

## **Appendix I2     Hydrology Study**

## Appendices

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Concept approved as submitted

# CONCEPTUAL HYDROLOGY STUDY

## LAGUNA NIGUEL CITY CENTER

Crown Valley Parkway & Alicia Parkway  
Laguna Niguel, CA

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## 1.0 INTRODUCTION

### 1.1 GEOGRAPHIC SETTING

The project area consists of 24.4 gross acres (23.3 acres net) and is located in the City of Laguna Niguel. The site is bounded by Pacific Island Drive on the north, Alica Parkway to the northeast, Laguna Niguel City Hall on the east (westerly corner of Crown Valley Parkway and Alicia Parkway), Crown Valley Parkway on the southeast, and townhomes, at the top of a manufactured slope, on the southwest and northwest. The County of Orange has a fire station on the north boundary of the project, fronting Pacific Island Drive, that is not a part of the project. The site's current access points on Crown Valley Parkway and Alicia Parkway are the two access points for Laguna Niguel City Hall.. The City Hall parcel is not a part of the project. The current building on site that will be demolished is a county courthouse and sheriff vehicle maintenance facility. There are currently two northern access points to the project site from Pacific Island Drive, which are shared with the fire station.

The existing site has various uses spread over the area. The existing site has various uses spread over the area. A city library is located on the south edge against Crown Valley Parkway; an Orange County Sheriff facility is on the northwest edge fronting Pacific Island Drive; a County Courthouse and various service facilities and parking lots are scattered over the site. These facilities are planned to be demolished to allow room for the proposed development.

### 1.2 PURPOSE OF THIS REPORT

The purpose of this report is to accomplish the following objectives:

To determine pre-developed and developed storm water discharges generated within the project area for determination of design feasibility, constructability and impact on existing facilities. (See Hydrology Studies in Appendices 1 and 2).

To demonstrate that the "storm water" and "flood" protection goals as outlined in Addendum No. 1 to the O.C. Design Manual can be met. See Appendix 3.

To establish that there are no significant impacts to the surrounding facilities and properties as a result of this development.

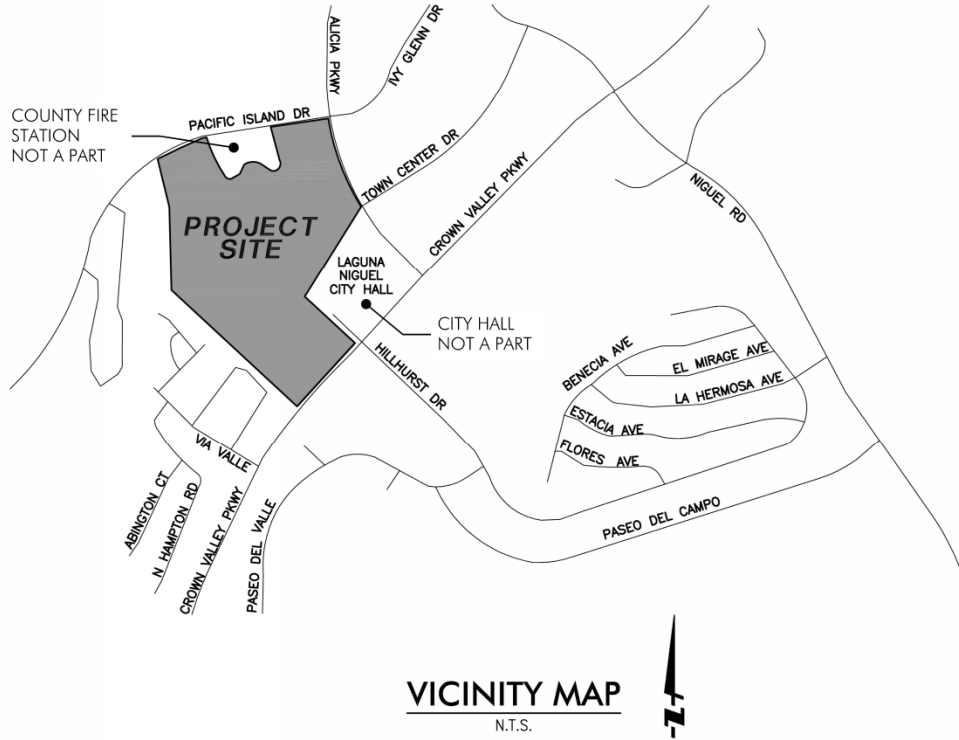
To determine site detention requirements, if any, for the project.

To size storm water inlet/outlet and conveyance facilities to support the project.

### 1.3 REFERENCES

- Orange County Hydrology Manual
- Orange County Local Drainage Manual
- City of Laguna Niguel Master Plan of Drainage
- Federal Emergency Management Agency (FEMA) (flood plain determination)

### 1.4 PROJECT SITE LOCATION MAP



## **2.0 EXISTING TOPOGRAPHIC & HYDROLOGIC CONDITIONS**

### **2.1 EXISTING TOPOGRAPHY**

The existing topography of the project site is very steep, dropping approximately 48-feet from the most northwest corner to the entry at Crown Valley Parkway. This results in an existing average slope of approximately 4.8 percent (0.048). The west side of the site is bounded by existing 2:1 manufactured slopes and there are manufactured 2:1 slopes on the easterly side dropping to Alicia Parkway. The site consists of rough brush covered terrain.

### **2.2 EXISTING DRAINAGE PATTERN**

The project site generally drains to the south. There are various inlets throughout the site that partially drain the slope on the west, the parking lots, and various minor facilities. The majority of these facilities drain to the existing public 60-inch storm drain discussed in section 2.3 below. These drainage systems will be removed during demolition of the site. A new drainage system will be designed to serve the proposed development.

### **2.3 EXISTING STORM DRAIN FACILITIES**

An existing public 60-inch diameter city storm drain winds through the site from Pacific Island Drive on the north to Crown Valley Parkway on the south. This facility will be realigned within the proposed development's roadways to make room for the proposed buildings. The storm drain size will remain the same and connect to the existing system on the north and south. There are inconsistencies in the record storm drain plans showing variable pipe diameters in the main line, flow tables that list the pipe as "full" but the listed velocities are too fast to support full flow at the Q given, and some other issues. Since the entire reach through the project is being replaced, new supporting calculations will be provided in the final hydrology/hydraulics report for this reach. See Appendix 4 for existing storm drain plans and the proposed hydrology map in Appendix 6 for the proposed storm drain alignment.

### 3.0 PROPOSED STORM DRAIN FACILITIES

The development will remove the existing public 60-inch RCP city storm drain discussed in Section 2.2 and 2.3 and install a new public 60" RCP city storm drain realigned to follow the alignment of the proposed private roadways. (See the proposed hydrology map in appendix 6 for the proposed storm drain alignment) The new alignment will connect to the existing 60-inch city storm drain at the intersection of Pacific Island Drive and Highlands Avenue, follow Pacific Island Drive easterly to the west entry of the development off Pacific Island Drive, follow the westerly alignment of the private roadway loop and cross the parking lot of the retail/market center on the south side of the project and reconnect to the existing 60-inch storm drain system just north of the north right of way of Crown Valley Parkway. This primary storm drain will convey flows originating from development north of the site (draining down Highlands Ave) through the site to the connection point at Crown Valley. These flows will bypass the development through this pipe and not contribute any tributary flow.

A secondary, private storm drain system will be constructed with the project roadways and convey the project flows through a detention system designed for hydromodification purposes. This detention system is proposed to be located under the parking lot of the retail/market area located on the south side of the project (where the current library is located). The detention basin will be sized and fully calculated in the final hydrology and hydraulics report.

Various area drains and water quality BMP's will be used throughout the site to route storm water to the private storm drain system. It is anticipated that these local drainage facilities will be in the 8-inch to 10-inch pipe diameter range. Small landscape drains will connect to the local drain with 4-inch or 6-inch drain pipes throughout the project.

The very easterly side of the proposed apartments located on the east side of the project will discharge to the existing landscape area above the slope and then be conveyed via pipe to a parkway culvert. Flow will not be allowed over the top of the slope. The volume and flow rate is anticipated to be less than the existing condition due to a much smaller drainage area. The majority of the easterly proposed apartments will convey flow to the private storm drain system in the project roadway.

The proposed apartments located in the northwest corner of the site will also convey flows to the private storm drain system.

The apartments site will have water quality BMP's to treat low flows before entering the private storm drain system - likely a Modular Wetland-type product. These will be fully discussed in the project's WQMP.

The retail area adjacent to Crown Valley Parkway on the south side of the project will drain overland, through water quality BMP's and convey flows via connection pipes to the detention system under the parking lot of that area. Final sizing of detention facility will be addressed in the final hydrology report. BMP sizing will be addressed in the final WQMP.



## 4.0 HYDROMODIFICATION

All Planned Development Projects (PDPs) must ensure that post-project runoff flow rates and durations for the PDP shall not exceed pre-development, naturally occurring, runoff flow rates and durations by more than 10% of the time, from 10% of the 2-year runoff event up to the 10-year runoff event. This project is subject to hydromodification requirements since the downstream storm drain facilities are not hardened and improved. A large detention area had been placed under the parking lot in the south retail area for this purpose. This detention system and its outlet control will regulate the outflow to pre-development flow rates. This system will be fully designed and calculated and included within the final hydrology report using the South Orange County Hydrology Model (SOHM).

## 5.0 Design Criteria

The proposed area drain system(s) will be designed to be consistent with the following goals and guidelines as presented in the Orange County Hydrology and the Orange County Local Drainage Manuals.

All habitable buildings shall be protected from flooding during a 100-year frequency storm. This site is in flood zone 'X' per Federal Emergency Management Agency (FEMA) maps 06059 C 0438K and 06059 C 0439J and flooding is not considered an issue on this site. Per FEMA definitions, Zone X is the area determined to be outside the 500-year flood and protected by levee from a 100-year flood.

Onsite storm drains are sized based on a 25-year frequency for overflow conditions outside the overall building envelope and 100-year frequency for areas within the enclosed proposed apartment courtyards, which are in sump conditions. Local area drains and drainage pipes (landscape applications) will be designed for a 10-year event. Events exceeding the 10-year event will flow overland in landscape areas to larger catchment devices. Catch basin sizing will be calculated in the final hydrology & hydraulics report.

Recommended design water surface elevations inside area drains shall be 0.5' below inlet grate elevation when possible. This ensures critical flow is achieved at drain inlets.

Pipe size may not be decreased downstream without the City's approval.

Branching of flow is not allowed.

Area drains and appurtenant piping shall be designed in conformance with the Orange County Hydraulics manual.

## 6.0 HYDROLOGY

### 6.1 STORM FREQUENCY

The storm frequency used for the storm drain design is the 25-year event. Peak runoff values for the 50 and 100-year events have also been calculated. This study indicates that these larger events will involve combined street and storm drain flow. The steepness of the site results in fast, but shallow flow depths.

### 6.2 METHODOLOGY

This study was prepared in conformance with the Orange County Hydrology Manual. The Rational Method was used for calculating the peak runoff. AES software was used to determine the proposed storm runoff and the small area unit hydrograph module of the same software was used to determine the detention requirements. See Appendices 2 and 3 for calculations.

The hydrology maps for the existing and proposed conditions are located in Appendices 5 and 6 respectively. A map showing the ponding analysis for 100-year event for the site is included in Appendix 6 (will be included within the final hydrology report).

The results using the 25-year rational method hydrology provide:

#### Existing Hydrology Area Summary for the 25-year storm event

Area ID	Flow (cfs)	Notes
A (103)	9	
B (203)	4	
C (305)	10	Areas A, B & C confluence at node 305. $Q_{25} = 23$ cfs
D (410)	573	Includes 485 cfs of upstream tributary area
TOTAL	596	Sum of nodes 305 & 410. Includes 485 cfs from 190 acres of upstream tributary area. Net existing flow = 596cfs-485cfs=111cfs

#### Proposed Hydrology Area Summary for the 25-year storm event

Area(s) ID	Flow (cfs)	Notes
A,	3	X
B	6	
C	15	
D	13	
E	42	
O	531	Includes 485 cfs of upstream tributary area
TOTAL	610	Sum of nodes 305 & 410. Includes 485 cfs from 190 acres of upstream tributary area. Net proposed flow = 610cfs-485cfs=125cfs

## 7.0 RESULTS AND CONCLUSIONS

### 7.1 SUMMARY OF EXISTING FLOWS, 10 THROUGH 100 YEAR EVENT

#### Existing Conditions

Area ID (Node)	Area (Acres)	Flow (cfs)	Notes
A (103)	2.5	Q <sub>10</sub> = 7 Q <sub>25</sub> = 9 Q <sub>100</sub> = 11	X
B (203)	1.4	Q <sub>10</sub> = 4 Q <sub>25</sub> = 4 Q <sub>100</sub> = 6	X
C (305)	3.2	Q <sub>10</sub> = 8 Q <sub>25</sub> = 10 Q <sub>100</sub> = 13	X
D (410)	24.0	Q <sub>10</sub> = 476 Q <sub>25</sub> = 573 Q <sub>100</sub> = 742	Includes upstream tributary flow in 60-inch SD pipe.
Total	31.1		

#### Proposed Conditions

Area ID	Area (Acres)	Flow (cfs)	Notes
A (103)	0.7	Q <sub>10</sub> = 2 Q <sub>25</sub> = 3 Q <sub>100</sub> = 4	
B (203)	1.1	Q <sub>10</sub> = 5 Q <sub>25</sub> = 6 Q <sub>100</sub> = 8	
C (305)	5.0	Q <sub>10</sub> = 12 Q <sub>25</sub> = 15 Q <sub>100</sub> = 20	
D (503)	3.3	Q <sub>10</sub> = 11 Q <sub>25</sub> = 13 Q <sub>100</sub> = 17	
E (605)	13.0	Q <sub>10</sub> = 35 Q <sub>25</sub> = 42 Q <sub>100</sub> = 54	
O (410)	8.0	Q <sub>10</sub> = 441 Q <sub>25</sub> = 531 Q <sub>100</sub> = 689	Includes upstream tributary flow in 60-inch SD pipe
Total	31.1		

## 7.2 CONCLUSIONS

The analysis provided in this report provides the following conclusions:

1. The project is feasible from a drainage standpoint and will have less than significant impact on the existing storm drain infrastructure. See discussion in section 3.0 for discussions of drainage facilities and project impacts.
2. Calculations in this report indicate that the adjacent public storm drain facilities will not be adversely affected by this development. Downstream impacts will be mitigated by the proposed detention system for both hydromodification and stormwater detention. The final hydrology & hydraulics report will contain detailed calculations.

These results indicate that the proposed project can be constructed in a manner that minimizes the impact of the proposed storm flow to the existing surrounding areas and neighborhood while providing safe and adequate drainage operation for the proposed project.

Catch basin sizing and hydraulic calculations will be derived for each drainage area serviced by an area drain and area drain pipe for the cumulative storm flows. Hydraulics from the sumps (apartment courtyard areas) will be based on the 100-year storm event for hydrostatic drainage via the courtyard storm drain system and a 10-year storm event for all others that have an overland overflow capability.

## 8.0 APPENDICES

- Appendix 1 10, 25 & 100-YEAR HYDROLOGY STUDIES, EXISTING
- Appendix 2 10, 25 & 100-YEAR HYDROLOGY STUDIES, PROPOSED
- Appendix 3 HYDRAULIC CALCULATIONS
- Appendix 4 SUPPORTING TABLES AND CHARTS
  - A. Firm Map
  - B. Soils Map
  - C. Master SD Plan excerpts
- Appendix 5 Existing Condition Hydrology Map (In Pocket)
- Appendix 6 Proposed Condition Hydrology Map (In Pocket)

APPENDIX 1  
10, 25, & 100 YEAR  
EXISTING  
CONDITIONS  
STUDIES

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
(c) Copyright 1983-2016 Advanced Engineering Software (aes)  
Ver. 23.0 Release Date: 07/01/2016 License ID 1355

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* LAGUNA NIGUEL TOWN CENTER \*  
\* EXISTING CONDITONS \*  
\* 10-YEAR STORM EVENT \*  
\*\*\*\*\*

FILE NAME: XLNTC10.DAT  
TIME/DATE OF STUDY: 20:51 09/24/2019

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT (YEAR) = 10.00  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 6.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/ SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
  2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
- \*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 330.00  
ELEVATION DATA: UPSTREAM (FEET) = 368.00 DOWNSTREAM (FEET) = 356.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 6.000  
\* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.657  
SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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COMMERCIAL D 1.46 0.20 0.100 75 6.00  
 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100  
 SUBAREA RUNOFF(CFS) = 4.78  
 TOTAL AREA(ACRES) = 1.46 PEAK FLOW RATE(CFS) = 4.78

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 356.00 DOWNSTREAM ELEVATION(FEET) = 347.00  
 STREET LENGTH(FEET) = 178.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 20.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.010  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.010

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.24  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.26  
 HALFSTREET FLOOD WIDTH(FEET) = 12.27  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.54  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.93  
 STREET FLOW TRAVEL TIME(MIN.) = 0.84  $T_c$ (MIN.) = 6.84  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.393

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
PUBLIC PARK	D	1.01	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.850  
 SUBAREA AREA(ACRES) = 1.01 SUBAREA RUNOFF(CFS) = 2.93  
 EFFECTIVE AREA(ACRES) = 2.47 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.08  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.41  
 TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 7.36

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.27 HALFSTREET FLOOD WIDTH(FEET) = 13.13  
 FLOW VELOCITY(FEET/SEC.) = 3.71 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.01  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 103.00 = 508.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 203.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 347.00 DOWNSTREAM ELEVATION(FEET) = 338.00  
 STREET LENGTH(FEET) = 435.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.36  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.40  
HALFSTREET FLOOD WIDTH(FEET) = 13.80  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.64  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.46  
STREET FLOW TRAVEL TIME(MIN.) = 1.99 Tc(MIN.) = 8.83  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.931  
SUBAREA AREA(ACRES) = 0.00 SUBAREA RUNOFF(CFS) = 0.00  
EFFECTIVE AREA(ACRES) = 2.47 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41  
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 7.36  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.80  
FLOW VELOCITY(FEET/SEC.) = 3.64 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.46  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 203.00 = 943.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 10  
-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 21  
-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 365.00 DOWNSTREAM(FEET) = 354.00

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.812  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.144  
SUBAREA Tc AND LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
RESIDENTIAL  
"5-7 DWELLINGS/ACRE" D 0.36 0.20 0.500 75 7.81  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500  
SUBAREA RUNOFF(CFS) = 0.99  
TOTAL AREA(ACRES) = 0.36 PEAK FLOW RATE(CFS) = 0.99

\*\*\*\*\*  
FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 51  
-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 354.00 DOWNSTREAM(FEET) = 338.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 268.00 CHANNEL SLOPE = 0.0597  
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 1.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 2.00  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.023  
SUBAREA LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS

LAND USE                      GROUP      (ACRES)      (INCH/HR)      (DECIMAL)      CN  
RESIDENTIAL  
"2 DWELLINGS/ACRE"              D              1.05              0.20              0.700              75  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.35  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.09  
AVERAGE FLOW DEPTH(FEET) = 0.54      TRAVEL TIME(MIN.) = 0.55  
Tc(MIN.) = 8.36  
SUBAREA AREA(ACRES) = 1.05              SUBAREA RUNOFF(CFS) = 2.72  
EFFECTIVE AREA(ACRES) = 1.41              AREA-AVERAGED Fm(INCH/HR) = 0.13  
AREA-AVERAGED Fp(INCH/HR) = 0.20      AREA-AVERAGED Ap = 0.65  
TOTAL AREA(ACRES) = 1.4              PEAK FLOW RATE(CFS) = 3.67

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.64      FLOW VELOCITY(FEET/SEC.) = 9.02  
LONGEST FLOWPATH FROM NODE 201.00 TO NODE 203.00 = 598.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	3.67	8.36	3.023	0.20( 0.13)	0.65	1.4	201.00
LONGEST FLOWPATH FROM NODE 201.00 TO NODE 203.00 = 598.00 FEET.							

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.36	8.83	2.931	0.20( 0.08)	0.41	2.5	101.00
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 203.00 = 943.00 FEET.							

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	10.87	8.36	3.023	0.20( 0.10)	0.50	3.7	201.00
2	10.92	8.83	2.931	0.20( 0.10)	0.49	3.9	101.00
TOTAL AREA(ACRES) = 3.9							

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 10.92      Tc(MIN.) = 8.830  
EFFECTIVE AREA(ACRES) = 3.88      AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20      AREA-AVERAGED Ap = 0.49  
TOTAL AREA(ACRES) = 3.9  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 203.00 = 943.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 305.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 338.00      DOWNSTREAM ELEVATION(FEET) = 327.00  
STREET LENGTH(FEET) = 235.00      CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.92  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.40  
 HALFSTREET FLOOD WIDTH(FEET) = 13.74  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.44  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.18  
 STREET FLOW TRAVEL TIME(MIN.) = 0.72 Tc(MIN.) = 9.55  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.802  
 SUBAREA AREA(ACRES) = 0.00 SUBAREA RUNOFF(CFS) = 0.00  
 EFFECTIVE AREA(ACRES) = 3.88 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.49  
 TOTAL AREA(ACRES) = 3.9 PEAK FLOW RATE(CFS) = 10.92  
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.74  
 FLOW VELOCITY(FEET/SEC.) = 5.44 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.18  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 305.00 = 1178.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
 ELEVATION DATA: UPSTREAM(FEET) = 355.00 DOWNSTREAM(FEET) = 344.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.812  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.144  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 RESIDENTIAL  
 "5-7 DWELLINGS/ACRE" D 0.81 0.20 0.500 75 7.81  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500  
 SUBAREA RUNOFF(CFS) = 2.22  
 TOTAL AREA(ACRES) = 0.81 PEAK FLOW RATE(CFS) = 2.22

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 344.00 DOWNSTREAM ELEVATION(FEET) = 341.50  
 STREET LENGTH(FEET) = 112.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 1.00  
INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 2.66  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH (FEET) = 0.30  
HALFSTREET FLOOD WIDTH (FEET) = 8.83  
AVERAGE FLOW VELOCITY (FEET/SEC.) = 2.96  
PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 0.90  
STREET FLOW TRAVEL TIME (MIN.) = 0.63 Tc (MIN.) = 8.44  
\* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.007

SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.33	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA (ACRES) = 0.33 SUBAREA RUNOFF (CFS) = 0.89  
EFFECTIVE AREA (ACRES) = 1.14 AREA-AVERAGED Fm (INCH/HR) = 0.08  
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.38  
TOTAL AREA (ACRES) = 1.1 PEAK FLOW RATE (CFS) = 3.01

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.31 HALFSTREET FLOOD WIDTH (FEET) = 9.37  
FLOW VELOCITY (FEET/SEC.) = 3.02 DEPTH\*VELOCITY (FT\*FT/SEC.) = 0.95  
LONGEST FLOWPATH FROM NODE 301.00 TO NODE 303.00 = 442.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 303.00 TO NODE 303.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION (MIN.) = 8.44  
RAINFALL INTENSITY (INCH/HR) = 3.01  
AREA-AVERAGED Fm (INCH/HR) = 0.08  
AREA-AVERAGED Fp (INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.38  
EFFECTIVE STREAM AREA (ACRES) = 1.14  
TOTAL STREAM AREA (ACRES) = 1.14  
PEAK FLOW RATE (CFS) AT CONFLUENCE = 3.01

\*\*\*\*\*

FLOW PROCESS FROM NODE 304.00 TO NODE 303.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 330.00  
ELEVATION DATA: UPSTREAM (FEET) = 366.00 DOWNSTREAM (FEET) = 341.50

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.495  
\* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.219  
SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS	Tc
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LAND USE                      GROUP      (ACRES)      (INCH/HR)      (DECIMAL)      CN      (MIN.)  
 RESIDENTIAL  
 "2 DWELLINGS/ACRE"              D              1.48              0.20              0.700              75              7.49  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700  
 SUBAREA RUNOFF(CFS) =              4.10  
 TOTAL AREA(ACRES) =              1.48      PEAK FLOW RATE(CFS) =              4.10

\*\*\*\*\*

FLOW PROCESS FROM NODE      303.00 TO NODE      303.00 IS CODE =      1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.49  
 RAINFALL INTENSITY(INCH/HR) = 3.22  
 AREA-AVERAGED Fm(INCH/HR) = 0.14  
 AREA-AVERAGED Fp(INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.70  
 EFFECTIVE STREAM AREA(ACRES) = 1.48  
 TOTAL STREAM AREA(ACRES) = 1.48  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.10

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	3.01	8.44	3.007	0.20( 0.08)	0.38	1.1	301.00
2	4.10	7.49	3.219	0.20( 0.14)	0.70	1.5	304.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.96	7.49	3.219	0.20( 0.11)	0.57	2.5	304.00
2	6.83	8.44	3.007	0.20( 0.11)	0.56	2.6	301.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 6.96      Tc(MIN.) = 7.49  
 EFFECTIVE AREA(ACRES) = 2.49      AREA-AVERAGED Fm(INCH/HR) = 0.11  
 AREA-AVERAGED Fp(INCH/HR) = 0.20      AREA-AVERAGED Ap = 0.57  
 TOTAL AREA(ACRES) = 2.6  
 LONGEST FLOWPATH FROM NODE      301.00 TO NODE      303.00 =      442.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE      303.00 TO NODE      305.00 IS CODE =      61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 341.50      DOWNSTREAM ELEVATION(FEET) = 327.00  
 STREET LENGTH(FEET) = 195.00      CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.76  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 10.82  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.02  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.06  
STREET FLOW TRAVEL TIME(MIN.) = 0.54 Tc(MIN.) = 8.03  
\* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.093

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"1 DWELLING/ACRE"	D	0.60	0.20	0.800	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.800					
SUBAREA AREA(ACRES) = 0.60		SUBAREA RUNOFF(CFS) = 1.58			
EFFECTIVE AREA(ACRES) = 3.09		AREA-AVERAGED Fm(INCH/HR) = 0.12			
AREA-AVERAGED Fp(INCH/HR) = 0.20		AREA-AVERAGED Ap = 0.62			
TOTAL AREA(ACRES) = 3.2		PEAK FLOW RATE(CFS) = 8.27			

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.14  
FLOW VELOCITY(FEET/SEC.) = 6.08 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.12  
LONGEST FLOWPATH FROM NODE 301.00 TO NODE 305.00 = 637.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.27	8.03	3.093	0.20( 0.12)	0.62	3.1	304.00
2	8.06	8.99	2.901	0.20( 0.12)	0.61	3.2	301.00
LONGEST FLOWPATH FROM NODE		301.00 TO NODE		305.00 =		637.00 FEET.	

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	10.87	9.08	2.884	0.20( 0.10)	0.50	3.7	201.00
2	10.92	9.55	2.802	0.20( 0.10)	0.49	3.9	101.00
LONGEST FLOWPATH FROM NODE		101.00 TO NODE		305.00 =		1178.00 FEET.	

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	18.61	8.03	3.093	0.20( 0.11)	0.55	6.4	304.00
2	18.88	8.99	2.901	0.20( 0.11)	0.55	6.9	301.00
3	18.88	9.08	2.884	0.20( 0.11)	0.55	7.0	201.00
4	18.68	9.55	2.802	0.20( 0.11)	0.55	7.1	101.00
TOTAL AREA(ACRES) =		7.1					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 18.88 Tc(MIN.) = 8.986  
EFFECTIVE AREA(ACRES) = 6.93 AREA-AVERAGED Fm(INCH/HR) = 0.11  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.55  
TOTAL AREA(ACRES) = 7.1  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 305.00 = 1178.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 400.00 TO NODE 400.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN.) = 10.00 RAINFALL INTENSITY(INCH/HR) = 2.73  
EFFECTIVE AREA(ACRES) = 190.00  
TOTAL AREA(ACRES) = 190.00 PEAK FLOW RATE(CFS) = 415.00  
AREA-AVERAGED Fm(INCH/HR) = 0.10 AREA-AVERAGED Fp(INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.50

NOTE: EFFECTIVE AREA IS USED AS THE TOTAL CONTRIBUTING AREA FOR ALL  
CONFLUENCE ANALYSES.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 366.00 DOWNSTREAM(FEET) = 345.00  
FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 60.0 INCH PIPE IS 38.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 31.50  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 415.00  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 10.21  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 401.00 = 1578.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.21  
RAINFALL INTENSITY(INCH/HR) = 2.70  
AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.50  
EFFECTIVE STREAM AREA(ACRES) = 190.00  
TOTAL STREAM AREA(ACRES) = 190.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 415.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 371.00 DOWNSTREAM(FEET) = 365.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.819

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.933

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.01	0.20	0.500	75	8.82



SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.500  
 SUBAREA RUNOFF(CFS) = 2.57  
 TOTAL AREA(ACRES) = 1.01 PEAK FLOW RATE(CFS) = 2.57

\*\*\*\*\*

FLOW PROCESS FROM NODE 403.00 TO NODE 404.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 365.00 DOWNSTREAM(FEET) = 363.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 96.00 CHANNEL SLOPE = 0.0208  
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 20.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 2.00

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.812

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
RESIDENTIAL					

"5-7 DWELLINGS/ACRE"	D	0.97	0.20	0.500	75
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SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.500

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.76

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.38

AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 0.67

$T_c$ (MIN.) = 9.49

SUBAREA AREA(ACRES) = 0.97 SUBAREA RUNOFF(CFS) = 2.37

EFFECTIVE AREA(ACRES) = 1.98 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.10

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.50

TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 4.83

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 2.56

LONGEST FLOWPATH FROM NODE 402.00 TO NODE 404.00 = 426.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 404.00 TO NODE 401.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 355.00 DOWNSTREAM(FEET) = 345.00

FLOW LENGTH(FEET) = 68.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.3 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 14.80

GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 4.83

PIPE TRAVEL TIME(MIN.) = 0.08  $T_c$ (MIN.) = 9.57

LONGEST FLOWPATH FROM NODE 402.00 TO NODE 401.00 = 494.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 9.57

RAINFALL INTENSITY(INCH/HR) = 2.80

AREA-AVERAGED  $F_m$ (INCH/HR) = 0.10

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20

AREA-AVERAGED  $A_p = 0.50$   
 EFFECTIVE STREAM AREA (ACRES) = 1.98  
 TOTAL STREAM AREA (ACRES) = 1.98  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 4.83

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	415.00	10.21	2.696	0.20 ( 0.10)	0.50	190.0	101.00
2	4.83	9.57	2.799	0.20 ( 0.10)	0.50	2.0	402.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	409.00	9.57	2.799	0.20 ( 0.10)	0.50	180.0	402.00
2	419.65	10.21	2.696	0.20 ( 0.10)	0.50	192.0	101.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE (CFS) = 419.65 Tc (MIN.) = 10.21  
 EFFECTIVE AREA (ACRES) = 191.98 AREA-AVERAGED Fm (INCH/HR) = 0.10  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
 TOTAL AREA (ACRES) = 192.0  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 401.00 = 1578.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 401.00 TO NODE 405.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 345.00 DOWNSTREAM (FEET) = 342.00  
 FLOW LENGTH (FEET) = 121.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 21.37  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER (INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 419.65  
 PIPE TRAVEL TIME (MIN.) = 0.09 Tc (MIN.) = 10.31  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 405.00 = 1699.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 405.00 TO NODE 405.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 10.31  
 RAINFALL INTENSITY (INCH/HR) = 2.68  
 AREA-AVERAGED Fm (INCH/HR) = 0.10  
 AREA-AVERAGED Fp (INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.50  
 EFFECTIVE STREAM AREA (ACRES) = 191.98  
 TOTAL STREAM AREA (ACRES) = 191.98  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 419.65

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 406.00 TO NODE 407.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 330.00  
ELEVATION DATA: UPSTREAM (FEET) = 367.60 DOWNSTREAM (FEET) = 357.60

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.963  
\* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 3.109

SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE SCS SOIL GROUP AREA (ACRES) Fp (INCH/HR) Ap (DECIMAL) SCS CN Tc (MIN.)  
RESIDENTIAL  
"5-7 DWELLINGS/ACRE" D 0.92 0.20 0.500 75 7.96  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500  
SUBAREA RUNOFF (CFS) = 2.49  
TOTAL AREA (ACRES) = 0.92 PEAK FLOW RATE (CFS) = 2.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 407.00 TO NODE 405.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM (FEET) = 345.00 DOWNSTREAM (FEET) = 342.00  
FLOW LENGTH (FEET) = 65.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.2 INCHES  
PIPE-FLOW VELOCITY (FEET/SEC.) = 8.09  
GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW (CFS) = 2.49  
PIPE TRAVEL TIME (MIN.) = 0.13 Tc (MIN.) = 8.10  
LONGEST FLOWPATH FROM NODE 406.00 TO NODE 405.00 = 395.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 405.00 TO NODE 405.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION (MIN.) = 8.10  
RAINFALL INTENSITY (INCH/HR) = 3.08  
AREA-AVERAGED Fm (INCH/HR) = 0.10  
AREA-AVERAGED Fp (INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.50  
EFFECTIVE STREAM AREA (ACRES) = 0.92  
TOTAL STREAM AREA (ACRES) = 0.92  
PEAK FLOW RATE (CFS) AT CONFLUENCE = 2.49

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	409.00	9.66	2.783	0.20 (0.10)	0.50	180.0	402.00
1	419.65	10.31	2.682	0.20 (0.10)	0.50	192.0	101.00
2	2.49	8.10	3.080	0.20 (0.10)	0.50	0.9	406.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
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1	383.10	8.10	3.080	0.20( 0.10)	0.50	151.7	406.00
2	411.25	9.66	2.783	0.20( 0.10)	0.50	180.9	402.00
3	421.81	10.31	2.682	0.20( 0.10)	0.50	192.9	101.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 421.81 Tc(MIN.) = 10.31  
EFFECTIVE AREA(ACRES) = 192.90 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
TOTAL AREA(ACRES) = 192.9  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 405.00 = 1699.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 405.00 TO NODE 408.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 342.00 DOWNSTREAM(FEET) = 326.00  
FLOW LENGTH(FEET) = 660.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 66.0 INCH PIPE IS 46.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.44  
GIVEN PIPE DIAMETER(INCH) = 66.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 421.81  
PIPE TRAVEL TIME(MIN.) = 0.47 Tc(MIN.) = 10.78  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 408.00 = 2359.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 408.00 TO NODE 408.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.78  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.615  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL FAIR COVER "OPEN BRUSH"	C	1.94	0.25	1.000	77

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000  
SUBAREA AREA(ACRES) = 1.94 SUBAREA RUNOFF(CFS) = 4.13  
EFFECTIVE AREA(ACRES) = 194.84 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
TOTAL AREA(ACRES) = 194.8 PEAK FLOW RATE(CFS) = 440.68

\*\*\*\*\*  
FLOW PROCESS FROM NODE 408.00 TO NODE 408.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.78  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.615  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "8-10 DWELLINGS/ACRE"	C	4.10	0.25	0.400	69
RESIDENTIAL "8-10 DWELLINGS/ACRE"	D	4.13	0.20	0.400	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.22  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400  
SUBAREA AREA(ACRES) = 8.23 SUBAREA RUNOFF(CFS) = 18.70  
EFFECTIVE AREA(ACRES) = 203.07 AREA-AVERAGED Fm(INCH/HR) = 0.10

AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
TOTAL AREA (ACRES) = 203.1 PEAK FLOW RATE (CFS) = 459.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 408.00 TO NODE 409.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 326.00 DOWNSTREAM(FEET) = 321.00  
FLOW LENGTH(FEET) = 145.00 MANNING'S N = 0.013  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.40  
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 459.38  
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 10.88  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 409.00 = 2504.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 409.00 TO NODE 409.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.88  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.600  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "1 DWELLING/ACRE"	C	1.62	0.25	0.800	69
RESIDENTIAL "1 DWELLING/ACRE"	D	1.62	0.20	0.800	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.800  
SUBAREA AREA(ACRES) = 3.24 SUBAREA RUNOFF(CFS) = 7.06  
EFFECTIVE AREA(ACRES) = 206.31 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51  
TOTAL AREA(ACRES) = 206.3 PEAK FLOW RATE(CFS) = 463.83

\*\*\*\*\*  
FLOW PROCESS FROM NODE 409.00 TO NODE 410.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 321.00 DOWNSTREAM(FEET) = 298.00  
FLOW LENGTH(FEET) = 393.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 60.0 INCH PIPE IS 39.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 33.63  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 463.83  
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 11.07  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 410.00 = 2897.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 410.00 TO NODE 410.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 11.07  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.574  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	D	6.89	0.20	0.850	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850					
SUBAREA AREA(ACRES) =		6.89	SUBAREA RUNOFF(CFS) =		14.91
EFFECTIVE AREA(ACRES) =		213.20	AREA-AVERAGED Fm(INCH/HR) =		0.10
AREA-AVERAGED Fp(INCH/HR) =		0.20	AREA-AVERAGED Ap =		0.52
TOTAL AREA(ACRES) =		213.2	PEAK FLOW RATE(CFS) =		473.86

\*\*\*\*\*  
FLOW PROCESS FROM NODE 410.00 TO NODE 410.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 11.07  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.574  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	C	0.40	0.25	0.850	69
PUBLIC PARK	D	0.41	0.20	0.850	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.22					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850					
SUBAREA AREA(ACRES) =		0.81	SUBAREA RUNOFF(CFS) =		1.74
EFFECTIVE AREA(ACRES) =		214.01	AREA-AVERAGED Fm(INCH/HR) =		0.10
AREA-AVERAGED Fp(INCH/HR) =		0.20	AREA-AVERAGED Ap =		0.52
TOTAL AREA(ACRES) =		214.0	PEAK FLOW RATE(CFS) =		475.59

END OF STUDY SUMMARY:

TOTAL AREA(ACRES)	=	214.0	TC(MIN.)	=	11.07
EFFECTIVE AREA(ACRES)	=	214.01	AREA-AVERAGED Fm(INCH/HR)	=	0.10
AREA-AVERAGED Fp(INCH/HR)	=	0.20	AREA-AVERAGED Ap	=	0.518
PEAK FLOW RATE(CFS)	=	475.59			

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	438.37	8.86	2.924	0.20( 0.11)	0.52	172.8	406.00
2	465.44	10.42	2.665	0.20( 0.11)	0.52	202.0	402.00
3	475.59	11.07	2.574	0.20( 0.10)	0.52	214.0	101.00

END OF RATIONAL METHOD ANALYSIS

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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Ver. 23.0 Release Date: 07/01/2016 License ID 1355

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* LAGUNA NIGUEL TOWN CENTER \*  
\* EXISTING CONDITIONS \*  
\* 25-YEAR STORM EVENT \*  
\*\*\*\*\*

FILE NAME: XLNTC25.DAT  
TIME/DATE OF STUDY: 09:20 09/25/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT (YEAR) = 25.00  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 6.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/ SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 330.00  
ELEVATION DATA: UPSTREAM (FEET) = 368.00 DOWNSTREAM (FEET) = 356.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 6.000  
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 4.351  
SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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COMMERCIAL D 1.46 0.20 0.100 75 6.00  
 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100  
 SUBAREA RUNOFF(CFS) = 5.69  
 TOTAL AREA(ACRES) = 1.46 PEAK FLOW RATE(CFS) = 5.69

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 356.00 DOWNSTREAM ELEVATION(FEET) = 347.00  
 STREET LENGTH(FEET) = 178.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 20.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.010  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.010

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.46  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.27  
 HALFSTREET FLOOD WIDTH(FEET) = 13.28  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.69  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.01  
 STREET FLOW TRAVEL TIME(MIN.) = 0.80  $T_c$ (MIN.) = 6.80

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.052

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
PUBLIC PARK	D	1.01	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.850  
 SUBAREA AREA(ACRES) = 1.01 SUBAREA RUNOFF(CFS) = 3.53  
 EFFECTIVE AREA(ACRES) = 2.47 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.08  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.41  
 TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 8.83

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 14.29  
 FLOW VELOCITY(FEET/SEC.) = 3.84 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.09  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 103.00 = 508.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 203.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 347.00 DOWNSTREAM ELEVATION(FEET) = 338.00  
 STREET LENGTH(FEET) = 435.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020



Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.83  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.42  
HALFSTREET FLOOD WIDTH(FEET) = 14.84  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.80  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.61  
STREET FLOW TRAVEL TIME(MIN.) = 1.91 Tc(MIN.) = 8.71  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.523  
SUBAREA AREA(ACRES) = 0.00 SUBAREA RUNOFF(CFS) = 0.00  
EFFECTIVE AREA(ACRES) = 2.47 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41  
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 8.83  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.84  
FLOW VELOCITY(FEET/SEC.) = 3.80 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.61  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 203.00 = 943.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 10  
-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 21  
-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 365.00 DOWNSTREAM(FEET) = 354.00

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.812  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.747  
SUBAREA Tc AND LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
RESIDENTIAL  
"5-7 DWELLINGS/ACRE" D 0.36 0.20 0.500 75 7.81  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500  
SUBAREA RUNOFF(CFS) = 1.18  
TOTAL AREA(ACRES) = 0.36 PEAK FLOW RATE(CFS) = 1.18

\*\*\*\*\*  
FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 51  
-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 354.00 DOWNSTREAM(FEET) = 338.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 268.00 CHANNEL SLOPE = 0.0597  
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 1.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 2.00  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.611  
SUBAREA LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS

LAND USE                    GROUP    (ACRES)    (INCH/HR)    (DECIMAL)    CN  
RESIDENTIAL  
"2 DWELLINGS/ACRE"            D            1.05        0.20        0.700        75  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =            2.82  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    8.48  
AVERAGE FLOW DEPTH(FEET) = 0.58    TRAVEL TIME(MIN.) = 0.53  
Tc(MIN.) = 8.34  
SUBAREA AREA(ACRES) = 1.05            SUBAREA RUNOFF(CFS) = 3.28  
EFFECTIVE AREA(ACRES) = 1.41        AREA-AVERAGED Fm(INCH/HR) = 0.13  
AREA-AVERAGED Fp(INCH/HR) = 0.20    AREA-AVERAGED Ap = 0.65  
TOTAL AREA(ACRES) = 1.4            PEAK FLOW RATE(CFS) = 4.42

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.68    FLOW VELOCITY(FEET/SEC.) = 9.45  
LONGEST FLOWPATH FROM NODE 201.00 TO NODE 203.00 = 598.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	4.42	8.34	3.611	0.20( 0.13)	0.65	1.4	201.00
LONGEST FLOWPATH FROM NODE 201.00 TO NODE 203.00 = 598.00 FEET.							

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	8.83	8.71	3.523	0.20( 0.08)	0.41	2.5	101.00
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 203.00 = 943.00 FEET.							

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	13.08	8.34	3.611	0.20( 0.10)	0.50	3.8	201.00
2	13.13	8.71	3.523	0.20( 0.10)	0.49	3.9	101.00
TOTAL AREA(ACRES) = 3.9							

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.13    Tc(MIN.) = 8.710  
EFFECTIVE AREA(ACRES) = 3.88    AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20    AREA-AVERAGED Ap = 0.49  
TOTAL AREA(ACRES) = 3.9  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 203.00 = 943.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 305.00 IS CODE = 61

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STANDARD CURB SECTION USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 338.00    DOWNSTREAM ELEVATION(FEET) = 327.00  
STREET LENGTH(FEET) = 235.00    CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.13  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.42  
 HALFSTREET FLOOD WIDTH(FEET) = 14.78  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.70  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.41  
 STREET FLOW TRAVEL TIME(MIN.) = 0.69 Tc(MIN.) = 9.40  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.375  
 SUBAREA AREA(ACRES) = 0.00 SUBAREA RUNOFF(CFS) = 0.00  
 EFFECTIVE AREA(ACRES) = 3.88 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.49  
 TOTAL AREA(ACRES) = 3.9 PEAK FLOW RATE(CFS) = 13.13  
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.42 HALFSTREET FLOOD WIDTH(FEET) = 14.78  
 FLOW VELOCITY(FEET/SEC.) = 5.70 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.41  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 305.00 = 1178.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
 ELEVATION DATA: UPSTREAM(FEET) = 355.00 DOWNSTREAM(FEET) = 344.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.812  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.747  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 RESIDENTIAL  
 "5-7 DWELLINGS/ACRE" D 0.81 0.20 0.500 75 7.81  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500  
 SUBAREA RUNOFF(CFS) = 2.66  
 TOTAL AREA(ACRES) = 0.81 PEAK FLOW RATE(CFS) = 2.66

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 344.00 DOWNSTREAM ELEVATION(FEET) = 341.50  
 STREET LENGTH(FEET) = 112.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 1.00  
INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 3.19  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH (FEET) = 0.32  
HALFSTREET FLOOD WIDTH (FEET) = 9.58  
AVERAGE FLOW VELOCITY (FEET/SEC.) = 3.08  
PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 0.98  
STREET FLOW TRAVEL TIME (MIN.) = 0.61 Tc (MIN.) = 8.42  
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.592

SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.33	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA (ACRES) = 0.33 SUBAREA RUNOFF (CFS) = 1.06  
EFFECTIVE AREA (ACRES) = 1.14 AREA-AVERAGED Fm (INCH/HR) = 0.08  
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.38  
TOTAL AREA (ACRES) = 1.1 PEAK FLOW RATE (CFS) = 3.61

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.33 HALFSTREET FLOOD WIDTH (FEET) = 10.12  
FLOW VELOCITY (FEET/SEC.) = 3.16 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.04  
LONGEST FLOWPATH FROM NODE 301.00 TO NODE 303.00 = 442.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 303.00 TO NODE 303.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION (MIN.) = 8.42  
RAINFALL INTENSITY (INCH/HR) = 3.59  
AREA-AVERAGED Fm (INCH/HR) = 0.08  
AREA-AVERAGED Fp (INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.38  
EFFECTIVE STREAM AREA (ACRES) = 1.14  
TOTAL STREAM AREA (ACRES) = 1.14  
PEAK FLOW RATE (CFS) AT CONFLUENCE = 3.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 304.00 TO NODE 303.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 330.00  
ELEVATION DATA: UPSTREAM (FEET) = 366.00 DOWNSTREAM (FEET) = 341.50

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.495  
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.836  
SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS	Tc
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LAND USE                      GROUP      (ACRES)      (INCH/HR)      (DECIMAL)      CN      (MIN.)  
 RESIDENTIAL  
 "2 DWELLINGS/ACRE"              D              1.48              0.20              0.700              75              7.49  
 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.700  
 SUBAREA RUNOFF(CFS) =              4.92  
 TOTAL AREA(ACRES) =              1.48      PEAK FLOW RATE(CFS) =              4.92

\*\*\*\*\*

FLOW PROCESS FROM NODE      303.00 TO NODE      303.00 IS CODE =      1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.49  
 RAINFALL INTENSITY(INCH/HR) = 3.84  
 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.14  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20  
 AREA-AVERAGED  $A_p$  = 0.70  
 EFFECTIVE STREAM AREA(ACRES) = 1.48  
 TOTAL STREAM AREA(ACRES) = 1.48  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.92

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p$ ( $F_m$ ) (INCH/HR)	$A_p$	$A_e$ (ACRES)	HEADWATER NODE
1	3.61	8.42	3.592	0.20( 0.08)	0.38	1.1	301.00
2	4.92	7.49	3.836	0.20( 0.14)	0.70	1.5	304.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	$F_p$ ( $F_m$ ) (INCH/HR)	$A_p$	$A_e$ (ACRES)	HEADWATER NODE
1	8.36	7.49	3.836	0.20( 0.11)	0.57	2.5	304.00
2	8.20	8.42	3.592	0.20( 0.11)	0.56	2.6	301.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 8.36      Tc(MIN.) = 7.49  
 EFFECTIVE AREA(ACRES) = 2.49      AREA-AVERAGED  $F_m$ (INCH/HR) = 0.11  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20      AREA-AVERAGED  $A_p$  = 0.57  
 TOTAL AREA(ACRES) = 2.6  
 LONGEST FLOWPATH FROM NODE      301.00 TO NODE      303.00 =      442.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE      303.00 TO NODE      305.00 IS CODE =      61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 341.50      DOWNSTREAM ELEVATION(FEET) = 327.00  
 STREET LENGTH(FEET) = 195.00      CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.31  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.36  
HALFSTREET FLOOD WIDTH(FEET) = 11.68  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.28  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.26  
STREET FLOW TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 8.01  
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.694

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
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RESIDENTIAL					
"1 DWELLING/ACRE"	D	0.60	0.20	0.800	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.800					
SUBAREA AREA(ACRES) = 0.60		SUBAREA RUNOFF(CFS) = 1.91			
EFFECTIVE AREA(ACRES) = 3.09		AREA-AVERAGED Fm(INCH/HR) = 0.12			
AREA-AVERAGED Fp(INCH/HR) = 0.20		AREA-AVERAGED Ap = 0.62			
TOTAL AREA(ACRES) = 3.2		PEAK FLOW RATE(CFS) = 9.95			

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.00  
FLOW VELOCITY(FEET/SEC.) = 6.38 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.34  
LONGEST FLOWPATH FROM NODE 301.00 TO NODE 305.00 = 637.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	9.95	8.01	3.694	0.20( 0.12)	0.62	3.1	304.00
2	9.71	8.94	3.472	0.20( 0.12)	0.61	3.2	301.00
LONGEST FLOWPATH FROM NODE		301.00 TO NODE		305.00 =		637.00 FEET.	

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	13.08	9.03	3.452	0.20( 0.10)	0.50	3.8	201.00
2	13.13	9.40	3.375	0.20( 0.10)	0.49	3.9	101.00
LONGEST FLOWPATH FROM NODE		101.00 TO NODE		305.00 =		1178.00 FEET.	

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	22.39	8.01	3.694	0.20( 0.11)	0.55	6.4	304.00
2	22.74	8.94	3.472	0.20( 0.11)	0.55	7.0	301.00
3	22.74	9.03	3.452	0.20( 0.11)	0.55	7.0	201.00
4	22.56	9.40	3.375	0.20( 0.11)	0.55	7.1	101.00
TOTAL AREA(ACRES) =		7.1					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 22.74 Tc(MIN.) = 8.940  
EFFECTIVE AREA(ACRES) = 6.96 AREA-AVERAGED Fm(INCH/HR) = 0.11  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.55  
TOTAL AREA(ACRES) = 7.1  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 305.00 = 1178.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 400.00 TO NODE 400.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN.) = 10.00 RAINFALL INTENSITY(INCH/HR) = 3.26  
EFFECTIVE AREA(ACRES) = 190.00  
TOTAL AREA(ACRES) = 190.00 PEAK FLOW RATE(CFS) = 485.00  
AREA-AVERAGED Fm(INCH/HR) = 0.10 AREA-AVERAGED Fp(INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.50

NOTE: EFFECTIVE AREA IS USED AS THE TOTAL CONTRIBUTING AREA FOR ALL  
CONFLUENCE ANALYSES.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 366.00 DOWNSTREAM(FEET) = 345.00  
FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 60.0 INCH PIPE IS 42.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 32.40  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 485.00  
PIPE TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 10.21  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 401.00 = 1578.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.21  
RAINFALL INTENSITY(INCH/HR) = 3.22  
AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.50  
EFFECTIVE STREAM AREA(ACRES) = 190.00  
TOTAL STREAM AREA(ACRES) = 190.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 485.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 371.00 DOWNSTREAM(FEET) = 365.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.819

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.499

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "5-7 DWELLINGS/ACRE"	D	1.01	0.20	0.500	75	8.82

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.500  
 SUBAREA RUNOFF(CFS) = 3.09  
 TOTAL AREA(ACRES) = 1.01 PEAK FLOW RATE(CFS) = 3.09

\*\*\*\*\*

FLOW PROCESS FROM NODE 403.00 TO NODE 404.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 365.00 DOWNSTREAM(FEET) = 363.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 96.00 CHANNEL SLOPE = 0.0208  
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 20.000  
 MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 2.00

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.366

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
RESIDENTIAL					

"5-7 DWELLINGS/ACRE"	D	0.97	0.20	0.500	75
----------------------	---	------	------	-------	----

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.500

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.52

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.58

AVERAGE FLOW DEPTH(FEET) = 0.08 TRAVEL TIME(MIN.) = 0.62

$T_c$ (MIN.) = 9.44

SUBAREA AREA(ACRES) = 0.97 SUBAREA RUNOFF(CFS) = 2.85

EFFECTIVE AREA(ACRES) = 1.98 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.10

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.50

TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 5.82

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 2.82

LONGEST FLOWPATH FROM NODE 402.00 TO NODE 404.00 = 426.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 404.00 TO NODE 401.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 355.00 DOWNSTREAM(FEET) = 345.00

FLOW LENGTH(FEET) = 68.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 15.63

GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 5.82

PIPE TRAVEL TIME(MIN.) = 0.07  $T_c$ (MIN.) = 9.51

LONGEST FLOWPATH FROM NODE 402.00 TO NODE 401.00 = 494.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 9.51

RAINFALL INTENSITY(INCH/HR) = 3.35

AREA-AVERAGED  $F_m$ (INCH/HR) = 0.10

AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20



AREA-AVERAGED  $A_p = 0.50$   
 EFFECTIVE STREAM AREA (ACRES) = 1.98  
 TOTAL STREAM AREA (ACRES) = 1.98  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 5.82

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	485.00	10.21	3.221	0.20 ( 0.10)	0.50	190.0	101.00
2	5.82	9.51	3.352	0.20 ( 0.10)	0.50	2.0	402.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	476.83	9.51	3.352	0.20 ( 0.10)	0.50	179.1	402.00
2	490.59	10.21	3.221	0.20 ( 0.10)	0.50	192.0	101.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE (CFS) = 490.59 Tc (MIN.) = 10.21  
 EFFECTIVE AREA (ACRES) = 191.98 AREA-AVERAGED Fm (INCH/HR) = 0.10  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
 TOTAL AREA (ACRES) = 192.0  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 401.00 = 1578.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 401.00 TO NODE 405.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 345.00 DOWNSTREAM (FEET) = 342.00  
 FLOW LENGTH (FEET) = 121.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 24.99  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER (INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 490.59  
 PIPE TRAVEL TIME (MIN.) = 0.08 Tc (MIN.) = 10.29  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 405.00 = 1699.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 405.00 TO NODE 405.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 10.29  
 RAINFALL INTENSITY (INCH/HR) = 3.21  
 AREA-AVERAGED Fm (INCH/HR) = 0.10  
 AREA-AVERAGED Fp (INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.50  
 EFFECTIVE STREAM AREA (ACRES) = 191.98  
 TOTAL STREAM AREA (ACRES) = 191.98  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 490.59

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 406.00 TO NODE 407.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 330.00
ELEVATION DATA: UPSTREAM (FEET) = 367.60 DOWNSTREAM (FEET) = 357.60

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)]\*\*0.20
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.963
\* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.707

SUBAREA Tc AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE SCS SOIL GROUP AREA (ACRES) Fp (INCH/HR) Ap (DECIMAL) SCS CN Tc (MIN.)
RESIDENTIAL
"5-7 DWELLINGS/ACRE" D 0.92 0.20 0.500 75 7.96
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500
SUBAREA RUNOFF (CFS) = 2.99
TOTAL AREA (ACRES) = 0.92 PEAK FLOW RATE (CFS) = 2.99

\*\*\*\*\*
FLOW PROCESS FROM NODE 407.00 TO NODE 405.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 345.00 DOWNSTREAM (FEET) = 342.00
FLOW LENGTH (FEET) = 65.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.5 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 8.53
GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 2.99
PIPE TRAVEL TIME (MIN.) = 0.13 Tc (MIN.) = 8.09
LONGEST FLOWPATH FROM NODE 406.00 TO NODE 405.00 = 395.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 405.00 TO NODE 405.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION (MIN.) = 8.09
RAINFALL INTENSITY (INCH/HR) = 3.67
AREA-AVERAGED Fm (INCH/HR) = 0.10
AREA-AVERAGED Fp (INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.50
EFFECTIVE STREAM AREA (ACRES) = 0.92
TOTAL STREAM AREA (ACRES) = 0.92
PEAK FLOW RATE (CFS) AT CONFLUENCE = 2.99

\*\* CONFLUENCE DATA \*\*

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp (Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists data for 2 streams.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp (Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. It lists peak flow rate data for 2 streams.

1	447.02	8.09	3.674	0.20( 0.10)	0.50	151.9	406.00
2	479.53	9.60	3.335	0.20( 0.10)	0.50	180.0	402.00
3	493.18	10.29	3.207	0.20( 0.10)	0.50	192.9	101.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 493.18 Tc(MIN.) = 10.29  
EFFECTIVE AREA(ACRES) = 192.90 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
TOTAL AREA(ACRES) = 192.9  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 405.00 = 1699.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 405.00 TO NODE 408.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 342.00 DOWNSTREAM(FEET) = 326.00  
FLOW LENGTH(FEET) = 660.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 66.0 INCH PIPE IS 53.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.80  
GIVEN PIPE DIAMETER(INCH) = 66.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 493.18  
PIPE TRAVEL TIME(MIN.) = 0.46 Tc(MIN.) = 10.75  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 408.00 = 2359.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 408.00 TO NODE 408.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.75  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.128  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL FAIR COVER "OPEN BRUSH"	C	1.94	0.25	1.000	77

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000  
SUBAREA AREA(ACRES) = 1.94 SUBAREA RUNOFF(CFS) = 5.02  
EFFECTIVE AREA(ACRES) = 194.84 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
TOTAL AREA(ACRES) = 194.8 PEAK FLOW RATE(CFS) = 530.70

\*\*\*\*\*  
FLOW PROCESS FROM NODE 408.00 TO NODE 408.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.75  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.128  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "8-10 DWELLINGS/ACRE"	C	4.10	0.25	0.400	69
RESIDENTIAL "8-10 DWELLINGS/ACRE"	D	4.13	0.20	0.400	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.22  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400  
SUBAREA AREA(ACRES) = 8.23 SUBAREA RUNOFF(CFS) = 22.50  
EFFECTIVE AREA(ACRES) = 203.07 AREA-AVERAGED Fm(INCH/HR) = 0.10

AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
TOTAL AREA (ACRES) = 203.1 PEAK FLOW RATE (CFS) = 553.20

\*\*\*\*\*  
FLOW PROCESS FROM NODE 408.00 TO NODE 409.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 326.00 DOWNSTREAM(FEET) = 321.00  
FLOW LENGTH(FEET) = 145.00 MANNING'S N = 0.013  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY(FEET/SEC.) = 28.17  
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 553.20  
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 10.83  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 409.00 = 2504.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 409.00 TO NODE 409.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.83  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.114  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "1 DWELLING/ACRE"	C	1.62	0.25	0.800	69
RESIDENTIAL "1 DWELLING/ACRE"	D	1.62	0.20	0.800	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.800  
SUBAREA AREA(ACRES) = 3.24 SUBAREA RUNOFF(CFS) = 8.56  
EFFECTIVE AREA(ACRES) = 206.31 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51  
TOTAL AREA(ACRES) = 206.3 PEAK FLOW RATE(CFS) = 559.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 409.00 TO NODE 410.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 321.00 DOWNSTREAM(FEET) = 298.00  
FLOW LENGTH(FEET) = 393.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 60.0 INCH PIPE IS 46.0 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 34.60  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 559.19  
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 11.02  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 410.00 = 2897.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 410.00 TO NODE 410.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 11.02  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.083  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	D	6.89	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850  
 SUBAREA AREA(ACRES) = 6.89      SUBAREA RUNOFF(CFS) = 18.07  
 EFFECTIVE AREA(ACRES) = 213.20      AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20      AREA-AVERAGED Ap = 0.52  
 TOTAL AREA(ACRES) = 213.2      PEAK FLOW RATE(CFS) = 571.62

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 410.00 TO NODE 410.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 11.02  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.083  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	C	0.40	0.25	0.850	69
PUBLIC PARK	D	0.41	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.22  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850  
 SUBAREA AREA(ACRES) = 0.81      SUBAREA RUNOFF(CFS) = 2.11  
 EFFECTIVE AREA(ACRES) = 214.01      AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20      AREA-AVERAGED Ap = 0.52  
 TOTAL AREA(ACRES) = 214.0      PEAK FLOW RATE(CFS) = 573.73

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 214.0      TC(MIN.) = 11.02  
 EFFECTIVE AREA(ACRES) = 214.01      AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20      AREA-AVERAGED Ap = 0.518  
 PEAK FLOW RATE(CFS) = 573.73

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	527.48	8.84	3.494	0.20( 0.11)	0.52	173.0	406.00
2	559.80	10.34	3.198	0.20( 0.11)	0.52	201.1	402.00
3	573.73	11.02	3.083	0.20( 0.10)	0.52	214.0	101.00

END OF RATIONAL METHOD ANALYSIS

\*\*\*\*\*  
RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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Ver. 23.0 Release Date: 07/01/2016 License ID 1355

Analysis prepared by:

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* LAGUNA NIGUEL TOWN CENTER \*  
\* EXISTING CONDITIONS \*  
\* 100-YEAR EVENT \*  
\*\*\*\*\*

FILE NAME: XLNTC100.DAT  
TIME/DATE OF STUDY: 09:22 09/25/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT (YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 6.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/ SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
  - (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
- \*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 330.00  
ELEVATION DATA: UPSTREAM (FEET) = 368.00 DOWNSTREAM (FEET) = 356.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 6.000  
\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 5.574

SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
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COMMERCIAL D 1.46 0.20 0.100 91 6.00  
 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.100  
 SUBAREA RUNOFF(CFS) = 7.30  
 TOTAL AREA(ACRES) = 1.46 PEAK FLOW RATE(CFS) = 7.30

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====  
 UPSTREAM ELEVATION(FEET) = 356.00 DOWNSTREAM ELEVATION(FEET) = 347.00  
 STREET LENGTH(FEET) = 178.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 20.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.010  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.010

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.59  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.29  
 HALFSTREET FLOOD WIDTH(FEET) = 14.87  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.88  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.13  
 STREET FLOW TRAVEL TIME(MIN.) = 0.76  $T_c$ (MIN.) = 6.76  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.203

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
PUBLIC PARK	D	1.01	0.20	0.850	91

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.850  
 SUBAREA AREA(ACRES) = 1.01 SUBAREA RUNOFF(CFS) = 4.58  
 EFFECTIVE AREA(ACRES) = 2.47 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.08  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20 AREA-AVERAGED  $A_p$  = 0.41  
 TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 11.39

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 15.88  
 FLOW VELOCITY(FEET/SEC.) = 4.09 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.23  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 103.00 = 508.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 203.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====  
 UPSTREAM ELEVATION(FEET) = 347.00 DOWNSTREAM ELEVATION(FEET) = 338.00  
 STREET LENGTH(FEET) = 435.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.39  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.46  
HALFSTREET FLOOD WIDTH(FEET) = 16.45  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.03  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.84  
STREET FLOW TRAVEL TIME(MIN.) = 1.80 Tc(MIN.) = 8.56  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.546  
SUBAREA AREA(ACRES) = 0.00 SUBAREA RUNOFF(CFS) = 0.00  
EFFECTIVE AREA(ACRES) = 2.47 AREA-AVERAGED Fm(INCH/HR) = 0.08  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.41  
TOTAL AREA(ACRES) = 2.5 PEAK FLOW RATE(CFS) = 11.39  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.46 HALFSTREET FLOOD WIDTH(FEET) = 16.45  
FLOW VELOCITY(FEET/SEC.) = 4.03 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.84  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 203.00 = 943.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 10  
-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 21  
-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 365.00 DOWNSTREAM(FEET) = 354.00

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.812  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.791  
SUBAREA Tc AND LOSS RATE DATA(AMC III):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
RESIDENTIAL  
"5-7 DWELLINGS/ACRE" D 0.36 0.20 0.500 91 7.81  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500  
SUBAREA RUNOFF(CFS) = 1.52  
TOTAL AREA(ACRES) = 0.36 PEAK FLOW RATE(CFS) = 1.52

\*\*\*\*\*  
FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 51  
-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 354.00 DOWNSTREAM(FEET) = 338.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 268.00 CHANNEL SLOPE = 0.0597  
CHANNEL BASE(FEET) = 0.00 "Z" FACTOR = 1.000  
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH(FEET) = 2.00  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.624  
SUBAREA LOSS RATE DATA(AMC III):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS



LAND USE                    GROUP    (ACRES)    (INCH/HR)    (DECIMAL)    CN  
 RESIDENTIAL  
 "2 DWELLINGS/ACRE"            D            1.05        0.20        0.700        91  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =            3.64  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =    8.94  
 AVERAGE FLOW DEPTH(FEET) = 0.64    TRAVEL TIME(MIN.) = 0.50  
 Tc(MIN.) = 8.31  
 SUBAREA AREA(ACRES) = 1.05            SUBAREA RUNOFF(CFS) = 4.24  
 EFFECTIVE AREA(ACRES) = 1.41        AREA-AVERAGED Fm(INCH/HR) = 0.13  
 AREA-AVERAGED Fp(INCH/HR) = 0.20    AREA-AVERAGED Ap = 0.65  
 TOTAL AREA(ACRES) = 1.4            PEAK FLOW RATE(CFS) = 5.70

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.75    FLOW VELOCITY(FEET/SEC.) = 10.07  
 LONGEST FLOWPATH FROM NODE 201.00 TO NODE 203.00 = 598.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 203.00 TO NODE 203.00 IS CODE = 11

-----  
 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
 =====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.70	8.31	4.624	0.20( 0.13)	0.65	1.4	201.00
LONGEST FLOWPATH FROM NODE 201.00 TO NODE 203.00 = 598.00 FEET.							

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.39	8.56	4.546	0.20( 0.08)	0.41	2.5	101.00
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 203.00 = 943.00 FEET.							

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	16.95	8.31	4.624	0.20( 0.10)	0.50	3.8	201.00
2	16.99	8.56	4.546	0.20( 0.10)	0.49	3.9	101.00
TOTAL AREA(ACRES) = 3.9							

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 16.99    Tc(MIN.) = 8.563  
 EFFECTIVE AREA(ACRES) = 3.88    AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20    AREA-AVERAGED Ap = 0.49  
 TOTAL AREA(ACRES) = 3.9  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 203.00 = 943.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 203.00 TO NODE 305.00 IS CODE = 61

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<  
 =====

UPSTREAM ELEVATION(FEET) = 338.00    DOWNSTREAM ELEVATION(FEET) = 327.00  
 STREET LENGTH(FEET) = 235.00    CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.99  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.45  
 HALFSTREET FLOOD WIDTH(FEET) = 16.39  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.06  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.75  
 STREET FLOW TRAVEL TIME(MIN.) = 0.65 Tc(MIN.) = 9.21  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.360  
 SUBAREA AREA(ACRES) = 0.00 SUBAREA RUNOFF(CFS) = 0.00  
 EFFECTIVE AREA(ACRES) = 3.88 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.49  
 TOTAL AREA(ACRES) = 3.9 PEAK FLOW RATE(CFS) = 16.99  
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.45 HALFSTREET FLOOD WIDTH(FEET) = 16.39  
 FLOW VELOCITY(FEET/SEC.) = 6.06 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.75  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 305.00 = 1178.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 10

-----  
 >>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<  
 =====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
 =====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
 ELEVATION DATA: UPSTREAM(FEET) = 355.00 DOWNSTREAM(FEET) = 344.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.812  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.791  
 SUBAREA Tc AND LOSS RATE DATA(AMC III):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 RESIDENTIAL  
 "5-7 DWELLINGS/ACRE" D 0.81 0.20 0.500 91 7.81  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500  
 SUBAREA RUNOFF(CFS) = 3.42  
 TOTAL AREA(ACRES) = 0.81 PEAK FLOW RATE(CFS) = 3.42

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 61

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<  
 =====

UPSTREAM ELEVATION(FEET) = 344.00 DOWNSTREAM ELEVATION(FEET) = 341.50  
 STREET LENGTH(FEET) = 112.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 1.00  
INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 4.10  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH (FEET) = 0.34  
HALFSTREET FLOOD WIDTH (FEET) = 10.66  
AVERAGE FLOW VELOCITY (FEET/SEC.) = 3.27  
PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 1.11  
STREET FLOW TRAVEL TIME (MIN.) = 0.57 Tc (MIN.) = 8.38  
\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 4.601

SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.33	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA (ACRES) = 0.33 SUBAREA RUNOFF (CFS) = 1.36  
EFFECTIVE AREA (ACRES) = 1.14 AREA-AVERAGED Fm (INCH/HR) = 0.08  
AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.38  
TOTAL AREA (ACRES) = 1.1 PEAK FLOW RATE (CFS) = 4.64

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.35 HALFSTREET FLOOD WIDTH (FEET) = 11.25  
FLOW VELOCITY (FEET/SEC.) = 3.36 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.18  
LONGEST FLOWPATH FROM NODE 301.00 TO NODE 303.00 = 442.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 303.00 TO NODE 303.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION (MIN.) = 8.38  
RAINFALL INTENSITY (INCH/HR) = 4.60  
AREA-AVERAGED Fm (INCH/HR) = 0.08  
AREA-AVERAGED Fp (INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.38  
EFFECTIVE STREAM AREA (ACRES) = 1.14  
TOTAL STREAM AREA (ACRES) = 1.14  
PEAK FLOW RATE (CFS) AT CONFLUENCE = 4.64

\*\*\*\*\*  
FLOW PROCESS FROM NODE 304.00 TO NODE 303.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 330.00  
ELEVATION DATA: UPSTREAM (FEET) = 366.00 DOWNSTREAM (FEET) = 341.50

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.495  
\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 4.907  
SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS	Tc
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LAND USE          GROUP  (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
RESIDENTIAL
"2 DWELLINGS/ACRE"  D      1.48      0.20      0.700     91   7.49
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700
SUBAREA RUNOFF(CFS) = 6.35
TOTAL AREA(ACRES) = 1.48 PEAK FLOW RATE(CFS) = 6.35

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*****
FLOW PROCESS FROM NODE 303.00 TO NODE 303.00 IS CODE = 1
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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====

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TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.49
RAINFALL INTENSITY(INCH/HR) = 4.91
AREA-AVERAGED Fm(INCH/HR) = 0.14
AREA-AVERAGED Fp(INCH/HR) = 0.20
AREA-AVERAGED Ap = 0.70
EFFECTIVE STREAM AREA(ACRES) = 1.48
TOTAL STREAM AREA(ACRES) = 1.48
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.35

```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	4.64	8.38	4.601	0.20( 0.08)	0.38	1.1	301.00
2	6.35	7.49	4.907	0.20( 0.14)	0.70	1.5	304.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	10.78	7.49	4.907	0.20( 0.11)	0.57	2.5	304.00
2	10.58	8.38	4.601	0.20( 0.11)	0.56	2.6	301.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 10.78 Tc(MIN.) = 7.49
EFFECTIVE AREA(ACRES) = 2.50 AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.57
TOTAL AREA(ACRES) = 2.6
LONGEST FLOWPATH FROM NODE 301.00 TO NODE 303.00 = 442.00 FEET.

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*****
FLOW PROCESS FROM NODE 303.00 TO NODE 305.00 IS CODE = 61
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>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====

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UPSTREAM ELEVATION(FEET) = 341.50 DOWNSTREAM ELEVATION(FEET) = 327.00
STREET LENGTH(FEET) = 195.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

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DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 1.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

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SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

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Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 12.01  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.39  
HALFSTREET FLOOD WIDTH(FEET) = 12.97  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.68  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.57  
STREET FLOW TRAVEL TIME(MIN.) = 0.49 Tc(MIN.) = 7.98  
\* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 4.733

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"1 DWELLING/ACRE"	D	0.60	0.20	0.800	91
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.800					
SUBAREA AREA(ACRES) = 0.60		SUBAREA RUNOFF(CFS) = 2.47			
EFFECTIVE AREA(ACRES) = 3.10		AREA-AVERAGED Fm(INCH/HR) = 0.12			
AREA-AVERAGED Fp(INCH/HR) = 0.20		AREA-AVERAGED Ap = 0.62			
TOTAL AREA(ACRES) = 3.2		PEAK FLOW RATE(CFS) = 12.86			

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 13.34  
FLOW VELOCITY(FEET/SEC.) = 6.77 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.66  
LONGEST FLOWPATH FROM NODE 301.00 TO NODE 305.00 = 637.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	12.86	7.98	4.733	0.20( 0.12)	0.62	3.1	304.00
2	12.56	8.87	4.454	0.20( 0.12)	0.61	3.2	301.00
LONGEST FLOWPATH FROM NODE		301.00 TO NODE		305.00 =		637.00 FEET.	

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	16.95	8.96	4.430	0.20( 0.10)	0.50	3.8	201.00
2	16.99	9.21	4.360	0.20( 0.10)	0.49	3.9	101.00
LONGEST FLOWPATH FROM NODE		101.00 TO NODE		305.00 =		1178.00 FEET.	

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	29.02	7.98	4.733	0.20( 0.11)	0.55	6.5	304.00
2	29.44	8.87	4.454	0.20( 0.11)	0.55	7.0	301.00
3	29.44	8.96	4.430	0.20( 0.11)	0.55	7.0	201.00
4	29.27	9.21	4.360	0.20( 0.11)	0.55	7.1	101.00
TOTAL AREA(ACRES) =		7.1					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 29.44 Tc(MIN.) = 8.874  
EFFECTIVE AREA(ACRES) = 6.99 AREA-AVERAGED Fm(INCH/HR) = 0.11  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.55  
TOTAL AREA(ACRES) = 7.1  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 305.00 = 1178.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 400.00 TO NODE 400.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN.) = 10.00 RAINFALL INTENSITY(INCH/HR) = 4.16  
EFFECTIVE AREA(ACRES) = 190.00  
TOTAL AREA(ACRES) = 190.00 PEAK FLOW RATE(CFS) = 640.00  
AREA-AVERAGED Fm(INCH/HR) = 0.10 AREA-AVERAGED Fp(INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.50

NOTE: EFFECTIVE AREA IS USED AS THE TOTAL CONTRIBUTING AREA FOR ALL  
CONFLUENCE ANALYSES.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 366.00 DOWNSTREAM(FEET) = 345.00  
FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY(FEET/SEC.) = 32.59  
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 640.00  
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 10.20  
LONGEST FLOWPATH FROM NODE 101.00 TO NODE 401.00 = 1578.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.20  
RAINFALL INTENSITY(INCH/HR) = 4.11  
AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.50  
EFFECTIVE STREAM AREA(ACRES) = 190.00  
TOTAL STREAM AREA(ACRES) = 190.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 640.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 371.00 DOWNSTREAM(FEET) = 365.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.819  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.470  
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						

"5-7 DWELLINGS/ACRE"           D           1.01           0.20           0.500           91           8.82  
 SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.500  
 SUBAREA RUNOFF(CFS) = 3.97  
 TOTAL AREA(ACRES) = 1.01   PEAK FLOW RATE(CFS) = 3.97

\*\*\*\*\*  
 FLOW PROCESS FROM NODE   403.00 TO NODE   404.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 365.00   DOWNSTREAM(FEET) = 363.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 96.00   CHANNEL SLOPE = 0.0208  
 CHANNEL BASE(FEET) = 20.00   "Z" FACTOR = 20.000  
 MANNING'S FACTOR = 0.015   MAXIMUM DEPTH(FEET) = 2.00  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.312  
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	$F_p$ (INCH/HR)	$A_p$ (DECIMAL)	SCS CN
RESIDENTIAL					
"5-7 DWELLINGS/ACRE"	D	0.97	0.20	0.500	91

SUBAREA AVERAGE PERVIOUS LOSS RATE,  $F_p$ (INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION,  $A_p$  = 0.500  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.81  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.81  
 AVERAGE FLOW DEPTH(FEET) = 0.09   TRAVEL TIME(MIN.) = 0.57  
 $T_c$ (MIN.) = 9.39  
 SUBAREA AREA(ACRES) = 0.97   SUBAREA RUNOFF(CFS) = 3.68  
 EFFECTIVE AREA(ACRES) = 1.98   AREA-AVERAGED  $F_m$ (INCH/HR) = 0.10  
 AREA-AVERAGED  $F_p$ (INCH/HR) = 0.20   AREA-AVERAGED  $A_p$  = 0.50  
 TOTAL AREA(ACRES) = 2.0   PEAK FLOW RATE(CFS) = 7.51

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.11   FLOW VELOCITY(FEET/SEC.) = 3.08  
 LONGEST FLOWPATH FROM NODE   402.00 TO NODE   404.00 = 426.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE   404.00 TO NODE   401.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 355.00   DOWNSTREAM(FEET) = 345.00  
 FLOW LENGTH(FEET) = 68.00   MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 16.80  
 GIVEN PIPE DIAMETER(INCH) = 18.00   NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 7.51  
 PIPE TRAVEL TIME(MIN.) = 0.07    $T_c$ (MIN.) = 9.46  
 LONGEST FLOWPATH FROM NODE   402.00 TO NODE   401.00 = 494.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE   401.00 TO NODE   401.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.46  
 RAINFALL INTENSITY(INCH/HR) = 4.29  
 AREA-AVERAGED  $F_m$ (INCH/HR) = 0.10

AREA-AVERAGED Fp (INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.50  
 EFFECTIVE STREAM AREA (ACRES) = 1.98  
 TOTAL STREAM AREA (ACRES) = 1.98  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 7.51

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	640.00	10.20	4.111	0.20 ( 0.10)	0.50	190.0	101.00
2	7.51	9.46	4.295	0.20 ( 0.10)	0.50	2.0	402.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	627.67	9.46	4.295	0.20 ( 0.10)	0.50	178.0	402.00
2	647.18	10.20	4.111	0.20 ( 0.10)	0.50	192.0	101.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 647.18 Tc (MIN.) = 10.20  
 EFFECTIVE AREA (ACRES) = 191.98 AREA-AVERAGED Fm (INCH/HR) = 0.10  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
 TOTAL AREA (ACRES) = 192.0  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 401.00 = 1578.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 401.00 TO NODE 405.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 345.00 DOWNSTREAM (FEET) = 342.00  
 FLOW LENGTH (FEET) = 121.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 32.96  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER (INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 647.18  
 PIPE TRAVEL TIME (MIN.) = 0.06 Tc (MIN.) = 10.27  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 405.00 = 1699.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 405.00 TO NODE 405.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 10.27  
 RAINFALL INTENSITY (INCH/HR) = 4.10  
 AREA-AVERAGED Fm (INCH/HR) = 0.10  
 AREA-AVERAGED Fp (INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.50  
 EFFECTIVE STREAM AREA (ACRES) = 191.98  
 TOTAL STREAM AREA (ACRES) = 191.98  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 647.18

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 406.00 TO NODE 407.00 IS CODE = 21



>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
 ELEVATION DATA: UPSTREAM(FEET) = 367.60 DOWNSTREAM(FEET) = 357.60

Tc = K \* [(LENGTH\*\* 3.00) / (ELEVATION CHANGE)] \*\* 0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.963  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.739

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
"5-7 DWELLINGS/ACRE"	D	0.92	0.20	0.500	91	7.96

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.500

SUBAREA RUNOFF(CFS) = 3.84  
 TOTAL AREA(ACRES) = 0.92 PEAK FLOW RATE(CFS) = 3.84

\*\*\*\*\*

FLOW PROCESS FROM NODE 407.00 TO NODE 405.00 IS CODE = 41

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 345.00 DOWNSTREAM(FEET) = 342.00  
 FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.18  
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.84  
 PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 8.08  
 LONGEST FLOWPATH FROM NODE 406.00 TO NODE 405.00 = 395.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 405.00 TO NODE 405.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.08  
 RAINFALL INTENSITY(INCH/HR) = 4.70  
 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.50  
 EFFECTIVE STREAM AREA(ACRES) = 0.92  
 TOTAL STREAM AREA(ACRES) = 0.92  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.84

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	627.67	9.52	4.278	0.20( 0.10)	0.50	178.0	402.00
1	647.18	10.27	4.097	0.20( 0.10)	0.50	192.0	101.00
2	3.84	8.08	4.699	0.20( 0.10)	0.50	0.9	406.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM	Q	Tc	Intensity	Fp(Fm)	Ap	Ae	HEADWATER
--------	---	----	-----------	--------	----	----	-----------

NUMBER	(CFS)	(MIN.)	(INCH/HR)	(INCH/HR)	(ACRES)	NODE
1	590.37	8.08	4.699	0.20( 0.10)	0.50	406.00
2	631.16	9.52	4.278	0.20( 0.10)	0.50	402.00
3	650.52	10.27	4.097	0.20( 0.10)	0.50	101.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 650.52 Tc(MIN.) = 10.27  
 EFFECTIVE AREA(ACRES) = 192.90 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
 TOTAL AREA(ACRES) = 192.9  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 405.00 = 1699.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 405.00 TO NODE 408.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 342.00 DOWNSTREAM(FEET) = 326.00  
 FLOW LENGTH(FEET) = 660.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 27.38  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER(INCH) = 66.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 650.52  
 PIPE TRAVEL TIME(MIN.) = 0.40 Tc(MIN.) = 10.67  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 408.00 = 2359.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 408.00 TO NODE 408.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.67  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.008  
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL FAIR COVER					
"OPEN BRUSH"	C	1.94	0.25	1.000	92

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000  
 SUBAREA AREA(ACRES) = 1.94 SUBAREA RUNOFF(CFS) = 6.56  
 EFFECTIVE AREA(ACRES) = 194.84 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
 TOTAL AREA(ACRES) = 194.8 PEAK FLOW RATE(CFS) = 685.03

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 408.00 TO NODE 408.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.67  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.008  
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	C	4.10	0.25	0.400	86
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	D	4.13	0.20	0.400	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.22  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400

SUBAREA AREA (ACRES) = 8.23 SUBAREA RUNOFF (CFS) = 29.02  
 EFFECTIVE AREA (ACRES) = 203.07 AREA-AVERAGED Fm (INCH/HR) = 0.10  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
 TOTAL AREA (ACRES) = 203.1 PEAK FLOW RATE (CFS) = 714.06

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 408.00 TO NODE 409.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 326.00 DOWNSTREAM (FEET) = 321.00  
 FLOW LENGTH (FEET) = 145.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 36.37  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER (INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 714.06  
 PIPE TRAVEL TIME (MIN.) = 0.07 Tc (MIN.) = 10.73  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 409.00 = 2504.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 409.00 TO NODE 409.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 10.73  
 \* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.994  
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "1 DWELLING/ACRE"	C	1.62	0.25	0.800	86
RESIDENTIAL "1 DWELLING/ACRE"	D	1.62	0.20	0.800	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.23  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.800  
 SUBAREA AREA (ACRES) = 3.24 SUBAREA RUNOFF (CFS) = 11.12  
 EFFECTIVE AREA (ACRES) = 206.31 AREA-AVERAGED Fm (INCH/HR) = 0.10  
 AREA-AVERAGED Fp (INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.51  
 TOTAL AREA (ACRES) = 206.3 PEAK FLOW RATE (CFS) = 722.57

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 409.00 TO NODE 410.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 321.00 DOWNSTREAM (FEET) = 298.00  
 FLOW LENGTH (FEET) = 393.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 36.80  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER (INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 722.57  
 PIPE TRAVEL TIME (MIN.) = 0.18 Tc (MIN.) = 10.91  
 LONGEST FLOWPATH FROM NODE 101.00 TO NODE 410.00 = 2897.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 410.00 TO NODE 410.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.91  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.956  
 SUBAREA LOSS RATE DATA(AMC III):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 PUBLIC PARK D 6.89 0.20 0.850 91  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850  
 SUBAREA AREA(ACRES) = 6.89 SUBAREA RUNOFF(CFS) = 23.48  
 EFFECTIVE AREA(ACRES) = 213.20 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.52  
 TOTAL AREA(ACRES) = 213.2 PEAK FLOW RATE(CFS) = 739.10

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 410.00 TO NODE 410.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.91  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.956  
 SUBAREA LOSS RATE DATA(AMC III):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 PUBLIC PARK C 0.40 0.25 0.850 86  
 PUBLIC PARK D 0.41 0.20 0.850 91  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.22  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850  
 SUBAREA AREA(ACRES) = 0.81 SUBAREA RUNOFF(CFS) = 2.74  
 EFFECTIVE AREA(ACRES) = 214.01 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.52  
 TOTAL AREA(ACRES) = 214.0 PEAK FLOW RATE(CFS) = 741.84

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 214.0 TC(MIN.) = 10.91  
 EFFECTIVE AREA(ACRES) = 214.01 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.518  
 PEAK FLOW RATE(CFS) = 741.84

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	681.38	8.79	4.478	0.20( 0.11)	0.52	173.2	406.00
2	722.18	10.18	4.116	0.20( 0.11)	0.52	200.1	402.00
3	741.84	10.91	3.956	0.20( 0.10)	0.52	214.0	101.00

END OF RATIONAL METHOD ANALYSIS

APPENDIX 2  
10, 25, & 100 YEAR DEVELOPED  
CONDITIONS STUDIES

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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 Ver. 23.0 Release Date: 07/01/2016 License ID 1355

Analysis prepared by:

fusco engineering  
 16795 Von Karman  
 Suite 100  
 Irvine, CA

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* Laguna Niguel Town Center \*  
 \* Proposed Condition Hydrology Analysis \*  
 \* 10-year storm event \*  
 \*\*\*\*\*

FILE NAME: PRLNT10.DAT  
 TIME/DATE OF STUDY: 16:45 09/25/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 \*DATA BANK RAINFALL USED\*  
 \*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- CROWN TO		STREET-CROSSFALL:		CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)	IN- / SIDE	OUT- / SIDE/ WAY		WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018	0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
  - (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)
- \*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
 \*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

A1

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 298.00  
 ELEVATION DATA: UPSTREAM(FEET) = 357.60 DOWNSTREAM(FEET) = 349.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.033

PRLNT10

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.645

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	D	0.70	0.20	0.100	75	6.03

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 2.28  
 TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 2.28

A1  
(to Pacific  
Island Pr.)

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 203.00 IS CODE = 61  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

B1

=====

UPSTREAM ELEVATION(FEET) = 349.00 DOWNSTREAM ELEVATION(FEET) = 338.00  
 STREET LENGTH(FEET) = 435.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 32.00

(Alicia Plamy)

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 27.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.79  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.33  
 HALFSTREET FLOOD WIDTH(FEET) = 10.04  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.37  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.10  
 STREET FLOW TRAVEL TIME(MIN.) = 2.15 Tc(MIN.) = 8.18  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.061

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	1.10	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 3.01  
 EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.93

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 11.25  
 FLOW VELOCITY(FEET/SEC.) = 3.56 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.25  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 203.00 = 733.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 203.00 TO NODE 305.00 IS CODE = 61  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

PRLNT10

UPSTREAM ELEVATION(FEET) = 338.00 DOWNSTREAM ELEVATION(FEET) = 327.00  
STREET LENGTH(FEET) = 235.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 27.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.93  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.32  
HALFSTREET FLOOD WIDTH(FEET) = 9.88  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.50  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.46  
STREET FLOW TRAVEL TIME(MIN.) = 0.87 Tc(MIN.) = 9.05  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.889  
SUBAREA AREA(ACRES) = 0.00 SUBAREA RUNOFF(CFS) = 0.00  
EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 4.93  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.88  
FLOW VELOCITY(FEET/SEC.) = 4.50 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.46  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 305.00 = 968.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.05  
RAINFALL INTENSITY(INCH/HR) = 2.89  
AREA-AVERAGED Fm(INCH/HR) = 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.10  
EFFECTIVE STREAM AREA(ACRES) = 1.80  
TOTAL STREAM AREA(ACRES) = 1.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.93

\*\*\*\*\*  
FLOW PROCESS FROM NODE 103.00 TO NODE 301.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

C1

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 357.60 DOWNSTREAM(FEET) = 349.20

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.444



C1

PRLNT10

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.510  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 COMMERCIAL D 2.80 0.20 0.100 75 6.44  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 8.80  
 TOTAL AREA(ACRES) = 2.80 PEAK FLOW RATE(CFS) = 8.80

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 301.00 TO NODE 305.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

C2

=====

ELEVATION DATA: UPSTREAM(FEET) = 349.20 DOWNSTREAM(FEET) = 327.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 527.00 CHANNEL SLOPE = 0.0421  
 CHANNEL BASE(FEET) = 70.00 "Z" FACTOR = 36.000  
 MANNING'S FACTOR = 0.016 MAXIMUM DEPTH(FEET) = 2.00  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.789  
 SUBAREA LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL D 2.20 0.20 0.100 75  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.57  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.76  
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 3.18  
 Tc(MIN.) = 9.63  
 SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 5.48  
 EFFECTIVE AREA(ACRES) = 5.00 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 5.00 PEAK FLOW RATE(CFS) = 12.46

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 2.97  
 LONGEST FLOWPATH FROM NODE 103.00 TO NODE 305.00 = 857.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.63  
 RAINFALL INTENSITY(INCH/HR) = 2.79  
 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 5.00  
 TOTAL STREAM AREA(ACRES) = 5.00  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.46

\*\* CONFLUENCE DATA \*\*  
 STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER

NUMBER	(CFS)	(MIN.)	(INCH/HR)	(INCH/HR)	PRLNT10	(ACRES)	NODE
1	4.93	9.05	2.889	0.20( 0.02)	0.10	1.8	102.00
2	12.46	9.63	2.789	0.20( 0.02)	0.10	5.0	103.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

**\*\* PEAK FLOW RATE TABLE \*\***

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	17.07	9.05	2.889	0.20( 0.02)	0.10	6.5	102.00
2	17.21	9.63	2.789	0.20( 0.02)	0.10	6.8	103.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 17.21 Tc(MIN.) = 9.63  
 EFFECTIVE AREA(ACRES) = 6.80 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 6.8  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 305.00 = 968.00 FEET.

*Q10 (proposed)  
 @ ex duty  
 @ Alicia Pkwy*

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 400.00 TO NODE 400.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<

*EX 60" S.D.*

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN.) = 10.00 RAINFALL INTENSITY(INCH/HR) = 2.73  
 EFFECTIVE AREA(ACRES) = 190.00  
 TOTAL AREA(ACRES) = 190.00 PEAK FLOW RATE(CFS) = 415.00  
 AREA-AVERAGED Fm(INCH/HR) = 0.10 AREA-AVERAGED Fp(INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.50

*@ Pacific  
 Island Dr.  
 & Highland*

NOTE: EFFECTIVE AREA IS USED AS THE TOTAL CONTRIBUTING AREA FOR ALL  
 CONFLUENCE ANALYSES.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

*public.  
 prop 60" through  
 project site  
 (realigned)*

ELEVATION DATA: UPSTREAM( FEET) = 361.50 DOWNSTREAM( FEET) = 333.30  
 FLOW LENGTH( FEET) = 942.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 60.0 INCH PIPE IS 47.7 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC.) = 24.81  
 GIVEN PIPE DIAMETER( INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW( CFS) = 415.00  
 PIPE TRAVEL TIME( MIN.) = 0.63 Tc( MIN.) = 10.63  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 401.00 = 1910.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

*01 (offsite)*

MAINLINE Tc(MIN.) = 10.63  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.635  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
-------------------------------	-------------------	-----------------	-----------------	-----------------	-----------

PRLNT10

RESIDENTIAL  
 "8-10 DWELLINGS/ACRE" C 0.70 0.25 0.400 69  
 RESIDENTIAL  
 "8-10 DWELLINGS/ACRE" D 0.70 0.20 0.400 75  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400  
 SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 3.21  
 EFFECTIVE AREA(ACRES) = 191.40 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
 TOTAL AREA(ACRES) = 191.4 PEAK FLOW RATE(CFS) = 436.62

01 (offsite)

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

02 (offsite)

=====

MAINLINE Tc(MIN.) = 10.63  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.635  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "8-10 DWELLINGS/ACRE"	C	1.10	0.25	0.400	69
RESIDENTIAL "8-10 DWELLINGS/ACRE"	D	1.00	0.20	0.400	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400  
 SUBAREA AREA(ACRES) = 2.10 SUBAREA RUNOFF(CFS) = 4.81  
 EFFECTIVE AREA(ACRES) = 193.50 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
 TOTAL AREA(ACRES) = 193.5 PEAK FLOW RATE(CFS) = 441.43

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 401.00 TO NODE 402.00 IS CODE = 41  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

Public  
 Realigned 60"  
 through  
 project site

=====

ELEVATION DATA: UPSTREAM(FEET) = 333.30 DOWNSTREAM(FEET) = 312.20  
 FLOW LENGTH(FEET) = 705.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 22.48  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 441.43  
 PIPE TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 11.16  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 402.00 = 2615.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 402.00 TO NODE 402.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 11.16  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.563  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					

```

PRINT10
"8-10 DWELLINGS/ACRE"   C      1.00   0.25   0.400   69
RESIDENTIAL
"8-10 DWELLINGS/ACRE"   D      3.10   0.20   0.400   75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.21
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400
SUBAREA AREA(ACRES) = 4.10   SUBAREA RUNOFF(CFS) = 9.14
EFFECTIVE AREA(ACRES) = 197.60   AREA-AVERAGED Fm(INCH/HR) = 0.10
AREA-AVERAGED Fp(INCH/HR) = 0.20   AREA-AVERAGED Ap = 0.50
TOTAL AREA(ACRES) = 197.6   PEAK FLOW RATE(CFS) = 441.43
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

```

03 (offsite)

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*****
FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 41
-----

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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====

```

Realigned 60" pipe  
through  
project  
site.

```

ELEVATION DATA: UPSTREAM(FEET) = 312.20   DOWNSTREAM(FEET) = 305.30
FLOW LENGTH(FEET) = 230.00   MANNING'S N = 0.013
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY(FEET/SEC.) = 22.48
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER(INCH) = 60.00   NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 441.43
PIPE TRAVEL TIME(MIN.) = 0.17   Tc(MIN.) = 11.33
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 403.00 = 2845.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 10
-----

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>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====

```

```

*****
FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 21
-----

```

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

```

D1

```

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 344.00   DOWNSTREAM(FEET) = 329.00

```

```

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.738
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.752
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/   SCS SOIL   AREA   Fp   Ap   SCS   Tc
LAND USE           GROUP   (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL         D       2.50   0.20   0.100   75   5.74
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 8.40
TOTAL AREA(ACRES) = 2.50   PEAK FLOW RATE(CFS) = 8.40

```

```

*****
FLOW PROCESS FROM NODE 502.00 TO NODE 503.00 IS CODE = 61
-----

```

```

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<

```

D2

D2

UPSTREAM ELEVATION(FEET) = 329.00 DOWNSTREAM ELEVATION(FEET) = 321.00  
STREET LENGTH(FEET) = 22.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 25.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.74  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 8.47  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 11.66  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 3.45  
STREET FLOW TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 5.77  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.740

SUBAREA LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
COMMERCIAL D 0.80 0.20 0.100 75  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 2.68  
EFFECTIVE AREA(ACRES) = 3.30 AREA-AVERAGED Fm(INCH/HR) = 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 3.3 PEAK FLOW RATE(CFS) = 11.05

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 8.96  
FLOW VELOCITY(FEET/SEC.) = 12.01 DEPTH\*VELOCITY(FT\*FT/SEC.) = 3.67  
LONGEST FLOWPATH FROM NODE 501.00 TO NODE 503.00 = 352.00 FEET.

to dry @  
Crown  
Valley  
Ph.ing

\*\*\*\*\*

FLOW PROCESS FROM NODE 601.00 TO NODE 602.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

[1]

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 359.50 DOWNSTREAM(FEET) = 356.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.917  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.120  
SUBAREA Tc AND LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
COMMERCIAL C 0.70 0.25 0.100 69 7.92  
COMMERCIAL D 2.00 0.20 0.100 75 7.92  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.21  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA RUNOFF(CFS) = 7.53  
TOTAL AREA(ACRES) = 2.70 PEAK FLOW RATE(CFS) = 7.53

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 602.00 TO NODE 603.00 IS CODE = 61

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

E2

=====

UPSTREAM ELEVATION(FEET) = 356.50 DOWNSTREAM ELEVATION(FEET) = 355.60  
 STREET LENGTH(FEET) = 49.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 25.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.22  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.42  
 HALFSTREET FLOOD WIDTH(FEET) = 14.81  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.55  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.50  
 STREET FLOW TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 8.15  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.069

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.50	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.50 SUBAREA RUNOFF(CFS) = 1.37  
 EFFECTIVE AREA(ACRES) = 3.20 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.21 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 3.2 PEAK FLOW RATE(CFS) = 8.78

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 15.21  
 FLOW VELOCITY(FEET/SEC.) = 3.61 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.55  
 LONGEST FLOWPATH FROM NODE 601.00 TO NODE 603.00 = 379.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 603.00 TO NODE 603.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

E3

=====

MAINLINE Tc(MIN.) = 8.15  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.069  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.30	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 0.82  
 EFFECTIVE AREA(ACRES) = 3.50 AREA-AVERAGED Fm(INCH/HR) = 0.02

PRLNT10

E3

AREA-AVERAGED Fp(INCH/HR) = 0.21 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 9.60

\*\*\*\*\*  
FLOW PROCESS FROM NODE 603.00 TO NODE 604.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

private s.d.

=====

ELEVATION DATA: UPSTREAM(FEET) = 345.00 DOWNSTREAM(FEET) = 330.00  
FLOW LENGTH(FEET) = 1041.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.53  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.60  
PIPE TRAVEL TIME(MIN.) = 2.31 Tc(MIN.) = 10.45  
LONGEST FLOWPATH FROM NODE 601.00 TO NODE 604.00 = 1420.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 604.00 TO NODE 604.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.45  
RAINFALL INTENSITY(INCH/HR) = 2.66  
AREA-AVERAGED Fm(INCH/HR) = 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.21  
AREA-AVERAGED Ap = 0.10  
EFFECTIVE STREAM AREA(ACRES) = 3.50  
TOTAL STREAM AREA(ACRES) = 3.50  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.60

\*\*\*\*\*  
FLOW PROCESS FROM NODE 601.00 TO NODE 605.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

t4

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 322.00  
ELEVATION DATA: UPSTREAM(FEET) = 359.50 DOWNSTREAM(FEET) = 349.30

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.108  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.620  
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	C	1.50	0.25	0.100	69	6.11
COMMERCIAL	D	1.00	0.20	0.100	75	6.11

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA RUNOFF(CFS) = 8.09  
TOTAL AREA(ACRES) = 2.50 PEAK FLOW RATE(CFS) = 8.09

\*\*\*\*\*  
FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81  
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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

E5

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=====
MAINLINE Tc(MIN.) = 6.11
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.620
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/   SCS SOIL   AREA   Fp   Ap   SCS
LAND USE            GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL          C       1.20   0.25  0.100 69
COMMERCIAL          D       0.20   0.20  0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.24
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.40   SUBAREA RUNOFF(CFS) = 4.53
EFFECTIVE AREA(ACRES) = 3.90   AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.23   AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 3.9   PEAK FLOW RATE(CFS) = 12.62

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*****
FLOW PROCESS FROM NODE 605.00 TO NODE 604.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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Private Sd.

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=====
ELEVATION DATA: UPSTREAM(FEET) = 340.00 DOWNSTREAM(FEET) = 330.00
FLOW LENGTH(FEET) = 485.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.14
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 12.62
PIPE TRAVEL TIME(MIN.) = 0.88 Tc(MIN.) = 6.99
LONGEST FLOWPATH FROM NODE 601.00 TO NODE 604.00 = 807.00 FEET.

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*****
FLOW PROCESS FROM NODE 604.00 TO NODE 604.00 IS CODE = 81
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>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

E6

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=====
MAINLINE Tc(MIN.) = 6.99
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.350
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/   SCS SOIL   AREA   Fp   Ap   SCS
LAND USE            GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL          C       0.20   0.25  0.100 69
COMMERCIAL          D       2.00   0.20  0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.20   SUBAREA RUNOFF(CFS) = 6.59
EFFECTIVE AREA(ACRES) = 6.10   AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.22   AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 6.1   PEAK FLOW RATE(CFS) = 18.27

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*****
FLOW PROCESS FROM NODE 604.00 TO NODE 604.00 IS CODE = 1
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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

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=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.99

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PRLNT10

RAINFALL INTENSITY(INCH/HR) = 3.35  
 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 6.10  
 TOTAL STREAM AREA(ACRES) = 6.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.27

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	9.60	10.45	2.661	0.21( 0.02)	0.10	3.5	601.00
2	18.27	6.99	3.350	0.22( 0.02)	0.10	6.1	601.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	26.37	6.99	3.350	0.22( 0.02)	0.10	8.4	601.00
2	24.08	10.45	2.661	0.22( 0.02)	0.10	9.6	601.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.37 Tc(MIN.) = 6.99  
 EFFECTIVE AREA(ACRES) = 8.44 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 9.6  
 LONGEST FLOWPATH FROM NODE 601.00 TO NODE 604.00 = 1420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 604.00 TO NODE 605.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

*Private S.d.*

=====

ELEVATION DATA: UPSTREAM(FEET) = 330.00 DOWNSTREAM(FEET) = 320.00  
 FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 16.32  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 26.37  
 PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 7.17  
 LONGEST FLOWPATH FROM NODE 601.00 TO NODE 605.00 = 1595.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 7.17  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.302  
 SUBAREA LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL D 0.30 0.20 0.100 75  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 0.89

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E7

EFFECTIVE AREA(ACRES) = 8.74 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 9.9 PEAK FLOW RATE(CFS) = 26.37  
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*

FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

E8

MAINLINE Tc(MIN.) = 7.17  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.302  
 SUBAREA LOSS RATE DATA(AMC II):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	C	0.60	0.25	0.100	69
COMMERCIAL	D	1.30	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.22  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 5.61  
 EFFECTIVE AREA(ACRES) = 10.64 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 11.8 PEAK FLOW RATE(CFS) = 31.41

\*\*\*\*\*

FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

E9

MAINLINE Tc(MIN.) = 7.17  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.302  
 SUBAREA LOSS RATE DATA(AMC II):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	C	1.00	0.25	0.100	69
COMMERCIAL	D	0.20	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.24  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 3.54  
 EFFECTIVE AREA(ACRES) = 11.84 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 13.0 PEAK FLOW RATE(CFS) = 34.95

Q10  
 ← total  
 to det.  
 tank

\*\*\*\*\*

FLOW PROCESS FROM NODE 605.00 TO NODE 403.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap (ACRES)	Ae (ACRES)	HEADWATER NODE
1	34.95	7.17	3.302	0.22( 0.02)	0.10	11.8	601.00
2	30.57	10.63	2.634	0.22( 0.02)	0.10	13.0	601.00

LONGEST FLOWPATH FROM NODE 601.00 TO NODE 403.00 = 1595.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap (ACRES)	Ae (ACRES)	HEADWATER NODE
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1 441.43 11.33 2.541 0.20( 0.10) 0.50 197.6 102.00  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 403.00 = 2845.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	401.52	7.17	3.302	0.20( 0.09)	0.46	136.9	601.00
2	460.89	10.63	2.634	0.20( 0.09)	0.47	198.5	601.00
3	470.90	11.33	2.541	0.20( 0.09)	0.47	210.6	102.00
TOTAL AREA(ACRES) =			210.6				

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 470.90 Tc(MIN.) = 11.326  
EFFECTIVE AREA(ACRES) = 210.60 AREA-AVERAGED Fm(INCH/HR) = 0.09  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47  
TOTAL AREA(ACRES) = 210.6  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 403.00 = 2845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

04 (offsite)

MAINLINE Tc(MIN.) = 11.33

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.541

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	C	0.30	0.25	0.850	69
PUBLIC PARK	D	0.10	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.24

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850

SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.84

EFFECTIVE AREA(ACRES) = 211.00 AREA-AVERAGED Fm(INCH/HR) = 0.09

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47

TOTAL AREA(ACRES) = 211.0 PEAK FLOW RATE(CFS) = 470.90

NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

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FLOW PROCESS FROM NODE 403.00 TO NODE 410.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

Join Pipe 60" SD

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

1020 x 6" SD

ELEVATION DATA: UPSTREAM(FEET) = 305.30 DOWNSTREAM(FEET) = 303.00

FLOW LENGTH(FEET) = 72.00 MANNING'S N = 0.013

ASSUME FULL-FLOWING PIPELINE

PIPE-FLOW VELOCITY(FEET/SEC.) = 23.98

PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)

GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 470.90

PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 11.38

LONGEST FLOWPATH FROM NODE 102.00 TO NODE 410.00 = 2917.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 211.0 TC(MIN.) = 11.38  
EFFECTIVE AREA(ACRES) = 211.00 AREA-AVERAGED Fm(INCH/HR) = 0.09  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.472  
PEAK FLOW RATE(CFS) = 470.90

PRLNT10

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	401.52	7.22	3.289	0.20( 0.09)	0.46	137.3	601.00
2	460.89	10.69	2.627	0.20( 0.09)	0.47	198.9	601.00
3	470.90	11.38	2.535	0.20( 0.09)	0.47	211.0	102.00

=====

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END OF RATIONAL METHOD ANALYSIS

↑

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 RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
 (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
 \* Laguna Niguel Town Center \*  
 \* Proposed Condition Hydrology Analysis \*  
 \* 25-year storm event \*  
 \*\*\*\*\*

FILE NAME: PRLNT25.DAT  
 TIME/DATE OF STUDY: 17:17 09/25/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00  
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00  
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
 \*DATA BANK RAINFALL USED\*  
 \*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/ SIDE / SIDE/ WAY	PARK- HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
 1. Relative Flow-Depth = 0.00 FEET  
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
 2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
 \*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
 OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
 \*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
 =====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 298.00  
 ELEVATION DATA: UPSTREAM(FEET) = 357.60 DOWNSTREAM(FEET) = 349.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.033

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\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.337  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 COMMERCIAL D 0.70 0.20 0.100 75 6.03  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 2.72  
 TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 2.72

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 203.00 IS CODE = 61

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 349.00 DOWNSTREAM ELEVATION(FEET) = 338.00  
 STREET LENGTH(FEET) = 435.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 27.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.53  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.34  
 HALFSTREET FLOOD WIDTH(FEET) = 10.83  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.51  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.20  
 STREET FLOW TRAVEL TIME(MIN.) = 2.07 Tc(MIN.) = 8.10

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.672  
 SUBAREA LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL D 1.10 0.20 0.100 75  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 3.62  
 EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 5.92

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.15  
 FLOW VELOCITY(FEET/SEC.) = 3.71 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.37  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 203.00 = 733.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 203.00 TO NODE 305.00 IS CODE = 61

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

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UPSTREAM ELEVATION(FEET) = 338.00 DOWNSTREAM ELEVATION(FEET) = 327.00  
STREET LENGTH(FEET) = 235.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 27.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.92  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 10.67  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.71  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.60  
STREET FLOW TRAVEL TIME(MIN.) = 0.83 Tc(MIN.) = 8.93  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.474  
SUBAREA AREA(ACRES) = 0.00 SUBAREA RUNOFF(CFS) = 0.00  
EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 5.92  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.67  
FLOW VELOCITY(FEET/SEC.) = 4.71 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.60  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 305.00 = 968.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.93  
RAINFALL INTENSITY(INCH/HR) = 3.47  
AREA-AVERAGED Fm(INCH/HR) = 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.10  
EFFECTIVE STREAM AREA(ACRES) = 1.80  
TOTAL STREAM AREA(ACRES) = 1.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.92

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 301.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 357.60 DOWNSTREAM(FEET) = 349.20

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.444

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\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.179  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 COMMERCIAL D 2.80 0.20 0.100 75 6.44  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 10.48  
 TOTAL AREA(ACRES) = 2.80 PEAK FLOW RATE(CFS) = 10.48

\*\*\*\*\*

FLOW PROCESS FROM NODE 301.00 TO NODE 305.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 349.20 DOWNSTREAM(FEET) = 327.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 527.00 CHANNEL SLOPE = 0.0421  
 CHANNEL BASE(FEET) = 70.00 "Z" FACTOR = 36.000  
 MANNING'S FACTOR = 0.016 MAXIMUM DEPTH(FEET) = 2.00

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.379  
 SUBAREA LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL D 2.20 0.20 0.100 75  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.82  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.99  
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 2.94  
 Tc(MIN.) = 9.38  
 SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 6.65  
 EFFECTIVE AREA(ACRES) = 5.00 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 5.0 PEAK FLOW RATE(CFS) = 15.11

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.07 FLOW VELOCITY(FEET/SEC.) = 3.17  
 LONGEST FLOWPATH FROM NODE 103.00 TO NODE 305.00 = 857.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.38  
 RAINFALL INTENSITY(INCH/HR) = 3.38  
 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 5.00  
 TOTAL STREAM AREA(ACRES) = 5.00  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.11

\*\* CONFLUENCE DATA \*\*

STREAM	Q	Tc	Intensity	Fp(Fm)	Ap	Ae	HEADWATER
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NUMBER	(CFS)	(MIN.)	(INCH/HR)	(INCH/HR)	(ACRES)	NODE
1	5.92	8.93	3.474	0.20( 0.02)	0.10	1.8 102.00
2	15.11	9.38	3.379	0.20( 0.02)	0.10	5.0 103.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap (ACRES)	Ae (ACRES)	HEADWATER NODE
1	20.71	8.93	3.474	0.20( 0.02)	0.10	6.6	102.00
2	20.87	9.38	3.379	0.20( 0.02)	0.10	6.8	103.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 20.87 Tc(MIN.) = 9.38  
 EFFECTIVE AREA(ACRES) = 6.80 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 6.8  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 305.00 = 968.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 400.00 TO NODE 400.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<  
=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
 TC(MIN.) = 10.00 RAINFALL INTENSITY(INCH/HR) = 3.26  
 EFFECTIVE AREA(ACRES) = 190.00  
 TOTAL AREA(ACRES) = 190.00 PEAK FLOW RATE(CFS) = 485.00  
 AREA-AVERAGED Fm(INCH/HR) = 0.10 AREA-AVERAGED Fp(INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.50  
 NOTE: EFFECTIVE AREA IS USED AS THE TOTAL CONTRIBUTING AREA FOR ALL  
 CONFLUENCE ANALYSES.

\*\*\*\*\*

FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 41

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 361.50 DOWNSTREAM(FEET) = 333.30  
 FLOW LENGTH(FEET) = 942.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 24.70  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 485.00  
 PIPE TRAVEL TIME(MIN.) = 0.64 Tc(MIN.) = 10.64  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 401.00 = 1910.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 81

-----  
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
=====

MAINLINE Tc(MIN.) = 10.64  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.147  
 SUBAREA LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS

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LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	C	0.70	0.25	0.400	69
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	D	0.70	0.20	0.400	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400					
SUBAREA AREA(ACRES) =		1.40	SUBAREA RUNOFF(CFS) =		3.85
EFFECTIVE AREA(ACRES) =		191.40	AREA-AVERAGED Fm(INCH/HR) =		0.10
AREA-AVERAGED Fp(INCH/HR) =		0.20	AREA-AVERAGED Ap =		0.50
TOTAL AREA(ACRES) =		191.4	PEAK FLOW RATE(CFS) =		524.83

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.64  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.147  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	C	1.10	0.25	0.400	69
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	D	1.00	0.20	0.400	75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400					
SUBAREA AREA(ACRES) =		2.10	SUBAREA RUNOFF(CFS) =		5.78
EFFECTIVE AREA(ACRES) =		193.50	AREA-AVERAGED Fm(INCH/HR) =		0.10
AREA-AVERAGED Fp(INCH/HR) =		0.20	AREA-AVERAGED Ap =		0.50
TOTAL AREA(ACRES) =		193.5	PEAK FLOW RATE(CFS) =		530.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 402.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 333.30 DOWNSTREAM(FEET) = 312.20  
 FLOW LENGTH(FEET) = 705.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 27.02  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 530.61  
 PIPE TRAVEL TIME(MIN.) = 0.43 Tc(MIN.) = 11.07  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 402.00 = 2615.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 402.00 TO NODE 402.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 11.07  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.076  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN

PRLNT25

RESIDENTIAL  
 "8-10 DWELLINGS/ACRE" C 1.00 0.25 0.400 69  
 RESIDENTIAL  
 "8-10 DWELLINGS/ACRE" D 3.10 0.20 0.400 75  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.21  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400  
 SUBAREA AREA(ACRES) = 4.10 SUBAREA RUNOFF(CFS) = 11.04  
 EFFECTIVE AREA(ACRES) = 197.60 AREA-AVERAGED Fm(INCH/HR) = 0.10  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
 TOTAL AREA(ACRES) = 197.6 PEAK FLOW RATE(CFS) = 530.61  
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*

FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 41

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 312.20 DOWNSTREAM(FEET) = 305.30  
 FLOW LENGTH(FEET) = 230.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 27.02  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 530.61  
 PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 11.21  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 403.00 = 2845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 10

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>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
 ELEVATION DATA: UPSTREAM(FEET) = 344.00 DOWNSTREAM(FEET) = 329.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.738  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.462  
 SUBAREA Tc AND LOSS RATE DATA(AMC II):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	D	2.50	0.20	0.100	75	5.74

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 9.99  
 TOTAL AREA(ACRES) = 2.50 PEAK FLOW RATE(CFS) = 9.99

\*\*\*\*\*

FLOW PROCESS FROM NODE 502.00 TO NODE 503.00 IS CODE = 61

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 329.00 DOWNSTREAM ELEVATION(FEET) = 321.00
STREET LENGTH(FEET) = 22.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 25.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.59
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.31
HALFSTREET FLOOD WIDTH(FEET) = 9.15
AVERAGE FLOW VELOCITY(FEET/SEC.) = 12.13
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 3.75
STREET FLOW TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 5.77
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.449

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL D 0.80 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 3.19
EFFECTIVE AREA(ACRES) = 3.30 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 3.3 PEAK FLOW RATE(CFS) = 13.15

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 9.64
FLOW VELOCITY(FEET/SEC.) = 12.56 DEPTH\*VELOCITY(FT\*FT/SEC.) = 4.01
LONGEST FLOWPATH FROM NODE 501.00 TO NODE 503.00 = 352.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 601.00 TO NODE 602.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00
ELEVATION DATA: UPSTREAM(FEET) = 359.50 DOWNSTREAM(FEET) = 356.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.917
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.719
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL C 0.70 0.25 0.100 69 7.92
COMMERCIAL D 2.00 0.20 0.100 75 7.92
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.21
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 8.99

PRLNT25

TOTAL AREA(ACRES) = 2.70 PEAK FLOW RATE(CFS) = 8.99

\*\*\*\*\*

FLOW PROCESS FROM NODE 602.00 TO NODE 603.00 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

UPSTREAM ELEVATION(FEET) = 356.50 DOWNSTREAM ELEVATION(FEET) = 355.60  
STREET LENGTH(FEET) = 49.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 25.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.80

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.44

HALFSTREET FLOOD WIDTH(FEET) = 15.89

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.71

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.65

STREET FLOW TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 8.14

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.662

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.50	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 0.50 SUBAREA RUNOFF(CFS) = 1.64

EFFECTIVE AREA(ACRES) = 3.20 AREA-AVERAGED Fm(INCH/HR) = 0.02

AREA-AVERAGED Fp(INCH/HR) = 0.21 AREA-AVERAGED Ap = 0.10

TOTAL AREA(ACRES) = 3.2 PEAK FLOW RATE(CFS) = 10.48

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.45 HALFSTREET FLOOD WIDTH(FEET) = 16.28

FLOW VELOCITY(FEET/SEC.) = 3.79 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.71

LONGEST FLOWPATH FROM NODE 601.00 TO NODE 603.00 = 379.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 603.00 TO NODE 603.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.14

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.662

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.30	0.20	0.100	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 0.98

PRLNT25

EFFECTIVE AREA(ACRES) = 3.50 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.21 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 11.47

\*\*\*\*\*
FLOW PROCESS FROM NODE 603.00 TO NODE 604.00 IS CODE = 31
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 345.00 DOWNSTREAM(FEET) = 330.00
FLOW LENGTH(FEET) = 1041.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.71
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.47
PIPE TRAVEL TIME(MIN.) = 2.25 Tc(MIN.) = 10.39
LONGEST FLOWPATH FROM NODE 601.00 TO NODE 604.00 = 1420.00 FEET.

\*\*\*\*\*
FLOW PROCESS FROM NODE 604.00 TO NODE 604.00 IS CODE = 1
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.39
RAINFALL INTENSITY(INCH/HR) = 3.19
AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.21
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 3.50
TOTAL STREAM AREA(ACRES) = 3.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.47

\*\*\*\*\*
FLOW PROCESS FROM NODE 601.00 TO NODE 605.00 IS CODE = 21
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 322.00
ELEVATION DATA: UPSTREAM(FEET) = 359.50 DOWNSTREAM(FEET) = 349.30

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.108
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.307

SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL C 1.50 0.25 0.100 69 6.11
COMMERCIAL D 1.00 0.20 0.100 75 6.11
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 9.64
TOTAL AREA(ACRES) = 2.50 PEAK FLOW RATE(CFS) = 9.64

\*\*\*\*\*
FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 =====

MAINLINE Tc(MIN.) = 6.11  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.307  
 SUBAREA LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL C 1.20 0.25 0.100 69  
 COMMERCIAL D 0.20 0.20 0.100 75  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.24  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 5.40  
 EFFECTIVE AREA(ACRES) = 3.90 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.23 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 3.9 PEAK FLOW RATE(CFS) = 15.04

\*\*\*\*\*

FLOW PROCESS FROM NODE 605.00 TO NODE 604.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 340.00 DOWNSTREAM(FEET) = 330.00  
 FLOW LENGTH(FEET) = 485.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.70  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 15.04  
 PIPE TRAVEL TIME(MIN.) = 0.83 Tc(MIN.) = 6.94  
 LONGEST FLOWPATH FROM NODE 601.00 TO NODE 604.00 = 807.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 604.00 TO NODE 604.00 IS CODE = 81

-----  
 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 =====

MAINLINE Tc(MIN.) = 6.94  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.006  
 SUBAREA LOSS RATE DATA(AMC II):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL C 0.20 0.25 0.100 69  
 COMMERCIAL D 2.00 0.20 0.100 75  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 7.89  
 EFFECTIVE AREA(ACRES) = 6.10 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 6.1 PEAK FLOW RATE(CFS) = 21.87

\*\*\*\*\*

FLOW PROCESS FROM NODE 604.00 TO NODE 604.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 6.94  
 RAINFALL INTENSITY(INCH/HR) = 4.01  
 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 6.10  
 TOTAL STREAM AREA(ACRES) = 6.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 21.87

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.47	10.39	3.189	0.21( 0.02)	0.10	3.5	601.00
2	21.87	6.94	4.006	0.22( 0.02)	0.10	6.1	601.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	31.51	6.94	4.006	0.22( 0.02)	0.10	8.4	601.00
2	28.85	10.39	3.189	0.22( 0.02)	0.10	9.6	601.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 31.51 Tc(MIN.) = 6.94  
 EFFECTIVE AREA(ACRES) = 8.44 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 9.6  
 LONGEST FLOWPATH FROM NODE 601.00 TO NODE 604.00 = 1420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 604.00 TO NODE 605.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 330.00 DOWNSTREAM(FEET) = 320.00  
 FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 16.85  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 31.51  
 PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 7.11  
 LONGEST FLOWPATH FROM NODE 601.00 TO NODE 605.00 = 1595.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 7.11  
 \* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.951  
 SUBAREA LOSS RATE DATA(AMC II):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.30	0.20	0.100	75

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100



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SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 1.06
EFFECTIVE AREA(ACRES) = 8.74 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 9.9 PEAK FLOW RATE(CFS) = 31.51
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*
FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.11
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.951
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL C 0.60 0.25 0.100 69
COMMERCIAL D 1.30 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.22
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 6.72
EFFECTIVE AREA(ACRES) = 10.64 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 11.8 PEAK FLOW RATE(CFS) = 37.62

\*\*\*\*\*
FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.11
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.951
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL C 1.00 0.25 0.100 69
COMMERCIAL D 0.20 0.20 0.100 75
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.24
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 4.24
EFFECTIVE AREA(ACRES) = 11.84 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 13.0 PEAK FLOW RATE(CFS) = 41.86

\*\*\*\*\*
FLOW PROCESS FROM NODE 605.00 TO NODE 403.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 41.86 7.11 3.951 0.22( 0.02) 0.10 11.8 601.00
2 36.70 10.56 3.159 0.22( 0.02) 0.10 13.0 601.00
LONGEST FLOWPATH FROM NODE 601.00 TO NODE 403.00 = 1595.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER

PRLNT25

NUMBER	(CFS)	(MIN.)	(INCH/HR)	(INCH/HR)	(ACRES)	NODE
1	530.61	11.21	3.054	0.20( 0.10)	0.50	102.00

LONGEST FLOWPATH FROM NODE 102.00 TO NODE 403.00 = 2845.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap (ACRES)	Ae (ACRES)	HEADWATER NODE
1	480.73	7.11	3.951	0.20( 0.09)	0.46	137.2	601.00
2	554.35	10.56	3.159	0.20( 0.09)	0.47	199.2	601.00
3	566.09	11.21	3.054	0.20( 0.09)	0.47	210.6	102.00
TOTAL AREA(ACRES) =		210.6					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 566.09 Tc(MIN.) = 11.212  
EFFECTIVE AREA(ACRES) = 210.60 AREA-AVERAGED Fm(INCH/HR) = 0.09  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47  
TOTAL AREA(ACRES) = 210.6  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 403.00 = 2845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 11.21

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.054

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	C	0.30	0.25	0.850	69
PUBLIC PARK	D	0.10	0.20	0.850	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.24

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850

SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.03

EFFECTIVE AREA(ACRES) = 211.00 AREA-AVERAGED Fm(INCH/HR) = 0.09

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47

TOTAL AREA(ACRES) = 211.0 PEAK FLOW RATE(CFS) = 566.09

NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*

FLOW PROCESS FROM NODE 403.00 TO NODE 410.00 IS CODE = 41

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 305.30 DOWNSTREAM(FEET) = 303.00

FLOW LENGTH(FEET) = 72.00 MANNING'S N = 0.013

ASSUME FULL-FLOWING PIPELINE

PIPE-FLOW VELOCITY(FEET/SEC.) = 28.83

PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)

GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 566.09

PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 11.25

LONGEST FLOWPATH FROM NODE 102.00 TO NODE 410.00 = 2917.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 211.0 TC(MIN.) = 11.25

EFFECTIVE AREA(ACRES) = 211.00 AREA-AVERAGED Fm(INCH/HR) = 0.09

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.472

PEAK FLOW RATE(CFS) = 566.09

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	480.73	7.16	3.936	0.20( 0.09)	0.46	137.6	601.00
2	554.35	10.61	3.152	0.20( 0.09)	0.47	199.6	601.00
3	566.09	11.25	3.048	0.20( 0.09)	0.47	211.0	102.00

=====  
=====

END OF RATIONAL METHOD ANALYSIS



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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)  
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Ver. 23.0 Release Date: 07/01/2016 License ID 1355

Analysis prepared by:

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Irvine, CA

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* Laguna Niguel Town Center \*  
\* Proposed Condition Hydrology Analysis \*  
\* 100-year storm event \*  
\*\*\*\*\*

FILE NAME: PRLNT100.DAT  
TIME/DATE OF STUDY: 17:30 09/25/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
\*DATA BANK RAINFALL USED\*  
\*ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/ SIDE / SIDE/ WAY	PARK- HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:  
1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*  
\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*  
FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 298.00  
ELEVATION DATA: UPSTREAM(FEET) = 357.60 DOWNSTREAM(FEET) = 349.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.033

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\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.556  
 SUBAREA Tc AND LOSS RATE DATA(AMC III):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 COMMERCIAL D 0.70 0.20 0.100 91 6.03  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 3.49  
 TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 3.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 203.00 IS CODE = 61

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 349.00 DOWNSTREAM ELEVATION(FEET) = 338.00  
 STREET LENGTH(FEET) = 435.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 27.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0160  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.83  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.37  
 HALFSTREET FLOOD WIDTH(FEET) = 12.04  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.72  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.36  
 STREET FLOW TRAVEL TIME(MIN.) = 1.95 Tc(MIN.) = 7.98  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.732

SUBAREA LOSS RATE DATA(AMC III):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL D 1.10 0.20 0.100 91  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 4.67  
 EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 7.63

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.46  
 FLOW VELOCITY(FEET/SEC.) = 3.95 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.56  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 203.00 = 733.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 203.00 TO NODE 305.00 IS CODE = 61

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STANDARD CURB SECTION USED)<<<<<

=====

PRLNT100

UPSTREAM ELEVATION(FEET) = 338.00 DOWNSTREAM ELEVATION(FEET) = 327.00  
STREET LENGTH(FEET) = 235.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 27.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.63  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.36  
HALFSTREET FLOOD WIDTH(FEET) = 11.88  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.99  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.82  
STREET FLOW TRAVEL TIME(MIN.) = 0.78 Tc(MIN.) = 8.77  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.485  
SUBAREA AREA(ACRES) = 0.00 SUBAREA RUNOFF(CFS) = 0.00  
EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 7.63  
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 11.88  
FLOW VELOCITY(FEET/SEC.) = 4.99 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.82  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 305.00 = 968.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.77  
RAINFALL INTENSITY(INCH/HR) = 4.48  
AREA-AVERAGED Fm(INCH/HR) = 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.20  
AREA-AVERAGED Ap = 0.10  
EFFECTIVE STREAM AREA(ACRES) = 1.80  
TOTAL STREAM AREA(ACRES) = 1.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.63

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 301.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<  
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
ELEVATION DATA: UPSTREAM(FEET) = 357.60 DOWNSTREAM(FEET) = 349.20

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.444

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\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.350  
 SUBAREA Tc AND LOSS RATE DATA(AMC III):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)  
 COMMERCIAL D 2.80 0.20 0.100 91 6.44  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 13.43  
 TOTAL AREA(ACRES) = 2.80 PEAK FLOW RATE(CFS) = 13.43

\*\*\*\*\*

FLOW PROCESS FROM NODE 301.00 TO NODE 305.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 349.20 DOWNSTREAM(FEET) = 327.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 527.00 CHANNEL SLOPE = 0.0421  
 CHANNEL BASE(FEET) = 70.00 "Z" FACTOR = 36.000  
 MANNING'S FACTOR = 0.016 MAXIMUM DEPTH(FEET) = 2.00  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.395  
 SUBAREA LOSS RATE DATA(AMC III):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL D 2.20 0.20 0.100 91  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.75  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.33  
 AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 2.64  
 Tc(MIN.) = 9.08  
 SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 8.66  
 EFFECTIVE AREA(ACRES) = 5.00 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 5.0 PEAK FLOW RATE(CFS) = 19.69

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 3.41  
 LONGEST FLOWPATH FROM NODE 103.00 TO NODE 305.00 = 857.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.08  
 RAINFALL INTENSITY(INCH/HR) = 4.39  
 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 5.00  
 TOTAL STREAM AREA(ACRES) = 5.00  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.69

\*\* CONFLUENCE DATA \*\*

STREAM	Q	Tc	Intensity	Fp(Fm)	Ap	Ae	HEADWATER
--------	---	----	-----------	--------	----	----	-----------

NUMBER	(CFS)	(MIN.)	(INCH/HR)	(INCH/HR)	(ACRES)	NODE
1	7.63	8.77	4.485	0.20( 0.02)	0.10	1.8 102.00
2	19.69	9.08	4.395	0.20( 0.02)	0.10	5.0 103.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap (ACRES)	Ae (ACRES)	HEADWATER NODE
1	27.03	8.77	4.485	0.20( 0.02)	0.10	6.6	102.00
2	27.17	9.08	4.395	0.20( 0.02)	0.10	6.8	103.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 27.17 Tc(MIN.) = 9.08  
 EFFECTIVE AREA(ACRES) = 6.80 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 6.8  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 305.00 = 968.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 400.00 TO NODE 400.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN.) = 10.00 RAINFALL INTENSITY(INCH/HR) = 4.16  
 EFFECTIVE AREA(ACRES) = 190.00  
 TOTAL AREA(ACRES) = 190.00 PEAK FLOW RATE(CFS) = 640.00  
 AREA-AVERAGED Fm(INCH/HR) = 0.10 AREA-AVERAGED Fp(INCH/HR) = 0.20  
 AREA-AVERAGED Ap = 0.50

NOTE: EFFECTIVE AREA IS USED AS THE TOTAL CONTRIBUTING AREA FOR ALL  
CONFLUENCE ANALYSES.

\*\*\*\*\*

FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 361.50 DOWNSTREAM(FEET) = 333.30  
 FLOW LENGTH(FEET) = 942.00 MANNING'S N = 0.013  
 ASSUME FULL-FLOWING PIPELINE  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 32.59  
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
 GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 640.00  
 PIPE TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 10.48  
 LONGEST FLOWPATH FROM NODE 102.00 TO NODE 401.00 = 1910.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.48  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.049  
 SUBAREA LOSS RATE DATA(AMC III):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS



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LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	C	0.70	0.25	0.400	86
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	D	0.70	0.20	0.400	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400  
SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 4.99  
EFFECTIVE AREA(ACRES) = 191.40 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
TOTAL AREA(ACRES) = 191.4 PEAK FLOW RATE(CFS) = 680.20

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 401.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.48  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.049  
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	C	1.10	0.25	0.400	86
RESIDENTIAL					
"8-10 DWELLINGS/ACRE"	D	1.00	0.20	0.400	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400  
SUBAREA AREA(ACRES) = 2.10 SUBAREA RUNOFF(CFS) = 7.48  
EFFECTIVE AREA(ACRES) = 193.50 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50  
TOTAL AREA(ACRES) = 193.5 PEAK FLOW RATE(CFS) = 687.68

\*\*\*\*\*

FLOW PROCESS FROM NODE 401.00 TO NODE 402.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 333.30 DOWNSTREAM(FEET) = 312.20  
FLOW LENGTH(FEET) = 705.00 MANNING'S N = 0.013  
ASSUME FULL-FLOWING PIPELINE  
PIPE-FLOW VELOCITY(FEET/SEC.) = 35.02  
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)  
GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 687.68  
PIPE TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 10.82  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 402.00 = 2615.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 402.00 TO NODE 402.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.82  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.976  
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN

PRLNT100

RESIDENTIAL

"8-10 DWELLINGS/ACRE" C 1.00 0.25 0.400 86

RESIDENTIAL

"8-10 DWELLINGS/ACRE" D 3.10 0.20 0.400 91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.21

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.400

SUBAREA AREA(ACRES) = 4.10 SUBAREA RUNOFF(CFS) = 14.36

EFFECTIVE AREA(ACRES) = 197.60 AREA-AVERAGED Fm(INCH/HR) = 0.10

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.50

TOTAL AREA(ACRES) = 197.6 PEAK FLOW RATE(CFS) = 689.42

\*\*\*\*\*

FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 41

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 312.20 DOWNSTREAM(FEET) = 305.30

FLOW LENGTH(FEET) = 230.00 MANNING'S N = 0.013

ASSUME FULL-FLOWING PIPELINE

PIPE-FLOW VELOCITY(FEET/SEC.) = 35.11

PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)

GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 689.42

PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 10.93

LONGEST FLOWPATH FROM NODE 102.00 TO NODE 403.00 = 2845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 10

-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00

ELEVATION DATA: UPSTREAM(FEET) = 344.00 DOWNSTREAM(FEET) = 329.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.738

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.718

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	D	2.50	0.20	0.100	91	5.74

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA RUNOFF(CFS) = 12.82

TOTAL AREA(ACRES) = 2.50 PEAK FLOW RATE(CFS) = 12.82

\*\*\*\*\*

FLOW PROCESS FROM NODE 502.00 TO NODE 503.00 IS CODE = 61

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

PRLNT100

=====

UPSTREAM ELEVATION(FEET) = 329.00 DOWNSTREAM ELEVATION(FEET) = 321.00  
 STREET LENGTH(FEET) = 22.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 25.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0160  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 14.87  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.33  
 HALFSTREET FLOOD WIDTH(FEET) = 10.22  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 12.78  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 4.23  
 STREET FLOW TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 5.77  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.702

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.80	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 4.09  
 EFFECTIVE AREA(ACRES) = 3.30 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 3.3 PEAK FLOW RATE(CFS) = 16.87

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 10.81  
 FLOW VELOCITY(FEET/SEC.) = 13.11 DEPTH\*VELOCITY(FT\*FT/SEC.) = 4.49  
 LONGEST FLOWPATH FROM NODE 501.00 TO NODE 503.00 = 352.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 601.00 TO NODE 602.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 330.00  
 ELEVATION DATA: UPSTREAM(FEET) = 359.50 DOWNSTREAM(FEET) = 356.50

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.917  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.755  
 SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	C	0.70	0.25	0.100	86	7.92
COMMERCIAL	D	2.00	0.20	0.100	91	7.92

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.21  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 11.50  
 TOTAL AREA(ACRES) = 2.70 PEAK FLOW RATE(CFS) = 11.50

PRLNT100

\*\*\*\*\*

FLOW PROCESS FROM NODE 602.00 TO NODE 603.00 IS CODE = 61

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 356.50 DOWNSTREAM ELEVATION(FEET) = 355.60
STREET LENGTH(FEET) = 49.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 25.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0160
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 12.55
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.48
HALFSTREET FLOOD WIDTH(FEET) = 17.45
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.97
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.89
STREET FLOW TRAVEL TIME(MIN.) = 0.21 Tc(MIN.) = 8.12

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.685

SUBAREA LOSS RATE DATA(AMC III):

Table with 6 columns: DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN. Includes rows for COMMERCIAL and summary statistics like SUBAREA AVERAGE PERVIOUS LOSS RATE, SUBAREA AREA, EFFECTIVE AREA, and TOTAL AREA.

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 17.94
FLOW VELOCITY(FEET/SEC.) = 4.03 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.95
LONGEST FLOWPATH FROM NODE 601.00 TO NODE 603.00 = 379.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 603.00 TO NODE 603.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 8.12
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.685
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/LAND USE, SCS SOIL GROUP, AREA (ACRES), Fp (INCH/HR), Ap (DECIMAL), SCS CN
COMMERCIAL D 0.30 0.20 0.100 91
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 1.26
EFFECTIVE AREA(ACRES) = 3.50 AREA-AVERAGED Fm(INCH/HR) = 0.02

PRLNT100

AREA-AVERAGED Fp(INCH/HR) = 0.21 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 14.69

\*\*\*\*\*

FLOW PROCESS FROM NODE 603.00 TO NODE 604.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 345.00 DOWNSTREAM(FEET) = 330.00  
FLOW LENGTH(FEET) = 1041.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.36  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 14.69  
PIPE TRAVEL TIME(MIN.) = 2.08 Tc(MIN.) = 10.20  
LONGEST FLOWPATH FROM NODE 601.00 TO NODE 604.00 = 1420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 604.00 TO NODE 604.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.20  
RAINFALL INTENSITY(INCH/HR) = 4.11  
AREA-AVERAGED Fm(INCH/HR) = 0.02  
AREA-AVERAGED Fp(INCH/HR) = 0.21  
AREA-AVERAGED Ap = 0.10  
EFFECTIVE STREAM AREA(ACRES) = 3.50  
TOTAL STREAM AREA(ACRES) = 3.50  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.69

\*\*\*\*\*

FLOW PROCESS FROM NODE 601.00 TO NODE 605.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 322.00  
ELEVATION DATA: UPSTREAM(FEET) = 359.50 DOWNSTREAM(FEET) = 349.30

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.108  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.517

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	C	1.50	0.25	0.100	86	6.11
COMMERCIAL	D	1.00	0.20	0.100	91	6.11

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.23  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA RUNOFF(CFS) = 12.36  
TOTAL AREA(ACRES) = 2.50 PEAK FLOW RATE(CFS) = 12.36

\*\*\*\*\*

FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
MAINLINE Tc(MIN.) = 6.11
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.517
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/   SCS SOIL   AREA      Fp        Ap        SCS
LAND USE            GROUP   (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL          C        1.20     0.25     0.100     86
COMMERCIAL          D        0.20     0.20     0.100     91
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.24
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.40     SUBAREA RUNOFF(CFS) = 6.92
EFFECTIVE AREA(ACRES) = 3.90     AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.23     AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 3.9     PEAK FLOW RATE(CFS) = 19.28

```

```

*****
FLOW PROCESS FROM NODE 605.00 TO NODE 604.00 IS CODE = 31
-----

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```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 340.00 DOWNSTREAM(FEET) = 330.00
FLOW LENGTH(FEET) = 485.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.15
ESTIMATED PIPE DIAMETER(INCH) = 21.00     NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 19.28
PIPE TRAVEL TIME(MIN.) = 0.80     Tc(MIN.) = 6.90
LONGEST FLOWPATH FROM NODE 601.00 TO NODE 604.00 = 807.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 604.00 TO NODE 604.00 IS CODE = 81
-----

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
MAINLINE Tc(MIN.) = 6.90
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.143
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/   SCS SOIL   AREA      Fp        Ap        SCS
LAND USE            GROUP   (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL          C        0.20     0.25     0.100     86
COMMERCIAL          D        2.00     0.20     0.100     91
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.20     SUBAREA RUNOFF(CFS) = 10.14
EFFECTIVE AREA(ACRES) = 6.10     AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.22     AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 6.1     PEAK FLOW RATE(CFS) = 28.11

```

```

*****
FLOW PROCESS FROM NODE 604.00 TO NODE 604.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.90

```

RAINFALL INTENSITY(INCH/HR) = 5.14  
 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22  
 AREA-AVERAGED Ap = 0.10  
 EFFECTIVE STREAM AREA(ACRES) = 6.10  
 TOTAL STREAM AREA(ACRES) = 6.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 28.11

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.69	10.20	4.113	0.21( 0.02)	0.10	3.5	601.00
2	28.11	6.90	5.143	0.22( 0.02)	0.10	6.1	601.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	40.56	6.90	5.143	0.22( 0.02)	0.10	8.5	601.00
2	37.15	10.20	4.113	0.22( 0.02)	0.10	9.6	601.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 40.56 Tc(MIN.) = 6.90  
 EFFECTIVE AREA(ACRES) = 8.47 AREA-AVERAGED Fm(INCH/HR) = 0.02  
 AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 9.6  
 LONGEST FLOWPATH FROM NODE 601.00 TO NODE 604.00 = 1420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 604.00 TO NODE 605.00 IS CODE = 31

-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 330.00 DOWNSTREAM(FEET) = 320.00  
 FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 18.10  
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 40.56  
 PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 7.07  
 LONGEST FLOWPATH FROM NODE 601.00 TO NODE 605.00 = 1595.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 7.07  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.075  
 SUBAREA LOSS RATE DATA(AMC III):  

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	0.30	0.20	0.100	91

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 0.30 SUBAREA RUNOFF(CFS) = 1.36

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EFFECTIVE AREA(ACRES) = 8.77 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 9.9 PEAK FLOW RATE(CFS) = 40.56
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*
FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.07
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.075
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL C 0.60 0.25 0.100 86
COMMERCIAL D 1.30 0.20 0.100 91
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.22
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 8.64
EFFECTIVE AREA(ACRES) = 10.67 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 11.8 PEAK FLOW RATE(CFS) = 48.53

\*\*\*\*\*
FLOW PROCESS FROM NODE 605.00 TO NODE 605.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.07
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.075
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL C 1.00 0.25 0.100 86
COMMERCIAL D 0.20 0.20 0.100 91
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.24
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 5.46
EFFECTIVE AREA(ACRES) = 11.87 AREA-AVERAGED Fm(INCH/HR) = 0.02
AREA-AVERAGED Fp(INCH/HR) = 0.22 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 13.0 PEAK FLOW RATE(CFS) = 53.98

\*\*\*\*\*
FLOW PROCESS FROM NODE 605.00 TO NODE 403.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE
1 53.98 7.07 5.075 0.22( 0.02) 0.10 11.9 601.00
2 47.42 10.36 4.075 0.22( 0.02) 0.10 13.0 601.00
LONGEST FLOWPATH FROM NODE 601.00 TO NODE 403.00 = 1595.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM Q Tc Intensity Fp(Fm) Ap Ae HEADWATER
NUMBER (CFS) (MIN.) (INCH/HR) (INCH/HR) (ACRES) NODE



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1 689.42 10.93 3.953 0.20( 0.10) 0.50 197.6 102.00  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 403.00 = 2845.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	629.56	7.07	5.075	0.20( 0.09)	0.46	139.6	601.00
2	721.93	10.36	4.075	0.20( 0.09)	0.47	200.4	601.00
3	735.42	10.93	3.953	0.20( 0.09)	0.47	210.6	102.00
TOTAL AREA(ACRES) =		210.6					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 735.42 Tc(MIN.) = 10.926  
EFFECTIVE AREA(ACRES) = 210.60 AREA-AVERAGED Fm(INCH/HR) = 0.09  
AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47  
TOTAL AREA(ACRES) = 210.6  
LONGEST FLOWPATH FROM NODE 102.00 TO NODE 403.00 = 2845.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 403.00 TO NODE 403.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 10.93

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.953

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	C	0.30	0.25	0.850	86
PUBLIC PARK	D	0.10	0.20	0.850	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.24

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850

SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.35

EFFECTIVE AREA(ACRES) = 211.00 AREA-AVERAGED Fm(INCH/HR) = 0.09

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.47

TOTAL AREA(ACRES) = 211.0 PEAK FLOW RATE(CFS) = 735.42

NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

\*\*\*\*\*

FLOW PROCESS FROM NODE 403.00 TO NODE 410.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 305.30 DOWNSTREAM(FEET) = 303.00

FLOW LENGTH(FEET) = 72.00 MANNING'S N = 0.013

ASSUME FULL-FLOWING PIPELINE

PIPE-FLOW VELOCITY(FEET/SEC.) = 37.45

PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)

GIVEN PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 735.42

PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 10.96

LONGEST FLOWPATH FROM NODE 102.00 TO NODE 410.00 = 2917.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 211.0 TC(MIN.) = 10.96

EFFECTIVE AREA(ACRES) = 211.00 AREA-AVERAGED Fm(INCH/HR) = 0.09

AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.472

PEAK FLOW RATE(CFS) = 735.42

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\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	629.56	7.10	5.060	0.20( 0.09)	0.46	140.0	601.00
2	721.93	10.39	4.068	0.20( 0.09)	0.47	200.8	601.00
3	735.42	10.96	3.947	0.20( 0.09)	0.47	211.0	102.00

=====  
=====

END OF RATIONAL METHOD ANALYSIS



APPENDIX 3  
HYDRAULIC  
CALCULATIONS  
(NOT INCLUDED IN  
CONCEPTUAL  
REPORT)

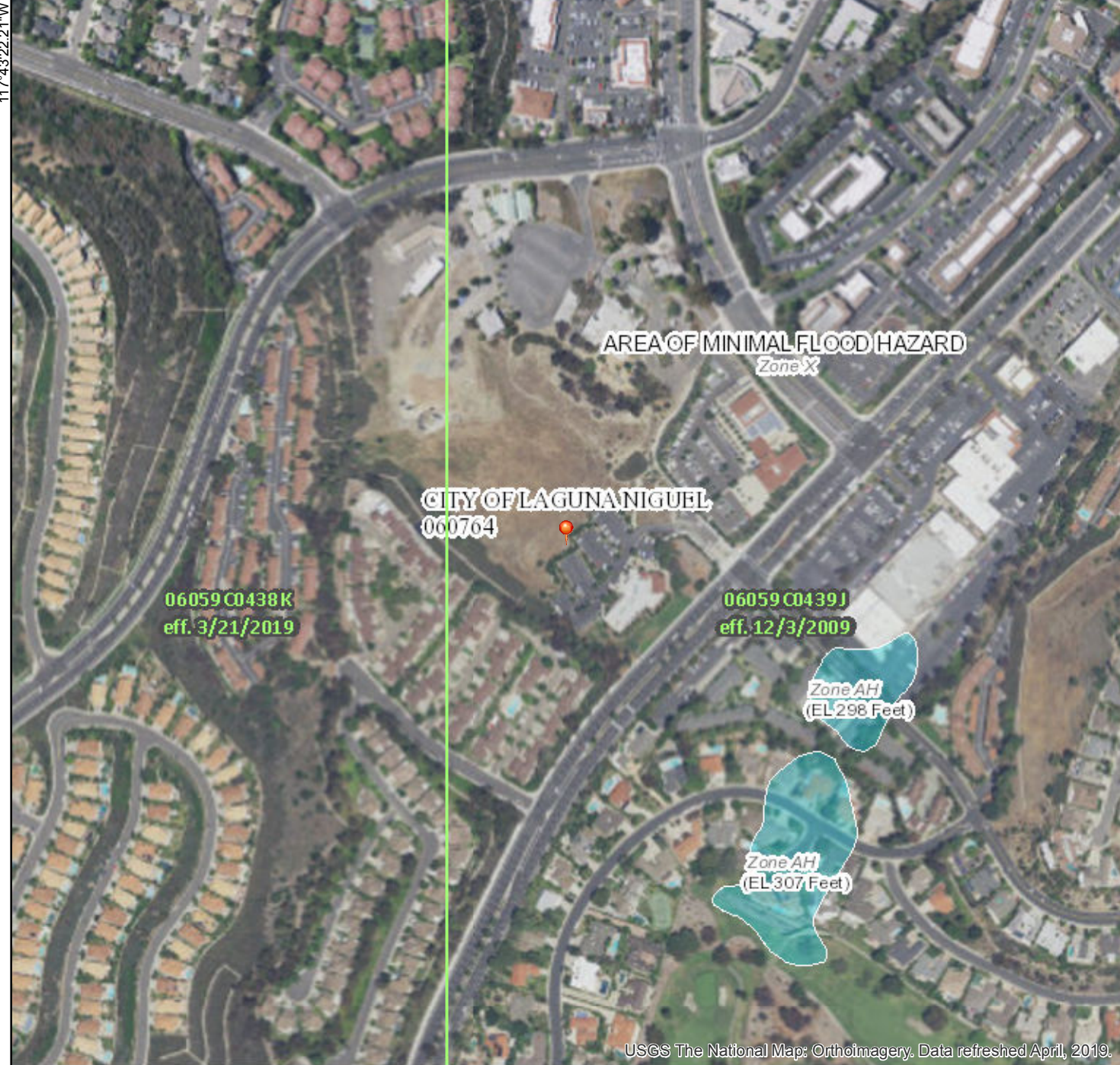
APPENDIX 4  
SUPPORTING  
DOCUMENTS

FIRM MAP  
SOILS MAP  
EXISTING 60" SD PLANS

# National Flood Hazard Layer FIRMette



33°31'37.85"N



## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

- |                                    |  |                                                                                                                                                                          |
|------------------------------------|--|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <b>SPECIAL FLOOD HAZARD AREAS</b>  |  | Without Base Flood Elevation (BFE)<br><i>Zone A, V, A99</i>                                                                                                              |
|                                    |  | With BFE or Depth <i>Zone AE, AO, AH, VE, AR</i>                                                                                                                         |
|                                    |  | Regulatory Floodway                                                                                                                                                      |
| <b>OTHER AREAS OF FLOOD HAZARD</b> |  | 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile <i>Zone X</i> |
|                                    |  | Future Conditions 1% Annual Chance Flood Hazard <i>Zone X</i>                                                                                                            |
|                                    |  | Area with Reduced Flood Risk due to Levee. See Notes. <i>Zone X</i>                                                                                                      |
|                                    |  | Area with Flood Risk due to Levee <i>Zone D</i>                                                                                                                          |
| <b>OTHER AREAS</b>                 |  | NO SCREEN Area of Minimal Flood Hazard <i>Zone X</i>                                                                                                                     |
|                                    |  | Effective LOMRs                                                                                                                                                          |
| <b>GENERAL STRUCTURES</b>          |  | Area of Undetermined Flood Hazard <i>Zone D</i>                                                                                                                          |
|                                    |  | Channel, Culvert, or Storm Sewer                                                                                                                                         |
|                                    |  | Levee, Dike, or Floodwall                                                                                                                                                |
| <b>OTHER FEATURES</b>              |  | 20.2 Cross Sections with 1% Annual Chance                                                                                                                                |
|                                    |  | 17.5 Water Surface Elevation                                                                                                                                             |
|                                    |  | Coastal Transect                                                                                                                                                         |
|                                    |  | Base Flood Elevation Line (BFE)                                                                                                                                          |
|                                    |  | Limit of Study                                                                                                                                                           |
| <b>MAP PANELS</b>                  |  | Jurisdiction Boundary                                                                                                                                                    |
|                                    |  | Coastal Transect Baseline                                                                                                                                                |
|                                    |  | Profile Baseline                                                                                                                                                         |
|                                    |  | Hydrographic Feature                                                                                                                                                     |
|                                    |  | Digital Data Available                                                                                                                                                   |
|                                    |  | No Digital Data Available                                                                                                                                                |
|                                    |  | Unmapped                                                                                                                                                                 |



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **9/24/2019 at 11:28:29 PM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

USGS The National Map: Orthoimagery. Data refreshed April, 2019.

0 250 500 1,000 1,500 2,000 Feet 1:6,000<sup>2-107</sup> 33°31'7.86"N

117°42'44.75"W



United States  
Department of  
Agriculture

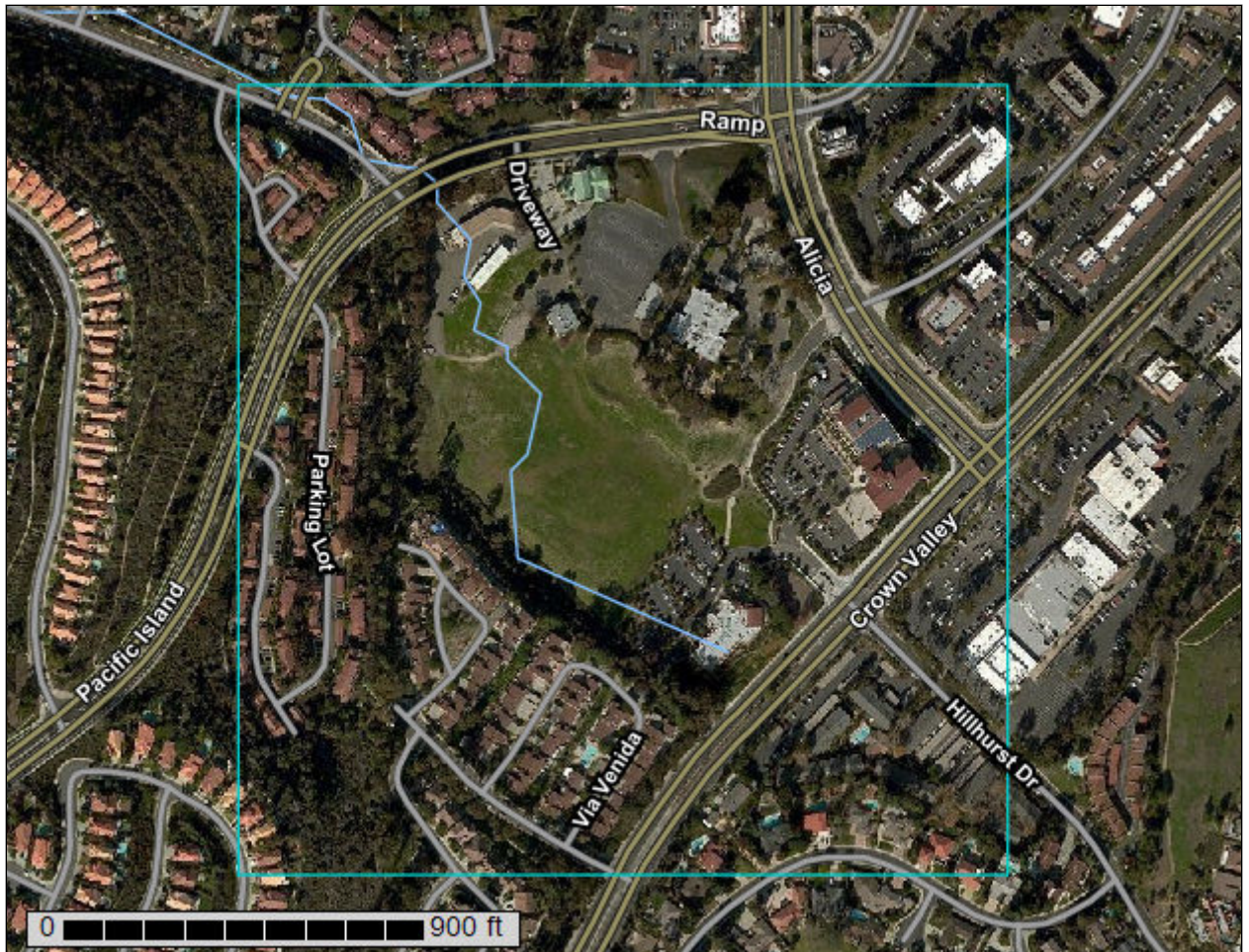
**NRCS**

Natural  
Resources  
Conservation  
Service

A product of the National  
Cooperative Soil Survey,  
a joint effort of the United  
States Department of  
Agriculture and other  
Federal agencies, State  
agencies including the  
Agricultural Experiment  
Stations, and local  
participants

# Custom Soil Resource Report for Orange County and Part of Riverside County, California

## Laguna Niguel Town Center



# Preface

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Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (<http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/>) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (<https://offices.sc.egov.usda.gov/locator/app?agency=nrcs>) or your NRCS State Soil Scientist ([http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2\\_053951](http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951)).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# How Soil Surveys Are Made

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Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

## Custom Soil Resource Report

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

## Custom Soil Resource Report

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

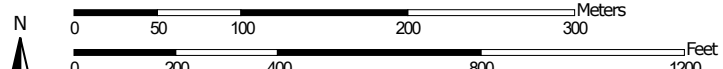
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The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

# Custom Soil Resource Report Soil Map



Map Scale: 1:4,530 if printed on A portrait (8.5" x 11") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 11N WGS84

### MAP LEGEND

**Area of Interest (AOI)**

 Area of Interest (AOI)




















**Soils**

 Soil Map Unit Polygons

 Soil Map Unit Lines


 Soil Map Unit Points

**Special Point Features**

-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh or swamp
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot

-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features

**Water Features**

 Streams and Canals

**Transportation**

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

**Background**

 Aerial Photography

### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Orange County and Part of Riverside County, California  
 Survey Area Data: Version 12, Sep 12, 2018

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jan 3, 2015—Jan 17, 2015

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background

**MAP LEGEND**

**MAP INFORMATION**

imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
101	Alo clay, 15 to 30 percent slopes, dry	40.8	47.1%
127	Bosanko clay, 15 to 30 percent slopes	16.5	19.1%
128	Bosanko clay, 30 to 50 percent slopes	4.9	5.7%
132	Botella clay loam, 2 to 9 percent slopes, warm MAAT, MLRA 19	1.7	2.0%
133	Botella clay loam, 9 to 15 percent slopes	12.8	14.8%
134	Calleguas clay loam, 50 to 75 percent slopes, eroded	2.0	2.3%
201	Soper gravelly loam, 15 to 30 percent slopes, MLRA 20	1.3	1.5%
202	Soper gravelly loam, 30 to 50 percent slopes, MLRA 20	6.6	7.6%
204	Soper-Rock outcrop complex, 30 to 75 percent slopes	0.0	0.0%
<b>Totals for Area of Interest</b>		<b>86.7</b>	<b>100.0%</b>

## Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different

## Custom Soil Resource Report

management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## Orange County and Part of Riverside County, California

### 101—Alo clay, 15 to 30 percent slopes, dry

#### Map Unit Setting

*National map unit symbol:* 2y8sm  
*Elevation:* 20 to 1,720 feet  
*Mean annual precipitation:* 13 to 16 inches  
*Mean annual air temperature:* 64 to 65 degrees F  
*Frost-free period:* 360 to 365 days  
*Farmland classification:* Not prime farmland

#### Map Unit Composition

*Alo and similar soils:* 85 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### Description of Alo

##### Setting

*Landform:* Ridges  
*Landform position (two-dimensional):* Summit, backslope  
*Landform position (three-dimensional):* Crest, side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Parent material:* Residuum weathered from calcareous sandstone or shale

##### Typical profile

*A - 0 to 15 inches:* clay  
*Bkss - 15 to 22 inches:* clay  
*Cr - 22 to 59 inches:* bedrock

##### Properties and qualities

*Slope:* 15 to 30 percent  
*Depth to restrictive feature:* 22 to 26 inches to paralithic bedrock  
*Natural drainage class:* Well drained  
*Runoff class:* Very high  
*Capacity of the most limiting layer to transmit water (Ksat):* Very low to moderately high (0.00 to 0.20 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum in profile:* 5 percent  
*Salinity, maximum in profile:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)  
*Available water storage in profile:* Low (about 3.5 inches)

##### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 4e  
*Hydrologic Soil Group:* D  
*Ecological site:* CLAYEY (1975) (R019XD001CA)  
*Hydric soil rating:* No

### Minor Components

#### **Bonsall, clay**

*Percent of map unit:* 5 percent  
*Landform:* Ridges  
*Landform position (two-dimensional):* Shoulder  
*Landform position (three-dimensional):* Crest  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

#### **Balcom, clay loam**

*Percent of map unit:* 5 percent  
*Landform:* Ridges  
*Landform position (two-dimensional):* Shoulder  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Ecological site:* CLAYEY (1975) (R019XD001CA)  
*Hydric soil rating:* No

#### **Anaheim, clay loam**

*Percent of map unit:* 5 percent  
*Landform:* Ridges  
*Landform position (two-dimensional):* Shoulder, backslope  
*Landform position (three-dimensional):* Crest, side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Ecological site:* CLAYEY (1975) (R019XD001CA)  
*Hydric soil rating:* No

## **127—Bosanko clay, 15 to 30 percent slopes**

### **Map Unit Setting**

*National map unit symbol:* 2xm5y  
*Elevation:* 120 to 1,080 feet  
*Mean annual precipitation:* 12 to 15 inches  
*Mean annual air temperature:* 63 to 65 degrees F  
*Frost-free period:* 353 to 365 days  
*Farmland classification:* Not prime farmland

### **Map Unit Composition**

*Bosanko and similar soils:* 85 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### **Description of Bosanko**

#### **Setting**

*Landform:* Hillslopes

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*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Parent material:* Acid residuum weathered from igneous rock

### Typical profile

*Ap - 0 to 5 inches:* clay  
*Bss - 5 to 25 inches:* clay  
*Bk - 25 to 35 inches:* clay  
*Cr - 35 to 79 inches:* bedrock

### Properties and qualities

*Slope:* 15 to 30 percent  
*Depth to restrictive feature:* 26 to 36 inches to paralithic bedrock  
*Natural drainage class:* Well drained  
*Runoff class:* Very high  
*Capacity of the most limiting layer to transmit water (Ksat):* Very low to moderately low (0.00 to 0.06 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum in profile:* 5 percent  
*Salinity, maximum in profile:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)  
*Available water storage in profile:* Low (about 5.5 inches)

### Interpretive groups

*Land capability classification (irrigated):* 4e  
*Land capability classification (nonirrigated):* 4e  
*Hydrologic Soil Group:* D  
*Ecological site:* CLAYEY (1975) (R019XD001CA)  
*Hydric soil rating:* No

### Minor Components

#### Balcom

*Percent of map unit:* 6 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

#### Alo

*Percent of map unit:* 6 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

#### Bonsall

*Percent of map unit:* 1 percent  
*Landform:* Hillslopes

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*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

### **Fallbrook**

*Percent of map unit:* 1 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

### **Vista**

*Percent of map unit:* 1 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

## **128—Bosanko clay, 30 to 50 percent slopes**

### **Map Unit Setting**

*National map unit symbol:* 2xm5x  
*Elevation:* 160 to 1,320 feet  
*Mean annual precipitation:* 13 to 16 inches  
*Mean annual air temperature:* 64 to 65 degrees F  
*Frost-free period:* 362 to 365 days  
*Farmland classification:* Not prime farmland

### **Map Unit Composition**

*Bosanko and similar soils:* 85 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### **Description of Bosanko**

#### **Setting**

*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Parent material:* Residuum weathered from granite

#### **Typical profile**

*Ap - 0 to 5 inches:* clay

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*Bss - 5 to 25 inches:* clay  
*Bk - 25 to 31 inches:* clay  
*Cr - 31 to 79 inches:* bedrock

### Properties and qualities

*Slope:* 30 to 50 percent  
*Depth to restrictive feature:* 22 to 32 inches to paralithic bedrock  
*Natural drainage class:* Well drained  
*Runoff class:* Very high  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately low (0.01 to 0.14 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum in profile:* 5 percent  
*Salinity, maximum in profile:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)  
*Available water storage in profile:* Low (about 4.9 inches)

### Interpretive groups

*Land capability classification (irrigated):* 6e  
*Land capability classification (nonirrigated):* 6e  
*Hydrologic Soil Group:* D  
*Ecological site:* CLAYEY (1975) (R019XD001CA)  
*Hydric soil rating:* No

### Minor Components

#### Balcom

*Percent of map unit:* 8 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

#### Alo

*Percent of map unit:* 7 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

## 132—Botella clay loam, 2 to 9 percent slopes, warm MAAT, MLRA 19

### Map Unit Setting

*National map unit symbol:* 2tyz8  
*Elevation:* 80 to 1,450 feet

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*Mean annual precipitation:* 14 to 16 inches  
*Mean annual air temperature:* 64 to 65 degrees F  
*Frost-free period:* 330 to 360 days  
*Farmland classification:* Prime farmland if irrigated

### Map Unit Composition

*Botella and similar soils:* 90 percent  
*Minor components:* 10 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Botella

#### Setting

*Landform:* Alluvial fans  
*Landform position (two-dimensional):* Toeslope  
*Landform position (three-dimensional):* Riser, flat  
*Down-slope shape:* Linear  
*Across-slope shape:* Convex  
*Parent material:* Alluvium derived from sedimentary rock

#### Typical profile

*A - 0 to 8 inches:* clay loam  
*2Bt - 8 to 35 inches:* silty clay loam  
*2C - 35 to 66 inches:* clay loam

#### Properties and qualities

*Slope:* 2 to 9 percent  
*Depth to restrictive feature:* More than 80 inches  
*Natural drainage class:* Well drained  
*Runoff class:* Medium  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high (0.20 to 0.60 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Available water storage in profile:* High (about 10.0 inches)

#### Interpretive groups

*Land capability classification (irrigated):* 2e  
*Land capability classification (nonirrigated):* 3e  
*Hydrologic Soil Group:* C  
*Ecological site:* CLAYEY (1975) (R019XD001CA)  
*Hydric soil rating:* No

### Minor Components

#### Sorrento

*Percent of map unit:* 6 percent  
*Landform:* Alluvial fans  
*Landform position (two-dimensional):* Footslope  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Hydric soil rating:* No

#### Mocho

*Percent of map unit:* 4 percent  
*Landform:* Alluvial fans



## Custom Soil Resource Report

*Landform position (two-dimensional):* Foothlope  
*Landform position (three-dimensional):* Tread  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Hydric soil rating:* No

### 133—Botella clay loam, 9 to 15 percent slopes

#### Map Unit Setting

*National map unit symbol:* hcm9  
*Elevation:* 50 to 800 feet  
*Mean annual precipitation:* 12 to 25 inches  
*Mean annual air temperature:* 57 to 59 degrees F  
*Frost-free period:* 260 to 350 days  
*Farmland classification:* Not prime farmland

#### Map Unit Composition

*Botella and similar soils:* 85 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### Description of Botella

##### Setting

*Landform:* Alluvial fans  
*Landform position (two-dimensional):* Toeslope  
*Landform position (three-dimensional):* Riser, flat  
*Down-slope shape:* Linear  
*Across-slope shape:* Convex  
*Parent material:* Alluvium derived from sedimentary rock

##### Typical profile

*H1 - 0 to 8 inches:* clay loam  
*H2 - 8 to 35 inches:* silty clay loam  
*H3 - 35 to 66 inches:* sandy clay loam

##### Properties and qualities

*Slope:* 9 to 15 percent  
*Depth to restrictive feature:* More than 80 inches  
*Natural drainage class:* Well drained  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high (0.20 to 0.57 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Available water storage in profile:* High (about 10.4 inches)

##### Interpretive groups

*Land capability classification (irrigated):* 3e  
*Land capability classification (nonirrigated):* 3e  
*Hydrologic Soil Group:* C

Custom Soil Resource Report

*Ecological site:* CLAYEY (1975) (R019XD001CA)  
*Hydric soil rating:* No

**Minor Components**

**Botella, loam**

*Percent of map unit:* 4 percent  
*Hydric soil rating:* No

**Sorrento, clay loam**

*Percent of map unit:* 4 percent  
*Hydric soil rating:* No

**Mocho, loam**

*Percent of map unit:* 4 percent  
*Hydric soil rating:* No

**Unnamed**

*Percent of map unit:* 3 percent  
*Hydric soil rating:* No

**134—Calleguas clay loam, 50 to 75 percent slopes, eroded**

**Map Unit Setting**

*National map unit symbol:* 2xm62  
*Elevation:* 220 to 2,110 feet  
*Mean annual precipitation:* 13 to 18 inches  
*Mean annual air temperature:* 64 to 65 degrees F  
*Frost-free period:* 353 to 365 days  
*Farmland classification:* Not prime farmland

**Map Unit Composition**

*Calleguas and similar soils:* 85 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

**Description of Calleguas**

**Setting**

*Landform:* Hillslopes  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Parent material:* Residuum weathered from calcareous shale

**Typical profile**

*A1 - 0 to 7 inches:* clay loam  
*A2 - 7 to 11 inches:* clay loam  
*A3 - 11 to 15 inches:* very channery clay loam  
*Cr - 15 to 59 inches:* bedrock

## Custom Soil Resource Report

### Properties and qualities

*Slope:* 50 to 75 percent  
*Depth to restrictive feature:* 10 to 20 inches to paralithic bedrock  
*Natural drainage class:* Well drained  
*Runoff class:* Very high  
*Capacity of the most limiting layer to transmit water (Ksat):* Very low to moderately low (0.00 to 0.06 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum in profile:* 5 percent  
*Salinity, maximum in profile:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)  
*Available water storage in profile:* Very low (about 2.2 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 7e  
*Hydrologic Soil Group:* D  
*Ecological site:* SHALLOW CLAYEY (1975) (R019XD071CA)  
*Hydric soil rating:* No

### Minor Components

#### Cieneba

*Percent of map unit:* 5 percent  
*Landform:* Hillslopes  
*Landform position (two-dimensional):* Summit  
*Landform position (three-dimensional):* Crest  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

#### Balcom

*Percent of map unit:* 5 percent  
*Landform:* Hillslopes  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

#### Anaheim

*Percent of map unit:* 5 percent  
*Landform:* Hillslopes  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

## 201—Soper gravelly loam, 15 to 30 percent slopes, MLRA 20

### Map Unit Setting

*National map unit symbol:* 2wv8d  
*Elevation:* 60 to 1,670 feet  
*Mean annual precipitation:* 13 to 21 inches  
*Mean annual air temperature:* 63 to 65 degrees F  
*Frost-free period:* 301 to 365 days  
*Farmland classification:* Not prime farmland

### Map Unit Composition

*Soper and similar soils:* 85 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Soper

#### Setting

*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Parent material:* Residuum weathered from sandstone

#### Typical profile

*A - 0 to 8 inches:* gravelly loam  
*Bt - 8 to 29 inches:* gravelly clay loam  
*Cr - 29 to 79 inches:* bedrock

#### Properties and qualities

*Slope:* 15 to 30 percent  
*Depth to restrictive feature:* 22 to 36 inches to paralithic bedrock  
*Natural drainage class:* Well drained  
*Runoff class:* High  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high (0.20 to 2.00 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Available water storage in profile:* Low (about 3.9 inches)

#### Interpretive groups

*Land capability classification (irrigated):* 4e  
*Land capability classification (nonirrigated):* 6e  
*Hydrologic Soil Group:* C  
*Ecological site:* LOAMY (1975) (R019XD029CA)  
*Hydric soil rating:* No

**Minor Components**

**Anaheim**

*Percent of map unit:* 6 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

**Fontana**

*Percent of map unit:* 4 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

**Cieneba**

*Percent of map unit:* 3 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

**Gaviota**

*Percent of map unit:* 2 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

**202—Soper gravelly loam, 30 to 50 percent slopes, MLRA 20**

**Map Unit Setting**

*National map unit symbol:* 2wv8f  
*Elevation:* 10 to 2,010 feet  
*Mean annual precipitation:* 13 to 18 inches  
*Mean annual air temperature:* 63 to 65 degrees F  
*Frost-free period:* 271 to 365 days  
*Farmland classification:* Not prime farmland

**Map Unit Composition**

*Soper and similar soils:* 85 percent

## Custom Soil Resource Report

*Minor components: 15 percent*

*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Soper

#### Setting

*Landform: Hills*

*Landform position (two-dimensional): Backslope*

*Landform position (three-dimensional): Side slope*

*Down-slope shape: Convex*

*Across-slope shape: Convex*

*Parent material: Residuum weathered from sandstone*

#### Typical profile

*A - 0 to 8 inches: gravelly loam*

*Bt - 8 to 29 inches: gravelly clay loam*

*Cr - 29 to 79 inches: bedrock*

#### Properties and qualities

*Slope: 30 to 50 percent*

*Depth to restrictive feature: 22 to 36 inches to paralithic bedrock*

*Natural drainage class: Well drained*

*Runoff class: High*

*Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)*

*Depth to water table: More than 80 inches*

*Frequency of flooding: None*

*Frequency of ponding: None*

*Available water storage in profile: Low (about 3.9 inches)*

#### Interpretive groups

*Land capability classification (irrigated): None specified*

*Land capability classification (nonirrigated): 7e*

*Hydrologic Soil Group: C*

*Ecological site: LOAMY (1975) (R019XD029CA)*

*Hydric soil rating: No*

### Minor Components

#### Cieneba

*Percent of map unit: 5 percent*

*Landform: Hills*

*Landform position (two-dimensional): Backslope*

*Landform position (three-dimensional): Side slope*

*Down-slope shape: Convex*

*Across-slope shape: Convex*

*Hydric soil rating: No*

#### Yorba

*Percent of map unit: 3 percent*

*Landform: Hills*

*Landform position (two-dimensional): Backslope*

*Landform position (three-dimensional): Side slope*

*Down-slope shape: Convex*

*Across-slope shape: Convex*

*Hydric soil rating: No*

**Gabino**

*Percent of map unit:* 3 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

**Gaviota**

*Percent of map unit:* 2 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

**Fontana**

*Percent of map unit:* 1 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

**Rock outcrop**

*Percent of map unit:* 1 percent  
*Landform:* Hills  
*Landform position (two-dimensional):* Backslope  
*Landform position (three-dimensional):* Side slope  
*Down-slope shape:* Convex  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

**204—Soper-Rock outcrop complex, 30 to 75 percent slopes**

**Map Unit Setting**

*National map unit symbol:* hcpl  
*Elevation:* 100 to 4,000 feet  
*Mean annual precipitation:* 8 to 25 inches  
*Mean annual air temperature:* 45 to 52 degrees F  
*Frost-free period:* 110 to 350 days  
*Farmland classification:* Not prime farmland

**Map Unit Composition**

*Soper and similar soils:* 60 percent  
*Soper, cobbly loam:* 20 percent  
*Rock outcrop:* 15 percent

## Custom Soil Resource Report

*Minor components: 5 percent*

*Estimates are based on observations, descriptions, and transects of the mapunit.*

### Description of Soper

#### Setting

*Landform: Hills*

*Landform position (two-dimensional): Backslope*

*Landform position (three-dimensional): Side slope*

*Down-slope shape: Convex*

*Across-slope shape: Convex*

*Parent material: Residuum weathered from sandstone*

#### Typical profile

*H1 - 0 to 4 inches: gravelly loam*

*H2 - 4 to 20 inches: gravelly clay loam, gravelly sandy clay loam, gravelly loam*

*H2 - 4 to 20 inches: weathered bedrock*

*H2 - 4 to 20 inches:*

*H3 - 20 to 59 inches:*

#### Properties and qualities

*Slope: 30 to 75 percent*

*Depth to restrictive feature: 20 to 24 inches to paralithic bedrock*

*Natural drainage class: Well drained*

*Capacity of the most limiting layer to transmit water (Ksat): Moderately high (0.20 to 0.57 in/hr)*

*Depth to water table: More than 80 inches*

*Frequency of flooding: None*

*Frequency of ponding: None*

*Available water storage in profile: Moderate (about 6.9 inches)*

#### Interpretive groups

*Land capability classification (irrigated): None specified*

*Land capability classification (nonirrigated): 7e*

*Hydrologic Soil Group: C*

*Ecological site: SHALLOW LOAMY - ROCK OUTCROP COMPLEX  
(R019XD073CA)*

*Hydric soil rating: No*

### Description of Soper, Cobbly Loam

#### Setting

*Landform: Hills*

*Landform position (two-dimensional): Backslope*

*Landform position (three-dimensional): Side slope*

*Down-slope shape: Convex*

*Across-slope shape: Convex*

*Parent material: Residuum weathered from sandstone*

#### Typical profile

*H1 - 0 to 4 inches: gravelly loam*

#### Properties and qualities

*Depth to restrictive feature: More than 80 inches*

*Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)*

*Depth to water table: More than 80 inches*

*Frequency of flooding: None*



## Custom Soil Resource Report

*Frequency of ponding:* None

*Available water storage in profile:* Very low (about 0.6 inches)

### Description of Rock Outcrop

#### Setting

*Landform:* Hills

*Landform position (two-dimensional):* Backslope

*Landform position (three-dimensional):* Side slope

*Down-slope shape:* Convex

*Across-slope shape:* Convex

*Parent material:* Residuum weathered from sandstone

#### Typical profile

*H1 - 0 to 60 inches:* unweathered bedrock

#### Properties and qualities

*Slope:* 30 to 75 percent

*Depth to restrictive feature:* 0 inches to lithic bedrock

#### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 8s

*Hydric soil rating:* No

### Minor Components

#### Cieneba, sandy loam

*Percent of map unit:* 3 percent

*Hydric soil rating:* No

#### Anaheim, loam

*Percent of map unit:* 2 percent

*Hydric soil rating:* No

# References

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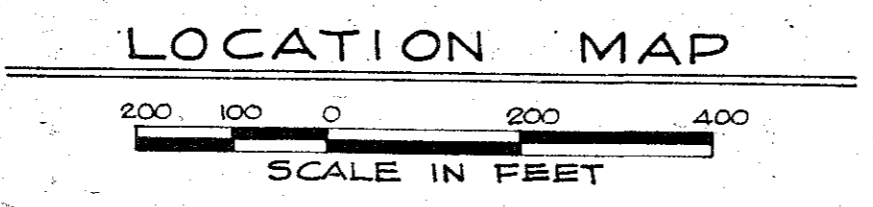
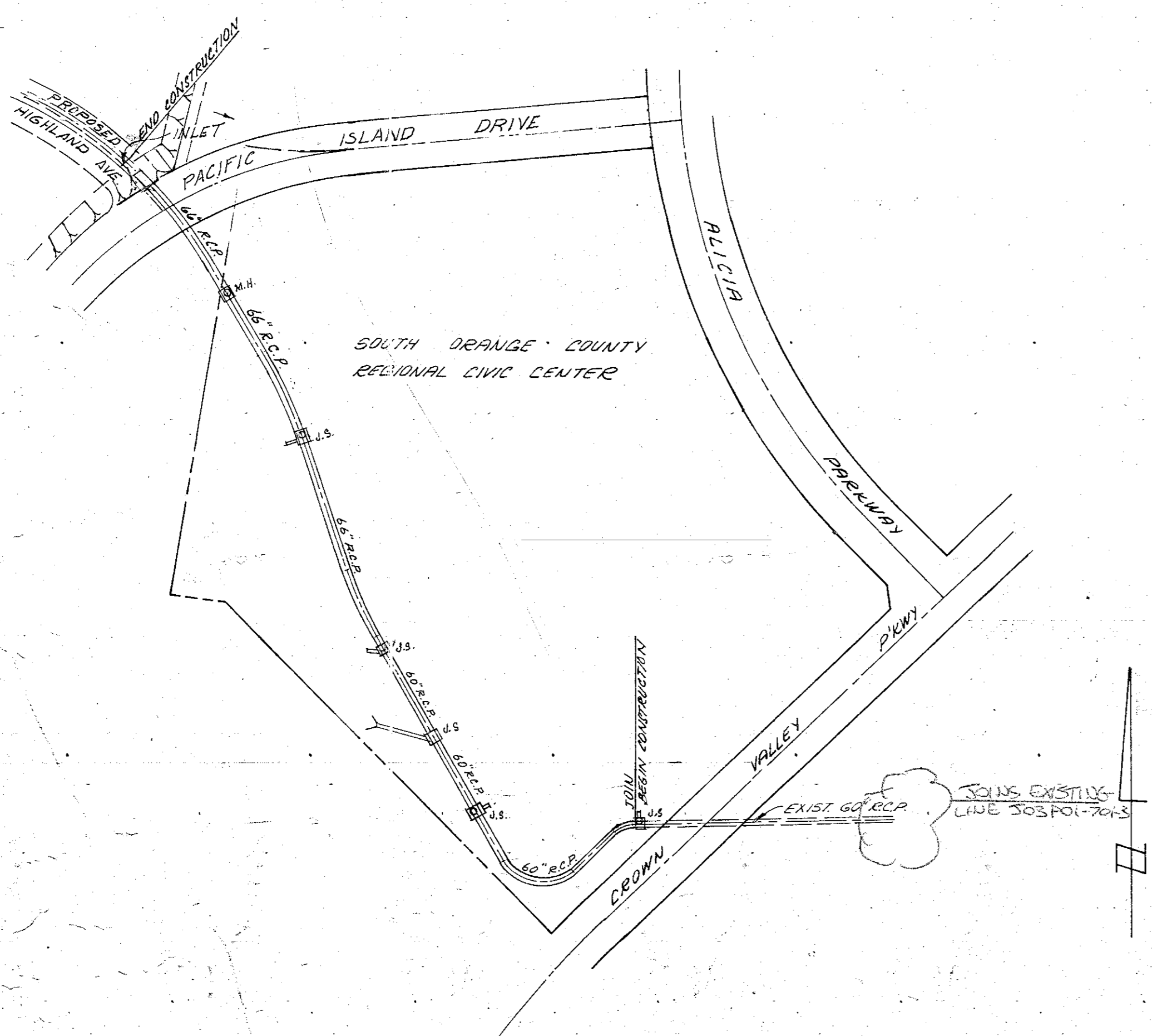
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- United States Department of Agriculture, Natural Resources Conservation Service. National range and pasture handbook. <http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/landuse/rangepasture/?cid=stelprdb1043084>

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**LIST OF UTILITIES**

UTILITY	TELEPHONE No.
1. SEWER	541-4471
2. WATER	541-4471
3. TELEPHONE	493-0052
4. GAS	495-4430
5. ELECTRIC	492-3644

**GENERAL NOTES**

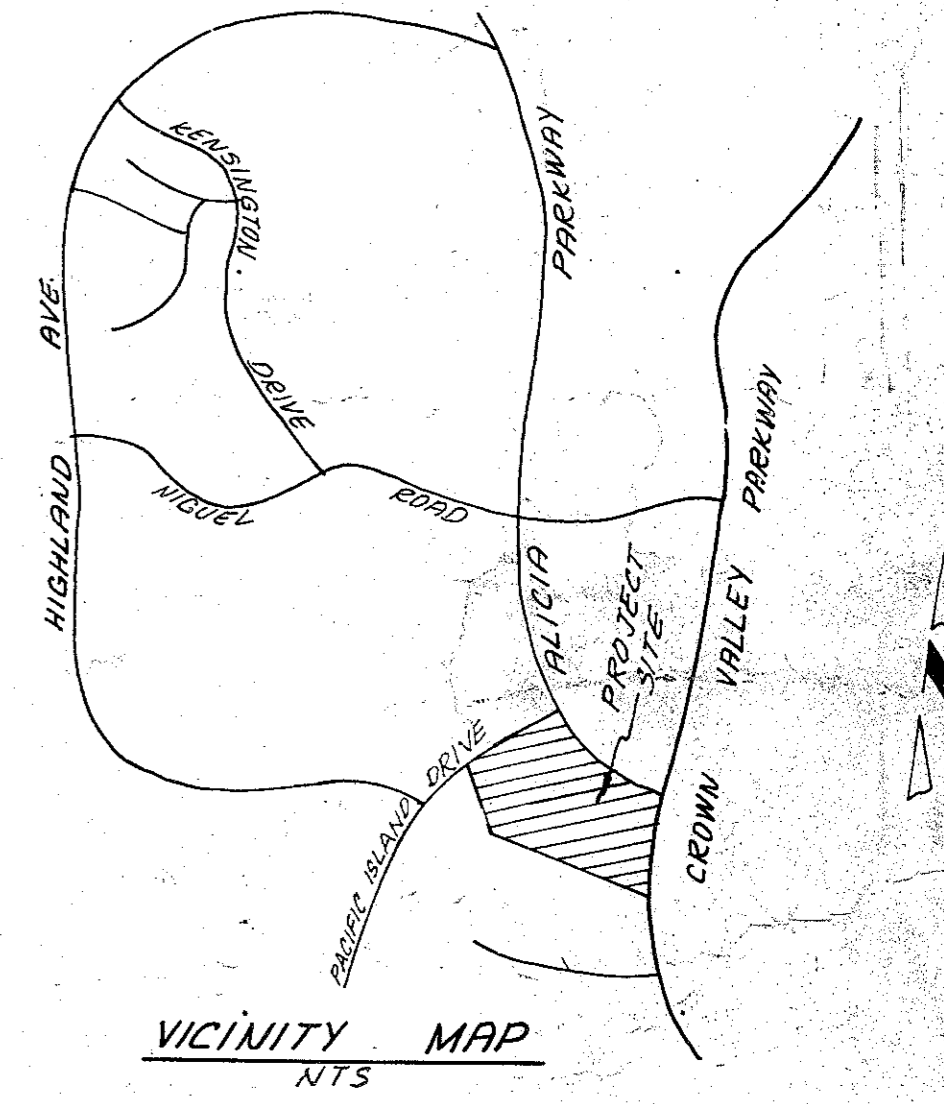
- ALL CONCRETE IN REINFORCED CONCRETE STRUCTURES MUST BE 3000 POUNDS PER SQUARE INCH, IN 28 DAYS, PORTLAND CEMENT CONCRETE, CLASS A.
- ALL PIPE LENGTHS ARE HORIZONTAL PROJECTIONS, UNLESS OTHERWISE SHOWN.
- LENGTH OF STRUCTURES MAY BE INCREASED TO MEET PIPE ENDS AT OPTION OF CONTRACTOR, AS LONG AS REINFORCING STEEL IS CONTINUED AS REQUIRED, ANY CHANGE IN SPUR LOCATION MUST BE APPROVED BY THE ENGINEER.
- ALL STEEL THAT IS TO BE CONTINUOUS MUST BE LAPPED A MINIMUM OF 30 BAR DIAMETERS.
- FLOOR OF STRUCTURE SHALL BE STEEL TROWELED TO SPRING LINE.
- BODY OF STRUCTURE, INCLUDING SPUR, MUST BE POURED IN ONE CONTINUOUS OPERATION, EXCEPT THAT A CONSTRUCTION JOINT AT THE SPRING LINE WITH A LONGITUDINAL KEYWAY IS PERMITTED.
- CLEARANCE BETWEEN EDGE OF CONCRETE AND REINFORCING STEEL MUST BE 1/2 INCHES MINIMUM UNLESS OTHERWISE CALLED FOR ON PLAN.
- ALL REINFORCING BARS MUST BE SECURELY HELD IN PLACE IN THE FORMS. TWO WAY MATS OF STEEL MUST BE WIRED TOGETHER BOTH WAYS AT ALTERNATIVE INTERSECTIONS.
- FOR TRENCH EXCAVATIONS IN NATIVE SOIL, SHORING SHALL BE PROVIDED TO SATISFY STATE OF CALIFORNIA SAFETY REQUIREMENTS.
- STORM DRAIN BACKFILL FOR ALL FACILITIES WITHIN STREET RIGHT-OF-WAY IS TO BE PLACED AND COMPACTED UNDER ORANGE COUNTY E.M.A.-DEVELOPMENT INSPECTION AND MEET OR EXCEED E.M.A.-DEVELOPMENT MINIMUM STANDARDS.
- PIPE CONSTRUCTION IN FILL AREAS MUST BE COORDINATED WITH THE GRADING TO INSURE THAT WHEN THE FILL OPERATION HAS BEEN COMPLETED TO A GRADE A MINIMUM OF ONE FOOT ABOVE THE TOP OF PIPE OR TO FIVE FEET (MAXIMUM) ABOVE THE PROPOSED SUB-GRADE OF THE PIPE, THE STORM DRAIN TRENCH SHALL BE EXCAVATED AND THE PIPE INSTALLED.
- ALL WORK MUST BE IN CONFORMANCE WITH THE ORANGE COUNTY E.M.A.-DEVELOPMENT STANDARD SPECIFICATIONS WHICH MAY BE PURCHASED FROM THE DISTRICT AND MUST BE KEPT ON THE JOB SITE AT ALL TIMES.
- THE CONTRACTOR MUST NOTIFY THE E.M.A.'S INSPECTOR AT LEAST 48 HOURS PRIOR TO COMMENCEMENT OF ANY CONSTRUCTION BY TELEPHONING 834-3410, OR BY WRITING THE ORANGE COUNTY ENVIRONMENTAL MANAGEMENT AGENCY, 400 CIVIC CENTER DRIVE WEST, SANTA ANA, CALIFORNIA.
- ALL FILL MUST BE COMPACTED TO 90% RELATIVE COMPACTION AS DETERMINED BY THE CALIFORNIA TEST METHOD NO. 216-F, 1963 'FIVE LAYER METHOD'. ALL BACKFILL MATERIAL MUST BE FREE FROM VEGETABLE MATTER.
- ALL SURVEYING REQUIRED FOR VERTICAL AND HORIZONTAL ALIGNMENT MUST BE PROVIDED BY THE CONTRACTOR OR DEVELOPER AND SUFFICIENT REFERENCE STAKING MUST BE IN ACCORDANCE WITH THE REQUEST OF THE E.M.A.'S INSPECTOR.
- ALL MATERIAL TESTINGS FOR THE STORM DRAIN FACILITIES AND RELATED CONSTRUCTION MUST BE PROVIDED BY THE CONTRACTOR OR DEVELOPER IN ACCORDANCE WITH THE NUMBER AND FREQUENCY REQUESTED BY THE E.M.A.-DEVELOPMENT INSPECTOR.
- ALL REINFORCED CONCRETE PIPE MUST BE BEDDED IN ACCORDANCE WITH PIPE BEDDING DETAIL SHOWN.
- REINFORCEMENT IN THICK WALL R.C.P. WHEN SPECIFIED, MUST HAVE A MINIMUM CONCRETE OF 1/2 INCHES CLEARANCE FROM INSIDE FACE OF THE PIPE.
- A PERMIT FOR WORK WITHIN EXISTING OR PROPOSED STREET RIGHT-OF-WAY IS REQUIRED FROM THE ORANGE COUNTY E.M.A.-DEVELOPMENT FOR ANY ENCROACHMENT NECESSARY FOR CONSTRUCTION.
- ALL PIPES TO BE BANDED AND GROUTED.
- PRIOR TO THE PLACEMENT OF STORM DRAIN IMPROVEMENTS, THE DEVELOPER'S SOIL ENGINEER SHALL CERTIFY IN WRITING TO THE E.M.A.'S INSPECTOR THAT THE STORM DRAIN SUB-GRADE IS OF ADEQUATE STRENGTH TO SUPPORT THE STRUCTURES AND ANY ANTICIPATED LOADS.
- PRIOR TO THE COMMENCEMENT OF CONSTRUCTION, THE DEVELOPER'S CONTRACTOR SHALL OBTAIN A PERMIT FROM THE STATE DIVISION OF INDUSTRIAL SAFETY. A COPY OF PERMIT SHALL BE KEPT ON THE JOB SITE AT ALL TIMES.
- WHENEVER APPLICABLE, THE DEVELOPER SHALL OBTAIN A PERMIT FROM THE STATE DEPARTMENT OF FISH AND GAME IN ACCORDANCE WITH SECTION 1602 OF THE CALIFORNIA FISH AND GAME CODE PRIOR TO COMMENCEMENT OF CONSTRUCTION.

**INDEX OF DRAWINGS**

SHEET NO.	DESCRIPTION
1	TITLE SHEET
2	STORM DRAIN PLAN & PROFILE STA. 0+00 TO 11+00
3	STORM DRAIN PLAN & PROFILE STA. 11+00 TO 17+18 AND J.S. DETAILS.

**QUANTITY ESTIMATE**

60" R.C.P.	1760 L.F.
J.S. TYPE II	6 EA.
INLET STR.	2 EA.
24" R.C.P.	103 L.F.
GROUTED RIP-RAP	300 S.F.



PLANS FOR IMPROVEMENT OF FACILITY NO. **J03P07** AS BUILT

FACILITY NO. J03P07 IS A COUNTY OF ORANGE MASTER PLAN OF DRAINAGE FACILITY BEING CONSTRUCTED IN ACCORDANCE WITH THE LAGUNA HILLS AREA MASTER PLAN OF DRAINAGE UNDER THE ADMINISTRATION AND SUPERVISION OF THE ENVIRONMENTAL MANAGEMENT AGENCY ACTING AS THE AGENT FOR THE COUNTY.

COUNTY OF ORANGE  
E.M.A. DEVELOPMENT DIVISION

BY *J. W. Schaefer* 11-5-79  
R.C.E. 8836 DATE

THIS PLAN IS SIGNED BY E.M.A. DEVELOPMENT FOR CONCEPT AND ADHERENCE TO COUNTY STANDARDS AND REQUIREMENTS ONLY. E.M.A. DEVELOPMENT IS NOT RESPONSIBLE FOR DESIGN ASSUMPTIONS OR ACCURACY.

BENCH MARK	BASIS OF BEARING
DATUM: O.C.S.-LEVELING ADJ. 1970-BM No. 303370 EL. 319.96' DESCRIPTION: IN THE SOUTHEAST PART OF THE INTERSECTION OF CROWN VALLEY PARKWAY AND HILLHURST DRIVE; ABOUT 55.3 FEET SOUTHWEST OF THE CENTER OF THE MEDIAN OF THE PARKWAY, 56 FEET SOUTHWEST OF THE CENTER LINE OF THE DRIVE, SET IN TOP OF THE NORTHWEST CORNER OF A 4 BY 8 FOOT CONCRETE CATCH BASIN, 1 FOOT HIGHER THAN THE GUTTER.	THE BEARING OF N 44° 35' 56" E ON THE CENTERLINE OF CROWN VALLEY PARKWAY AS SHOWN ON BOOK 87 PAGE 11 OF RECORDS OF SURVEYS, COUNTY OF ORANGE, CALIFORNIA.

PLANS PREPARED UNDER THE SUPERVISION OF:

*James O. Miller* R.C.E. NO. 23434 DATE 1-3-78

IN THE OFFICE OF  
**GENGE CONSULTANTS**  
2021 BUSINESS CENTER DRIVE  
IRVINE, CALIFORNIA 92715  
(714) 953-2721

DATE	BY	DESCRIPTION	APP'D.	DATE
REVISIONS				

FACILITY NO. **J03P07**

FROM CROWN VALLEY PARKWAY TO PACIFIC ISLAND DRIVE

DWG. NO. J03 P07-1/3-3-A

AUG 30 1981

OF 3

DRAWING NUMBER  
1 of 3

DRAWING NUMBER  
1 of 3

DRAWING NUMBER  
J03P07-713-3-A

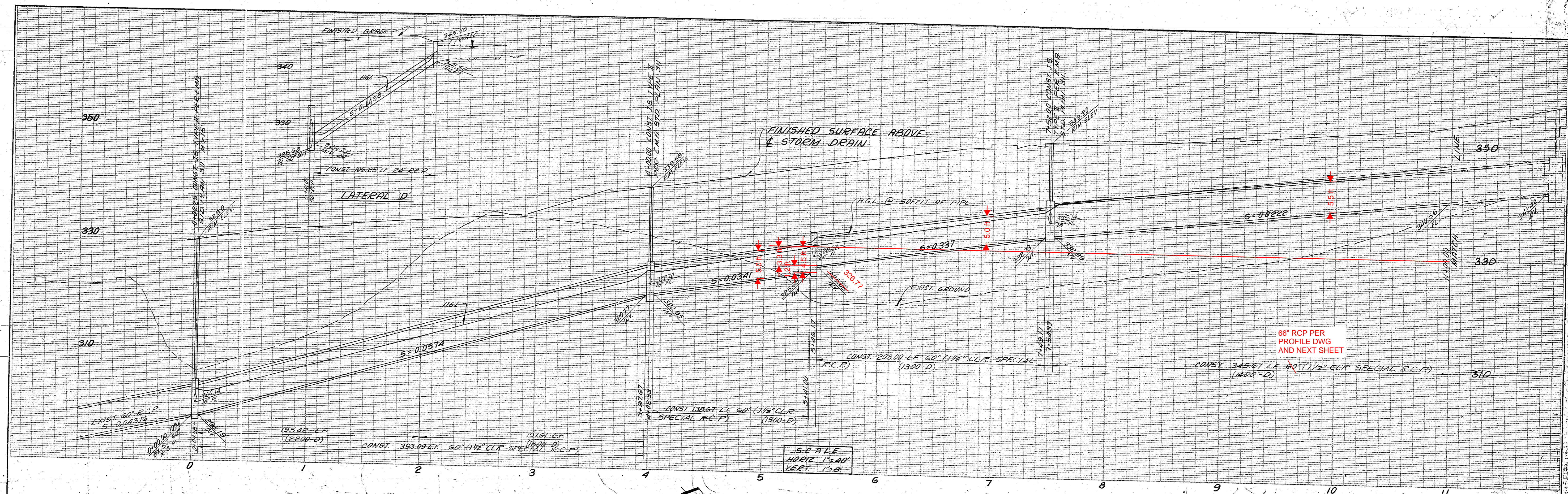
NUMBER

DRAWING NUMBER  
SAFECO PRODUCTS • NEW HOPE, MINNESOTA  
REORDER BY PART NUMBER 6032

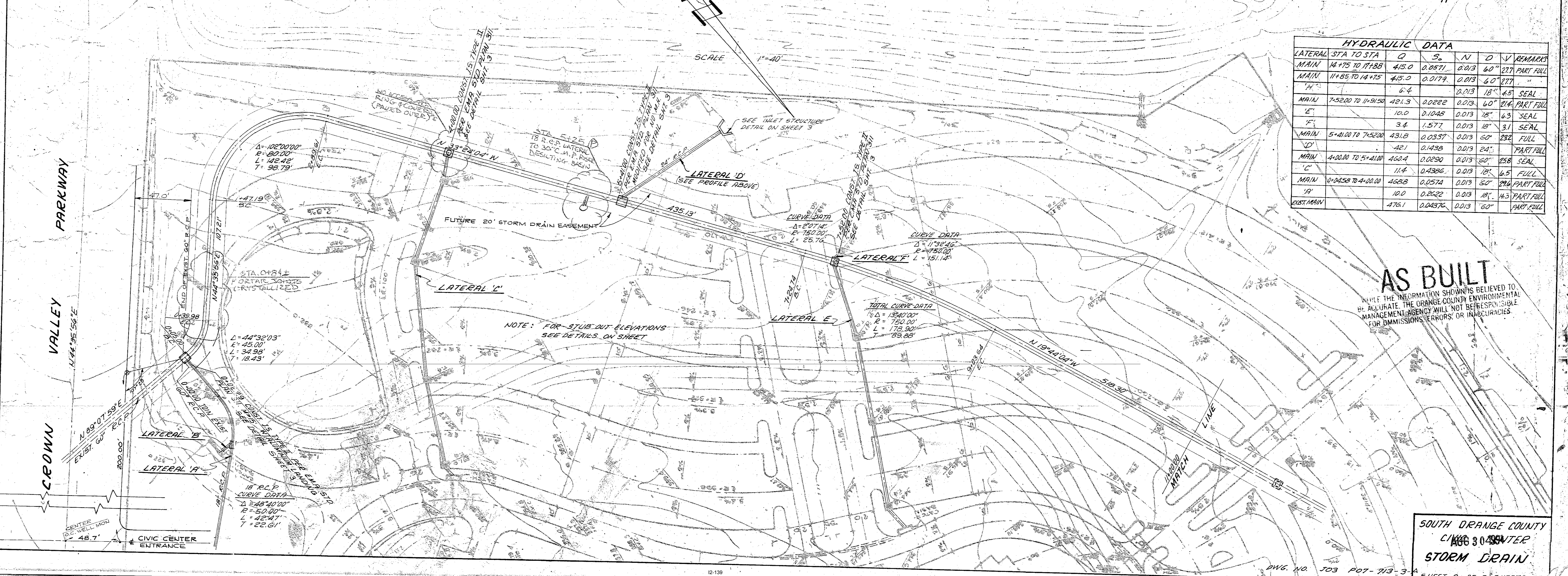
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2 of 3  
SAFECO PRODUCTS • NEW HOPE, MINNESOTA  
REORDER BY PART NUMBER 6032

DRAWING NUMBER  
303POT-713-3-A  
SAFECO PRODUCTS • NEW HOPE, MINNESOTA  
REORDER BY PART NUMBER 6032

NUMBER  
SAFECO PRODUCTS • NEW HOPE, MINNESOTA  
REORDER BY PART NUMBER 6032



LATERAL	STA TO STA	Q	S <sub>0</sub>	N	D	REMARKS
MAIN	14+75 TO 17+85	415.0	0.0571	0.013	60"	277 PART FULL
MAIN	11+85 TO 14+75	415.0	0.0179	0.013	60"	277 "
"		6.4		0.013	18"	4.5 SEAL
MAIN	7+52.00 TO 11+91.50	421.3	0.0222	0.013	60"	274 PART FULL
"		10.0	0.1048	0.013	18"	6.3 SEAL
"		3.4	1.577	0.013	18"	3.1 SEAL
MAIN	5+41.00 TO 7+52.00	431.8	0.0337	0.013	60"	232 FULL
"		42.1	0.1438	0.013	24"	PART FULL
MAIN	4+00.00 TO 5+41.00	460.4	0.0290	0.013	60"	258 SEAL
"		11.4	0.4386	0.013	18"	6.5 FULL
MAIN	0+04.58 TO 4+00.00	468.8	0.0574	0.013	60"	246 PART FULL
"		10.0	0.2622	0.013	18"	4.3 PART FULL
EXIST. MAIN		476.1	0.04376	0.013	60"	PART FULL



SOUTH ORANGE COUNTY  
CIVIL ENGINEER  
303 POT-713-3-A  
STORM DRAIN  
DWG. NO. 303 POT-713-3-A SHEET 2 OF 3 SHEETS  
J.M. 50074

DRAWING NUMBER  
3 OF 3

DRAWING NUMBER  
3 OF 3

DRAWING NUMBER  
J03 P07-713-3-A

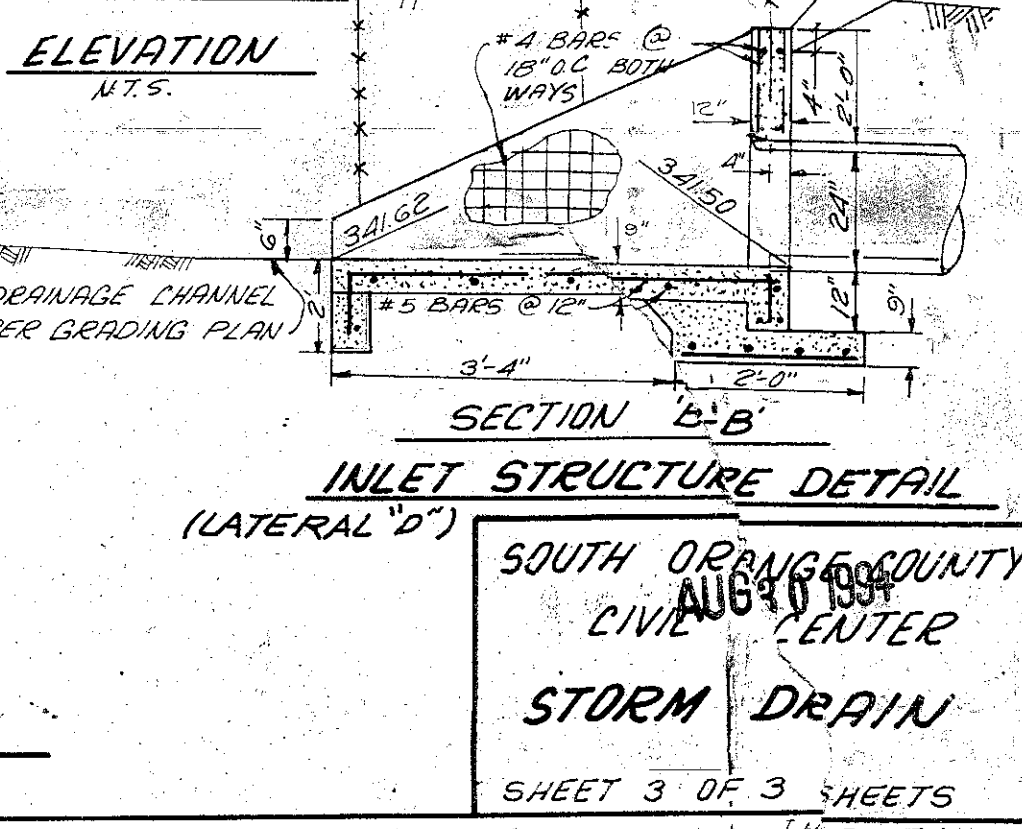
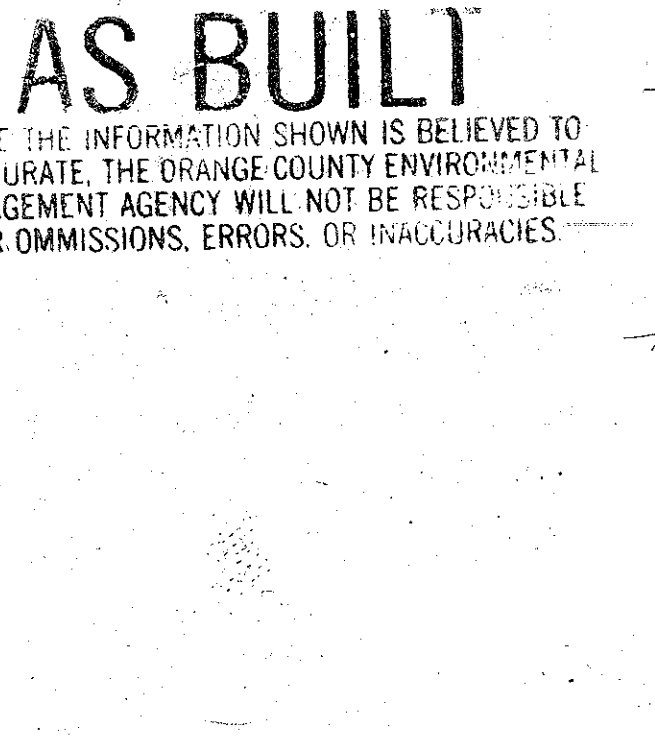
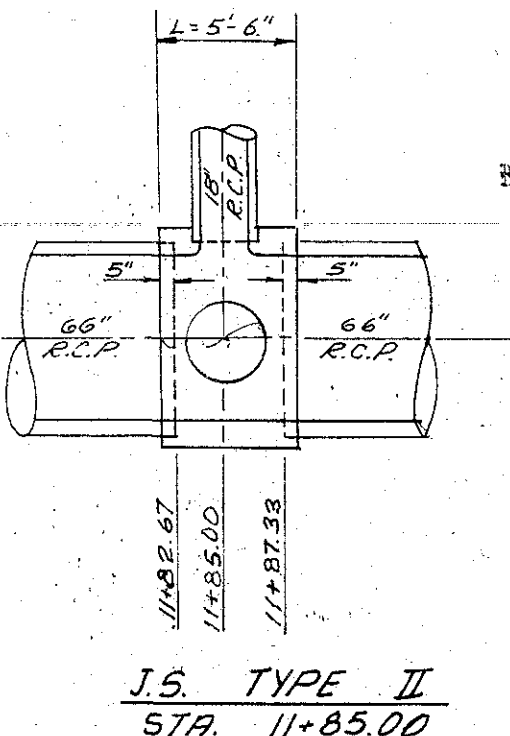
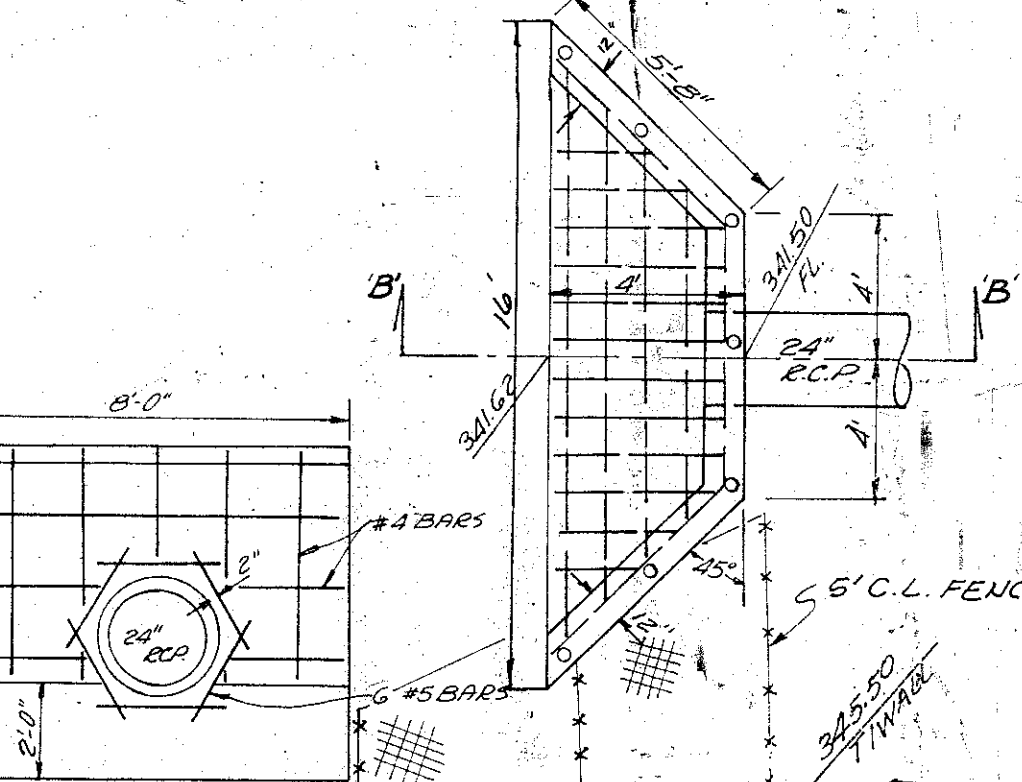
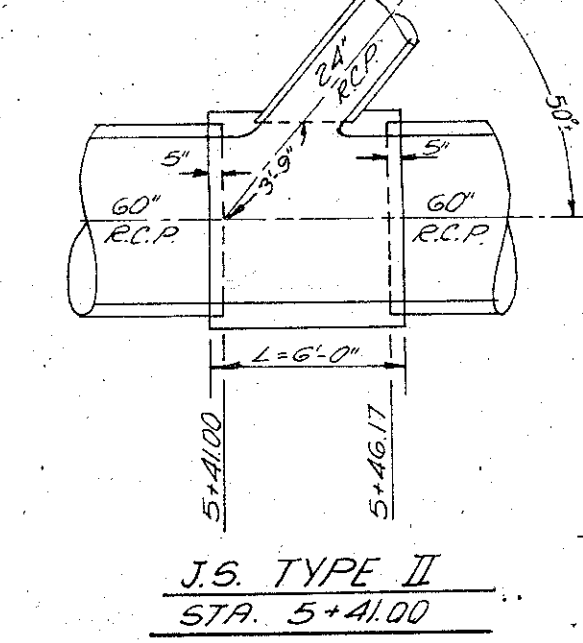
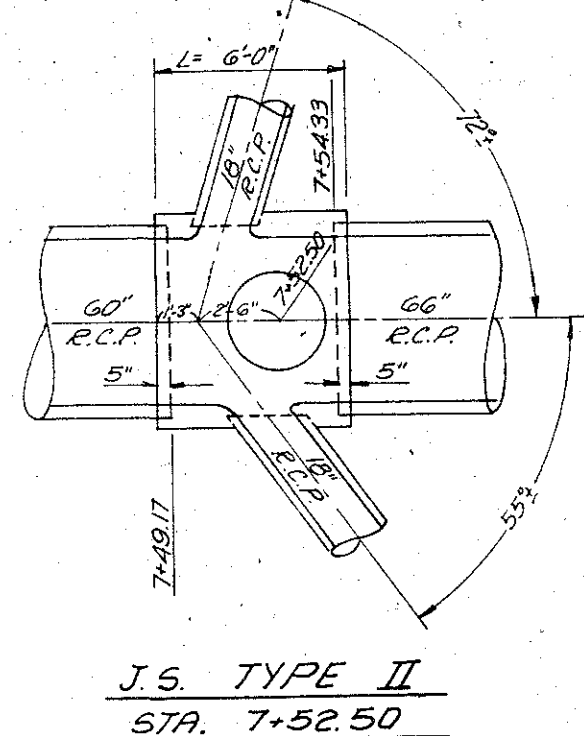
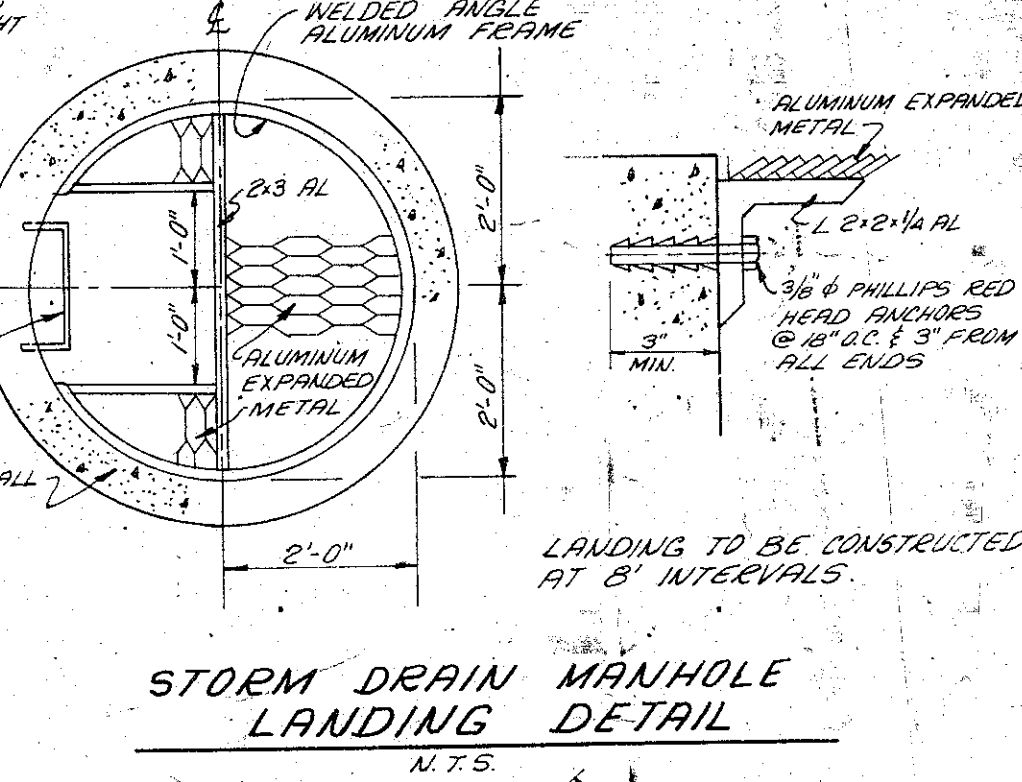
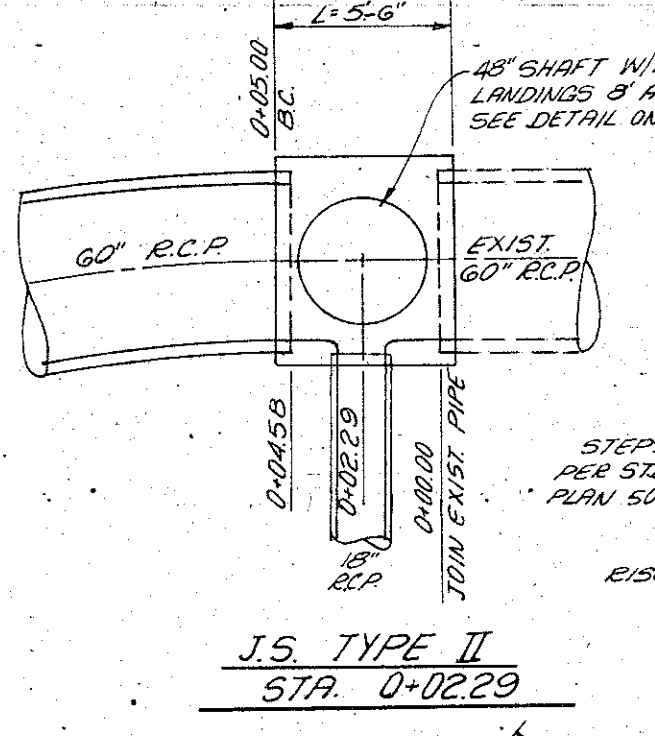
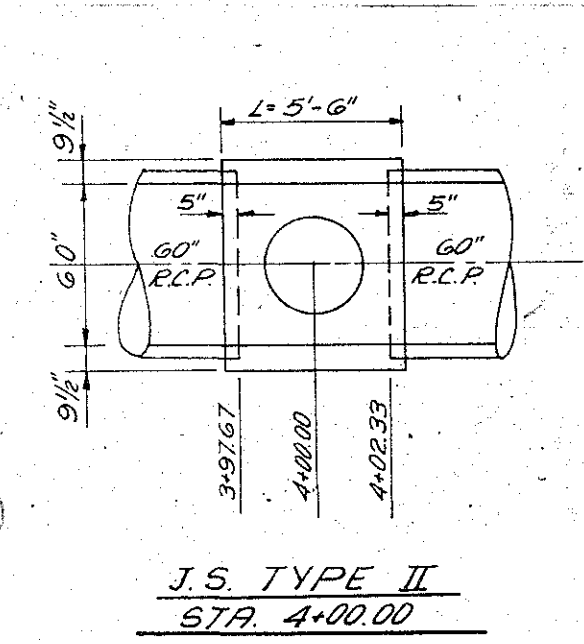
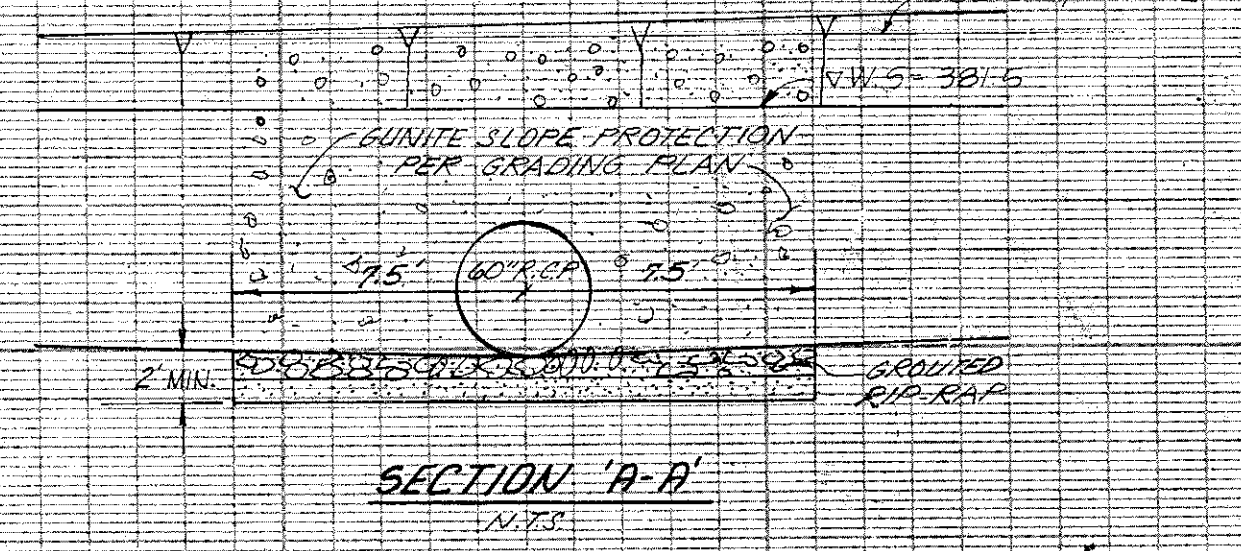
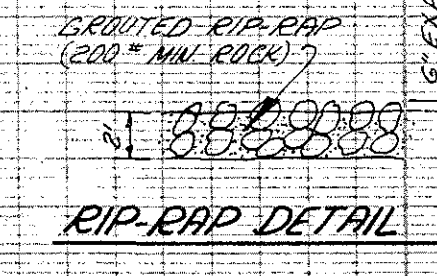
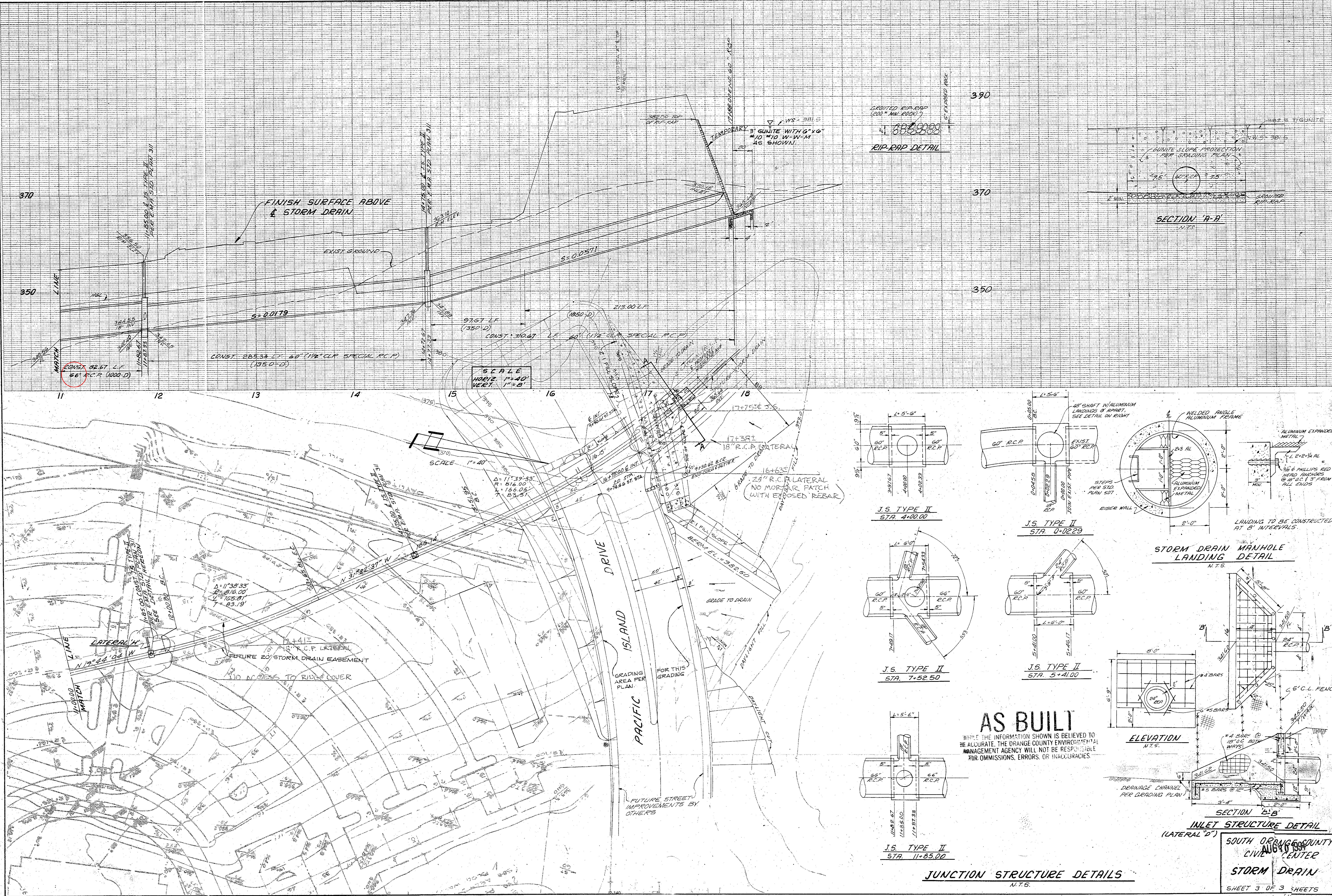
DRAWING NUMBER

SAYDO PRODUCTS • NEW HOPE, MINNESOTA  
REORDER BY PART NUMBER 8522

SAYDO PRODUCTS • NEW HOPE, MINNESOTA  
REORDER BY PART NUMBER 8522

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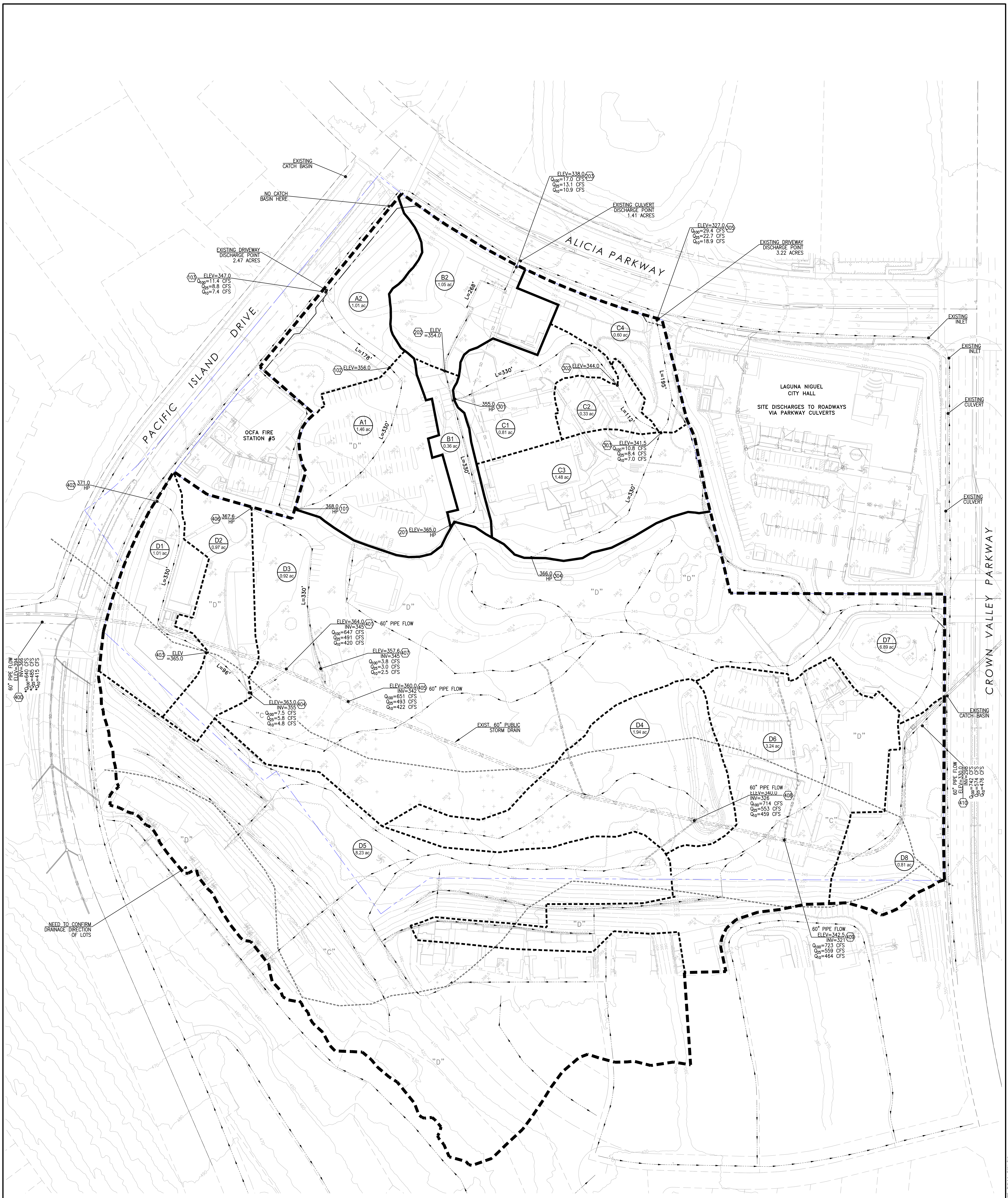


**AS BUILT**  
 WHILE THE INFORMATION SHOWN IS BELIEVED TO BE ACCURATE, THE ORANGE COUNTY ENVIRONMENTAL MANAGEMENT AGENCY WILL NOT BE RESPONSIBLE FOR OMISSIONS, ERRORS, OR INACCURACIES.

**JUNCTION STRUCTURE DETAILS**  
 N.T.S.

**SOUTH ORANGE COUNTY CIVIL CENTER STORM DRAIN**  
 SHEET 3 OF 3 SHEETS  
 AUG 4 1994

APPENDIX 5  
HYDROLOGY MAP  
EXISTING CONDITIONS



**HYDROLOGIC SITE DATA**

GROSS STUDY AREA: 24.4  
 SOIL CLASSIFICATION: "D" AND "C"  
 EXISTING DEVELOPMENT: VACANT LAND AND COMMERCIAL (GOVERNMENT USES)

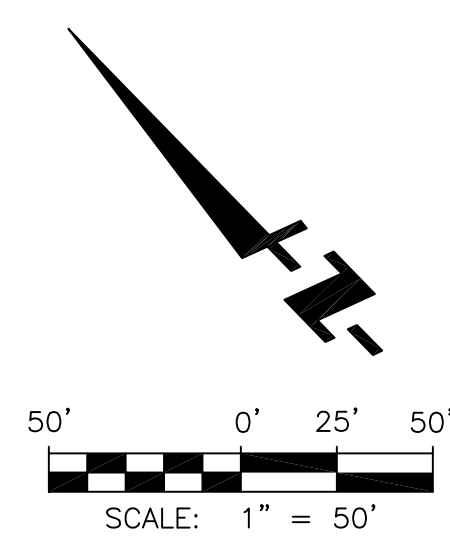
**ABBREVIATIONS:**

AC ACRES  
 CFS CUBIC FEET PER SECOND  
 FS FINISH SURFACE  
 L LENGTH

**LEGEND:**

- RIGHT-OF-WAY LINE
- CENTERLINE
- WATERSHED BOUNDARY
- WATERSHED MAJOR-BOUNDARY
- WATERSHED SUB-BOUNDARY
- SOIL CLASSIFICATION BOUNDARY
- FLOW LINE
- STORM DRAIN LINE
- SUBAREA DESIGNATION AREA (ACRES)
- HYDROLOGY NODE
- CALCULATED RUNOFF (CFS) FOR "X" YEAR FREQUENCY
- SOIL CLASSIFICATION

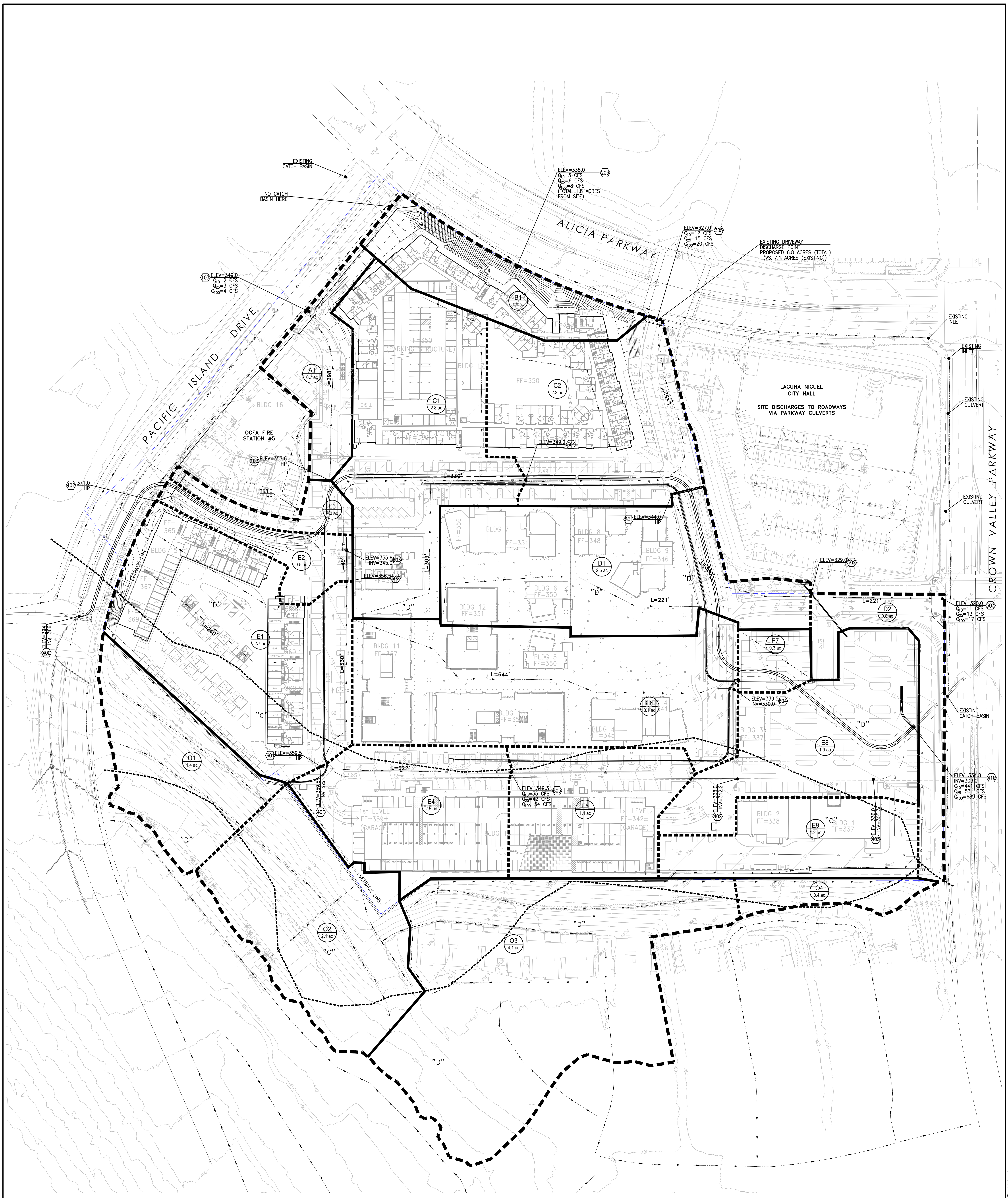
\* RECORD DRAWINGS FOR THE EXIST. 60" PUBLIC STORM DRAIN ONLY HAVE DATA FOR A 10-YEAR STORM EVENT. HIGHER FLOWS FROM UPSTREAM TRIBUTARY AREAS MAY BE INLET CONTROLLED AND NOT BE ABLE TO ENTER THE STORM DRAIN SYSTEM. VALUES SHOWN ARE CALCULATED USING THE LINEAR RELATIONSHIP IN THE REGRESSION EQUATIONS FOR RAINFALL INTENSITY. ACTUAL FLOWS IN THE 60" STORM DRAIN MAY BE LESS.



PREPARED BY:  16795 Von Karman, Suite 100 Irvine, California 92618 tel 949.474.1900 • fax 949.474.5315 www.fuscoe.com	<b>PRELIMINARY EXISTING HYDROLOGY MAP</b> LAGUNA NIGUEL CITY CENTER ALICIA PARKWAY & CROWN VALLEY PARKWAY PREPARED ON: 10/24/2019	SHEET <b>1</b>
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**APPENDIX 6  
HYDROLOGY MAP  
DEVELOPED CONDITIONS**



EXISTING CATCH BASIN  
NO CATCH BASIN HERE

ELEV=338.0  
Q<sub>10</sub>=5 CFS  
Q<sub>25</sub>=6 CFS  
Q<sub>50</sub>=8 CFS  
(TOTAL 1.8 ACRES FROM SITE)

ELEV=327.0  
Q<sub>10</sub>=12 CFS  
Q<sub>25</sub>=15 CFS  
Q<sub>50</sub>=20 CFS

EXISTING DRIVEWAY DISCHARGE POINT PROPOSED 6.8 ACRES (TOTAL) (VS. 7.1 ACRES (EXISTING))

ELEV=349.0  
Q<sub>10</sub>=2 CFS  
Q<sub>25</sub>=3 CFS  
Q<sub>50</sub>=4 CFS

EXISTING INLET  
EXISTING CULVERT

LAGUNA NIGUEL CITY HALL  
SITE DISCHARGES TO ROADWAYS VIA PARKWAY CULVERTS

EXISTING INLET  
EXISTING CULVERT

EXISTING CULVERT

EXISTING CULVERT

EXISTING CULVERT

EXISTING CULVERT

EXISTING CATCH BASIN

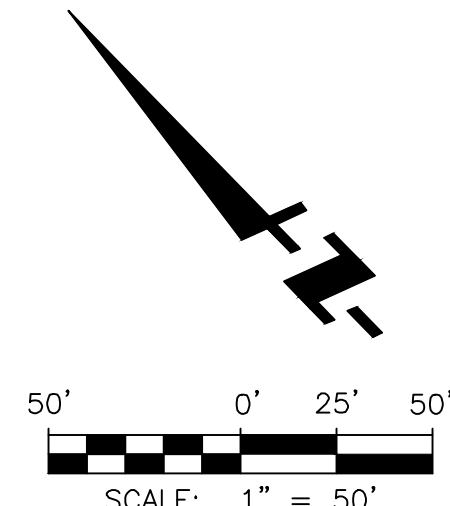
ELEV=320.0  
Q<sub>10</sub>=11 CFS  
Q<sub>25</sub>=13 CFS  
Q<sub>50</sub>=17 CFS

ELEV=334.8  
Q<sub>10</sub>=441 CFS  
Q<sub>25</sub>=531 CFS  
Q<sub>50</sub>=689 CFS

**HYDROLOGIC SITE DATA**  
GROSS STUDY AREA: 24.4  
SOIL CLASSIFICATION: "D" AND "C"  
EXISTING DEVELOPMENT: VACANT & COMMERCIAL (GOVERNMENT)

**ABBREVIATIONS:**  
AC ACRES  
CFS CUBIC FEET PER SECOND  
FS FINISH SURFACE  
L LENGTH

**LEGEND:**  
— RIGHT-OF-WAY LINE  
— CENTERLINE  
- - - WATERSHED BOUNDARY  
- - - WATERSHED MAJOR-BOUNDARY  
- - - WATERSHED SUB-BOUNDARY  
- - - SOIL CLASSIFICATION BOUNDARY  
— FLOW LINE  
- - - STORM DRAIN LINE  
○ SUBAREA DESIGNATION AREA (ACRES)  
○ HYDROLOGY NODE  
○ CALCULATED RUNOFF (CFS) FOR "X" YEAR FREQUENCY  
○ SOIL CLASSIFICATION



PREPARED BY:  
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Irvine, California 92618  
Tel 949.474.1900 • Fax 949.474.5315  
www.fuscoecorp.com

**PRELIMINARY PROPOSED HYDROLOGY MAP**  
LAGUNA NIGUEL CITY CENTER  
ALICIA PARKWAY & CROWN VALLEY PARKWAY  
PREPARED ON: 08/17/2021

SHEET  
**1**