69 75 WL	0.86 WESTE 1.5 WT 130 165 129 126 128 116 104 109 119 153 150 143	000 0.5 WR 19 27 17 26 22 20 17 16 25 20 WR	0 WU 0 1 1 1 0 0 0 0 0	TOTAL 1010 1027 995 989 1040 1060 1070 997 1112 1074 1110 1038 TOTAL 12522
PIV 3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:00 PM 4:30 PM 4:30 PM 4:45 PM 5:15 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR:	1 NL 16 23 15 17 11 20 14 8 15 16 13 NL 188 4.58%	0.8' NORTH 2 7 236 228 247 213 245 224 269 239 274 228 268 215 NT 2886 70.37% 05:00 PM -	75 BOUND 1 NR 95 80 65 65 73 94 109 95 89 91 13 374 NR 1024 NR 1024 24.97%	0 NU 0 0 0 0 0 0 0 1 1 1 0 0 1 0 0 0 0 0 0	1 SL 20 13 16 17 17 14 17 13 16 17 17 14 SL 191 6.69%	0.8i SOUTH 2 ST 187 179 215 197 209 206 211 170 242 180 216 168 ST 2380 83.39%	BOUND 0 SR 22 18 25 17 21 24 20 25 33 26 25 27 SR 283 9.92%	0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 EL 45 39 23 32 29 26 27 27 27 28 28 EL 372 12.40%	0.73 EASTB 2 ET 176 185 169 201 184 251 209 216 207 211 201 249 ET 2459 81.99%	0UND 0 ER 13 11 14 18 13 18 13 15 14 12 ER 168 5.60%	0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WL 51 58 59 55 62 67 55 54 58 66 69 75 WL 729 28.39%	0.86 WESTE 1.5 WT 130 165 129 126 128 116 104 109 119 153 150 143 WT 1572 61.21%	000 0.5 WR 19 27 17 26 22 20 17 16 25 20 WR 264 10.28%	0 WU 0 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1010 1027 995 1040 1060 1070 997 1112 1074 1110 1038 TOTAL 12522
3:00 PM 3:15 PM 3:30 PM 3:30 PM 3:30 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR: PEAK HR:	1 NL 16 23 15 17 11 20 20 14 8 15 16 13 NL 188 4.58%	0.8' NORTH 2 NT 236 228 247 213 245 224 269 239 274 228 268 215 NT 2886 70.37% 05.00 PM - 985	75 BOUND 1 NR 95 80 65 73 94 76 109 95 89 91 83 74 NR 1024 24.97% 06:00 PM 337	0 NU 0 0 0 0 0 0 0 1 1 1 0 1 0 0 1 0 0 0 0	1 SL 20 13 16 17 17 14 17 13 16 17 17 14 15 SL 191 6.69%	0.8i SOUTH 2 ST 187 179 215 197 209 206 211 170 242 180 216 168 ST 2380 83.39%	BOUND 0 SR 22 18 25 17 21 24 20 25 33 36 26 25 27 SR 283 9.92%	0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 EL 45 39 23 32 29 29 26 27 39 28 EL 372 12.40%	0.73 EASTB 2 ET 176 185 169 201 184 251 209 216 207 211 201 249 ET 2459 81.99%	OUND O ER 13 11 14 14 18 13 13 15 14 12 ER 168 5.60%	0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WL 51 58 59 55 62 67 55 54 66 69 75 WL 729 28.39%	0.86 WESTE 1.5 WT 130 165 129 126 128 116 104 109 119 153 150 143 WT 1572 61.21%	96 SOUND 0.5 WR 19 27 17 26 22 20 17 16 25 33 22 20 WR 264 10.28%	0 WU 0 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1010 1027 995 989 1040 1060 1070 997 1112 1074 1110 1038 TOTAL 12522
PIV 3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:00 PM 4:30 PM 4:30 PM 4:45 PM 5:15 PM 5:15 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR:	1 NL 16 23 15 17 11 20 14 8 15 16 13 NL 188 4.58%	0.8' NORTH 2 7 236 228 247 213 245 224 269 239 274 228 268 215 NT 2886 70.37% 05:00 PM -	75 BOUND 1 1 NR 95 80 65 73 94 76 109 95 89 91 1024 24,97% 06:00 PM 337	0 NU 0 0 0 0 0 0 0 1 1 1 0 0 1 0 0 0 0 0 0	1 SL 20 13 16 17 17 14 17 13 16 17 17 14 SL 191 6.69%	0.8i SOUTH 2 ST 187 179 215 197 209 206 211 170 242 180 216 168 ST 2380 83.39%	BOUND 0 SR 22 18 25 17 21 24 20 25 33 26 25 27 SR 283 9.92% 111 0.841	0 SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 EL 45 39 23 32 29 26 27 27 27 28 28 EL 372 12.40%	0.73 EASTB 2 ET 176 185 169 201 184 251 209 216 207 211 201 249 ET 2459 81.99%	OUND 0 ER 13 11 14 14 18 13 13 15 14 12 ER 168 5.60%	0 EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 WL 51 58 59 55 62 67 55 54 58 66 69 75 WL 729 28.39%	0.86 WESTE 1.5 WT 130 165 129 126 128 116 104 109 119 153 150 143 WT 1572 61.21%	00000000000000000000000000000000000000	0 WU 0 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1010 1027 995 989 1040 1060 1070 997 1112 1074 1110 1038 TOTAL 12522

STREET: North/South	La Ciene	ga Blvd											
East/West	Beverly I	Blvd											
Day:	Thursday	1	Date:		05/17/2	018	Weather:		SUNNY				
Hours:					(hekrs:	NDS		-				
School Day:		Yes		-			I/S CO	DE					
	N/B			S/B			E/B		_	W/B			
DUAL- WHEELED BIKES BUSES	106 22 50			92 21 54			125 15 55			93 30 53			
	N/B	TIME		S/B	TIME		E/B	TIME	- <u>-</u>	W/B	TIME		
AM PK 15 MIN	287	7.45		340	8.45		217	9.30		430	7.45		
PM PK 15 MIN	426	17.45		319	17.00		391	17.00		325	17.15		
AM PK HOUR	1047	9.00	1	1330	8.30		841	9.00		1649	7.15		
PM PK HOUR	1550	17.00	1	1200	16.15		1450	17.00		1207	17.00		
NORTHBOUND Ap	proach				SOUTHE	OUND Appr	oach				TOTAL	XING S/L	XING N/L
Hours Lt 7-8 7.8 8-9 6 9-10 6 15-16 11: 16-17 8 17-18 9	5 747 1 806 2 976 3 996 5 1053	149 169 180 331 345 402	812 981 1047 1419 1424 1550		Hours 7-8 8-9 9-10 15-16 16-17	Lt 31 46 78 115 109	988 952 891 924 950	Rt 167 274 250 139 127 125	1145 1160 1189		N-S 2030 2289 2327 2564 2584 2739	Ped Sch 26 5 41 5 63 1 127 14 167 5 174 0	Ped Sch 24 4 40 6 31 5 36 4 62 2 70 4
TOTAL 48 EASTBOUND Appre		1576	7233		TOTAL WESTBO	493 OUND Appro	5725 ach	1082	7300	Ţ	14533 FOTAL	598 30 XING W/L	263 25 XING E/L
Hours Lt 7-8 10 8-9 13 9-10 14 15-16 24 16-17 31 17-18 28	2 571 2 607 5 930 5 911	Rt 29 82 92 126 112 135	785 841 1301 1338 1450		Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 394 489 416 285 261 298	900 952 722 668	81 160 153 145	1454 1449	-	E-W 2149 2239 2290 2468 2420 2657	Ped Sch 35 5 52 12 62 9 106 4 122 9 129 1	Ped Sch 33 5 55 6 87 3 141 9 121 5 161 2

TOTAL 1223 4464 576 6263 TOTAL 2143 5160 657 7960 14223 506 40 598 30

La Cienega Blvd & Beverly Blvd



Location: La Cienega Blvd & Beverly Blvd
City: Los Angeles
Control: Signalized Project ID: 18-05338-011 Date: 5/17/2018

-	Total																
NS/EW Streets:		La Ciene	ga Blvd			La Ciene	ga Blvd			Beverly	Blvd			Beverly	Blvd		
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	BOUND		
AM	1	2	1	0	1	3	0	0	2	2	1	0	2	2	1	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	23	121	12	0	3	252	35	0	13	67	6	0	57	252	13	0	854
7:15 AM	13	125	27	0	8	246	42	0	7	81	5	0	91	319	12	0	976
7:30 AM	12	151	41	0	7	275	47	0	45	131	11	0	108	303	16	0	1147
7:45 AM	22	196	69	0	13	247	43	0	35	140	7	0	138	280	12	0	1202
8:00 AM	16	183	45	0	14	243	60	0	38	143	25	0	132	226	12	0	1137
8:15 AM	16	190	46	0	15	231	66	0	33	144	20	0	127	216	21	0	1125
8:30 AM 8:45 AM	15	194	36 42	0	9 8	263 251	67 81	0	38 23	153	17 20	0	81	210	14 18	0	1097
9:00 AM	18 16	180 205	44	0	30	228	72	0	34	131 150	30	0	149 117	248	19	0	1169 1172
9:00 AM 9:15 AM	14	205	39	0	12	241	68	0	38	146	30 14	0	120	242	14	0	11/2
9:30 AM	17	179	43	0	20	220	55	0	32	163	22	0	100	258	23	0	1132
9:45 AM	14	210	54	0	16	263	55	0	38	148	26	0	79	225	25	0	1153
7.43 AW		210	34	Ů	2	203	33	Ů	30	140	20	Ů	.,	223	23	·	1133
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	196	2146	498	0	155	2960	691	0	374	1597	203	0	1299	3006	199	0	13324
APPROACH %'s:	6.90%	75.56%	17.54%	0.00%	4.07%	77.77%	18.16%	0.00%	17.20%	73.46%	9.34%	0.00%	28.84%	66.74%	4.42%	0.00%	
PEAK HR :		08:45 AM -															TOTAL
PEAK HR VOL :	65	776	168	0	70	940	276	0	127	590	86	0	486	975	74	0	4633
PEAK HR FACTOR :	0.903	0.915	0.955	0.000	0.583	0.936	0.852	0.000	0.836	0.905	0.717	0.000	0.815	0.945	0.804	0.000	0.988
		0.9	52			0.94	16			0.92	25			0.92	25		0.700
																	0.700
PM	1	NORTH	BOUND	0	1	SOUTH	BOUND	0	2	EASTB	OUND	0	2	WESTE	BOUND	0	0.700
PM	1 NI	NORTH 2	BOUND 1	O NU	1 SI	SOUTH 3	BOUND 0	0 SU	2 FI	EASTB 2	OUND 1	0 FU	2 WI	WESTE 2	BOUND 1	0 WU	
PM 3:00 PM	1 NL 23	NORTH	BOUND	0 NU 0	1 SL 32	SOUTH	BOUND	0 SU 0	2 EL 70	EASTB	OUND	0 EU 0	2 WL 75	WESTE	BOUND	0 WU 0	TOTAL 1266
	NL	NORTH 2 NT	BOUND 1 NR	NU	SL	SOUTH 3 ST	BOUND 0 SR	SU	EL	EASTB 2 ET	OUND 1 ER	EU	WL	WESTE 2 WT	SOUND 1 WR	WU	TOTAL
3:00 PM	NL 23	NORTH 2 NT 233	BOUND 1 NR 75	NU 0	SL 32	SOUTH 3 ST 216	BOUND 0 SR 42	SU 0	EL 70	EASTB 2 ET 246	OUND 1 ER 33	EU 0	WL 75	WESTE 2 WT 185	BOUND 1 WR 36	WU 0	TOTAL 1266
3:00 PM 3:15 PM 3:30 PM 3:45 PM	NL 23 22 35 32	NORTH 2 NT 233 247 241 255	BOUND 1 NR 75 93 74 89	NU 0 0 0	SL 32 25 29 29	SOUTH 3 ST 216 205 223 247	BOUND 0 SR 42 35 33 29	0 0 0 0	FL 70 58 62 55	EASTB 2 ET 246 233 240 211	OUND 1 ER 33 22 40 31	0 0	WL 75 85 60 65	WESTE 2 WT 185 185 171 181	80UND 1 WR 36 45 38 41	WU 0 0 0 0	TOTAL 1266 1255 1246 1265
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM	NL 23 22 35 32 25	NORTH 2 NT 233 247 241 255 232	BOUND 1 NR 75 93 74 89	NU 0 0 0 0	SL 32 25 29 29	SOUTH 3 ST 216 205 223 247 225	BOUND 0 SR 42 35 33 29 29	SU 0 0 0 0	EL 70 58 62 55 77	EASTB 2 ET 246 233 240 211 239	OUND 1 ER 33 22 40 31 31	0 0 0	WL 75 85 60 65	WESTE 2 WT 185 185 171 181	36 45 38 41 34	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM	NL 23 22 35 32 25 17	NORTH 2 NT 233 247 241 255 232 258	BOUND 1 NR 75 93 74 89 72 86	NU 0 0 0 0 0	SL 32 25 29 29 29 25 27	SOUTH 3 ST 216 205 223 247 225 252	BOUND 0 SR 42 35 33 29 29 29 22	SU 0 0 0 0	EL 70 58 62 55 77 82	EASTB 2 ET 246 233 240 211 239 184	OUND 1 ER 33 22 40 31 31 31	EU 0 0 0 0 0	WL 75 85 60 65 59 72	WESTE 2 WT 185 185 171 181 191 156	80UND 1 WR 36 45 38 41 34 43	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM	NL 23 22 35 32 25 17 13	NORTH 2 NT 233 247 241 255 232 258 254	BOUND 1 NR 75 93 74 89 72 86 89	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29	SOUTH 3 ST 216 205 223 247 225 252 215	BOUND 0 SR 42 35 33 29 29 29 22 38	SU 0 0 0 0 0	EL 70 58 62 55 77 82 82	EASTB 2 ET 246 233 240 211 239 184 258	OUND 1 ER 33 22 40 31 31 31 26	EU 0 0 0 0 0	WL 75 85 60 65 59 72 63	WESTE 2 WT 185 185 171 181 191 156 143	80UND 1 WR 36 45 38 41 34 43 38	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 23 22 35 32 25 17 13 28	NORTH 2 NT 233 247 241 255 232 258 254 252	BOUND 1 NR 75 93 74 89 72 86 89 98	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29 28	SOUTHI 3 ST 216 205 223 247 225 252 215 232	BOUND 0 SR 42 35 33 29 29 22 38 38	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	FL 70 58 62 55 77 82 82 74	EASTB 2 ET 246 233 240 211 239 184 258 230	OUND 1 ER 33 22 40 31 31 31 26 24	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67	WESTE 2 WT 185 185 171 181 191 156 143 178	36 45 38 41 34 43 38 38 38	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM	NL 23 22 35 32 25 17 13 28 26	NORTH 2 NT 233 247 241 255 232 258 254 252 240	BOUND 1 NR 75 93 74 89 72 86 89 98 100	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29 28 41	SOUTH 3 ST 216 205 223 247 225 252 215 232 247	BOUND 0 SR 42 35 33 29 29 22 38 38 31	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	FL 70 58 62 55 77 82 82 74 96	EASTB 2 ET 246 233 240 211 239 184 258 230 240	OUND 1 ER 33 22 40 31 31 31 26 24 55	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67	WESTE 2 WT 185 171 181 191 156 143 178 168	36 45 38 41 34 43 38 40	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:10 PM	NL 23 22 35 32 25 17 13 28 26 19	NORTH 2 NT 233 247 241 255 232 258 254 252 240 280	BOUND 1 NR 75 93 74 89 72 86 89 98 100 96	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29 28 41 21	SOUTH 3 ST 216 205 223 247 225 252 215 232 247 231	BOUND 0 SR 42 35 33 29 29 22 38 38 31 41	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 70 58 62 55 77 82 82 74 96 70	EASTB 2 ET 246 233 240 211 239 184 258 230 240 259	OUND 1 ER 33 22 40 31 31 31 26 24 55 28	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67 69 77	WESTE 2 WT 185 185 171 181 191 156 143 178 168 207	36 45 38 41 34 43 38 38 41	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287 1353
3:00 PM 3:15 PM 3:30 PM 3:345 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM 5:30 PM	NL 23 22 35 32 25 17 13 28 26 19 23	NORTH 2 NT 233 247 241 255 232 258 254 252 240 280 246	BOUND 1 NR 75 93 74 89 72 86 89 98 100 96 94	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 29 25 27 29 28 41 21 23	SOUTH 3 ST 216 205 223 247 225 252 215 232 247 231 226	BOUND 0 SR 42 35 33 29 29 22 38 38 31 41 28	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 70 58 62 55 77 82 82 74 96 70 65	EASTB 2 ET 246 233 240 211 239 184 258 230 240 259 274	OUND 1 ER 33 22 40 31 31 31 26 24 55 28 28	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67 69 77 60	WESTE 2 WT 185 185 171 181 191 156 143 178 168 207 195	36 45 38 41 34 43 38 41 34 43 38 40 41 30	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287 1353 1370 1292
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:00 PM 5:10 PM	NL 23 22 35 32 25 17 13 28 26 19	NORTH 2 NT 233 247 241 255 232 258 254 252 240 280	BOUND 1 NR 75 93 74 89 72 86 89 98 100 96	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29 28 41 21	SOUTH 3 ST 216 205 223 247 225 252 215 232 247 231	BOUND 0 SR 42 35 33 29 29 22 38 38 31 41	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 70 58 62 55 77 82 82 74 96 70	EASTB 2 ET 246 233 240 211 239 184 258 230 240 259	OUND 1 ER 33 22 40 31 31 31 26 24 55 28	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67 69 77	WESTE 2 WT 185 185 171 181 191 156 143 178 168 207	36 45 38 41 34 43 38 38 41	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287 1353 1370
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:10 PM 5:15 PM 5:30 PM 5:45 PM	NL 23 22 35 32 25 17 13 28 26 19 23 27	NORTH 2 NT 233 247 241 255 232 258 254 252 240 280 246 287 NT	BOUND 1 NR 75 93 74 89 72 86 89 98 100 96 94 112 NR	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29 28 41 21 23 29	SOUTH 3 ST 216 205 223 247 225 252 215 232 247 231 226 246 ST	BOUND 0 SR 42 35 33 32 29 29 22 38 38 38 31 41 28 25 SR	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 70 58 62 55 77 82 82 74 96 70 65 58	EASTB 2 ET 246 233 240 211 239 184 258 230 240 259 274 253 ET	OUND 1 ER 33 22 40 31 31 31 26 24 55 28 28 24 ER	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67 69 77 60 92	WESTE 2 WT 185 185 185 187 171 181 191 156 143 178 168 207 195 194 WT	30UND 1 WR 36 45 38 41 34 43 38 38 40 41 30 34 WR	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1230 1248 1287 1353 1370 1292 1381
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 5:30 PM 5:15 PM 5:30 PM 5:45 PM	NL 23 22 25 35 32 25 17 13 28 26 19 23 27 NL 290	NORTH 2 NT 233 247 241 255 232 258 254 252 240 280 246 287 NT 3025	BOUND 1 NR 75 93 74 89 72 86 89 100 96 1112 NR 1078	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29 28 41 21 23 29 SL 338	SOUTHI 3 ST 216 205 223 247 225 252 215 232 247 231 226 246 ST 2765	BOUND 0 SR 42 35 33 32 29 29 22 38 38 31 41 28 25 SR 391	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 70 58 62 55 77 82 82 74 96 70 65 58 EL 849	EASTB 2 ET 246 233 240 211 239 184 258 230 240 259 274 253 ET 2867	OUND 1 ER 333 22 40 31 31 31 26 55 28 28 28 24 ER 373	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67 69 77 60 92	WESTE 2 WT 185 185 171 181 191 156 143 178 168 207 195 194 WT 2154	30UND 1 WR 36 45 38 41 34 43 38 38 40 41 30 34 41 30 34 41 30 34 41 41 30 34 41 41 41 41 41 41 41 41 41 41 41 41 41	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287 1353 1370 1292
3:00 PM 3:15 PM 3:30 PM 3:30 PM 4:00 PM 4:15 PM 4:30 PM 4:345 PM 5:00 PM 5:30 PM 5:30 PM 5:345 PM	NL 23 22 25 35 32 25 17 13 28 26 19 23 27 NL 290 6.60%	NORTH 2 NT 233 247 241 255 232 258 254 252 240 280 246 287 NT 3025 68.86%	BOUND 1 NR 75 93 74 89 72 86 89 98 100 96 94 112 NR 1078 24.54%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29 28 41 21 23 29	SOUTH 3 ST 216 205 223 247 225 252 215 232 247 231 226 246 ST	BOUND 0 SR 42 35 33 32 29 29 22 38 38 38 31 41 28 25 SR	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 70 58 62 55 77 82 82 74 96 70 65 58	EASTB 2 ET 246 233 240 211 239 184 258 230 240 259 274 253 ET	OUND 1 ER 33 22 40 31 31 31 26 24 55 28 28 24 ER	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67 69 77 60 92	WESTE 2 WT 185 185 185 187 171 181 191 156 143 178 168 207 195 194 WT	30UND 1 WR 36 45 38 41 34 43 38 38 40 41 30 34 WR	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287 1353 1370 1292 1381 TOTAL 15432
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:500 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	NL 23 22 25 35 32 25 17 13 28 26 19 23 27 NL 290 6.60%	NORTH 2 NT 233 247 241 255 232 258 254 252 240 280 246 287 NT 3025 68.86% 55:00 PM -	BOUND 1 NR 75 93 74 89 72 86 89 100 96 1112 NR 1078 1078 1078 24.54%	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29 28 41 21 23 29 SL 338 9.67%	SOUTHI 3 ST 216 205 223 247 225 252 252 247 231 226 246 ST 2765 79.14%	BOUND 0 SR 42 35 33 29 29 22 38 31 41 28 25 SR 391 11.19%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 70 58 62 55 77 82 82 74 96 70 65 58 EL 849 20.76%	EASTB 2 ET 246 233 240 211 239 184 258 230 240 259 274 253 ET 2867 70.11%	OUND 1 ER 33 22 40 31 31 26 62 45 55 28 24 ER 373 9.12%	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67 77 60 92 WL 844 24.42%	WESTE 2 WT 185 185 171 181 191 156 143 178 168 207 195 194 WT 2154 62.33%	SOUND 1 WR 36 45 38 41 34 43 38 40 41 30 34 WR 458 13.25%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287 1353 1370 1292 1381 TOTAL
3:00 PM 3:15 PM 3:30 PM 3:35 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:30 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s: PEAK HR: 1	NL 23 22 35 32 25 17 13 38 26 19 23 27 NL 290 6.60%	NORTH 2 NT 233 247 241 255 232 258 254 252 240 280 246 287 NT 3025 68.86% 05:00 PM - 1053	BOUND 1 NR 75 93 74 89 72 86 89 98 100 96 94 112 NR 1078 24.54% 06:00 PM 402	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 29 25 27 29 28 41 21 23 29 SL 338 9.67%	SOUTHI 3 ST 216 205 205 223 247 225 232 247 231 226 246 ST 2765 79.14%	BOUND 0 SR 42 35 33 32 99 22 38 38 31 41 28 25 SR 391 11.19%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 70 58 62 55 77 82 82 82 74 96 70 65 58 EL 849 20.76%	EASTB 2 ET 246 233 240 211 239 184 258 230 240 259 274 253 ET 2867 70.11%	OUND 1 ER 33 32 22 40 31 31 31 26 24 55 28 28 28 28 21 ER 373 9.12%	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67 69 77 69 22 WL 844 24.42%	WESTE 2 WT 185 185 187 171 181 191 156 143 178 168 207 194 WT 2154 62.33%	30UND 1 WR 36 45 38 41 34 43 38 40 41 30 34 WR 458 13.25%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287 1353 1370 1292 1381 TOTAL 15432
3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:500 PM 5:15 PM 5:30 PM 5:30 PM 5:45 PM TOTAL VOLUMES: APPROACH %'s:	NL 23 22 25 35 32 25 17 13 28 26 19 23 27 NL 290 6.60%	NORTH 2 NT 233 247 241 255 232 258 254 252 240 280 246 287 NT 3025 68.86% 55:00 PM -	BOUND 1 NR 75 93 74 89 72 86 89 98 100 94 112 NR 1078 24.54% 06:00 PM 402	NU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SL 32 25 29 29 25 27 29 28 41 21 23 29 SL 338 9.67%	SOUTHI 3 ST 216 205 223 247 225 252 252 247 231 226 246 ST 2765 79.14%	BOUND 0 SR 42 35 33 29 29 22 38 38 31 41 28 25 SR 391 111.19%	SU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EL 70 58 62 55 77 82 82 74 96 70 65 58 EL 849 20.76%	EASTB 2 ET 246 233 240 211 239 184 258 230 240 259 274 253 ET 2867 70.11%	OUND 1 ER 33 22 40 31 31 31 26 24 55 28 28 24 ER 373 9.12%	EU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	WL 75 85 60 65 59 72 63 67 77 60 92 WL 844 24.42%	WESTE 2 WT 185 185 171 181 191 156 143 178 168 207 195 194 WT 2154 62.33%	SOUND 1 WR 36 45 45 38 41 34 43 38 40 41 30 34 WR 458 13.25%	WU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TOTAL 1266 1255 1246 1265 1239 1230 1248 1287 1353 1370 1292 1381 TOTAL

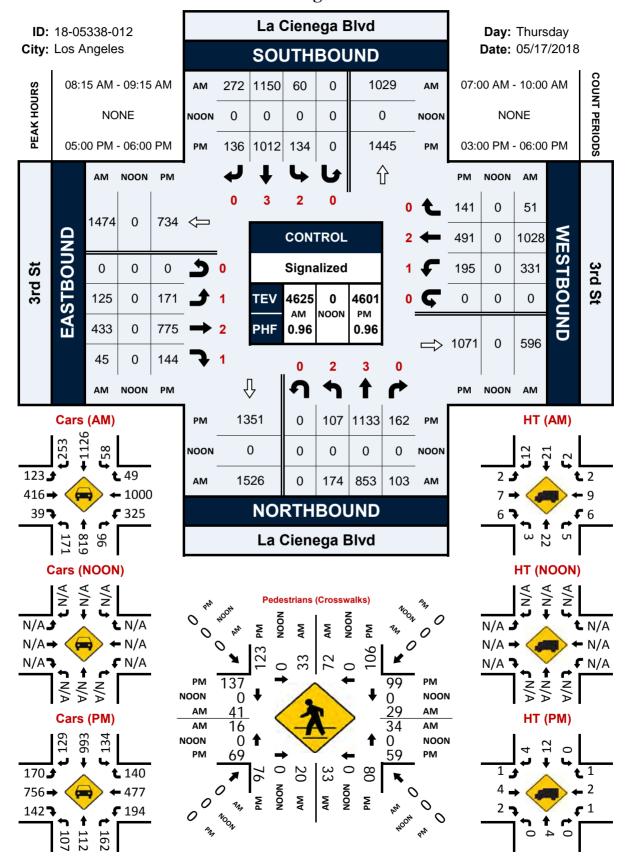
STREET: North/South	La Ciene	ga Blvd					_					
East/West	3rd St	3rd St										
Day:	Thursday	Date:		05/17/2018	Weather:	SUN	INY					
Hours:				Chekrs:	NDS							
School Day:		Yes			I/S COD	DE						
	N/B		S/B		E/B		W/B					
DUAL- WHEELED	112		151		50		65					
BIKES BUSES	21 51		27 76		32 80		18 86					
	N/B	TIME	S/B	TIME	E/B	TIME	W/B	TIMI				
AM PK 15 MIN	314	8.45	405	8.00	192	9.30	378	7.3				
PM PK 15 MIN	373	17.30	370	17.00	286	17.00	243	15.13				
AM PK HOUR	1133	8.45	1536	7.30	649	8.45	1438	8.0				
PM PK HOUR	1412	16.45	1288	16.15	1106	16.45	921	15.0				

NORTHBOUND Approach					SOUTHBOUN	SOUTHBOUND Approach						XING	S/L	XING N/L		
Hours	Lt	Th	Rt	Total	Hours	Lt	Th	Rt	Total		N-S	Ped	Sch	Ped	Sch	
7-8	67	693	60	820	7-8	29	1083	264	1376		2196	31	2	44	4	
8-9	145	830	95	1070	8-9	60	1172	276	1508		2578	52	2	85	4	
9-10	111	900	107	1118	9-10	59	1092	198	1349		2467	53	6	107	7	
15-16	69	1083	178	1330	15-16	117	937	128	1182		2512	143	2	193	1	
16-17	81	1130	153	1364	16-17	142	950	131	1223		2587	134	3	201	0	
17-18	107	1133	162	1402	17-18	134	1012	136	1282		2684	151	5	224	5	
TOTAL	580	5769	755	7104	TOTAL	541	6246	1133	7920		15024	564	20	854	21	

EASTBOUNI	WESTBOUNI	WESTBOUND Approach							XING W/L			E/L				
Hours	Lt	Th	Rt	Total	Hours	Lt	Th	Rt	Total		E-W	Peo	Sch		Ped	Sch
7-8	86	306	49	441	7-8	297	943	57	1297		1738	34	. 0		40	4
8-9	120	418	47	585	8-9	340	1041	57	1438		2023	60	0		60	3
9-10	138	458	47	643	9-10	273	863	76	1212		1855	70	4		65	2
15-16	159	659	112	930	15-16	230	513	178	921		1851	180	1		166	3
16-17	169	776	124	1069	16-17	211	484	161	856		1925	213	4		161	1
17-18	171	775	144	1090	17-18	195	491	141	827		1917	193	13		156	2
										-						
TOTAL	843	3392	523	4758	TOTAL	1546	4335	670	6551	1	11309	762	22	. [648	15

La Cienega Blvd & 3rd St

Peak Hour Turning Movement Count



National Data & Surveying Services

Intersection Turning Movement Count

Location: La Cienega Blvd & 3rd St City: Los Angeles Control: Signalized

Project ID: 18-05338-012 Date: 5/17/2018

Control:	Signalized													Date:	5/1//2018		
_								To	tal								_
NS/EW Streets:		La Ciene	ga Blvd			La Ciene	ga Blvd			3rd	St			3rd	St		ł
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	OUND		
AM	2	3	0	0	2	3	0	0	1	2	1	0	1	2	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	15	128	11	0	4	256	44	0	13	58	8	0	56	198	15	0	806
7:15 AM	18	134	14	0	9	240	72	0	16	53	12	0	74	240	15	0	897
7:30 AM	15	181	14	0	7	296	73	0	19	105	13	0	80	288	10	0	1101
7:45 AM	19	250	21	0	9	291	75	0	38	90	16	0	87	217	17	0	1130
8:00 AM	17	194	19	0	17	320	68	0	27	93	9	0	79	264	21	0	1128
8:15 AM	37	216	25	0	8	308	64	0	25	103	10	0	81	261	14	0	1152
8:30 AM	35	195	18	0	17	250	77	0	41	105	13	0	91	267	13	0	1122
8:45 AM	56	225	33	0	18	294	67	0	27	117	15	0	89	249	9	0	1199
9:00 AM	46	217	27	0	17	298	64	0	32	108	7	0	70	251	15	0	1152
9:15 AM	27	223	29	0	12	266	40	0	31	108	12	0	68	225	12	0	1053
9:30 AM	17	212	21	0	14	264	47	0	45	133	14	0	73	197	17	0	1054
9:45 AM	21	248	30	0	16	264	47	0	30	109	14	0	62	190	32	0	1063
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	323	2423	262	0	148	3347	738	0	344	1182	143	0	910	2847	190	0	12857
APPROACH %'s :	10.74%	80.55%	8.71%	0.00%	3.50%	79.07%	17.43%	0.00%	20.61%	70.82%	8.57%	0.00%	23.06%	72.13%	4.81%	0.00%	
PEAK HR :		08:15 AM -															TOTAL
PEAK HR VOL :	174	853	103	0	60	1150	272	0	125	433	45	0	331	1028	51	0	4625
PEAK HR FACTOR :	0.777	0.948	0.780	0.000	0.833	0.933	0.883	0.000	0.762	0.925	0.750	0.000	0.909	0.963	0.850	0.000	0.964
		0.9	00			0.9	75			0.9	48			0.9	50		0.701
554		NORTH				SOUTH				EASTB	OUND			WESTE			
PM	2	3	0	0	2	3	0	0	1	2	1	0	1	2	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
3:00 PM	19	275	44	0	32	243	43	1	37	158	21	0	52	130	40	0	1095

		NORTH	BOUND			3001H	BOUND			EASIE	UNIDO			WEST	JUND		
PM	2	3	0	0	2	3	0	0	1	2	1	0	1	2	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
3:00 PM	19	275	44	0	32	243	43	1	37	158	21	0	52	130	40	0	1095
3:15 PM	16	243	45	0	30	201	32	0	42	173	24	0	61	127	55	0	1049
3:30 PM	14	281	43	0	30	260	27	0	36	175	31	0	63	119	38	0	1117
3:45 PM	20	284	46	0	24	233	26	0	44	153	36	0	54	137	45	0	1102
4:00 PM	19	273	41	1	32	241	31	1	36	199	27	0	56	121	43	0	1121
4:15 PM	20	276	42	0	38	265	31	0	44	207	32	0	54	130	24	0	1163
4:30 PM	15	284	37	0	36	241	33	0	41	189	26	0	47	116	51	0	1116
4:45 PM	26	297	33	0	35	203	36	0	47	181	39	1	54	117	43	0	1112
5:00 PM	20	282	41	0	33	297	40	0	42	208	36	0	38	128	33	0	1198
5:15 PM	34	263	43	0	31	208	25	0	39	191	37	0	52	128	39	0	1090
5:30 PM	24	314	35	0	36	272	34	0	43	193	49	0	48	108	34	0	1190
5:45 PM	29	274	43	0	34	235	37	0	47	183	22	0	57	127	35	0	1123
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	256	3346	493	1	391	2899	395	2	498	2210	380	1	636	1488	480	0	13476
APPROACH %'s :	6.25%	81.69%	12.04%	0.02%	10.60%	78.63%	10.71%	0.05%	16.12%	71.54%	12.30%	0.03%	24.42%	57.14%	18.43%	0.00%	
PEAK HR :		05:00 PM -															TOTAL
PEAK HR VOL :	107	1133	162	0	134	1012	136	0	171	775	144	0	195	491	141	0	4601
PEAK HR FACTOR :	0.787	0.902	0.942	0.000	0.931	0.852	0.850	0.000	0.910	0.931	0.735	0.000	0.855	0.959	0.904	0.000	0.960
		0.9	40			0.86	66			0.9	53			0.9	44		0.700

TOTAL

868 5259 92 6219

STREET: North/South	La Ciene	ga Blvd									
East/West	San Vicer	nte Blvd									
Day:	Thursday	Date:		05/17/20)18	Weather:	SU	UNNY			
Hours:				C	hekrs:	NDS					
School Day:		Yes	-			I/S CO	DE				
DUAL-	N/B	-	S/B			E/B		_	W/B		
WHEELED BIKES BUSES	132 14 80		132 29 46			164 32 34			209 47 21		
	N/B	TIME	S/B	TIME		E/B	TIME	_	W/B	TIME	
AM PK 15 MIN	243	9.00	429	8.15		325	9.15		617	9.00	
PM PK 15 MIN	370	17.00	369	16.15		673	17.15		402	15.00	
AM PK HOUR	906	9.00	1566	7.30		1157	8.45		2229	8.15	
PM PK HOUR	1386	17.00	1320	15.30		2308	17.00		1470	15.00	
NORTHBOUND Ap	proach			SOUTHB	OUND App	roach				TOTAL	XING S/L
Hours Lt 7-8 12 8-9 12 9-10 14 15-16 14 16-17 14 17-18 18	1 724 7 751 3 991 8 1067	Rt Total 8 681 9 854 8 906 21 1155 22 1237 24 1386		Hours 7-8 8-9 9-10 15-16 16-17 17-18		Th 0 1182 0 1311 0 1202 0 1129 0 1147 0 1204	Rt To 190 251 208 122 108 113	1372 1562 1410 1251 1255 1317		N-S 2053 2416 2316 2406 2492 2703	Ped Sch 6 1 5 0 7 0 18 0 23 1 22 1

TOTAL

EASTBOUN	D Approac	ch			WESTBOUN	D Approa	ch			•	TOTAL	XING	W/L	XING	E/L
Hours	Lt	Th	Rt	Total	Hours	Lt	Th	Rt	Total		E-W	Ped	Sch	Ped	Sch
7-8	0	513	138	651	7-8	0	1545	228	1773		2424	49	2	4	1
8-9	0	896	173	1069	8-9	0	1927	247	2174		3243	50	0	17	0
9-10	0	946	189	1135	9-10	0	1744	307	2051		3186	45	1	16	1
15-16	1	1739	223	1963	15-16	0	1063	407	1470		3433	70	0	26	3
16-17	5	1976	194	2175	16-17	0	930	360	1290		3465	74	1	36	0
17-18	2	2101	205	2308	17-18	0	1069	358	1427		3735	60	3	25	1
TOTAL	8	8171	1122	9301	TOTAL	0	8278	1907	10185	1	19486	348	7	124	6

0 7175 992 8167

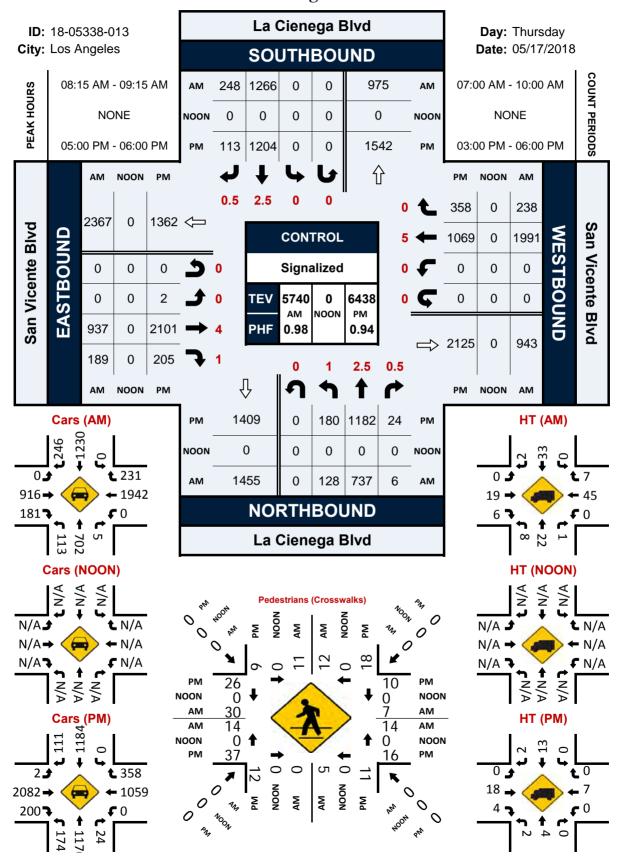
XING N/L

34 27

81 3 155 4

La Cienega Blvd & San Vicente Blvd

Peak Hour Turning Movement Count



National Data & Surveying Services

Intersection Turning Movement Count

City: Los Angeles
Control: Signalized Project ID: 18-05338-013 Date: 5/17/2018

_								To	tal								
NS/EW Streets:		La Ciene	ga Blvd			La Ciene	ga Blvd			San Vicer	nte Blvd			San Vicer	nte Blvd		
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	BOUND		
AM	1	2.5	0.5	0	0	2.5	0.5	0	0	4	1	0	0	5	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
7:00 AM	38	116	1	0	0	273	22	0	0	85	32	0	0	361	42	0	970
7:15 AM	35	109	3	0	0	282	47	0	0	101	25	0	0	307	38	0	947
7:30 AM	31	151	2	0	0	283	64	0	0	122	39	0	0	446	57	0	1195
7:45 AM	25	168	2	0	0	344	57	0	0	205	42	0	0	431	91	0	1365
8:00 AM	28	194	4	0	0	332	57	0	0	177	31	0	0	484	78	0	1385
8:15 AM	37	156	3	0	0	367	62	0	0	250	50	0	0	457	61	0	1443
8:30 AM	31	199	0	0	0	275	56	0	0	204	41	0	0	528	56	0	1390
8:45 AM	25	175	2	0	0	337	76	0	0	265	51	0	0	458	52	0	1441
9:00 AM	35	207 179	1	0	0	287	54	0	0	218 282	47	0	0	548	69 87	0	1466 1430
9:15 AM 9:30 AM	31 43	179	2	0	0	329 280	56 47	0	0	282	43 42	0	0	422 425	87 74	0	1298
9:45 AM	38	189	4	0	0	306	47 51	0	0	209	42 57	0	0	349	77	0	1308
9:45 AIVI	38	189	4	U	U	300	51	U	0	237	57	U	U	349	- //	U	1308
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	397	2019	25	0	0	3695	649	0	0	2355	500	0	0	5216	782	0	15638
APPROACH %'s:	16.26%	82.71%	1.02%	0.00%	0.00%	85.06%	14.94%	0.00%	0.00%	82.49%	17.51%	0.00%	0.00%	86.96%	13.04%	0.00%	
PEAK HR :		08:15 AM -						_				_	_				TOTAL
PEAK HR VOL :	128	737	6	0	0	1266	248	0	0	937	189	0	0	1991	238	0	5740
PEAK HR FACTOR :	0.865	0.890	0.500	0.000	0.000	0.862	0.816	0.000	0.000	0.884	0.926	0.000	0.000	0.908	0.862	0.000	0.979
		0.8	90			0.88	32			0.8	71			0.90	J3		
		NORTH	BOUND			SOUTH	BOUND			EASTB	OUND			WESTE	ROUND		
PM	1	2.5	0.5	0	0	2.5	0.5	0	0	4	1	0	0	5	0	0	
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
3:00 PM	32	276	8	0	0	294	19	0	0	387	72	0	0	303	99	0	1490
3:15 PM	35	217	3	0	0	258	30	0	1	460	58	0	0	228	112	0	1402
3:30 PM	37	263	6	0	0	285	36	0	0	403	50	0	0	265	100	0	1445
3:45 PM	39	235	4	0	0	292	37	0	0	489	43	0	0	267	96	0	1502
4:00 PM	39	291	4	0	0	267	34	0	0	432	50	0	0	242	81	0	1440
4:15 PM	32	252	7	0	0	343	26	0	1	525	52	0	0	202	98	0	1538
4:30 PM	43	283	5	0	0	259	21	0	0	475	52	0	0	237	93	0	1468
4:45 PM	34	241	6	0	0	278	27	0	4	544	40	0	0	249	88	0	1511
5:00 PM 5:15 PM	45	320	5	0	0	287	32 24	0	0	459	47	0	0	242 276	76	0	1513
	46	287	4	_	0	316		-	1	619	53	0			86	_	1712
5:30 PM 5:45 PM	46	306	5	0	0	284 317	22 35	0	0	487 536	41 64	0	0	276 275	101 95	0	1569 1644
	40	2/0							0	536	64	U	U				1644
3.43 T W	43	269	10	0	0	317											
	NL	NT	NR	NU	SL	ST	SR	SU	EL	ET	ER	EU	WL	WT	WR	WU	TOTAL
TOTAL VOLUMES :	NL 471	NT 3240	NR 67	NU 0	SL 0	ST 3480	SR 343	SU 0	8	5816	622	0	0	WT 3062	WR 1125	WU 0	TOTAL 18234
TOTAL VOLUMES : APPROACH %'s :	NL 471 12.47%	NT 3240 85.76%	NR 67 1.77%	NU	SL	ST	SR	SU						WT	WR	WU	18234
TOTAL VOLUMES : APPROACH %'s : PEAK HR :	NL 471 12.47%	NT 3240 85.76% 05:00 PM -	NR 67 1.77% 06:00 PM	NU 0 0.00%	SL 0 0.00%	ST 3480 91.03%	SR 343 8.97%	SU 0 0.00%	8 0.12%	5816 90.23%	622 9.65%	0.00%	0 0.00%	WT 3062 73.13%	WR 1125 26.87%	WU 0 0.00%	18234 TOTAL
TOTAL VOLUMES : APPROACH %'s :	NL 471 12.47%	NT 3240 85.76%	NR 67 1.77%	NU 0	SL 0	ST 3480	SR 343	SU 0	8	5816	622	0	0	WT 3062	WR 1125	WU 0	18234

TOTAL

746 3068 521 4335

TOTAL

STREET: North/South	La Ciene	ga Blvd											
East/West	Wilshire	Blvd											
Day:	Thursday		Date:		05/17/2	018	Weather:		SUNNY				
Hours:					(Chekrs:	NDS						
School Day:		Yes		-			I/S CO	DE					
	N/B		=	S/B			E/B		_	W/B			
DUAL- WHEELED BIKES BUSES	135 19 81			148 24 56			50 37 100			73 36 110			
	N/B	TIME	=	S/B	TIME		E/B	TIME		W/B	TIME		
AM PK 15 MIN	257	9.45		298	8.00		175	7.45		311	7.30		
PM PK 15 MIN	302	17.15		298	16.15		236	15.15		239	17.30		
AM PK HOUR	958	9.00		1121	7.45		640	8.15		1161	8.00		
PM PK HOUR	1167	16.45		1115	17.00		852	17.00		857	16.45		
NORTHBOUND Ap	proach				SOUTHE	BOUND Appr	oach				TOTAL	XING S/L	XING N/L
Hours Lt 7-8 13' 8-9 15. 9-10 13' 15-16 99 16-17 11. 17-18 13	4 708 0 763 2 760 6 884	Rt 31 60 65 67 66 74	768 922 958 919 1066 1162		Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 23 51 52 83 86 85	Th 838 843 784 743 885 934	Rt 143 221 198 124 118 96	Total 1004 1115 1034 950 1089 1115		N-S 1772 2037 1992 1869 2155 2277	Ped Sch 43 0 87 6 65 1 84 4 71 0 77 0	Ped Sch 40 0 43 1 59 2 42 4 46 4 50 1
TOTAL 76	6 4666	363	5795		TOTAL	380	5027	900	6307	[12102	427 11	280 12
EASTBOUND Appre	oach				WESTBO	OUND Approa	ach				TOTAL	XING W/L	XING E/L
Hours Lt 7-8 12 8-9 12 9-10 12 15-16 12 16-17 11 17-18 13	1 439 7 389 4 607 9 629	84 64 100 110 90 73	Total 564 624 616 841 838 852		Hours 7-8 8-9 9-10 15-16 16-17 17-18	Lt 94 108 143 178 183 231	Th 969 1016 827 501 541 573	Rt 28 37 58 72 39 50	Total 1091 1161 1028 751 763 854		E-W 1655 1785 1644 1592 1601 1706	Ped Sch 56 0 55 0 91 1 77 4 74 4 93 1	Ped Sch 23 0 44 0 50 0 45 8 39 1 47 0

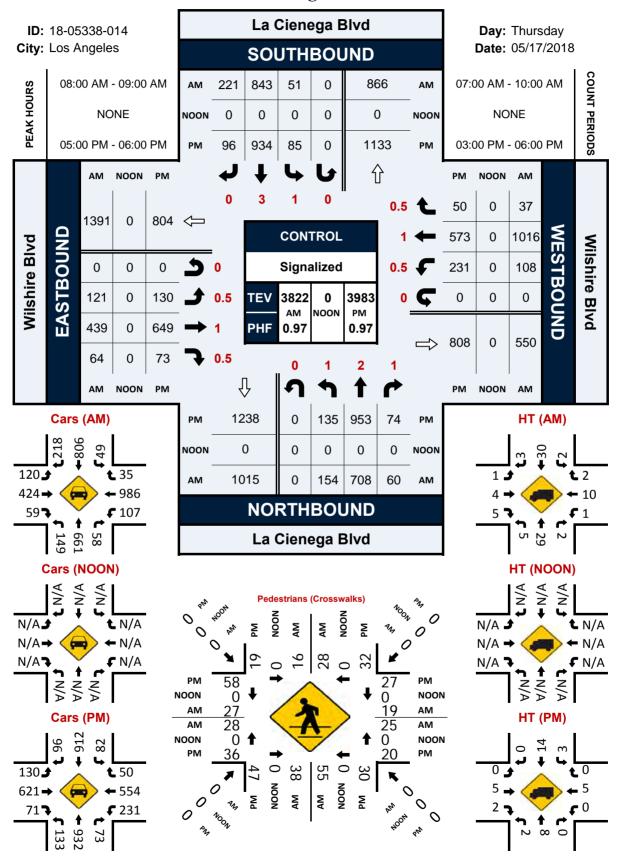
937 4427 284 5648

446 10

9983

La Cienega Blvd & Wilshire Blvd

Peak Hour Turning Movement Count



National Data & Surveying Services

Intersection Turning Movement Count

City: Los Angeles
Control: Signalized Project ID: 18-05338-014 Date: 5/17/2018

NS/EW Streets: La Cienega Blvd La Cienega Blvd Wilshire Blvd Wilshire Blvd Wilshire Blvd Wilshire Blvd Wilshire Blvd Wilshire Blvd	0 WU TOTAL 0 771 0 861 0 862
AVI 1 2 1 0 1 3 0 0 0.5 1 0.5 0 0.5 1 0.5 1 0.5	WU TOTAL 0 771 0 861
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR 7:00 AM 36 135 5 0 9 217 21 0 23 68 19 0 25 205 8 7:15 AM 37 144 7 0 7 214 26 0 25 97 27 0 29 242 6 7:30 AM 26 146 6 0 3 197 43 0 32 72 26 0 15 288 8 7:45 AM 40 173 13 0 4 210 53 0 45 118 12 0 25 234 6 8:00 AM 39 160 12 0 18 225 55 0 24 104 9 0 20 269 13	WU TOTAL 0 771 0 861
7:00 AM 36 135 5 0 9 217 21 0 23 68 19 0 25 205 8 7:15 AM 37 144 7 0 7 214 26 0 25 97 27 0 29 242 6 7:30 AM 26 146 6 0 3 197 43 0 32 72 26 0 15 288 8 7:45 AM 40 173 13 0 4 210 53 0 45 118 12 0 25 234 6 8:00 AM 39 160 12 0 18 225 55 0 24 104 9 0 20 269 13	0 771 0 861
7:15 AM 37 144 7 0 7 214 26 0 25 97 27 0 29 242 6 7:30 AM 26 146 6 0 3 197 43 0 32 72 26 0 15 288 8 7:45 AM 40 173 13 0 4 210 53 0 45 118 12 0 25 234 6 8:00 AM 39 160 12 0 18 225 55 0 24 104 9 0 20 269 13	0 861
7:30 AM 26 146 6 0 3 197 43 0 32 72 26 0 15 288 8 7:45 AM 40 173 13 0 4 210 53 0 45 118 12 0 25 234 6 8:00 AM 39 160 12 0 18 225 55 0 24 104 9 0 20 269 13	
7:45 AM 40 173 13 0 4 210 53 0 45 118 12 0 25 234 6 8:00 AM 39 160 12 0 18 225 55 0 24 104 9 0 20 269 13	
8:00 AM 39 160 12 0 18 225 55 0 24 104 9 0 20 269 13	
	0 933 0 948
	0 948
8:30 AM 38 180 11 0 15 202 41 0 18 106 18 0 29 272 4	0 934
8:45 AM	0 953
9:00 AM 29 182 17 0 7 188 56 0 35 92 26 0 44 235 9	0 920
9:15 AM 38 186 15 0 13 211 45 0 34 100 18 0 30 206 15	0 911
9:30 AM 34 183 17 0 17 174 51 0 25 93 20 0 33 219 20	0 886
9:45 AM 29 212 16 0 15 211 46 0 33 104 36 0 36 167 14	0 919
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR	WU TOTAL
TOTAL VOLUMES: 423 2069 156 0 126 2465 562 0 373 1183 248 0 345 2812 123	0 10885
APPROACH %'s: 15.97% 78.13% 5.89% 0.00% 4.00% 78.18% 17.82% 0.00% 20.68% 65.58% 13.75% 0.00% 10.52% 85.73% 3.75%	0.00%
PEAK HR: 08:00 AM - 09:00 AM	TOTAL
PEAK HR VOL: 154 708 60 0 51 843 221 0 121 439 64 0 108 1016 37	0 3822
PEAK HR FACTOR: 0.875 0.941 0.750 0.000 0.708 0.893 0.789 0.000 0.672 0.922 0.842 0.000 0.818 0.934 0.661 0.952 0.956 0.935 0.897 0.897 0.952	0.000 0.968
0.930 0.933 0.677 0.932	
NORTHBOUND SOUTHBOUND EASTBOUND WESTBOUND	
PM 1 2 1 0 1 3 0 0 0.5 1 0.5 0 0.5 1 0.5	0
NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR 3:00 PM 32 176 20 0 21 177 26 0 30 141 32 0 56 127 22	WU TOTAL 0 860
3:00 PM 32 170 20 0 21 177 25 0 30 141 32 0 350 127 22 315 PM 8 172 19 0 19 180 38 0 37 174 25 0 36 135 16	0 859
3.30 PM 25 196 12 0 27 180 29 0 24 135 18 0 47 129 17 180 180 180 180 180 180 180 180 180 180	0 839
3:45 PM 27 216 16 0 16 206 31 0 33 157 35 0 39 110 17	0 903
4:00 PM 33 205 21 0 23 204 32 0 32 146 24 0 55 139 9	0 923
4:15 PM 23 212 18 0 21 250 27 0 26 168 27 0 41 124 11	0 948
4.13 FW 25 212 10 0 21 230 27 0 20 100 27 0 41 124 11	
4.13 PM 25 212 10 0 21 250 27 0 20 100 27 0 41 124 11 430 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12	0 909
4:30 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12 4:45 PM 28 250 7 0 18 219 30 0 42 174 15 0 51 135 7	0 976
4:30 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12 4:45 PM 28 250 7 0 18 219 30 0 42 174 15 0 51 135 7 5:00 PM 29 236 32 0 23 226 21 0 29 149 14 0 50 155 14	0 976 0 978
4:30 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12 4:45 PM 28 250 7 0 18 219 30 0 42 174 15 0 51 135 7 5:00 PM 29 236 32 0 23 226 21 0 29 149 14 0 50 155 14 5:15 PM 41 242 19 0 23 247 23 0 40 173 15 0 52 145 9	0 976 0 978 0 1029
4:30 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12 4:45 PM 28 250 7 0 18 219 30 0 42 174 15 0 51 135 7 5:00 PM 29 236 32 0 23 226 21 0 29 149 14 0 50 155 14 5:15 PM 41 242 19 0 23 247 23 0 40 173 15 0 52 145 9 5:30 PM 40 234 9 0 22 219 24 0 28 149 21 0 81 140 18	0 976 0 978 0 1029 0 985
4:30 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12 4:45 PM 28 250 7 0 18 219 30 0 42 174 15 0 51 135 7 5:00 PM 29 236 32 0 23 226 21 0 29 149 14 0 50 155 14 5:15 PM 41 242 19 0 23 247 23 0 40 173 15 0 52 145 9 5:30 PM 40 234 9 0 22 219 24 0 28 149 21 0 81 140 18 5:45 PM 25 241 14 0 17 242 28 0 33 178 23 0 48 133 9	0 976 0 978 0 1029 0 985 0 991
4:30 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12 4:45 PM 28 250 7 0 18 219 30 0 42 174 15 0 51 135 7 5:00 PM 29 236 32 0 23 226 21 0 29 149 14 0 50 155 14 5:15 PM 41 242 19 0 23 247 23 0 40 173 15 0 52 145 9 5:30 PM 40 234 9 0 22 219 24 0 28 149 21 0 81 140 18 5:45 PM 25 241 14 0 17 242 28 0 33 178 23 0 48 133 9 NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR NT WR	0 976 0 978 0 1029 0 985
4:30 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12 4:45 PM 28 250 7 0 18 219 30 0 42 174 15 0 51 135 7 5:00 PM 29 236 32 0 23 226 21 0 29 149 14 0 50 155 14 5:15 PM 41 242 19 0 23 247 23 0 40 173 15 0 52 145 9 5:30 PM 40 234 9 0 22 219 24 0 28 149 21 0 81 140 18 5:45 PM 25 241 14 0 17 242 28 0 33 178 23 0 48 133 9 TOTAL VOLUMES: 343 2597 207 0 254 2562 338 0 373 1885 273 0 592 1615 161	0 976 0 978 0 1029 0 985 0 991 WU TOTAL 0 11200
4:30 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12 4:45 PM 28 250 7 0 18 219 30 0 42 174 15 0 51 135 7 5:00 PM 29 236 32 0 23 226 21 0 29 149 14 0 50 155 14 5:15 PM 41 242 19 0 23 247 23 0 40 173 15 0 52 145 9 5:30 PM 40 234 9 0 22 219 24 0 28 149 21 0 81 140 18 5:45 PM 25 241 14 0 17 242 28 0 33 178 23 0 48 133 9 TOTAL VOLUMES: NL NT NR NU SL ST	0 976 0 978 0 1029 0 985 0 991 WU TOTAL 0 11200
4:30 PM 32 217 20 0 24 212 29 0 19 141 24 0 36 143 12 4:45 PM 28 250 7 0 18 219 30 0 42 174 15 0 51 135 7 5:00 PM 29 236 32 0 23 226 21 0 29 149 14 0 50 155 14 5:15 PM 41 242 19 0 23 247 23 0 40 173 15 0 52 145 9 5:30 PM 40 234 9 0 22 219 24 0 28 149 21 0 81 140 18 5:45 PM 25 241 14 0 17 242 28 0 33 178 23 0 48 133 9 TOTAL VOLUMES: 343 2597 207 0 254 2562 338 0 373 1885 273 0 592 1615 161 APPROACH %6's: 10.90% 82.5	0 976 0 978 0 1029 0 985 0 991 WU TOTAL 0 11200 0.00%
A:30 PM	0 976 0 978 0 1029 0 985 0 991 WU TOTAL 0 11200 0.00%
A:30 PM	0 976 0 978 0 1029 0 985 0 991 WU TOTAL 0 11200 0.00%

VOLUME

Holt Ave S/O 3rd St

 Day: Thursday
 City: Los Angeles

 Date: 5/17/2018
 Project #: CA18_5352_002

	D	AILY T	TOT <i>E</i>	ALS		NB 977		SB 1,002		EB 0		WB 0	,							tal 979
AM Period	NB		SB		EB	WB			TAL	PM Period	NB		SB		EB		WB			TAL
00:00	1		2					3		12:00	9		10						19	
00:15	1		1					2		12:15	23		15						38	
00:30 00:45	2 1	5	2 0	5				4 1	10	12:30 12:45	18 19	69	17 12	54					35 31	123
01:00	0		1	<u> </u>				1	10	13:00	17	03	14	<u> </u>					31	123
01:15	2		2					4		13:15	24		24						48	
01:30	1	2	0	4				1	7	13:30	15	co	16	71					31	1.40
01:45 02:00	3	3	2	4				1 5	7	13:45 14:00	13 22	69	17 13	71					30 35	140
02:15	1		1					2		14:15	25		15						40	
02:30	3		1					4		14:30	16		20						36	
02:45 03:00	0	7	0	4				0	11	14:45 15:00	20 19	83	15 18	63					35 37	146
03:15	0		0					0		15:15	18		22						40	
03:30	1		Ö					1		15:30	15		20						35	
03:45	3	4	0					3	4	15:45	19	71	16	76					35	147
04:00 04:15	1		1 0					2		16:00 16:15	16 22		13 16						29 38	
04:15	2		0					2		16:30	11		16 27						38	
04:45	5	8	Ö	1				5	9	16:45	19	68	21	77					40	145
05:00	8		1					9		17:00	14		15						29	
05:15	3 7		2					5		17:15 17:30	9 13		15 25						24 38	
05:30 05:45	8	26	0 3	6				7 11	32	17:45	24	60	25 15	70					38 39	130
06:00	10		5					15		18:00	13		17						30	100
06:15	3		7					10		18:15	16		14						30	
06:30	7	20	11	27				18	CF	18:30	15	CO	14	F.C					29	124
06:45 07:00	<u>8</u>	28	14 15	37				22	65	18:45 19:00	24	68	11 12	56					35 34	124
07:15	2		15					17		19:15	22		12						34	
07:30	7		22					29		19:30	25		9						34	
07:45	8	23	18	70				26	93	19:45	12	81	20	53					32	134
08:00 08:15	7 7		18 25					25 32		20:00 20:15	13 6		11 16						24 22	
08:30	10		17					27		20:30	6		10						16	
08:45	6	30	14	74				20	104	20:45	10	35	6	43					16	78
09:00	14		21					35		21:00	10		4						14	
09:15 09:30	13 13		16 16					29 29		21:15 21:30	6 1		7 7						13 8	
09:45	13	53	24	77				37	130	21:45	15	32	5	23					20	55
10:00	11		13					24		22:00	9		6						15	
10:15	17		17					34		22:15	7		1						8	
10:30 10:45	13 9	50	20 15	65				33 24	115	22:30 22:45	8 5	29	3 1	11					11 6	40
11:00	8	50	16	- 55				24	113	23:00	2		0						2	-10
11:15	21		12					33		23:15	1		2						3	
11:30	19	C 1	17	E0.				36	122	23:30	5	11	1	2					6 3	1.4
11:45 TOTALS	16	64 301	14	59 402				30	123 703	23:45 TOTALS	3	11 676	0	3 600					3	14 1276
SPLIT %		42.8%		57.2%					35.5%	SPLIT %		53.0%		47.0%						64.5%
J. 211 /0		12.070		37.2/0					55.570					17.070						
	D	AILY 1	TOT!	ALS		NB		SB		EB		WB								tal
						977		1,002		0		0							1,5	979
AM Peak Hour		11:30		07:30					09:00	PM Peak Hour		18:45		16:15						14:15
AM Pk Volume		67		83					130	PM Pk Volume		93		79						148
Pk Hr Factor		0.728		0.830					0.878	Pk Hr Factor		0.930		0.731						0.925
7 - 9 Volume		53		144					197	4 - 6 Volume		128		147						275
7 - 9 Peak Hour		07:45		07:30					07:30	4 - 6 Peak Hour		16:00		16:15						16:00
7 - 9 Pk Volume		32		83					112	4 - 6 Pk Volume		68		79 0.731						145
Pk Hr Factor		0.800		0.830	0.00	U	0.000		0.875	Pk Hr Factor		0.773		0.731		0.000		0.000		0.906

VOLUME

Sherbourne Dr S/O 3rd St

Day: Thursday Date: 5/17/2018 City: Los Angeles
Project #: CA18_5352_001

	D	AILY 1	TOT/	\LS		NB		SB		EB		WB								otal
						857		1,382		0		0							2,2	239
AM Period	NB		SB		EB	WB			TAL	PM Period	NB		SB		EB		WB			TAL
00:00 00:15	0		0					0		12:00 12:15	10 16		18 21						28 37	
00:30	0		4					4		12:30	10		22						32	
00:45 01:00	0	2	0	6				4 0	8	12:45 13:00	24 13	60	19 26	80					43 39	140
01:15	0		0					0		13:15	19		24						43	
01:30	0	4	0	2				0	2	13:30	18	70	25	00					43	100
01:45 02:00	0	11	0	2				3 0	3	13:45 14:00	20 25	70	23 28	98					43 53	168
02:15	0		2					2		14:15	19		23						42	
02:30 02:45	0		1 0	3				1 0	3	14:30 14:45	13 10	67	28 32	111					41 42	178
03:00	1		0	<u> </u>				1		15:00	11	- 07	28						39	170
03:15	1		0					1		15:15 15:30	13		34						47	
03:30 03:45	0	2	1 1	2				1 1	4	15:45	8 18	50	31 34	127					39 52	177
04:00	2		2					4		16:00	19		42						61	
04:15 04:30	0		1 0					1 3		16:15 16:30	11 13		43 45						54 58	
04:45	2	7	2	5				4	12	16:45	10	53	34	164					44	217
05:00	3		0					3		17:00	7		49						56	
05:15 05:30	0		0 2					0		17:15 17:30	9 10		42 43						51 53	
05:45	4	7	1	3				5	10	17:45	8	34	27	161					35	195
06:00 06:15	3 6		1 4					4 10		18:00 18:15	7 10		23 27						30 37	
06:30	10		3					13		18:30	16		21						37	
06:45	7	26	11	19				18	45	18:45	8	41	23	94					31	135
07:00 07:15	20 17		3 8					23 25		19:00 19:15	4 5		17 21						21 26	
07:30	22		14					36		19:30	8		25						33	
07:45 08:00	30 28	89	9 11	34				39 39	123	19:45 20:00	13 4	30	17 18	80					30 22	110
08:15	29		16					45		20:15	8		13						21	
08:30	19		15					34	4=0	20:30	1		11						12	
08:45 09:00	19 21	95	<u>13</u> 9	55				32 30	150	20:45 21:00	<u>2</u>	15	<u>7</u> 7	49					<u>9</u> 8	64
09:15	17		26					43		21:15	5		6						11	
09:30 09:45	15 14	67	26 15	76				41 29	143	21:30 21:45	2 5	13	6 3	22					8 8	35
10:00	23	67	28	76				51	145	22:00	2	13	7	22					9	33
10:15	19		16					35		22:15	0		4						4	
10:30 10:45	10 22	74	26 29	99				36 51	173	22:30 22:45	4 2	8	1 1	13					5 3	21
11:00	14		17					31		23:00	2		3						5	
11:15 11:30	12 9		13 22					25 31		23:15 23:30	1 0		2 1						3 1	
11:45	8	43	21	73				29	116	23:45	0	3	0	6					0	9
TOTALS		413		377					790	TOTALS		444		1005						1449
SPLIT %		52.3%		47.7%					35.3%	SPLIT %		30.6%		69.4%						64.7%
		A 1134-	· O.T.	110		NB		SB		EB		WB							Τo	tal
	D	AILY 1	TO I A	ALS.		857		1,382		0		0								239
AM Peak Hour		07:30		10:00					10:00	PM Peak Hour		13:15		16:15						15:45
AM Pk Volume		109		99					173	PM Pk Volume		82		171						225
Pk Hr Factor		0.908		0.853					0.848	Pk Hr Factor		0.820		0.872						0.922
7 - 9 Volume		184 07:30		89 08:00					273 07:30	4 - 6 Volume 4 - 6 Peak Hour		87 16:00		325 16:15						412 16:00
7 - 9 Peak Hour 7 - 9 Pk Volume		109		08:00 55					159	4 - 6 Peak Hour 4 - 6 Pk Volume		53		16:15 171						217
Pk Hr Factor		0.908		0.859	0.00	0	0.000		0.883	Pk Hr Factor		0.697		0.872		0.000	(0.000		0.889

Appendix B
CMA and Levels of Service Explanation CMA Data Worksheets – Weekday AM and PM Peak Hours

CRITICAL MOVEMENT ANALYSIS (CMA) DESCRIPTION

Level of Service is a term used to describe prevailing conditions and their effect on traffic. Broadly interpreted, the Level of Service concept denotes any one of a number of differing combinations of operating conditions which may take place as a roadway is accommodating various traffic volumes. Level of Service is a qualitative measure of the effect of such factors as travel speed, travel time, interruptions, freedom to maneuver, safety, driving comfort and convenience.

Six Levels of Service, A through F, have been defined in the 1965 *Highway Capacity Manual*. Level of Service A describes a condition of free flow, with low traffic volumes and relatively high speeds, while Level of Service F describes forced traffic flow at low speeds with jammed conditions and queues which cannot clear during the green phases.

Critical Movement Analysis (CMA) is a procedure which provides a capacity and level of service geometry and traffic signal operation and results in a level of service determination for the intersection as a whole operating unit.

The per lane volume for each movement in the intersection is determined and the per lane intersection capacity based on the Transportation Research Board (TRB) Report 212 (*Interim Materials on Highway Capacity*). The resulting CMA represents the ratio of the intersection's cumulative volume over its respective capacity (V/C ratio). Critical Movement Analysis takes into account lane widths, bus and truck operations, pedestrian activity and parking activity, as well as number of lanes and geometrics.

The Level of Service (abbreviated from the *Highway Capacity Manual*) are listed here with their corresponding CMA and Load Factor equivalents. Load Factor is that proportion of the signal cycles during the peak hour which are fully loaded; i.e. when all of the vehicles waiting at the beginning of green are not able to clear on that green phase.

Critical Mo	vement Analysis Characte	ristics
Level of Service	Load Factor	Equivalent CMA
A (free flow)	0.0	0.00 - 0.60
B (rural design)	0.0 - 0.1	0.61 - 0.70
C (urban design)	0.1 - 0.3	0.71 - 0.80
D (maximum urban design)	0.3 - 0.7	0.81 - 0.90
E (capacity)	0.7 - 1.0	0.91 - 1.00
F (force flow)	Not Applicable	Not Applicable

SERVICE LEVEL A

There are no loaded cycles and few are even close to loaded at this service level. No approach phase is fully utilized by traffic and no vehicle waits longer than one red indication.

SERVICE LEVEL B

This level represents stable operation where an occasional approach phase is fully utilized and a substantial number are approaching full use. Many drivers begin to feel restricted within platoons of vehicles.

SERVICE LEVEL C

At this level stable operation continues. Loading is still intermittent but more frequent than at Level B. Occasionally drivers may have to wait through more one red signal indication and backups may develop behind turning vehicles. Most drivers feel somewhat restricted, but not objectionably so.

SERVICE LEVEL D

This level encompasses a zone of increasing restriction approaching instability at the intersection. Delays to approaching vehicles may be substantial during short peaks within the peak hour, but enough cycles with lower demand occur to permit periodic clearance of queues, thus preventing excessive backups. Drivers frequently have to wait through more than one red signal. This level is the lower limit of acceptable operation to most drivers.

SERVICE LEVEL E

This represents near capacity and capacity operation. At capacity (CMA = 1.0) it represents the most vehicles that the particular intersection can accommodate. However, full utilization of every signal cycle is seldom attained no matter how great the demand. At this level all drivers wait through more than one red signal, and frequently through several.

SERVICE LEVEL F

Jammed conditions. Traffic backed up from a downstream location on one of the street restricts or prevents movement of traffic through the intersection under consideration.





(Circular 212 Method)

I/S #:	North	n-South Street:	Roberts	son Bouleva	ard		Year	of Count:	2018	Amb	ient Grow	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA01	Eas	st-West Street:	3rd Stre	eet			Projec	tion Year:	2024		Pea	ak Hour:	AM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project
	1		Phases			2			2				2				2				2
Oppo	osed Ø'i	ing: N/S-1, E/W-2 or	Both-3?			0			0				0				0				0
Right	Turns: I	FREE-1, NRTOR-2 o	r OLA-3?	NB 0 EB 0	SB WB	0	NB EB	0 SE		NB EB	0	SB WB	0	NB EB	0	SB WB	0	NB EB	0	SB WB	0
	Αī	TSAC-1 or ATSAC+/	ATCS-2?	EB 0	WD	2	ED	U VV	2	ED	U	VV D	2		U	WD	2	ED	U	VV D	2
		Override (Capacity			0			0				0				0				0
				EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTUR	E CONDITI	ON W/O PF	ROJECT	FUTU	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
₽	J	Left		26	1	26	0	26	26	0	28	1	28	0	28	1	28	0	28	1	28
NORTHBOUND	7	Left-Through		466	0	C45	0	466	040	3	498	0 0	CO2	0	498	0	004	0	498	0	004
BO		Through Through-Right		400	1	645	U	400	646	3	490	1	693	U	490	1	694	"	490	1	694
E	<u> </u>	Right		179	0	0	1	180	0	5	195	0	0	1	196	0	0	0	196	0	0
P, O	↔	Left-Through-Ri	ght		0	ŭ		.00	, and the second			0	ŭ			0	ŭ			0	ŭ
Z	₹	Left-Right	•		0							0				0				0	
₽	Ĺ	Left		18	1	18	1	19	19	0	19	1	19	1	20	1	20	0	20	1	20
	l i	Left-Through Through		389	0	439	0	389	439	7	420	0 0	473	0	420	0 0	473	0	420	0 0	473
BC	ا با	Through-Right		309	1	439	U	309	439	,	420	1	4/3	U	420	1	4/3	"	420	1	4/3
ΙĒ	ڒؠ	Right		50	0	0	0	50	0	0	53	0	0	0	53	0	0	0	53	0	0
SOUTHBOUND	\leftrightarrow	Left-Through-Ri	ght		0							0				0				0	
0)	٠,	Left-Right			0							0				0				0	
	ر ا	Left		38	1	38	0	38	38	0	40	1	40	0	40	1	40	0	40	1	40
9	<u></u>	Left-Through		30	Ó	30	U	30	30	U	40	Ó	40	U	40	0	40	"	40	0	40
Į	\rightarrow	Through		347	1	196	1	348	196	10	378	1	213	1	379	1	213	0	379	1	213
EASTBOUND		Through-Right			1							1				1				1	
\S1	3	Right		44	0	44	0	44	44	0	47	0	47	0	47	0	47	0	47	0	47
E/	-	Left-Through-Ri Left-Right	ght		0							0				0 0				0 0	
	ı ¬>	Leit-Right		l	U							U				<u> </u>				U	
	C	Left		133	1	133	0	133	133	0	141	1	141	0	141	1	141	0	141	1	141
WESTBOUND	\checkmark	Left-Through			0							0				0				0	
0	<u>₹</u>	Through		731	1	386	2	733	389	9	785	1	415	2	787	1	417	0	787	1	417
E I	1	Through-Right		44	1 0	44		4.4	4.4	^	4.4	1 0	4.4	2	A =7	1 0	47	_	47	1 0	47
ÆS	→	Right Left-Through-Ri	aht	41	0	41	3	44	44	0	44	0	44	3	47	0	47	0	47	0	47
>	}-	Left-Right	a-·•		0							0				0				0	
		-		_	th-South:	663	No	rth-South:	665			th-South:	712		Nor	th-South:	714			th-South:	714
		CRITICAL VO	DLUMES	Ea	ast-West:	424	l E	ast-West:	427		Ea	ast-West:	455		Ea	ast-West:	457		E	ast-West:	457
		ME (OADAOITY (1/10)	DATIO		SUM:	1087		SUM:	1092			SUM:	1167			SUM:	1171			SUM:	1171
		ME/CAPACITY (V/C)				0.725			0.728				0.778				0.781				0.781
V/C		TSAC/ATCS ADJUS				0.625			0.628				0.678				0.681				0.681
		LEVEL OF SERVIC	E (LOS):			В			В				В				В				В

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project:	0.003	△v/c after mitigation:	0.003
Significant impacted?	NO	Fully mitigated?	N/A

3/8/2019-11:50 AM 1 CMA01





(Circular 212 Method)

I/S #:	Nort	th-South Street:	Roberts	son Bouleva	ard		Year	of Count:	2018	Amb	ient Grow	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA01	Ea	ast-West Street:	3rd Str	eet			Projec	tion Year:	2024		Pea	ak Hour:	PM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project
	<u>l</u>		f Phases			2			2				2				2				2
Oppo	osed Ø	ຽ'ing: N/S-1, E/W-2 o	Both-3?			0			0				0				0				0
Right	Turns:	: FREE-1, NRTOR-2	or OLA-3?	NB 0 EB 0	SB WB	0	NB EB	0 SE		NB EB	0	SB WB	0	NB EB	0	SB WB	0	NB EB	0	SB WB	0
	,	ATSAC-1 or ATSAC+	ATCS-2?	LB 0	WD	2	LD	U VV	2	LD	U	VV D	2		U	VV D	2		U	VV D	2
		Override	Capacity			0			0				0				0				0
				EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTUR	E CONDITI	ON W/O PF	ROJECT	FUTUF	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
<u> </u>				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
Ω	J	Left		35	1	35	0	35	35	0	37	1	37	0	37	1	37	0	37	1	37
NORTHBOUND	7	Left-Through Through		541	0	670	0	541	673	7	581	0 0	736	0	581	0	739	0	581	0	739
BO		Through-Right		341	1	670	U	341	6/3	,	361	1	730	0	361	1	739	"	301	1	139
H		Right		129	Ó	0	3	132	0	18	155	Ö	0	3	158	0	0	0	158	0	0
P.	→	Left-Through-R	ight		0				·			0				0				0	
Z	\checkmark	Left-Right	_		0							0				0				0	
9	L.	Left		45	1 0	45	3	48	48	0	48	1 0	48	3	51	1 0	51	0	51	1 0	51
Ď	ľ	Left-Through Through		374	0	432	0	374	432	5	402	0	464	0	402	0	464	0	402	0	464
BG	j	Through-Right		3/4	1	432	U	3/4	402	3	402	1	404	0	402	1	404		402	1	404
	نہ	Right		58	0	0	0	58	0	0	62	0	0	0	62	0	0	0	62	0	0
SOUTHBOUND	↔	Left-Through-R	ight		0							0				0				0	
0,	λ,	Left-Right			0							0				0				0	
	ال ا	Left		74	1	74	0	74	74	0	79	1	79	0	79	1	79	0	79	1	79
9	<u></u>	Left-Through		74	Ö	74	U	74	74	U	13	0	13	U	13	Ö	13		19	0	19
EASTBOUND	\rightarrow	Through		337	1	204	2	339	205	27	385	1	230	2	387	1	231	0	387	1	231
l BC	7	Through-Right			1							1				1				1	
ΔS	<u>}</u>	Right	!l. 4	71	0	71	0	71	71	0	75	0 0	75	0	75	0	75	0	75	0	75
Ē	(ز	Left-Through-R Left-Right	ignt		0							0				0				0	
	1 1	Loit-Right																			
	<i>(</i>	Left		164	1	164	0	164	164	0	174	1	174	0	174	1	174	0	174	1	174
WESTBOUND	7	Left-Through			0							0				0				0	
ŭ	<u>↓</u>	Through		448	1	248	1	449	250	17	493	1	272	1	494	1	274	0	494	1	274
======================================	1	Through-Right Right		48	0	48	2	50	50	0	51	0	51	2	53	0	53	0	53	0	53
Ki	₹	Left-Through-R	ight	40	0	40	_	30	50	U	JI	0	31	_	JJ	0	33	"	33	0	33
>	}	Left-Right			0							0				0				0	
	North-South:			715	_	rth-South:	721			th-South:	784			th-South:	790			th-South:	790		
	CRITICAL VOLUMES East-West:			368	"	East-West:	369		Ea	ast-West:	404		Ea	ast-West:	405		E	ast-West:	405		
<u> </u>	VOLUME/CAPACITY (V/C) RATIO:			SUM:	1083		SUM:	1090			SUM:	1188			SUM:	1195			SUM:	1195	
	, ,					0.722			0.727				0.792				0.797				0.797
V/C	C LESS ATSAC/ATCS ADJUSTMENT:					0.622			0.627				0.692				0.697				0.697
		LEVEL OF SERVICE	E (LOS):			В			В				В				В				В

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

0.005

Change in v/c due to project:	0.005	∆v/c after mitigation:	
Significant impacted?	NO	Fully mitigated?	





(Circular 212 Method)

I/S #:	North-	-South Street:	Roberts	son Bouleva	ard		Year	of Count:	2018	Amb	ient Grov	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA02	Eas	t-West Street:	Burton	Way			Projec	tion Year:	2024		Pea	ak Hour:	AM	Revie	wed by:	J/	AS	Project:	Our Lady o	f Mt. Leban	on Project
1		ng: N/S-1, E/W-2 or		NB 0	SB	3 0 0	NB	0 Si	3 0 3 0	NB	0	SB	3 0 0	NB	0	SB	3 0 0	NB	0	SB	3 0
Right	: Turns: F	REE-1, NRTOR-2 o	r OLA-3?	EB 0	WB	0	EB	0 W		EB	0	WB	0	EB	0	WB	0	EB	0	WB	0
	AT	SAC-1 or ATSAC+A Override (2			2				2				2				2
		Override	зарасну	EXIST	NG CONDI	•	EXIST	NG PLUS P	_	FUTUR	E CONDITI	ON W/O PF		FUTUF	E CONDIT	ION W/ PR		FUTURE	W/ PROJE	CT W/ MIT	•
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
Ω	*	Left		56	1	56	0	56	56	7	66	1	66	0	66	1	66	0	66	1	66
NORTHBOUND	1	Left-Through Through		501	0 1	501	1	502	502	1	533	0 1	533	1	534	0 1	534	0	534	0	534
<u>B</u>		Through-Right		301	0	301		302	302		333	0	333	'	334	0	334		334	0	334
I È	7	Right		39	1	0	1	40	0	0	41	1	0	1	42	1	0	0	42	1	0
ğ	↔	Left-Through-Ri	ght		0							0				0				0	
_	~	Left-Right			0							0				0				0	
	<u> </u>	Left		26	1	26	0	26	26	0	28	1	28	0	28	1	28	0	28	1	28
SOUTHBOUND	>	Left-Through		20	0	20		20	20		20	0	20	Ů	20	0	20		20	0	20
ಠ್ಣ	↓	Through		464	0	510	0	464	510	0	493	0	549	0	493	0	549	0	493	0	549
l ≝	4	Through-Right		40	1 0	0	0	40	0	-	50	1 0	0		50	1	0		50	1 0	0
5	→ →	Right Left-Through-Ri	aht	46	0	0	0	46	0	7	56	0	0	0	56	0 0	0	0	56	0	0
SC	į,	Left-Right	9		0							0				0				0	
۵		Left		100	1 0	100	0	100	100	7	113	1 0	113	0	113	1 0	113	0	113	1 0	113
EASTBOUND	\rightarrow	Left-Through Through		720	3	240	1	721	240	0	764	3	255	1	765	3	255	0	765	3	255
80	\rightarrow	Through-Right		720	0	240	'	121	240		704	0	200	'	700	0	200		700	0	200
ST	7	Right		126	1	98	0	126	98	3	137	1	104	0	137	1	104	0	137	1	104
Ð	7	Left-Through-Ri	ght		0							0				0				0	
	I	Left-Right		I	0							0				0				0	
	C	Left		178	1	178	5	183	183	0	189	1	189	5	194	1	194	0	194	1	194
WESTBOUND	7	Left-Through			0							0		1		0				0	
ಠ್ಣ	<u>₹</u>	Through Through-Right		1370	3	457	3	1373	458	12	1466	3	489	3	1469	3 0	490	0	1469	3 0	490
STE	Ž.	Right		81	1	68	0	81	68	0	86	1	72	0	86	1	72	0	86	1	72
Ķ	→	Left-Through-Ri	ght	01	Ö	00		01	00		00	Ö	12		00	0	12	"	00	0	12
	}	Left-Right			0							0				0				0	
	North-Sout					566	_	rth-South:	566			th-South:	615	1		th-South:	615			th-South:	615
	CRITICAL VOLUMES East-West SUM				557 1123	"	ast-West: SUM:	558 1124		E	ast-West: SUM:	602 1217	1	Ea	ast-West: SUM:	603 1218		E	ast-West: SUM:	603 1218	
	VOLUME/CAPACITY (V/C) RATIO:				30W.	0.788		30111.	0.789			30W.	0.854			30W.	0.855			30W.	0.855
V/C	C LESS ATSAC/ATCS ADJUSTMENT:					0.766			0.789				0.054 0.754				0.055 0.755				0.055 0.755
"	LEVEL OF SERVICE (LOS):					0.666 B			0.689 B				0.754 C	1			0.755 C				0.755 C
<u></u>		LL4LL OF SERVICE	_ (LU3).	<u> </u>		D			D				U				U				U

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

3/8/2019-11:51 AM CMA02





(Circular 212 Method)

I/S #:	Noi	rth-S	outh Street:	Roberts	son Bouleva	ard		Year	of Count:	2018	Amb	ient Grow	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA02	Е	East-\	West Street:	Burton	Way			Projec	tion Year:	2024		Pea	ak Hour:	PM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project
	4)-			Phases			3			3				3				3	-			3
Oppo	osed (Ø'ing	: N/S-1, E/W-2 or	Both-3?			0			0		_		0				0				0
Right	Turns	s: FR	EE-1, NRTOR-2 o	r OLA-3?	NB 0	SB	0	NB	0 SE		NB	0	SB	0	NB	0	SB	0	NB	0	SB	0
		ΔΤς	AC-1 or ATSAC+A	TCS-22	EB 0	WB	0 2	EB	0 W	B 0 2	EB	0	WB	0 2	EB	U	WB	0 2	EB	0	WB	2
		A10/	Override C				0			0				0				0				0
					EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTUR	E CONDITI	ON W/O PR	ROJECT	FUTUF	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		N	OVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
					Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
٥	J.		Left		85	1	85	0	85	85	5	95	1	95	0	95	1	95	0	95	1	95
N S	4		Left-Through			0							0				0				0	
NORTHBOUND	Î		Through		504	1	504	3	507	507	4	539	1	539	3	542	1	542	0	542	1	542
IE	l Î	→	Through-Right		72	0	30	2	74	30	0	76	0 1	31	2	78	0	32	0	78	0	32
N.	[_ ^ _	_	Right Left-Through-Rig	nht	12	0	30	2	74	30	U	76	0	31	2	10	0	32	"	70	0	32
ž	↑		Left-Right	giit		0							0				0				0	
	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	→	Left		82	1	82	0	82	82	0	87	1	87	0	87	1	87	0	87	1	87
Z)	→	Left-Through			0							0				0				0	
l o			Through		489	0	534	0	489	534	0	519	0	572	0	519	0	572	0	519	0	572
SOUTHBOUND	4		Through-Right Right		45	0	0	0	45	0	5	5 0	1 0	0	0	50	1 0	0	0	5 0	0	0
).	4	→	Left-Through-Rig	nht	43	0	U	U	43	U	3	53	0	U	U	53	0	U	"	53	0	U
SC	بلہ		Left-Right	J		Ö							0				Ö				0	
	1		Left		170	1	170	0	170	170	21	201	1	201	0	201	1	201	0	201	1	201
N N	<i>→</i>		Left-Through			0							0				0				0	
l ŭ	7		Through Through-Right		1452	3 0	484	3	1455	485	0	1541	3 0	514	3	1544	3 0	515	0	1544	3 0	515
) TE	7,		Right		61	1	19	0	61	19	7	72	1	25	0	72	1	25	0	72	1	25
EASTBOUND	\downarrow	>	Left-Through-Rig	ght		0	10	· ·	01				0	20			0	20			0	20
	\dashv		Left-Right			0							0				0				0	
							-															
۵	7	_	Left Left-Through		85	1 0	85	3	88	88	0	90	1 0	90	3	93	1 0	93	0	93	1 0	93
WESTBOUND	↓		Through		931	3	310	2	933	311	13	1001	3	334	2	1003	3	334	0	1003	3	334
BO	1	-	Through-Right		331	0	310	_	900	311	13	1001	0	004	_	1003	0	554		1000	0	554
ST	<u>,</u>	-	Right		67	1	26	0	67	26	0	71	1	28	0	71	1	28	0	71	1	28
WE	→	-	Left-Through-Rig	ght		0							0				0				0	
	├	-	Left-Right			0				0.10			0				0				0	0.5=
	North-South: CRITICAL VOLUMES East-West:			619	_	rth-South:	619 572			th-South:	667			th-South:	667			th-South:	667			
	CRITICAL VOLUMES East-West: SUM:			569 1188	"	East-West: SUM:	573 1192		E	ast-West: SUM:	604 1271		E	ast-West: SUM:	608 1275		E	ast-West: SUM:	608 1275			
	VOLUME/CAPACITY (V/C) RATIO:			JUNI.			30W.	0.836			30111.	0.892			JOINI.	0.895			30141.			
V/C	//C LESS ATSAC/ATCS ADJUSTMENT:					0.834															0.895	
V/C							0.734			0.736				0.792				0.795				0.795
	LEVEL OF SERVICE (LOS):			= (LUS):			С			С				С				С				С

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project:	0.003	△v/c after mitigation:	0.003
Significant impacted?	NO	Fully mitigated?	N/A





(Circular 212 Method)

I/S #:	North	n-South Street:	Willama	n Drive			Year	of Count:	2018	Amb	ient Grov	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA05	Eas	st-West Street:	Burton	Way			Projec	tion Year:	2024		Pea	ak Hour:	AM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project
Орро	osed Ø'iı	No. of ng: N/S-1, E/W-2 or	f Phases Both-3?	NB 0	SB	3 0 0	NB	0 SI	3 0 3 0	NB	0	SB	3 0 0	NB	0	SB	3 0 0	NB	0	SB	3 0 0
Right	Turns: F	FREE-1, NRTOR-2 o	or OLA-3?	NB 0 EB 0	ЗВ WВ	0	NB EB	0 SI 0 W		NB EB	0	ЗВ WB	0	NВ ЕВ	0	ЗВ WВ	0	EB	0	ЗВ WB	0
	ΑT	TSAC-1 or ATSAC+	ATCS-2?			2			2				2				2				2
		Override (Capacity			0			0				0				0				0
		MOVEMENT		EXISTI	ING CONDI			ING PLUS P				ON W/O PR			RE CONDIT				W/ PROJE		
		MOVEMENT		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
٥	Ĵ	Left		77	0	77	0	77	77	0	82	0	82	0	82	0	82	0	82	0	82
NORTHBOUND	1	Left-Through		204	0 0	200	0	204	200	0	217	0	309	0	217	0 0	200	0	217	0	200
BO	 ↑.	Through Through-Right		204	0	290	0	204	290	U	217	0	309	0	217	0	309	0	217	0	309
l ₽		Right		9	0	0	0	9	0	0	10	0	0	0	10	0	0	0	10	0	0
Ö	\leftrightarrow	Left-Through-Ri	ight		1							1				1				1	
_		Left-Right			0							0				0				0	
	,	Left		36	0	36	0	36	36	0	38	0	38	0	38	0	38	0	38	0	38
l N	>	Left-Through			0						00	0	•		00	0			00	0	
30	+	Through		64	0	130	0	64	130	0	68	0	138	0	68	0	138	0	68	0	138
SOUTHBOUND	7	Through-Right Right		30	0	0	0	30	0	0	32	0	0	0	32	0	0	0	32	0	0
Ō	4	Left-Through-Ri	ight	30	1	U	0	30	U	U	32	1	U	0	32	1	U	U	32	1	U
Ś	٠,	Left-Right			0							0				0				0	
	ر	Left		457	1	157	2	450	159	0	167	1	167	2	100	1	169	0	400	1	169
9	<u></u>	Left-Through		157	0	157		159	159	U	107	0	107		169	0	109	0	169	0	109
l a	→	Through		608	3	203	0	608	203	0	645	3	215	0	645	3	215	0	645	3	215
EASTBOUND	77	Through-Right		00	0	00		00	00		-00	0 1	00		00	0 1	00		00	0	00
AS	*	Right Left-Through-Ri	iaht	22	0	22	0	22	22	0	23	0	23	0	23	0	23	0	23	0	23
ш П	₹	Left-Right	· 9···		0							0				0				0	
9	↓	Left Left-Through		53	1 0	53	0	53	53	0	56	1 0	56	0	56	1 0	56	0	56	1 0	56
WESTBOUND	←	Through		1540	3	513	8	1548	516	0	1635	3	545	8	1643	3	548	0	1643	3	548
TB(م ک	Through-Right			0							0				0				0	
ES)	Right Left-Through-Ri	iaht	29	1 0	29	0	29	29	0	31	1 0	31	0	31	1 0	31	0	31	1 0	31
>	<u>`</u>	Left-Right	igiit		0							0				0				0	
	North-So		th-South:	326		rth-South:	326			th-South:	347			th-South:	347			th-South:	347		
	CRITICAL VOLUMES East-West: SUM:			4	East-West:	675 1001		E	ast-West:	712		Ea	ast-West:	717		Ea	ast-West:	717			
 	VOLUM	ME/CAPACITY (V/C)) RATIO:		SUM:			SUM:	1001			SUM:	1059			SUM:	1064			SUM:	1064
V/C		, ,				0.699			0.702				0.743				0.747				0.747
V/C	//C LESS ATSAC/ATCS ADJUSTMENT: LEVEL OF SERVICE (LOS):					0.599 A			0.602 B				0.643 B				0.647 B				0.647 B
<u></u>			MARKS:			A			D				D				D				D

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT





(Circular 212 Method)

I/S #:	North	h-South Street:	Willama	an Drive			Year	of Count:	2018	Amb	ient Grow	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA05	Eas	st-West Street:	Burton	Way			Projec	tion Year:	2024		Pea	ak Hour:	PM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project
	<u> </u>	No. of	Phases			3			3				3				3				3
Oppo	osed Ø'i	ing: N/S-1, E/W-2 or	Both-3?			0			0				0				0				0
Right	Turns:	FREE-1, NRTOR-2 o	r OLA-3?	NB 0	SB	0	NB	0 SE		NB	0	SB	0	NB	0	SB	0	NB	0	SB	0
	۸-	TSAC-1 or ATSAC+A	TCS 22	EB 0	WB	0 2	EB	0 W	B 0 2	EB	0	WB	0 2	EB	0	WB	0 2	EB	0	WB	0 2
	^	Override (0			0				0				0				0
				EXISTI	NG CONDI	_	EXIST	ING PLUS P	_	FUTUR	E CONDITI	ON W/O PR	ROJECT	FUTU	RE CONDIT	ION W/ PR		FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
0	7	Left		50	0	50	0	50	50	0	53	0	53	0	53	0	53	0	53	0	53
NORTHBOUND	\prec	Left-Through			0							0				0				0	
30	1	Through		132	0	210	0	132	210	0	140	0	223	0	140	0	223	0	140	0	223
≝	1	Through-Right			0	_	_					0				0				0	
I K	^	Right		28	0	0	0	28	0	0	30	0	0	0	30	0	0	0	30	0	0
N	\Rightarrow	Left-Through-Ri	ght		1 0							1 0				1 0				1 0	
	$\uparrow \uparrow$	Left-Right		<u> </u>	U							U				U				U	
	<i>(</i>	Left		141	0	141	0	141	141	0	150	0	150	0	150	0	150	0	150	0	150
¥	\rightarrow	Left-Through			0							0				0	.00			0	.00
0	↓	Through		160	0	325	0	160	325	0	170	0	345	0	170	0	345	0	170	0	345
H	4	Through-Right			0							0				0				0	
5	لہ	Right		24	0	0	0	24	0	0	25	0	0	0	25	0	0	0	25	0	0
SOUTHBOUND	*	Left-Through-Ri	ght		1 0							1 0				1 0				1 0	
	٠,	Left-Right		I	U							U				U				U	
	J	Left		163	1	163	5	168	168	0	173	1	173	5	178	1	178	0	178	1	178
9	<u> </u>	Left-Through			0		_					0				0				0	
EASTBOUND	\rightarrow	Through		1614	3	538	0	1614	538	0	1713	3	571	0	1713	3	571	0	1713	3	571
IB($\overrightarrow{\downarrow}$	Through-Right			0							0				0				0	
AS.	<u>}</u>	Right	4	32	1	32	0	32	32	0	34	1	34	0	34	1	34	0	34	1	34
J.	(ز	Left-Through-Ri Left-Right	gnt		0							0				0				0 0	
	, J	Leit-Nigiit			<u> </u>							J				J				U	
	√	Left		112	1	112	0	112	112	0	119	1	119	0	119	1	119	0	119	1	119
Z	\checkmark	Left-Through			0							0				0				0	
0	<i>₹</i>	Through		863	3	288	5	868	289	0	916	3	305	5	921	3	307	0	921	3	307
18	1	Through-Right			0	6-	_	~-		_	c=	0	6-	_	c=	0				0	6-
WESTBOUND	→	Right	aht.	35	1 0	35	0	35	35	0	37	1 0	37	0	37	1	37	0	37	1 0	37
>	<u>`</u>	Left-Through-Ri Left-Right	yııt		0							0				0				0	
	North-South:			375	No	rth-South:	375		Nor	th-South:	398		Nor	th-South:	398		Nor	th-South:	398		
	CRITICAL VOLUMES East-West: 6			650	_	East-West:	650			ast-West:	690			ast-West:	690			ast-West:	690		
	SUM:			1025		SUM:	1025			SUM:	1088			SUM:	1088			SUM:	1088		
	VOLUME/CAPACITY (V/C) RATIO:			0.719			0.719				0.764				0.764				0.764		
V/C	//C LESS ATSAC/ATCS ADJUSTMENT:					0.619			0.619				0.664				0.664				0.664
	LEVEL OF SERVICE (LOS):					В			В				В				В				В
<u> </u>			<u> </u>																	_	

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project:	0.000	∆v/c after mitigation:	0.00
Significant impacted?	NO	Fully mitigated?	N/A





(Circular 212 Method)

I/S #:	North	h-South Street:	San Vic	ente Boule	/ard		Year	of Count:	2018	Amb	ient Grow	/th: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA06	Eas	st-West Street:	Beverly	Boulevard			Projec	tion Year:	2024		Pea	ak Hour:	AM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Leban	on Project
	1	No. o	f Phases			4			4				4				4				4
Opp	osed Ø'i	ing: N/S-1, E/W-2 or	Both-3?			0			0				0				0				0
Right	Turns:	FREE-1, NRTOR-2	or OLA-3?	NB 0	SB	3	NB	0 SE		NB	0	SB	3	NB	0	SB	3	NB	0	SB	3
	Λ.	TSAC-1 or ATSAC+	ATCS-22	EB 3	WB	3 2	EB	3 W	B 3 2	EB	3	WB	3 2	EB	3	WB	3 2	EB	3	WB	3 2
	^	Override				0			0				0				0				0
				EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTUR	E CONDITION	ON W/O PF	ROJECT	FUTUF	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
	1	Left		84	1	84	0	84	84	18	107	1	107	0	107	1	107	0	107	1	107
Į	4	Left-Through			0							0				0				0	
l õ	1	Through		685	2	343	3	688	344	7	734	2	367	3	737	2	369	0	737	2	369
IE	Ì~	Through-Right		444	0	50	0	444	50		404	0	05	•	404	0	05		404	0	0.5
NORTHBOUND	_^_	Right Left-Through-R	iaht	114	1 0	59	0	114	59	3	124	1 0	65	0	124	1 0	65	0	124	1 0	65
ž	↑	Left-Right	igni		0							0				0				0	
		Lon ragin		<u> </u>																	
	<u> </u>	Left		85	1	85	0	85	85	0	90	1	90	0	90	1	90	0	90	1	90
	→	Left-Through			0							0				0				0	
l Ö		Through		493	2	247	1	494	247	3	526	2	263	1	527	2	264	0	527	2	264
SOUTHBOUND	ل ر	Through-Right Right		182	0 1	129	0	182	129	0	193	0 1	137	0	193	0 1	137	0	193	0	137
ΙŻ	4	Left-Through-R	iaht	102	0	129	U	102	129	U	193	0	137	U	193	0	137	"	193	0	137
Š	بنہ	Left-Right	-5		Ō							0				0				0	
0	<i>_</i> 1	Left		53	1	53	0	53	53	0	56	1	56	0	56	1	56	0	56	1	56
Į	$\stackrel{\longrightarrow}{\longrightarrow}$	Left-Through		007	0 2	04.4	0	007	04.4	07	700	0 2	050	•	700	0 2	050		700	0 2	050
l g	7	Through Through-Right		627	0	314	0	627	314	37	703	0	352	0	703	0	352	0	703	0	352
STE	7	Right		127	1	43	0	127	43	14	149	1	42	0	149	1	42	0	149	1	42
EASTBOUND	\rightarrow	Left-Through-R	ight		0							0				0				0	
	$\sqcup \prec$	Left-Right			0							0				0				0	
	· ~	1 -44		140	1	440		440	440		440	4	440		440	4	440		440	4	440
₽	*	Left Left-Through		110	1 0	110	0	110	110	1	118	1 0	118	0	118	1 0	118	0	118	1 0	118
WESTBOUND	←	Through		1154	2	577	0	1154	577	33	1258	2	629	0	1258	2	629	0	1258	2	629
<u> </u>	4	Through-Right			0	-,,				30	50	0			55	0		l	55	0	
ST	↓	Right		129	1	44	0	129	44	0	137	1	47	0	137	1	47	0	137	1	47
×	T.	Left-Through-R	ight		0							0				0				0	
<u> </u>	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	Left-Right		A1	0	420	A1-	wth Courte	429		Al	0	AE7		Al	0	450		Ale	0	4F0
					428 630		rth-South: East-West:	429 630			th-South: ast-West:	457 685			h-South: st-West:	459 685			th-South: ast-West:	459 685	
				1058	'	SUM:	1059		Le	SUM:	1142			SUM:			E	SUM:	1144		
	101111111111111111111111111111111111111			0.769			0.770				0.831				0.832				0.832		
V/C	//C LESS ATSAC/ATCS ADJUSTMENT:					0.669			0.670				0.031				0.032				0.032
"						0.669 B			0.670 B				0.731 C				0.732 C				0.732 C
<u> </u>	LEVEL OF SERVICE (LOS):					D			Ď				U				U				U

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

3/8/2019-11:53 AM 1 CMA06





(Circular 212 Method)

I/S #:	Nort	th-South Street:	San Vio	cente Boule	vard		Year	of Count:	2018	Amb	ient Grow	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA06	Ea	ast-West Street:	Beverly	/ Boulevard			Projec	tion Year:	2024		Pea	ak Hour:	PM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project
	<u>.</u>		f Phases			4			4				4				4	-			4
Oppo	osed Ø	ö'ing: N/S-1, E/W-2 or	Both-3?		ı	0			0			ı	0			ı	0				0
Right	Turns	: FREE-1, NRTOR-2	or OLA-3?	NB 0	SB	3	NB EB	0 SE 3 W		NB	0 3	SB WB	3	NB EB	0	SB WB	3	NB EB	0	SB WB	3
		ATSAC-1 or ATSAC+	ATCS-22	EB 3	WB	3 2	EB	3 W	B 3 2	EB	3	WB	3	EB	3	WB	3 2	EB	3	WB	3 2
	•	Override				0			0				0				0				0
				EXISTI	NG CONDI	TION	EXIST	ING PLUS PI	ROJECT	FUTUR	E CONDITI	ON W/O PR	ROJECT	FUTUF	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
٥	J.	Left		108	1	108	0	108	108	37	152	1	152	0	152	1	152	0	152	1	152
N N	4	Left-Through			0							0				0				0	
90	Î	Through		713	2	357	2	715	358	8	765	2	383	2	767	2	384	0	767	2	384
NORTHBOUND	Ŷ	Through-Right		424	0	384	0	424	384	2	452	0 1	408	0	452	0	408	0	452	0	408
OR.	←	Right Left-Through-R	iaht	424	0	304	U	424	304	2	432	0	400	U	432	0	400	"	432	0	400
ž	₹	Left-Right	·g···		0							0				0				0	
D	<u> </u>	Left		215	1	215	0	215	215	0	228	1	228	0	228	1	228	0	228	1	228
N S	→	Left-Through			0		_					0				0		_		0	
BO	ز ا	Through Through-Right		481	2	241	3	484	242	11	522	2	261	3	525	2	263	0	525	2	263
∓	ر ا	Right		127	1	56	0	127	56	0	135	1	60	0	135	1	60	0	135	1	60
SOUTHBOUND	4	Left-Through-R	ight	121	0	30	0	127	30	U	100	0	00		100	0	00	"	155	0	00
Š	, ا	Left-Right			0							0				0				0	
٥	<i>→</i>	Left Left-Through		71	1 0	71	0	71	71	0	75	1 0	75	0	75	1 0	75	0	75	1 0	75
N	\rightarrow	Through		828	2	414	0	828	414	74	953	2	477	0	953	2	477	0	953	2	477
EASTBOUND	7	Through-Right		020	0	717		020	7.7	74	300	0	711		300	0	4//	"	333	0	7//
ST	7	Right		72	1	0	0	72	0	32	108	1	0	0	108	1	0	0	108	1	0
EA	1	Left-Through-R	ight		0							0				0				0	
	I ≺_	Left-Right			0							0				0				0	
	· ~	Left		80	1	80	0	80	80	3	88	1	88	0	88	1	88	0	88	1	88
N N	7	Left-Through		00	Ö	00		00	00	3	00	0	00		00	0	00		00	0	00
WESTBOUND	←	Through		768	2	384	0	768	384	78	893	2	447	0	893	2	447	0	893	2	447
∥ IB(<u></u>	Through-Right			0							0				0				0	
ES.	→	Right	! I- 4	137	1	0	0	137	0	0	145	1	0	0	145	1	0	0	145	1	0
>	\ _	Left-Through-R Left-Right	ignt		0							0				0				0	
				Non	th-South:	599	No	rth-South:	599		Non	th-South:	636		Non	th-South:	636		Nor	th-South:	636
	CRITICAL VOLUMES East-Wes				494		ast-West:	494			ast-West:	565			ast-West:	565			ast-West:	565	
				SUM:	1093		SUM:	1093			SUM:	1201			SUM:	1201			SUM:	1201	
	VOLUME/CAPACITY (V/C) RATIO:					0.795			0.795				0.873				0.873				0.873
V/C	/C LESS ATSAC/ATCS ADJUSTMENT:					0.695			0.695				0.773				0.773				0.773
	LEVEL OF SERVICE (LOS):					В			В				С				С				С
<u>ш</u>				<u> </u>																	

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT





(Circular 212 Method)

I/S #:	North	-South Street:	Sherbo	urne Drive			Year	of Count:	2018	Amb	ient Grow	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA07	Eas	st-West Street:	3rd Stre	eet			Projec	tion Year:	2024		Pea	ak Hour:	AM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project
	<u> </u>		Phases			2			2				2				2	-			2
Oppo	osed Ø'ir	ng: N/S-1, E/W-2 or	Both-3?			0			0			ı	0			ı	0				0
Right	Turns: F	FREE-1, NRTOR-2 o	r OLA-3?	NB 0	SB	0	NB EB	0 SE		NB	0	SB WB	0	NB EB	0	SB WB	0	NB EB	0	SB	0
	ΔΤ	SAC-1 or ATSAC+	ATCS-22	EB 0	WB	0 2	EB	0 W	B 0 2	EB	U	WB	2	EB	U	WB	0 2	EB	0	WB	2
	^'	Override (0			0				0				0				0
				EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTUR	E CONDITI	ON W/O PR	ROJECT	FUTU	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
Q	j	Left		19	0	19	5	24	24	0	20	0	20	5	25	0	25	0	25	0	25
	4	Left-Through			0							0				0				0	
l o	1	Through		80	0	114	0	80	119	0	85	0	121	0	85	0	126	0	85	0	126
∄	P ₂	Through-Right		45	0	0	0	45	0	0	40	0	0		40	0	0		40	0	0
NORTHBOUND		Right Left-Through-Ri	aht	15	1	0	0	15	0	0	16	1	U	0	16	1	U	0	16	1	0
ž	*	Left-Right	gnı		0							0				0				0	
		LCIT-Right		<u>l</u>																	
	\ \	Left		34	0	34	0	34	34	0	36	0	36	0	36	0	36	0	36	0	36
SOUTHBOUND	>	Left-Through			0							0				0				0	
l g	Through Through-Right			3	0	81	0	3	81	0	3	0	86	0	3	0	86	0	3	0	86
1 2 1	Through Through-Right			0		•				47	0 0			47	0	•		47	0 0	0	
5	→	Right Left-Through-Ri	aht	44	1	0	0	44	0	0	47	1	0	0	47	1	0	0	47	1	0
S	,	Left-Right	9		0							0				0				0	
				l																	
		Left		139	1	139	0	139	139	0	148	1	148	0	148	1	148	0	148	1	148
l ĭ	<i>→</i>	Left-Through			0		_			_		0		_		0				0	
l g	$\overrightarrow{7}$	Through Through-Right		547	1	278	3	550	280	7	588	1	299	3	591	1	301	0	591	1	301
l E	7	Right		9	0	9	0	9	9	0	10	0	10	0	10	0	10	0	10	0	10
EASTBOUND	→	Left-Through-Ri	aht	3	0	9	U	3	3	0	10	0	10	U	10	0	10	"	10	0	10
ш ш	⊰	Left-Right	•		0							0				0				0	
	,			-																	
۵	₹	Left		54	1	54	0	54	54	0	57	1	57	0	57	1	57	0	57	1	57
3	<i>↓</i>	Left-Through Through		4400	0 2	552	0	4400	550	_	4470	0 2	500		4470	0 2	500		4470	0 2	500
<u>8</u>	ئ	Through-Right		1103	0	552	0	1103	552	7	1178	0	589	0	1178	0	589	0	1178	0	589
STI	<u>~</u>	Right		214	1	214	0	214	214	0	227	1	227	0	227	1	227	0	227	1	227
WESTBOUND	→	Left-Through-Ri	ght		0							0				0				0	
	>	Left-Right	_		0							0				0				0	
					148	_	rth-South:	153			th-South:	157			th-South:	162			th-South:	162	
				691	"	East-West:	691		Ea	ast-West:	737		Ea	ast-West:	737		E	ast-West:	737		
<u> </u>	VOLUME/CAPACITY (V/C) RATIO:			839		SUM:	844			SUM:	894			SUM:	899			SUM:	899		
	, ,				0.559			0.563				0.596				0.599				0.599	
V/C	C LESS ATSAC/ATCS ADJUSTMENT:					0.459			0.463				0.496				0.499				0.499
	LEVEL OF SERVICE (LOS):					Α			Α				Α				Α	<u></u>			Α

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project: 0.003 Significant impacted? NO

 $\Delta v/c$ after mitigation: 0.003 Fully mitigated? N/A

CMA07

3/8/2019-11:55 AM





(Circular 212 Method)

I/S #:	North	n-South Street:	Sherbo	urne Drive			Year	of Count:	2018	Amb	ient Grow	/th: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA07	Eas	st-West Street:	3rd Str	eet				tion Year:			Pea	k Hour:	PM		wed by:		AS		Our Lady o		on Project
	<u> </u>	No. o	f Phases			2			2				2				2	,			2
Oppo	osed Ø'i	ing: N/S-1, E/W-2 or	Both-3?			0			0				0				0				0
Right	Turns:	FREE-1, NRTOR-2	or OLA-3?	NB 0	SB	0	NB	0 SI		NB	0	SB	0	NB	0	SB	0	NB	0	SB	0
		TSAC-1 or ATSAC+		EB 0	WB	0	EB	0 W		EB	0	WB	0 2	EB	0	WB	0	EB	0	WB	0 2
	A	Override				2			2				0				2				0
		Override	Oupdoity	EXISTI	NG CONDI		EXIST	NG PLUS P	•	FUTUR	E CONDITION	ON W/O PR		FUTUE	RE CONDIT	ON W/ PR	•	FUTURE	W/ PROJE	CT W/ MIT	_
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
0	7	Left		12	0	12	3	15	15	0	13	0	13	3	16	0	16	0	16	0	16
NORTHBOUND	4	Left-Through			0							0				0				0	
) M	1	Through		37	0	84	0	37	87	0	39	0	89	0	39	0	92	0	39	0	92
IE	Ì~	Through-Right		0.5	0		•	0.5	•	•	07	0	•		07	0	0		07	0	0
L K	. 1	Right	: 4	35	0	0	0	35	0	0	37	0 1	0	0	37	0	0	0	37	0	0
ĭ	♦	Left-Through-R Left-Right	igiit		0							0				0			1 0		
		Leit-Right		<u> </u>																<u> </u>	
	Ģ	Left		138	0	138	0	138	138	0	146	0	146	0	146	0	146	0	146	0	146
SOUTHBOUND	>	Left-Through			0							0				0				0	
l g	1	Through		97	0	391	0	97	391	0	103	0	415	0	103	0	415	0	103	0	415
IE	4	Through-Right		450	0	0	0	450	0	0	400	0	0		400	0	0		400	0	0
5	↓	Right Left-Through-R	iaht	156	1	0	0	156	0	0	166	0 1	0	0	166	1	0	0	166	0	0
SC	<i>_</i>	Left-Right	igiit		0							0				0				0	
	٨	Left		49	1	49	0	49	49	0	52	1	52	0	52	1	52	0	52	1	52
l ₹		Left-Through			0							0				0				0	
EASTBOUND	$\overrightarrow{\gamma}$	Through		683	1	362	8	691	366	16	741	1	393	8	749	1	397	0	749	1	397
l E	7	Through-Right Right		41	0	41	0	41	41	0	44	0	44	0	44	0	44	0	44	0	44
- AS	→	Left-Through-R	iaht	41	0	41	U	41	41	U	44	0	44	0	44	0	44		44	0	44
ш ш	⊰	Left-Right	J		0							0				0				0	
۵	<i>√</i>	Left		55	1	55	0	55	55	0	58	1	58	0	58	1	58	0	58	1	58
3	<i>₹</i>	Left-Through		500	0 2	000	0	500	000	45	00.4	0	047		00.4	0 2	047		004	0 2	047
WESTBOUND	4	Through Through-Right		583	0	292	0	583	292	15	634	2	317	0	634	0	317	0	634	0	317
STI	Ć.	Right		58	1	58	0	58	58	0	62	1	62	0	62	1	62	0	62	1	62
۷Ë	→	Left-Through-R	ight		0			00			0_	0	0_			0	02			0	02
	}	Left-Right			0							0				0				0	
		ODITIO	01.11450		th-South:	403		rth-South:	406			h-South:	428			h-South:	431			th-South:	431
		CRITICAL V	OLUMES	Ea	ast-West:	417 820	"	East-West:	421 827		Ea	ast-West:	451 879		Ea	st-West:	455 886		E	ast-West:	455 886
 	VOLU	ME/CAPACITY (V/C) PATIO:		SUM:			SUM:				SUM:				SUM:				SUM:	
		• •	•			0.547			0.551				0.586				0.591				0.591
V/C		TSAC/ATCS ADJUS				0.447			0.451				0.486				0.491				0.491
		LEVEL OF SERVIC	E (LOS):			Α			Α				Α				Α				Α

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project: 0.005 $\Delta v/c$ after Significant impacted? NO Fully

 $\triangle v/c$ after mitigation: 0.005 Fully mitigated? N/A





(Circular 212 Method)

I/S #:	Nort	E FREE-1 NRIUR-2 OF ULA-37 I		vard		Year	of Count:	2018	Amb	ient Grov	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019		
CMA08	Ea	No. of Phases Fing: N/S-1, E/W-2 or Both-3? FREE-1, NRTOR-2 or OLA-3? NB 0 SB-					Projec	tion Year:	2024		Pe	ak Hour:	AM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project
1		'ing: N/S-1, E/W-2 or	Both-3?	NP 0	C.D.	2 0 0	NB	0 SI	2 0 8 0	NB	0	SB	2 0 0	NB	0	SB	2 0 0	NB	0	SB	2 0 0
Right	Turns:	FREE-1, NRTOR-2 o	or OLA-3?		ЗВ WB	0	NB EB		B 0	NB EB	0	3В WВ	0	NB EB	0	3В WВ	0	NB EB	0	ЗВ WB	0
	Δ	ATSAC-1 or ATSAC+				2		-	2				2				2				2
		Override (Capacity			0			0				0				0				0
		MOVEMENT		EXIST	NG CONDI			ING PLUS P		Added	Total	ON W/O PR	Lane	Added	RE CONDIT	No. of		Added	Total	No. of	
		MOVEMENT		Volume	Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Volume	Volume	No. of Lanes	Volume	Volume	Volume	Lanes	Lane Volume	Volume	Volume	Lanes	Lane Volume
D	J .	Left		102	1	102	0	102	102	2	110	1	110	0	110	1	110	0	110	1	110
NORTHBOUND	7	Left-Through Through		572	0 1	293	0	572	293	21	628	0 1	346	0	628	0 1	346	0	628	0	346
<u>B</u> C	 	Through-Right		312	1	293	U	312	293	21	020	1	340	0	020	1	340		020	1	340
革	<u>ب</u>	Right		13	0	13	0	13	13	49	63	0	63	0	63	0	63	0	63	0	63
9 N	\(\phi\)	Left-Through-Ri	ght		0							0				0				0	
	$\uparrow \uparrow$	Left-Right		L	0							0				0				0	
		Left		116	1	116	0	116	116	3	126	1	126	0	126	1	126	0	126	1	126
SOUTHBOUND	→	Left-Through			0							0				0				0	
BO	1	Through Through-Right		447	2	224	1	448	224	9	483	2	242	1	484	2	242	0	484	2	242
I	زہ	Right		92	1	51	0	92	50	7	105	1	58	0	105	1	57	0	105	1	57
nog	\leftrightarrow	Left-Through-Ri	ght		0					-		0				0	-			0	
0,	٠,	Left-Right			0							0				0				0	
	<i>J</i>	Left		82	1	82	3	85	85	7	94	1	94	3	97	1	97	0	97	1	97
9		Left-Through		02	0	02		00			0.	0	-		01	0	Ů.		O,	0	V.
9	$\overrightarrow{\gamma}$	Through		483	2	242	8	491	246	6	519	2	260	8	527	2	264	0	527	2	264
EASTBOUND	\rightarrow	Through-Right Right		68	0 1	17	1	69	18	3	75	0 1	20	1	76	0 1	21	0	76	0 1	21
EAS	→	Left-Through-Ri	ght	00	0	.,	•	00	10		70	0	20	•	70	0	21		70	0	21
	\dashv	Left-Right			0							0				0				0	
	<i>(</i>	Left		54	1	54	1	55	55	3	60	1	60	1	61	1	61	0	61	1	61
Q.	,	Left-Through		J-7	Ö	J-1	' '	55	55		50	0	30	'	01	Ö	- 51		51	0	51
WESTBOUND	<u>₹</u>	Through		1217	1	704	0	1217	704	0	1292	1	748	0	1292	1	748	0	1292	1	748
TB.	₹.	Through-Right Right		191	1 0	191	0	191	191	0	203	1 0	203	0	203	1 0	203	0	203	1 0	203
VES	→	Left-Through-Ri	ght	191	0	191	U	191	191	U	203	0	203	U	203	0	203		203	0	203
_	}	Left-Right			0							0				0				0	
		CRITICAL VO	OI LIMES		th-South: ast-West:	409 786		rth-South: East-West:	409 789			th-South: ast-West:	472 842			th-South: ast-West:	472 845			th-South: ast-West:	472 845
		CHITOAL V			ast-west: SUM:		'	:ast-west: SUM:	1198		E	SUM:	1314		E	SUM:	1317		E	SUM:	845 1317
	VOLU	JME/CAPACITY (V/C)	RATIO:			0.797			0.799				0.876				0.878				0.878
V/C	LESS A	ATSAC/ATCS ADJUS	TMENT:			0.697			0.699				0.776				0.778				0.778
		LEVEL OF SERVIC	E (LOS):			В			В				С				С				С
<u> </u>		DE	MARKS:																		

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

3/8/2019-11:55 AM 1 CMA08





(Circular 212 Method)

I/S #:	North	h-South Street:	San Vic	ente Boule	/ard		Year	of Count:	2018	Amb	ient Grow	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA08	Eas	st-West Street:			Projec	tion Year:	2024		Pea	ak Hour:	PM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project		
	Į.		Phases			2			2				2				2	-			2
Oppo	osed Ø'i	ing: N/S-1, E/W-2 or	Both-3?			0			0			ı	0			ı	0				0
Right	Turns:	FREE-1, NRTOR-2 o	r OLA-3?	NB 0	SB	0	NB EB	0 SE		NB	0	SB WB	0	NB EB	0	SB WB	0	NB EB	0	SB WB	0
	Δ.	TSAC-1 or ATSAC+	ATCS-22	EB 0	WB	0 2	EB	0 W	B 0 2	EB	U	WB	2	EB	U	WB	0 2	EB	U	WB	2
	^	Override (0			0				0				0				0
				EXISTI	NG CONDI	TION	EXIST	ING PLUS PI	ROJECT	FUTUR	E CONDITI	ON W/O PR	ROJECT	FUTUF	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
٥	j	Left		46	1	46	0	46	46	2	51	1	51	0	51	1	51	0	51	1	51
N S	4	Left-Through			0							0				0				0	
NORTHBOUND	Î	Through		451	1	244	0	451	244	29	508	1	292	0	508	1	292	0	508	1	292
IE	Ŷ	Through-Right		36	1 0	26	0	36	36	37	75	1 0	75	0	75	1 0	75	0	75	1 0	75
N.		Right Left-Through-Ri	aht	30	0	36	U	30	30	31	75	0	75	U	75	0	75	"	75	0	75
ž	♦	Left-Right	giit		0							0				0				0	
	_ '			l																	
	<i>-</i>	Left		298	1	298	0	298	298	6	322	1	322	0	322	1	322	0	322	1	322
SOUTHBOUND	>	Left-Through			0							0				0				0	
l o		Through		577	2	289	3	580	290	26	638	2	319	3	641	2	321	0	641	2	321
본	ر ا	Through-Right Right		170	0	98	0	170	97	15	195	0 1	110	0	195	0 1	109	0	195	0	109
).	4	Left-Through-Ri	aht	170	0	90	U	170	91	15	195	0	110	U	195	0	109	"	195	0	109
SC	į,	Left-Right	g		0							0				Ö				0	
	<i></i>	Left		145	1	145	2	147	147	16	170	1	170	2	172	1	172	0	172	1	172
ΙŽ	<i>→</i>	Left-Through		007	0 2	00.4	_	070	000	40	704	0	004	_	700	0	000		700	0 2	000
EASTBOUND	7	Through Through-Right		667	0	334	5	672	336	13	721	2	361	5	726	2	363	0	726	0	363
STE	<i>-</i> ,	Right		51	1	28	2	53	30	16	70	1	45	2	72	1	47	0	72	1	47
EA	\rightarrow	Left-Through-Ri	ght		0		_					0				0				0	
		Left-Right			0							0				0				0	
	· ~	l oft			1	0		40	40	4.4	0.4	4	0.4		07	1	07		07	1	07
₽	₹	Left Left-Through		9	0	9	3	12	12	14	24	1 0	24	3	27	0	27	0	27	1 0	27
WESTBOUND	←	Through		525	1	342	0	525	342	0	557	1	363	0	557	1	363	0	557	1	363
_BC	4	Through-Right		323	1			0_0		Ĭ		1				1				1	
EST	₹	Right		158	0	158	0	158	158	0	168	0	168	0	168	0	168	0	168	0	168
WE		Left-Through-Ri	ght		0							0				0				0	
	Γ	Left-Right		A'	0	E40	A1-	with Counties	542		A/	0	61.4		A/	0	614		A/	0	614
		CRITICAL VO	DLUMES	-	th-South: ast-West:	542 487	_	rth-South: East-West:	542 489			th-South: ast-West:	614 533			th-South: ast-West:	614 535			th-South: ast-West:	614 535
		S. HI I OF LE V		[SUM:	1029	"	SUM:	1031		E	SUM:	1147		E	SUM:	1149		E	SUM:	1149
	VOLU	ME/CAPACITY (V/C)	RATIO:			0.686		30	0.687				0.765			J J	0.766			20	0.766
V/C		ATSAC/ATCS ADJUS				0.586			0.587				0.765				0.766				0.766
1,0		LEVEL OF SERVIC											0.000 B				В				
<u> </u>		LEVEL OF SERVIC	L (LU3):			Α			Α				B				В				В

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT





(Circular 212 Method)

I/S #:	North	h-South Street:	San Vic	ente Boule	vard-Le D	oux Roa	Year	of Count:	2018	Amb	ient Grov	/th: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA09	Eas	st-West Street:	No. of Phases 1, E/W-2 or Both-3? NRTOR-2 or OI A-32 NBTOR-2 or OI A-32				Projec	tion Year:	2024		Pea	ak Hour:	AM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Leban	on Project
	1					3			3				3				3				3
Oppo	osed Ø'i	ing: N/S-1, E/W-2 or	Both-3?			0			0		_		0				0				0
Right	Turns:	FREE-1, NRTOR-2 o	r OLA-3?	NB 0 EB 0	SB WB	0	NB EB	0 SE 0 W		NB EB	0	SB WB	0	NB EB	0	SB WB	0	NB EB	0	SB WB	0
	Δ-	TSAC-1 or ATSAC+A	ATCS-27	EB U	WB	2	EB	U VVI	2	EB	U	WB	2	EB	U	WB	2	EB	U	WB	2
	^	Override (0			0				0				0				0
				EXISTI	NG CONDI	TION	EXIST	ING PLUS PI	ROJECT	FUTUR	E CONDITI	ON W/O PR	OJECT	FUTUF	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
D	j	Left		29	1	29	0	29	29	0	31	1	31	0	31	1	31	0	31	1	31
NORTHBOUND	4	Left-Through		_	0		_	_		_		0		_		0	_		_	0	_
90	1	Through		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
₹	ŕ	Through-Right		24	0	15	0	24	15	0	25	0 1	15	0	25	0	15	0	25	0	15
OR.	↔	Right Left-Through-Ri	aht	24	0	15	0	24	15	U	25	0	15	U	25	0	15	"	25	0	15
ž	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	Left-Right	giit		0							0				0				0	
	•											-									
٥	<i>-</i>	Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
N	<u>}</u>	Left-Through			0							0				0				0	
90	1	Through		460	1	281	8	468	285	7	495	1	301	8	503	1	305	0	503	1	305
SOUTHBOUND	رُ	Through-Right Right		101	0	101	0	101	101	0	107	0	107	0	107	0	107	0	107	0	107
l in	4	Left-Through-Ri	aht	101	0	101	0	101	101	U	107	0	107	U	107	0	107	"	107	0	107
Š	بلہ	Left-Right	•		0							0				0				0	
	<i>→</i>	Left		12	0	0	0	12	0	0	13	0	0	0	13	0	0	0	13	0	0
ΙZ	\rightarrow	Left-Through Through		caa	0 2	224		000	004		070	0 2	225	0	070	0 2	225		670	0 2	225
EASTBOUND	7	Through-Right		633	1	221	0	633	221	0	672	1	235	0	672	1	235	0	672	1	235
STI	<i>-</i> }	Right		31	0	31	0	31	31	0	33	0	33	0	33	0	33	0	33	0	33
EA	\rightarrow	Left-Through-Ri	ght		0							0				0				0	
	_ ≺	Left-Right			0							0				0				0	
	<i>(</i>	Left		10	1	10		10	10		20	1	20	0	20	1	20		20	1	20
9	*	Left Left-Through		19	0	19	0	19	19	0	20	0	20	0	20	0	20	0	20	0	20
á	←	Through		1612	2	584	4	1616	585	12	1723	2	624	4	1727	2	625	0	1727	2	625
WESTBOUND	4	Through-Right			1						0	1		·		1				1	
EST	€	Right		722	1	0	0	722	0	7	773	1	0	0	773	1	0	0	773	1	0
×	\(Left-Through-Ri	ght		0							0				0				0	
	<i></i>	Left-Right		Non	th-South:	310	Al-	rth-South:	314		Non	th-South:	332		Non	th-South:	336		Non	th-South:	336
		CRITICAL VO	DLUMES		ın-souun: ast-West:	584	_	East-West:	585			ast-West:	624			ın-souun: ast-West:	625			ast-West:	625
			-	[SUM:	894	_	SUM:	899			SUM:	956			SUM:	961		_	SUM:	961
	VOLUI	ME/CAPACITY (V/C)	RATIO:			0.627			0.631				0.671				0.674			0.674	
V/C	LESS A	ATSAC/ATCS ADJUS	TMENT:			0.527			0.531				0.571				0.574				0.574
		LEVEL OF SERVICE				Α			Α				Α					Α			0.374 A
<u></u>		LL.LL OI OLIVIO	_ (200).			A			A				A				A				A

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

3/8/2019-11:55 AM 1 CMA09





(Circular 212 Method)

I/S #:	Nort	h-South Street:	San Vic	ente Boule	/ard-Le D	oux Roa	Year	of Count:	2018	Amb	ient Grow	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA09	Ea	st-West Street:			Projec	tion Year:	2024		Pea	ak Hour:	PM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project		
	Į.		Phases			3			3				3				3	-			3
Oppo	osed Ø'	'ing: N/S-1, E/W-2 or	Both-3?			0			0			ı	0			ı	0				0
Right	Turns:	FREE-1, NRTOR-2 o	r OLA-3?	NB 0	SB	0	NB	0 SE		NB	0	SB	0	NB	0	SB	0	NB	0	SB	0
	Δ	ATSAC-1 or ATSAC+/	ATCS-22	EB 0	WB	0 2	EB	0 W	B 0 2	EB	0	WB	0 2	EB	0	WB	0 2	EB	0	WB	0 2
		Override (0			0				0				0				0
				EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTUR	E CONDITI	ON W/O PR	ROJECT	FUTU	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
٥	j	Left		67	1	67	0	67	67	0	71	1	71	0	71	1	71	0	71	1	71
NORTHBOUND	\dashv	Left-Through			0							0				0				0	
90	Î	Through		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
IE	<u>F</u>	Through-Right		38	0	20	0	38	20	0	40	0 1	21	0	40	0	21	0	40	0	21
R.		Right Left-Through-Ri	aht	30	0	20	U	30	20	U	40	0	21	U	40	0	21	"	40	0	21
ž	†	Left-Right	giit		0							0				0				0	
		Lon ragin		<u> </u>																	
	, ·	Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
SOUTHBOUND	>	Left-Through			0							0				0				0	
30	∤	Through		450	1	238	5	455	240	15	493	1	260	5	498	1	263	0	498	1	263
≝	4	Through-Right Right		0.5	1 0	25	0	25	0.5	0	07	1 0	07	0	07	1 0	27		07	1 0	07
	4	Left-Through-Ri	aht	25	0	25	0	25	25	U	27	0	27	U	27	0	27	0	27	0	27
SC	j	Left-Right	9111		0							0				0				0	
		J																			
		Left		20	0	0	0	20	0	0	21	0	0	0	21	0	0	0	21	0	0
l ĭ	<i>→</i>	Left-Through			0		_			_		0		_		0		_		0	
EASTBOUND	$\overrightarrow{\neg}$	Through Through-Right		1820	2	623	0	1820	623	0	1932	2	661	0	1932	2	661	0	1932	2	661
TE	7	Right		48	0	48	0	48	48	0	51	0	51	0	51	0	51	0	51	0	51
SE	→	Left-Through-Ri	ght	40	0	40	U	40	70	0	31	0	31		31	0	31		31	0	31
	₹	Left-Right	•		0							0				0				0	
				-																	
۵	<i>₹</i>	Left		36	1	36	0	36	36	0	38	1	38	0	38	1	38	0	38	1	38
S	<i>↓</i>	Left-Through Through		046	0 2	339	12	920	242	10	970	0 2	267	10	902	0 2	370	0	892	0 2	270
	₹_	Through-Right		816	1	339	13	829	342	13	879	1	367	13	892	1	370	"	092	1	370
STI	<u></u>	Right		540	1	0	0	540	0	16	589	1	0	0	589	i	0	0	589	1	0
WESTBOUND	→	Left-Through-Ri	ght		0							0				0		-		0	-
	}	Left-Right			0							0				0				0	
		CDITICAL V	N LIMES	_	th-South:	305	_	rth-South:	307			th-South:	331			th-South:	334			th-South:	334
		CRITICAL VO	DLUMES	l Ea	ast-West:	659 964	"	East-West:	659 966		Ea	ast-West:	699 1030		Ea	ast-West:	699 1033		E	ast-West:	699
 	VOLU	IME/CAPACITY (V/C)	DATIO:		SUM:			SUM:				SUM:				SUM:				SUM:	1033
14/2		• •				0.676			0.678				0.723				0.725				0.725
V/C	LESS A	ATSAC/ATCS ADJUS				0.576			0.578				0.623				0.625				0.625
		LEVEL OF SERVIC	E (LOS):			Α			Α				В				В				В

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project:	0.002	∆v/c after mitigation:	0.002
Significant impacted?	NO	Fully mitigated?	N/A





(Circular 212 Method)

I/S #:	North	S: FREE-1. NRTUR-2 OF ULA-3 ()		ard		Year	of Count:	2018	Amb	ient Grov	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019		
CMA11	Eas	No. of Phases ing: N/S-1, E/W-2 or Both-3? FREE-1 NRTOR-2 or OLA-32					Projec	tion Year:	2024		Pea	ak Hour:	AM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Lebano	on Project
		ing: N/S-1, E/W-2 or	Both-3?	NB 3	SB	4 0 0	NB	3 SI	4 0 8 0	NB	3	SB	4 0 0	NB	3	SB	4 0 0	NB	3	SB	4 0 0
Kigiit		•		EB 3	WB	3	EB	3 W		EB	3	WB	3	EB	3	WB	3	EB	3	WB	3
	A	TSAC-1 or ATSAC+/ Override				2			2				2				2				2
				EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTUR	E CONDITI	ON W/O PR	OJECT	FUTUF	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
ļ				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
9		Left Left-Through		65	1 0	65	0	65	65	2	71	1 0	71	0	71	1 0	71	0	71	1 0	71
NORTHBOUND	7	Through		776	2	388	3	779	390	21	845	2	423	3	848	2	424	0	848	2	424
Ĕ	<u> </u>	Through-Right			0							0				0				0	
I.R.	<u> </u>	Right		168	1	0	2	170	0	1	179	1	0	2	181	1	0	0	181	1	0
ž	$\overset{\diamondsuit}{\rightsquigarrow}$	Left-Through-Ri Left-Right	ght		0							0				0				0	
		Lort-ragin		<u>I</u>																	
Ω	نہ	Left		70	1	70	0	70	70	8	82	1	82	0	82	1	82	0	82	1	82
SOUTHBOUND		Left-Through Through		940	0 2	405	1	941	406	28	1026	0 2	444	1	1027	0 2	445	0	1027	0 2	445
單	4	Through-Right		340	1	403	'	341	700	20	1020	1		'	1027	1	440		1027	1	445
5	ر ا	Right		276	0	276	0	276	276	14	307	0	307	0	307	0	307	0	307	0	307
SO	→ →	Left-Through-Ri Left-Right	ght		0 0							0				0 0				0 0	
	24	Lort-ragin		I																	
0		Left		127	2	70	0	127	70	14	149	2	82	0	149	2	82	0	149	2	82
N S	$\stackrel{\longrightarrow}{\rightarrow}$	Left-Through Through		590	0 2	295	0	590	295	24	650	0 2	325	0	650	0 2	325	0	650	0 2	325
99	_ ₹	Through-Right		000	0	200		000	200		000	0	020		000	0	020		000	0	020
EASTBOUND	<u>}</u>	Right	1-4	86	1	21	0	86	21	3	94	1	23	0	94	1 0	23	0	94	1	23
Э	→	Left-Through-Ri Left-Right	gnt		0							0				0				0 0	
		J																			
Ω	₹	Left Left-Through		486	2 0	267	1	487	268	1	517	2 0	284	1	518	2	285	0	518	2	285
WESTBOUND	←	Through		975	2	488	0	975	488	19	1054	2	527	0	1054	2	527	0	1054	2	527
I BE	4	Through-Right			0							0				0				0	
ĘŞ.	→	Right Left-Through-Ri	aht.	74	1 0	4	0	74	4	4	83	1 0	1	0	83	1 0	1	0	83	1 0	1
>	<u>;</u>	Left-Right	gni		0							0				0				0	
		CRITICAL VO	OLUMES		th-South: ast-West:	470 562		rth-South: East-West:	471 563			th-South: ast-West:	515 609			th-South: ast-West:	516 610			th-South: ast-West:	516 610
					SUM:			SUM:	1034			SUM:	1124			SUM:				SUM:	1126
	VOLU	ME/CAPACITY (V/C)	RATIO:			0.751			0.752				0.817				0.819				0.819
V/C	LESS A	ATSAC/ATCS ADJUS	TMENT:			0.651			0.652				0.717				0.719				0.719
		LEVEL OF SERVICE (LOS):		В			В				С				С				С		
		DE	WARKS:																		

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project:	0.002	∆v/c after mitigation:	0.002
Significant impacted?	NO	Fully mitigated?	N/A

3/8/2019-11:56 AM 1 CMA11





(Circular 212 Method)

I/S #:	Nort	th-South Street:	La Cien	ega Boulev	ard		Year	of Count:	2018	Amb	ient Grov	vth: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA11	E	ast-West Street:	Beverly	Boulevard			Projec	tion Year:	2024		Pe	ak Hour:	PM	Revie	wed by:	J	AS	Project:	Our Lady o	f Mt. Leban	on Project
,			f Phases			4			4				4				4				4
1		i'ing: N/S-1, E/W-2 or		NB 3	SB	0	NB	3 SI	0 B 0	NB	3	SB	0	NB	3	SB	0	NB	3	SB	0
Right	Turns	: FREE-1, NRTOR-2 o	or OLA-3?	EB 3	WB	3	EB	3 W		EB	3	WB	3	EB	3	WB	3	EB	3	WB	3
		ATSAC-1 or ATSAC+				2			2				2				2				2
		Override	Capacity			0			0				0				0				0
		MOVEMENT		EXISTI	NG CONDI			ING PLUS P	1			ON W/O PR			RE CONDIT				W/ PROJE		
		MOVEMENT		Volume	No. of Lanes	Lane Volume	Project Traffic	Total Volume	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume	Added Volume	Total Volume	No. of Lanes	Lane Volume
	1	Left		95	1	95	0	95	95	4	105	1	105	0	105	1	105	0	105	1	105
R	4	Left-Through			0					-		0				0				0	
NORTHBOUND	Ì	Through		1053	2	527	2	1055	528	38	1156	2	578	2	1158	2	579	0	1158	2	579
ᄩ	Ì	Through-Right		400	0	000		400	000		400	0	054		400	0	050	•	400	0	050
S	م ح1ء	Right Left-Through-Ri	iaht	402	1	238	1	403	238	2	429	1 0	254	1	430	1	253	0	430	1 0	253
ž	$\stackrel{\leftrightarrow}{\gamma}$	Left-Right	igiit		0							0				0				0	
		- J																			
₽	Ĺ	Left		114	1	114	0	114	114	10	131	1	131	0	131	1	131	0	131	1 0	131
Ž	1	Left-Through Through		950	0 2	358	3	953	359	38	1046	0 2	404	3	1049	0 2	405	0	1049	2	405
BG	j	Through-Right		950	1	336	3	900	309	36	1040	1	404	3	1049	1	405	U	1049	1	405
上与	ر	Right		125	0	125	0	125	125	33	166	0	166	0	166	0	166	0	166	0	166
SOUTHBOUND	+	Left-Through-Ri	ight		0							0				0				0	
•	<i>بلہ</i>	Left-Right			0							0				0				0	
	Ĵ	Left		289	2	159	0	289	159	29	336	2	185	0	336	2	185	0	336	2	185
9		Left-Through			0							0				0				0	
9	$\overrightarrow{\rightarrow}$	Through		1026	2	513	0	1026	513	41	1130	2	565	0	1130	2	565	0	1130	2	565
EASTBOUND	→,	Through-Right Right		135	1	40	0	135	40	6	149	0 1	44	0	149	1	44	0	149	1	44
I AS	7	Left-Through-Ri	ight	133	0	40	U	133	40	U	143	Ö		0	143	0	44	U	143	0	44
	\dashv	Left-Right			0							0				0				0	
		Left		200	2	164		200	465	2	210	2	175		221	2	477		221	2	477
9	*	Leπ Left-Through		298	0	164	2	300	165	3	319	0	175	2	321	0	177	0	321	0	177
Ď	←	Through		764	2	382	0	764	382	44	855	2	428	0	855	2	428	0	855	2	428
TB(<u>↑</u>	Through-Right			0							0				0				0	
WESTBOUND	₹	Right Left-Through-Ri	iaht	145	1 0	31	0	145	31	9	163	1 0	32	0	163	1 0	32	0	163	1 0	32
>	<u>`</u>	Left-Right	ignt		0							0				0				0	
	*			Nor	th-South:	641	No	rth-South:	642		Nor	th-South:	709	<u> </u>	Nor	th-South:	710		Nor	th-South:	710
		CRITICAL V	OLUMES	Ea	ast-West:	677	l i	East-West:	678		E	ast-West:	740		E	ast-West:			E	ast-West:	742
<u> </u>	VO: :	IME/CADACITY /1//) DATIO:		SUM:			SUM:	1320			SUM:	1449	-		SUM:				SUM:	
		JME/CAPACITY (V/C)				0.959			0.960				1.054				1.056				1.056
V/C I	LESS	ATSAC/ATCS ADJUS				0.859			0.860				0.954				0.956				0.956
<u></u>		LEVEL OF SERVIC	E (LOS):			D			D				E				E				E

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project:	0.002	∆v/c after mitigation:	0.002
Significant impacted?	NO	Fully mitigated?	N/A





(Circular 212 Method)

I/S #:	North	n-South Street:	La Cier	nega Boulev	ard		Year	of Count:	2018	Amb	ient Grow	/th: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA12	Eas	st-West Street:	3rd Stre	eet			Projec	tion Year:	2024		Pea	ak Hour:	AM		wed by:		AS	Project:	Our Lady o	f Mt. Leban	on Project
	!}	No. o	f Phases			4	-		4				4		,		4		,		4
Oppo	osed Ø'i	ing: N/S-1, E/W-2 or	Both-3?			0			0				0				0				0
Right	Turns:	FREE-1, NRTOR-2	or OLA-3?	NB 0	SB	0	NB	0 SE		NB	0	SB	0	NB	0	SB	0	NB	0	SB	0
	Λ.	TSAC-1 or ATSAC+	ATCS-22	EB 0	WB	0 2	EB	0 W	B 0 2	EB	0	WB	0 2	EB	0	WB	0 2	EB	0	WB	0 2
	^	Override				0			0				0				0				0
				EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTUR	E CONDITION	ON W/O PF	OJECT	FUTUF	RE CONDIT	ION W/ PR	OJECT	FUTURE	W/ PROJE	CT W/ MIT	IGATION
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
٥	j	Left		174	2	96	0	174	96	0	185	2	102	0	185	2	102	0	185	2	102
N	4	Left-Through			0							0				0				0	
NORTHBOUND	1	Through		853	2	319	0	853	319	14	919	2	344	0	919	2	344	0	919	2	344
l 분	Ì	Through-Right		103	1 0	102	0	102	102	3	110	1 0	112	0	110	1 0	112	0	110	1 0	112
OR.	_ (^ 	Right Left-Through-R	iaht	103	0	103	U	103	103	3	112	0	112	U	112	0	112	U	112	0	112
ž	↑	Left-Right	igiit		0							0				0				0	
	- '																				
Ω	\ \	Left		60	2	33	0	60	33	0	64	2	35	0	64	2	35	0	64	2	35
N	→	Left-Through			0							0				0				0	
90		Through		1150	2	474	2	1152	475	30	1251	2 1	514	2	1253	2 1	514	0	1253	2	514
SOUTHBOUND	4	Through-Right Right		272	0	272	0	272	272	1	290	0	290	0	290	0	290	0	290	0	290
) C	→	Left-Through-R	iaht	212	0	212	U	212	212		290	0	290	U	290	0	290	0	290	0	290
Ñ	٠,	Left-Right	•		0							0				0				0	
۵	<i>→</i>	Left		125	1 0	125	5	130	130	8	141	1	141	5	146	1 0	146	0	146	1 0	146
N	\rightarrow	Left-Through Through		433	2	217	3	436	218	7	467	0 2	234	3	470	2	235	0	470	2	235
EASTBOUND	7	Through-Right		400	0	217	3	430	210	,	407	0	254	3	470	0	233	0	470	0	233
STI	7	Right		45	1	0	0	45	0	43	91	1	40	0	91	1	40	0	91	1	40
EA	\rightarrow	Left-Through-R	ight		0							0				0				0	
	∟≺_	Left-Right		<u> </u>	0							0				0				0	
	· ~	Left		331	1	331	0	331	331	3	354	1	354	0	354	1	354	0	354	1	354
9	,	Left-Through		331	0	331		331	331	3	304	0	354	U	304	0	304	l '	354	0	354
WESTBOUND	←	Through		1028	1	540	1	1029	540	1	1092	1	573	1	1093	1	574	0	1093	1	574
l M	4	Through-Right			1							1				1				1	
ESI	₹	Right		51	0	51	0	51	51	0	54	0	54	0	54	0	54	0	54	0	54
Ž		Left-Through-R Left-Right	ight		0							0				0				0	
	. ↓	Leit-Rigiit		Non	th-South:	570	No	rth-South:	571		Nort	th-South:	616		Non	th-South:	616		Nor	th-South:	616
		CRITICAL V	OLUMES		ast-West:	665		East-West:	670			ast-West:	714			ast-West:	720			ast-West:	720
					SUM:	1235		SUM:	1241			SUM:	1330			SUM:				SUM:	1336
	VOLU	ME/CAPACITY (V/C) RATIO:			0.898			0.903				0.967				0.972				0.972
V/C	LESS A	TSAC/ATCS ADJUS	STMENT:			0.798			0.803				0.867				0.872				0.872
		LEVEL OF SERVICE	E (LOS):			C			D				D				D			D	
<u> </u>			MADKC.																		

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

3/8/2019-11:56 AM 1 CMA12





(Circular 212 Method)

I/S #:	Nort	th-South Street:	La Cier	ega Boulev	ard		Year	of Count:	2018	Amb	ient Grow	/th: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA12	Ea	ast-West Street:	3rd Str	eet				tion Year:			Pea	k Hour:	PM		wed by:		AS		Our Lady o		on Project
	!!	No. o	of Phases			4	-		4				4				4	,			4
Opp	osed Ø	i'ing: N/S-1, E/W-2 o	r Both-3?			0			0				0				0				0
Right	Turns:	: FREE-1, NRTOR-2	or OLA-3?	NB 0	SB	0	NB	0 SI		NB	0	SB	0	NB	0	SB	0	NB	0	SB	0
		ATSAC-1 or ATSAC-		EB 0	WB	0	EB	0 W		EB	0	WB	0 2	EB	0	WB	0	EB	0	WB	0 2
	,		Capacity			2			2				0				2				0
		Overnae	Gupuony	EXISTI	NG CONDI		EXIST	NG PLUS P	•	FUTUR	E CONDITION	ON W/O PR	OJECT	FUTUF	RE CONDIT	ION W/ PR	•	FUTURE	W/ PROJE	CT W/ MIT	•
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
0	7	Left		107	2	59	0	107	59	0	114	2	63	0	114	2	63	0	114	2	63
Į	\dashv	Left-Through			0							0				0				0	
NORTHBOUND	1	Through		1133	2	432	0	1133	432	30	1233	2	470	0	1233	2	470	0	1233	2	470
l ≝	Ì~	Through-Right		400	1	400	•	400	400		470	1	470		470	1	470		470	1	470
<u>K</u>		Right Left-Through-F	7:ls.4	162	0 0	162	0	162	162	4	176	0	176	0	176	0	176	0	176	0 0	176
ž	↑	Left-Right	rigiit		0							0				0				0	
		Lent-ragin																			
	, <u>, , , , , , , , , , , , , , , , , , </u>	Left		134	2	74	0	134	74	0	142	2	78	0	142	2	78	0	142	2	78
Į	\rightarrow	Left-Through			0							0				0				0	
l g	∤	Through		1012	2	383	5	1017	384	37	1111	2	421	5	1116	2	422	0	1116	2	422
SOUTHBOUND	ل ر	Through-Right Right		400	1 0	400	0	400	400	7	454	1 0	454	0	454	1 0	454	0	454	1 0	454
ΙŽ	→	Left-Through-F	Right	136	0	136	U	136	136	/	151	0	151	U	151	0	151	U	151	0	151
S	į,	Left-Right	g		0							0				0				0	
	<u> </u>	Left		171	1	171	3	174	174	10	192	1	192	3	195	1	195	0	195	1	195
۱₹	<i>→</i>	Left-Through			0		_					0				0				0	
EASTBOUND	$\overrightarrow{\neg}$	Through Through-Right		775	2	388	2	777	389	8	831	2	416	2	833	2	417	0	833	2	417
l H	7	Right		144	1	115	0	144	115	39	192	1	161	0	192	1	161	0	192	1	161
l š	\rightarrow	Left-Through-F	Right		0	110	· ·		110	00	102	0			102	0	101		102	0	101
_	\dashv	Left-Right			0							0				0				0	
	. ~						_							_				_			
₽	<i>₹</i>	Left Left-Through		195	1 0	195	0	195	195	8	215	1 0	215	0	215	1 0	215	0	215	1 0	215
WESTBOUND	↓	Through		491	1	316	3	494	318	7	528	1	339	3	531	1	341	0	531	1	341
B0	7	Through-Right		701	i	310	3	707	310	,	520	1	000		551	1	J+1		551	1	J - 1
ST	1	Right		141	0	141	0	141	141	0	150	0	150	0	150	0	150	0	150	0	150
ME	\	Left-Through-F	Right		0							0				0				0	
<u> </u>	_	Left-Right			0	560			500			0	F			0	F 10			0	F.(2)
		CRITICAL V	OLUMES		th-South: ast-West:	506 583		rth-South:	506 584			h-South:	548 631			h-South:	548 632			th-South:	548 632
		OKITIOAL V	CLUMICS	E	SUM:	1089	'	East-West: SUM:	1090		Eá	st-West: SUM:	1179		Eá	ast-West: SUM:			E	ast-West: SUM:	1180
	VOLI	JME/CAPACITY (V/C	C) RATIO:		30.W.	0.792		30W.	0.793			JOH.	0.857			JOH.	0.858			30W.	0.858
V/C		ATSAC/ATCS ADJU	•																		
V/C	LEGG					0.692			0.693				0.757				0.758				0.758
<u> </u>		LEVEL OF SERVI	JE (LUS):			В			В				С				С				С

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT





(Circular 212 Method)

I/S #:	North	h-South Street:	La Cier	nega Boulev	ard		Year	of Count:	2018	Amb	ient Grow	/th: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA13	Eas	st-West Street:	San Vic	ente Boulev	/ard		Projection Year: 2024 Peak Hour:				k Hour:	AM		wed by:		AS	Project:	Our Lady o	f Mt. Leban	on Project	
	<u> </u>	No. o	Phases			2	-		2				2		,		2		,		2
Oppo	osed Ø'i	ing: N/S-1, E/W-2 or	Both-3?			0			0				0				0				0
Right	Turns:	FREE-1, NRTOR-2	or OLA-3?	NB 0	SB	0	NB	0 SE		NB	0	SB	0	NB	0	SB	0	NB	0	SB	0
	ATSAC-1 or ATSAC+ATCS-2?			EB	0 W	B 0 2	EB	0	WB	0	EB	0	WB	0 2	EB	0	WB	0 2			
	^	Override				0			0	2 0				2 0				0			
				EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTUR	E CONDITION	ON W/O PF	OJECT	FUTURE CONDITION W/ PROJECT				FUTURE W/ PROJECT W/ MITIGATION			
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added	Total	No. of	Lane	Added Total No. of Lane			
	-			Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
٥	J	Left		128	1	128	1	129	129	2	138	1	138	1	139	1	139	0	139	1	139
NORTHBOUND	\dashv	Left-Through			0							0				0				0	
90	Î	Through		737	2	248	0	737	248	26	808	2	271	0	808	2	271	0	808	2	271
IE	À	Through-Right		6	1 0	6	0	6	6	0	6	1 0	6	0	6	1 0	6	0	6	1 0	6
OR.	_^^_	Right Left-Through-R	aht	0	0	0	U	0	0	U	0	0	0	U	6	0	0	U	О	0	0
ž	↑	Left-Right	giit		0							0				0				0	
	• · ·																				
Ω	\ \	Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
N	→	Left-Through			0							0				0				0	
90	1	Through		1266	2	505	0	1266	505	49	1393	2 1	556	0	1393	2 1	557	0	1393	2	557
IE	ل ر	Through-Right Right		248	0	248	2	250	250	12	275	0	275	2	277	0	277	0	277	0	277
SOUTHBOUND	4	Left-Through-R	aht	240	0	240	2	230	250	12	2/3	0	2/3	2	211	0	211	U U	211	0	211
Š	J.	Left-Right	•		0							0				0				0	
				_																	
	<i>_</i> 1	Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
N	\rightarrow	Left-Through Through		937	0 4	234	5	942	236	0	995	0 4	249	5	1000	0 4	250	0	1000	0 4	250
EASTBOUND	7	Through-Right		937	0	234	5	942	230	U	995	0	249	5	1000	0	250	U	1000	0	250
STI	7	Right		189	1	125	3	192	128	0	201	1	132	3	204	1	135	0	204	1	135
EA	→	Left-Through-R	ght		0							0				0				0	
	L ≺_	Left-Right		L	0							0				0				0	
	· ~	Left		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	7	Leπ Left-Through		U	0	U	U	U	U	U	U	0	U	U	U	0	U	U U	U	0	U
WESTBOUND	←	Through		1991	4	498	2	1993	498	2	2115	4	529	2	2117	4	529	0	2117	4	529
<u>B</u>	<u>↓</u>	Through-Right			0						-	0				0		-		0	
ESI	↓	Right		238	1	238	0	238	238	3	256	1	256	0	256	1	256	0	256	1	256
Ž	\$_	Left-Through-R	ght		0							0				0				0	
	. ↓	Left-Right		Non	th-South:	633	Ma	rth-South	634		Non	th-South:	694		Non	th-South:	696		Nor	th-South:	696
		CRITICAL V	DLUMES		ast-West:	498	North-South: 634 East-West: 498					ast-West:	529			ast-West:	529			ast-West:	529
					SUM:	1131		SUM:	1132			SUM:	1223			SUM:				SUM:	1225
	VOLU	ME/CAPACITY (V/C	RATIO:		•	0.754	_		0.755				0.815	_			0.817				0.817
V/C	LESS A	ATSAC/ATCS ADJUS	TMENT:			0.654			0.655				0.715				0.717				0.717
		LEVEL OF SERVICE	E (LOS):			В			В				C				C				C
LEVEL OF SERVICE (LOS):				1		<u> </u>			<u> </u>								•				-

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

3/8/2019-11:56 AM 1 CMA13





(Circular 212 Method)

I/S #:	Nor	rth-South Street:	La Cier	nega Boulev	ard		Year	of Count:	2018	Amb	ient Grow	/th: (%):	1.0	Condu	cted by:	NDS		Date:		3/8/2019	
CMA13	Е	East-West Street:	San Vio	cente Boulev	vard		Projection Year: 2024				Pea	k Hour:	PM	Revie	wed by:	J/	AS	Project:	Our Lady o	f Mt. Leban	on Project
	<u>.</u>	N	o. of Phases			2			2				2				2				2
Oppo	osed Ø	Ø'ing: N/S-1, E/W-	2 or Both-3?			0			0				0				0				0
Right	Turns	s: FREE-1, NRTOF	R-2 or OLA-3?	NB 0	SB	0	NB EB	0 SE 0 W		NB EB	0 0	SB WB	0	NB EB	0	SB WB	0	NB EB	0 0	SB WB	0 0
	ATSAC-1 or ATSAC+ATCS-2?			ED	U VV	2	ED	U	WD	2	ED	U	WD	2	ED	U	VV D	2			
	Override Capacity							0	2 0				0				0				
				EXISTI	NG CONDI	TION	EXIST	ING PLUS P	ROJECT	FUTURE CONDITION W/O PROJECT				FUTURE CONDITION W/ PROJECT				FUTURE W/ PROJECT W/ MITIGATION			
		MOVEMENT			No. of	Lane	Project	Total	Lane	Added	Total	No. of	Lane	Added Total No. of Lane				Added Total No. of Lane			
				Volume	Lanes	Volume	Traffic	Volume	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume	Volume	Volume	Lanes	Volume
Ω	\mathcal{J}	Left		180	1	180	3	183	183	10	201	1	201	3	204	1	204	0	204	1	204
NORTHBOUND	1	Left-Throug Through	n	1182	0 2	402	0	1182	402	52	1307	0 2	444	0	1307	0 2	444	0	1307	0 2	444
ВО		Through → Through-Rig	aht	1102	1	402	U	1102	402	52	1307	1	444	0	1307	1	444	"	1307	1	444
H	P	→ Right	Jiit.	24	0	24	0	24	24	0	25	0	25	0	25	0	25	0	25	0	25
P.	↔	•	h-Right		0							0				0				0	
Z	⟨ \				0							0				0				0	
9	Ĵ	→ Left → Left-Throug	L	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0 0	0
Ĭ	ľ	Through	п	1204	2	439	0	1204	441	69	1347	2	493	0	1347	2	495	0	1347	2	495
I BC	į	Through-Rig	ght	1204	1	400	U	1204	771	03	1047	1	733		1041	1	433		1047	1	733
∥ Է	زہ ا	Right	-	113	0	113	5	118	118	13	133	0	133	5	138	0	138	0	138	0	138
SOUTHBOUND	4		h-Right		0							0				0				0	
0,	, ا	Left-Right			0							0				0				0	
	J	Left		2	0	0	0	2	0	0	2	0	0	0	2	0	0	0	2	0	0
9	<u></u>		h		0	U	U	2	U		2	0	U		2	0	U		2	0	U
EASTBOUND	\rightarrow	iiiiougii		2101	4	525	3	2104	526	0	2230	4	558	3	2233	4	558	0	2233	4	558
IB(ght		0							0				0				0	
AS.	→		h Dimb4	205	1 0	115	2	207	116	0	218	1 0	118	2	220	1 0	118	0	220	1 0	118
Ē	(Left-Right	n-Right		0							0				0				0	
	. <i>t</i>				Ť																
	· C			0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
WESTBOUND	7	•	h		0		_					0				0				0	
∥ ŏ	<u>7</u>		aht.	1069	4 0	267	5	1074	269	11	1146	4 0	287	5	1151	4 0	288	0	1151	4 0	288
STE	₹.	- Dialet	yıı.	358	1	358	0	358	358	7	387	1	387	0	387	1	387	0	387	1	387
	→	Left-Throug	h-Right	330	0	000		550	000	'	551	0	001		551	0	001		551	0	557
	}	Left-Right			0							0				0				0	
		ODITIOA			th-South:	619	North-South: 624					h-South:	694			h-South:	699			th-South:	699
		CRITICA	L VOLUMES	Ea	ast-West: SUM:	525	'	East-West: SUM:	526 1150		Ea	ast-West:	558 1252		Ea	st-West: SUM:	558 1257		E	ast-West: SUM:	558 1257
 	VOI	UME/CAPACITY (V/C) RATIO:	1	SUIVI:	1144		SUIVI:				SUM:				SUIVI:				SUIVI:	1257
1//0		•	•			0.763			0.767				0.835				0.838				0.838
V/C	LESS	ATSAC/ATCS AD				0.663			0.667				0.735				0.738				0.738
		LEVEL OF SER	VICE (LOS):			В			В				С				С				С

REMARKS:

Version: 1i Beta; 8/4/2011

PROJECT IMPACT

Change in v/c due to project:	0.003	∆v/c after mitigation:	0.003
Significant impacted?	NO	Fully mitigated?	N/A

APPENDIX C	
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ICU AND LEVELS OF SERVICE EXPLANATION ICU DATA WORKSHEETS – WEEKDAY AM AND PM PEAK HOURS

INTERSECTION CAPACITY UTILIZATION (ICU) DESCRIPTION

Level of Service is a term used to describe prevailing conditions and their effect on traffic. Broadly interpreted, the Levels of Service concept denotes any one of a number of differing combinations of operating conditions which may occur as a roadway is accommodating various traffic volumes. Level of Service is a qualitative measure of the effect of such factors as travel speed, travel time, traffic interruptions, freedom to maneuver, safety, driving comfort and convenience.

Six Levels of Service, A through F, have been defined in the 1965 *Highway Capacity Manual*, published by the Transportation Research Board. Level of Service A describes a condition of free flow, with low traffic volumes and relatively high speeds, while Level of Service F describes forced traffic flow at low speeds with jammed conditions and queues which cannot clear during the green phases.

The Intersection Capacity Utilization (ICU) method of intersection capacity analysis has been used in our studies. It directly relates traffic demand and available capacity for key intersection movements, regardless of present signal timing, The capacity per hour of green time for each approach is calculated based on the methods of the *Highway Capacity Manual*. The proportion of total signal time needed by each key movement is determined and compared to the total time available (100 percent of the hour). The result of summing the requirements of the conflicting key movements plus an allowance for clearance times is expressed as a decimal fraction. Conflicting key traffic movements are those opposing movements whose combined green time requirements are greatest.

The resulting ICU represents the proportion of the total hour required to accommodate intersection demand volumes if the key conflicting traffic movements are operating at capacity. Other movements may be operating near capacity, or may be operating at significantly better levels. The ICU may be translated to a Level of Service as tabulated below.

The Levels of Service (abbreviated from the *Highway Capacity Manual*) are listed here with their corresponding ICU and Load Factor equivalents. Load Factor is that proportion of the signal cycles during the peak hour which are fully loaded; i.e. when all of the vehicles waiting at the beginning of green are not able to clear on that green phase.

Intersection Capacity Utilization Characteristics											
Level of Service	Load Factor	Equivalent ICU									
A	0.0	0.00 - 0.60									
В	0.0 - 0.1	0.61 - 0.70									
C	0.1 - 0.3	0.71 - 0.80									
D	0.3 - 0.7	0.81 - 0.90									
E	0.7 - 1.0	0.91 - 1.00									
F	Not Applicable	Not Applicable									

SERVICE LEVEL A

There are no loaded cycles and few are even close to loaded at this service level. No approach phase is fully utilized by traffic and no vehicle waits longer than one red indication.

SERVICE LEVEL B

This level represents stable operation where an occasional approach phase is fully utilized and a substantial number are approaching full use. Many drivers begin to feel restricted within platoons of vehicles.

SERVICE LEVEL C

At this level stable operation continues. Loading is still intermittent but more frequent than at Level B. Occasionally drivers may have to wait through more than one red signal indication and backups may develop behind turning vehicles. Most drivers feel somewhat restricted, but not objectionably so.

SERVICE LEVEL D

This level encompasses a zone of increasing restriction approaching instability at the intersection. Delays to approaching vehicles may be substantial during short peaks within the peak hour, but enough cycles with lower demand occur to permit periodic clearance of queues, thus preventing excessive backups. Drivers frequently have to wait through more than one red signal. This level is the lower limit of acceptable operation to most drivers.

SERVICE LEVEL E

This represents near capacity and capacity operation. At capacity (ICU = 1.0) it represents the most vehicles that the particular intersection can accommodate. However, full utilization of every signal cycle is seldom attained no matter how great the demand. At this level all drivers wait through more than one red signal, and frequently through several.

SERVICE LEVEL F

Jammed conditions. Traffic backed up from a downstream location on one of the street restricts or prevents movement of traffic through the intersection under consideration.

LINSCOTT, LAW & GREENSPAN, ENGINEERS

Burton Way

N-S St:

E-W St:

20931 Burbank Boulevard, Suite C, Woodland Hills, CA (818) 835-8648 Fax (818) 835-8649

INTERSECTION CAPACITY UTILIZATION

Robertson Boulevard @ Burton Way

Robertson Boulevard Peak hr: AM Annual Growth: 1%

Project: 5-17-0315-1/ Our Lady of Mt. Lebanon CITY OF BEVERLY HILLS File: ICU-2

	2018	EXIST. TR	AFFIC	2018	W/PROJE	CT SITE T	RAFFIC	2024	WITHOUT	PROJECT		2024	W/PROJE	CT	
	1	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C
Movement	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio
Nb Left	56	1600	0.035 *	0	56	1600	0.035 *	7	66	1600	0.041 *	0	66	1600	0.041 *
Nb Thru	501	1600	0.313	1	502	1600	0.314	1	533	1600	0.333	1	534	1600	0.334
Nb Right	39	1600	0.024	1	40	1600	0.025	0	41	1600	0.026	1	42	1600	0.026
Sb Left	26	1600	0.016	0	26	1600	0.016	0	28	1600	0.017	0	28	1600	0.017
Sb Thru	464	1600	0.319 *	0	464	1600	0.319 *	0	493	1600	0.343 *	0	493	1600	0.343 *
Sb Right	46	0	-	0	46	0	-	7	56	0	-	0	56	0	-
Eb Left	100	1600	0.063 *	0	100	1600	0.063 *	7	113	1600	0.071 *	0	113	1600	0.071 *
Eb Thru	720	4800	0.150	1	721	4800	0.150	0	764	4800	0.159	1	765	4800	0.159
Eb Right	126	1600	0.079	0	126	1600	0.079	3	137	1600	0.085	0	137	1600	0.085
Wb Left	178	1600	0.111	5	183	1600	0.114	0	189	1600	0.118	5	194	1600	0.121
Wb Thru	1370	4800	0.285 *	3	1373	4800	0.286 *	12	1466	4800	0.305 *	3	1469	4800	0.306 *
Wb Right	81	1600	0.051	0	81	1600	0.051	0	86	1600	0.054	0	86	1600	0.054
Yellow Allow	ance:		0.100 *				0.100 *				0.100 *				0.100 *
ICU LOS			0.802 D				0.802 D				0.860 D			[0.861

03/08/2019

2018

2024

Date:

Date of Count:

Projection Year:

^{*} Key conflicting movement as a part of ICU 1 Counts conducted by: NDS

² Capacity expressed in veh/hour of green

LINSCOTT, LAW & GREENSPAN, ENGINEERS

Burton Way

N-S St:

E-W St:

20931 Burbank Boulevard, Suite C, Woodland Hills, CA (818) 835-8648 Fax (818) 835-8649

INTERSECTION CAPACITY UTILIZATION

Robertson Boulevard @ Burton Way

Robertson Boulevard Peak hr: PMAnnual Growth: 1% 5-17-0315-1/ Our Lady of Mt. Lebanon

Project: CITY OF BEVERLY HILLS File:

	2018	EXIST. TR	AFFIC	2018	W/PROJE	CT SITE TE	RAFFIC	2024	WITHOUT	PROJECT		2024	W/PROJE	СТ	
	1	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C
Movement	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio
Nb Left	85	1600	0.053 *	0	85	1600	0.053 *	5	95	1600	0.059 *	0	95	1600	0.059 *
Nb Thru	504	1600	0.315	3	507	1600	0.317	4	539	1600	0.337	3	542	1600	0.339
Nb Right	72	1600	0.045	2	74	1600	0.046	0	76		0.048	2	78	1600	0.049
Sb Left	82	1600	0.051	0	82	1600	0.051	0	87	1600	0.054	0	87	1600	0.054
Sb Thru	489	1600	0.334 *	0	489	1600	0.334 *	0	519	1600	0.357 *	0	519	1600	0.357 *
Sb Right	45	0	-	0	45	0	-	5	53	0	-	0	53	0	-
Eb Left	170	1600	0.106	0	170	1600	0.106	21	201	1600	0.126	0	201	1600	0.126
Eb Thru	1452	4800	0.303 *	3	1455	4800	0.303 *	0	1541	4800	0.321 *	3	1544	4800	0.322 *
Eb Right	61	1600	0.038	0	61	1600	0.038	7	72	1600	0.045	0	72	1600	0.045
Wb Left	85	1600	0.053 *	3	88	1600	0.055 *	0	90	1600	0.056 *	3	93	1600	0.058 *
Wb Thru	931	4800	0.194	2	933	4800	0.194	13	1001	4800	0.209	2	1003	4800	0.209
Wb Right	67	1600	0.042	0	67	1600	0.042	0	71	1600	0.044	0	71	1600	0.044
Yellow Allow	wance:		0.100 *				0.100 *				0.100 *				0.100 *
ICU LOS			0.843 D				0.845 D				0.894 D				0.897 D

03/08/2019

2018

2024

Date:

Date of Count:

Projection Year:

^{*} Key conflicting movement as a part of ICU

¹ Counts conducted by: NDS

² Capacity expressed in veh/hour of green

20931 Burbank Boulevard, Suite C, Woodland Hills, CA (818) 835-8648 Fax (818) 835-8649

INTERSECTION CAPACITY UTILIZATION

Robertson Boulevard @ Wilshire Boulevard

N-S St: Robertson Boulevard Peak hr: AM E-W St: Wilshire Boulevard Annual Growth: 1% Project: 5-17-0315-1 / Our Lady of Mt. Lebanon

CITY OF BEVERLY HILLS File: ICU-3

	2018	EXIST. TR	AFFIC	2018	W/PROJE	CT SITE TI	RAFFIC	2024	WITHOUT	PROJECT		2024	W/PROJE	CT	
	1	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C
Movement	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio
Nb Left	198	1600	0.124 *	0	198	1600	0.124 *	0	210	1600	0.131 *	0	210	1600	0.131 *
Nb Thru	634	3200	0.235	1	635	3200	0.235	o o	673	3200	0.249	1	674	3200	0.249
Nb Right	117	0	-	0	117	0	-	o o	124	0	-	0	124	0	-
Sb Left	59	1600	0.037	0	59	1600	0.037	3	66	1600	0.041	0	66	1600	0.041
Sb Thru	592	3200	0.224 *	3	595	3200	0.226 *	0	628	3200	0.238 *	3	631	3200	0.239 *
Sb Right	125	0	-	2	127	0	-	0	133	0	-	2	135	0	-
Eb Left	116	1600	0.073 *	1	117	1600	0.073 *	1	124	1600	0.077 *	1	125	1600	0.078 *
Eb Thru	750	4800	0.180	0	750	4800	0.180	48	844	4800	0.201	0	844	4800	0.201
Eb Right	114	0	-	0	114	0	-	0	121	0	-	0	121	0	-
Wb Left	119	1600	0.074	0	119	1600	0.074	0	126	1600	0.079	0	126	1600	0.079
Wb Thru	1623	4800	0.338 *	0	1623	4800	0.338 *	42	1765	4800	0.368 *	0	1765	4800	0.368 *
Wb Right	105	1600	0.066	0	105	1600	0.066	7	118	1600	0.074	0	118	1600	0.074
Yellow Allow	/ance:		0.100 *				0.100 *				0.100 *				0.100 *
ICU LOS			0.858 D				0.861 D				0.914 E				0.916 E

03/08/2019

2018

2024

Date:

Date of Count:

Projection Year:

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² Capacity expressed in veh/hour of green

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INTERSECTION CAPACITY UTILIZATION

Robertson Boulevard @ Wilshire Boulevard

N-S St: Robertson Boulevard Peak hr: PM
E-W St: Wilshire Boulevard Annual Growth: 1%
Project: 5-17-0315-1 / Our Lady of Mt. Lebanon

File: ICU-3 CITY OF BEVERLY HILLS

	2018	EXIST. TR	AFFIC	2018	W/PROJE	CT SITE T	RAFFIC	2024	WITHOUT	PROJECT		2024	W/PROJE	СТ	
	1	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C
Movement	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio
Nb Left	208	1600	0.130 *	0	208	1600	0.130 *	0	221	1600	0.138 *	0	221	1600	0.138 *
Nb Thru	479	3200	0.177	3	482	3200	0.178	0	508	3200	0.187	3	511	3200	0.188
Nb Right	87	0	-	0	87	0	-	0	92	0	-	0	92	0	-
Sb Left	79	1600	0.049	0	79	1600	0.049	7	91	1600	0.057	0	91	1600	0.057
Sb Thru	630	3200	0.218 *	2	632	3200	0.219 *	0	669	3200	0.232 *	2	671	3200	0.233 *
Sb Right	69	0	-	1	70	0	-	0	73	0	-	1	74	0	-
Eb Left	161	1600	0.101	2	163	1600	0.102	4	175	1600	0.109	2	177	1600	0.110
Eb Thru	1336	4800	0.319 *	0	1336	4800	0.319 *	63	1481	4800	0.352 *	0	1481	4800	0.352 *
Eb Right	197	0	-	0	197	0	-	0	209	0	-	0	209	0	-
Wb Left	119	1600	0.074 *	0	119	1600	0.074 *	0	126	1600	0.079 *	0	126	1600	0.079 *
Wb Thru	857	4800	0.179	0	857	4800	0.179	61	971	4800	0.202	0	971	4800	0.202
Wb Right	55	1600	0.034	0	55	1600	0.034	5	63	1600	0.040	0	63	1600	0.040
Yellow Allov	vance:		0.100 *				0.100 *				0.100 *				0.100 *
ICU LOS			0.842 D				0.843 D				0.901 E				0.902 E

03/08/2019

2018

2024

Date:

Date of Count:

Projection Year:

^{*} Key conflicting movement as a part of ICU

¹ Counts conducted by: NDS

² Capacity expressed in veh/hour of green

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INTERSECTION CAPACITY UTILIZATION

La Cienega Boulevard @ San Vicente Boulevard

03/08/2019

2018

2024

Date:

Date of Count:

Projection Year:

N-S St: La Cienega Boulevard Peak hr: AM E-W St: San Vicente Boulevard Annual Growth: 1%

Project: 5-17-0315-1 / Our Lady of Mt. Lebanon

File: ICU-13

CITY OF BEVERLY HILLS

	2018	EXIST. TR	AFFIC	2018	W/PROJE	CT SITE TI	RAFFIC	2024	WITHOUT	PROJECT		2024	W/PROJE	СТ	
	1	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C
Movement	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio
Nb Left	128	1600	0.080 *	1	129	1600	0.081 *	2	138	1600	0.086 *	1	139	1600	0.087 *
Nb Thru	737	4800	0.060	0	737		0.061	26	808		0.000	0	808	4800	0.067
Nb Right	6	0	-	0	6		-	0	6		-	0	6	0	-
Sb Left	0	0	0.000	0	0	0	0.000	0	0	0	0.000	0	0	0	0.000
Sb Thru	1266	4800	0.315 *	0	1266	4800	0.316 *	49	1393	4800	0.347 *	0	1393	4800	0.348 *
Sb Right	248	0	-	2	250	0	-	12	275	0	-	2	277	0	-
Eb Left	0	0	0.000 *	0	0	0	0.000 *	0	0	0	0.000 *	0	0	0	0.000 *
Eb Thru	937	6400	0.146	5	942	6400	0.147	0	995	6400	0.155	5	1000	6400	0.156
Eb Right	189	1600	0.118	3	192	1600	0.120	0	201	1600	0.126	3	204	1600	0.128
Wb Left	0	0	0.000	0	0	0	0.000	0	0	0	0.000	0	0	0	0.000
Wb Thru	1991	6400	0.311 *	2	1993	6400	0.311 *	2	2115	6400	0.330 *	2	2117	6400	0.331 *
Wb Right	238	1600	0.149	0	238	1600	0.149	3	256	1600	0.160	0	256	1600	0.160
Yellow Allow	/ance:		0.100 *				0.100 *				0.100 *				0.100 *
ICU LOS			0.807 D				0.808 D				0.864 D			1	0.865 O

^{*} Key conflicting movement as a part of ICU

¹ Counts conducted by: NDS

² Capacity expressed in veh/hour of green

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INTERSECTION CAPACITY UTILIZATION

La Cienega Boulevard @ San Vicente Boulevard

03/08/2019

2018

2024

Date:

Date of Count:

Projection Year:

N-S St: La Cienega Boulevard Peak hr: PM E-W St: San Vicente Boulevard Annual Growth: 1%

Project: 5-17-0315-1 / Our Lady of Mt. Lebanon

File: ICU-13

CITY OF BEVERLY HILLS

	2018	EXIST. TR	AFFIC	2018	W/PROJE	CT SITE TE	RAFFIC	2024	WITHOUT	PROJECT		2024	W/PROJE	CT	
	1	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C
Movement	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio
NIII I aft	400	4000	0.440 *	•	183	1600	0.114 *	40	204	4000	0.126 *	2	204	4000	0.127 *
Nb Left	180	1600	0.113 *	3				10	201	1600		3		1600	
Nb Thru	1182	4800	0.251	0	1182	4800	0.251	52	1307	4800	0.278	0	1307	4800	0.278
Nb Right	24	0	-	0	24	0	-	0	25	0	-	0	25	0	-
Sb Left	0	0	0.000	0	0	0	0.000	0	0	0	0.000	0	0	0	0.000
Sb Thru	1204	4800	0.274 *	0	1204	4800	0.275 *	69	1347	4800	0.308 *	0	1347	4800	0.309 *
Sb Right	113	0	-	5	118	0	-	13	133	0	-	5	138	0	-
Eb Left	2	0	0.000	0	2	0	0.000	0	2	0	0.000	0	2	0	0.000
Eb Thru	2101	6400	0.329 *	3	2104	6400	0.329 *	0	2230		0.349 *	3	2233	6400	0.349 *
Eb Right	205	1600	0.128	2	207	1600	0.129	0	218	1600	0.136	2	220	1600	0.138
Wb Left	0	0	0.000 *	0	0	0	0.000 *	0	0	0	0.000 *	0	0	0	0.000 *
Wb Thru	1069	6400	0.167	5	1074	6400	0.168	11	1146	6400	0.179	5	1151	6400	0.180
Wb Right	358	1600	0.224	0	358	1600	0.224	7	387	1600	0.242	0	387	1600	0.242
Yellow Allow	rance:		0.100 *				0.100 *	ı			0.100 *				0.100 *
ICU LOS			0.815 D				0.819 D				0.883 D				0.886 D

^{*} Key conflicting movement as a part of ICU

¹ Counts conducted by: NDS

² Capacity expressed in veh/hour of green

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INTERSECTION CAPACITY UTILIZATION

La Cienega Boulevard @ Wilshire Boulevard

N-S St: La Cienega Boulevard Peak hr: AM E-W St: Wilshire Boulevard Annual Growth: 1% Project: 5-17-0315-1 / Our Lady of Mt. Lebanon

CITY OF BEVERLY HILLS File: ICU-14

	2018	EXIST. TR	AFFIC	2018	W/PROJE	CT SITE TI	RAFFIC	2024	WITHOUT	PROJECT	•	2024	W/PROJE	CT	
	1	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C
Movement	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio
Nb Left	154	1600	0.096 *	0	154	1600	0.096 *	3	166	1600	0.104 *	0	166	1600	0.104 *
Nb Thru	708	4800	0.160	1	709	4800	0.160	44	796		0.179	1	797	4800	0.180
Nb Right	60	0	-	0	60	0	-	1	65		-	0	65	0	-
Sb Left	51	1600	0.032	0	51	1600	0.032	0	54	1600	0.034	0	54	1600	0.034
Sb Thru	843	4800	0.222 *	3	846	4800	0.222 *	33	928	4800	0.244 *	3	931	4800	0.244 *
Sb Right	221	0	-	0	221	0	-	7	242	0	-	0	242	0	-
Eb Left	121	1600	0.076 *	0	121	1600	0.076 *	2	130	1600	0.081 *	0	130	1600	0.081 *
Eb Thru	439	4800	0.105	0	439	4800	0.105	46	512	4800	0.121	0	512	4800	0.121
Eb Right	64	0	-	0	64	0	-	3	71	0	-	0	71	0	-
Wb Left	108	1600	0.068	0	108	1600	0.068	4	119	1600	0.074	0	119	1600	0.074
Wb Thru	1016	4800	0.219 *	0	1016	4800	0.219 *	39	1118	4800	0.241 *	0	1118	4800	0.241 *
Wb Right	37	0	-	0	37	0	-	0	39	0	-	0	39	0	-
Yellow Allow	ance:		0.100 *				0.100 *				0.100 *				0.100 *
ICU LOS			0.713 C				0.714 C				0.770 C				0.771 C

03/08/2019

2018

2024

Date:

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^{*} Key conflicting movement as a part of ICU 1 Counts conducted by: NDS

² Capacity expressed in veh/hour of green

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INTERSECTION CAPACITY UTILIZATION

La Cienega Boulevard @ Wilshire Boulevard

N-S St: La Cienega Boulevard Peak hr: PM
E-W St: Wilshire Boulevard Annual Growth: 1%
Project: 5-17-0315-1 / Our Lady of Mt. Lebanon

File: ICU-14 CITY OF BEVERLY HILLS

	2018	EXIST. TR	AFFIC	2018	W/PROJE	CT SITE TE	RAFFIC	2024	WITHOUT	PROJECT		2024	W/PROJE	CT	
	1	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C	Added	Total	2	V/C
Movement	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio	Volume	Volume	Capacity	Ratio
Nb Left	135	1600	0.084 *	0	135	1600	0.084 *	6	149	1600	0.093 *	0	149	1600	0.093 *
Nb Thru	953	4800	0.214	3	956	4800	0.215	67	1079		0.243	3	1082	4800	0.243
Nb Right	74	0	-	0	74	0	-	6	85	0	-	0	85	0	-
Sb Left	85	1600	0.053	0	85	1600	0.053	0	90	1600	0.056	0	90	1600	0.056
Sb Thru	934	4800	0.215 *	2	936	4800	0.215 *	64	1055	4800	0.243 *	2	1057	4800	0.243 *
Sb Right	96	0	-	0	96	0	-	8	110	0	-	0	110	0	-
Eb Left	130	1600	0.081	0	130	1600	0.081	6	144	1600	0.090	0	144	1600	0.090
Eb Thru	649	4800	0.150 *	0	649	4800	0.150 *	58	747	4800	0.173 *	0	747	4800	0.173 *
Eb Right	73	0	-	0	73	0	-	5	82	0	-	0	82	0	-
Wb Left	231	1600	0.144 *	0	231	1600	0.144 *	5	250	1600	0.156 *	0	250	1600	0.156 *
Wb Thru	573	4800	0.130	0	573	4800	0.130	52	660	4800	0.149	0	660	4800	0.149
Wb Right	50	0	-	0	50	0	-	0	53	0	-	0	53	0	-
Yellow Allow	vance:		0.100 *				0.100 *				0.100 *				0.100 *
ICU LOS			0.694 B				0.694 B				0.765 C				0.765 C

03/08/2019

2018

2024

Date:

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² Capacity expressed in veh/hour of green

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HCM and Levels of Service Explanation HCM Data Worksheets – Weekday AM and PM Peak Hours

LEVEL OF SERVICE FOR SIGNALIZED INTERSECTIONS

In the *Highway Capacity Manual (HCM)*, published by the Transportation Research Board, 2000, level of service for signalized intersections is defined in terms of delay, which is a measure of driver discomfort, frustration, fuel consumption, and increased travel time. The delay experienced by a motorist is made up of a number of factors that relate to control, geometrics, traffic, and incidents. Total delay is the difference between the travel time actually experienced and the reference travel time that would result during base conditions: in the absence of traffic control, in the absence of geometric delay, in the absence of incidents, and when there are no other vehicles on the road. Only the portion of total delay attributed to the control facility is quantified. This delay is called *control delay*. Control delay includes initial deceleration delay, queue move-up time, stopped delay, and final acceleration delay.

Level of Service criteria for traffic signals are stated in terms of the average control delay per vehicle. Delay is a complex measure and is dependent on a number of variables, including the quality of progression, the cycle length, the green ratio, and the v/c ratio for the lane group in question.

Level of Service Criteri	a for Signalized Intersections
Level of Service	Control Delay (Sec/Veh)
A	≤ 10
В	$> 10 \text{ and} \le 20$
C	$> 20 \text{ and} \le 35$
D	$> 35 \text{ and} \le 55$
E	$> 55 \text{ and} \le 80$
F	> 80

Level of Service (LOS) values are used to describe intersection operations with service levels varying from LOS A (free flow) to LOS F (jammed condition). The following descriptions summarize *HCM* criteria for each level of service:

LOS A describes operations with very low control delay, up to 10 seconds per vehicle. This level of service occurs when progression is extremely favorable and most vehicles arrive during the green phase. Most vehicles do not stop at all. Short cycle lengths may also contribute to low delay values.

LOS B describes operations with control delay greater than 10 and up to 20 seconds per vehicle. This level generally occurs with good progression, short cycle lengths, or both. More vehicles stop than with LOS A, causing higher levels of delay.

LOS C describes operations with control delay greater than 20 and up to 35 seconds per vehicle. These higher delays may result from fair progression, longer cycle lengths, or both. Individual cycle failures may begin to appear at this level. The number of vehicles stopping is significant at this level, though many still pass through the intersection without stopping.

LOS D describes operations with control delay greater than 35 and up to 55 seconds per vehicle. At LOS D, the influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, or high v/c ratios. Many vehicles stop, and the proportion of vehicles not stopping declines. Individual cycle failures are noticeable.

LOS E describes operations with control delay greater than 55 and up to 80 seconds per vehicle. This level is considered by many agencies to be the limit of acceptable delay. These high delay values generally indicate poor progression, long cycle lengths, and high v/c ratios. Individual cycle failures are frequent occurrences.

LOS F describes operations with control delay in excess of 80 seconds per vehicle. This level, considered to be unacceptable to most drivers, often occurs with oversaturation, that is, when arrival flow rates exceed the capacity of the lane groups. It may also occur at high *v/c* ratios with many individual cycle failures. Poor progression and long cycle lengths may also be major contributing factors to such delay levels.

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing - AM 1.00 **Urban Street** San Vicente / Melrose Analysis Year 2018 **Analysis Period** 1>7:00 File Name Intersection Intersection #4 04AM - Existing.xus **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R 745 Demand (v), veh/h 88 489 41 251 169 67 575 98 76 429 52 Signal Information sili. Cycle, s 90.0 Reference Phase 2 542 Offset, s 0 Reference Point End 0.0 0.0 Green 55.2 26.8 0.0 0.0 Uncoordinated No Simult. Gap E/W On Yellow 4.0 0.0 0.0 0.0 0.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 2 6 8 4 Case Number 6.0 5.0 6.0 5.0 Phase Duration, s 59.2 59.2 30.8 30.8 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 0.0 0.0 3.2 3.2 Queue Clearance Time (g_s), s 16.1 24.4 Green Extension Time (g_e), s 0.0 0.0 3.0 2.4 Phase Call Probability 1.00 1.00 0.03 0.26 Max Out Probability SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 16 3 8 18 7 4 14 1 6 88 268 262 251 745 169 67 344 329 76 429 52 Adjusted Flow Rate (v), veh/h 727 1900 1848 887 1900 1900 1803 777 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln 1610 974 7.9 5.7 5.7 22.4 14.1 2.1 Queue Service Time (g_s), s 16.0 4.1 5.3 14.0 8.4 8.5 5.7 Cycle Queue Clearance Time (g_c), s 30.4 5.7 21.8 22.4 4.1 13.7 14.0 14.1 22.4 8.5 2.1 Green Ratio (g/C) 0.61 0.61 0.61 0.61 0.61 0.61 0.30 0.30 0.30 0.30 0.30 0.30 Capacity (c), veh/h 344 1166 1134 567 1166 988 278 565 536 190 1076 479 Volume-to-Capacity Ratio (X) 0.256 0.230 0.231 0.442 0.639 0.171 0.610 0.613 0.400 0.399 0.109 0.241 Back of Queue (Q), ft/ln (95 th percentile) 65.3 98.5 96.8 146 344.8 60.2 54.9 255.4 246.3 70.7 159.1 35.2 Back of Queue (Q), veh/ln (95 th percentile) 2.6 3.9 3.9 5.8 13.8 2.4 2.2 10.2 9.9 2.8 6.4 1.4 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 20.7 7.8 7.8 12.7 11.0 7.5 30.7 27.1 27.2 36.8 25.2 23.0 Incremental Delay (d 2), s/veh 1.8 0.5 0.5 2.5 2.7 0.4 0.2 0.4 0.4 0.5 0.1 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 22.5 8.3 8.3 15.2 13.7 7.9 30.8 27.5 27.6 37.3 25.3 23.0 Level of Service (LOS) С Α Α В В Α С С С D С С 10.3 В В 27.9 С 26.7 С Approach Delay, s/veh / LOS 13.2 Intersection Delay, s/veh / LOS 18.6 В **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.23 В 2.28 2.39 В В 2.11 В Bicycle LOS Score / LOS 1.00 Α 2.41 1.10 Α 0.95 Α

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing - PM 1.00 **Urban Street** San Vicente / Melrose Analysis Year 2018 **Analysis Period** 1>7:00 File Name 04PM - Existing.xus Intersection Intersection #4 **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R Demand (v), veh/h 104 604 78 139 425 210 84 669 159 109 470 108 Signal Information Cycle, s 90.0 Reference Phase 2 542 Offset, s 0 Reference Point End 0.0 0.0 Green 46.5 35.5 0.0 0.0 Uncoordinated No Simult. Gap E/W On Yellow 4.0 0.0 0.0 0.0 0.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 2 6 8 4 Case Number 6.0 5.0 6.0 5.0 Phase Duration, s 50.5 50.5 39.5 39.5 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 0.0 0.0 3.3 3.3 Queue Clearance Time (g_s), s 17.9 31.6 Green Extension Time (g_e), s 0.0 0.0 4.4 4.1 Phase Call Probability 1.00 1.00 0.01 0.07 Max Out Probability SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 16 3 8 18 7 4 14 1 6 104 347 335 139 425 210 84 428 400 109 470 108 Adjusted Flow Rate (v), veh/h 978 1900 1900 938 1900 1773 673 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln 1823 771 1610 9.7 9.7 12.5 15.9 15.9 8.2 3.9 Queue Service Time (g_s), s 6.6 11.7 6.5 6.2 13.7 Cycle Queue Clearance Time (g_c), s 19.2 9.7 9.7 21.4 12.5 6.5 14.3 15.9 15.9 29.6 8.2 3.9 Green Ratio (g/C) 0.52 0.52 0.52 0.52 0.52 0.52 0.39 0.39 0.39 0.39 0.39 0.39 1418 Capacity (c), veh/h 452 987 947 397 987 836 363 745 695 225 631 Volume-to-Capacity Ratio (X) 0.230 0.352 0.353 0.431 0.251 0.232 0.575 0.576 0.485 0.332 0.171 0.351 Back of Queue (Q), ft/ln (95 th percentile) 71.6 182.4 176.6 100.8 225.3 104.4 274.8 260.7 98.4 147.6 63.4 60.1 Back of Queue (Q), veh/ln (95 th percentile) 2.9 7.3 7.1 4.0 9.0 4.2 2.4 11.0 10.4 3.9 5.9 2.5 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 19.3 12.7 12.7 19.1 13.4 12.0 24.1 21.5 21.5 33.1 19.1 17.8 Incremental Delay (d 2), s/veh 1.2 1.0 1.0 2.4 1.4 0.7 0.1 0.3 0.3 0.6 0.1 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 20.5 13.7 13.8 21.5 14.8 12.7 24.2 21.7 21.8 33.7 19.2 17.9 Level of Service (LOS) С В В С В В С С С С В В 14.6 В 15.4 В 22.0 С 21.3 С Approach Delay, s/veh / LOS Intersection Delay, s/veh / LOS 18.4 В **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.25 В 2.40 2.27 В В 2.10 В Bicycle LOS Score / LOS 1.14 Α 1.76 1.24 Α 1.05 Α

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Intersection	4	Intersection #6		File Na	ame	UbAIVI	- Existi	ng.xu	S					বাক্ষ	10.7
Project Descript	tion	Our Lady of Mt. Let	oanon P	roject											
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Offset, s	0	Reference Point	End	Green		31.6	4.4	5.					<u> </u>	I L	
Uncoordinated	No	Simult. Gap E/W	On	Yellow	_	4.0	4.0	4.0				/		7_	P
Force Mode	Fixed	Simult. Gap N/S	On	Red	0.0	0.0	0.0	0.0	0.0	0.0		5	6	7	8
Timer Results				EBI		EBT	WB		WBT	NE	SI .	NBT	SBI		SBT
Assigned Phase	 е			5	_	2	1	_	6	3		8	7	_	4
Case Number	-			2.0		3.0	2.0		3.0	2.		3.0	2.0		3.0
Phase Duration	, S			8.4		44.0	11.1		46.6	9.	5	25.5	9.5		25.5
Change Period,	<u> </u>	c). s		4.0		4.0	4.0		4.0	4.		4.0	4.0		4.0
Max Allow Head		·		3.1		0.0	3.1		0.0	3.		3.1	3.1		3.1
Queue Clearan		<u>·</u>		4.6			7.4	$\overline{}$		6.		18.0	6.2		12.8
Green Extensio					0.4		0.2	_	0.0	0.		3.5	0.0	_	3.7
Phase Call Prob		(3 //		0.73		0.0	0.94	_		0.8		1.00	0.88	_	1.00
Max Out Probal				1.00			0.00	_		0.0		0.04	0.37	7	0.01
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Movement Gro		sults			EB	T 5	.	WI		+ .	NB —		<u> </u>	SB	
Approach Move				<u> </u>	T	R	L	Т	R	L	T	R	<u> </u>	T	R
Assigned Move				5	2	12	1	6	16	3	8	18	7	4	14
Adjusted Flow F		,		53	627	127	110	115		84	685	114	85	493	182
Queue Service		ow Rate (s), veh/h/l	n	1810	1809	1610	1810	180 22.				1610	1810	1809	1610
Cycle Queue C		· · · · · · · · · · · · · · · · · · ·		2.6	10.5 10.5	3.8	5.4 5.4	22.	_	4.1	16.0	5.2 5.2	4.2	10.8	8.2
Green Ratio (g		e Tille (<i>g c)</i> , s		0.05	0.44	0.51	0.08	0.4	_		0.24	0.24	0.06	0.24	0.29
Capacity (c), v				89	1607	813	142	171		110	864	385	110	863	463
Volume-to-Capa		atio (X)		0.598	0.390	0.156	0.775	0.67	_			0.296	0.774	0.571	0.393
		/In (95 th percentile))	53.4	190.9		111.1	348		_	277.3	88.5	87.7	202	96.5
		eh/ln (95 th percenti		2.1	7.6	2.5	4.4	13.	_	3.5	11.1	3.5	3.5	8.1	3.9
	• •	RQ) (95 th percent		0.00	0.00	0.00	0.00	0.0	_		0.00	0.00	0.00	0.00	0.00
	uiform Delay (d 1), s/veh			41.9	16.8	12.0	40.7	18.		41.6	32.2	28.1	41.7	30.2	1.4
	ncremental Delay (d 2), s/veh			2.4	0.7	0.4	3.4	2.1	0.4	4.1	0.6	0.2	4.3	0.2	0.2
Initial Queue De	itial Queue Delay (d 3), s/veh			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Control Delay (Control Delay (d), s/veh				17.5	12.4	44.1	20.	4 1.6	45.7	32.8	28.2	46.0	30.4	1.6
Level of Service	Level of Service (LOS)				В	В	D	С	А	D	С	С	D	С	Α
Approach Delay	y, s/veh	/ LOS		18.5	5	В	20.6	6	С	33	4	С	25.3	3	С
Intersection Del	lay, s/ve	h / LOS				24	1.0						С		
84-14:								147			NE			00	
Multimodal Re Pedestrian LOS		/1.08		0.40	EB	D	0.40	WI		2.4	NB	D	0.44	SB	
				2.42		В	2.46	_	B B	2.4		В	2.44		В
Bicycle LOS Sc	OIE / LC	73		1.15	,	Α	1.64	t	D	1.2	. <u> </u>	Α	1.11		Α

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing - PM 1.00 **Urban Street** San Vicente / Beverly Analysis Year 2018 **Analysis Period** 1>7:00 06PM - Existing.xus Intersection Intersection #6 File Name **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R 481 Demand (v), veh/h 71 828 72 80 768 137 108 713 424 215 127 Signal Information Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End Green 5.0 28.6 18.2 5.5 6.9 1.9 Uncoordinated No Simult. Gap E/W On Yellow 4.0 4.0 4.0 4.0 4.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 5 2 6 8 1 3 7 4 Case Number 2.0 3.0 2.0 3.0 2.0 3.0 2.0 3.0 Phase Duration, s 31.2 9.5 31.7 10.9 32.6 16.8 38.5 9.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 3.1 0.0 3.1 0.0 3.1 3.1 3.1 3.1 Queue Clearance Time (g_s), s 5.5 5.9 7.3 24.0 12.4 10.5 Green Extension Time (g_e), s 0.1 0.0 0.4 0.0 0.1 4.6 0.4 4.8 Phase Call Probability 0.83 0.86 0.93 1.00 1.00 1.00 0.00 0.02 0.02 0.00 0.00 Max Out Probability 1.00 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 1 16 3 8 18 7 4 14 6 71 828 72 80 768 137 108 713 424 215 481 127 Adjusted Flow Rate (v), veh/h Adjusted Saturation Flow Rate (s), veh/h/ln 1810 1610 1810 1809 1810 1809 1610 1810 1809 1610 1809 1610 3.5 2.6 3.9 16.8 15.1 22.0 4.3 Queue Service Time (g_s), s 18.6 4.6 5.3 10.4 8.5 Cycle Queue Clearance Time (g c), s 3.5 18.6 2.6 3.9 16.8 4.6 5.3 15.1 22.0 10.4 8.5 4.3 Green Ratio (g/C) 0.06 0.30 0.38 0.06 0.31 0.45 80.0 0.32 0.32 0.14 0.38 0.44 Capacity (c), veh/h 100 1094 610 110 1113 724 138 1149 511 256 1385 706 Volume-to-Capacity Ratio (X) 0.709 0.757 0.118 0.729 0.690 0.189 0.783 0.621 0.829 0.838 0.347 0.180 Back of Queue (Q), ft/ln (95 th percentile) 72.5 330.1 28.8 88.4 298.7 76.8 109.6 258.2 267.6 205.7 154.4 68 Back of Queue (Q), veh/ln (95 th percentile) 2.9 13.2 1.2 3.5 11.9 3.1 4.4 10.3 10.7 8.2 6.2 2.7 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 41.8 28.4 2.2 41.5 27.4 14.9 40.8 26.1 3.3 37.6 19.8 15.4 Incremental Delay (d 2), s/veh 3.4 4.9 0.4 8.5 3.5 0.6 3.6 0.2 1.4 2.8 0.1 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 45.2 33.3 2.6 50.0 30.9 15.5 44.5 26.3 4.7 40.4 19.8 15.5 Level of Service (LOS) D С Α D С В D С Α D В В 20.5 31.9 С 30.3 С С 24.5 С Approach Delay, s/veh / LOS Intersection Delay, s/veh / LOS 26.5 С **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.46 В 2.42 2.43 В 2.43 В В Bicycle LOS Score / LOS 1.29 Α 1.30 Α 1.51 В 1.17 Α

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing - AM 1.00 **Urban Street** La Cienega / Melrose Analysis Year 2018 **Analysis Period** 1>7:00 File Name Intersection Intersection #10 10AM - Existing.xus **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R Demand (v), veh/h 53 377 34 501 895 38 47 591 160 58 841 154 Signal Information ٨. Cycle, s 90.0 Reference Phase 2 542 Offset, s 0 Reference Point End 0.0 Green 19.8 24.3 33.9 0.0 0.0 Uncoordinated No Simult. Gap E/W On Yellow 4.0 4.0 0.0 0.0 0.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 2 6 8 1 4 Case Number 5.3 1.0 3.0 5.0 6.0 Phase Duration, s 28.3 23.8 52.1 37.9 37.9 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 0.0 3.1 0.0 3.2 3.2 Queue Clearance Time (g_s), s 18.8 29.3 22.7 Green Extension Time (g_e), s 0.0 1.0 0.0 4.8 5.0 Phase Call Probability 1.00 1.00 1.00 0.08 0.03 Max Out Probability 0.00 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 16 3 8 18 7 4 14 1 6 53 377 34 501 895 38 47 591 160 58 511 484 Adjusted Flow Rate (v), veh/h 632 1809 1610 1810 1809 575 1809 1610 839 1900 Adjusted Saturation Flow Rate (s), veh/h/ln 1797 7.6 13.7 6.2 20.7 Queue Service Time (g_s), s 6.0 1.4 16.8 6.8 11.0 5.0 20.7 1.4 16.8 20.7 Cycle Queue Clearance Time (g_c), s 6.2 7.6 13.7 27.3 11.0 6.2 15.8 20.7 Green Ratio (g/C) 0.27 0.27 0.27 0.51 0.53 0.38 0.38 0.38 0.38 0.38 0.38 Capacity (c), veh/h 249 978 435 666 1936 165 1360 605 294 714 675 Volume-to-Capacity Ratio (X) 0.212 0.385 0.078 0.752 0.462 0.284 0.435 0.264 0.197 0.716 0.716 Back of Queue (Q), ft/ln (95 th percentile) 45.6 150.3 25.5 262.7 226 42.6 196.8 100.2 43.9 342.8 327.6 Back of Queue (Q), veh/ln (95 th percentile) 1.8 6.0 1.0 10.5 9.0 1.7 7.9 4.0 1.8 13.7 13.1 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 26.3 26.7 24.5 15.8 12.9 35.6 21.0 19.5 26.8 24.0 24.0 Incremental Delay (d 2), s/veh 1.9 1.1 0.4 0.7 8.0 0.3 0.1 0.1 0.1 0.5 0.5 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 28.2 27.9 24.8 16.5 13.7 0.0 35.9 21.0 19.6 26.9 24.5 24.5 Level of Service (LOS) С С С В В Α D С В С С С 27.7 С 14.3 В С 24.6 С Approach Delay, s/veh / LOS 21.6 Intersection Delay, s/veh / LOS 20.4 С **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.44 В 2.25 2.42 2.42 В В В Bicycle LOS Score / LOS 0.87 Α 1.67 1.15 Α 1.36

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing - PM 1.00 **Urban Street** La Cienega / Melrose Analysis Year 2018 **Analysis Period** 1>7:00 File Name 10PM - Existing.xus Intersection Intersection #10 **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R Demand (v), veh/h 122 868 54 268 565 100 54 985 337 64 806 111 Signal Information ٨. Cycle, s 90.0 Reference Phase 2 542 Offset, s 0 Reference Point End 37.2 0.0 Green 10.7 30.1 0.0 0.0 Uncoordinated No Simult. Gap E/W On Yellow 4.0 0.0 0.0 0.0 4.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 2 6 8 1 4 Case Number 5.3 1.0 3.0 5.0 6.0 Phase Duration, s 34.1 14.7 48.8 41.2 41.2 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 0.0 3.1 0.0 3.3 3.3 Queue Clearance Time (g_s), s 10.2 25.9 30.7 Green Extension Time (g_e), s 0.0 0.5 0.0 7.2 6.7 Phase Call Probability 1.00 1.00 1.00 0.15 0.23 Max Out Probability 0.00 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 16 3 8 18 7 4 14 1 6 122 868 54 268 565 100 54 985 337 64 468 449 Adjusted Flow Rate (v), veh/h 859 1809 1610 1810 1809 1809 1610 580 1900 1819 Adjusted Saturation Flow Rate (s), veh/h/ln 619 9.9 2.1 14.0 Queue Service Time (g_s), s 18.9 8.2 8.3 6.7 19.8 9.0 17.3 17.3 Cycle Queue Clearance Time (g_c), s 10.0 18.9 2.1 8.2 8.3 23.9 19.8 14.0 28.7 17.3 17.3 Green Ratio (g/C) 0.33 0.33 0.33 0.48 0.50 0.41 0.41 0.41 0.41 0.41 0.41 Capacity (c), veh/h 368 1214 541 375 1804 217 1492 664 192 783 750 Volume-to-Capacity Ratio (X) 0.332 0.715 0.100 0.714 0.313 0.249 0.660 0.508 0.333 0.598 0.598 Back of Queue (Q), ft/ln (95 th percentile) 97.6 326 36.4 145.2 147.1 44.2 312 215.8 56.1 291.8 281.8 Back of Queue (Q), veh/ln (95 th percentile) 3.9 13.0 1.5 5.8 5.9 1.8 12.5 8.6 2.2 11.7 11.3 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 23.2 26.1 20.5 18.6 13.4 29.9 21.4 19.7 32.9 20.6 20.6 Incremental Delay (d 2), s/veh 2.4 3.6 0.4 1.0 0.5 0.2 0.2 0.2 0.4 0.3 0.3 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 25.6 29.7 20.9 19.5 13.9 0.0 30.1 21.5 19.9 33.3 20.9 20.9 Level of Service (LOS) С С С В В Α С С В С С С 21.5 28.8 С 14.0 В С 21.7 С Approach Delay, s/veh / LOS Intersection Delay, s/veh / LOS С 21.7 **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.43 В 2.25 2.42 2.42 В В В Bicycle LOS Score / LOS 1.35 Α 1.26 Α 1.62 В 1.30 Α

HCS7 Signalized Intersection Results Summary 1414141 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing with 1.00 Project - AM **Urban Street** Analysis Year 2018 1> 7:00 San Vicente / Melrose **Analysis Period** File Name Intersection Intersection #4 04AM - Existing + Project.xus **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 88 489 41 251 745 169 67 578 98 76 430 52 Signal Information Cycle, s 90.0 Reference Phase 2 $\P A Z$ Offset, s 0 Reference Point End Green 55.1 26.9 0.0 0.0 0.0 0.0 Uncoordinated No Simult, Gap E/W On Yellow 4.0 0.0 0.0 0.0 0.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 2 6 8 4 Case Number 6.0 5.0 6.0 5.0 Phase Duration, s 59.1 59.1 30.9 30.9 4.0 4.0 Change Period, (Y+Rc), s 4.0 4.0 Max Allow Headway (MAH), s 0.0 0.0 3.2 3.2 Queue Clearance Time (g_s), s 16.1 24.5 Green Extension Time (g_e), s 0.0 0.0 3.0 2.4 Phase Call Probability 1.00 1.00 Max Out Probability 0.03 0.27 SB **Movement Group Results** EΒ WB NB Approach Movement L Т R L Т R L Т R L Т R 5 2 12 3 18 7 4 14 **Assigned Movement** 1 6 16 8 Adjusted Flow Rate (v), veh/h 88 268 262 251 745 169 67 346 330 76 430 52 727 1900 1848 887 1900 1610 973 1900 1804 775 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 7.9 5.7 5.8 16.0 22.5 4.1 5.3 14.1 14.1 8.4 8.5 2.1 Cycle Queue Clearance Time (gc), s 30.5 5.7 5.8 21.9 22.5 13.8 14.1 14.1 22.5 8.5 4.1 2.1 Green Ratio (g/C) 0.61 0.61 0.61 0.61 0.61 0.61 0.30 0.30 0.30 0.30 0.30 0.30 343 1164 1133 566 987 567 538 190 1079 480 Capacity (c), veh/h 1164 279 Volume-to-Capacity Ratio (X) 0.256 0.230 0.231 0.443 0.640 0.171 0.240 0.611 0.613 0.400 0.399 0.108 Back of Queue (Q), ft/ln (95 th percentile) 65.6 98.8 97.2 146.7 345.6 60.4 54.9 256 246.9 70.7 159.2 35.1 1.4 Back of Queue (Q), veh/ln (95 th percentile) 2.6 4.0 3.9 5.9 13.8 2.4 2.2 10.2 9.9 2.8 6.4 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 20.8 7.9 7.9 12.8 11.1 7.5 30.6 27.1 27.1 36.7 25.2 22.9 Incremental Delay (d 2), s/veh 1.8 0.5 0.5 2.5 2.7 0.4 0.2 0.4 0.4 0.5 0.1 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 22.6 15.3 37.3 Control Delay (d), s/veh 8.3 8.3 13.8 7.9 30.8 27.5 27.5 25.2 22.9 Level of Service (LOS) С Α Α В В Α С С С D С С Approach Delay, s/veh / LOS 10.4 В 13.3 В С 26.7 С 27.8 Intersection Delay, s/veh / LOS 18.6 R **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.23 2.28 В 2.39 В В 2.11 В Bicycle LOS Score / LOS 1.00 Α 2.41 В 1.10 Α 0.95 Α

HCS7 Signalized Intersection Results Summary 1414141 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing with 1.00 Project - PM **Urban Street** Analysis Year 2018 1> 7:00 San Vicente / Melrose **Analysis Period** File Name Intersection Intersection #4 04PM - Existing + Project.xus **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R 109 Demand (v), veh/h 104 604 78 139 425 210 84 671 159 473 108 Signal Information Cycle, s 90.0 Reference Phase 2 $\P A Z$ Offset, s 0 Reference Point End Green 46.4 35.6 0.0 0.0 0.0 0.0 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 0.0 0.0 0.0 0.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 2 6 8 4 Case Number 6.0 5.0 6.0 5.0 Phase Duration, s 50.4 50.4 39.6 39.6 4.0 4.0 Change Period, (Y+Rc), s 4.0 4.0 Max Allow Headway (MAH), s 0.0 0.0 3.3 3.3 Queue Clearance Time (g_s), s 18.0 31.6 Green Extension Time (g_e), s 0.0 0.0 4.5 4.2 Phase Call Probability 1.00 1.00 Max Out Probability 0.01 0.07 **Movement Group Results** ΕB WB NB SB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 3 18 7 4 14 1 6 16 8 429 Adjusted Flow Rate (v), veh/h 104 347 335 139 425 210 84 401 109 473 108 978 1900 1823 771 1900 1610 935 1900 1773 671 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 6.7 9.7 9.7 11.7 12.5 6.5 6.2 15.9 16.0 13.7 8.2 3.9 Cycle Queue Clearance Time (g c), s 19.2 9.7 9.7 21.5 12.5 6.5 14.4 15.9 16.0 29.6 8.2 3.9 Green Ratio (g/C) 0.52 0.52 0.52 0.52 0.52 0.52 0.40 0.40 0.40 0.40 0.40 0.40 451 985 945 396 985 835 362 746 696 225 1420 632 Capacity (c), veh/h Volume-to-Capacity Ratio (X) 0.231 0.353 0.354 0.351 0.431 0.252 0.232 0.575 0.576 0.485 0.333 0.171 Back of Queue (Q), ft/ln (95 th percentile) 71.7 183.3 177.1 101 225.7 104.7 60.2 274.9 260.9 98.3 148.3 63.3 Back of Queue (Q), veh/ln (95 th percentile) 2.9 7.3 7.1 4.0 9.0 4.2 2.4 11.0 10.4 3.9 5.9 2.5 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 12.8 Uniform Delay (d 1), s/veh 19.4 12.8 19.1 13.4 12.0 24.1 21.4 21.4 33.0 19.1 17.8 Incremental Delay (d 2), s/veh 1.2 1.0 1.0 2.4 1.4 0.7 0.1 0.3 0.3 0.6 0.1 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 20.6 14.8 24.2 21.7 Control Delay (d), s/veh 13.8 13.8 21.6 12.7 21.7 33.6 19.1 17.8 Level of Service (LOS) С В В С В В С С С С В В 14.7 Approach Delay, s/veh / LOS В 15.5 В С 21.2 С 21.9 Intersection Delay, s/veh / LOS 18.4 R **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.25 2.27 В 2.40 В В 2.10 В Bicycle LOS Score / LOS 1.14 Α 1.76 В 1.24 Α 1.06 Α

HCS7 Signalized Intersection Results Summary 1414141 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing with 1.00 Project - AM **Urban Street** Analysis Year 2018 1> 7:00 San Vicente / Beverly **Analysis Period** File Name Intersection Intersection #6 06AM - Existing + Project.xus **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 53 627 127 110 1154 129 84 688 114 85 494 182 Signal Information Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End Green 7.1 31.5 4.4 5.5 21.6 0.0 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 4.0 4.0 4.0 0.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 5 2 6 3 8 1 7 4 Case Number 2.0 3.0 2.0 3.0 2.0 3.0 2.0 3.0 Phase Duration, s 8.4 43.9 11.1 46.6 9.5 25.6 9.5 25.6 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 3.1 0.0 3.1 0.0 3.1 3.1 3.1 3.1 Queue Clearance Time (g_s), s 4.6 7.4 6.1 18.1 6.2 12.8 Green Extension Time (g_e), s 0.4 0.0 0.2 0.0 0.1 3.5 0.0 3.7 Phase Call Probability 0.73 0.94 0.88 1.00 0.88 1.00 Max Out Probability 1.00 0.00 0.00 0.04 0.37 0.01 **Movement Group Results** EB WB NB SB L Т R L Т R L Т R L Т R Approach Movement **Assigned Movement** 5 2 12 3 18 7 4 14 1 6 16 8 Adjusted Flow Rate (v), veh/h 53 627 127 110 1154 129 84 688 114 85 494 182 1810 1809 1610 1810 1809 1610 1810 1809 1610 1810 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 2.6 10.5 3.8 5.4 22.2 3.7 4.1 16.1 5.2 4.2 10.8 8.2 Cycle Queue Clearance Time (g c), s 2.6 10.5 3.8 5.4 22.2 16.1 5.2 4.2 10.8 3.7 4.1 8.2 Green Ratio (g/C) 0.05 0.44 0.50 0.08 0.47 0.53 0.06 0.24 0.24 0.06 0.24 0.29 89 1604 812 142 859 867 386 866 464 Capacity (c), veh/h 1711 110 110 0.675 Volume-to-Capacity Ratio (X) 0.598 0.391 0.156 0.775 0.150 0.763 0.793 0.295 0.774 0.570 0.392 Back of Queue (Q), ft/ln (95 th percentile) 53.4 190.9 61.6 111.1 349.7 30.9 86.3 278 88.4 87.7 202.1 96.3 Back of Queue (Q), veh/ln (95 th percentile) 2.1 7.6 2.5 4.4 14.0 1.2 3.5 11.1 3.5 3.5 8.1 3.9 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 41.9 16.9 12.0 40.7 18.4 1.2 41.6 32.1 28.0 41.7 30.1 1.4 Incremental Delay (d 2), s/veh 2.4 0.7 0.4 3.4 2.1 0.4 4.1 0.6 0.2 4.3 0.2 0.2 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 44.3 46.0 Control Delay (d), s/veh 17.6 12.4 44.1 20.5 1.6 45.7 32.8 28.2 30.4 1.6 Level of Service (LOS) D В В D С Α D C С D С Α В 20.6 С С 25.2 С Approach Delay, s/veh / LOS 18.5 33.4 Intersection Delay, s/veh / LOS 24.0 С **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.42 2.44 В 2.46 В В 2.44 В Bicycle LOS Score / LOS 1.15 Α 1.64 В 1.22 Α 1.12 Α

HCS7 Signalized Intersection Results Summary 1414141 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing with 1.00 Project - PM **Urban Street** Analysis Year 2018 1> 7:00 San Vicente / Beverly **Analysis Period** File Name Intersection Intersection #6 06PM - Existing + Project.xus **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R 137 Demand (v), veh/h 71 828 72 80 768 108 715 424 215 484 127 Signal Information Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End Green 5.0 6.9 1.9 28.6 18.2 5.5 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 4.0 4.0 4.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 5 2 6 3 8 1 7 4 Case Number 2.0 3.0 2.0 3.0 2.0 3.0 2.0 3.0 Phase Duration, s 9.0 31.2 9.5 31.7 10.9 32.6 16.8 38.5 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 3.1 0.0 3.1 0.0 3.1 3.1 3.1 3.1 Queue Clearance Time (g_s), s 5.5 5.9 7.3 24.0 12.4 10.6 Green Extension Time (g_e), s 0.1 0.0 0.4 0.0 0.1 4.6 0.4 4.8 Phase Call Probability 0.83 0.86 0.93 1.00 1.00 1.00 Max Out Probability 0.00 1.00 0.02 0.02 0.00 0.00 **Movement Group Results** EB WB NB SB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 3 18 7 4 14 1 6 16 8 424 Adjusted Flow Rate (v), veh/h 71 828 72 80 768 137 108 715 215 484 127 1810 1809 1610 1810 1809 1610 1810 1809 1610 1810 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 3.5 18.6 2.6 3.9 16.8 4.6 5.3 15.1 22.0 10.4 8.6 4.3 Cycle Queue Clearance Time (g c), s 3.5 18.6 2.6 3.9 16.8 4.6 15.1 22.0 10.4 8.6 5.3 4.3 Green Ratio (g/C) 0.06 0.30 0.38 0.06 0.31 0.45 0.08 0.32 0.32 0.14 0.38 0.44 100 1093 609 723 256 Capacity (c), veh/h 110 1112 138 1149 511 1386 706 Volume-to-Capacity Ratio (X) 0.709 0.757 0.118 0.729 0.690 0.189 0.783 0.622 0.829 0.838 0.349 0.180 Back of Queue (Q), ft/ln (95 th percentile) 72.5 330.1 28.8 88.4 298.7 76.8 109.6 258.7 267.6 205.7 155.4 68 Back of Queue (Q), veh/ln (95 th percentile) 2.9 13.2 1.2 3.5 11.9 3.1 4.4 10.3 10.7 8.2 6.2 2.7 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 41.8 28.4 2.2 41.5 27.4 14.9 40.8 26.1 3.3 37.6 19.8 15.4 Incremental Delay (d 2), s/veh 3.4 4.9 0.4 8.5 3.5 0.6 3.6 0.2 1.3 2.8 0.1 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 45.2 50.0 44.5 40.4 Control Delay (d), s/veh 33.3 2.6 30.9 15.5 26.3 4.7 19.8 15.4 Level of Service (LOS) D С D С В D С Α D В В Α С 30.3 С С 24.5 С Approach Delay, s/veh / LOS 31.9 20.5 Intersection Delay, s/veh / LOS 26.5 С **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.46 2.43 В 2.43 В В 2.42 В Bicycle LOS Score / LOS 1.29 Α 1.30 Α 1.52 В 1.17 Α

HCS7 Signalized Intersection Results Summary 14747 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing with 1.00 Project - AM **Urban Street** La Cienega / Melrose Analysis Year 2018 1> 7:00 **Analysis Period** File Name Intersection Intersection #10 10AM - Existing + Project.xus **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 53 377 34 501 895 38 47 594 160 58 842 154 Signal Information ٨. Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End Green 19.8 34.0 0.0 0.0 24.2 0.0 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 4.0 0.0 0.0 0.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 2 6 8 4 1 Case Number 5.3 1.0 3.0 5.0 6.0 Phase Duration, s 28.2 23.8 52.0 38.0 38.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s 4.0 Max Allow Headway (MAH), s 0.0 3.1 0.0 3.2 3.2 Queue Clearance Time (g_s), s 18.8 29.3 22.7 Green Extension Time (g_e), s 0.0 1.0 0.0 4.8 5.0 Phase Call Probability 1.00 1.00 1.00 Max Out Probability 0.00 0.08 0.03 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L R 5 2 12 3 18 7 4 14 **Assigned Movement** 1 6 16 8 Adjusted Flow Rate (v), veh/h 53 377 34 501 895 38 47 594 160 58 512 484 632 1809 1610 1810 1809 574 1809 1610 836 1900 1797 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 6.0 7.6 1.4 16.8 13.8 6.8 11.0 6.2 5.0 20.7 20.7 Cycle Queue Clearance Time (gc), s 13.8 6.2 7.6 1.4 16.8 27.3 11.0 6.2 15.9 20.7 20.7 Green Ratio (g/C) 0.27 0.27 0.27 0.51 0.53 0.38 0.38 0.38 0.38 0.38 0.38 249 976 434 666 1935 1361 606 294 Capacity (c), veh/h 165 715 676 Volume-to-Capacity Ratio (X) 0.213 0.386 0.078 0.753 0.463 0.284 0.436 0.264 0.198 0.716 0.716 Back of Queue (Q), ft/ln (95 th percentile) 45.6 150.5 25.6 263.2 226 42.6 197.9 100.2 43.9 343.1 327.9 Back of Queue (Q), veh/ln (95 th percentile) 1.8 6.0 1.0 10.5 9.0 1.7 7.9 4.0 1.8 13.7 13.1 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 26.3 26.8 24.5 15.8 12.9 35.5 20.9 19.4 26.8 24.0 24.0 Incremental Delay (d 2), s/veh 1.9 1.2 0.4 0.7 8.0 0.3 0.1 0.1 0.1 0.5 0.5 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 13.7 35.9 26.9 Control Delay (d), s/veh 28.3 27.9 24.9 16.5 0.0 21.0 19.5 24.5 24.5 Level of Service (LOS) С С С В В D C В С С С Α Approach Delay, s/veh / LOS 27.8 С 14.3 В С 24.6 С 21.6 Intersection Delay, s/veh / LOS 20.4 С **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.44 2.42 В 2.25 В В 2.42 В Bicycle LOS Score / LOS 0.87 Α 1.67 В 1.15 Α 1.36 Α

HCS7 Signalized Intersection Results Summary 14747 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Existing with 1.00 Project - PM **Urban Street** La Cienega / Melrose Analysis Year 2018 1> 7:00 **Analysis Period** File Name Intersection Intersection #10 10PM - Existing + Project.xus **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 122 868 54 268 565 100 54 987 337 64 809 111 Signal Information ٨. Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End Green 10.7 30.0 37.3 0.0 0.0 0.0 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 4.0 0.0 0.0 0.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 2 6 8 4 1 Case Number 5.3 1.0 3.0 5.0 6.0 Phase Duration, s 34.0 14.7 48.7 41.3 41.3 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s 4.0 Max Allow Headway (MAH), s 0.0 3.1 0.0 3.3 3.3 Queue Clearance Time (g_s), s 10.2 26.0 30.7 Green Extension Time (g_e), s 0.0 0.5 0.0 7.2 6.7 Phase Call Probability 1.00 1.00 1.00 Max Out Probability 0.00 0.15 0.24 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R 5 2 12 3 7 4 14 **Assigned Movement** 1 6 16 8 18 122 470 Adjusted Flow Rate (v), veh/h 868 54 268 565 100 54 987 337 64 450 859 1809 1610 1810 1809 617 1809 1610 579 1900 1819 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 9.9 18.9 2.1 8.2 8.4 6.7 19.8 14.0 9.0 17.4 17.4 Cycle Queue Clearance Time (g c), s 10.0 18.9 8.2 8.4 24.0 19.8 14.0 28.7 17.4 2.1 17.4 Green Ratio (g/C) 0.33 0.33 0.33 0.48 0.50 0.41 0.41 0.41 0.41 0.41 0.41 1211 539 1802 1494 665 192 Capacity (c), veh/h 367 375 216 785 751 Volume-to-Capacity Ratio (X) 0.333 0.716 0.100 0.715 0.314 0.250 0.661 0.507 0.333 0.599 0.599 Back of Queue (Q), ft/ln (95 th percentile) 97.7 326.6 36.5 145.5 147.1 44.2 312.6 215.6 56.1 293 283 Back of Queue (Q), veh/ln (95 th percentile) 3.9 13.1 1.5 5.8 5.9 1.8 12.5 8.6 2.2 11.7 11.3 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 23.3 26.2 20.6 18.6 13.4 29.9 21.3 19.6 32.9 20.6 20.6 Incremental Delay (d 2), s/veh 2.4 3.7 0.4 1.0 0.5 0.2 0.2 0.2 0.4 0.3 0.3 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 13.9 33.3 Control Delay (d), s/veh 25.7 29.8 21.0 19.6 0.0 30.1 21.5 19.8 20.9 20.9 Level of Service (LOS) С С С В В Α С C В С С С 28.9 Approach Delay, s/veh / LOS С 14.0 В С 21.7 С 21.4 Intersection Delay, s/veh / LOS 21.7 С **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.43 2.42 В 2.25 В В 2.42 В Bicycle LOS Score / LOS 1.35 Α 1.26 Α 1.62 В 1.30 Α

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future - AM 1.00 **Urban Street** San Vicente / Melrose Analysis Year 2024 **Analysis Period** 1>7:00 File Name 04AM - Future.xus Intersection Intersection #4 **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R 466 Demand (v), veh/h 93 521 44 270 794 179 71 625 108 81 55 Signal Information sili. Cycle, s 90.0 Reference Phase 2 542 Offset, s 0 Reference Point End 0.0 0.0 Green 52.9 29.1 0.0 0.0 Uncoordinated No Simult. Gap E/W On Yellow 4.0 0.0 0.0 0.0 0.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 2 6 8 4 Case Number 6.0 5.0 6.0 5.0 Phase Duration, s 56.9 56.9 33.1 33.1 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 0.0 0.0 3.3 3.3 Queue Clearance Time (g_s), s 17.1 26.4 Green Extension Time (g_e), s 0.0 0.0 3.4 2.6 Phase Call Probability 1.00 1.00 0.04 Max Out Probability 0.31 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 16 3 8 18 7 4 14 1 6 93 286 279 270 794 179 71 376 357 81 466 55 Adjusted Flow Rate (v), veh/h 694 1900 1848 859 1900 1610 1900 1802 735 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln 941 9.9 20.0 26.6 15.0 15.1 9.0 2.2 Queue Service Time (g_s), s 6.6 6.6 4.6 5.7 9.4 2.2 Cycle Queue Clearance Time (g_c), s 36.5 6.6 6.6 26.7 26.6 4.6 14.7 15.0 15.1 24.4 9.0 Green Ratio (g/C) 0.59 0.59 0.59 0.59 0.59 0.59 0.32 0.32 0.32 0.32 0.32 0.32 Capacity (c), veh/h 283 1118 1087 522 1118 948 290 613 581 194 1167 519 Volume-to-Capacity Ratio (X) 0.329 0.256 0.257 0.517 0.710 0.189 0.613 0.615 0.417 0.399 0.106 0.245 Back of Queue (Q), ft/ln (95 th percentile) 81.5 116.3 114.2 183.3 410.4 70.3 56.9 268.5 258.5 75 166.9 35.6 Back of Queue (Q), veh/ln (95 th percentile) 3.3 4.7 4.6 7.3 16.4 2.8 2.3 10.7 10.3 3.0 6.7 1.4 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 26.0 9.0 9.0 15.5 13.1 8.6 29.4 25.7 25.8 36.1 23.7 21.4 Incremental Delay (d 2), s/veh 3.1 0.6 0.6 3.6 3.8 0.4 0.2 0.4 0.5 0.5 0.1 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 29.1 9.5 9.5 19.1 16.9 9.0 29.5 26.2 26.2 36.6 23.8 21.4 Level of Service (LOS) С Α Α В В Α С С С D С С 12.3 В В 26.5 С 25.3 С Approach Delay, s/veh / LOS 16.2 Intersection Delay, s/veh / LOS 19.6 В **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.24 В 2.28 2.39 В В 2.11 В Bicycle LOS Score / LOS 1.03 Α 2.54 1.15 Α 0.98 Α

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future - PM 1.00 **Urban Street** San Vicente / Melrose Analysis Year 2024 **Analysis Period** 1>7:00 File Name 04PM - Future.xus Intersection Intersection #4 **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R Demand (v), veh/h 110 646 83 157 456 223 89 734 177 116 528 115 Signal Information sili. Cycle, s 90.0 Reference Phase 2 542 Offset, s 0 Reference Point End 0.0 0.0 Green 43.4 38.6 0.0 0.0 Uncoordinated No Simult. Gap E/W On Yellow 4.0 0.0 0.0 0.0 0.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 2 6 8 4 Case Number 6.0 5.0 6.0 5.0 Phase Duration, s 47.4 47.4 42.6 42.6 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 0.0 0.0 3.4 3.4 Queue Clearance Time (g_s), s 19.0 34.7 Green Extension Time (g_e), s 0.0 0.0 5.1 4.0 Phase Call Probability 1.00 1.00 0.03 Max Out Probability 0.31 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 16 3 8 18 7 4 14 1 6 110 372 357 157 456 223 89 471 440 116 528 115 Adjusted Flow Rate (v), veh/h 950 1900 738 1900 1900 1772 622 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln 1824 1610 889 8.0 11.3 14.7 7.5 17.0 8.8 4.0 Queue Service Time (g_s), s 11.3 15.6 6.7 17.0 15.7 Cycle Queue Clearance Time (g_c), s 22.7 11.3 11.3 27.0 14.7 7.5 15.5 17.0 17.0 32.7 8.8 4.0 Green Ratio (g/C) 0.48 0.48 0.48 0.48 0.48 0.48 0.43 0.43 0.43 0.43 0.43 0.43 Capacity (c), veh/h 384 918 881 343 918 778 374 813 758 229 1549 689 Volume-to-Capacity Ratio (X) 0.287 0.405 0.406 0.457 0.497 0.287 0.579 0.580 0.507 0.341 0.167 0.238 Back of Queue (Q), ft/ln (95 th percentile) 86.8 212.5 206.7 135 263 123.3 61.2 285.4 270.4 103.9 155.9 62.6 Back of Queue (Q), veh/ln (95 th percentile) 3.5 8.5 8.3 5.4 10.5 4.9 2.4 11.4 10.8 4.2 6.2 2.5 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 23.6 15.0 15.0 23.6 15.8 14.0 22.4 19.6 19.6 32.0 17.2 15.8 Incremental Delay (d 2), s/veh 1.9 1.3 1.4 4.3 1.9 0.9 0.1 0.2 0.3 0.6 0.0 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 25.4 16.3 16.3 28.0 17.7 14.9 22.5 19.8 19.8 32.6 17.3 15.9 Level of Service (LOS) С В В С В В С В В С В В 17.5 В В 20.1 С 19.4 В Approach Delay, s/veh / LOS 18.9 Intersection Delay, s/veh / LOS 19.0 В **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.26 В 2.26 2.41 В В 2.10 В Bicycle LOS Score / LOS 1.18 Α 1.87 1.31 Α 1.11 Α

HCS7 Signalized Intersection Results Summary 147477 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future - AM 1.00 **Urban Street** San Vicente / Beverly Analysis Year 2024 **Analysis Period** 1>7:00 File Name 06AM - Future.xus Intersection Intersection #6 **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R Demand (v), veh/h 56 703 149 118 1258 137 107 734 124 90 526 193 Signal Information Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End 5.8 Green 7.5 29.2 4.5 1.1 21.8 Uncoordinated No Simult. Gap E/W On Yellow 4.0 4.0 4.0 4.0 4.0 0.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 5 2 6 8 1 3 7 4 Case Number 2.0 3.0 2.0 3.0 2.0 3.0 2.0 3.0 Phase Duration, s 41.8 11.5 44.8 10.9 26.9 8.5 9.8 25.8 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 3.1 0.0 3.1 0.0 3.1 3.1 3.1 3.1 Queue Clearance Time (g_s), s 4.7 7.8 7.2 19.1 6.4 13.6 Green Extension Time (g_e), s 0.4 0.0 0.2 0.0 0.2 3.9 0.0 4.0 Phase Call Probability 0.75 0.95 0.93 1.00 0.89 1.00 1.00 0.03 0.52 0.01 Max Out Probability 0.00 0.00 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 16 3 8 18 7 4 14 1 6 56 703 149 118 1258 137 107 734 124 90 526 193 Adjusted Flow Rate (v), veh/h Adjusted Saturation Flow Rate (s), veh/h/ln 1810 1809 1610 1810 1810 1809 1610 1810 1809 1610 1809 1610 2.7 12.6 5.8 26.2 5.2 17.1 5.6 8.7 Queue Service Time (g_s), s 4.6 4.0 4.4 11.6 Cycle Queue Clearance Time (g c), s 5.6 11.6 2.7 12.6 4.6 5.8 26.2 4.0 5.2 17.1 4.4 8.7 Green Ratio (g/C) 0.05 0.42 0.50 0.08 0.45 0.52 80.0 0.25 0.25 0.06 0.24 0.29 Capacity (c), veh/h 91 1518 799 151 1639 833 139 922 410 116 877 471 Volume-to-Capacity Ratio (X) 0.616 0.463 0.186 0.780 0.768 0.165 0.773 0.796 0.302 0.776 0.600 0.410 Back of Queue (Q), ft/ln (95 th percentile) 56.5 223.3 75 118.6 411.1 35.6 108.3 290.8 94.4 92.5 213.1 101.1 Back of Queue (Q), veh/ln (95 th percentile) 2.3 8.9 3.0 4.7 16.4 1.4 4.3 11.6 3.8 3.7 8.5 4.0 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 41.5 Uniform Delay (d 1), s/veh 41.9 18.8 12.6 40.4 20.6 1.2 40.8 31.3 27.1 30.2 1.4 Incremental Delay (d 2), s/veh 2.5 1.0 0.5 3.3 3.5 0.4 3.4 0.6 0.2 4.2 0.2 0.2 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 44.4 19.8 13.1 43.7 24.2 1.6 44.2 31.9 27.2 45.6 30.5 1.6 Level of Service (LOS) D В В D С Α D С С D С Α 20.2 С 23.6 С 32.7 С 25.3 С Approach Delay, s/veh / LOS Intersection Delay, s/veh / LOS 25.3 С **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.42 В 2.44 2.44 2.46 В В В Bicycle LOS Score / LOS 1.24 Α 1.74 1.28 Α 1.16 Α

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future - PM 1.00 **Urban Street** San Vicente / Beverly Analysis Year 2024 **Analysis Period** 1>7:00 File Name 06PM - Future.xus Intersection Intersection #6 **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R Demand (v), veh/h 75 953 108 88 893 145 152 765 452 228 522 135 Signal Information Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End Green 5.1 0.0 27.7 17.9 5.9 9.4 Uncoordinated No Simult. Gap E/W On Yellow 4.0 4.0 4.0 4.0 4.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 5 2 6 8 1 3 7 4 Case Number 2.0 3.0 2.0 3.0 2.0 3.0 2.0 3.0 Phase Duration, s 31.0 9.9 31.8 13.4 31.7 17.4 35.8 9.1 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 3.1 0.0 3.1 0.0 3.1 3.1 3.1 3.1 Queue Clearance Time (g_s), s 5.7 6.3 9.4 26.3 13.0 11.8 Green Extension Time (g_e), s 0.0 0.0 0.3 0.0 0.2 1.4 0.4 5.0 Phase Call Probability 0.85 0.89 0.98 1.00 1.00 1.00 1.00 1.00 0.00 0.05 Max Out Probability 1.00 0.00 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 1 16 3 8 18 7 4 14 6 75 953 108 88 893 145 152 765 452 228 522 Adjusted Flow Rate (v), veh/h 135 Adjusted Saturation Flow Rate (s), veh/h/ln 1810 1610 1810 1809 1610 1810 1610 1810 1809 1610 1809 1809 3.7 22.5 7.4 16.7 24.3 4.9 Queue Service Time (g_s), s 3.9 4.3 20.4 4.8 11.0 9.8 Cycle Queue Clearance Time (g c), s 3.7 22.5 3.9 4.3 20.4 4.8 7.4 16.7 24.3 11.0 9.8 4.9 Green Ratio (g/C) 0.06 0.30 0.40 0.07 0.31 0.46 0.10 0.31 0.31 0.15 0.35 0.41 Capacity (c), veh/h 102 1085 651 118 1117 737 189 1115 496 269 1276 659 Volume-to-Capacity Ratio (X) 0.734 0.878 0.166 0.745 0.799 0.197 0.806 0.686 0.911 0.846 0.409 0.205 Back of Queue (Q), ft/ln (95 th percentile) 76.9 406 28 102.8 358.9 80.4 151.3 286.4 365.9 215.2 180.1 77.6 Back of Queue (Q), veh/ln (95 th percentile) 3.1 16.2 1.1 4.1 14.4 3.2 6.1 11.5 14.6 8.6 7.2 3.1 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 41.8 29.9 4.4 41.3 28.5 14.5 39.4 27.3 3.4 37.3 22.0 17.1 Incremental Delay (d 2), s/veh 3.8 10.1 0.5 12.5 6.0 0.6 3.1 1.3 19.5 2.8 0.1 0.1 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 45.6 40.0 5.0 53.8 34.6 15.1 42.5 28.6 22.9 40.1 22.1 17.2 Level of Service (LOS) D D Α D С В D С С D С В 37.1 D 33.6 С 28.3 С 26.0 С Approach Delay, s/veh / LOS Intersection Delay, s/veh / LOS 31.4 С **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.46 В 2.43 2.43 В 2.43 В В Bicycle LOS Score / LOS 1.42 Α 1.42 Α 1.62 В 1.22

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future - AM 1.00 **Urban Street** La Cienega / Melrose Analysis Year 2024 **Analysis Period** 1>7:00 File Name 10AM - Future.xus Intersection Intersection #10 **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R L R L R Demand (v), veh/h 56 406 36 533 957 40 50 665 171 62 942 163 Signal Information ٨. Cycle, s 90.0 Reference Phase 2 542 Offset, s 0 Reference Point End 37.7 0.0 Green 22.8 17.5 0.0 0.0 Uncoordinated No Simult. Gap E/W On Yellow 4.0 0.0 0.0 0.0 4.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 2 6 8 1 4 Case Number 5.3 1.0 3.0 5.0 6.0 Phase Duration, s 26.8 48.3 41.7 41.7 21.5 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 0.0 3.1 0.0 3.2 3.2 Queue Clearance Time (g_s), s 21.8 32.2 24.4 Green Extension Time (g_e), s 0.0 1.0 0.0 5.6 5.9 Phase Call Probability 1.00 1.00 1.00 0.11 0.04 Max Out Probability 0.00 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 16 3 8 18 7 4 14 1 6 56 406 36 533 957 40 50 665 171 62 567 538 Adjusted Flow Rate (v), veh/h 596 1809 1610 1810 1809 518 1809 1610 783 1900 1802 Adjusted Saturation Flow Rate (s), veh/h/ln 7.5 11.8 6.2 22.3 22.4 Queue Service Time (g_s), s 9.1 1.7 19.8 16.4 8.0 5.5 22.3 Cycle Queue Clearance Time (g_c), s 7.7 9.1 1.7 19.8 16.4 30.2 11.8 6.2 17.3 22.4 Green Ratio (g/C) 0.19 0.19 0.19 0.47 0.49 0.42 0.42 0.42 0.42 0.42 0.42 670 Capacity (c), veh/h 196 711 317 632 1790 168 1506 304 791 750 Volume-to-Capacity Ratio (X) 0.285 0.571 0.114 0.844 0.535 0.298 0.442 0.255 0.204 0.717 0.718 Back of Queue (Q), ft/ln (95 th percentile) 56.2 189.4 31 326.6 266.4 44.7 206.3 99.4 45.1 360.9 346 Back of Queue (Q), veh/ln (95 th percentile) 2.2 7.6 1.2 13.1 10.7 1.8 8.3 4.0 1.8 14.4 13.8 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 32.2 32.7 29.7 19.2 15.6 34.4 18.8 17.2 24.9 21.9 21.9 Incremental Delay (d 2), s/veh 3.6 3.3 0.7 4.2 1.1 0.4 0.1 0.1 0.1 0.5 0.6 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 35.8 36.0 30.4 23.4 16.8 0.0 34.8 18.9 17.2 25.0 22.4 22.4 Level of Service (LOS) D D С С В Α С В В С С С 35.6 D В 19.4 В 22.6 С Approach Delay, s/veh / LOS 18.6 Intersection Delay, s/veh / LOS 22.0 С **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.45 В 2.26 2.42 2.42 В В В Bicycle LOS Score / LOS 0.90 Α 1.75 1.22 Α 1.45 Α

HCS7 Signalized Intersection Results Summary 1474767 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency JAS Analyst Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future - PM 1.00 **Urban Street** La Cienega / Melrose Analysis Year 2024 **Analysis Period** 1>7:00 10PM - Future.xus File Name Intersection Intersection #10 **Project Description** Our Lady of Mt. Lebanon Project **Demand Information** EB **WB** NB SB Approach Movement L R L R R L R Demand (v), veh/h 130 934 57 286 614 106 57 1119 361 68 935 118 Signal Information ٨. Cycle, s 90.0 Reference Phase 2 542 Offset, s 0 Reference Point End 37.8 0.0 Green 11.5 28.7 0.0 0.0 Uncoordinated No Simult. Gap E/W On Yellow 4.0 0.0 0.0 0.0 4.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL** WBT NBL **NBT** SBL SBT **Assigned Phase** 2 6 8 1 4 Case Number 5.3 1.0 3.0 5.0 6.0 Phase Duration, s 32.7 15.5 48.2 41.8 41.8 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 0.0 3.1 0.0 3.3 3.3 Queue Clearance Time (g_s), s 11.0 31.1 37.0 Green Extension Time (g_e), s 0.0 0.5 0.0 4.4 8.0 Phase Call Probability 1.00 1.00 1.00 0.77 1.00 Max Out Probability 0.00 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 16 3 8 18 7 4 14 1 6 130 934 57 286 614 106 57 1119 361 68 537 Adjusted Flow Rate (v), veh/h 516 821 1809 1610 1810 1809 544 1809 1610 511 1900 1825 Adjusted Saturation Flow Rate (s), veh/h/ln 21.3 2.2 8.5 23.4 15.1 Queue Service Time (g_s), s 11.5 9.0 9.4 11.6 20.6 20.6 2.2 29.1 Cycle Queue Clearance Time (g_c), s 11.5 21.3 9.0 9.4 23.4 15.1 35.0 20.6 20.6 Green Ratio (g/C) 0.32 0.32 0.32 0.47 0.49 0.42 0.42 0.42 0.42 0.42 0.42 514 Capacity (c), veh/h 342 1155 361 1777 184 1520 676 162 798 767 Volume-to-Capacity Ratio (X) 0.380 0.809 0.111 0.793 0.346 0.309 0.736 0.534 0.420 0.673 0.673 Back of Queue (Q), ft/ln (95 th percentile) 110.3 371.5 39.8 161.6 166 49.8 366 229.4 64.4 345.3 334.7 Back of Queue (Q), veh/ln (95 th percentile) 4.4 14.9 1.6 6.5 6.6 2.0 14.6 9.2 2.6 13.8 13.4 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 24.8 28.1 21.6 19.7 14.0 32.9 21.9 19.5 36.6 21.1 21.1 Incremental Delay (d 2), s/veh 3.2 6.1 0.4 1.5 0.5 0.4 1.7 0.4 0.6 1.8 1.9 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 Control Delay (d), s/veh 28.0 34.3 22.1 21.2 14.6 0.0 33.2 23.6 19.9 37.2 22.9 23.0 Level of Service (LOS) С С С С В Α С С В D С С 32.9 С 14.9 В 23.1 С 23.8 С Approach Delay, s/veh / LOS Intersection Delay, s/veh / LOS 23.8 С **Multimodal Results** ΕB WB NB Pedestrian LOS Score / LOS 2.43 В 2.26 2.42 2.42 В В В Bicycle LOS Score / LOS 1.41 Α 1.32 Α 1.76 В 1.41 Α

HCS7 Signalized Intersection Results Summary 1414141 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future with 1.00 Project - AM **Urban Street** Analysis Year 1> 7:00 San Vicente / Melrose 2024 **Analysis Period** File Name 04AM - Future + Project.xus Intersection Intersection #4 **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 93 521 44 270 794 179 71 628 108 81 467 55 Signal Information Cycle, s 90.0 Reference Phase 2 $\mathbb{S}12$ Offset, s 0 Reference Point End Green 52.9 0.0 0.0 0.0 29.1 0.0 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 0.0 0.0 0.0 0.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 2 6 8 4 Case Number 6.0 5.0 6.0 5.0 Phase Duration, s 56.9 56.9 33.1 33.1 Change Period, (Y+Rc), s 4.0 4.0 4.0 4.0 Max Allow Headway (MAH), s 0.0 0.0 3.3 3.3 Queue Clearance Time (g_s), s 17.1 26.5 Green Extension Time (g_e), s 0.0 0.0 3.4 2.6 Phase Call Probability 1.00 1.00 Max Out Probability 0.04 0.31 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R 5 2 12 3 18 7 4 14 **Assigned Movement** 1 6 16 8 Adjusted Flow Rate (v), veh/h 93 286 279 270 794 179 71 377 359 81 467 55 Adjusted Saturation Flow Rate (s), veh/h/ln 694 1900 1848 859 1900 1610 941 1900 1802 733 1809 1610 Queue Service Time (g_s), s 9.9 6.6 6.6 20.1 26.6 4.6 5.7 15.1 15.1 9.4 9.0 2.2 Cycle Queue Clearance Time (gc), s 36.6 6.6 6.6 26.7 26.6 4.6 14.7 15.1 15.1 24.5 9.0 2.2 Green Ratio (g/C) 0.59 0.59 0.59 0.59 0.59 0.59 0.32 0.32 0.32 0.32 0.32 0.32 282 1086 946 290 615 583 194 Capacity (c), veh/h 1117 521 1117 1170 521 Volume-to-Capacity Ratio (X) 0.616 0.330 0.256 0.257 0.518 0.711 0.189 0.244 0.614 0.417 0.399 0.106 Back of Queue (Q), ft/ln (95 th percentile) 81.7 117 114.6 184.1 412 70.6 56.9 269.5 259.1 75 167 35.6 Back of Queue (Q), veh/ln (95 th percentile) 3.3 4.7 4.6 7.4 16.5 2.8 2.3 10.8 10.4 3.0 6.7 1.4 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 26.1 9.0 9.0 15.5 13.1 8.6 29.3 25.7 25.7 36.0 23.7 21.3 Incremental Delay (d 2), s/veh 3.1 0.6 0.6 3.6 3.9 0.4 0.2 0.5 0.5 0.5 0.1 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 29.3 19.2 17.0 36.6 Control Delay (d), s/veh 9.6 9.6 9.1 29.5 26.2 26.2 23.7 21.4 Level of Service (LOS) С Α Α В В Α С С С D С С Approach Delay, s/veh / LOS 12.4 В 16.3 В С 25.2 С 26.5 Intersection Delay, s/veh / LOS 19.6 R **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.24 2.28 В 2.39 В В 2.11 В Bicycle LOS Score / LOS 1.03 Α 2.54 1.15 Α 0.99 Α

HCS7 Signalized Intersection Results Summary 1414141 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future with 1.00 Project - PM **Urban Street** Analysis Year 1> 7:00 San Vicente / Melrose 2024 **Analysis Period** File Name 04PM - Future + Project.xus Intersection Intersection #4 **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 110 646 83 157 456 223 89 736 177 116 531 115 Signal Information Cycle, s 90.0 Reference Phase 2 $\P A Z$ Offset, s 0 Reference Point End Green 43.3 38.7 0.0 0.0 0.0 0.0 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 0.0 0.0 0.0 0.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 2 6 8 4 Case Number 6.0 5.0 6.0 5.0 Phase Duration, s 47.3 47.3 42.7 42.7 Change Period, (Y+Rc), s 4.0 4.0 4.0 4.0 Max Allow Headway (MAH), s 0.0 0.0 3.4 3.4 Queue Clearance Time (g_s), s 19.0 34.7 Green Extension Time (g_e), s 0.0 0.0 5.1 4.0 Phase Call Probability 1.00 1.00 Max Out Probability 0.03 0.31 SB **Movement Group Results** ΕB WB NB Approach Movement L Т R L Т R L Т R L Т R 5 2 12 3 18 7 4 14 **Assigned Movement** 1 6 16 8 472 Adjusted Flow Rate (v), veh/h 110 372 357 157 456 223 89 441 116 531 115 Adjusted Saturation Flow Rate (s), veh/h/ln 950 1900 1824 738 1900 1610 887 1900 1772 621 1809 1610 Queue Service Time (g_s), s 8.0 11.3 11.4 15.7 14.7 7.5 6.7 17.0 17.0 15.7 8.8 4.0 Cycle Queue Clearance Time (gc), s 7.5 22.7 11.3 11.4 27.0 14.7 15.6 17.0 17.0 32.7 8.8 4.0 Green Ratio (g/C) 0.48 0.48 0.48 0.48 0.48 0.48 0.43 0.43 0.43 0.43 0.43 0.43 383 916 880 343 916 815 760 229 1551 690 Capacity (c), veh/h 777 373 Volume-to-Capacity Ratio (X) 0.287 0.405 0.406 0.458 0.498 0.287 0.239 0.580 0.580 0.507 0.342 0.167 Back of Queue (Q), ft/ln (95 th percentile) 87 212.6 206.7 135.3 263.1 123.3 61.2 286.4 270.9 103.9 157.1 62.6 Back of Queue (Q), veh/ln (95 th percentile) 3.5 8.5 8.3 5.4 10.5 4.9 2.4 11.5 10.8 4.2 6.3 2.5 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 23.6 15.0 15.0 23.7 15.9 14.0 22.4 19.5 19.5 32.0 17.2 15.8 Incremental Delay (d 2), s/veh 1.9 1.3 1.4 4.4 1.9 0.9 0.1 0.2 0.3 0.6 0.0 0.0 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 25.5 17.8 32.6 Control Delay (d), s/veh 16.3 16.4 28.1 14.9 22.5 19.8 19.8 17.3 15.9 Level of Service (LOS) С В В С В В С В В С В В 20.0 Approach Delay, s/veh / LOS 17.6 В 19.0 В С 19.4 В Intersection Delay, s/veh / LOS 19.0 R **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.26 2.26 В 2.41 В В 2.10 В Bicycle LOS Score / LOS 1.18 Α 1.87 В 1.31 Α 1.12 Α

HCS7 Signalized Intersection Results Summary 1414141 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future with 1.00 Project - AM **Urban Street** Analysis Year 1> 7:00 San Vicente / Beverly 2024 **Analysis Period** File Name 06AM - Future + Project.xus Intersection Intersection #6 **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 56 703 149 118 1258 137 107 737 124 90 527 193 Signal Information Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End Green 7.5 29.2 4.5 5.8 1.1 21.9 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 4.0 4.0 0.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 5 2 6 3 8 1 7 4 Case Number 2.0 3.0 2.0 3.0 2.0 3.0 2.0 3.0 Phase Duration, s 8.5 41.7 11.5 44.7 10.9 27.0 9.8 25.9 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 3.1 0.0 3.1 0.0 3.1 3.1 3.1 3.1 Queue Clearance Time (g_s), s 4.7 7.8 7.2 19.1 6.4 13.6 Green Extension Time (g_e), s 0.4 0.0 0.2 0.0 0.2 3.9 0.0 4.0 Phase Call Probability 0.75 0.95 0.93 1.00 0.89 1.00 Max Out Probability 1.00 0.00 0.00 0.03 0.52 0.01 **Movement Group Results** EB WB NB SB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 3 18 7 4 14 1 6 16 8 Adjusted Flow Rate (v), veh/h 56 703 149 118 1258 137 107 737 124 90 527 193 1810 1810 1809 1610 1810 1809 1610 1809 1610 1810 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 2.7 12.6 4.6 5.8 26.3 4.0 5.2 17.1 5.6 4.4 11.6 8.7 Cycle Queue Clearance Time (g c), s 2.7 12.6 4.6 5.8 26.3 4.0 17.1 5.6 4.4 11.6 5.2 8.7 Green Ratio (g/C) 0.05 0.42 0.50 0.08 0.45 0.52 80.0 0.26 0.26 0.06 0.24 0.29 91 1515 798 831 925 412 116 473 Capacity (c), veh/h 151 1636 139 880 Volume-to-Capacity Ratio (X) 0.616 0.464 0.187 0.780 0.769 0.165 0.773 0.797 0.301 0.776 0.599 0.408 Back of Queue (Q), ft/ln (95 th percentile) 56.5 223.7 75.2 118.6 411.8 35.8 108.3 291.4 94.2 92.5 213.7 100.9 Back of Queue (Q), veh/ln (95 th percentile) 2.3 8.9 3.0 4.7 16.5 1.4 4.3 11.7 3.8 3.7 8.5 4.0 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 41.5 Uniform Delay (d 1), s/veh 41.9 18.9 12.6 40.4 20.7 1.2 40.8 31.3 27.0 30.2 1.4 Incremental Delay (d 2), s/veh 2.5 1.0 0.5 3.3 3.5 0.4 3.4 0.6 0.2 4.2 0.2 0.2 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 44.4 43.7 24.2 44.2 45.6 Control Delay (d), s/veh 19.9 13.1 1.6 31.9 27.2 30.4 1.6 Level of Service (LOS) D В В D С Α D С С D С Α 20.3 С 23.7 С 32.7 С 25.2 С Approach Delay, s/veh / LOS Intersection Delay, s/veh / LOS 25.3 С **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.42 2.44 В 2.46 В В 2.44 В Bicycle LOS Score / LOS 1.24 Α 1.74 В 1.29 Α 1.16 Α

HCS7 Signalized Intersection Results Summary 1414141 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future with 1.00 Project - PM **Urban Street** Analysis Year 1> 7:00 San Vicente / Beverly 2024 **Analysis Period** File Name 06PM - Future + Project.xus Intersection Intersection #6 **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 75 953 108 88 893 145 152 767 452 228 525 135 Signal Information Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End Green 5.1 9.4 0.0 27.3 18.4 5.9 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 4.0 4.0 4.0 4.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 5 2 6 3 8 1 7 4 Case Number 2.0 3.0 2.0 3.0 2.0 3.0 2.0 3.0 Phase Duration, s 9.1 31.5 9.9 32.3 13.4 31.3 17.4 35.3 4.0 4.0 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s 4.0 Max Allow Headway (MAH), s 3.1 0.0 3.1 0.0 3.1 3.1 3.1 3.1 Queue Clearance Time (g_s), s 5.7 6.3 9.4 26.5 13.0 12.0 Green Extension Time (g_e), s 0.0 0.0 0.3 0.0 0.2 8.0 0.4 4.9 Phase Call Probability 0.85 0.89 0.98 1.00 1.00 1.00 Max Out Probability 1.00 1.00 0.00 1.00 0.00 0.06 **Movement Group Results** EB WB NB SB Approach Movement L Т R L Т R L Т R L Т R **Assigned Movement** 5 2 12 3 18 7 4 14 1 6 16 8 452 228 Adjusted Flow Rate (v), veh/h 75 953 108 88 893 145 152 767 525 135 1810 1809 1610 1810 1809 1610 1810 1809 1610 1810 1809 1610 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 3.7 22.4 3.8 4.3 20.2 4.8 7.4 16.9 24.5 11.0 10.0 4.9 Cycle Queue Clearance Time (g c), s 3.7 22.4 3.8 4.3 20.2 4.8 16.9 24.5 11.0 10.0 7.4 4.9 Green Ratio (g/C) 0.06 0.31 0.41 0.07 0.31 0.46 0.10 0.30 0.30 0.15 0.35 0.40 102 1104 659 745 1096 488 269 651 Capacity (c), veh/h 118 1136 188 1258 Volume-to-Capacity Ratio (X) 0.734 0.863 0.164 0.745 0.786 0.195 0.807 0.700 0.927 0.847 0.417 0.207 Back of Queue (Q), ft/ln (95 th percentile) 76.9 398.6 28.6 102.8 354.1 79.2 151.3 290.4 381.4 215.2 183.1 78.4 Back of Queue (Q), veh/ln (95 th percentile) 3.1 15.9 1.1 4.1 14.2 3.2 6.1 11.6 15.3 8.6 7.3 3.1 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 27.7 Uniform Delay (d 1), s/veh 41.8 29.5 4.2 41.3 28.1 14.3 39.4 3.4 37.3 22.4 17.4 Incremental Delay (d 2), s/veh 3.8 9.0 0.5 12.5 5.5 0.6 3.1 1.6 23.0 2.8 0.1 0.1 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 45.6 42.5 40.1 Control Delay (d), s/veh 38.5 4.7 53.8 33.6 14.9 29.4 26.4 22.5 17.5 Level of Service (LOS) D D D С В D C С D С В Α D 32.8 С 29.8 С 26.3 С Approach Delay, s/veh / LOS 35.7 Intersection Delay, s/veh / LOS 31.4 С **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.46 2.43 В 2.43 В В 2.43 В Bicycle LOS Score / LOS 1.42 Α 1.42 Α 1.62 В 1.22 Α

HCS7 Signalized Intersection Results Summary 14747 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future with 1.00 Project - AM **Urban Street** La Cienega / Melrose Analysis Year 1> 7:00 2024 **Analysis Period** File Name 10AM - Future + Project.xus Intersection Intersection #10 **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 56 406 36 533 957 40 50 668 171 62 943 163 Signal Information Cycle, s 90.0 Reference Phase 2 Offset, s 0 Reference Point End Green 22.8 37.7 0.0 0.0 17.5 0.0 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 4.0 0.0 0.0 0.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 2 6 8 4 1 Case Number 5.3 1.0 3.0 5.0 6.0 Phase Duration, s 21.5 26.8 48.3 41.7 41.7 4.0 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s Max Allow Headway (MAH), s 0.0 3.1 0.0 3.2 3.2 Queue Clearance Time (g_s), s 21.8 32.2 24.4 Green Extension Time (g_e), s 0.0 1.0 0.0 5.6 6.0 Phase Call Probability 1.00 1.00 1.00 Max Out Probability 0.00 0.11 0.04 **Movement Group Results** ΕB WB NB SB Approach Movement L Т R L Т R L Т R L Т R 5 2 12 3 18 7 4 14 **Assigned Movement** 1 6 16 8 62 Adjusted Flow Rate (v), veh/h 56 406 36 533 957 40 50 668 171 567 539 596 1809 1610 1810 1809 518 1809 1610 781 1900 1802 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 7.5 9.1 1.7 19.8 16.4 8.0 11.9 6.2 5.5 22.4 22.4 Cycle Queue Clearance Time (gc), s 7.7 19.8 16.4 30.2 11.9 6.2 17.3 22.4 9.1 1.7 22.4 Green Ratio (g/C) 0.19 0.19 0.19 0.47 0.49 0.42 0.42 0.42 0.42 0.42 0.42 196 709 631 1789 1507 303 Capacity (c), veh/h 316 168 671 792 751 Volume-to-Capacity Ratio (X) 0.286 0.572 0.114 0.844 0.535 0.298 0.443 0.255 0.205 0.717 0.718 Back of Queue (Q), ft/ln (95 th percentile) 56.3 189.5 31 326.8 266.4 44.7 207.1 99.4 45.1 361.2 346.3 Back of Queue (Q), veh/ln (95 th percentile) 2.3 7.6 1.2 13.1 10.7 1.8 8.3 4.0 1.8 14.4 13.9 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 32.2 32.8 29.7 19.2 15.6 34.4 18.8 17.1 24.9 21.8 21.8 Incremental Delay (d 2), s/veh 3.6 3.3 0.7 4.2 1.2 0.4 0.1 0.1 0.1 0.5 0.6 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 35.9 Control Delay (d), s/veh 36.1 30.5 23.4 16.8 0.0 34.7 18.9 17.2 25.1 22.4 22.4 Level of Service (LOS) D D С С В С В В С С Α С Approach Delay, s/veh / LOS D 18.7 В В 22.5 С 35.7 19.4 Intersection Delay, s/veh / LOS 22.0 С **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.45 2.42 В 2.26 В В 2.42 В Bicycle LOS Score / LOS 0.90 Α 1.75 В 1.22 Α 1.45 Α

HCS7 Signalized Intersection Results Summary 14747 **General Information Intersection Information** LLG Engineers Duration, h 0.25 Agency Analyst JAS Analysis Date Mar 11, 2019 Area Type Other PHF Jurisdiction City of West Hollywood Time Period Future with 1.00 Project - PM **Urban Street** La Cienega / Melrose Analysis Year 1> 7:00 2024 **Analysis Period** File Name 10PM - Future + Project.xus Intersection Intersection #10 **Project Description** Our Lady of Mt. Lebanon Project EΒ WB NB SB **Demand Information** Approach Movement L R L R L R L R Demand (v), veh/h 130 934 57 286 614 106 57 1121 361 68 938 118 Signal Information ٨. Cycle, s 90.0 Reference Phase 2 $\mathbb{S} \mathbb{A} \mathbb{Z}$ Offset, s 0 Reference Point End Green 11.5 28.7 37.8 0.0 0.0 0.0 Uncoordinated No Simult, Gap E/W On Yellow 4.0 4.0 4.0 0.0 0.0 0.0 Force Mode Fixed Simult. Gap N/S On Red 0.0 0.0 0.0 0.0 0.0 0.0 **Timer Results EBL EBT WBL WBT NBL NBT** SBL SBT **Assigned Phase** 2 6 8 4 1 Case Number 5.3 1.0 3.0 5.0 6.0 Phase Duration, s 32.7 15.5 48.2 41.8 41.8 4.0 4.0 4.0 4.0 Change Period, (Y+Rc), s 4.0 Max Allow Headway (MAH), s 0.0 3.1 0.0 3.3 3.3 Queue Clearance Time (g_s), s 11.0 31.2 37.0 Green Extension Time (g_e), s 0.0 0.5 0.0 4.4 8.0 Phase Call Probability 1.00 1.00 1.00 Max Out Probability 0.00 0.77 1.00 **Movement Group Results** ΕB WB NB SB Approach Movement L Т R L Т R L Т R L Т R 5 2 12 3 7 4 **Assigned Movement** 1 6 16 8 18 14 Adjusted Flow Rate (v), veh/h 130 934 57 286 614 106 57 1121 361 68 539 517 821 1809 1610 1810 1809 543 1809 1610 510 1900 1825 Adjusted Saturation Flow Rate (s), veh/h/ln Queue Service Time (g_s), s 11.5 21.3 2.2 9.0 9.4 8.5 23.4 15.1 11.6 20.6 20.6 Cycle Queue Clearance Time (g c), s 11.5 21.3 2.2 9.0 9.4 29.2 23.4 15.1 35.0 20.6 20.6 Green Ratio (g/C) 0.32 0.32 0.32 0.47 0.49 0.42 0.42 0.42 0.42 0.42 0.42 342 1154 514 360 184 162 Capacity (c), veh/h 1776 1520 677 798 767 Volume-to-Capacity Ratio (X) 0.380 0.809 0.111 0.794 0.346 0.310 0.737 0.533 0.421 0.674 0.675 Back of Queue (Q), ft/ln (95 th percentile) 110.3 371.6 39.8 161.6 166 49.9 367.1 229.3 64.5 346.8 336.1 Back of Queue (Q), veh/ln (95 th percentile) 4.4 14.9 1.6 6.5 6.6 2.0 14.7 9.2 2.6 13.9 13.4 Queue Storage Ratio (RQ) (95 th percentile) 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 Uniform Delay (d 1), s/veh 24.8 28.1 21.6 19.7 14.0 32.9 21.9 19.5 36.6 21.1 21.1 Incremental Delay (d 2), s/veh 3.2 6.2 0.4 1.5 0.5 0.4 1.7 0.4 0.6 1.8 1.9 Initial Queue Delay (d 3), s/veh 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 21.2 37.3 Control Delay (d), s/veh 28.0 34.3 22.1 14.6 0.0 33.3 23.6 19.9 22.9 23.0 Level of Service (LOS) С С С С В С C В D С С Α 23.1 Approach Delay, s/veh / LOS С 14.9 В С 23.8 С 33.0 Intersection Delay, s/veh / LOS 23.9 С **Multimodal Results** FB WB NB SB Pedestrian LOS Score / LOS 2.43 2.42 В 2.26 В В 2.42 В Bicycle LOS Score / LOS 1.41 Α 1.32 Α 1.76 В 1.41 Α

	Appendix E
	APPENDIX E
	TRAFFIC STUDY MEMORANDUM OF UNDERSTANDING
LINSCOTT, LAW & GREENSPAN, engineers	LLG Ref. 5-17-0315-1 Our Lady of Mt. Lebanon Project

Transportation Impact Study Memorandum of Understanding (MOU)

This MOU acknowledges that the Transportation Impact Study for the following Project will be prepared in accordance with the latest version of LADOT's Transportation Impact Study Guidelines:

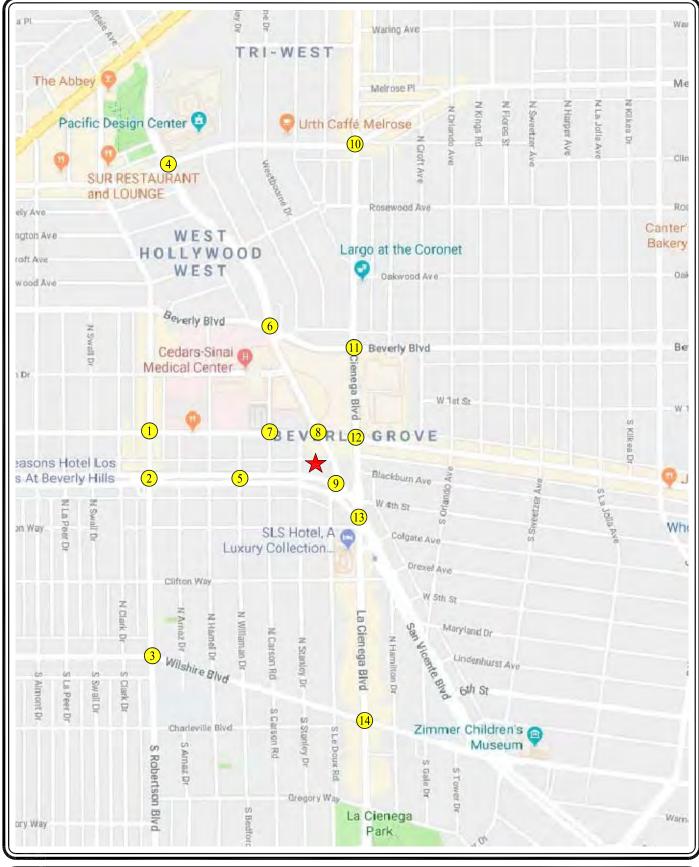
I. PROJECT	INFORMATION				
Project Name:	Mt. Lebanon Mixed-				
Project Address:	333. S. San Vicente				
Project Description:	Development of 153			its and 30,800) square feet
	of church floor area	(11,582 square feet	net new).		
LADOT Project Case Nu	mber:				
Project Site Plan [Figure		ired) x Yes	No		
,		<i>'</i>	_		
II. TRIP GENE	ERATION				
Geographic Distribution:	N 25%		<u>25% </u>	E <u>25%</u>	W <u>25%</u>
Illustration of Project trip Study intersections [Figu			No		
Olday intersections [r iga	ie i-ij allacheu: (itel		_110		
Trip Generation Adjust	ments (Exact amount	of credit subject to	approval by L	ADOT)	
		Yes N	lo		
Transit Usage		x			
_	Managament		_		
Transportation Demand	•	2	K		
Existing Active Land Use	;	X			
Previous Land Use		2	K		
Internal Trip		2	K		
Pass-by Trip		3	K		
0	! D-4-/-\2	ITE 40th E-liti	O41		
Source of Trip Generat	ion Rate(s)?	x ITE 10th Edition	_Other:		
Trip generation table [Ta	ble 7-1] including a de	escription of the pro	posed land us	es, ITE rates,	
estimated morning and a					C.
attached? (Required)			<u>x</u> Yes	No	
	In Out	Total			
AM Trips	<u>In</u> <u>Out</u> 16 47	<u>Total</u> 63			
PM Trips	49 30	79			
·					
	EA AND ASSUMP				
Project Buildout Year:	2023	Ambient or CN	MP Growth Ra	te: <u>1.0</u>	% Per Yr.
Related Projects List [Ta	hle 6-11 researched h	w the consultant			
and approved by LADOT			x Yes	No	
,		•	*Forthco	ming	
Subject to Freeway Impa				x No	olioo
(Freeway analysis screen that at least one criteria v		iust be included in t	riis iviou, seie	cuing yes imp	JIIES
*No freeway mainlines a		roject vicinity.			
•					
Map of Study Intersection			x Yes	No	
(May be subject to LADC	T revision after initial	impact analysis)			
Is this Project located on	a street within the Hig	ah Injury Network?	Yes	x No	

IV.	CONTACT INFORMATION		
	<u>Consultant</u>		Developer
Name	Linscott, Law & Greenspan, Engineers	Name	Successor Trustee of Our Lady of
Address	20931 Burbank Boulevard, Suite C		Mt. Lebanon - St. Peter Maronite
	Woodland Hills, CA 91367		Catholic Cathedral - Los Angeles
Phone No.	818.835.8648		Real Estate Trust
E-Mail	jshender@llgengineers.com	Address	333 S. San Vicente Boulevard
			Los Angeles, CA 90048
		Phone No.	310.275.6634
		E-Mail	bishop@eparchy.org
Approved I	by: 5/9/20 Consultant's Representative Date	18	211/18 LADOT's Representative Date

Study Intersections

CEN18-47891

- 1. Roberston Boulevard / 3rd Street
- 2. Robertson Boulevard / Burton Way (City of Los Angeles / City of Beverly Hills)
- 3. Robertson Boulevard / Wilshire Boulevard (City of Beverly Hills)
- 4. San Vicente Boulevard / Melrose Avenue (City of West Hollywood)
- 5. Willaman Drive / Burton Way
- 6. San Vicente Boulevard / Beverly Boulevard (City of Los Angeles / City of West Hollywood)
- 7. Sherbourne Drive / 3rd Street
- 8. San Vicente Boulevard / 3rd Street
- 9. San Vicente Boulevard / Burton Way
- 10. La Cienega Boulevard / Melrose Avenue (City of West Hollywood)
- 11. La Cienega Boulevard / Beverly Boulevard
- 12. La Cienega Boulevard / 3rd Street
- 13. La Cienega Boulevard / San Vicente Boulevard (City of Los Angeles / City of Beverly Hills)
- 14. La Cienega Boulevard / Wilshire Boulevard (City of Beverly Hills)





MAP SOURCE: GOOGLE MAPS

★ PROJECT SITE

STUDY INTERSECTION

FIGURE 1-1 VICINITY MAP

LINSCOTT, LAW & GREENSPAN, engineers

MT. LEBANON MIXED-USE PROJECT

o:\0315\dwg\f1-1.dwg 05/09/2018 14:46:20 jshender llg exhibits color.ctb



FIGURE 2-1
PROJECT SITE PLAN
GROUND FLOOR PLAN

MT. LEBANON MIXED-USE PROJECT

MAP SOURCE: NADEL ARCHITECTURE + PLANNING

NOT TO SCALE

LINSCOTT, LAW & GREENSPAN, engineers

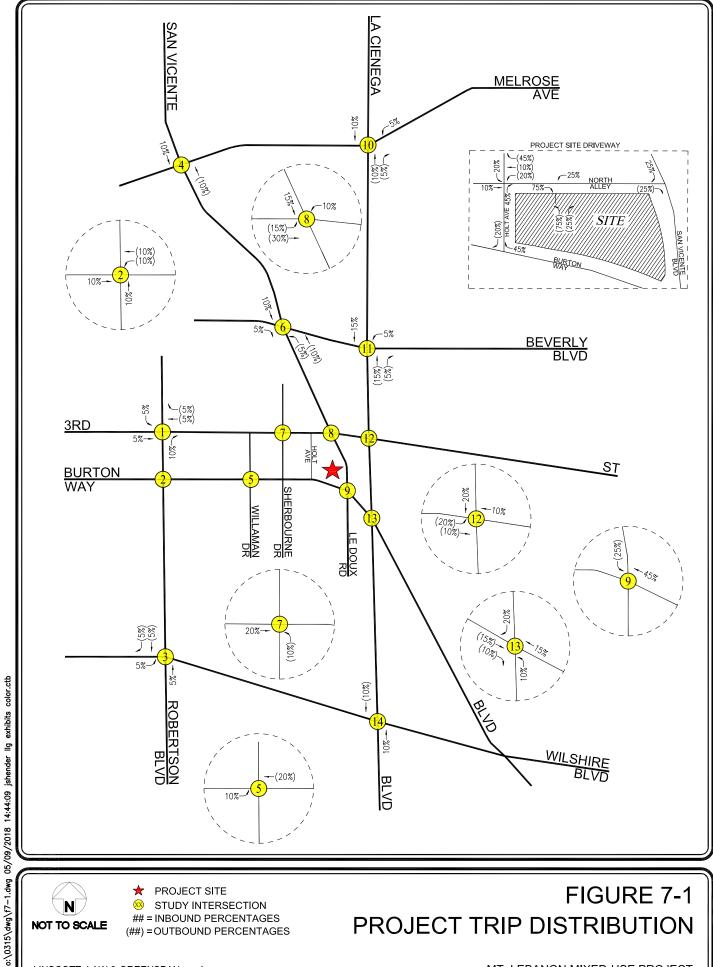
Table 7-1 PROJECT TRIP GENERATION [1]

09-May-18

		DAILY TRIP ENDS [2]	AM PEAK HOUR VOLUMES [2]			PM PEAK HOUR VOLUMES [2]		
LAND USE	SIZE	VOLUMES	IN	OUT	TOTAL	IN	OUT	TOTAL
Proposed Project								
Apartments [3]	153 DU	1,120	16	54	70	54	32	86
Church [4]	30,800 GSF	214	<u>6</u>	4	<u>10</u>	7	8	<u>15</u>
Subtotal	,	1,334	22	58	80	61	40	101
Transit Trips [5]								
Apartments (15%)		(168)	(2)	(8)	(10)	(8)	(5)	(13)
Church (15%)		(32)	(1)	(1)	(2)	(1)	(1)	(2)
Subtotal		(200)	(3)	(9)	(12)	(9)	(6)	(15)
Subtotal Project Driveway Trips		1,134	19	49	68	52	34	86
Existing Site								
Church [4]	(19,218) GSF	(134)	(4)	(2)	(6)	(4)	(5)	(9)
Transit Trips [5]								
Church (15%)		20	1	0	1	1	1	2
Subtotal Existing Driveway Trips		(114)	(3)	(2)	(5)	(3)	(4)	(7)
NET INCREASE DRIVEWAY TRIPS		1,020	16	47	63	49	30	79

- [1] Source: ITE "Trip Generation", 10th Edition, 2017.
- [2] Trips are one-way traffic movements, entering or leaving.
- [3] ITE Land Use Code 220 (Apartment) trip generation average rates.
 - Daily Trip Rate: 7.32 trips/dwelling unit; 50% inbound/50% outbound
 - AM Peak Hour Trip Rate: 0.46 trips/dwelling unit; 23% inbound/77% outbound
 - PM Peak Hour Trip Rate: 0.56 trips/dwelling unit; 63% inbound/37% outbound
- [4] ITE Land Use Code 560 (Church) trip generation average rates.
 - Daily Trip Rate: 6.95 trips/1,000 SF of floor area; 50% inbound/50% outbound
 - AM Peak Hour Trip Rate: 0.33 trips/1,000 SF of floor area; 60% inbound/40% outbound
 - PM Peak Hour Trip Rate: 0.49 trips/1,000 SF of floor area; 45% inbound/55% outbound
- [5] The Project site is located within 1/4 mile of a Metro Rapid bus stop. The trip reduction for transit trips has been applied to all components of the project based on the "LADOT Transportation Impact Study

Guidelines", December 2016 for developments within a 1/4 mile walking distance of a transit station or a RapidBus stop.



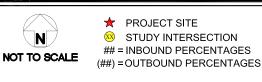
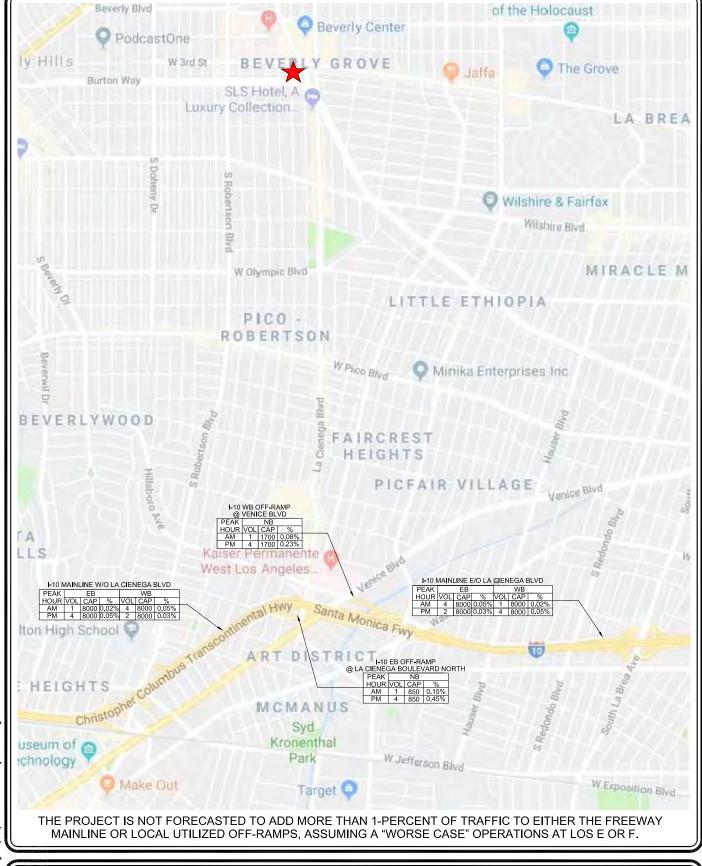


FIGURE 7-1 PROJECT TRIP DISTRIBUTION

MT. LEBANON MIXED-USE PROJECT LINSCOTT, LAW & GREENSPAN, engineers





MAP SOURCE: GOOGLE MAPS

★ PROJECT SITE

PROJECT FREEWAY MAINLINE AND FREEWAY TRAFFIC VOLUMES

LINSCOTT, LAW & GREENSPAN, engineers

MT. LEBANON MIXED-USE PROJECT

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