# Draft Environmental Impact Report Technical Appendices

SCH #2020099017

Volume 3 of 3 Appendices F to L

#### **KUDU SOLAR PROJECT**

by 69SV 8ME LLC (8Minute Energy) (PP20405)

Zone Change Case No. 14, Map No. 152; Conditional Use Permit No. 28, Map No. 152; General Plan Amendment No. 10, Map No. 152 (Circulation); Non-Summary Vacations of Public Access Easements



Kern County Planning and Natural Resources Department Bakersfield, California

November 2021

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Kern County Planning and Natural Resources Department

> Technical Assistance by: Michael Baker International

> > November 2021

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# **Appendix F**

**Energy Consumption Technical Memorandum** 

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# Memo

| Date:    | July 16, 2020   |
|----------|---|
| Project: | Kudu Solar Farm Project                                   |
| To:      | Erec DeVost, 8minute Solar Energy                         |
| From:    | Sharyn Del Rosario, Project Manager, HDR                  |
| Subject: | Kudu Solar Farm – Energy Consumption Technical Memorandum |

#### Introduction

This memorandum assesses possible construction and operational energy demand impacts by the development of the Kudu Solar Farm project.

# **Project Description**

The project site is located in portions of unincorporated Kern County and California City, north of the California City Municipal Airport. The majority of the project site is bisected by Washburn Boulevard (which is also the California City boundary) and Neuralia Road. State Route 14, a four-lane divided highway, provides regional access to the project site. The project site is adjacent to the approved Eland Solar Farm, south of the existing Springbok 1 and 2 Solar Farms and southeast of the Los Angeles Department of Water and Power Beacon solar facility.

The project proponent proposes to develop a photovoltaic solar facility and energy storage system capable of producing up to 500 megawatts (MW) of alternating current (AC) power, and 600 MW hours of storage capacity on approximately 1,955 acres of privately-owned land. The project would be supported by a 230-kilovolt gen-tie overhead and/or underground electrical transmission line(s) originating from one or more on-site substations and terminating at the Los Angeles Department of Water and Power's Barren Ridge Substation. The proposed project intends to share the Eland gen-tie line and right-of-way, which may require stringing additional line on the Eland transmission structures, or increasing the capacity of the Eland gen-tie by reconductoring the line with thicker cable. If the proposed project cannot share these facilities, a new gen-tie line would be developed within one of the routes previously analyzed in the Eland Solar Project Supplemental Environmental Impact Report (State Clearinghouse No. 2012011029). The project's permanent facilities would include, service roads, a power collection system, communication cables, overhead and underground transmission lines, electrical switchyards, project substations, energy storage system(s), and operations and maintenance facilities.

The construction period for the proposed project from site preparation through construction, testing, and commercial operation is expected to commence as early as Q4 2021 and would extend for approximately 12 to 18 months.

# **Fuel Consumption Standards of Significance**

The 2019 CEQA Guidelines Appendix G includes Section VI – *Energy*, which is an analysis of potential impacts of a project related to the consumption of energy resources. The thresholds as written in the Guidelines are:

- Would the project result in a potentially significant environmental impact due to wasteful, inefficient, or unnecessary consumption of energy resources, during project construction or operation?
- Would the project conflict with or obstruct a state or local plan for renewable energy or energy efficiency?

While no quantitative thresholds related to energy are included, the Guidelines states as follows:

The goal of conserving energy implies the wise and efficient use of energy. The means of achieving this goal include:

- 1. Decreasing overall per capita energy consumption;
- 2. Decreasing reliance on natural gas and oil, and
- 3. Increasing reliance on renewable energy resources.

# **Fuel Consumption Impact Analysis**

### Methodology

The diesel and gasoline fuel consumptions were calculated using the CO<sub>2</sub> emissions contained in the *Air Quality and Greenhouse Gas Assessment* (Stantec 2020) and EPA's default emission rates of 19.4 pounds of CO<sub>2</sub> per gallon of gasoline and 22.2 pounds of CO<sub>2</sub> per gallon of diesel<sup>1</sup>. The fuel consumption calculations are provided in Appendix A. Fuel consumption calculations are based on the emissions estimates provided in Appendix C of the Kudu Solar Farm Project *Air Quality and Greenhouse Gas Assessment* (Stantec 2020).

#### **CONSTRUCTION PHASE ENERGY USAGE**

**Electricity.** Electricity is not expected to be consumed in large quantity during project construction, as construction equipment and vehicles are typically diesel- or gas-powered, not electric. Electricity for construction would be provided by Southern California Edison and a hookup would be installed on the project site (and this hookup would also provide electricity onsite for the operational phase of the project); however, electricity usage from such connection is anticipated to be minimal (i.e. mostly for security lighting). Therefore, electricity associated with construction-or decommissioning-related activities was not calculated.

<sup>&</sup>lt;sup>1</sup> U.S. EPA, Average Carbon Dioxide Emissions Resulting from Gasoline and Diesel Fuel, February 2005.

**Natural Gas.** Natural gas is not expected to be consumed in large quantity during project construction (i.e., no natural gas-powered equipment or vehicles). Therefore, natural gas associated with construction activities was not calculated.

**Diesel and Gasoline.** Regarding transportation-related fuel consumption during construction, it is assumed that only diesel fuel would be used in off-road construction equipment and for haul trucks used during delivery of solar panels to the project site. On-road vehicles for construction workers are assumed to be solely powered by gasoline.

Construction of the project would result in fuel consumption from the use of construction tools and equipment, haul truck trips, and vehicle trips generated from construction workers traveling to and from the site. Project construction is expected to consume a total of approximately 640,000 gallons of diesel fuel from construction equipment and vendor, hauling, and water truck trips, and approximately 350,000 gallons of gasoline from construction worker vehicle trips.

Construction activities and corresponding fuel energy consumption would be temporary and localized, as the use of diesel fuel and heavy-duty equipment would not be a typical condition of the project. The gasoline consumed during construction represents approximately 0.09 percent of all gasoline sold within Kern County in 2018 (396 millions of gallons) (California Energy Commission 2019). The diesel consumed during project construction would represent approximately 0.6 percent of all diesel sold in Kern County in 2018 (108 millions of gallons) (California Energy Commission 2019). In addition, there are no unusual project characteristics that would cause the use of construction equipment to be less energy efficient compared with other similar construction sites in other parts of the State. Therefore, construction-related fuel consumption by the project would not result in inefficient, wasteful, or unnecessary energy use compared with other construction sites in the region. The project would have a less than significant impact on gasoline and diesel consumption.

#### **OPERATION PHASE ENERGY USAGE**

Operational energy usage would be minimal involving a very limited amount of worker trips for facility maintenance including the occasional washing of solar panels.

**Electricity.** Electricity required during operation (e.g., to operate lights and air conditioners) would be greatly offset by the electricity produced by the solar facility. As discussed in Section 4.8, *Greenhouse Gas Emissions*, of this EIR, construction and operation of renewable energy facilities would offset GHG emissions by replacing energy generated by fossil-fueled power plants. The project would generate solar-generated electricity that would be added to the power grid and be used in place of electricity generated by fossil-fuel sources. Based on these considerations, the project would have a less than significant impact on electricity consumption.

**Natural Gas.** Natural gas is not expected to be consumed during construction, decommissioning-, or operation-related activities by construction equipment (i.e., no natural gaspowered equipment or vehicles). Therefore, the proposed project would have no significant impact on natural gas consumption.

**Diesel and Gasoline.** During operation, it is estimated that the operational and maintenance activities would consume approximately 18,421 gasoline gallons annually. The proposed project would not consume diesel during operation.

# **Potential Changes in Electricity Usage**

No major changes in electricity usage are anticipated throughout the construction and operation of the proposed project. The project would generate solar-generated electricity over a 30-year life span and this production is anticipated to remain relatively constant throughout the operation of the proposed project. Additionally, the electricity required to construct and operate the project is anticipated to be negligible compared to the amount of electricity generated by the project. Activities involved with the decommissioning of the solar facility would be similar to those involved with construction but would be expected to result in lower fuel demand, as technology improves, and equipment becomes more fuel efficient.

# **Compliance with State and Local Renewable Energy Plans**

Executive Order S-14-08

Executive Order S-14-08 was established by California Governor Schwarzenegger in November 2008. The order establishes a Renewables Portfolio Standard (RPS) for all retail sellers of electricity. The specifics of this executive order including the following:

- Requires retail sellers of electricity to serve 33 percent of their load with renewable energy by 2020;
- Requires various state agencies to streamline processes for the approval of new renewable energy facilities and determine priority renewable energy zones; and.
- Establishes the requirement for the creation/adoption of the Desert Renewable Energy Conservation Plan (DRECP) process for the Mojave and Colorado Desert regions.

Climate Change Scoping Plan/California's Renewable Portfolio Standard (RPS) Program

First established in 2002 under Senate Bill (SB) 1078, California's RPS requires retail sellers of electric services to increase procurement from eligible renewable energy resources to 33 percent by 2020 and 50 percent by 2030 (California Public Utilities Commission 2019).

In 2018, SB 100 further increased California's RPS and required retail sellers and local publicly owned electric utilities to procure eligible renewable electricity for 44 percent of retail sales by the end of 2024, 52 percent by the end of 2027, and 60 percent by the end of 2030; and that the California Air Resources Board (CARB) should plan for 100 percent eligible renewable energy resources and zero-carbon resources by the end of 2045. The California Public Utilities Commission (CPUC) and the California Energy Commission jointly implement the RPS program. The CPUC's responsibilities include: (1) determining annual procurement targets and enforcing compliance; (2) reviewing and approving each investor-owned utility's renewable energy procurement plan; (3) reviewing contracts for RPS-eligible energy; and (4) establishing the standard terms and conditions used in contracts for eligible renewable energy. Refer to Section 4.8, *Greenhouse Gas Emissions*, of the Kudu Solar Farm EIR for additional details regarding this regulation.

#### KERN COUNTY GENERAL PLAN

The goals, policies, and implementation measures in the Energy Element of the Kern County General Plan (Kern County 2009) applicable to energy, as related to the project, are provided below. The Kern County General Plan contains additional policies, goals, and implementation measures that are more general in nature and not specific to development such as the project. Therefore, they are not listed below.

#### **Chapter 5. Energy Element**

5.4.5 Solar Energy Development

Goal

Goal 1: Encourage safe and orderly commercial solar development.

**Policies** 

Policy 1: The County shall encourage domestic and commercial solar energy uses to

conserve fossil fuels and improve air quality.

Policy 3: The County should permit solar energy development in the desert and valley

planning regions that does not pose significant environmental or public health and

safety hazards.

#### Construction

Construction equipment would comply with federal, State, and regional requirements where applicable. With respect to truck fleet operators, the U.S. Environmental Protection Agency (USEPA) and National Highway Traffic Safety Administration (NHTSA) have adopted fuel efficiency standards for medium- and heavy-duty trucks. The Phase 1 heavy-duty truck standards apply to combination tractors, heavy-duty pickup trucks and vans, and vocational vehicles for model years 2014 through 2018 and will result in a reduction in fuel consumption from 6 to 23 percent over the 2010 baseline, depending on the vehicle type. The USEPA and NHTSA also adopted the Phase 2 heavy-duty truck standards, which cover model years 2021 through 2027 and require the phase-in of a 5 to 25 percent reduction in fuel consumption over the 2017 baseline depending on the compliance year and vehicle type. The energy modeling for trucks does not take into account specific fuel reductions from these regulations, since they would apply to fleets as they incorporate newer trucks meeting the regulatory standards; however, these regulations would have an overall beneficial effect on reducing fuel consumption from trucks over time as older trucks are replaced with newer models that meet the standards.

In addition, construction equipment and trucks are required to comply with CARB regulations regarding heavy-duty truck idling limits of five minutes at a location and the phase-in of off-road emission standards that result in an increase in energy savings in the form of reduced fuel consumption from more fuel efficient engines. Although these regulations are intended to reduce criteria pollutant emissions, compliance with the anti-idling and emissions regulations would also result in the efficient use of construction-related energy.

#### **Operations**

In order to meet the AB 32 GHG emissions reduction mandate, the Climate Change Scoping Plan relies on achievement of the 33 percent RPS by 2020 and 50 percent by 2030. The project and other similar projects are essential to achieving the RPS. Further, as discussed previously, the project is reasonably expected to displace region-wide and statewide emissions of GHGs over the expected life of the project. The reduction in GHG emissions are a direct result of increasing the share of renewable energy available to investor owned utilities required to meet RPS. The project directly aligns with the goals of RPS by generating solar-generated electricity.

Furthermore, as the project would have an electric power generating capacity of approximately 500 MW alternating current, the project would be consistent with the Attorney General's recommended measures to reduce GHG emissions. Specifically, the project complies with the Attorney General's Recommended Measure to "Install solar and wind power systems, solar and tankless hot water heaters, and energy efficient heating ventilation and air conditioning." Therefore, the project would be compliant with the Attorney General's Recommended Measure regarding renewable energy. Because the project is below regional regulatory thresholds and could result in a reduction of GHG emissions, no mitigation measures are required. Additionally, development of the project would be consistent with the goal and related policies in the Energy Element of the Kern County General Plan to encourage safe and orderly commercial solar development, like the project.

Overall, because the main objectives of the project are to assist California Investor-Owned utilities in meeting their obligations under California's RPS Program and assist California in meeting the GHG emissions reduction goal of 1990 level GHG emissions by 2020, as required by AB 32, and the future reduction goal of 40 percent below 1990 levels by 2030, the project would be compliant with the applicable recommended actions of the CARB Climate Change Scoping Plan, as well as applicable federal, State, and local policies. Specifically, the project would assist the State and regulated utility providers to generate a greater portion of energy from renewable sources consistent with the 2020 and 2030 RPS. Therefore, this impact would be less than significant.

# **Energy Saving Measures Included in the Project**

The construction of the proposed project would result in the annual generation of 500 MW of electricity over a 30-year life span. Because the project is intended to generate electricity from a renewable source of energy, operation of the project would displace energy production that would otherwise be generated by non-renewable energy facilities using either natural gas or coal.

Approximately 398,439 MTCO<sub>2</sub>e of net greenhouse gases annually would be displaced by the implementation of the project. Over the lifetime of the project, the total displaced emissions would be approximately 11,953,170 MTCO<sub>2</sub>e which would assist in the attainment of the State's goal to reduced GHG emissions to 1990 levels by 2020.

#### Conclusion

The construction phase of the proposed project would result in the consumption of approximately 640,000 gallons of diesel fuel and 350,000 gallons of gasoline, while the operation phase would result in a yearly consumption of approximately 18,421 gallons of gasoline annually. The proposed project would not consume diesel during operation. Once operational, the project would result in the annual generation of 500 MW of electricity over a 30-year life span. Because the project is intended to generate electricity from a renewable source of energy, operation of the

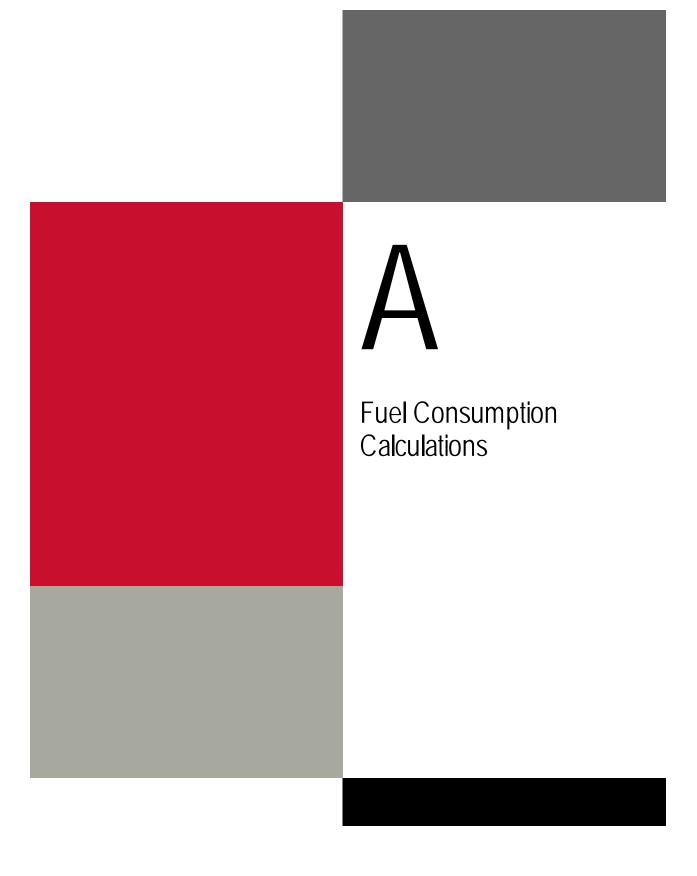
project would displace energy production that would otherwise be generated by non-renewable energy facilities using either natural gas or coal.

The project would therefore not result in potentially significant impacts due to wasteful, inefficient or unnecessary consumption of energy resources. In addition, the project will be consistent and not conflict with or obstruct a State or local plan for renewable energy. Impacts would be less than significant.

#### **RERENCES**

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#### Kudu Solar Project - Energy

#### **Construction Activities**

#### **Construction - Off-road Emissions**

|                                   |                 | CO2 (Metric Tons) |          | Fuel (Gallons) |          |
|-----------------------------------|-----------------|-------------------|----------|----------------|----------|
| Phase                             | Duration (days) | Diesel            | Gasoline | Diesel         | Gasoline |
| Phase 1 - Site Prep and Grading   | 84              | 567.2             | 0.0      | 56,326.5       | 0.0      |
| Phase 2 - Tracker Foundations     | 125             | 1,088.0           | 0.0      | 108,045.3      | 0.0      |
| Phase 3 - Underground Cabling     | 125             | 585.4             | 0.0      | 58,133.9       | 0.0      |
| Phase 4 - Mechanical Installation | 146             | 1,451.5           | 0.0      | 144,143.1      | 0.0      |
| Phase 5 - Electrical Installation | 167             | 1,571.5           | 0.0      | 156,059.9      | 0.0      |
| Tot                               | al              | 5,263.6           | 0.0      | 522,708.7      | 0.0      |

#### **Construction - On-road Emissions**

|                                   |                 | CO2 (Metric Tons) |          | Fuel (Gallons) |           |
|-----------------------------------|-----------------|-------------------|----------|----------------|-----------|
| Phase                             | Duration (days) | Diesel            | Gasoline | Diesel         | Gasoline  |
| Phase 1 - Site Prep and Grading   | 84              | 305.0             | 646.6    | 30,288.4       | 73,479.1  |
| Phase 2 - Tracker Foundations     | 125             | 489.2             | 1,743.9  | 48,580.6       | 198,175.4 |
| Phase 3 - Underground Cabling     | 125             | 74.3              | 62.3     | 7,378.5        | 7,079.7   |
| Phase 4 - Mechanical Installation | 146             | 76.6              | 72.8     | 7,606.9        | 8,272.9   |
| Phase 5 - Electrical Installation | 167             | 217.6             | 572.5    | 21,609.1       | 65,058.4  |
| То                                | tal             | 1,162.7           | 3,098.1  | 115,463.4      | 352,065.5 |

Total Construction Diesel Gallons = 638,172.1 Total Construction Gasoline Gallons = 352,065.5

#### **Operational Activities**

|                          | CO2 (Metric Tons) |        | etric Tons) | Fuel (Gallons) |          |
|--------------------------|-------------------|--------|-------------|----------------|----------|
| Activity                 | Duration (days)   | Diesel | Gasoline    | Diesel         | Gasoline |
| On-road Mobile Emissions | 244               | 0.0    | 162.1       | 0.0            | 18,420.9 |
|                          |                   | 0.0    | 162.1       | 0.0            | 18,420.9 |

Annual Operational Diesel Gallons = 0.0 Annual Operational Gasoline Gallons = 18,420.9

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Appendix G-1
CEQA Level
Geotechnical Study

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# **CEQA Level Geotechnical Study**

California City & Kern County

October 15, 2019

Prepared for:

69SV 8ME LLC c/o 8minute Solar Energy 250 Sutter Street, Suite 600 San Francisco, CA 94108

Prepared by:

Stantec Consulting Services Inc.



#### **CEQA LEVEL GEOTECHNICAL STUDY**

This document entitled CEQA Level Geotechnical Study was prepared by Stantec Consulting Services Inc. ("Stantec") for the account of 69SV 8me LLC (the "Client").

Prepared by

(signature)

Jaret Fischer, PE

Principal Engineer

\_ . . (

(signature)

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Principal, Senior Geotechnical Engineer

Reviewed by

(signature)

**Caitlin Barns** 

Senior Biologist, Project Manager

# **Table of Contents**

| ACRONYMS AND ABBREVIATIONS |                     |  |    |  |
|----------------------------|---------------------|--|----|--|
| EXE                        | CUTIVE SUI          | MMARY                                    | I  |  |
| 1.0                        | PROJECT             | T DESCRIPTION                            | 1  |  |
| 1.1                        |                     | JCTION                                   |    |  |
| 1.2                        |                     | Γ INFORMATION                            |    |  |
|                            | 1.2.1               | Project Site Information                 |    |  |
|                            | 1.2.2               | Location                                 |    |  |
| 1.3                        | DESCRIP             | TION OF PROPOSED PROJECT                 |    |  |
|                            | 1.3.1               | PV Module Configuration                  |    |  |
|                            | 1.3.2               | Inverter Stations                        |    |  |
|                            | 1.3.3               | Energy Storage System                    |    |  |
|                            | 1.3.4               | Substation                               | 5  |  |
|                            | 1.3.5               | Generation-tie Line                      |    |  |
|                            | 1.3.6               | Water Usage                              | 6  |  |
|                            | 1.3.7               | Water Storage Tank(s)                    |    |  |
|                            | 1.3.8               | Operations and Maintenance Building      |    |  |
|                            | 1.3.9               | Project Site Security and Fencing        |    |  |
|                            | 1.3.10              | Project Lighting                         | 7  |  |
| 1.4                        | CONSTR              | UCTION ACTIVITIES                        | 7  |  |
| 1.5                        | WORK FO             | DRCE                                     | 8  |  |
| 1.6                        | PROJEC <sup>1</sup> | Γ FEATURES AND BEST MANAGEMENT PRACTICES | 8  |  |
|                            | 1.6.1               | Waste and Hazardous Materials Management | 3  |  |
|                            | 1.6.2               | Spill Prevention and Containment         |    |  |
|                            | 1.6.3               | Wastewater/Septic System                 |    |  |
|                            | 1.6.4               | Inert Solids                             |    |  |
|                            | 1.6.5               | Health and Safety                        | 9  |  |
| 2.0                        | STUDY M             | IETHODS                                  | 10 |  |
| 2.1                        |                     | E AND SCOPE OF WORK                      |    |  |
| 2.2                        |                     | D ACTIVITIES                             |    |  |
| 2.2<br>2.4                 |                     | PLORATION ACTIVITIES                     |    |  |
|                            |                     |  |    |  |
| 2.5                        | LABORA              | TORY SOIL TESTING                        | 12 |  |
| 3.0                        |                     | S  |    |  |
| 3.1                        |                     | AL GEOLOGY                               |    |  |
| 3.2                        | SUBSURI             | FACE CONDITIONS IN TEST PIT EXPLORATIONS | 15 |  |
| 3.3                        | REGIONA             | AL GROUNDWATER                           | 15 |  |
| 3.4                        |                     | AL SEISMICITY                            |    |  |
| -                          | 3.4.1               | Fault Rupture Hazard                     |    |  |
|                            | 3.4.2               | Strong Ground Shaking                    |    |  |
|                            | 3.4.3               | Liquefaction                             |    |  |
|                            | 3.4.4               | Lateral Spreading                        | 19 |  |



| 3.5   | SUBSID       | ENCE                                     | 19  |
|-------|--------------|--|-----|
| 3.6   | EXPANS       | SIVE SOIL POTENTIAL                      | 20  |
| 3.7   | SLOPES       | S  | 20  |
| 3.8   | EROSIC       | DN                                       | 20  |
| 4.0   | CONCL        | USIONS                                   | 21  |
| 5.0   | REFERE       | ENCES                                    | 23  |
| LIST  | OF TABL      | ES                                       |     |
| Table | : 1: Kudu F  | Parcels                                  | 1   |
|       |              | ary of Laboratory Tests                  |     |
|       |              | within 30 Miles of the Project Area      |     |
| LIST  | OF FIGUR     | RES                                      |     |
| Figur | e 1. Site Lo | ocation Map                              | 11  |
|       |              | ırface Exploration Map                   |     |
|       |              | nal Geologic Map                         |     |
| Figur | e 4. Regio   | nal Faulting and Seismicity              | 18  |
| LIST  | OF APPE      | NDICES                                   |     |
| APPI  | ENDIX A      | TEST PIT LOGS                            | A.1 |
| APPI  | ENDIX B      | LABORATORY TEST RESULTS                  | B.1 |
| APPI  | ENDIX C      | CEQA GUIDELINES FORM – GEOLOGY AND SOILS | C.1 |

# **Acronyms and Abbreviations**

AC alternating electrical current

Applicant 69SV 8me LLC

ASTM ASTM International

CAL California

CDMG California Department of Conservation, Department of

Mines and Geology

CEQA California Environmental Quality Act

CO<sub>2</sub>e Carbon dioxide equivalent
CUP Conditional Use Permit

CGS California Geological Survey

Client 69SV 8me LLC

DC direct electrical current

DWR California Department of Water Resources

ESS Energy Storage System

g acceleration due to gravity

gen-tie generation tie

ISO International Organization for Standardization

kV kilovolt
MW megawatt

MWh megawatt-hour

O&M operations and maintenance

Project Kudu Solar Farm Project

PV photovoltaic

SCE Southern California Edison

Stantec Stantec Consulting Services Inc.

USCS Unified Soil Classification System

USCS Unified Soil Classification System

USGS U.S. Geological Survey



i

# **Executive Summary**

Stantec Consulting Services Inc. (Stantec) has prepared this California Environmental Quality Act (CEQA) Level Geotechnical Study for the proposed Kudu Solar Farm Project (Project), located approximately one mile northeast of the intersection of the State Route (SR) 14 and Phillips Road, in California City and unincorporated Kern County, California. 69SV 8me LLC (Applicant) is seeking approval of a conditional use permit (CUP) for the construction of an up to 500-megawatt (MW) alternating electrical current (AC) utility-scale solar farm with an up to 500 megawatt-hour (MWh) Energy Storage System (ESS). The Project is comprised of 79 assessor's parcels (Project area) totaling about 2,136 gross acres.

This geotechnical investigation report outlines subsurface information for the Project area, describes methods undertaken to excavate and sample test pits and perform soil mechanics laboratory testing on select soil samples, and presents results of Stantec's evaluations of the geotechnical properties of soils pertinent to the CEQA Guidelines and recommended mitigation.

Nineteen shallow test pits (KTP1 through KTP15 and KTP17 through KTP20) were advanced at locations throughout the Project area to a depth of 10 feet using a California (CAL) sampler and following ASTM International (ASTM) D3550 (Standard Practice for Ring-Lined Barrel Sampling of Soils) procedures. Disturbed bulk samples were excavated at locations where CAL sampling could not be completed. Samples were classified in the field using the Unified Soil Classification System (USCS), in accordance with ASTM D2488 (Standard Practice for Description and Identification of Soils [Visual-Manual Method]) procedures. The laboratory testing confirmed or modified field classifications for presentation on the boring logs.

The near surface (approximately 10 feet deep) soils encountered in the test pits performed are composed of sand (SP, SW, SW-SM, and SM USCS soil type), silt (ML USCS soil type), and gravel (GP and GP-GM USCS soil type). Near surface sandy soil with variable amounts of silt, gravel, and cobbles were encountered in most of the test pits. The near surface low plasticity silts were dry and were encountered in test pit KTP-2, KTP-4, KTP-11, and KTP-19 between approximately 2.5 and 10 feet. The near surface gravels were dry and encountered in test pit KTP17 through KTP19 between the ground surface and the maximum depth of exploration. Slight to moderately cemented soils were encountered at depths between approximately 7 feet and 10 feet in KTP-2, KTP-4, KTP-17, KTP-18, and KTP-20, respectively. Cobbles were encountered in KTP-7, KTP-8, KTP-15, and KTP-17 through KTP-20. Groundwater was not encountered in the test performed for this investigation, but groundwater data from a production well on the eastern end of the Project indicates that the depth to groundwater is approximately 255 feet below the ground surface (DWR 2010).

The Project site is not located within currently a mapped Alquist-Priolo Special Studies Fault Zone, California Liquefaction Hazard Zone, or subsidence area, and is not located near free faces, steep slopes, or bodies of water. Therefore, the following geologic hazards are considered to be low-risk: fault rupture, liquefaction-related ground failure including liquefaction, lateral spreading, subsidence, presence of expansive soils, and landslides. However, the predominately coarse-grained soils underlying the site are potentially susceptible to erosion or the loss of topsoil due to surface water flows. In addition, strong ground shaking can be expected at the site during moderate to severe earthquakes in the general region. This is common to most areas in southern California.



#### **CEQA LEVEL GEOTECHNICAL STUDY**

Mitigation of soil erosion may include selective grading, establishment of anchoring vegetation, design of runoff control features such as drainage ditches, and construction of erosion control features such as pavements and surface mats. These mitigation options should be addressed in the design level evaluations for the Project.



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### 1.0 PROJECT DESCRIPTION

#### 1.1 INTRODUCTION

Stantec Consulting Services Inc. (Stantec) has prepared this California Environmental Quality Act (CEQA) Level Geotechnical Study to provide support documentation for the Environmental Checklist Form in accordance with the CEQA Guidelines for the proposed Kudu Solar Farm, located approximately 1 mile northeast of the intersection of the State Route (SR) 14 and Phillips Road, in California City and unincorporated Kern County, California.

#### 1.2 PROJECT INFORMATION

69SV 8me LLC (applicant) is seeking approval of a conditional use permits (CUPs) for the construction and operation of an up to 500 megawatt (MW)-alternating electrical current (AC) utility-scale solar farm with energy storage, known as the Kudu Solar Project (Project) in unincorporated Kern County and California City, California (Figure 1). The applicant proposes to construct, own, and operate the Project and would secure CUPs from both Kern County and California City along with permits from other relevant agencies as required by law.

#### 1.2.1 Project Site Information

The Project is comprised of 79 assessor's parcels (Project area) totaling approximately 2,136 gross acres (Table 1). The permanent disturbance acreage associated with development of the solar facility and associated infrastructure (Project site) within the Project area would be less than the gross acreage of the Project area. The Project area is adjacent to the approved Eland 1 Solar Farm, south of the existing Springbok 1 & 2 Solar Farms, and southeast of the Los Angeles Department of Water and Power (LADWP) Beacon Solar facility. The topography of the Project area is relatively flat.

#### 1.2.2 Location

The Project area is located in portions of unincorporated Kern County and California City, north of the California City Municipal Airport. The majority of the Project is bisected by Washburn Boulevard (which is also the California City boundary) and Neuralia Road (Figure 1).

**Table 1: Kudu Parcels** 

| No.             | APN             | Acres  |  |  |  |
|-----------------|-----------------|--------|--|--|--|
| California City | California City |        |  |  |  |
| 1               | 302-020-08      | 40.17  |  |  |  |
| 2               | 302-020-09      | 80.09  |  |  |  |
| 3               | 302-020-11      | 163.68 |  |  |  |
| 4               | 302-020-14      | 40.99  |  |  |  |
| 5               | 302-020-15      | 10.52  |  |  |  |
| 6               | 302-020-16      | 10.15  |  |  |  |



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| No.                | APN                   | Acres    |
|--------------------|-----------------------|----------|
| 7                  | 302-020-17            | 9.59     |
| 8                  | 302-020-18            | 9.98     |
| 9                  | 302-290-03            | 83.58    |
| 10                 | 302-305-15            | 43.54    |
| 11                 | 302-321-01            | 160.93   |
| 12                 | 302-322-01            | 10.10    |
| 13                 | 302-322-02            | 10.09    |
| 14                 | 302-322-04            | 10.24    |
| 15                 | 302-322-05            | 10.28    |
| 16                 | 302-322-06            | 40.04    |
| 17                 | 302-322-08            | 10.33    |
| 18                 | 302-322-09            | 40.50    |
| 19                 | 302-322-10            | 10.27    |
| 20                 | 302-322-11            | 10.29    |
| 21                 | 302-325-49            | 9.74     |
| 22                 | 302-330-33            | 20.21    |
| 23                 | 302-330-37            | 20.38    |
| 24                 | 302-341-29            | 168.79   |
| 25                 | 302-342-01            | 40.23    |
| 26                 | 302-342-11            | 2.67     |
| 27                 | 302-342-12            | 2.66     |
| 28                 | 302-342-19            | 29.69    |
| 29                 | 302-342-25            | 40.77    |
| 30                 | 302-342-26            | 39.89    |
| 31                 | 302-342-27            | 40.29    |
| 32                 | 302-342-28            | 40.68    |
| 33                 | 302-470-14            | 20.20    |
|                    | California City Total | 1,281.51 |
| Unincorporated Ker | n County              |          |
| 34                 | 469-170-10            | 10.02    |
| 35                 | 469-170-18            | 39.49    |
| 36                 | 470-020-08            | 2.31     |
| 37                 | 470-020-19            | 4.38     |
| 38                 | 470-030-01            | 79.22    |
| 39                 | 470-080-15            | 20.27    |
| 40                 | 470-080-16            | 10.07    |
| 41                 | 470-080-17            | 10.10    |



| No. | APN        | Acres |
|-----|------------|-------|
| 42  | 470-080-32 | 10.07 |
| 43  | 470-100-08 | 64.83 |
| 44  | 470-100-09 | 81.11 |
| 45  | 470-151-09 | 19.62 |
| 46  | 470-151-15 | 20.23 |
| 47  | 470-151-16 | 20.40 |
| 48  | 470-151-17 | 19.98 |
| 49  | 470-152-01 | 39.32 |
| 50  | 470-152-18 | 10.32 |
| 51  | 470-152-19 | 4.93  |
| 52  | 470-302-24 | 2.59  |
| 53  | 470-302-25 | 2.62  |
| 54  | 470-302-26 | 2.52  |
| 55  | 470-322-13 | 2.39  |
| 56  | 470-322-15 | 9.96  |
| 57  | 470-322-39 | 2.37  |
| 58  | 470-330-01 | 5.06  |
| 59  | 470-330-02 | 4.77  |
| 60  | 470-330-03 | 19.86 |
| 61  | 470-330-04 | 20.15 |
| 62  | 470-330-06 | 9.95  |
| 63  | 470-330-07 | 10.02 |
| 64  | 470-330-14 | 4.89  |
| 65  | 470-330-15 | 5.23  |
| 66  | 470-350-04 | 18.65 |
| 67  | 470-350-05 | 18.91 |
| 68  | 470-350-06 | 18.89 |
| 69  | 470-350-07 | 18.57 |
| 70  | 470-350-08 | 19.93 |
| 71  | 470-360-01 | 18.43 |
| 72  | 470-360-02 | 17.85 |
| 73  | 470-360-05 | 21.15 |
| 74  | 470-360-06 | 32.23 |
| 75  | 470-380-01 | 19.92 |
| 76  | 470-380-04 | 21.35 |
| 77  | 470-380-05 | 17.34 |
| 78  | 470-380-06 | 19.88 |



| No.           | APN                              | Acres    |
|---------------|----------------------------------|----------|
| 79 470-380-07 |                                  | 21.95    |
|               | Unincorporated Kern County Total | 854.10   |
|               | Total                            | 2,135.61 |

Note:

APN = Assessor Parcel Number

#### 1.3 DESCRIPTION OF PROPOSED PROJECT

The applicant proposes to develop a photovoltaic (PV) energy facility and energy storage system (ESS) that is capable of producing up to 500 MW of AC power, and 600 MW hours (MWh) of storage capacity. Power generated by the Project would be collected using up to 230 kilovolt (kV) collector lines which run underground and/or overhead to a dedicated Project substation, or to the Eland 1 Substation. The Project may also share the Eland 1 generation tie- (gen-tie) line facilities, or gen-tie rights-of-way. The Eland 1 substation and gen-tie line have gone through environmental analysis and subsequent approval by Kern County and are not part of the Project.

Additionally, the Project may share an operations & maintenance (O&M) building, ESS, and/or transmission facilities, as necessary, with one or more nearby solar Projects, and/or may be remotely operated. Any unused O&M building, substation, and/or transmission facility areas onsite may be covered by solar panels under such scenarios.

The applicant has considered the following in its selection of the Project site for detailed evaluation:

- Land availability (approximately 2,136 gross acres)
- · Land use zoning: primarily agriculture located away from high-density residential developments
- Proximity to interconnecting substation (approximately 7 miles away) and ability to share facilities with other solar Projects

Up to 20 full-time employees would operate the Project. Typically, most staff would work during the day shift (sunrise to sunset), and the remainder would work during the night shifts and weekends. If the Project shared O&M, substation, and/or transmission facilities with one or more nearby solar Projects, and/or became remotely, the Project's onsite staff could be reduced.

After the useful life of the Project, the panels would be disassembled from the mounting frames, and the Project site would be restored to its pre-development condition.

#### 1.3.1 PV Module Configuration

The Project would use PV panels or modules<sup>1</sup> on mounting frameworks to convert sunlight into electricity. Individual panels would be installed on either fixed-tilt or tracker mount systems (single- or dual- axis, using galvanized steel or aluminum). If the panels are configured for fixed tilt, they would be oriented toward the south. For tracking systems, the panels would rotate to follow the sun over the course of the day. Although the panels could stand up to 20 feet

<sup>&</sup>lt;sup>1</sup> Including but not limited to bi-facial or concentrated photovoltaic (CPV) technology



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high, depending on the mounting system used and county building codes, panels are expected to remain between 6 and 8 feet high.

The foundations for the mounting structures can extend up to 10 feet below ground, depending on the mounting structure, soil conditions, and wind loads, and may be encased in concrete or use small concrete footings. Final solar panel layout and spacing would be optimized for site characteristics and the desired energy production profile.

#### 1.3.2 Inverter Stations

Direct Current (DC) energy is delivered from the panels via cables to inverter stations, generally located near the center of each block. Inverter stations convert the DC energy to AC energy, which can be dispatched to the transmission system. Inverter stations are typically comprised of one or more inverter modules with a rated power of up to 2 MW each, a unit transformer, and voltage switch gear. The unit transformer and voltage switch gear are housed in steel enclosures, while the inverter module(s) are housed in cabinets. Depending on the supplier selected, the inverter station may lie within an enclosed or canopied metal structure, typically on a skid or concrete mounted pad.

#### 1.3.3 Energy Storage System

The Project may include one or more ESS, located at or near a substation/switchyard (onsite or shared) and/or at the inverter stations, or elsewhere onsite. Such large-scale ESSs would be up to 600 MW AC in capacity and occupy up to 25 acres in total area. ESSs consist of modular and scalable battery packs and battery control systems that conform to U.S. national safety standards. The ESS modules, which could include commercially available lithium or flow batteries, typically consist of International Organization of Standardization (ISO) standard containers (40 feet long by 8 feet wide by 8 feet high) housed in pad- or post-mounted, stackable metal structures, but may also be housed in a dedicated building(s) in compliance with applicable regulations. The maximum height of the structure is not expected to exceed 25 feet. The actual dimensions and number of energy storage modules and structures would vary depending on the application, supplier, and configuration chosen, as well as on offtaker/power purchase agreement requirements and on county building standards. The Project may share an ESS with one or more nearby solar Projects or may operate one or more standalone ESS facilities within the Project site.

#### 1.3.4 Substation

Output from the inverter stations would be transferred via electrical conduits and electrical conductor wires to one or more Project substations or switchyards (collectively referred to as substations herein), or the Eland 1 Substation. The Project and any associated ESS would have their own dedicated substation equipment located either within the Project site, or within the Eland 1 Substation footprint. Dedicated equipment may incorporate several components, including auxiliary power transformers, distribution cabinets, revenue metering systems, a microwave transmission tower, and voltage switch gear. Each substation would occupy an area of up to approximately 5 acres, secured separately by a chain-link fence. The final location(s) of each component would be determined before the issuance of building permits.

Substations typically include a small control building (roughly 500 square feet) standing 10 feet tall. The building would either be prefabricated concrete or steel housing, with rooms for the voltage switch gear and metering



equipment, a room for the station supply transformer, and a separate control technology room within which the main computer, intrusion detection system, and main distribution equipment are housed. Components of this building (e.g., control technology room and intrusion detection system) may instead be located at an O&M building below.

#### 1.3.5 Generation-tie Line

Power generated by the Project would be transmitted to the Los Angeles Department of Water and Power (LADWP) Barren Ridge Substation via a 230kV overhead and/or underground generation-tie (gen-tie). The Project intends to share the Eland 1 gen-tie line and right-of-way, which may require stringing additional line on the Eland 1 transmission structures or increasing the capacity of the Eland 1 gen-tie by reconductoring the line with thicker cable. If the Project cannot share these facilities, a new gen-tie line would be developed within one of the routes previously analyzed in the Eland 1 Environmental Impact Report.

#### 1.3.6 Water Usage

Water demand for panel washing and O&M use is not expected to exceed 50 acre-feet per year (afy). Water usage during construction, primarily for dust-suppression purposes, is not expected to exceed 400 acre-feet (af). It is anticipated that water would be obtained from existing onsite wells. Alternatively, water may be obtained from one or more offsite source(s) and delivered to the Project area via truck. If offsite water is used, it would likely be obtained from one of the nearby Springbok Projects, the Eland 1 Project, or from a commercial source. If the applicant determines that offsite water would be used, the applicant would submit a Will Serve Letter from the proposed offsite water purveyor(s). A small water treatment system may be installed to provide deionized water for panel washing.

#### 1.3.7 Water Storage Tank(s)

One or more aboveground water storage tanks with a total capacity of up to 50,000 gallons may be placed onsite near the O&M building. The storage tank(s) near the O&M building would have the appropriate fire department connections to be used for fire suppression.

#### 1.3.8 Operations and Maintenance Building

The Project may include an O&M building approximately 40 feet long by 80 feet wide, with associated onsite parking. The O&M building would be steel framed, with metal siding and roof panels. The O&M building may include the following:

- 1. Office
- 2. Repair building/parts storage
- 3. Control room
- 4. Restroom
- 5. Septic tank and leach field

Roads, driveways, and parking lot entrances would be constructed in accordance with Kern County and California City improvement standards. Parking spaces and walkways would be constructed in conformance with all California accessibility regulations.



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#### 1.3.9 Project Site Security and Fencing

The Project site would be enclosed within a chain link fence with barbed wire measuring up to 8 feet above finished grade. An intrusion alarm system would be integrated into the perimeter fence, with intrusion detection cabinets placed every 1,500 feet along the perimeter fence. An intrusions control unit or similar technology may include additional security measures including but not limited to barbed wire, low voltage fencing with warning reflective signage, controlled access points, security alarms, security camera systems, and security guard vehicle patrols to deter trespassing and/or unauthorized activities.

Gates would be maintained at the main entrances to the Project site to restrict access. Project site access would be provided to offsite emergency responders in the event of an after-hours emergency. Enclosure gates would be manually operated with a key provided in an identified key box location.

#### 1.3.10 Project Lighting

Project lighting would be directed away from public rights-of-way and would be minimal. Site lighting may include motion sensor lights for added security purposes. Lighting would be of the lowest intensity, in compliance with any applicable regulations, measured at the property line after dark.

#### 1.4 CONSTRUCTION ACTIVITIES

Site preparation through construction, testing, and commercial operation, is expected to commence as early as Q4 2021 and would extend for 12 to 18 months.

Construction would include the following:

- site preparation
- grading and earthwork
- · concrete foundations
- structural steel work
- electrical/instrumentation work
- collector line installation
- architecture and landscaping

No roads would be affected by the Project, except during construction. Construction traffic would access the site from Philips Road, Gantt Road, and Neuralia Road, or through the Eland 1 Project site. Up to 1,000 workers per day (during peak construction periods) would be required during the construction of the Project.

Heavy construction would occur between 6:00 AM and 5:00 PM, Monday through Friday. Additional hours may be necessary to make up schedule deficiencies or to complete critical construction activities. Some activities may continue 24 hours per day, seven days per week. Low-level noise activities may occur between 10:00 PM and 7:00 AM. Nighttime activities could include but are not limited to refueling equipment, staging materials, quality assurance and control, and commissioning.



Truck deliveries would normally occur during daylight. However, there would be offloading and/or transporting to the Project area on weekends and during evenings.

Earth moving is expected to be limited to the construction of the access roads, O&M building, substation, ESS(s), and any stormwater protection or storage (detention) facilities. Final grading may include revegetation with low growing or applying earth-binding materials to disturbed areas.

#### 1.5 WORK FORCE

Once the Project is constructed, maintenance would generally be limited to the following:

- 1. Cleaning of PV panels
- 2. Monitoring electricity generation
- 3. Providing site security
- 4. Facility maintenance: replacing or repairing inverters, wiring, and PV modules

The project would require up to 20 full-time O&M employees. If the project uses shared O&M, substation, ESS, and/or transmission facilities with any future projects share personnel would reduce O&M staff.

The facility would operate seven days a week, 24 hours a day, generating electricity during normal daylight hours when the solar energy is available. Maintenance activities may occur seven days a week, 24 hours a day to ensure PV panel output when solar energy is available.

#### 1.6 PROJECT FEATURES AND BEST MANAGEMENT PRACTICES

The following sections describe standard Project features and best management practices that would be applied during construction and long-term operation of the Project to maintain safety and minimize or avoid environmental impact.

#### 1.6.1 Waste and Hazardous Materials Management

The Project would have minimal levels of materials onsite that have been defined as hazardous under 40 Code of Federal Regulations (CFR), Part 261. The following materials are expected to be used during the construction, operation, and long-term maintenance of the Project:

- · Insulating oil: used for electrical equipment
- Lubricating oil: used for maintenance vehicles
- Various solvents and detergents: equipment cleaning
- Gasoline: used for maintenance vehicles

Hazardous materials and wastes would be managed, used, handled, stored, and transported in accordance with applicable local and state regulations. All hazardous wastes would be maintained at quantities below the threshold requiring a Hazardous Material Management Program (HMMP): one 55-gallon drum. Though not expected, should any onsite storage of hazardous materials exceed one 55-gallon drum, an HMMP would be prepared and implemented.



#### 1.6.2 Spill Prevention and Containment

Less than 55 gallons of hazardous materials would be stored onsite. Spill prevention and containment for construction and operation of the Project would adhere to the Environmental Protection Agency's guidance on Spill Prevention Control and Countermeasures.

#### 1.6.3 Wastewater/Septic System

A standard onsite septic tank and leach field may be used at the O&M building to dispose sanitary wastewater and would be designed to meet O&M guidelines required by Kern County laws, ordinances, regulations, and standards.

#### 1.6.4 Inert Solids

Inert solid wastes resulting from construction activities may include recyclable items such as paper, cardboard, solid concrete and block, metals, wire, glass, type 1-4 plastics, drywall, wood, and lubricating oils. Non-recyclable items include insulation, other plastics, food waste, vinyl flooring and base, carpeting, paint containers, packing materials, and other construction wastes. A construction waste management plan would be prepared for review by the county and California City. Consistent with local regulations and the California Green Building Code, the plan would provide for diversion of a minimum of 50 percent of construction waste from landfill.

Chemical storage tanks (if any) would be designed and installed to meet applicable local and state regulations. Any wastes classified as hazardous, such as solvents, degreasing agents, concrete curing compounds, paints, adhesives, chemicals, or chemical containers, would be stored in an approved storage facility/shed/structure and disposed of as required by local and state regulations. Material quantities of hazardous wastes are not expected.

#### 1.6.5 Health and Safety

Safety precautions and emergency systems would be implemented as part of the design and construction of the Project to ensure safe and reliable operation. Administrative controls would include classroom and hands-on training in O&M procedures, general safety items, and a planned maintenance program. These would work with the system design and monitoring features to enhance safety and reliability.

The Project would have an emergency response plan (ERP). The ERP would address potential emergencies including chemical releases, fires, and injuries. All employees would be provided with communication devices, cell phones, or walkie-talkies to provide aid in the event of an emergency.



# 2.0 STUDY METHODS

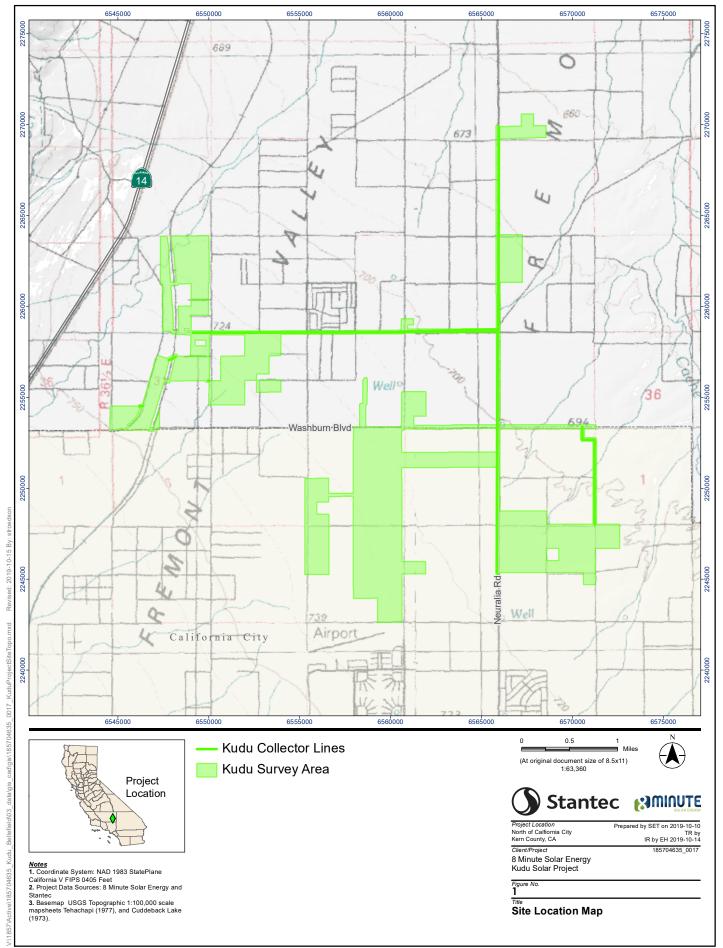
## 2.1 PURPOSE AND SCOPE OF WORK

- Review available subsurface information for the sites,
- excavate and sample 19 test pits to a depth of 10 feet,
- perform soil mechanics laboratory testing on select soil samples,
- evaluate geotechnical properties of soils pertinent to the CEQA Guidelines, and
- summarize findings, conclusions, and recommendations in this study.

#### 2.2 PRE-FIELD ACTIVITIES

Test pit locations were selected based on review of conceptual development plans and confirmed in the field at the time of field sampling. In addition, a site-specific Health and Safety Plan was developed in accordance with California Occupational Safety and Health Administration requirements to guide field activities.





#### 2.4 FIELD EXPLORATION ACTIVITIES

Nineteen shallow test pits (KTP1 through KTP15 and KTP17 through KTP20) were advanced at selected locations throughout the site to a depth of 10 feet (Figures 2 and 3). Relatively undisturbed samples were obtained using a modified California (CAL) sampler, which is a ring-lined split tube sampler with a 3-inch outer diameter and 2.5-inch inner diameter. CAL sampling followed ASTM International (ASTM) D3550 (Standard Practice for Ring-Lined Barrel Sampling of Soils) procedures. Disturbed bulk samples were excavated at locations where CAL sampling could not be completed. The CAL sampler was advanced with a backhoe bucket.

Samples were classified in the field using the United Soil Classification System (USCS), in accordance with ASTM D2488 (Standard Practice for Description and Identification of Soils [Visual-Manual Method]) procedures. The laboratory testing confirmed or modified field classifications as necessary for presentation on the boring logs. Soil samples were removed from the samplers, placed in appropriate containers, and transported in accordance with ASTM D4220 (Standard Practice for Preserving and Transporting Soil Samples).

The test pit logs are located in Appendix A. Soils are classified in accordance with the USCS, which is explained in "Symbols and Terms Used on Borehole and Test Pit Records" in Appendix A. The approximate test pit locations are shown on Figures 2 and 3.

#### 2.5 LABORATORY SOIL TESTING

The following laboratory tests were performed on samples collected at the Site either in general accordance with the ASTM or contemporary practices of the soil engineering profession (Table 2):

**Table 2. Summary of Laboratory Tests** 

| Type of Test                               | ASTM Designation        | Number<br>Performed |
|--|-------------------------|---------------------|
| Sieve Analysis                             | ASTM D422 and ASTM C136 | 18                  |
| Materials Finer than 75 μm (No. 200) Sieve | ASTM D1140              | 1                   |
| Atterberg Limits                           | ASTM D4318              | 1                   |
| Chemical Tests for Corrosion Potential     | Caltrans test methods   | 3                   |

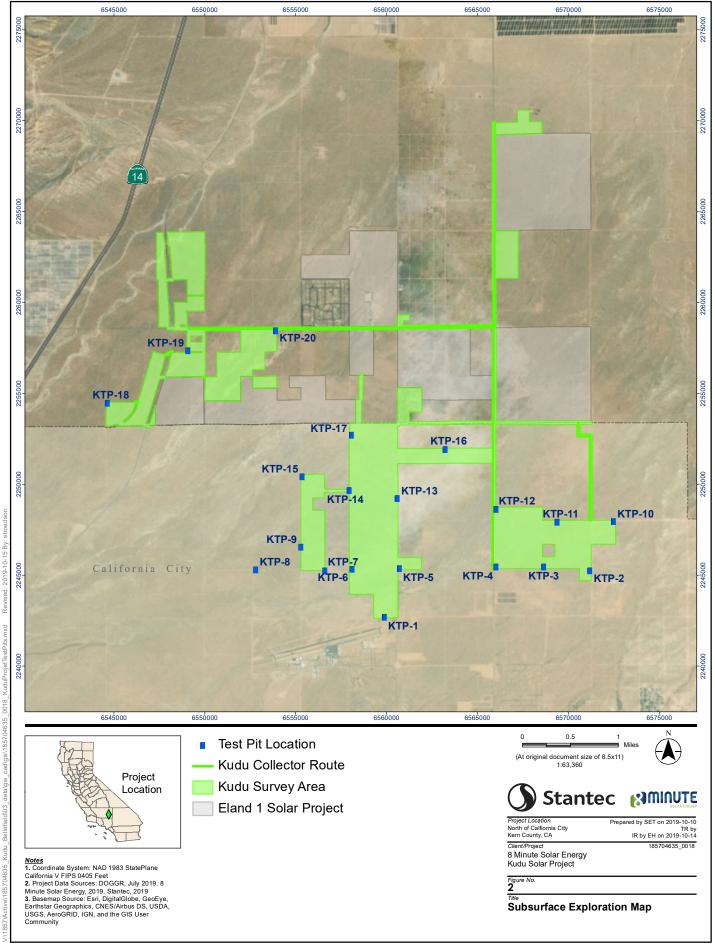
Notes:

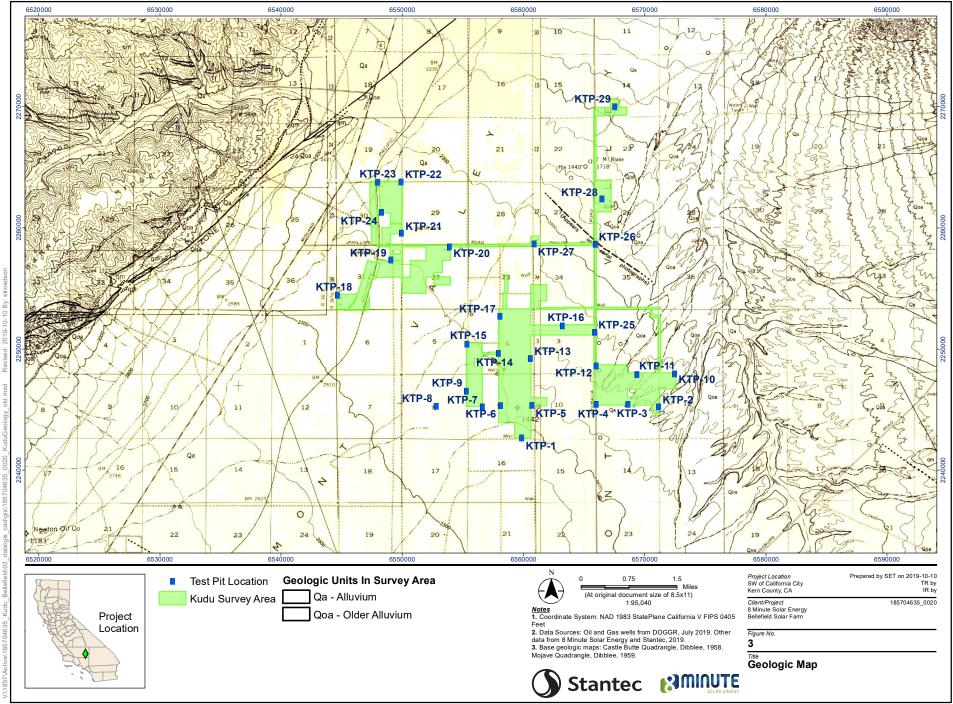
ASTM = ASTM International

Caltrans = California Department of Transportation

The results of the laboratory tests are presented in Appendix B.







#### 3.0 RESULTS

#### 3.1 REGIONAL GEOLOGY

The site is located in the western portion of the Mojave Desert Geomorphic Province in the southern part of California. The surface topography within the province is controlled by two sets of faults—a prominent northwest to southeast trending set and a secondary set trending east to west.

According to the California Geological Survey (CGS) website, the Mojave Desert Geomorphic Province is a broad interior region of isolated mountains separated by desert plains with an enclosed drainage system. The Mojave Desert Geomorphic Province is wedged in a sharp angle between the San Andreas and Garlock faults (CGS 2008). Displacement along both faults is predominantly strike slip (right-lateral in the case of the San Andreas Fault; left lateral in the case of the Garlock Fault).

Geologic mapping presented in the United States Geological Survey (USGS) Geologic Map of the Mojave Quadrangle (USGS, 1959) indicates the Site is underlain by Quaternary Alluvium and Quaternary Older Alluvium deposits. Literature from the CGS indicates the alluvium and older alluvium deposits include unconsolidated and undissected valley fill derived from adjacent highlands consisting of cobbles, gravel, sand, and silt.

#### 3.2 SUBSURFACE CONDITIONS IN TEST PIT EXPLORATIONS

The near surface (approximately 10 feet deep) soils encountered in the test pits performed are composed of sand (SP, SW, SW-SM, and SM USCS soil type), silt (ML USCS soil type), and gravel (GP and GP-GM USCS soil type). Near surface sandy soil with variable amounts of silt, gravel, and cobbles were encountered in most of the test pits. The near surface low plasticity silts were dry and were encountered in test pit KTP-2, KTP-4, KTP-11, and KTP-19 between approximately 2.5 and 10 feet. The near surface gravels were dry and encountered in test pit KTP17 through KTP19 between the ground surface and the maximum depth of exploration. Slight to moderately cemented soils were encountered at depths between approximately 7 feet and 10 feet in KTP-2, KTP-4, KTP-17, KTP-18, and KTP-20, respectively. Cobbles were encountered in KTP-7, KTP-8, KTP-15, and KTP-17 through KTP-20.

The subsurface soils were not difficult to penetrate, and the test pit excavations did not cave to the maximum depth of exploration during the course of the field investigation program. Groundwater was not encountered during this investigation.

#### 3.3 REGIONAL GROUNDWATER

Fremont Valley Groundwater Basin underlies the western portion of the Mojave Desert and is part of the South Lahontan Hydrologic Region. The basin is bounded on the northwest by the Garlock Fault Zone, on the east by crystalline rocks of the Summit Range, Red Mountain, Lava Mountains, Rand Mountains, Castle Butte, Bissel Hills, and Rosamond Hills, and on the southwest and southeast by the Antelope Valley Groundwater Basin (DWR 2004).

Static groundwater was not encountered in the test performed for this investigation. Groundwater data from a production well on the eastern end of the Project indicates that the depth to groundwater is approximately 255 feet



below the ground surface (DWR 2010). Groundwater levels may fluctuate in the future due to rainfall, irrigation, broken pipes, or changes in site drainage.

#### 3.4 REGIONAL SEISMICITY

The Project site is located within a highly active seismic zone. A regional faulting and seismicity map is presented in Figure 4. This fault map also provides information regarding recent earthquakes in the Project area. Several of the more recent earthquakes in the Project area include the 1992 Johnson earthquake, the 1992 Big Bear earthquake, the 1994 Northridge earthquake, and the 1999 Hector Mine earthquake (CGS 1999).

The estimated distance of the site to the nearest expected surface expression of an active fault is presented in Table 3. The distance measurement was taken from a location in the middle of the site as the site lies between the Garlock (Center) and Garlock (West) faults; the closest active faults relative to the site. The location from which measurements were obtained has a latitude of 35.179540°, and a longitude of -118.011887°.

Table 3. Faults within 30 Miles of the Project Area

| Fault                              | Distance<br>(miles) <sup>1</sup> | Maximum Moment<br>Magnitude <sup>1</sup> |
|------------------------------------|----------------------------------|--|
| Garlock (West)                     | 4.2                              | 7.5                                      |
| Garlock (Center)                   | 7.2                              | 7.7                                      |
| South Sierra Nevada                | 7.9                              | 7.5                                      |
| Lenwood-Lockhart-Old Woman Springs | 13.5                             | 7.5                                      |
| Helendale – South Lockhart         | 24.0                             | 7.4                                      |
| South San Andreas                  | 29.6                             | 8.1                                      |

Note:

#### 3.4.1 Fault Rupture Hazard

The site is not located within a currently mapped Alquist-Priolo Special Studies Fault Zone (CDMG 2002). As noted above, the nearest active faults area the Garlock (West) and Garlock (Center) fault, located approximately 4 miles northwest and 7 miles northeast of the Site, respectively. The Garlock (Center) fault trace is shown in Figure 4 relative to the project site. As shown on Figure 4, the Garlock (Center) fault trace trends in a northeast – southwest direction. The fault trace does project toward a portion of the site. Based on proximity, the Garlock (Center) fault is considered to be the fault most likely to cause surface rupture at the project site. There is potential for surface rupture of the Garlock (Center). Based on the fault's distance from the project site and since the fault does project towards the project in the southeast portion of the site, it is our opinion that the potential for surface fault rupture to occur on the project site is moderate.

#### 3.4.2 Strong Ground Shaking

Strong ground shaking can be expected at the site during moderate to severe earthquakes in the general region. This is common to most areas in southern California.



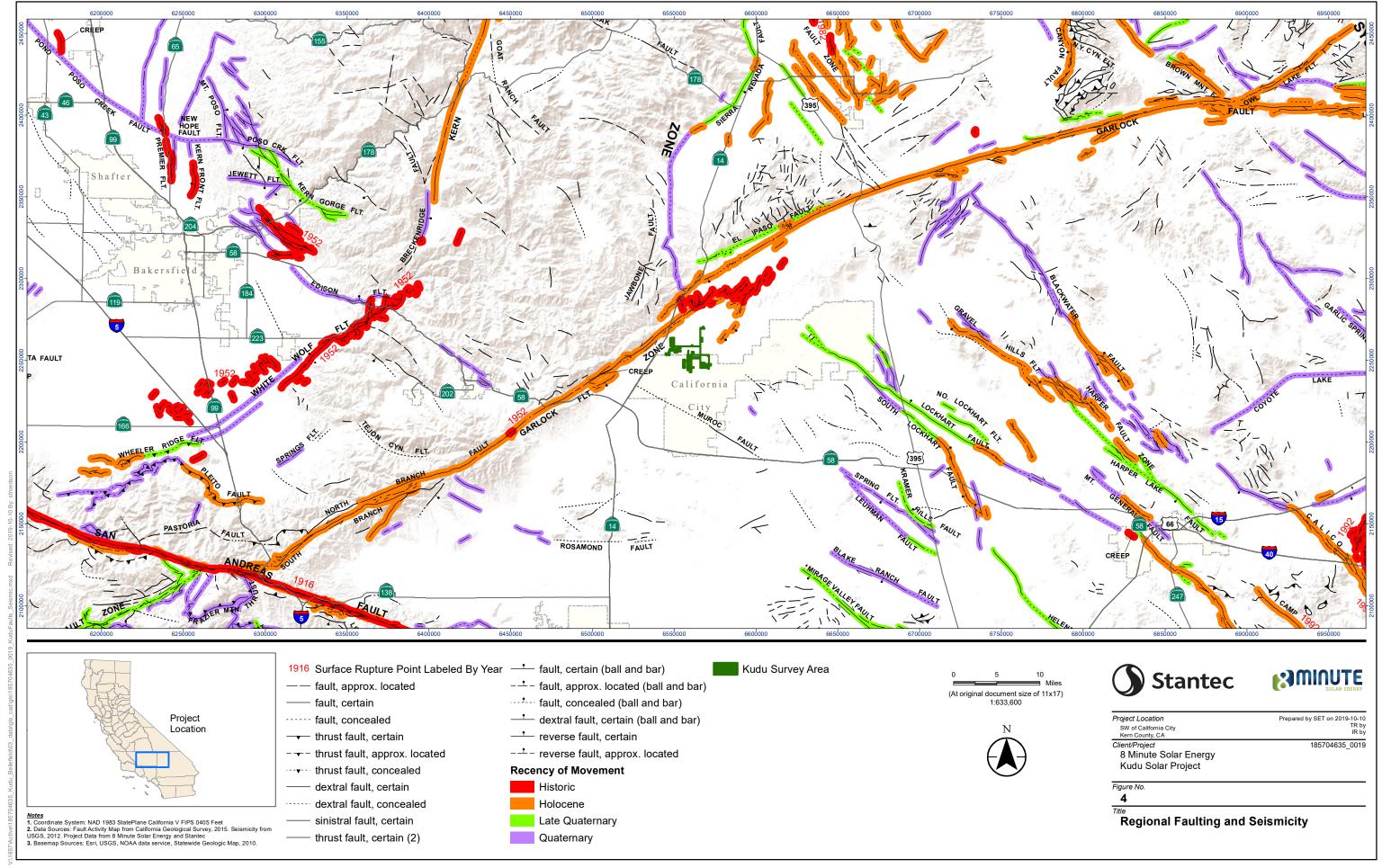
<sup>1.</sup> Measured from 2008 National Seismic Hazard Maps—Source Parameters Website—USGS (USGS 2008).

#### **CEQA LEVEL GEOTECHNICAL STUDY**

Information published by USGS indicates the peak ground acceleration with a 2 percent probability of being exceeded at the site in 50 years is 0.56g (USGS 2008), where g is the acceleration due to gravity determined in accordance with the U.S. Seismic Design Maps web site. Mitigation of strong ground shaking is typically provided by designing structures in accordance with the latest addition of the California Building Code.



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#### 3.4.3 Liquefaction

Liquefaction of saturated sandy soils is generally caused by the sudden decrease in soil shear strength due to vibration. During cyclic shaking typically caused by an earthquake, the soil mass is distorted, and inter-particle stresses are transferred from the soil particles to the pore water. As pore pressure increases, the bearing capacity decreases, and the soil may behave temporarily as a viscous fluid (liquefaction), and consequently loses its capacity to support the structures founded thereon.

Engineering research of soil liquefaction potential (Seed, et al. 1985, Seed and Idris 1982) indicates that generally, the following three basic factors must exist concurrently for liquefaction to occur:

- A source of ground shaking such as an earthquake capable of generating soil mass distortions.
- A relatively loose sandy soil fabric exhibiting a potential for volume reduction.
- A relative shallow groundwater table (within approximately 50 feet below ground surface) or completely saturated soil conditions that would allow positive pore pressure generation.

The site is not located within a current, mapped California Liquefaction Hazard Zone. In addition, groundwater in the Project area is expected to be approximately 133 feet below the ground surface (DWR 2010). Based on the near surface soil conditions and depth to groundwater, it is our opinion that the potential for liquefaction-related ground failure, including liquefaction, is low.

#### 3.4.4 Lateral Spreading

Lateral spreading typically occurs as a form of horizontal displacement of relatively flat-lying alluvial material toward an open or "free" face such as an open body of water, channel, or excavation. This movement is generally due to failure along a weak plane and may often be associated with liquefaction. As cracks develop within the weakened material, blocks of soil displace laterally toward the open face. Cracking and lateral movement may gradually propagate away from the face as blocks continue to break free.

Due to the low potential for liquefaction, the depth of groundwater, and the fact that the site is not located near free faces or bodies of water, the potential for lateral spreading is considered low.

#### 3.5 SUBSIDENCE

Groundwater levels in the Antelope Valley adjacent to the east of the Fremont Valley where the site is located have declined more than 270 feet since the 1970s (USGS 2017) in some parts of the groundwater basin, especially near the City of Lancaster. These groundwater-level declines have caused the aquifer system to compact, resulting in land subsidence. Land subsidence within the Antelope Valley has been most recently evaluated by the USGS through the use of Interferometric Synthetic Aperture Radar between 1992 and 2009 (USGS 2000). Based on these recent studies, the site is not within an area that has sustained measurable subsidence due to groundwater draw down. Due to the depth of groundwater and the fact that the site is not located in a mapped subsidence area, the potential for subsidence is considered low.



#### 3.6 EXPANSIVE SOIL POTENTIAL

Expansion and contraction of volume can occur when expansive soils undergo alternating cycles of wetting (swelling) and drying (shrinking). Since near-surface soils encountered during the recent geotechnical investigation are mostly sandy soils whose expansion potential is considered low, special design for expansive soils would likely not be necessary for the proposed development.

#### 3.7 SLOPES

The site is relatively flat, with a topographic gradient less than 2 percent. Permanent slopes steeper than 5:1 (horizontal to vertical) or higher than 5 feet are not anticipated to be constructed or built upon for the Project. Due to the existing topography and the proposed grading, landslides are not considered a potential hazard for the Project. The stability of slopes, if any, should be verified when design-grading information becomes available.

#### 3.8 EROSION

The predominantly coarse-grained soils underlying the site are potentially susceptible to erosion or the loss of topsoil due to surface water flows.

Mitigation of soil erosion may include selective grading, establishment of anchoring vegetation, design of runoff control features such as drainage ditches, and construction of erosion control features such as pavements and surface mats. These mitigation options should be addressed in the design-level evaluations for the Project.



## 4.0 CONCLUSIONS

Based on the currently planned development, it is our opinion that the soils would require additional assessment to determine mitigation measures for strong ground shaking and erosion.

Mitigation options for these hazards are provided in the preceding sections. Impacts should be mitigated through the application of standard conditions of development, which require preparation of a design-level geotechnical study as a condition of grading permit issuance.

Based on the findings of this CEQA Level Geotechnical Study, a completed CEQA questionnaire for the Geology and Soils Section has been included as Appendix C. As recommended above, items checked as "Less than Significant with Mitigation" should be addressed in the scope of a future design-level geotechnical investigation.





## 5.0 REFERENCES



## **CEQA LEVEL GEOTECHNICAL STUDY**

Appendix A Test Pit Logs

# Appendix A TEST PIT LOGS



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING:

COMPLETED: 8/28/19 INSTALLATION: STARTED 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-01** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 9' 17.824" GROUND ELEV (ft): 2394

INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

LOGGED BY: **GB** 

EASTING (ft):

LONGITUDE: -118° 0' 21.528"

Stantec

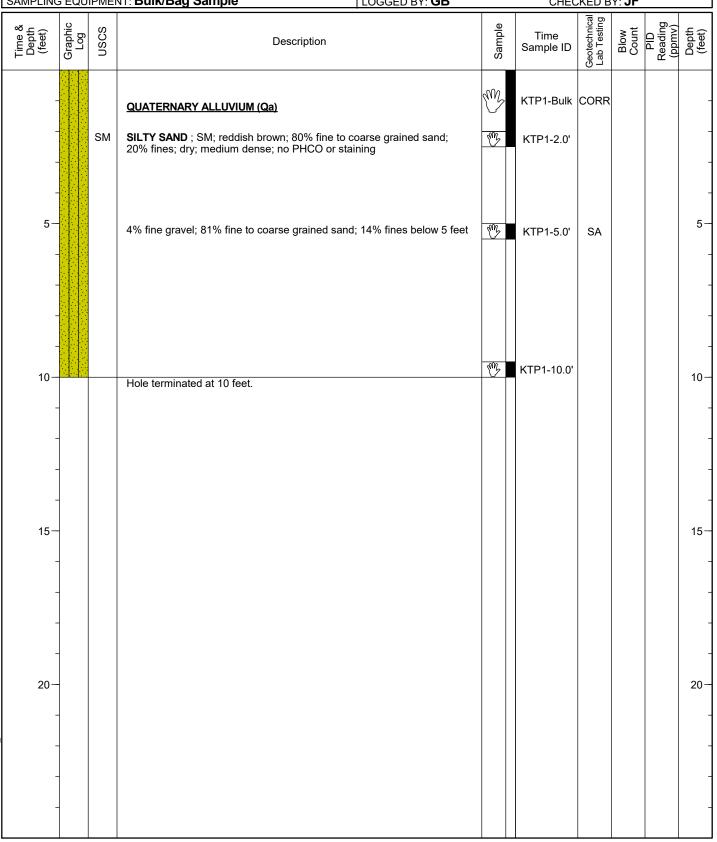
TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING: INSTALLATION: STARTED 8/28/19

COMPLETED: 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-02** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 9' 44.51"

GROUND ELEV (ft): 2337 INITIAL DTW (ft): NE

STATIC DTW (ft): **NE** WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -117° 58' 5.948"

Stantec

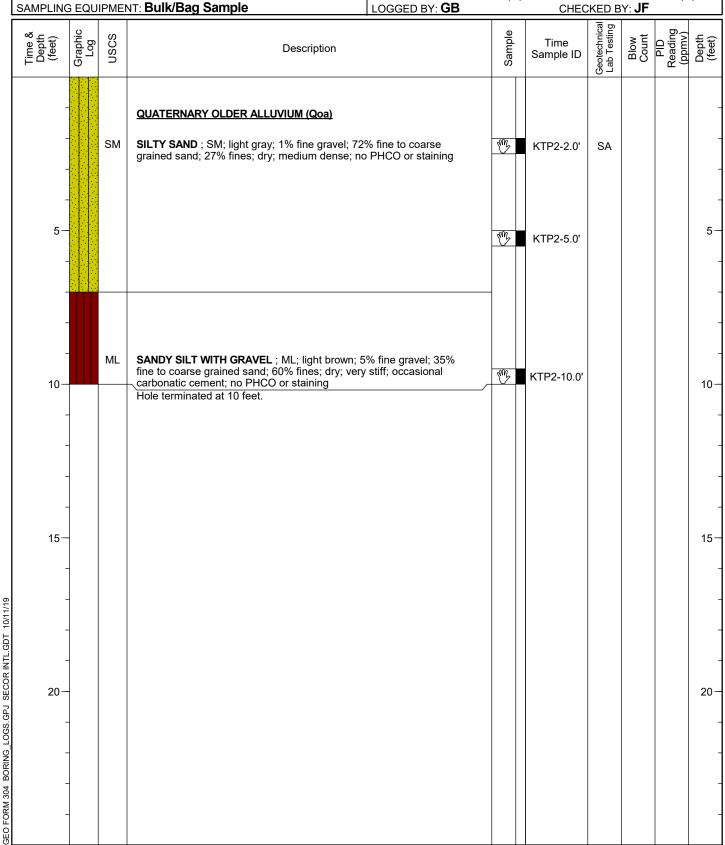
TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING: INSTALLATION: STARTED 8/28/19

COMPLETED: 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-03** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 9' 45.155" GROUND ELEV (ft): 2335

INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

LOGGED BY: **GB** 

EASTING (ft):

LONGITUDE: -117° 58' 35.933

Stantec

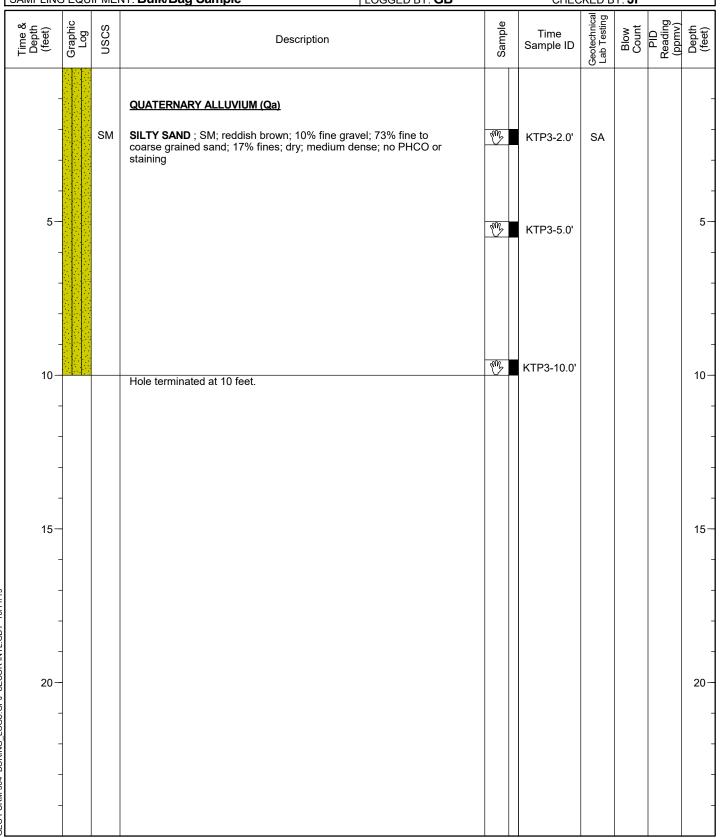
TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING:

COMPLETED: 8/28/19 INSTALLATION: STARTED 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-04** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 9' 45.166" GROUND ELEV (ft): 2345

INITIAL DTW (ft): NE STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -117° 59' 7.426"

Stantec

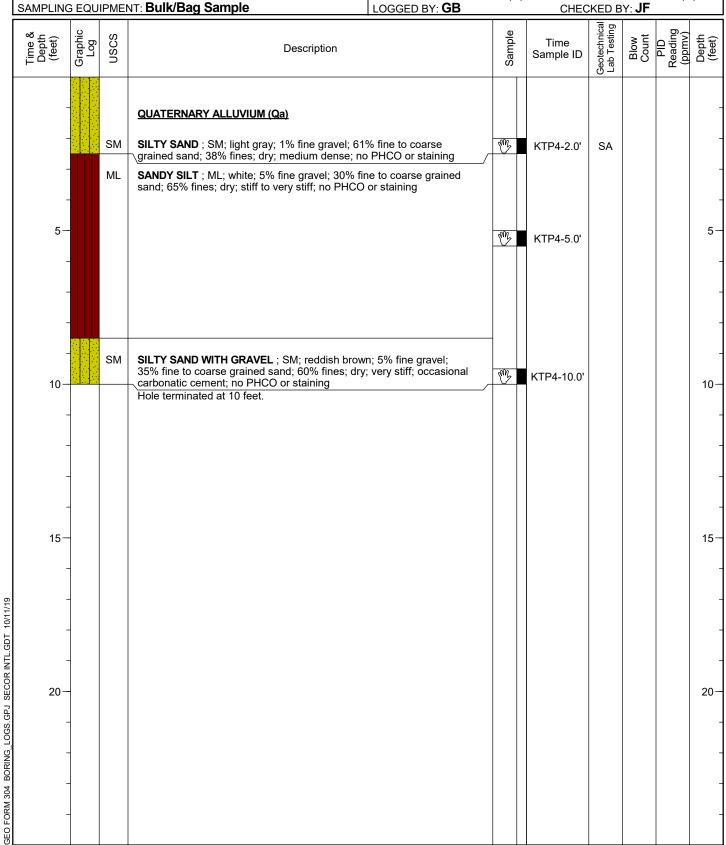
TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING:

COMPLETED: 8/28/19 INSTALLATION: STARTED 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING FOUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-05** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 9' 44.456" GROUND ELEV (ft): 2379

INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

LOGGED BY: GB

EASTING (ft):

LONGITUDE: -118° 0' 13.5"

Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF

| SAMPLING EQUIPMENT: Bulk/Bag Sample LOGGED BY: GB CHECKED BY: JF                                     |   |      |   |   |        |                   |                             |               |                          |                     |
|--|---|------|---|---|--------|-------------------|-----------------------------|---------------|--------------------------|---------------------|
| Time &<br>Depth<br>(feet)  | Graphic<br>Log                            | nscs | Description   |   | Sample | Time<br>Sample ID | Geotechnical<br>Lab Testing | Blow<br>Count | PID<br>Reading<br>(ppmv) | Depth<br>(feet)     |
|  |   | SM   | QUATERNARY ALLUVIUM (Qa)  WELL GRADED SAND WITH GRAVEL; SM; ligh gravel; 81% fine to coarse grained sand; 11% fin no PHCO or staining | t gray; 8% fine<br>es; dry; medium dense;   | 4m     | KTP5-2.0'         | SA                          |               |                          | -                   |
| 5-   |   | SP   | POORLY GRADED SAND; SP; reddish brown; 1 fine to coarse grained sand; 5% fines; dry; mediu staining                                   | 0% fine gravel; 85%<br>im dense; no PHCO or | dus.   | KTP5-5.0'         |                             |               |                          | 5-                  |
| 10-  | - (1) (1) (1) (1) (1) (1) (1) (1) (1) (1) |      | Hole terminated at 10 feet.   |   | anz.   | KTP5-10.0'        |                             |               |                          | 10                  |
| 15-  | -<br>-<br>-                               |      |   |   |        |                   |                             |               |                          | -<br>15 —<br>-<br>- |
| GEO FORM 304 BORING LOGS, GPJ SECOR IN L.GDI 1071719  50  61  62  64  64  64  64  64  64  64  64  64 | -   |      |   |   |        |                   |                             |               |                          | 20 -                |

LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/27/19 DRILLING: INSTALLATION: STARTED 8/27/19 COMPLETED: 8/27/19 COMPLETED: 8/27/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-06** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 9' 44.01" GROUND ELEV (ft): 2403

INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -118° 0' 42.66"

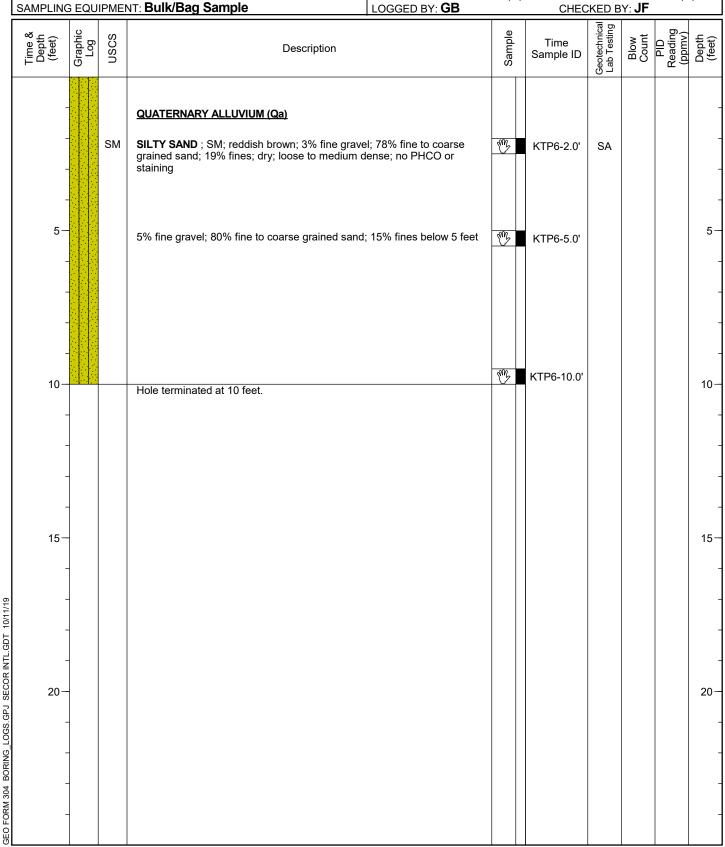
Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/27/19 DRILLING:

COMPLETED: 8/27/19 INSTALLATION: STARTED 8/27/19 COMPLETED: 8/27/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching

WELL / TEST PIT / BOREHOLE NO:

## **KTP-07** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 9' 43.369" GROUND ELEV (ft): 2412

INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -118° 1' 3.439"

Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

| SAMPLIN   | SAMPLING EQUIPMENT: Bulk/Bag Sample LOGGED BY: GB |      |   |                             |                |                   | KED B                       | Y: <b>JF</b>  | `                        | ,               |
|---|---|------|---|-----------------------------|----------------|-------------------|-----------------------------|---------------|--------------------------|-----------------|
| Time &<br>Depth<br>(feet)                                 | Graphic<br>Log                                    | nscs | Description   |                             | Sample         | Time<br>Sample ID | Geotechnical<br>Lab Testing | Blow<br>Count | PID<br>Reading<br>(ppmv) | Depth<br>(feet) |
|   |   | SM   | QUATERNARY ALLUVIUM (Qa)  SILTY SAND; SM; reddish brown; 1% fine gravel; 59 grained sand; 40% fines; dry; loose; no PHCO or sta | 9% fine to coarse<br>aining | un a           | KTP7-2.0'         | SA                          |               |                          |                 |
| 5-  |   |      | 5% fine gravel; 80% fine to coarse grained sand; 15   | % fines below 5 feet        | m <sub>2</sub> | KTP7-5.0'         |                             |               |                          | 5-              |
|   |   |      | Occasional cobbles up to 5 inches in diameter below   | v 7 feet                    |                |                   |                             |               |                          | -               |
| 10-   |   |      | Hole terminated at 10 feet.   |                             | W.S.           | KTP7-10.0'        |                             |               |                          | 10-             |
|   | -<br>-  |      |   |                             |                |                   |                             |               |                          | -               |
| 15-   | _   |      |   |                             |                |                   |                             |               |                          | 15-             |
| INTL:GDT 10/11/19   | -   |      |   |                             |                |                   |                             |               |                          | -<br>-          |
| 20 - 20 - 20 - 20 - 20 - 20 - 20 - 20 -                   | _   |      |   |                             |                |                   |                             |               |                          | 20-             |
| GEO FORM 304 BORING_LOGS, GPJ SECOR INTL. GDT 10/11/19 00 | -<br>-<br>-                                       |      |   |                             |                |                   |                             |               |                          | -<br>-<br>-     |
| GEO   |   |      |   |                             |                |                   |                             |               |                          |                 |

LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/27/19 DRILLING:

COMPLETED: 8/27/19 INSTALLATION: STARTED 8/27/19 COMPLETED: 8/27/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching

WELL / TEST PIT / BOREHOLE NO:

## **KTP-08** PAGE 1 OF 1

NORTHING (ft): LATITUDE: **35° 12' 46.519"** 

GROUND ELEV (ft): 2335 INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -118° 2' 33.27"

Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 11.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

| SAMPLING                  | SAMPLING EQUIPMENT: Bulk/Bag Sample LOGGED BY: GB CHECKED BY: JF |      |   |  |        | .,                |                             |               |                          |                 |
|---------------------------|--|------|---|--|--------|-------------------|-----------------------------|---------------|--------------------------|-----------------|
| Time &<br>Depth<br>(feet) | Graphic<br>Log   | nscs | Description   |  | Sample | Time<br>Sample ID | Geotechnical<br>Lab Testing | Blow<br>Count | PID<br>Reading<br>(ppmv) | Depth<br>(feet) |
| -                         |  | SM   | QUATERNARY ALLUVIUM (Qa)  SILTY SAND; SM; reddish brown; 7% fine grave grained sand; 9% fines; dry; loose to medium de staining | el; 84% fine to coarse<br>nse; no PHCO or      | M.     | KTP8-2.0'         | SA                          |               |                          | -               |
| 5-                        |  | SP   | POORLY GRADED SAND WITH GRAVEL; SP; I gravel; 90% fine to coarse grained sand; 5% fine up to 6 inches in diameter               | ight brown; 5% fine<br>s below 5 feet; cobbles | W      | KTP8-5.0'         |                             |               |                          | 5-              |
| 10-                       |  |      | Hole terminated at 11 feet.   |  | W.     | KTP8-10.0'        |                             |               |                          | 10              |
| 15                        |  |      |   |  |        |                   |                             |               |                          | 15 -            |
| 20 -                      |  |      |   |  |        |                   |                             |               |                          | 20-             |

LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING:

COMPLETED: 8/28/19 INSTALLATION: STARTED 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-09** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 9' 59.188" GROUND ELEV (ft): 2423

INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -118° 1' 16.014"

Stantec

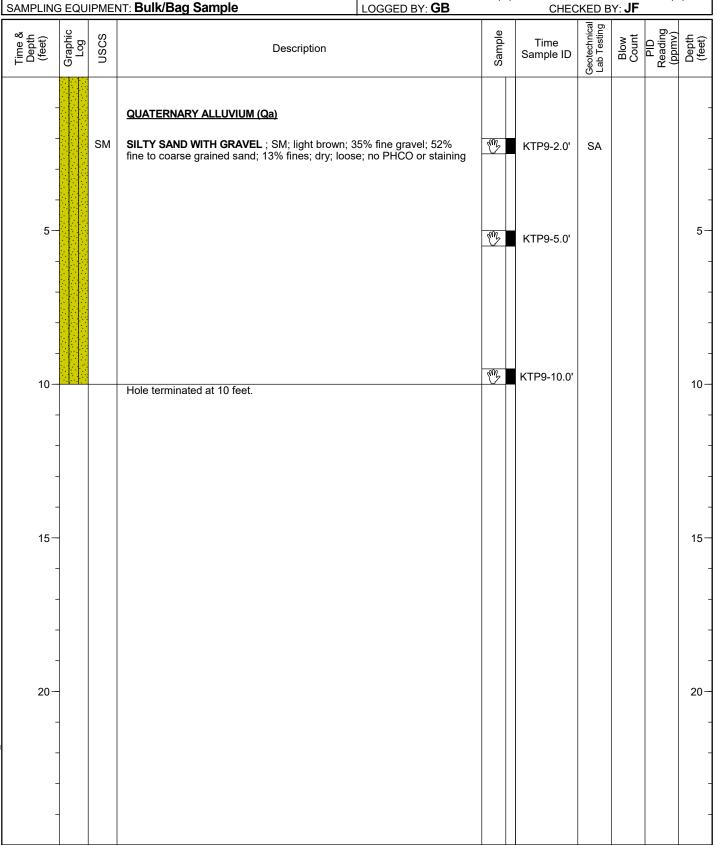
TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING:

COMPLETED: 8/28/19 INSTALLATION: STARTED 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-10** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 10' 9.131" GROUND ELEV (ft): 2318

INITIAL DTW (ft): NE STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -117° 57' 49.759

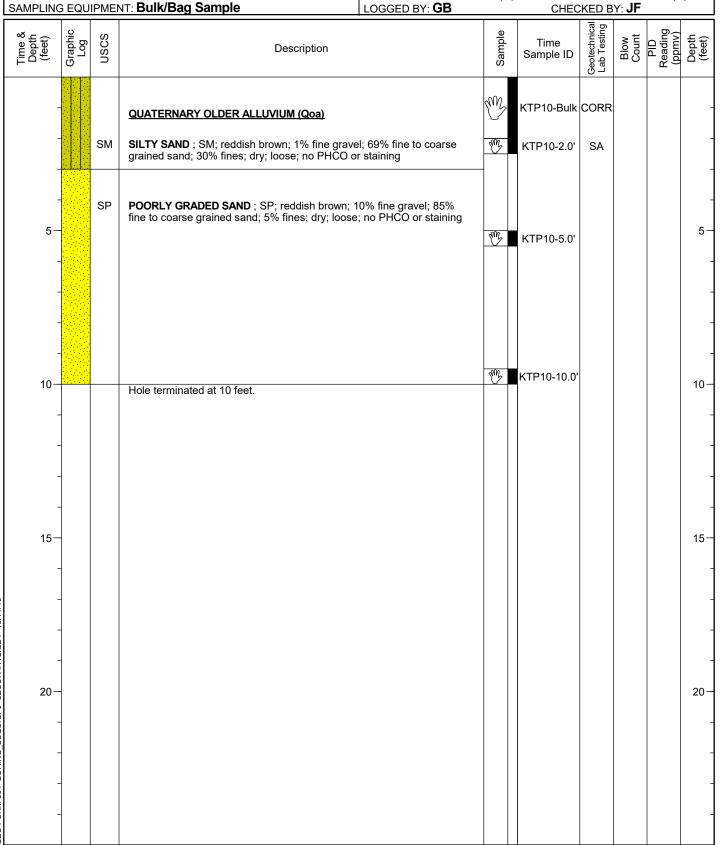
Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING:

COMPLETED: 8/28/19 INSTALLATION: STARTED 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-11** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 10' 8.976" GROUND ELEV (ft): 2323

INITIAL DTW (ft): NE STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---LOGGED BY: GB

EASTING (ft):

LONGITUDE: -117° 58' 26.249

Stantec

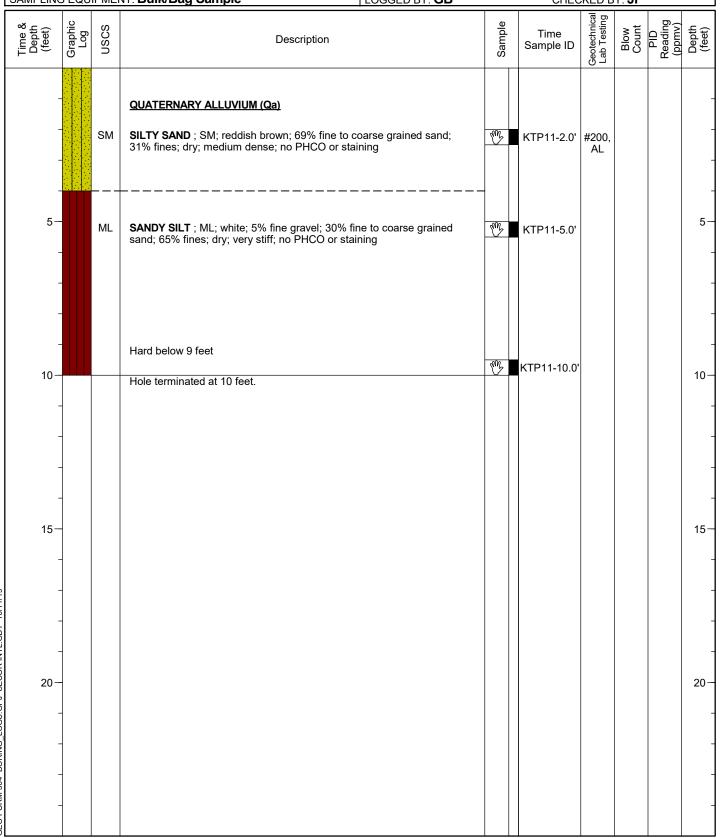
TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING: INSTALLATION: STARTED 8/28/19 COMPLETED: 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-12** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 10' 9.329" GROUND ELEV (ft): 2335

INITIAL DTW (ft): NE STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -117° 59' 6.914"

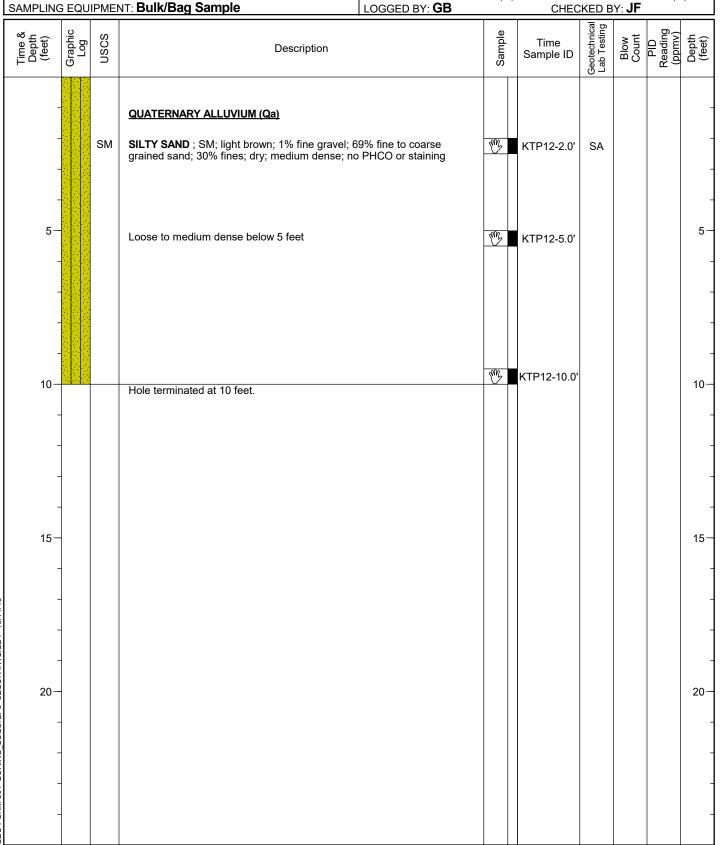
Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/28/19 DRILLING: INSTALLATION: STARTED 8/28/19

COMPLETED: 8/28/19 COMPLETED: 8/28/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-13** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 10' 11.096"

GROUND ELEV (ft): 2372 INITIAL DTW (ft): NE STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -118° 0' 12.744"

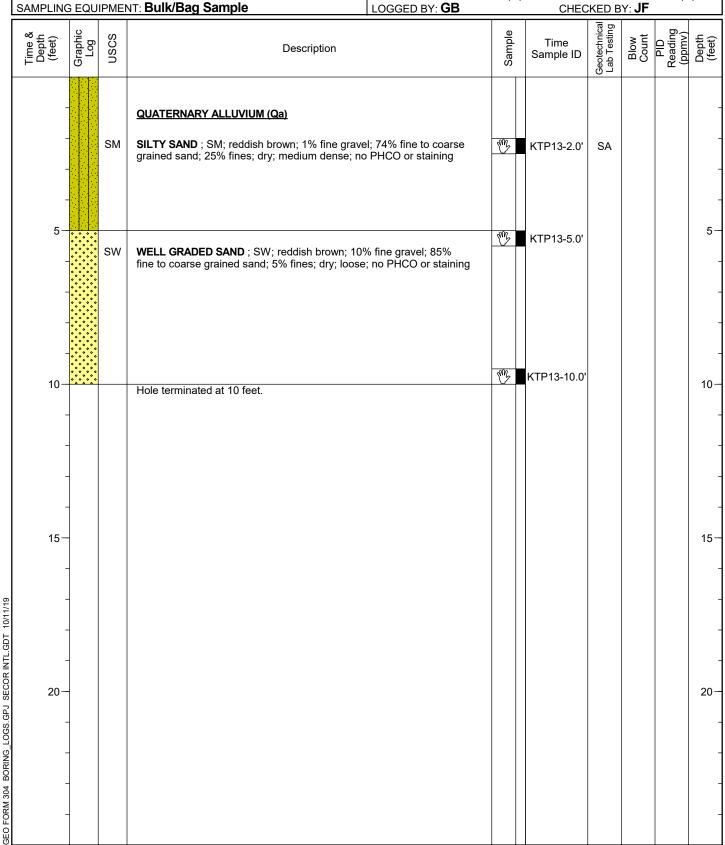
Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/27/19 DRILLING:

COMPLETED: 8/27/19 INSTALLATION: STARTED 8/27/19 COMPLETED: 8/27/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-14** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 10' 20.244" GROUND ELEV (ft): 2390

INITIAL DTW (ft): NE STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

LOGGED BY: GB

EASTING (ft):

LONGITUDE: -118° 0' 43.646"

Stantec

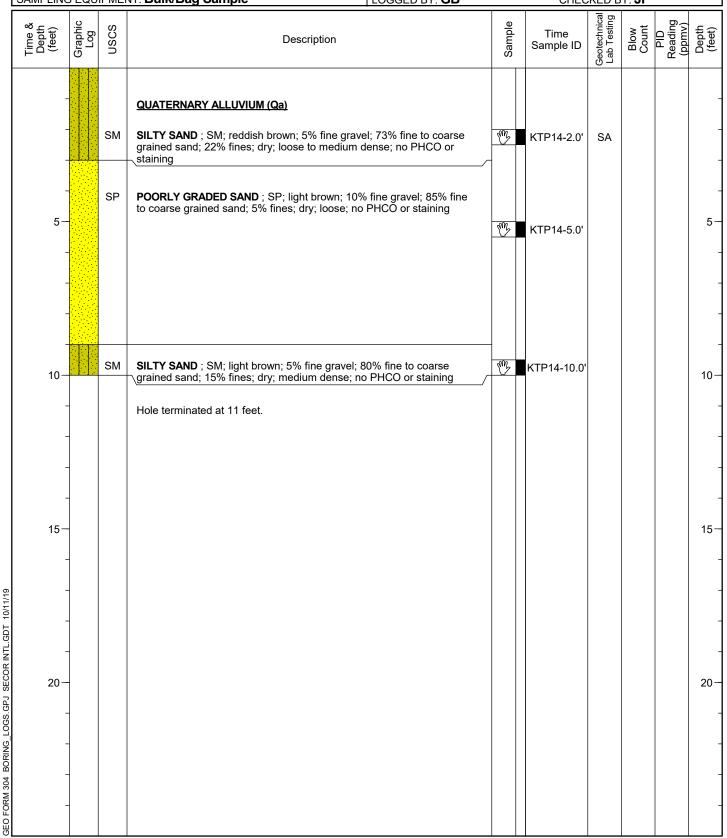
TOC ELEV (ft):

BOREHOLE DEPTH (ft): 11.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/27/19 DRILLING: INSTALLATION: STARTED 8/27/19 COMPLETED: 8/27/19 COMPLETED: 8/27/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

#### **KTP-15** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 10' 34.266"

GROUND ELEV (ft): 2402

INITIAL DTW (ft): NE STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -118° 1' 16.036"

Stantec

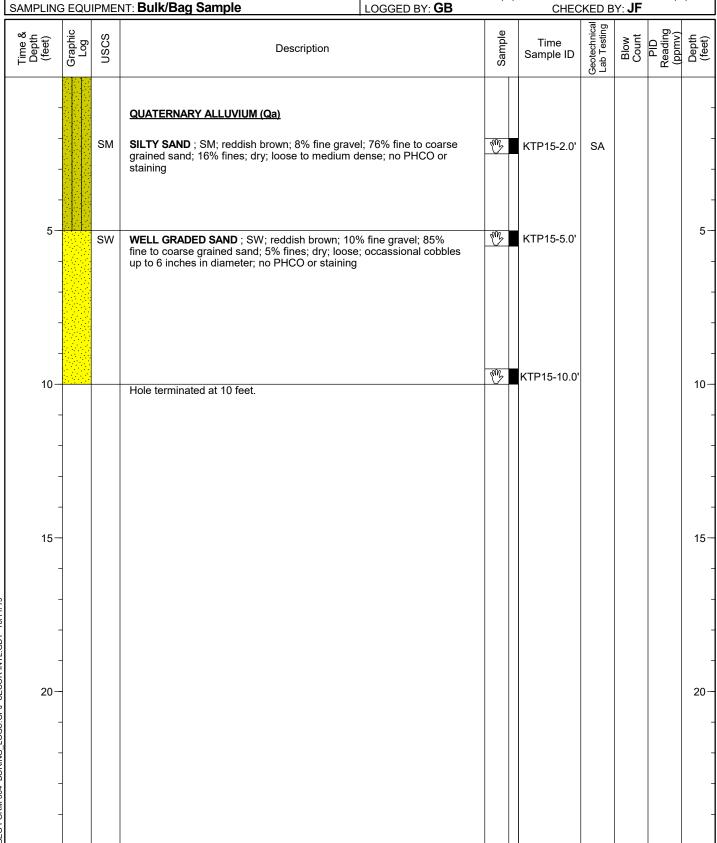
TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/27/19 DRILLING: INSTALLATION: STARTED 8/27/19 COMPLETED: 8/27/19 COMPLETED: 8/27/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING FOLIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-17** PAGE 1 OF 1

NORTHING (ft): LATITUDE: **35° 10' 46.344"** 

GROUND ELEV (ft): 2376 INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -118° 0' 42.793"

Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

| SAMPLING                  | SAMPLING EQUIPMENT: Bulk/Bag Sample LOGGED BY: GB CHECKED BY: JF |           |  |   |        |                   |                             |               |                          |                    |
|---------------------------|--|-----------|--|---|--------|-------------------|-----------------------------|---------------|--------------------------|--------------------|
| Time &<br>Depth<br>(feet) | Graphic<br>Log   | nscs      | Description  |   | Sample | Time<br>Sample ID | Geotechnical<br>Lab Testing | Blow<br>Count | PID<br>Reading<br>(ppmv) | Depth<br>(feet)    |
| -                         |  | GP-<br>GM | QUATERNARY ALLUVIUM (Qa)  POORLY GRADED GRAVEL WITH SILT AND SA 54% fine gravel; 39% fine to coarse grained san- medium dense; some cobbles up to 5 inches in o staining | d; 7% fines; dry;                         | m      | KTP17-2.0'        | SA                          |               |                          | -                  |
| 5<br>-<br>-               |  | SW        | WELL GRADED SAND WITH GRAVEL; SW; rec fine gravel; 85% fine to coarse grained sand; 5% PHCO or staining  Dense with carbonatic cement below 7 feet                       | ldish brown; 10%<br>fines; dry; loose; no | an     | KTP17-5.0'        |                             |               |                          | 5 —<br>-<br>-<br>- |
| -<br>10-<br>-<br>-        |  |           | Cobbles up to 4 inches in diameter below 9 feet  Hole terminated at 10 feet.   |   | m      | KTP17-10.0'       |                             |               |                          | 10-                |
| -<br>15-<br>-             |  |           |  |   |        |                   |                             |               |                          | 15-                |
| 20-                       |  |           |  |   |        |                   |                             |               |                          | 20-                |
| )<br>                     |  |           |  |   |        |                   |                             |               |                          |                    |

LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

DRILLING: STARTED 8/27/19

COMPLETED: 8/27/19 INSTALLATION: STARTED 8/27/19 COMPLETED: 8/27/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching

WELL / TEST PIT / BOREHOLE NO:

## **KTP-18** PAGE 1 OF 1

NORTHING (ft): LATITUDE: **35° 11' 9.992"** 

GROUND ELEV (ft): 2459

INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -118° 3' 24.448"

Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

| SAMPLIN  | SAMPLING EQUIPMENT: Bulk/Bag Sample LOGGED BY: GB CHECKED BY: JF |           |   |   |        |                   |                             |               |                          |                 |
|--|--|-----------|---|---|--------|-------------------|-----------------------------|---------------|--------------------------|-----------------|
| Time &<br>Depth<br>(feet)  | Graphic<br>Log   | nscs      | Description   |   | Sample | Time<br>Sample ID | Geotechnical<br>Lab Testing | Blow<br>Count | PID<br>Reading<br>(ppmv) | Depth<br>(feet) |
|  |  | SW-<br>SM | QUATERNARY ALLUVIUM (Qa)  WELL GRADED SAND WITH SILT; SW-SM; light by gravel; 81% fine to coarse grained sand; 11% fines no PHCO or staining  | orown; 8% fine<br>s; dry; medium dense; | any.   | KTP18-2.0'        | SA                          |               |                          | -               |
| 5-   |  | SW        | WELL GRADED SAND; SW; reddish brown; 10% fine to coarse grained sand; 5% fines; dry; loose; sinches in diameter; no PHCO or staining  Dense with carbonatic cement below 7 feet       | fine gravel; 85%<br>ome cobbles up to 4 | ans.   | KTP18-5.0'        |                             |               |                          | 5-<br>-<br>-    |
| 10-  |  | GP        | POORLY GRADED GRAVEL; GP; white; black; tar<br>40% fine to coarse grained sand; 5% fines; dry; loc<br>some cobbles up to 7 inches in diameter; no PHCC<br>Hole terminated at 10 feet. | se to medium dense;                     | ans.   | KTP18-10.0'       |                             |               |                          | 10-             |
| 15-  | _  |           |   |   |        |                   |                             |               |                          | -<br>-<br>15-   |
| 81.101<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>109.11<br>10 | _  |           |   |   |        |                   |                             |               |                          | 20-             |
| GEO FORM 304 BORING_LUGS, GPO SECOR IN I., GDI 10/17/19  | _  |           |   |   |        |                   |                             |               |                          | -               |

LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/27/19 DRILLING:

COMPLETED: 8/27/19 INSTALLATION: STARTED 8/27/19 COMPLETED: 8/27/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching SAMPLING EQUIPMENT: Bulk/Bag Sample WELL / TEST PIT / BOREHOLE NO:

## **KTP-19** PAGE 1 OF 1

NORTHING (ft):

LATITUDE: 35° 11' 41.161"

GROUND ELEV (ft): 2398 INITIAL DTW (ft): NE

STATIC DTW (ft): **NE** WELL CASING DIAMETER (in): ---

Stantec

EASTING (ft):

LONGITUDE: -118° 2' 29.8"

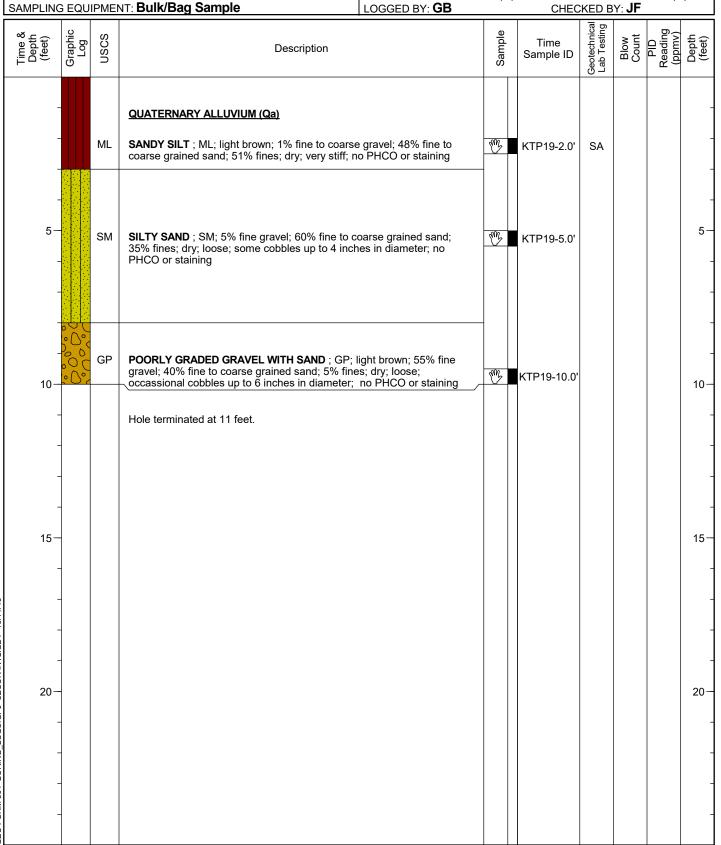
TOC ELEV (ft):

BOREHOLE DEPTH (ft): 11.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

CHECKED BY: JF



LOCATION: Northwest of California City, Kern County, CA

PROJECT NUMBER: 185704635

STARTED 8/27/19 DRILLING:

COMPLETED: 8/27/19 INSTALLATION: STARTED 8/27/19 COMPLETED: 8/27/19

DRILLING COMPANY: 4Granite DRILLING EQUIPMENT: Backhoe

DRILLING METHOD: Backhoe trenching

WELL / TEST PIT / BOREHOLE NO:

## **KTP-20** PAGE 1 OF 1

NORTHING (ft): LATITUDE: **35° 11' 41.161"** 

GROUND ELEV (ft): 2358 INITIAL DTW (ft): **NE** STATIC DTW (ft): **NE** 

WELL CASING DIAMETER (in): ---

EASTING (ft):

LONGITUDE: -118° 2' 29.8"

Stantec

TOC ELEV (ft):

BOREHOLE DEPTH (ft): 10.0

WELL DEPTH (ft): ---

BOREHOLE DIAMETER (in): 36

| SAMPLING EQUIPMENT: Bulk/Bag Sample LOGGED BY: GB |                |      | ()  |  | KED B      |                          | . 1 L I \ (II               | .,            |                          |                 |
|---|----------------|------|---|--|------------|--------------------------|-----------------------------|---------------|--------------------------|-----------------|
| Time &<br>Depth<br>(feet)                         | Graphic<br>Log | nscs | Description   |  | Sample     | Time<br>Sample ID        | Geotechnical<br>Lab Testing | Blow<br>Count | PID<br>Reading<br>(ppmv) | Depth<br>(feet) |
| -   |                | SP   | QUATERNARY ALLUVIUM (Qa)  POORLY GRADED SAND WITH GRAVEL; SP; I gravel; 68% fine to coarse grained sand; 1% fine organics; no PHCO or staining                        | ight brown; 31% fine<br>s; dry; loose; few | ~~~<br>~~~ | KTP20-Bulk<br>KTP20-2.0' | CORR<br>SA                  |               |                          | -               |
| 5   |                | SM   | SILTY SAND; SM; reddish brown; 10% fine grav<br>coarse grained sand; 25% fines; dry; loose; no P<br>Dense with carbonatic cement below 7 feet                         | rel; 65% fine to<br>HCO or staining        | 4MZ        | KTP20-5.0'               |                             |               |                          | 5-              |
| 10-   |                | SP   | POORLY GRADED SAND; SP; light brown; 30% to coarse grained sand; 5% fines; dry; loose to noccassional cobbles up to 6 inches in diameter; Hole terminated at 10 feet. | nedium dense;                              | - CM       | KTP20-10.0'              |                             |               |                          | 10-             |
| -<br>15-  |                |      |   |  |            |                          |                             |               |                          | 15-             |
| 20-   |                |      |   |  |            |                          |                             |               |                          | 20-             |
| -   |                |      |   |  |            |                          |                             |               |                          | -               |

#### **CEQA LEVEL GEOTECHNICAL STUDY**

Appendix B Laboratory Test Results

# **Appendix B LABORATORY TEST RESULTS**









Sample Dry Mass (g)

Moisture Content (%)

 Project Name
 8me Kudu
 Project Number
 185704635

 Source
 Grab
 Lab ID
 KTP1-5'

 Date Received
 09-12-2019

 Preparation Method
 ASTM D 1140 Method A
 Preparation Date
 09-21-2019

 Particle Shape
 Test Date
 09-22-2019

 Particle Hardness
 Test Date
 09-22-2019

Analysis based on total sample.

| Т          | _        | 0.4      | 21      |
|------------|----------|----------|---------|
|            | Grams    | %        | %       |
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| 3/8"       | 3.30     | 0.7      | 99.3    |
| No. 4      | 15.40    | 3.5      | 95.8    |
| No. 8      | 36.70    | 8.3      | 87.5    |
| No. 16     | 59.20    | 13.4     | 74.1    |
| No. 30     | 69.70    | 15.7     | 58.4    |
| No. 50     | 97.20    | 22.0     | 36.4    |
| No. 100    | 62.90    | 14.2     | 22.2    |
| No. 200    | 34.54    | 7.8      | 14.4    |
| Pan        | 63.76    | 14.4     |         |

442.70

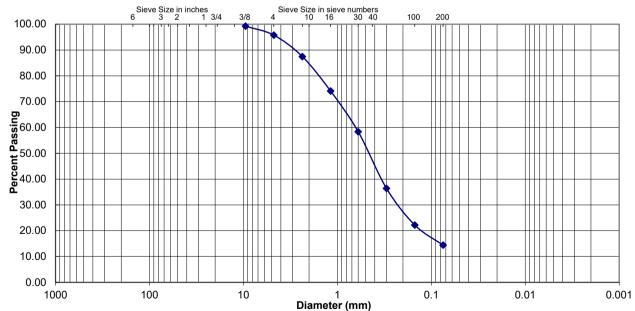
| % Gravel             | 4.2  |
|----------------------|------|
| % Sand               | 81.4 |
| % Fines              | 14.4 |
| Fines Classification | ML   |
| •                    |      |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
| •                    |      |
| Cu                   | N/A  |
| Сс                   | N/A  |
|                      |      |

#### Classification

Silty Sand (SM)

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments





Sample Dry Mass (g) \_\_\_\_ Moisture Content (%) \_\_\_

| Project Name 8me Kudu                   | Project Number_  | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP2-2'    |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-21-2019 |
| Particle Shape                          | Test Date        | 09-22-2019 |
| Particle Hardness                       | _                |            |

Analysis based on total sample.

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| No. 4      | 3.30     | 8.0      | 99.2    |
| No. 8      | 16.20    | 4.1      | 95.1    |
| No. 16     | 26.80    | 6.8      | 88.3    |
| No. 30     | 40.00    | 10.1     | 78.1    |
| No. 50     | 80.10    | 20.3     | 57.8    |
| No. 100    | 77.30    | 19.6     | 38.2    |
| No. 200    | 42.30    | 10.7     | 27.5    |
| Pan        | 108.40   | 27.5     |         |

394.40

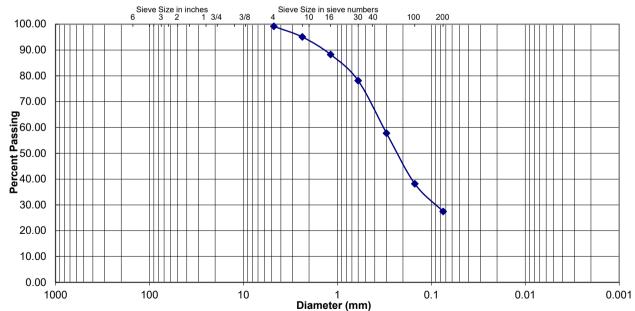
| % Gravel             | 0.8  |
|----------------------|------|
| % Sand               | 71.7 |
| % Fines              | 27.5 |
| Fines Classification | ML   |
|                      |      |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
| •                    |      |
| Cu                   | N/A  |
| Сс                   | N/A  |
|                      |      |

Classification

Silty Sand (SM)

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments





| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP3-2'    |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-21-2019 |
| Particle Shape                          | Test Date        | 09-22-2019 |
| Particle Hardness                       | _                |            |

Sample Dry Mass (g) 442.80 Moisture Content (%) 3.2

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| 3/4"       | 28.90    | 6.5      | 93.5    |
| 1/2"       | 0.00     | 0.0      | 93.5    |
| 3/8"       | 5.60     | 1.3      | 92.2    |
| No. 4      | 8.80     | 2.0      | 90.2    |
| No. 8      | 22.30    | 5.0      | 85.2    |
| No. 16     | 41.00    | 9.3      | 75.9    |
| No. 30     | 59.60    | 13.5     | 62.5    |
| No. 50     | 80.40    | 18.2     | 44.3    |
| No. 100    | 73.70    | 16.6     | 27.7    |
| No. 200    | 47.70    | 10.8     | 16.9    |
| Pan        | 74.80    | 16.9     |         |

| % Gravel             | 9.8  |
|----------------------|------|
| % Sand               | 73.3 |
| % Fines              | 16.9 |
| Fines Classification | ML   |
|                      | _    |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
| •                    |      |
| Cu                   | N/A  |
| Сс                   | N/A  |

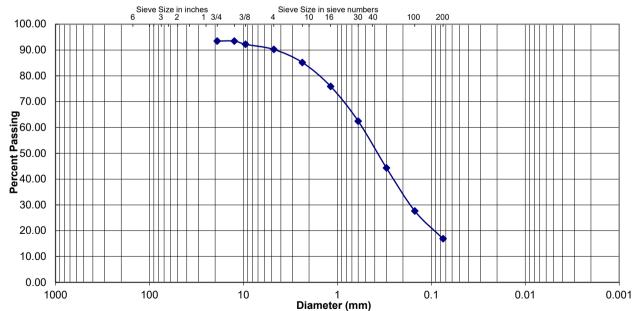
Analysis based on total sample.

-

Classification
Silty Sand (SM)

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments





Sample Dry Mass (g) \_\_\_\_ Moisture Content (%) \_\_\_

| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP4-2'    |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-21-2019 |
| Particle Shape                          | Test Date        | 09-22-2019 |
| Particle Hardness                       | _                |            |

402.70 Analysis based on total sample.

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| No. 4      | 2.00     | 0.5      | 99.5    |
| No. 8      | 7.60     | 1.9      | 97.6    |
| No. 16     | 16.20    | 4.0      | 93.6    |
| No. 30     | 28.50    | 7.1      | 86.5    |
| No. 50     | 57.70    | 14.3     | 72.2    |
| No. 100    | 78.80    | 19.6     | 52.6    |
| No. 200    | 57.70    | 14.3     | 38.3    |
| Pan        | 154.20   | 38.3     |         |

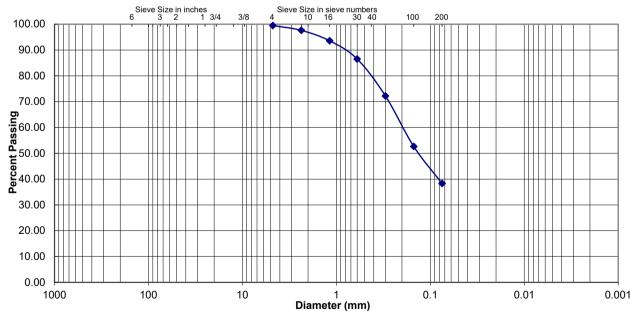
| % Gravel             | 0.5  |
|----------------------|------|
| % Sand               | 61.2 |
| % Fines              | 38.3 |
| Fines Classification | ML   |
|                      |      |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
| •                    |      |
| Cu                   | N/A  |
| Сс                   | N/A  |
| •                    |      |
| Classification       | nn . |

#### Classification



Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments Reviewed By







| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP5-2'    |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-21-2019 |
| Particle Shape                          | Test Date        | 09-22-2019 |
| Dartiela Hardness                       | _                |            |

F

Particle Hardness
Sample Dry Mass (g) 359.00
Moisture Content (%) 3.4

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| 3/8"       | 9.50     | 2.6      | 97.4    |
| No. 4      | 19.50    | 5.4      | 91.9    |
| No. 8      | 30.30    | 8.4      | 83.5    |
| No. 16     | 47.60    | 13.3     | 70.2    |
| No. 30     | 59.10    | 16.5     | 53.8    |
| No. 50     | 71.30    | 19.9     | 33.9    |
| No. 100    | 55.40    | 15.4     | 18.5    |
| No. 200    | 25.70    | 7.2      | 11.3    |
| Pan        | 40.60    | 11.3     |         |

| % Gravel             | 8.1    |
|----------------------|--------|
| % Sand               | 80.6   |
| % Fines              | 11.3   |
| ines Classification  | ML     |
| •                    |        |
| D <sub>10</sub> (mm) | 0.0661 |
| D <sub>30</sub> (mm) | 0.2518 |
| D <sub>60</sub> (mm) | 0.7353 |
|                      | _      |
| Cu                   | 11.13  |
| Сс                   | 1.31   |
| •                    |        |

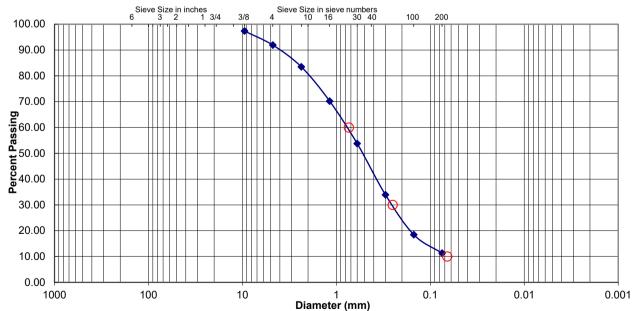
Analysis based on total sample.

#### Classification

Well Graded Sand (SW-SM) with Silt

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments





| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP6-2'    |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-21-2019 |
| Particle Shape                          | Test Date        | 09-22-2019 |
| Particle Hardness                       | _                |            |

Sample Dry Mass (g) 357.40
Moisture Content (%) 2.8

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| No. 4      | 9.80     | 2.7      | 97.3    |
| No. 8      | 21.90    | 6.1      | 91.1    |
| No. 16     | 46.30    | 13.0     | 78.2    |
| No. 30     | 54.50    | 15.2     | 62.9    |
| No. 50     | 66.80    | 18.7     | 44.2    |
| No. 100    | 55.20    | 15.4     | 28.8    |
| No. 200    | 35.40    | 9.9      | 18.9    |
| Pan        | 67.50    | 18.9     |         |

| % Gravel                                     | 2.7        |
|--|------------|
| % Sand                                       | 78.4       |
| % Fines                                      | 18.9       |
| Fines Classification                         | ML         |
| •  |            |
| D <sub>10</sub> (mm)                         | N/A        |
|  |            |
| D <sub>30</sub> (mm)                         | N/A        |
| D <sub>30</sub> (mm)<br>D <sub>60</sub> (mm) | N/A<br>N/A |
| · · · · · ·                                  |            |

Cu N/A Cc N/A

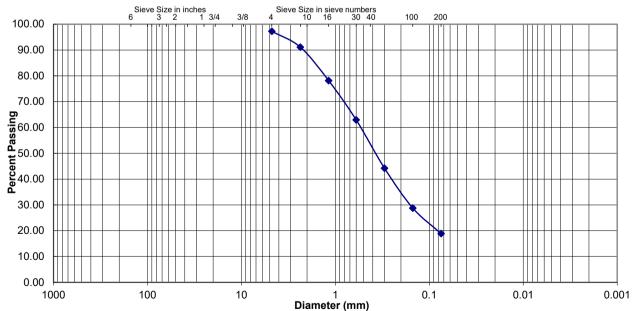
Analysis based on total sample.

#### Classification

Silty Sand (SM)

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments

# **Gradation Analysis**

ASTM D 422



| Project Name 8me Kudu                   | Project Number_  | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP7-2'    |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-21-2019 |
| Particle Shape                          | Test Date        | 09-22-2019 |
| Particle Hardness                       | _                |            |

Sample Dry Mass (g) 324.60
Moisture Content (%) 3.5

|            |          | 1 4      | •       |
|------------|----------|----------|---------|
|            | Grams    | %        | %       |
| Sieve Size | Retained | Retained | Passing |
| ·          | · ·      |          |         |
| ·          | · ·      |          |         |
| ·          | · ·      |          |         |
|            |          |          |         |
| ·          | ,        |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| No. 4      | 4.70     | 1.4      | 98.6    |
| No. 8      | 9.00     | 2.8      | 95.8    |
| No. 16     | 15.20    | 4.7      | 91.1    |
| No. 30     | 21.40    | 6.6      | 84.5    |
| No. 50     | 32.80    | 10.1     | 74.4    |
| No. 100    | 54.80    | 16.9     | 57.5    |
| No. 200    | 57.70    | 17.8     | 39.7    |
| Pan        | 129.00   | 39.7     |         |

| % Gravel             | 1.4  |
|----------------------|------|
| % Sand               | 58.8 |
| % Fines              | 39.7 |
| Fines Classification | ML   |
| •                    |      |

| D <sub>10</sub> (mm) | N/A |
|----------------------|-----|
| D <sub>30</sub> (mm) | N/A |
| D <sub>60</sub> (mm) | N/A |

Cu N/A

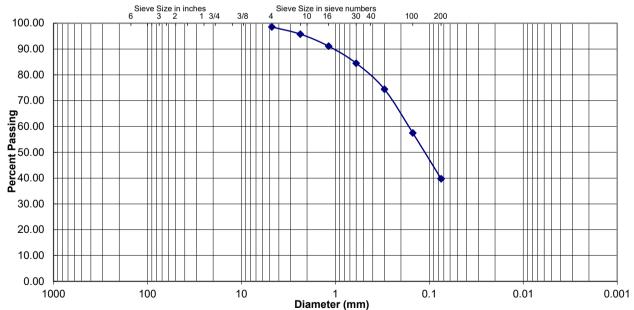
Analysis based on total sample.

#### Classification

| 0::: 0 :   | (014)  |
|------------|--------|
| Silty Sand | (SM)   |
| only ouria | (0.11) |
|            |        |

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments







| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP8-2'    |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-21-2019 |
| Particle Shape                          | Test Date        | 09-22-2019 |
| Particle Hardness                       | _                |            |

Sample Dry Mass (g) 431.80
Moisture Content (%) 1.4

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
| ·          | ·        |          | ,       |
|            | _        |          |         |
| ·          |          |          | ·       |
|            |          |          |         |
|            |          |          |         |
| ·          | ·        |          | ,       |
| 3/8"       | 11.50    | 2.7      | 97.3    |
| No. 4      | 17.00    | 3.9      | 93.4    |
| No. 8      | 28.50    | 6.6      | 86.8    |
| No. 16     | 58.80    | 13.6     | 73.2    |
| No. 30     | 70.90    | 16.4     | 56.8    |
| No. 50     | 88.20    | 20.4     | 36.3    |
| No. 100    | 76.80    | 17.8     | 18.6    |
| No. 200    | 40.70    | 9.4      | 9.1     |
| Pan        | 39.40    | 9.1      |         |

| % Gravel             | 6.6    |
|----------------------|--------|
| % Sand               | 84.3   |
| % Fines              | 9.1    |
| Fines Classification | ML     |
| •                    |        |
| D <sub>10</sub> (mm) | 0.0800 |
| D <sub>30</sub> (mm) | 0.2344 |
| D <sub>60</sub> (mm) | 0.6556 |
| •                    |        |
| Cu                   | 8.20   |
| Сс                   | 1.05   |
| •                    |        |

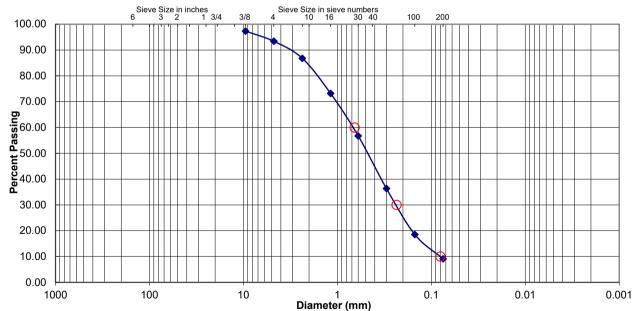
#### Classification

Well Graded Sand (SW-SM) with Silt

Analysis based on total sample.

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments





| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP9-2'    |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-22-2019 |
| Particle Shape                          | Test Date        | 09-23-2019 |
| Particle Hardness                       | _                |            |

Sample Dry Mass (g) 498.60
Moisture Content (%) 1.5

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| 1"         | 70.50    | 14.1     | 85.9    |
| 3/4"       | 42.00    | 8.4      | 77.4    |
| 1/2"       | 33.50    | 6.7      | 70.7    |
| 3/8"       | 15.60    | 3.1      | 67.6    |
| No. 4      | 15.50    | 3.1      | 64.5    |
| No. 8      | 26.60    | 5.3      | 59.1    |
| No. 16     | 38.40    | 7.7      | 51.4    |
| No. 30     | 40.10    | 8.0      | 43.4    |
| No. 50     | 49.90    | 10.0     | 33.4    |
| No. 100    | 59.90    | 12.0     | 21.4    |
| No. 200    | 43.00    | 8.6      | 12.8    |
| Pan        | 63.60    | 12.8     |         |

| % Gravel             | 35.5 |
|----------------------|------|
| % Sand               | 51.7 |
| % Fines              | 12.8 |
| Fines Classification | ML   |
| •                    |      |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
|                      |      |
| Cu                   | N/A  |
| Cc                   | N/A  |

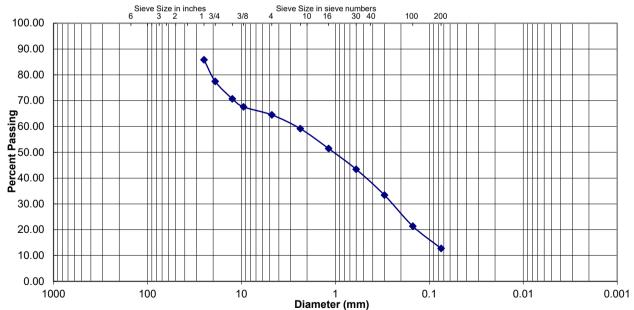
Analysis based on total sample.

#### Classification

Silty Sand (SM) with Gravel

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments





Sample Dry Mass (g) \_\_\_\_ Moisture Content (%) \_\_\_

| Project Name 8me Kudu                   | Project Number_  | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP10-2'   |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-22-2019 |
| Particle Shape                          | Test Date        | 09-23-2019 |
| Particle Hardness                       | _                |            |

Analysis based on total sample.

| Sieve Size | Grams<br>Retained | %<br>Retained | %<br>Passing |
|------------|-------------------|---------------|--------------|
| 0.070 0.20 |                   | . 10100       |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
| No. 4      | 2.30              | 0.5           | 99.5         |
| No. 8      | 13.00             | 2.9           | 96.6         |
| No. 16     | 33.60             | 7.5           | 89.1         |
| No. 30     | 52.20             | 11.6          | 77.4         |
| No. 50     | 98.40             | 22.0          | 55.5         |
| No. 100    | 75.20             | 16.8          | 38.7         |
| No. 200    | 35.90             | 8.0           | 30.7         |
| Pan        | 137.50            | 30.7          |              |

448.10

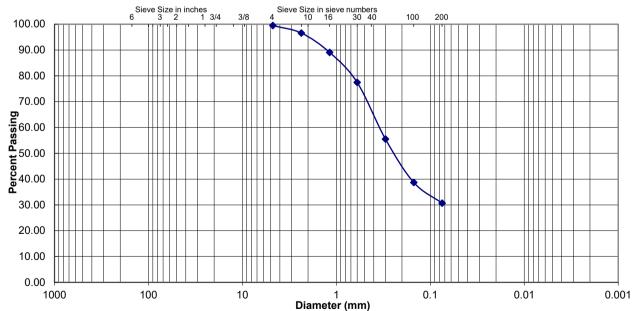
| % Gravel             | 0.5  |
|----------------------|------|
| % Sand               | 68.8 |
| % Fines              | 30.7 |
| Fines Classification | ML   |
|                      |      |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
|                      |      |
| Cu                   | N/A  |
| Cc                   | N/A  |
|                      |      |

#### Classification



Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments Reviewed By



# Materials Finer Than 75µm (No. 200) Sieve

ASTM D 1140

| Project Name 8me Kudu  | Project Number _ | 185704635  |
|--|------------------|------------|
| Source Grab  | Lab ID           | KTP11-2'   |
|  | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A  | Test Date        | 09-22-2019 |
| Initial Sample Wet Mass (g) 283.00 Moisture Content Initial Oven Dry Sample Mass (g) 189.20  Materials Finer Than 75µm (No. 200) Sieve (g) 83.20  Percent Finer Than 75µm (No. 200) Sieve (%) 30.5 | nt (%) 3.9       |            |
| Comments   |                  |            |
|  | Reviewed By_     |            |
|  |                  |            |

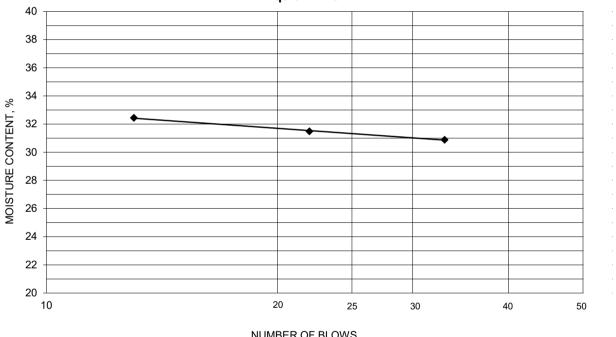




Project 8me Kudu Project No. 185704635 Source Grab Lab ID KTP11-2' Test Method ASTM D 4318 Tested By M.P. % + No. 40 30 Need! Input **Test Date** Prepared Date Received 09-12-2019 Dry

| Wet Soil and<br>Tare Mass<br>(g) | Dry Soil and<br>Tare Mass<br>(g) | Tare Mass<br>(g) | Number of<br>Blows | Water Content<br>(%) | Liquid Limit |
|----------------------------------|----------------------------------|------------------|--------------------|----------------------|--------------|
| 19.51                            | 18.12                            | 13.62            | 33                 | 30.9                 |              |
| 20.56                            | 18.91                            | 13.67            | 22                 | 31.5                 |              |
| 21.67                            | 19.74                            | 13.79            | 13                 | 32.4                 | 31           |
|                                  |                                  |                  |                    |                      |              |
|                                  |                                  |                  |                    |                      |              |

#### **Liquid Limit**



#### NUMBER OF BLOWS

#### PLASTIC LIMIT AND PLASTICITY INDEX

| Wet Soil and | Dry Soil and |           | Water   |               |                  |
|--------------|--------------|-----------|---------|---------------|------------------|
| Tare Mass    | Tare Mass    | Tare Mass | Content |               |                  |
| (g)          | (g)          | (g)       | (%)     | Plastic Limit | Plasticity Index |
| 23.72        | 21.96        | 13.54     | 20.9    | 21            | 10               |
|              |              |           |         |               |                  |

| Remarks: |             |
|----------|-------------|
| •        | Reviewed By |





Sample Dry Mass (g) \_\_\_\_ Moisture Content (%) \_\_\_

| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP12-2'   |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-22-2019 |
| Particle Shape                          | Test Date        | 09-23-2019 |
| Particle Hardness                       | _                |            |

Analysis based on total sample.

| Sieve Size | Grams<br>Retained | %<br>Retained | %<br>Passing |
|------------|-------------------|---------------|--------------|
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
| No. 4      | 3.70              | 1.0           | 99.0         |
| No. 8      | 16.00             | 4.4           | 94.6         |
| No. 16     | 30.70             | 8.5           | 86.1         |
| No. 30     | 43.20             | 11.9          | 74.2         |
| No. 50     | 55.30             | 15.3          | 58.9         |
| No. 100    | 56.90             | 15.7          | 43.2         |
| No. 200    | 48.10             | 13.3          | 29.9         |
| Pan        | 108.20            | 29.9          |              |

362.10

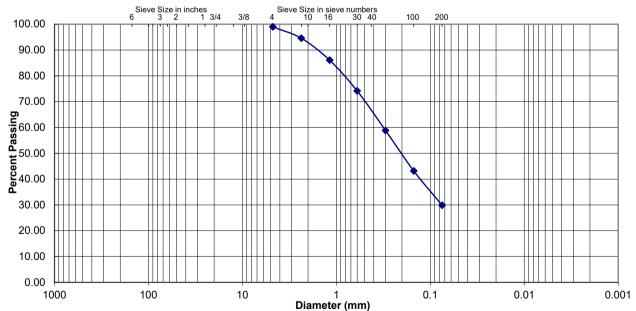
| % Gravel             | 1.0  |
|----------------------|------|
| % Sand               | 69.1 |
| % Fines              | 29.9 |
| Fines Classification | ML   |
| •                    |      |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
| •                    |      |
| Cu                   | N/A  |
| Сс                   | N/A  |
|                      |      |

#### Classification



Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments





Sample Dry Mass (g) \_\_\_\_ Moisture Content (%) \_\_\_

| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP13-2'   |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-22-2019 |
| Particle Shape                          | Test Date        | 09-23-2019 |
| Particle Hardness                       | _                |            |

Analysis based on total sample.

| Sieve Size     | Grams<br>Retained | %<br>Retained | %<br>Passing |
|----------------|-------------------|---------------|--------------|
|                |                   |               |              |
|                |                   |               |              |
|                |                   |               |              |
|                |                   |               |              |
|                |                   |               |              |
|                |                   |               |              |
|                |                   |               |              |
| No. 4          | 4.70              | 1.4           | 00.6         |
| No. 4<br>No. 8 | 4.70<br>15.10     | 1.4<br>4.6    | 98.6<br>94.0 |
| No. 16         | 33.20             | 10.1          | 83.9         |
| No. 30         | 42.00             | 12.7          | 71.2         |
| No. 50         | 52.00             | 15.8          | 55.5         |
| No. 100        | 57.30             | 17.4          | 38.1         |
| No. 200        | 43.20             | 13.1          | 25.0         |
| Pan            | 82.60             | 25.0          |              |

330.10

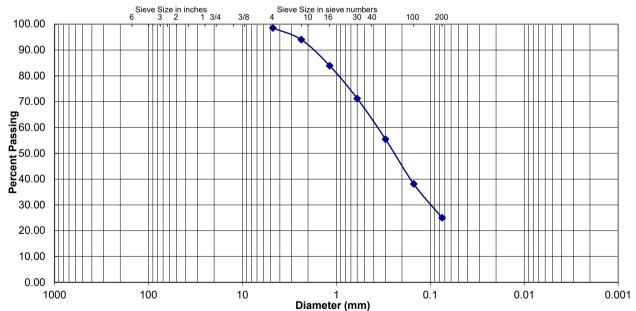
| % Gravel             | 1.4  |
|----------------------|------|
| % Sand               | 73.6 |
| % Fines              | 25.0 |
| Fines Classification | ML   |
|                      |      |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
|                      |      |
| Cu <u>N/A</u>        |      |
| Cc N/A               |      |
|                      |      |

#### Classification

| Silty Sand (SM) |  |
|-----------------|--|
|                 |  |

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments







| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP14-2'   |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-22-2019 |
| Particle Shape                          | Test Date        | 09-23-2019 |
| Particle Hardness                       | _                |            |

Sample Dry Mass (g) 379.30 Moisture Content (%) 2.5

|            |          | 0.4      | 0.1     |
|------------|----------|----------|---------|
|            | Grams    | %        | %       |
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| No. 4      | 20.10    | 5.3      | 94.7    |
| No. 8      | 22.90    | 6.0      | 88.7    |
| No. 16     | 32.00    | 8.4      | 80.2    |
| No. 30     | 35.80    | 9.4      | 70.8    |
| No. 50     | 49.50    | 13.1     | 57.7    |
| No. 100    | 74.60    | 19.7     | 38.1    |
| No. 200    | 61.30    | 16.2     | 21.9    |
| Pan        | 83.10    | 21.9     |         |

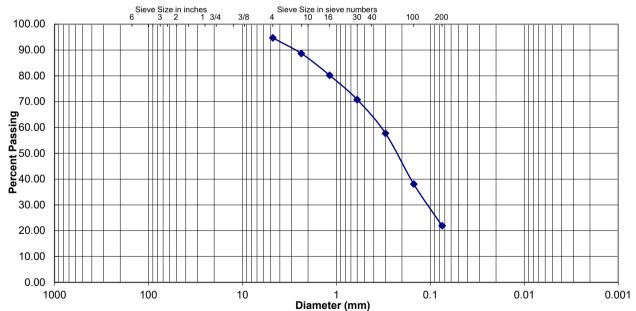
| % Gravel             | 5.3  |
|----------------------|------|
| % Sand               | 72.8 |
| % Fines              | 21.9 |
| Fines Classification | ML   |
|                      |      |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
|                      |      |
| Cu                   | N/A  |
| Сс                   | N/A  |

Analysis based on total sample.

Classification
Silty Sand (SM)

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments







| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP15-2'   |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-22-2019 |
| Particle Shape                          | Test Date        | 09-23-2019 |
| Particle Hardness                       | _                |            |

Sample Dry Mass (g) 332.60
Moisture Content (%) 3.1

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| No. 4      | 25.30    | 7.6      | 92.4    |
| No. 8      | 34.50    | 10.4     | 82.0    |
| No. 16     | 47.20    | 14.2     | 67.8    |
| No. 30     | 49.20    | 14.8     | 53.0    |
| No. 50     | 52.40    | 15.8     | 37.3    |
| No. 100    | 43.30    | 13.0     | 24.3    |
| No. 200    | 27.50    | 8.3      | 16.0    |
| Pan        | 53.20    | 16.0     |         |

| % Gravel             | 7.6  |
|----------------------|------|
| % Sand               | 76.4 |
| % Fines              | 16.0 |
| Fines Classification | ML   |
|                      |      |
| D <sub>10</sub> (mm) | N/A  |

 $\begin{array}{c|cccc} D_{10} \ (mm) & N/A \\ D_{30} \ (mm) & N/A \\ D_{60} \ (mm) & N/A \\ \end{array}$ 

Cu N/A

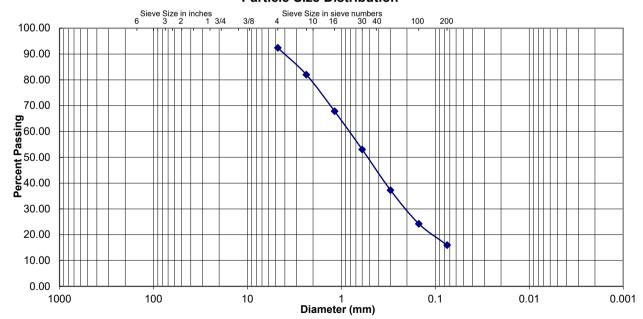
Analysis based on total sample.

#### Classification

Silty Sand (SM)

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments





| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP17-2'   |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-22-2019 |
| Particle Shape                          | Test Date        | 09-23-2019 |
| Particle Hardness                       | _                |            |

Sample Dry Mass (g) 671.50

Moisture Content (%) 1.4

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| l          |          |          |         |
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| 1 1/2"     | 122.30   | 18.2     | 81.8    |
| 1"         | 56.60    | 8.4      | 73.4    |
| 3/4"       | 39.40    | 5.9      | 67.5    |
| 1/2"       | 33.10    | 4.9      | 62.6    |
| 3/8"       | 34.10    | 5.1      | 57.5    |
| No. 4      | 74.70    | 11.1     | 46.4    |
| No. 8      | 44.40    | 6.6      | 39.7    |
| No. 16     | 54.00    | 8.0      | 31.7    |
| No. 30     | 53.10    | 7.9      | 23.8    |
| No. 50     | 50.80    | 7.6      | 16.2    |
| No. 100    | 37.50    | 5.6      | 10.6    |
| No. 200    | 21.70    | 3.2      | 7.4     |
| Pan        | 49.80    | 7.4      |         |

| % Gravel             | 53.6   |
|----------------------|--------|
| % Sand               | 38.9   |
| % Fines              | 7.4    |
| Fines Classification | ML     |
| •                    |        |
| D <sub>10</sub> (mm) | 0.1305 |
| D <sub>30</sub> (mm) | 1.0199 |
| D <sub>60</sub> (mm) | 9.5841 |
| •                    |        |
| Cu                   | 73.42  |
| Cc                   | 0.83   |
| •                    |        |

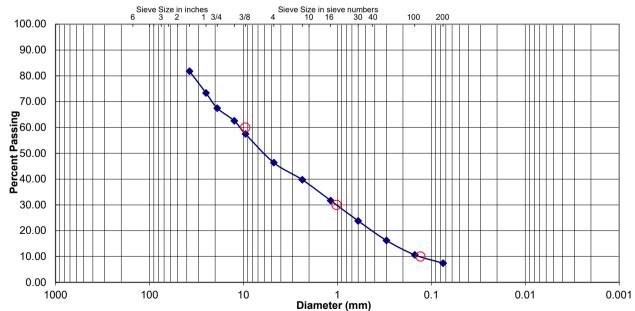
#### Classification

Poorly Graded Gravel (GP-GM) with Silt and Sand

Analysis based on total sample.

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments







| Project Name 8me Kudu                   | Project Number   | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP18-2'   |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-22-2019 |
| Particle Shape                          | Test Date        | 09-23-2019 |
| Particle Hardness                       | _                |            |

F

Sample Dry Mass (g) 442.90 Moisture Content (%) 1.7

|            | Grams    | %        | %       |
|------------|----------|----------|---------|
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| 3/8"       | 16.10    | 3.6      | 96.4    |
| No. 4      | 20.00    | 4.5      | 91.8    |
| No. 8      | 27.70    | 6.3      | 85.6    |
| No. 16     | 51.40    | 11.6     | 74.0    |
| No. 30     | 57.80    | 13.1     | 60.9    |
| No. 50     | 83.80    | 18.9     | 42.0    |
| No. 100    | 83.60    | 18.9     | 23.1    |
| No. 200    | 53.90    | 12.2     | 11.0    |
| Pan        | 48.60    | 11.0     |         |

| % Gravel             | 8.2    |
|----------------------|--------|
| % Sand               | 80.9   |
| % Fines              | 11.0   |
| ines Classification  | ML     |
| •                    |        |
| D <sub>10</sub> (mm) | 0.0710 |
| D <sub>30</sub> (mm) | 0.1930 |
| D <sub>60</sub> (mm) | 0.5497 |
|                      | _      |
| Cu                   | 7.75   |
| Cc                   | 0.95   |
| •                    |        |

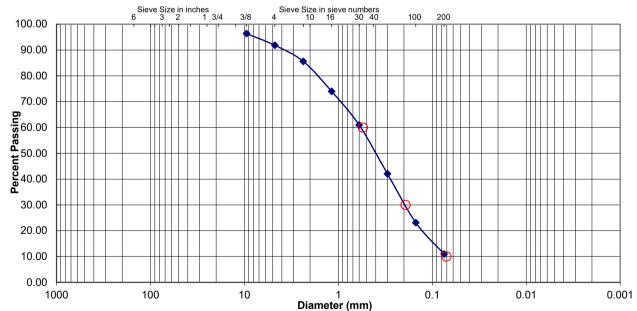
Analysis based on total sample.

#### Classification

Well Graded Sand (SW-SM) with Silt

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments





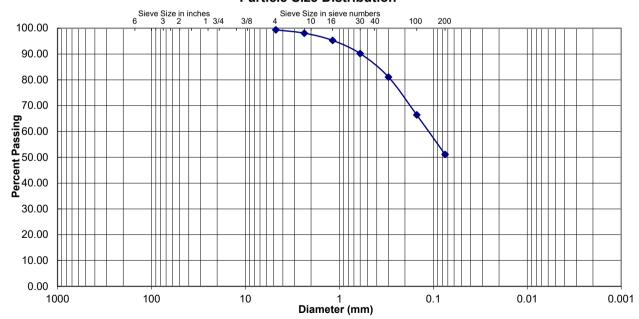
| Project Name 8me Kudu                   | Project Number          | 185704635  |
|---|-------------------------|------------|
| Source Grab                             | Lab ID                  | KTP19-2'   |
|   | Date Received           | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date        | 09-22-2019 |
| Particle Shape                          | Test Date               | 09-23-2019 |
| Particle Hardness                       | _                       |            |
| Sample Dry Mass (g) 313.40              | Analysis based on total | sample.    |

| Sample Dry Mass (g)  | 313.40 |
|----------------------|--------|
| Moisture Content (%) | 2.9    |
| •                    |        |

|            | _        |          |         |
|------------|----------|----------|---------|
|            | Grams    | %        | %       |
| Sieve Size | Retained | Retained | Passing |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
|            |          |          |         |
| No. 4      | 2.00     | 0.6      | 99.4    |
| No. 8      | 4.00     | 1.3      | 98.1    |
| No. 16     | 8.80     | 2.8      | 95.3    |
| No. 30     | 16.00    | 5.1      | 90.2    |
| No. 50     | 28.50    | 9.1      | 81.1    |
| No. 100    | 46.00    | 14.7     | 66.4    |
| No. 200    | 47.90    | 15.3     | 51.1    |
| Pan        | 160.20   | 51.1     |         |

| % Gravel             | 0.6  |
|----------------------|------|
| % Sand               | 48.2 |
| % Fines              | 51.1 |
| Fines Classification | ML   |
|                      |      |
| D <sub>10</sub> (mm) | N/A  |
| D <sub>30</sub> (mm) | N/A  |
| D <sub>60</sub> (mm) | N/A  |
|                      |      |
| Cu                   | N/A  |
| Сс                   | N/A  |
|                      |      |

#### **Particle Size Distribution**



Comments





Sample Dry Mass (g) \_\_\_\_ Moisture Content (%) \_\_\_

| Project Name 8me Kudu                   | Project Number_  | 185704635  |
|---|------------------|------------|
| Source Grab                             | Lab ID           | KTP20-5'   |
|   | Date Received    | 09-12-2019 |
| Preparation Method ASTM D 1140 Method A | Preparation Date | 09-22-2019 |
| Particle Shape                          | Test Date        | 09-23-2019 |
| Particle Hardness                       | _                |            |

Analysis based on total sample.

| Sieve Size | Grams<br>Retained | %<br>Retained | %<br>Passing |
|------------|-------------------|---------------|--------------|
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
|            |                   |               |              |
| 1"         | 18.40             | 4.1           | 95.9         |
| 3/4"       | 38.40             | 8.6           | 87.3         |
| 1/2"       | 27.50             | 6.2           | 81.1         |
| 3/8"       | 15.90             | 3.6           | 77.6         |
| No. 4      | 38.60             | 8.6           | 68.9         |
| No. 8      | 59.20             | 13.3          | 55.6         |
| No. 16     | 70.60             | 15.8          | 39.8         |
| No. 30     | 62.50             | 14.0          | 25.8         |
| No. 50     | 63.90             | 14.3          | 11.5         |
| No. 100    | 39.40             | 8.8           | 2.7          |
| No. 200    | 8.50              | 1.9           | 8.0          |
| Pan        | 3.50              | 0.8           |              |

446.40

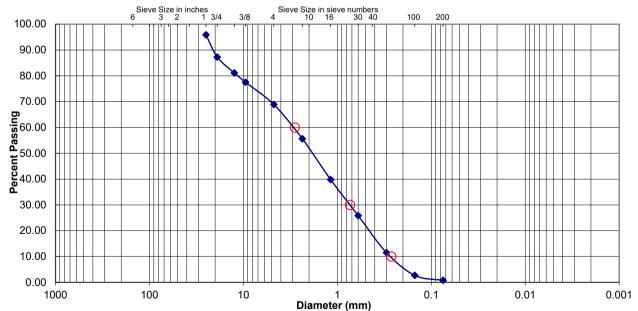
| % Gravel             | 31.1   |
|----------------------|--------|
| % Sand               | 68.1   |
| % Fines              | 0.8    |
| Fines Classification | ML     |
| •                    |        |
| D <sub>10</sub> (mm) | 0.2664 |
| D <sub>30</sub> (mm) | 0.7339 |
| D <sub>60</sub> (mm) | 2.8394 |
| •                    |        |
| Cu                   | 10.66  |
| Сс                   | 0.71   |
| •                    |        |

#### Classification

Poorly Graded Sand (SP) with Gravel

Classification determined by ASTM D 2487. -200 material classification determined by visual assessment, ASTM D 2488.

#### **Particle Size Distribution**



Comments

# **CORROSION TEST RESULTS**

| Client Name:  | Stantec   | AP Job No.: | 19-0916  |
|---------------|-----------|-------------|----------|
| Project Name: | 8me Kudu  | Date:       | 09/16/19 |
| Project No.:  | 185704635 |             |          |

| Boring<br>No. | Sample<br>Type | Depth<br>(feet) | Soil Type | Minimum<br>Resistivity (ohm-cm) | рН  | Sulfate Content (ppm) | Chloride Content (ppm) |
|---------------|----------------|-----------------|-----------|---------------------------------|-----|-----------------------|------------------------|
|               |                |                 |           |                                 |     |                       |                        |
| TP1           | Grab           | 2               | SC        | 4253                            | 8.8 | 35                    | 37                     |
| TP10          | Grab           | 5               | SW-SM     | 7245                            | 9.7 | 38                    | 38                     |
| TP20          | Grab           | 2               | SC        | 5291                            | 8.9 | 36                    | 33                     |
|               |                |                 |           |                                 |     |                       |                        |
|               |                |                 |           |                                 |     |                       |                        |
|               |                |                 |           |                                 |     |                       |                        |
|               |                |                 |           |                                 |     |                       |                        |
|               |                |                 |           |                                 |     |                       |                        |
|               |                |                 |           |                                 |     |                       |                        |
|               |                |                 |           |                                 |     |                       |                        |

NOTES: Resistivity Test and pH: California Test Method 643

Sulfate Content : California Test Method 417
Chloride Content : California Test Method 422

ND = Not Detectable

NA = Not Sufficient Sample

NR = Not Requested

#### **CEQA LEVEL GEOTECHNICAL STUDY**

Appendix C CEQA Guidelines form – Geology and Soils

# Appendix C CEQA GUIDELINES FORM – GEOLOGY AND SOILS



## **CEQA LEVEL GEOTECHNICAL STUDY**

Appendix C CEQA Guidelines form – Geology and Soils

| GEOLOGY AND SOILS  | Potentially<br>Significant<br>Impact | Less Than<br>Significant with<br>Mitigation<br>Incorporated | Less Than<br>Significant<br>Impact | No<br>Impact | Not<br>Applicable |
|--|--------------------------------------|---|------------------------------------|--------------|-------------------|
| Would the project:   |                                      |   |                                    |              |                   |
| a) Expose people or structures to potential substantial adverse effects, including the risk of loss, injury, or death involving:   |                                      |   |                                    |              |                   |
| i) Rupture of a known earthquake fault, as delineated on the most recent Alquist-Priolo Earthquake Fault Zoning Map issued by the State Geologist for the area or based on other substantial evidence of a known fault (refer to CDMG Special Publication 42)? |                                      |   | Х                                  |              |                   |
| ii) Strong Seismic ground shaking?   |                                      | Х   |                                    |              |                   |
| iii) Seismic-related ground failure, including liquefaction?   |                                      |   | Х                                  |              |                   |
| iv) Landslides?  |                                      |   | Х                                  |              |                   |
| b) Result in substantial soil erosion or the loss of topsoil?  |                                      | Χ   |                                    |              |                   |
| c) Be located on a geologic unit or soil that is unstable, or that would become unstable as a result of the project, and potentially result in onsite or offsite landslide, lateral spreading, subsidence, liquefaction, or collapse?                          |                                      |   | Х                                  |              |                   |
| d) Be located on expansive soil, as identified in Table 18-1-B of the Uniform Building Code (1994), creating substantial risks to life or property?  |                                      |   | X                                  |              |                   |
| e) Have soils incapable of adequately supporting the use of septic tanks or alternative waste water disposal systems where sewers are not available for disposal of waste water?   |                                      |   | Х                                  |              |                   |



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# Appendix G-2 Paleontological Inventory Report

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# PALEONTOLOGICAL INVENTORY REPORT

# Kudu Solar Project

69SV 8me LLC



Prepared for: Stantec

555 Capitol Mall, Suite 650 Sacramento, CA 95814-4583

Prepared by: Paleo Solutions, Inc.

911 S. Primrose Ave., Unit N

Monrovia, CA 91016

Courtney Richards, M.S. - Principal Investigator

Joey Raum, B.S. - Report Author

PSI Report: CA19KernSTA01R

February 4, 2020

STANTEC KUDU SOLAR PROJECT PSI REPORT NO.: CA19KERNSTA01R



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# **Table of Contents**

| 1.0     | EXECUTIVE SUMMARY                                       | 4  |
|---------|---|----|
| 2.0     | INTRODUCTION  | 6  |
| 2.1     | Project Description                                     | 6  |
| 2.2     | Project Location  |    |
| 3.0     | DEFINITION AND SIGNIFICANCE OF PALEONTOLOGICAL RESO     |    |
| 4.0     | LAWS, ORDINANCES, REGULATIONS, AND STANDARDS            | 11 |
| 4.1     | State Regulatory Setting                                |    |
| 4       | -1.1 California Environmental Quality Act (CEQA)        | 11 |
| 4       | -1.2 State of California Public Resources Code          | 11 |
| 4.2     | Local Regulatory Setting                                | 11 |
| 4       | -2.1 Kern County  | 11 |
| 5.0     | METHODS   | 12 |
| 5.1     | Analysis of Existing Data                               |    |
| 5.2     | Criteria for Evaluating Paleontological Potential       | 12 |
| 6.0     | ANALYSIS OF EXISTING DATA                               | 14 |
| 6.1     | Geologic Map and Literature Review                      | 15 |
| 6       | 5.1.1 Younger Alluvium (Qa) (Holocene)                  | 15 |
| 6       | 5.1.2 Older Alluvium (Qoa) (Pleistocene)                | 16 |
| 6.2     |   | 16 |
| 7.0     | IMPACTS TO PALEONTOLOGICAL RESOURCES                    |    |
| 8.0     | CONCLUSIONS AND RECOMMENDATIONS                         | 20 |
|         | RENCES  |    |
| APPE    | NDIX A  | 23 |
| APPE    | NDIX B  | 26 |
|         |   |    |
|         | Figures   |    |
| Figure  | 1. Project Location Map.                                | 7  |
| Figure  | 2. Project Overview Map.                                | 8  |
| Figure  | 3. Project Geology Map                                  | 17 |
|         |   |    |
|         | Tables  |    |
|         | 1. Kudu Solar Project Summary                           |    |
|         | 2. Potential Fossil Yield Classification (BLM, 2016)    |    |
| Table 3 | 3. Paleontological Literature and Record Search Results | 18 |



## 1.0 EXECUTIVE SUMMARY

This report presents the results of the paleontological technical study conducted by Paleo Solutions, Inc. (Paleo Solutions) in support of the 69SV 8me LLC Kudu Solar Project (Project) located in Kern County, California (see Figures 1 and 2). Paleo Solutions was contracted by Stantec to conduct an analysis of existing paleontological data and to provide recommendations for mitigation based on the geological and paleontological data. All paleontological work was completed in compliance with the California Environmental Quality Act (CEQA), local regulations, and best practices in mitigation paleontology (Murphey et al., 2019). See Table 1 for a Project summary.

69SV 8me LLC is developing a photovoltaic (PV) energy facility (up to 500 megawatt alternating current [MWac]) within the approximately 1,955-acre Project area. The Project area includes private parcels in both unincorporated Kern County and California City. The Project is located in the Mojave Desert Geomorphic Province, a region characterized by vast, arid expanses of barren mountain ranges, broad alluvial-filled flatlands, desiccated riverbeds and washes, extensive mesas, sand dunes, playas, volcanic cinder cones, and basaltic lava flows (Norris and Webb, 1990; Sylvester and O'Black Gans, 2016). The Project is specifically located on the United States Geological Survey (USGS) California City North (2018) and Mojave Northeast (2018) 7.5' topographic quadrangles in Townships 31 and 32 South, Range 37 East (see Appendix B).

The paleontological potential of the Project area was evaluated based on an analysis of existing paleontological data. The three components of the analysis of existing data included a geologic map review, a literature search, and an institutional record search. Geologic mapping indicates that the Project area is primarily underlain by Holocene-age younger alluvial gravel, sand, and silt of undissected valley fills derived from adjacent higher ground (Holocene-age younger alluvium; Qa) with a small amount of Pleistocene-age fanglomerate, gravel, sand, and silt of dissected older valley fills and alluvial fans, derived from adjacent highlands (Pleistocene-age older alluvium; Qoa) within the southeastern portion of the Project area (Dibblee and Minch, 2008; see Figure 3). Additionally, Pleistocene-age older alluvium (Qoa) often occurs at depth beneath Holocene-age younger alluvium or occurs as a mixture of undifferentiated alluvium with these younger deposits within the Mojave Desert Geomorphic Province (Dibblee and Minch, 2008; Reynolds, 1989).

According to the record search and the literature search, there are no previously recorded fossil localities within the Project area; however, the Natural History Museum of Los Angeles County (LACM) reported that there are three vertebrate fossil localities recorded in the Project vicinity from sedimentary deposits similar to those that occur in the Project area (McLeod, 2019). Furthermore, literature and database reviews also identified numerous vertebrate fossils recovered from Pleistocene-age older alluvium (Qoa) and other Pleistocene-age sedimentary deposits elsewhere in Kern County and southern California (see Table 3; Cooper and Eisentraut, 2002; Jahns, 1954; Jefferson, 1991; UCMP, 2019).

The Potential Fossil Yield Classification (PFYC) system was applied to the results of the analysis of existing data (see Table 2). Pleistocene-age older alluvium (Qoa) has a moderate paleontological potential (PFYC 3). Holocene-age younger alluvium (Qa) is estimated to be less than 11,000 years old and has a low paleontological potential (PFYC 2), because these deposits are too young to contain *in-situ* fossils. However, these younger deposits often overlie older geologic units with higher paleontological potential, which may be impacted at depth.

Based on the ground disturbance necessary to complete the Project, there is potential for adverse impacts to scientifically significant paleontological resources within Pleistocene-age older alluvium (Qoa) where mapped at the surface and where encountered in the subsurface beneath the Holocene-age younger alluvium (Qa). Therefore, it is recommended that excavations in locations of the Project area mapped as Pleistocene-age

STANTEC KUDU SOLAR PROJECT PSI REPORT NO.: CA19KERNSTA01R



older alluvium (Qoa) (PFYC 3) be initially monitored to determine whether Project excavations will disturb Pleistocene-age sedimentary deposits and scientifically significant fossils that may be preserved within them. Areas mapped as Holocene-age younger alluvium (Qa) should be spot-checked during excavations that exceed depths of 5 feet to check for underlying, paleontologically sensitive Pleistocene-age older alluvium (Qoa). If it is determined that only Holocene-age younger alluvium (Qa) (PFYC 2) is impacted, the monitoring program should be reduced or suspended.

Prior to the start of construction, a paleontological resource monitoring and mitigation plan (PRMMP) should be prepared. The PRMMP should provide detailed recommended monitoring locations including locations with moderate paleontological potential; a description of a worker training program; detailed procedures for monitoring, fossil recovery, laboratory analysis, and museum curation; and notification procedures in the event of a fossil discovery by paleontological monitors or other project personnel. A curation agreement with the LACM or another accredited repository should also be obtained and included as part of the PRMMP. Any subsurface bones or potential fossils that are unearthed during construction should be evaluated by a Qualified Paleontologist.



#### 2.0 INTRODUCTION

This report presents the results of the paleontological technical study conducted by Paleo Solutions in support of the 69SV 8me LLC Kudu Solar Project located in Kern County, California (Figures 1 and 2). Paleo Solutions was contracted by Stantec to conduct an analysis of existing paleontological data and to provide recommendations for mitigation based on the geological and paleontological data. All paleontological work was completed in compliance with CEQA, local regulations, and best practices in mitigation paleontology (Murphey et al., 2019). See Table 1 for a Project summary.

#### 2.1 Project Description

69SV 8me LLC is developing a PV energy facility (up to 500 MWac) within the approximately 1, 955-acre Project area. The Project area includes private parcels in both unincorporated Kern County and California City. Power generated by Kudu Solar will be delivered from the Project site via up to 230 kilovolt (kV) overhead general transmission lines (gen-tie) originating from the Eland 1 Substation and terminating at the Los Angeles Department of Water and Power (LADWP) Barren Ridge Substation. Upgrades needed to connect Kudu to the Eland 1 Substation will be covered in the Kudu Conditional Use Permits (CUPs), while the gen-tie right-of-way (ROW) has been analyzed in the Eland 1 Environmental Impact Report. The Project may also include a battery energy storage system (BESS) within the Project area, or a connection to the Eland 1 BESS.

#### 2.2 Project Location

The Project is located in the Mojave Desert Geomorphic Province, a region characterized by vast, arid expanses of barren mountain ranges, broad alluvial-filled flatlands, desiccated riverbeds and washes, extensive mesas, sand dunes, playas, volcanic cinder cones, and basaltic lava flows (Norris and Webb, 1990; Sylvester and O'Black Gans, 2016). The Project is located within and to the north of California City and south of the unincorporated community of Cantil on the USGS California City North (2018) and Mojave Northeast (2018) 7.5' topographic quadrangles in Townships 31 and 32 South, Range 37 East (Figures 1 and 2; Appendix B).

Geologic mapping indicates that the Project area is underlain by Holocene-age younger alluvium (Qa) and Pleistocene-age older alluvium (Qoa) (Dibblee and Minch, 2008; Figure 3). Additionally, Pleistocene-age older alluvium (Qoa) often occurs at depth beneath Holocene-age younger alluvium or occurs as a mixture of undifferentiated alluvium with these younger deposits within the Mojave Desert Geomorphic Province (Dibblee and Minch, 2008; Reynolds, 1989).



7

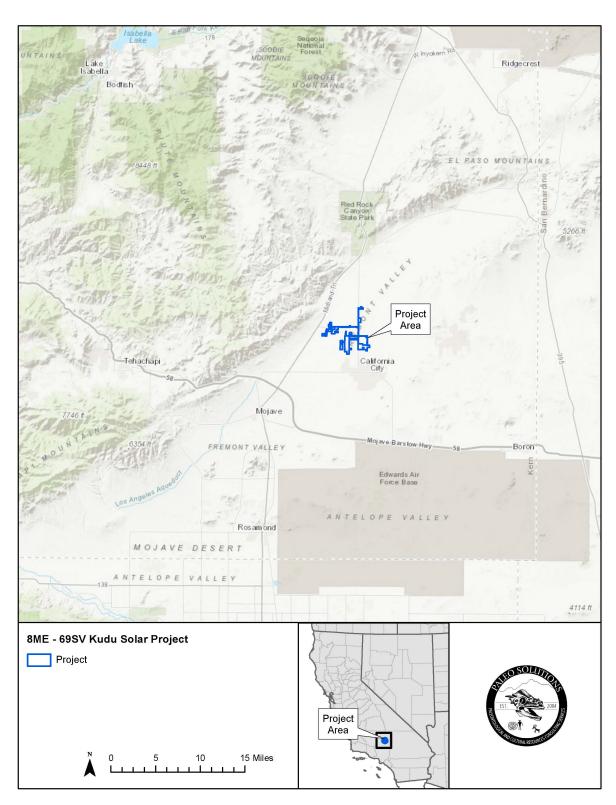


Figure 1. Project Location Map.



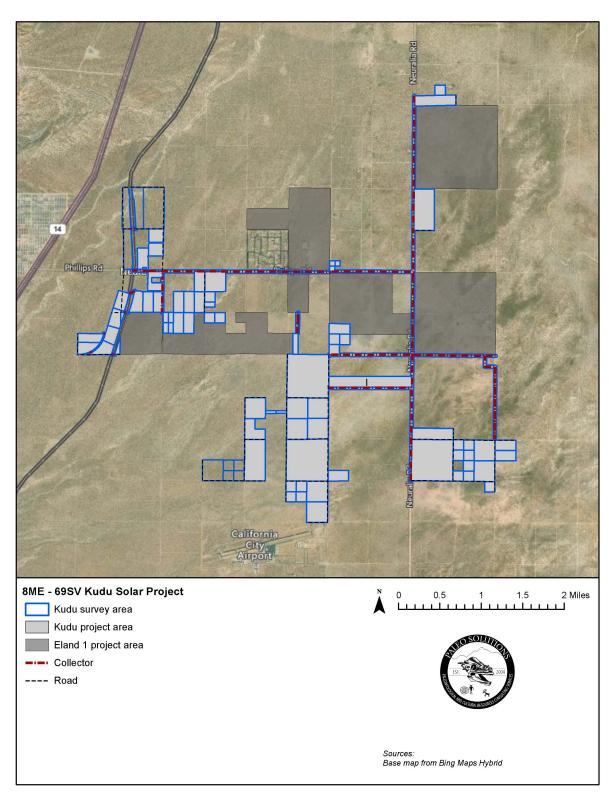


Figure 2. Project Overview Map.



9

Table 1. Kudu Solar Project Summary

| Project Name  | Kudu Solar Project   |         |                  |          |                 |                        |
|---|--|---------|------------------|----------|-----------------|------------------------|
| Project Description   | 69SV 8me LLC is developing a PV energy facility (up to 500 MWac) within the approximately 1,955-acre Project area. Power generated by Kudu Solar will be delivered from the Project site via up to 230 kV overhead gen-tie originating from the Eland 1 Substation and terminating at the LADWP Barren Ridge Substation. The Project may also include a BESS within the Project area, or a connection to the Eland 1 BESS.   |         |                  |          |                 |                        |
| Project Area  | The Project is located in the Mojave Desert Geomorphic Province, and is specifically located within and to the north of California City and south of the unincorporated community of Cantil in Kern County, California.  |         |                  |          |                 |                        |
| Total Acreage   | 1, 9551 acres  |         |                  |          |                 |                        |
| T (DI 00)   | Quarter-Quarter  |         | Section          | Т        | ownship         | Range                  |
| Location (PLSS)   |  |         | See App          | endix B  |                 | -1                     |
| Land Ownership  | Private  |         |                  |          |                 |                        |
| Topographic Map(s)  | USGS California City No  | orth (2 | 2018) and Mojav  | e North  | east (2018) 7.5 | ' Quadrangles          |
| Geologic Map(s)   | Geologic Map of the Mo<br>(Dibblee and Minch 2008  |         | nd Castle Butte  | 15' Qua  | drangles, Kern  | County, California     |
| Mapped Geologic   | Geologic Unit and M<br>Symbol  | ap      | Age              | Age      |                 | gical Potential (PFYC) |
| Units(s) and Age(s)   | Younger alluvium (Qa   | a)      | Holocene         |          |                 | 2 (Low)                |
|   | Older alluvium (Qoa)   | )       | Pleistoce        | ne       | 3 (Moderate)    |                        |
| Permits   | No permits were required   | d for t | the paleontologi | cal work | conducted.      |                        |
| Previously Documented Fossil Localities within the Project Area | The LACM reported that there are no vertebrate fossil localities recorded from within the Project area. However, there are several localities recorded from within the Project vicinity and other areas of California from sediments similar to those mapped within the Project area (see Section 5.2).  |         |                  |          |                 |                        |
| Recommendations   | Based on the ground disturbance necessary to complete the Project, there is potential for adverse impacts to scientifically significant paleontological resources within Pleistocene-age older alluvium (Qoa) where mapped at the surface and where encountered in the subsurface beneath the Holocene-age younger alluvium (Qa). Therefore, it is recommended that excavations in locations of the Project area mapped as Pleistocene-age older alluvium (Qoa) (PFYC 3) be initially monitored to determine whether Project excavations will disturb Pleistocene-age sedimentary deposits and scientifically significant fossils that may be preserved within them. Areas mapped as Holocene-age younger alluvium (Qa) should be spot-checked during excavations that exceed depths of 5 feet to check for underlying, paleontologically sensitive Pleistocene-age older alluvium (Qoa). If it is determined that only Holocene-age younger alluvium (Qa) (PFYC 2) is impacted, the monitoring program should be reduced or suspended. Prior to the start of construction, a PRMMP should be prepared. The PRMMP should provide detailed recommended monitoring locations including locations with moderate paleontological potential; a description of a worker training program; detailed procedures for monitoring, fossil recovery, laboratory analysis, and museum curation; and notification procedures in the event of a fossil discovery by paleontological monitors or other project personnel. A curation agreement with the LACM or another accredited repository should also be obtained and included as part of the PRMMP. Any subsurface bones or potential fossils that are unearthed during construction should be evaluated by a Qualified Paleontologist. |         |                  |          |                 |                        |



# 3.0 DEFINITION AND SIGNIFICANCE OF PALEONTOLOGICAL RESOURCES

As defined by Murphey and Daitch (2007): "Paleontology is a multidisciplinary science that combines elements of geology, biology, chemistry, and physics in an effort to understand the history of life on earth. Paleontological resources, or fossils, are the remains, imprints, or traces of once-living organisms preserved in rocks and sediments. These include mineralized, partially mineralized, or unmineralized bones and teeth, soft tissues, shells, wood, leaf impressions, footprints, burrows, and microscopic remains. Paleontological resources include not only fossils themselves, but also the associated rocks or organic matter and the physical characteristics of the fossils' associated sedimentary matrix.

The fossil record is the only evidence that life on earth has existed for more than 3.6 billion years. Fossils are considered non-renewable resources because the organisms they represent no longer exist. Thus, once destroyed, a fossil can never be replaced. Fossils are important scientific and educational resources because they are used to:

- Study the phylogenetic relationships amongst extinct organisms, as well as their relationships to modern groups;
- Elucidate the taphonomic, behavioral, temporal, and diagenetic pathways responsible for fossil preservation, including the biases inherent in the fossil record;
- Reconstruct ancient environments, climate change, and paleoecological relationships;
- Provide a measure of relative geologic dating that forms the basis for biochronology and biostratigraphy, and which is an independent and corroborating line of evidence for isotopic dating;
- Study the geographic distribution of organisms and tectonic movements of land masses and ocean basins through time;
- Study patterns and processes of evolution, extinction, and speciation; and
- Identify past and potential future human-caused effects to global environments and climates."

Fossil resources vary widely in their relative abundance and distribution and not all are regarded as significant. According to the Bureau of Land Management (BLM) Instructional Memorandum (IM) 2009-011, a "Significant Paleontological Resource" is defined as:

"Any paleontological resource that is considered to be of scientific interest, including most vertebrate fossil remains and traces, and certain rare or unusual invertebrate and plant fossils. A significant paleontological resource is considered to be of scientific interest if it is a rare or previously unknown species, it is of high quality and well-preserved, it preserves a previously unknown anatomical or other characteristic, provides new information about the history of life on earth, or has an identified educational or recreational value. Paleontological resources that may be considered not to have scientific significance include those that lack provenience or context, lack physical integrity due to decay or natural erosion, or that are overly redundant or are otherwise not useful for research. Vertebrate fossil remains and traces include bone, scales, scutes, skin impressions, burrows, tracks, tail drag marks, vertebrate coprolites (feces), gastroliths (stomach stones), or other physical evidence of past vertebrate life or activities" (BLM, 2008).



Vertebrate fossils, whether preserved remains or track ways, are classified as significant by most state and federal agencies and professional groups (and are specifically protected under the California Public Resources Code). In some cases, fossils of plants or invertebrate animals are also considered significant and can provide important information about ancient local environments.

The full significance of fossil specimens or fossil assemblages cannot be accurately predicted before they are collected, and in many cases, before they are prepared in the laboratory and compared with previously collected fossils. Pre-construction assessment of significance associated with an area or formation must be made based on previous finds, characteristics of the sediments, and other methods that can be used to determine paleoenvironmental and taphonomic conditions.

# 4.0 LAWS, ORDINANCES, REGULATIONS, AND STANDARDS

This section of the report presents the regulatory requirements pertaining to paleontological resources that apply to this Project.

### 4.1 State Regulatory Setting

### 4.1.1 California Environmental Quality Act (CEQA)

The procedures, types of activities, persons, and public agencies required to comply with the California Environmental Quality Act (CEQA) are defined in the Guidelines for Implementation of CEQA (State CEQA Guidelines), as amended on March 18, 2010 (Title 14, Section 15000 et seq. of the California Code of Regulations) and further amended January 4, 2013 and December 28, 2018. One of the questions listed in the CEQA Environmental Checklist is: "Would the project directly or indirectly destroy a unique paleontological resource or site or unique geologic feature?" (State CEQA Guidelines Appendix G, Section VII, Part F).

#### 4.1.2 State of California Public Resources Code

The State of California Public Resources Code (Chapter 1.7), Sections 5097 and 30244, includes additional state level requirements for the assessment and management of paleontological resources. These statutes require reasonable mitigation of adverse impacts to paleontological resources resulting from development on state lands, and define the excavation, destruction, or removal of paleontological "sites" or "features" from public lands without the express permission of the jurisdictional agency as a misdemeanor. As used in Section 5097, "state lands" refers to lands owned by, or under the jurisdiction of, the state or any state agency. "Public lands" is defined as lands owned by, or under the jurisdiction of, the state, or any city, county, district, authority, or public corporation, or any agency thereof.

### 4.2 Local Regulatory Setting

#### 4.2.1 Kern County

Paleontological resources are briefly mentioned in the Land Use, Open Space and Conservation element of the Kern County General Plan (Kern County, 2009) in Section 1.10.3, "Archaeological, Paleontological, Cultural, and Historical Preservation." Policy 25 states that the County will promote the preservation of cultural and historic resources which provide ties with the past and constitute a heritage value to residents and visitors. Implementation measure M is the only measure which directly or indirectly addresses paleontological resources, and it states that in areas of known paleontological resources, the County should address the preservation of these resources where feasible.



### 5.0 METHODS

The paleontological analysis of existing data included a geologic map review, literature review, and an institutional record search. The goal of this report is to evaluate the paleontological potential of the Project area and make recommendations for the mitigation of adverse impacts on paleontological resources that may occur as a result of the Project. Paleontological sensitivity assignments were determined using the PFYC system (BLM, 2016) and best practices in mitigation paleontology (Murphey et al., 2019). Joey Raum, B.S. (Field Director), performed the background research and co-authored this report with Courtney Richards, M.S. (Principal Investigator). Courtney Richards performed the technical review of this report. GIS maps were prepared by Barbara Webster, M.S.

Copies of this report will be submitted to 69SV 8me LLC, Stantec, and Kern County. Paleo Solutions will retain archival copy of all project information including maps and other data.

### 5.1 Analysis of Existing Data

Paleo Solutions reviewed geologic mapping of the Project site and half-mile buffer by T.W. Dibblee and J.A. Minch (2008). The literature reviewed included published and unpublished scientific papers. A paleontological museum record search was conducted at the LACM. Samuel McLeod, Ph.D., conducted the search (dated September 9, 2019), which is included as Appendix A. Additional record searches of online databases were completed by Paleo Solutions staff.

### 5.2 Criteria for Evaluating Paleontological Potential

The PFYC system was developed by the BLM (BLM, 2016). Because of its demonstrated usefulness as a resource management tool, the PFYC has been utilized for many years for projects across the country, regardless of land ownership. It is a predictive resource management tool that classifies geologic units on their likelihood to contain paleontological resources on a scale of 1 (very low potential) to 5 (very high potential). This system is intended to aid in predicting, assessing, and mitigating paleontological resources. The PFYC ranking system is summarized in Table 2.

Table 2. Potential Fossil Yield Classification (BLM, 2016).

| BLM PFYC<br>Designation | Assignment Criteria Guidelines and Management Summary (PFYC System)                |  |  |
|-------------------------|--|--|--|
|                         | Geologic units are not likely to contain recognizable paleontological resources.   |  |  |
|                         | Units are igneous or metamorphic, excluding air-fall and reworked volcanic ash     |  |  |
| 1 = Very Low            | units.   |  |  |
| Potential               | Units are Precambrian in age.  |  |  |
|                         | Management concern is usually negligible, and impact mitigation is unnecessary     |  |  |
|                         | except in rare or isolated circumstances.  |  |  |
|                         | Geologic units are not likely to contain paleontological resources.                |  |  |
|                         | Field surveys have verified that significant paleontological resources are not     |  |  |
|                         | present or are very rare.  |  |  |
|                         | Units are generally younger than 10,000 years before present.                      |  |  |
| 2 = Low Potential       | Recent eolian deposits.  |  |  |
|                         | Sediments exhibit significant physical and chemical changes (i.e., diagenetic      |  |  |
|                         | alteration) that make fossil preservation unlikely.                                |  |  |
|                         | Management concern is generally low, and impact mitigation is usually unnecessary  |  |  |
|                         | except in occasional or isolated circumstances.                                    |  |  |
| 3 = Moderate            | Sedimentary geologic units where fossil content varies in significance, abundance, |  |  |
| Potential               | and predictable occurrence.  |  |  |
| 1 Otellual              | Marine in origin with sporadic known occurrences of paleontological resources.     |  |  |



| BLM PFYC                 | Assistance of Criteria Criteria Criteria   |
|--------------------------|--|
| Designation              | Assignment Criteria Guidelines and Management Summary (PFYC System)  |
|                          | Paleontological resources may occur intermittently, but these occurrences are widely scattered.  |
|                          | The potential for authorized land use to impact a significant paleontological resource is known to be low-to-moderate.   |
|                          | Management concerns are moderate. Management options could include record searches, pre-disturbance surveys, monitoring, mitigation, or avoidance.  Opportunities may exist for hobby collecting. Surface-disturbing activities may require sufficient assessment to determine whether significant paleontological resources occur in the area of a proposed action and whether the action could affect the paleontological resources. |
|                          | Geologic units that are known to contain a high occurrence of paleontological resources.   |
|                          | Significant paleontological resources have been documented but may vary in occurrence and predictability.  |
| 4 = High Potential       | Surface-disturbing activities may adversely affect paleontological resources.  Rare or uncommon fossils, including nonvertebrate (such as soft body  |
| 0                        | preservation) or unusual plant fossils, may be present.  |
|                          | Illegal collecting activities may impact some areas.   |
|                          | Management concern is moderate to high depending on the proposed action. A field survey by a qualified paleontologist is often needed to assess local conditions. On-site monitoring or spot-checking may be necessary during land disturbing  |
|                          | activities. Avoidance of known paleontological resources may be necessary.   |
|                          | Highly fossiliferous geologic units that consistently and predictably produce significant paleontological resources.   |
|                          | Significant paleontological resources have been documented and occur consistently.   |
| 5 = Very High            | Paleontological resources are highly susceptible to adverse impacts from surface disturbing activities.  |
| Potential                | Unit is frequently the focus of illegal collecting activities.   |
|                          | Management concern is high to very high. A field survey by a qualified paleontologist is almost always needed and on-site monitoring may be necessary during land use activities. Avoidance or resource preservation through controlled access, designation of areas of avoidance, or special management designations should be considered.  |
|                          | Geologic units that cannot receive an informed PFYC assignment.  |
|                          | Geological units may exhibit features or preservational conditions that suggest significant paleontological resources could be present, but little information about the actual paleontological resources of the unit or area is known.  |
|                          | Geologic units represented on a map are based on lithologic character or basis of origin but have not been studied in detail.  |
| U = Unknown<br>Potential | Scientific literature does not exist or does not reveal the nature of paleontological resources.   |
|                          | Reports of paleontological resources are anecdotal or have not been verified.  |
|                          | Area or geologic unit is poorly or under-studied.  |
|                          | BLM staff has not yet been able to assess the nature of the geologic unit.   |
|                          | Until a provisional assignment is made, geologic units with unknown potential  |
|                          | have medium to high management concerns. Field surveys are normally necessary,   |
|                          | especially prior to authorizing a ground-disturbing activity.  |

STANTEC KUDU SOLAR PROJECT PSI REPORT NO.: CA19KERNSTA01R



### 6.0 ANALYSIS OF EXISTING DATA

The Project area is located within the Mojave Desert Geomorphic Province. A geomorphic province is a geographical area of distinct landscape character, with related geophysical features, including relief, landforms, orientations of valleys and mountains, type of vegetation, and other geomorphic attributes (Harden, 2004). Attributes of the Mojave Desert Geomorphic Province consist of vast, and expanses of barren mountain ranges, broad alluvial-filled flatlands, desiccated riverbeds and washes, extensive mesas, sand dunes, playas, volcanic cinder cones, and basaltic lava flows (Norris and Webb, 1990; Sylvester and O'Black Gans, 2016). Within California, the Mojave Desert Geomorphic Province occupies approximately 25,000 square miles of southeastern California and is bounded on the west by the Western Transverse Ranges, the San Gabriel Mountains, and the San Andreas Fault; on the north and northeast by the Garlock Fault, the Tehachapi Mountains, and the Basin and Range Geomorphic Province; on the east by the Nevada State Line and the Colorado River; and on the south by the Eastern Transverse Ranges, the San Andreas Fault, the Salton Trough, and the Colorado Desert, which generally coincide with the San Bernardino-Riverside counties boundary (Norris and Webb, 1990; Harden, 2004; Hall, 2007). Topographically, the Mojave Desert has a more subdued landform than the Basin and Range Geomorphic Province of California despite their related geologic histories, with the Mojave Desert containing relatively shorter and lower ranges and broader valleys than the Basin and Range (Harden, 2004). Additionally, the southeastern Mojave Desert lacks the northsouth-trending mountain ranges and basins typical of the Basin and Range (Sylvester and O'Black Gans, 2016). Despite its more subdued topography, the Mojave Desert Geomorphic Province has elevations typically above 2,000 feet above sea level, unlike the southern and adjacent Colorado Desert, which has some areas with elevations below sea level.

The geologic history of the Mojave Desert is related to the complex development of the Basin and Range of the southwestern United States and spans from the Proterozoic Eon to the Holocene Epoch (Norris and Webb, 1990; Harden, 2004; Hall, 2007; Sylvester and O'Black Gans, 2016; Prothero, 2017). Little is known about the geologic environment of southeastern California before the development of the passive continental margin, with the oldest rocks being of latest Proterozoic age (Harden, 2004). According to Norris and Webb (1990), between 2.5 and 1.7 billion years ago, the principal rocks in the region consisted of plutonic and extrusive igneous rocks and sedimentary rocks, which were subsequently metamorphosed to gneissic and highly schistose rocks and are exposed today in the Ord Mountains, the Old Woman Mountains, and the Marble Mountains of the Mojave Desert (Hall, 2007; Sylvester and O'Black Gans, 2016). Also around 2.5 and 1.7 billion years ago, magmatism and plutonic processes resulted in the deposition of Proterozoic-age granites and other igneous rocks in the region, followed by a brief geologic period of erosion and nondeposition (Norris and Webb, 1990; Harden, 2004). By the latest Neoproterozoic Era, the continental shelf edge subsided and supercontinents in the region broke apart, resulting in continental rifting and the formation of the passive continental margin (Norris and Webb, 1990; Harden, 2004; Hall, 2007). Due to continental divergence during the latest Neoproterozoic and the Cambrian Period, sandstone and calcareous mudstones were deposited (Norris and Webb, 1990).

Unlike the Basin and Range Geomorphic Province, the Mojave Desert Geomorphic Province yields only partial Paleozoic-age sections, which are mainly present within its eastern ranges and are relatively thinner than those exposed in the Basin and Range. For example, the lower Paleozoic sections of the Mojave Desert are represented by less than 5,000 feet of cumulative rock, with no continuous sections greater than 2,500 to 3,000 feet thick throughout most of the province; however, the thickest marine Paleozoic section within the Mojave Desert is exposed in the Providence Mountains, totaling approximately 10,000 feet, and upper Paleozoic strata are recognized in the Ord Mountains and near Victorville (Norris and Webb, 1990; Hall, 2007). Throughout most of the Paleozoic Era, shallow seas dominated the Mojave Desert region, with the deposition of limestone and dolomite representing deposition on a relatively stable continental platform (Norris and Webb, 1990; Hall, 2007).



During the Mesozoic Era, metamorphosed sedimentary rocks in the Mojave Desert were intruded by plutonic rocks (Norris and Webb, 1990). During the Triassic and early Jurassic periods, the region consisted of lowlands and regions of shallow seas, while the Mojave Desert region west of Barstow was rifted away and the typical north-south coastline of California was established (Hall, 2007). Marine early Triassic rocks are present in the Providence Mountains and represent a vast shallow sea that experienced episodic transgressions and regressions along the shoreline, which was located somewhere northwest of the eastern Mojave Desert during that time (Norris and Webb, 1990). However, by the early Jurassic, shallow seas had completely regressed to the northwest due to the Nevadan Orogeny uplifting the Mojave Desert block, causing arid conditions throughout most of the southwestern United States. These conditions are made evident by the deep red, oxidized eolian deposits and other nonmarine deposits (Norris and Webb, 1990). Throughout the middle Jurassic and the early Cretaceous, erosion and nondeposition occurred within the Mojave Desert region until the middle to late Cretaceous, when several pulses of magmatism resulted in plutonic rock intrusions into older rocks, resulting in local contact metamorphism of older geologic units (Hall, 2007). Mesozoic-age granitic rocks are abundant in the Mojave Desert region due to a large system of batholiths that formed along the subduction zone on the western edge of North America (Sylvester and O'Black Gans, 2016). According to Hall (2007), during the Cretaceous magmatism, tectonic forces resulted in the thrusting of older strata onto younger strata, and following the Cretaceous magmatism, extensional, normal, and detachment faults developed, offsetting Cretaceous-age plutonic rocks.

The oldest Cenozoic-age rocks in the Mojave Desert are of Oligocene age. Between the late Cretaceous and the Oligocene, widespread erosion or nondeposition were present within the Mojave Desert due to the degradation of the Nevadan Orogeny, which resulted in the reduction of the Mojave Desert to an area of relatively low relief by the latest Cretaceous (Hall, 2007). Despite the degradation of the Nevadan Orogeny, the Mojave Desert block had been uplifted approximately 10,000 to 15,000 feet by the beginning of the Miocene (Norris and Webb, 1990). During the middle and late Miocene, the Mojave Desert and Basin and Range regions experienced tectonic extension, with normal faults and related detachment faults characteristic of both provinces.

### 6.1 Geologic Map and Literature Review

Geologic mapping by Dibblee and Minch (2008) indicates that the Project area is primarily underlain by Holocene-age younger alluvium (Qa) with a small amount of Pleistocene-age older alluvium (Qoa) within the southeastern portion of the Project area. Pleistocene-age older alluvium (Qoa) is also known to occur at depth beneath Holocene-age younger alluvium (Qa) as a mixture of undifferentiated alluvium with these younger deposits within the Mojave Desert Province (Reynolds, 1989). The distributions of the geologic units in the Project area and vicinity, as mapped by Dibblee and Minch (2008), are provided in Figure 3.

#### 6.1.1 Younger Alluvium (Qa) (Holocene)

Holocene-age younger alluvium (Qa) consists of clay, silt, sand, and gravel that comprise valleys and alluvial fans. These sediments are generally poorly consolidated and represent sedimentation associated with current or former river and stream systems. Gravel is composed of igneous and metamorphic rocks that range from granule to cobble-sized and which generally vary between subangular to subrounded depending on the source proximity. Holocene-age younger alluvium (Qa) is mapped at the surface of the majority of the Project area (Dibblee and Minch, 2008; Figure 3). Fossils are generally unknown from Holocene-age younger alluvium (Qa), due to its young age. Reworked paleontological material from older deposits may be present but would lack critical stratigraphic contextual data. Holocene-age younger alluvium (Qa) is therefore considered to have a low paleontological potential (PFYC 2) using BLM (2016) guidelines. However, these sediments may overlie older, paleontologically sensitive deposits at depth.



### 6.1.2 Older Alluvium (Qoa) (Pleistocene)

Pleistocene-age older alluvium (Qoa) comprise fluvial sediments deposited on broad canyon floors by ancient river and stream systems. Sediments consist of medium- to coarse-grained sand and gravel from alluvial fans derived from the uplift of adjacent mountains, particularly the Rand Mountains located to the northeast of the Project area. These deposits are generally characterized by their low-moderate to moderate relief and dissected surfaces. They are relatively elevated and contrast the lower lying Holocene-age younger alluvium (Qa). Pleistocene-age older alluvium (Qoa) is mapped within the southeastern portion of the Project area, as well as in areas adjacent to the eastern portion of the Project area within the Project vicinity (Dibblee and Minch, 2008; Figure 3). Furthermore, these sediments likely occur at depth beneath younger Holocene-age younger alluvium (Qa) within the Project area (Reynolds, 1989).

Ice Age taxa have been recovered from Pleistocene-age deposits of Kern County, including specimens of extinct horse (Equus occidentalis), rabbit (Leporinae), camel (Procamelus), dog (Canidae), rodent (Thomomys, Microtus, Dipodomys, Neotoma), frog (Hyla), and lizard (Lacertilia) (UCMP, 2019; Table 3). Approximately 30,000 fossil specimens have been collected from Pleistocene-age sediments at McKittrick Tar Pits in western Kern County. These specimens include a diversity of species of rodents, rabbits, birds, camels, horses, bison, pronghorn antelope, and mammoths, as well as plants and preserved insects (UCMP, 2019; Table 3). Furthermore, numerous localities have been documented from Pleistocene-age lake deposits in Manix Lake, San Bernardino County, which is located approximately 90 miles northeast of the Project area. Recorded specimens include pond turtle (Emydidae), western pond turtle (Actinemys marmorata), stork (Ciconia maltha), flamingo (Phoenicopterus minutus, Phoenicopterus copei), golden eagle (Aquila chrysaetos), pelican (Pelecanus), American white pelican (Pelecanus erythrorhynchos), western grebe (Aechmophorus occidentalis), double-crested cormorant (Phalacrocorax auratus), great horned owl (Bubo virginianus), bony fish (Osteichthyes), chub (Gila mojavensis), hare or jackrabbit (Lepus), cat (Felis), saber-toothed cat (Smilodon californicus), short-faced bear (Arctodus), mammoth (Mammuthus), bison (Bison antiquus), horse (Equus), oreodont (Merychyus calaminthus), miniature camel (Stenomylus), camel (Camelidae, Camelops, Camelus, Hemiauchenia, Tanupolama, Tanupolama stevensi), pronghorn (Antilocapra), bighorn sheep (Ovis canadensis), coyote (Canis latrans), ground sloth (Nothrotheriops) (UCMP, 2019; Table 3). While the depositional environments of the McKittrick Tar Pit locality and the Manix Lake localities differ from that of the Project area, there is the potential for similar fauna to be recovered during Project excavations. Additional localities recorded from Pleistocene-age sedimentary deposits throughout southern California have produced specimens including mammoth (Mammuthus), mastodon (Mammut), camel (Camelidae), horse (Equidae), bison (Bison), giant ground sloth (Megatherium), peccary (Tayassuidae), cheetah (Acinonyx), lion (Panthera), saber-toothed cat (Smilodon), capybara (Hydrochoerus), dire wolf (Canis dirus), and numerous taxa of smaller mammals (Rodentia) (Cooper and Eisentraut, 2002; Jahns, 1954; Jefferson, 1991; Table 3). Pleistocene older alluvium is considered to have moderate paleontological potential (PFYC 3) using BLM (2016) guidelines.

### 6.2 Paleontological Record Search Results

Paleo Solutions requested a paleontological search of records maintained by the Natural History Museum of Los Angeles County. The museum responded on September 9, 2019 that there were no localities within the Project area (McLeod, 2019; Appendix A). However, there are fossil localities recorded in the Project vicinity from similar sedimentary deposits as those that likely occur at depth in the Project area (Table 3). Locality LACM 3721, located northeast of the Project area in Goler Gulch, is recorded from Pleistocene-age older alluvium (Qoa) at depth beneath Holocene-age younger alluvium (Qa) and produced fossil horse (Equus conversidens) (McLeod, 2019; Table 3). Locality 3722, located west-southwest of the Project area, is recorded from Pleistocene-age older alluvium (Qoa) at depth beneath Holocene-age younger alluvium (Qa) and produced fossil horse (Equus) (McLeod, 2019; Table 3). Locality 7891, located southwest of the Project area, is recorded from Pleistocene-age older alluvium (Qoa) and produced fossil camel (Hemiauchenia) (McLeod, 2019; Table 3).



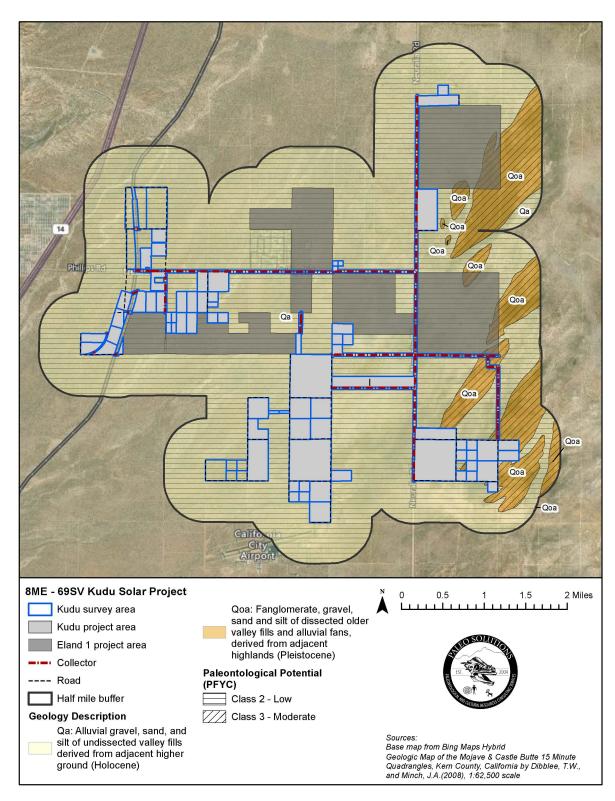


Figure 3. Project Geology Map.



Table 3. Paleontological Literature and Record Search Results

| Institutional<br>Locality<br>Number/Name   | Geologic<br>Unit                               | Taxon   | Common Name  | Location  | Source          |
|--|--|---|--|---|-----------------|
| LACM 3721  | Pleistocene- age older alluvium (Qoa)          |   | horse  | Goler Gulch,<br>northeast of<br>Project area                              | McLeod,<br>2019 |
| LACM 3722 Pleistocene-<br>age older<br>alluvium<br>(Qoa)   |  | Equus   | horse  | City of<br>Tehachapi,<br>west-<br>southwest of<br>Project area            | McLeod,<br>2019 |
| LACM 7891  | Pleistocene-<br>age older<br>alluvium<br>(Qoa) | Hemiauchenia  | camel  | Between Tehachapi Mountains and Rosamond Hills, southwest of Project area | McLeod,<br>2019 |
| Not Reported   | Pleistocene-<br>age older<br>alluvium<br>(Qoa) | Lacertilia Hyla Thomomys Microtus Dipodomys Neotoma Leporinae Canidae Equus occidentalis Procamelus   | lizard frog rodent rodent rodent rodent rodent dog horse camel   | Kern County   | UCMP,<br>2019   |
| McKittrick Tar<br>Pits   | Pleistocene-<br>age asphaltic<br>seep deposit  | -<br>-<br>-<br>-<br>-<br>-<br>-   | plant insect bird rodent rabbit camel horse bison pronghorn antelope mammoth   | McKittrick<br>Tar Pits (Kern<br>County)                                   | UCMP,<br>2019   |
| UCMP RV6735,<br>UCMP RV6736,<br>UCMP RV6738,<br>UCMP RV6746,<br>UCMP RV6751,<br>UCMP RV6752,<br>UCMP RV6758,<br>UCMP RV7021,<br>UCMP RV7051,<br>UCMP RV7053,<br>UCMP RV7054,<br>UCMP RV7054, | Pleistocene-<br>age Manix<br>Lake<br>Formation | Emydidae Actinemys marmorata Ciconia maltha Phoenicopterus minutus Phoenicopterus copei Aquila chrysaetos Pelecanus Pelecanus erythrorhynchos Aechmophorus occidentalis Phalacrocorax auratus Bubo virginianus Osteichthyes Gila mojavensis | pond turtle western pond turtle stork flamingo flamingo golden eagle pelican American white pelican western grebe double-crested cormorant great horned owl bony fish chub | Manix Lake,<br>San<br>Bernardino<br>County                                | UCMP,<br>2019   |



| Institutional Locality Number/Name | Geologic<br>Unit | Taxon                 | Common Name        | Location   | Source      |
|------------------------------------|------------------|-----------------------|--------------------|------------|-------------|
| UCMP RV7063,                       |                  | Lepus                 | hare or jackrabbit |            |             |
| UCMP RV7109,                       |                  | Felis                 | cat                |            |             |
| UCMP RV7131,                       |                  | Smilodon californicus | saber-toothed cat  |            |             |
| UCMP RV7139,                       |                  | Arctodus              | short-faced bear   |            |             |
| UCMP RV7140,                       |                  | Mammuthus             | mammoth            |            |             |
| UCMP RV6925,                       |                  | Bison antiquus        | bison              |            |             |
| UCMP V92103                        |                  | Equus                 | horse              |            |             |
|                                    |                  | Merychyus calaminthus | oreodont           |            |             |
|                                    |                  | Stenomylus            | miniature camel    |            |             |
|                                    |                  | Camelidae             | camel              |            |             |
|                                    |                  | Camelops              | camel              |            |             |
|                                    |                  | Camelus               | camel              |            |             |
|                                    |                  | Hemiauchenia          | camel              |            |             |
|                                    |                  | Tanupolama            | camel              |            |             |
|                                    |                  | Tanupolama stevensi   | camel              |            |             |
|                                    |                  | Antilocapra           | pronghorn          |            |             |
|                                    |                  | Ovis canadensis       | bighorn sheep      |            |             |
|                                    |                  | Canis latrans         | coyote             |            |             |
|                                    |                  | Nothrotheriops        | ground sloth       |            |             |
|                                    |                  | Mammuthus             | mammoth            |            |             |
|                                    |                  | Mammut                | mastodon           |            |             |
|                                    |                  | Camelidae             | camel              |            | Cooper      |
|                                    |                  | Equidae               | horse              |            | and         |
|                                    | Pleistocene-     | Bison                 | bison              |            | Eisentraut, |
| Not Reported                       | age              | Megatherium           | giant ground sloth | Southern   | 2002;       |
|                                    | sedimentary      | Tayassuidae           | peccary            | California | Jahns,      |
|                                    | ,                | Acinony $x$           | cheetah            | Camorna    | 1954;       |
|                                    | deposits         | Panthera              | lion               |            | Jefferson,  |
|                                    |                  | Smilodon              | saber-toothed cat  |            | 1991        |
|                                    |                  | Hydrochoerus          | capybara           |            | 1991        |
|                                    |                  | Canis dirus           | dire wolf          |            |             |
|                                    |                  | Rodentia              | rodent             |            |             |

### 7.0 IMPACTS TO PALEONTOLOGICAL RESOURCES

Impacts on paleontological resources can generally be classified as either direct, indirect, or cumulative. Direct adverse impacts on surface or subsurface paleontological resources are the result of destruction by breakage and crushing as the result of surface disturbing actions including construction excavations. In areas that contain paleontologically sensitive geologic units, ground disturbance has the potential to adversely impact surface and subsurface paleontological resources of scientific importance. Without mitigation, these fossils and the paleontological data they could provide if properly recovered and documented, could be adversely impacted (damaged or destroyed), rendering them permanently unavailable to science and society.

Indirect impacts typically include those effects which result from the continuing implementation of management decisions and resulting activities, including normal ongoing operations of facilities constructed within a given project area. They also occur as the result of the construction of new roads and trails in areas that were previously less accessible. This increases public access and therefore increases the likelihood of the loss of paleontological resources through vandalism and unlawful collecting. Human activities that increase erosion also cause indirect impacts to surface and subsurface fossils as the result of exposure, transport, weathering, and reburial.



Cumulative impacts can result from incrementally minor but collectively significant actions taking place over a period of time. The incremental loss of paleontological resources over time as a result of construction-related surface disturbance or vandalism and unlawful collection would represent a significant cumulative adverse impact because it would result in the destruction of non-renewable paleontological resources and the associated irretrievable loss of scientific information.

Excavations within the Project area that impact Pleistocene-age older alluvium (Qoa), either at the surface or at depth beneath Holocene-age younger alluvium (Qa), may well result in an adverse direct impact on scientifically important paleontological resources. Surface grading or shallow excavations entirely within Holocene-age younger alluvium (Qa) in the Project area are unlikely to uncover significant fossil vertebrate remains, since any recovered resources will lack stratigraphic context. However, these deposits may shallowly overlie older *in situ* sedimentary deposits. Therefore, grading and other earthmoving activities may potentially result in significant adverse direct impacts to paleontological resources throughout the entirety of the Project area.

No direct or cumulative impacts are anticipated from any of the planned Project activities.

### 8.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the ground disturbance necessary to complete the Project, there is potential for adverse impacts to scientifically significant paleontological resources within Pleistocene-age older alluvium (Qoa) where mapped at the surface and where encountered in the subsurface beneath the Holocene-age younger alluvium (Qa). Therefore, it is recommended that excavations in locations of the Project area mapped as Pleistocene-age older alluvium (Qoa) (PFYC 3) be initially monitored to determine whether Project excavations will disturb Pleistocene-age sedimentary deposits and scientifically significant fossils that may be preserved within them. Areas mapped as Holocene-age younger alluvium (Qa) should be spot-checked during excavations that exceed depths of 5 feet to check for underlying, paleontologically sensitive Pleistocene-age older alluvium (Qoa). If it is determined that only Holocene-age younger alluvium (Qa) (PFYC 2) is impacted, the monitoring program should be reduced or suspended.

Prior to the start of construction, a PRMMP should be prepared. The PRMMP should provide detailed recommended monitoring locations including locations with moderate paleontological potential; a description of a worker training program; detailed procedures for monitoring, fossil recovery, laboratory analysis, and museum curation; and notification procedures in the event of a fossil discovery by paleontological monitors or other project personnel. A curation agreement with the LACM or another accredited repository should also be obtained and included as part of the PRMMP. Any subsurface bones or potential fossils that are unearthed during construction should be evaluated by a Qualified Paleontologist.



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STANTEC KUDU SOLAR PROJECT PSI REPORT NO.: CA19KERNSTA01R



UCMP. 2019. Online records search of the University of California Museum of Paleontology Database, performed September 9-13, 2019.



### **APPENDIX A**

Natural History Museum of Los Angeles County Paleontological Record Search





Natural History Museum of Los Angeles County 900 Exposition Boulevard Los Angeles, CA 90007

tel 213.763.DINO www.nhm.org

Vertebrate Paleontology Section Telephone: (213) 763-3325

e-mail: smcleod@nhm.org

9 September 2019

Paleo Solutions, Inc. 911 South Primrose Avenue, Unit N Monrovia, CA 91016

Attn: Barbara Webster, GIS Specialist & Archaeologist

re: Paleontological resources for the proposed Kudu Solar Project, near California City, Kern County, project area

#### Dear Barbara:

I have conducted a thorough search of our paleontology collection records for the locality and specimen data for the proposed Kudu Solar Project, near California City, Kern County, project area as outlined on the portions of the Mojave NE and California City North USGS topographic quadrangle maps that you sent to me via e-mail on 26 August 2019. We do not have any vertebrate fossil localities that lie directly within the proposed project area boundaries, but we do have localities somewhat nearby from the same or similar sedimentary deposits as occur in the proposed project area, either at the surface or at depth.

In the slightly elevated terrain on the eastern margin of the proposed project area there are surface deposits that consist of relatively coarse older Quaternary Alluvium, derived as alluvial fan deposits from the Rand Mountains to the east and northeast. Otherwise the proposed project area has surface deposits of younger Quaternary Alluvium, derived as alluvial fan deposits from the Piute Mountains to the west and from the Rand Mountains to the east. These Quaternary deposits typically do not contain significant vertebrate fossils, at least in the uppermost layers. Our closest vertebrate fossil locality from these deposits is LACM 3722, west-southwest of the proposed project area and found during excavation for a sewer line within the city of Tehachapi, that produced a specimen of fossil horse, *Equus*. Our next closest vertebrate fossil locality from these deposits is probably LACM 3721, northeast of the proposed project area in Goler Gulch

Inspiring wonder, discovery and responsibility for our natural and cultural worlds.



northeast of Garlock, that produced a fossil specimen of horse, *Equus conversidens*. Further to the southwest of the proposed project area, near the California Aqueduct between the Tehachapi Mountains and the Rosamond Hills north of Willow Springs, our older Quaternary locality LACM 7891 produced a fossil specimen of camel, *Hemiauchenia*, at a depth of 21 feet below the surface.

Shallow excavations in the uppermost few feet of the older and younger Quaternary alluvial fan deposits in the proposed project area probably will not uncover significant fossil vertebrate remains. Deeper excavations in the proposed project area that extend down into older and perhaps finer-grained Quaternary deposits, however, may well encounter significant vertebrate fossils. Any substantial excavations in the proposed project area, therefore, should be closely monitored to quickly and professionally collect any specimens without impeding development. Also, sediment samples should be collected and processed to determine the small fossil potential in the proposed project area. Any fossils recovered during mitigation should be deposited in an accredited and permanent scientific institution for the benefit of current and future generations.

This records search covers only the vertebrate paleontology records of the Natural History Museum of Los Angeles County. It is not intended to be a thorough paleontological survey of the proposed project area covering other institutional records, a literature survey, or any potential on-site survey.

Sincerely,

Samuel A. McLeod, Ph.D. Vertebrate Paleontology

Summel a. M. Lead

enclosure: invoice



### **APPENDIX B**

**Public Land Survey System** 



| Quarter-Quarter   | Section  | Township | Range  |
|---|----------|----------|--------|
| SWSW, NWSW, SWNW, NWNW  | Sec.01   | -        |        |
| SWSW, SESW, SWSE, SESE, NWSW, NESE, SWNW,                                       | S = = 02 |          |        |
| SENE, NWNW, NENW, NWNE, NENE  | Sec.02   |          |        |
| SWSW, SESE, NWSW, NESE, SWNW, SENW, SWNE,                                       | Sec.03   |          |        |
| SENE, NWNW, NENW, NWNE, NENE  | Sec.03   |          |        |
| SWSW, SESW, SWSE, SESE, NWSW, NESW, NWSE,<br>NESE, SWNW, SWNE, SENE, NWNE, NENE | Sec.04   | T32S     |        |
| NENW  | Sec.06   |          |        |
| NWSE, NESE, SWNE, SENE  | Sec.08   |          |        |
| SWSE, SESE, NWSW, NWSE, NESE, SWNW, SWNE, SENE, NWNW, NENW, NWNE, NENE          | Sec.09   |          |        |
| NWSW, NESE, SWNW, SENE, NWNW, NENE  | Sec.10   |          |        |
| NWSW, NWSE, NESE, SWNW, SENW, SWNE, SENE, NWNW, NENW, NWNE, NENE                | Sec.11   |          |        |
| SWNW, SENW, NWNW, NENW  | Sec.12   |          |        |
| SWSW, SESW  | Sec.14   |          |        |
| SESE  | Sec.15   |          | R37E   |
| SESW, SWSE, SESE  | Sec.19   |          | II.57E |
| SWSW  | Sec.20   |          |        |
| SESE, NESE, SENE, NENE  | Sec.22   |          |        |
| SWSW, NWSW, SWNW, NWNW, NENW  | Sec.23   |          |        |
| SWSW, NWSW, NESW, SWNW, SENW, NWNW, NENW  | Sec.26   |          |        |
| SWSW, SESW, SWSE, SESE, NESE, SENE, NENE  | Sec.27   |          |        |
| SWSW, SESW, SWSE, SESE  | Sec.28   |          |        |
| SWSW, SESW, SWSE, SESE, SWNW, NWNW  | Sec.29   |          |        |
| SWSE, SESE, NWSE, NESE, NENW, NWNE, NENE, SENW, SWNE, SENE                      | Sec.30   | T31S     |        |
| SWSW, SESW, NWSW, NESW, NWSE, NESE, SENW,<br>SWNE, SENE, NENW, NWNE, NENE       | Sec.31   |          |        |
| NWSW, NESW, NWSE, NESE, SWNW, SENW, SWNE, SENE, NWNW, NENW, NWNE, NENE          | Sec.32   |          |        |
| SWSE, SESE, NWSE, NESE, SWNE, NWNW, NENW, NWNE, NENE                            | Sec.33   |          |        |
| NWNW, NENW, NWNE, NENE, SWSW, SESW, SWSE, SESE, NWSW, NESW, NESE, SENE          | Sec.34   |          |        |
| NWNW, NWSW, SWNW, SWSW, SESW, SWSE, SESE  | Sec.35   |          |        |
| SWSW  | Sec.36   |          |        |

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# **Appendix H**

Phase I Environmental Site Assessment

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### Kudu Solar Farm Phase I Environmental Site Assessment

December 4, 2019

### Prepared for:

69SV 8me LLC Eland 2 Solar CEI Parent, LLC 250 Sutter Street, Suite 600 San Francisco, CA 94108

### Prepared by:

Stantec Consulting Services Inc. 100 California Street, Suite 1000 San Francisco, CA 94111



This document entitled Phase I Environmental Site Assessment was prepared by Stantec Consulting Services Inc. ("Stantec") for the account of 69SV 8me LLC and Eland 2 Solar CEI Parent, LLC (the "Client"). Any reliance on this document by any third party is strictly prohibited. The material in it reflects Stantec's professional judgment in light of the scope, schedule and other limitations stated in the document and in the contract between Stantec and the Client. The opinions in the document are based on conditions and information existing at the time the document was published and do not take into account any subsequent changes. In preparing the document, Stantec did not verify information supplied to it by others. Any use which a third party makes of this document is the responsibility of such third party. Such third party agrees that Stantec shall not be responsible for costs or damages of any kind, if any, suffered by it or any other third party as a result of decisions made or actions taken based on this document.

All information, conclusions, and recommendations provided by Stantec in this document regarding the Phase I ESA have been prepared under the supervision of and reviewed by the professionals whose signatures appear below.

I declare that, to the best of my professional knowledge and belief, I meet the definition of Environmental Professional as defined in § 312.10 of 40 CFR 312. I have the specific qualifications based on education, training, and experience to assess a property of the nature, history, and setting of the Property. I have developed and performed all the appropriate inquiries in conformance with the standards and practices set forth in 40 CFR Part 312.

Prepared by (signature)

Dion Monge, Senior Scientist

Reviewed by Kylin D (signature)

Kyle Emerson, C.E.G., Managing Principal Geologist

Approved by \_\_\_\_\_\_

(signature)

Caitlin Barns, Senior Biologist

## **Table of Contents**

| ABB | REVIATIO                     | NS  |     |  |  |  |  |
|-----|------------------------------|---|-----|--|--|--|--|
| 1.0 | SUMMA                        | RY  | 1.1 |  |  |  |  |
| 2.0 | INTROD                       | OUCTION   | 2.1 |  |  |  |  |
| 2.1 |                              | RTY DESCRIPTION   |     |  |  |  |  |
| 2.2 |                              | L TERMS, CONDITIONS, AND SIGNIFICANT ASSUMPTIONS                  |     |  |  |  |  |
| 2.3 |                              | TIONS AND LIMITING CONDITIONS                                     |     |  |  |  |  |
| 2.4 |                              | NNEL QUALIFICATIONS   |     |  |  |  |  |
| 3.0 | USER-P                       | ROVIDED INFORMATION   | 3.1 |  |  |  |  |
| 4.0 | RECOR                        | DS REVIEW   | 4.1 |  |  |  |  |
| 4.1 | PHYSIC                       | AL SETTING  | 4.1 |  |  |  |  |
|     | 4.1.1                        | Property Topography and Surface Water Flow                        | 4.1 |  |  |  |  |
|     | 4.1.2                        | Regional and Property Geology                                     | 4.1 |  |  |  |  |
|     | 4.1.3                        | Regional and Property Hydrogeology                                |     |  |  |  |  |
| 4.2 | FEDER/                       | AL, STATE AND TRIBAL ENVIRONMENTAL RECORDS                        | 4.2 |  |  |  |  |
|     | 4.2.1                        | Listings for Property   |     |  |  |  |  |
|     | 4.2.2                        | Listings for Nearby Sites with Potential to Impact Property       |     |  |  |  |  |
| 4.3 | LOCAL/                       | REGIONAL ENVIRONMENTAL RECORDS                                    |     |  |  |  |  |
|     | 4.3.1                        | Kern County Department of Environmental Health                    |     |  |  |  |  |
|     | 4.3.2                        | Regional Water Quality Control Board (RWQCB)                      |     |  |  |  |  |
|     | 4.3.3                        | Department of Toxic Substances Control (DTSC)                     | 4.3 |  |  |  |  |
|     | 4.3.4                        | California City Building Department                               |     |  |  |  |  |
|     | 4.3.5                        | California Division of Oil, Gas, and Geothermal Resources (DOGGR) |     |  |  |  |  |
| 4.4 |                              | ICAL RECORDS REVIEW   |     |  |  |  |  |
|     | 4.4.1                        | Land Title Records/Deeds  |     |  |  |  |  |
|     | 4.4.2                        | Aerial Photographs  |     |  |  |  |  |
|     | 4.4.3                        | Historical Fire Insurance Maps                                    |     |  |  |  |  |
|     | 4.4.4                        | Historical Topographic Maps                                       |     |  |  |  |  |
|     | 4.4.5                        | Other Historical Sources  | 4.6 |  |  |  |  |
| 5.0 | SITE RE                      | CONNAISSANCE  | 5.1 |  |  |  |  |
| 5.1 | SITE RE                      | CONNAISSANCE METHODOLOGY  | 5.1 |  |  |  |  |
| 5.2 | GENER.                       | AL DESCRIPTION  | 5.1 |  |  |  |  |
| 5.3 | HAZARI                       | DOUS SUBSTANCES AND PETROLEUM PRODUCTS                            | 5.2 |  |  |  |  |
| 5.4 | INTERIO                      | OR OBSERVATIONS   | 5.2 |  |  |  |  |
| 5.5 | EXTERI                       | EXTERIOR OBSERVATIONS5.2  |     |  |  |  |  |
| 5.6 |                              | GROUND STORAGE TANKS/STRUCTURES                                   |     |  |  |  |  |
| 5.7 | ABOVEGROUND STORAGE TANKS5.3 |   |     |  |  |  |  |
| 5.8 |                              | ING PROPERTIES  |     |  |  |  |  |
|     | 5.8.1                        | Current Uses of Adjoining Properties                              |     |  |  |  |  |
|     | 5.8.2                        | Observed Evidence of Past Uses of Adjoining Properties            |     |  |  |  |  |



i

|      | 5.8.3              | Pits, Ponds or Lagoons on Adjoining Properties                | 5.4 |
|------|--------------------|---|-----|
| 5.9  | OBSER              | VED PHYSICAL SETTING  | 5.4 |
| 6.0  | INTERV             | 'IEWS   | 6.1 |
| 7.0  | EVALU              | ATION   | 7.1 |
| 7.1  | FINDIN             | GS AND OPINIONS   | 7.1 |
| 7.2  | DATA G             | 6APS  | 7.2 |
| 7.3  | CONCL              | USIONS  | 7.2 |
| 8.0  | NON-S              | COPE CONSIDERATIONS   | 8.1 |
| 8.1  | LEAD-B             | ASED PAINT  | 8.1 |
| 8.2  | ASBES <sup>*</sup> | TOS   | 8.1 |
| 8.3  | RADON              |   | 8.1 |
| 9.0  | REFER              | ENCES   | 9.1 |
| LIST | OF FIGUI           | RES   |     |
|      |                    | Property Location Map Property Details and Photo Location Map |     |
| LIST | OF APPE            | NDICES  |     |
| APP  | ENDIX A            | PHOTOGRAPHS OF THE PROPERTY AND VICINITY                      | A.1 |
| APP  | ENDIX B            | STANTEC RESUMES   | B.1 |
| APP  | ENDIX C            | ENVIRONMENTAL AGENCY DATABASE SEARCH REPORT                   | C.1 |
| APP  | ENDIX D            | HISTORICAL RECORDS  | D.1 |



### **Abbreviations**

AAI All Appropriate Inquiry

ACM asbestos-containing material

amsl Above mean sea level

AST aboveground storage tank

ASTM American Society for Testing and Materials

bgs below ground surface

CERCLA Comprehensive Environmental Response, Compensation, and Liability Act

CFR Code of Federal Regulations

Client 69SV 8me LLC and Eland 2 Solar CEI Parent, LLC

CREC controlled recognized environmental conditions

DOGGR California Division of Oil, Gas, and Geothermal Resources

DTSC Department of Toxic Substances Control

EP Environmental Professional

EPA United States Environmental Protection Agency

ESA Environmental Site Assessment

gen-tie generation tie

HREC historical recognized environmental conditions

LADWP Los Angeles Department of Water and Power

LBP lead-based paint

pCi/L PicoCuries per liter

Project/Property the proposed Kudu Solar Farm, 72 parcels of land or portions thereof located

approximately 1 mile east of the intersection of State Route 14 and Philips Road

REC recognized environmental conditions

SR State Route

Stantec Stantec Consulting Services Inc.

User 69SV 8me LLC and Eland 2 Solar CEI Parent, LLC

USGS United States Geological Survey

UST underground storage tank



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### 1.0 SUMMARY

This assessment has revealed no evidence of recognized environmental conditions (RECs) in connection with the Property. No further investigation appears to be warranted at this time.

Stantec Consulting Services Inc. (Stantec) has completed a Phase I Environmental Site Assessment (ESA) report for the proposed Kudu Solar Farm (alternatively, the Project), located approximately 1 mile east of the intersection of State Route (SR) 14 and Philips Road (Property), on behalf of 69SV 8me, LLC and Eland 2 Solar CEI Parent, LLC (Client or User). The work was performed according to Stantec's proposal and terms and conditions dated August 5, 2019. 69SV 8me, LLC has been designated as the User of this report.

The Phase I ESA was conducted in conformance with the requirements of American Society for Testing and Materials (ASTM) Designation E 1527-13, and All Appropriate Inquiry (AAI) as defined by the United States Environmental Protection Agency (EPA) in Title 40 of the Code of Federal Regulations (CFR), Part 312, except as may have been modified by the scope of work, and terms and conditions, requested by 8minute Solar Energy. Any exceptions to, or deletions from, the ASTM or AAI practice are described in Section 2.3, Exceptions and Limiting Conditions.

The Property is located in portions of unincorporated Kern County and California City, north of the California City Municipal Airport. It consists of 72 parcels totaling 1,965.95 acres of predominantly vacant and undeveloped land in unincorporated Kern County and California City. The User has proposed the construction and operation of an up to 500 megawatt-alternating current (MW-AC) utility-scale solar farm with energy storage, known as the Kudu Solar Farm, on the Property.

The Property is adjacent to the approved Eland 1 Solar Farm, south of the existing Springbok 1 & 2 Solar Farms, and southeast of the Los Angeles Department of Water and Power (LADWP) Beacon Solar facility. A Property location map is provided as Figure 1. A Property map illustrating the main features of the Property is provided as Figure 2. Photographs taken during the site reconnaissance visit are provided in Appendix A.

We have performed a Phase I ESA in conformance with the scope and limitations of ASTM Practice E1527 for the Property. Any exceptions to or deletions from this practice are described in Section 7.2, Data Gaps. This assessment has revealed no evidence of recognized environmental conditions (RECs) in connection with the Property. No further investigation appears to be warranted at this time.

However, the following items of note were identified during this ESA:

• Oil Wells. Based on Stantec's review of the California Division of Oil, Gas, and Geothermal Resources' (DOGGR's) Well Finder online database, and as confirmed by measurements provided in the individual well records, there are two oil wells on the Property. The wells are identified as National Security Oil Co. "1" (API: 0402932491) and Childs-Wall "1" (API: 0402932490). According to the records, National Security Oil Co. "1" was drilled in the early 1920s to 111 feet below ground surface (bgs) and deemed a dry hole. The handwritten location in the record is not clearly written so there are two potential locations for the well, but both would fall in the northern portion of APN: 302-32-101, as shown on Figure 2.



1.1

The Childs-Wall "1" well was drilled in 1945 to a depth of 2,232 feet bgs and found to be a dry hole. The records indicate that there is no casing in the hole and that it is a square wood conductor box that was cemented in place. The well was "closed" with a board nailed to the conductor box so the property owner could potentially convert it to a water well at a later date. According to the locational information provided in the well record, this well is located in the northwest portion of APN: 302-020-14.

Based on a review of available well records, the wells do not have any casing and therefore would not be able to be located using geophysical survey methods. Given that the wells were determined to be "dry holes" and because of the proposed use of the Property as a solar farm, the wells are not considered a REC, but they may be encountered during development. If these wells are encountered during grading or development, Stantec recommends that work be stopped in the area and DOGGR be contacted for evaluation and determination for any further requirements.

Adjacent Railroad Easement. A railroad easement crosses through the Property, but a buffer of undeveloped
land that is approximately 75 feet or more is present between the boundary and the railroad tracks. The one
exception to this is in areas where the proposed generation tie (gen-tie) lines would cross the railroad tracks.

Given the distance from the Property boundary to the railroad tracks, no further assessment is recommended. However, if subsurface work is proposed for the installation of gen-tie lines or poles in areas that are within 20 feet of the railroad tracks, Stantec would recommend evaluation of soil samples to determine whether metals concentrations in soil are above California hazardous waste levels or regulatory thresholds that may pose a risk to future onsite construction workers.

 Potential Water Wells. Suspect water wells were observed during the field reconnaissance near the Property boundaries. Stantec recommends that all known and unknown (those encountered during proposed development activities) water wells be abandoned in accordance with applicable regulations unless the wells would be used for the Project.

The preceding summary is intended for informational purposes only. Reading of the full body of this report is recommended.



1.2

Introduction December 4, 2019

### 2.0 INTRODUCTION

The objective of this Phase I ESA was to perform AAI into the past ownership and uses of the Property consistent with good commercial or customary practice as outlined by the ASTM in "Standard Practice for Environmental Site Assessments: Phase I Environmental Site Assessment Process", Designation E1527-13. AAI is the process for evaluating a property's environmental conditions for the purpose of qualifying for landowner liability protections under the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA). following final rule of 40 CFR Part 312. The purpose of this Phase I ESA was to identify, to the extent feasible, adverse environmental conditions including RECs of the Property.

The ASTM E1527-13 standard indicates that the purpose of the Phase I ESA is to identify RECs, including historical recognized environmental conditions (HRECs), and controlled recognized environmental conditions (CRECs) that may exist at a property. The term "recognized environmental conditions" means the presence or likely presence of any hazardous substances or petroleum products in, on, or at a property:

- 1. due to any release to the environment;
- 2. under conditions indicative of a release to the environment; or
- 3. under conditions that pose a material threat of a future release to the environment.

ASTM defines HREC as a REC that has occurred in connection with a property but has been addressed to the satisfaction of the applicable regulatory authority and meets current unrestricted use criteria established by a regulatory authority without subjecting the property to any required controls (e.g., property use restrictions, activity and use limitations, institutional controls, or engineering controls). Before calling the past release a HREC, the environmental professional (EP) must determine whether the past release is a REC when the current Phase I ESA is conducted (e.g., if there has been a change in the regulations). If the EP considers the past release to be a REC at the time the Phase I ESA is conducted, the condition shall be included in the conclusions section of the report as a REC.

ASTM defines CREC as a REC resulting from a past release of hazardous substances or petroleum products that has been addressed to the satisfaction of the applicable regulatory authority (e.g., as evidenced by the issuance of a no further action letter or equivalent, or meeting risk-based criteria established by regulatory authority), but with hazardous substances or petroleum products allowed to remain in place subject to the implementation of required controls (e.g., property use restrictions, activity and use limitations, institutional controls, or engineering controls).

As defined by ASTM, RECs can include hazardous substances or petroleum products present under conditions in compliance with laws if that presence represents a material threat of future release. The presence of hazardous substances or petroleum products is, however, not a REC if that presence is a *de minimis* condition. *De minimis* conditions are minor occurrences of contamination that generally do not present a material risk to human health and would not likely be subject to enforcement action if brought to the attention of governmental agencies.

This Phase I ESA was conducted in accordance with our proposal to 8minutenergy dated August 5, 2019, and Client's authorization on August 12, 2019. The scope of work conducted during this Phase I ESA consisted of a visual reconnaissance of the Property, interviews with key individuals, and review of reasonably obtainable documents. The



Introduction December 4, 2019

scope of work did <u>not</u> include an assessment for environmental regulatory compliance of any facility ever operated at the Property (past or present), or sampling and analyzing of environmental media. Stantec was not contracted to perform an independent evaluation of the purchase or lease price of the Property and its relationship to current fair market value. The conclusions presented in this Phase I ESA report are professional opinions based on data described herein. The opinions are subject to the limitations described in Section 2.3, Exceptions and Limiting Conditions.

ASTM E1527-13 notes that the availability of record information varies by source. The User or EP is not obligated to identify, obtain, or review every possible source that might exist with respect to a property. Instead, ASTM identifies record information that is reasonably ascertainable from standard sources. "Reasonably ascertainable" is defined as follows:

- 1. information that is publicly available;
- 2. information that is obtainable from its source within reasonable time and cost constraints; and
- 3. information that is practicably reviewable.

#### 2.1 PROPERTY DESCRIPTION

The Property is located in portions of unincorporated Kern County and California City, north of the California City Municipal Airport. It consists of 72 parcels totaling 1,965.95 acres of predominantly vacant and undeveloped land in unincorporated Kern County and California City. The User has proposed the construction and operation of an up to 500 MW-AC utility-scale solar farm with energy storage, known as the Kudu Solar Farm.

The Property is adjacent to the approved Eland 1 Solar Farm, south of the existing Springbok 1 & 2 Solar Farms and southeast of the LADWP Beacon Solar facility. A Property location map is provided as Figure 1. A Property map illustrating the main features of the Property is provided as Figure 2. Photographs taken during the site reconnaissance visit are provided in Appendix A.

The table below provides a summary of the parcel numbers and acreage that are a part of the Property:

| APN             | Acres | Owner                                  |  |
|-----------------|-------|--|--|
| Kern County Par | cels  |  |  |
| 469-170-10      | 10.02 | KEREN & ASSCS, LLC                     |  |
| 469-170-18      | 39.49 | KEREN & ASSCS, LLC                     |  |
| 470-020-19      | 4.38  | JANIEKAY, LLC                          |  |
| 470-030-01      | 79.22 | ANDARI, GHAZI N.                       |  |
| 470-080-15      | 20.27 | AEK GLOBAL INVESTMENT, LLC             |  |
| 470-080-16      | 10.07 | WOLFE, JEFFREY                         |  |
| 470-080-17      | 10.10 | WOLFE, JEFFREY                         |  |
| 470-080-32      | 10.07 | MOORE, JOHN T. & DONNA L. FAMILY TRUST |  |
| 470-151-09      | 19.62 | MAZIN FAMILY TRUST                     |  |
| 470-151-15      | 20.23 | ARAGON, GENARO & GUADALUPE             |  |
| 470-151-16      | 20.40 | AHN, HYUNG                             |  |



Introduction December 4, 2019

| APN                     | Acres  | Owner                                      |  |  |
|-------------------------|--------|--|--|--|
| 470-151-17              | 19.98  | CLERICO, ROBERT W. TRUST                   |  |  |
| 470-152-01              | 39.32  | DHUPAR, SURINDER K. ET AL.                 |  |  |
| 470-152-18              | 10.32  | JOHANSING, LOYDELL H. & DAVID A.           |  |  |
| 470-152-19              | 4.93   | MITCHELL, LORI LYNN                        |  |  |
| 470-322-15              | 9.96   | INLAND MANAGEMENT, LLC                     |  |  |
| 470-330-01              | 5.06   | OAK INVS, LLC                              |  |  |
| 470-330-02              | 4.77   | OAK INVS, LLC                              |  |  |
| 470-330-03              | 19.86  | MEUNIER, PHYLLIS TRUST                     |  |  |
| 470-330-04              | 20.15  | MEUNIER, PHYLLIS TRUST                     |  |  |
| 470-330-06              | 9.95   | KANE, MARY                                 |  |  |
| 470-330-07              | 10.02  | AZAM, JAVED & ROOBILA NAZ FAMILY TRUST     |  |  |
| 470-330-14              | 4.89   | OAK INVS, LLC                              |  |  |
| 470-330-15              | 5.23   | YABLONSKI FAMILY TRUST A                   |  |  |
| 470-350-04              | 18.65  | HILBON, STEVEN                             |  |  |
| 470-350-05              | 18.91  | DISCOUNTLAND, INC.                         |  |  |
| 470-350-06              | 18.89  | KHATIBI, EBRAHIM                           |  |  |
| 470-350-07              | 18.57  | DISCOUNTLAND, INC.                         |  |  |
| 470-350-08              | 19.93  | WESTPALM DEV. CO.                          |  |  |
| 470-380-01              | 19.92  | HILBON, STEVEN                             |  |  |
| 470-380-04              | 21.35  | ROBERTO FAMILY TRUST ET AL.                |  |  |
| 470-380-05              | 17.34  | SMITH, ALVA E. & BETTY M. REV LIVING TRUST |  |  |
| 470-380-06              | 19.88  | HIGGINS, MICHAEL                           |  |  |
| 470-380-07              | 21.95  | CABLE, JAMEY                               |  |  |
| California City Parcels |        |  |  |  |
| 302-020-08              | 40.17  | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-020-09              | 80.09  | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-020-11              | 163.67 | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-020-14              | 40.99  | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-020-15              | 10.52  | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-020-16              | 10.15  | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-020-17              | 9.59   | ORTON FAMILY TRUST                         |  |  |
| 302-020-18              | 9.98   | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-290-03              | 83.58  | PEACE, JUDY ET AL.                         |  |  |
| 302-305-15              | 43.54  | WANG, NATHAN & LINDA                       |  |  |
| 302-321-01              | 160.93 | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-322-01              | 10.10  | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-322-02              | 10.09  | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |
| 302-322-04              | 10.24  | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |  |  |



Introduction December 4, 2019

| APN           | Acres    | Owner                                      |
|---------------|----------|--|
| 302-322-05    | 10.28    | ORTON FAMILY TRUST                         |
| 302-322-06    | 40.04    | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |
| 302-322-08    | 10.33    | ORTON FAMILY TRUST                         |
| 302-322-09    | 40.49    | ORTON FAMILY TRUST                         |
| 302-322-10    | 10.27    | ORTON, DAVID M. & PATRICIA D. FAMILY TRUST |
| 302-322-11    | 10.29    | ORTON FAMILY TRUST                         |
| 302-325-49    | 9.74     | STILLIENS, MARVIN E. & CAROLYN M.          |
| 302-330-33    | 20.21    | O'LAUGHLIN, JEANIE & RANDALL               |
| 302-330-37    | 20.38    | STALKNEGT FAMILY TRUST                     |
| 302-341-29    | 168.79   | BESSONART, DENIS & JULIE LIVING TRUST      |
| 302-342-01    | 40.22    | INLAND MANAGEMENT, LLC                     |
| 302-342-11    | 2.67     | POLAN, HAROLD E. & AUDREY A.               |
| 302-342-12    | 2.66     | O'BRIEN, SUSAN                             |
| 302-342-19    | 29.69    | KOLLAR, M M TR & MONTONNA WM               |
| 302-342-25    | 40.77    | REINELT FAMILY TRUST                       |
| 302-342-26    | 39.89    | REINELT FAMILY TRUST                       |
| 302-342-27    | 40.29    | REINELT FAMILY TRUST                       |
| 302-342-28    | 40.68    | REINELT FAMILY TRUST                       |
| 302-381-12    | 40.06    | GEPHART, ROSS & JUDITH M.                  |
| 302-381-13    | 9.94     | GEPHART, ROSS & JUDITH M.                  |
| 302-381-14    | 10.07    | GEPHART, ROSS & JUDITH M.                  |
| 302-381-15    | 10.38    | GEPHART, ROSS & JUDITH M.                  |
| 302-381-16    | 10.27    | GEPHART, ROSS & JUDITH M.                  |
| 302-470-14    | 20.20    | CAMARA, MARGARET ELDRED TRUST              |
| Total Acreage | 1,965.95 |  |

### 2.2 SPECIAL TERMS, CONDITIONS, AND SIGNIFICANT ASSUMPTIONS

There were no special terms, conditions, associated with the Phase I ESA. However, there is an unknown condition, where it is unclear as of this date if certain features (pipeline and wells) are part of the property to be acquired.

### 2.3 EXCEPTIONS AND LIMITING CONDITIONS

This report documents work that was performed in accordance with generally accepted professional standards at the time and location in which the services were provided and given the schedule and budget constraints established by the Client. No other representations, warranties, or guarantees are made concerning the accuracy or completeness of the data or conclusions contained within this report, including no assurance that this work has uncovered all potential and actual liabilities and conditions associated with the Property.



Introduction December 4, 2019

This report provides an evaluation of selected environmental conditions associated with the Property that was assessed at the time that the work was conducted and is based on information obtained by and/or provided to Stantec at that time. There are no assurances regarding the accuracy and completeness of this information. All information received from the Client or third parties in the preparation of this report has been assumed by Stantec to be correct. Stantec assumes no responsibility for any deficiency or inaccuracy in information received from others.

Conclusions made within this report consist of Stantec's professional opinion as of the time of the writing of this report and are based solely on the scope of work described in the report, the limited data available, and the results of the work. They are not a certification of the Property's environmental condition.

The Client did not provide or contract Stantec to provide recorded title records or search results for environmental liens or activity and use limitations encumbering the Property or in connection with the Property. Stantec did not obtain historical records that document the Property history in 5-year intervals. Although this resulted in data gaps, these data gaps are not considered significant. Based on the information obtained during this ESA and general knowledge of development at and near the Property, the absence of this information did not affect the ability of the EPs to identify RECs, CRECs, or *de minimis* conditions.

This report relates solely to the project for which Stantec was retained and the stated purpose for which this report was prepared and shall not be used or relied upon by the Client for any variation or extension of this project, any other project, or any other purpose.

This report has been prepared for the exclusive use of the Client identified herein, and any use of or reliance on this report by any third party is prohibited except as may be consented to in writing by Stantec or as required by law. The provision of any such consent is at Stantec's sole and unfettered discretion and will only be authorized pursuant to the conditions of Stantec's standard form reliance letter. Stantec assumes no responsibility for losses, damages, liabilities, or claims, howsoever arising, from third party use of this report.

Project-specific limiting conditions are provided in Section 2.2, Special Terms, Conditions, and Significant Assumptions.

The locations of any utilities, buildings and structures, and Property boundaries illustrated in or described within this report, if any, including pole lines, conduits, water mains, sewers and other surface or sub-surface utilities and structures, are not guaranteed. Before starting site work, the exact location of all such utilities and structures must be confirmed by the Client and the party performing the work, and Stantec assumes no liability resulting from damage to such utilities and structures.

The conclusions are based on the conditions encountered at the Property by Stantec at the time the work was conducted.

As the purpose of this report is to identify Property conditions that may pose an environmental risk; the identification of non-environmental risks to structures or people on the Property is beyond the scope of this assessment.

The findings, observations, and conclusions expressed by Stantec in this report are not an opinion concerning the compliance of any past or present owner or operator of the Property that is the subject of this report with any federal, state, provincial, or local law or regulation.



Introduction December 4, 2019

This report presents professional opinions and findings of a scientific and technical nature. It does not and shall not be construed to offer a legal opinion or representations as to the requirements of or compliance with, environmental laws, rules, regulations or policies of federal, state, provincial, or local governmental agencies. It is recommended that issues raised by the report should be reviewed for the Client by its legal counsel.

Stantec specifically disclaims any responsibility to update the conclusions in this report if new or different information later becomes available or if the conditions or activities on the property subsequently change.

### 2.4 PERSONNEL QUALIFICATIONS

This Phase I ESA was conducted by or under the supervision of an individual that meets the ASTM definition of an EP. The credentials of the EP and other key Stantec personnel involved in conducting this Phase I ESA are provided in Appendix B.



User-Provided Information December 4, 2019

### 3.0 USER-PROVIDED INFORMATION

ASTM E1527-13 describes responsibilities of the User to complete certain tasks in connection with the performance of AAI into the Property. The ASTM standard requires that the EP request information from the User on the results of those tasks because that information can assist in the identification of RECs, CRECs, HRECs, or *de minimis* conditions in connection with the Property. Towards that end, Stantec requested that the User provide the following documents and information:

| Description of Information                                    | Provided<br>(Yes / No) | Description and/or Key Findings  |
|---|------------------------|--|
| User Questionnaire and/or Interview                           | No                     | A completed user questionnaire was not provided. Given the historical documents available for the Property, the lack of a completed user questionnaire is not considered a significant data gap. |
| Environmental Liens or Activity Use<br>Limitations            | No                     | Land title records and deeds were not provided by the User, and public records were not searched by Stantec.   |
| Previous Environmental Permits or Reports<br>Provided by User | No                     | None provided  |
| Purpose of the Phase I ESA                                    | Yes                    | Due diligence  |



3.1

Records Review December 4, 2019

### 4.0 RECORDS REVIEW

The objective of consulting historical sources of information is to develop the history of the Property and surrounding area and evaluate if past uses may have resulted in RECs. Physical setting records are evaluated to determine if the physical setting may have contributed to adverse environmental conditions in connection with the Property. During the review of historical records, Stantec attempted to identify uses of the Property from the present to the first developed use of the Property. Stantec's research included the reasonably ascertainable and useful records described in this section.

### 4.1 PHYSICAL SETTING

A summary of the physical setting of the Property is provided in the table below with additional details in the following subsections:

| Topography:  | Most of the Property topography slopes to the northeast at elevations range from approximately 2,440 feet above mean sea level (amsl) to approximately 2,280 feet amsl.   |
|--|---|
| Soil/Bedrock Data:   | The Property is underlain by Holocene or later Pleistocene sandy alluvium, which in turn overlies older, Plio-Pleistocene clayey Alluvium.  |
| Estimated Depth to Groundwater/ Estimated Direction of Gradient: | Due to the wide range in topography across the Property, the depth to groundwater is expected to vary. The Environmental Data Resources, Inc. (EDR) DataMap™ Well Search records indicated the depth to water in nearby water wells ranges between 190 feet bgs to more than 300 feet bgs (EDR 2019). Location-specific groundwater direction and elevations are not known. |

Note: Site-specific groundwater flow direction and depth can be determined only by site-specific testing, which Stantec has not conducted.

### 4.1.1 Property Topography and Surface Water Flow

There is at least 160 feet of topographic relief at the Property with elevations ranging from 2,440 feet amsl in the southwest to 2,280 feet amsl in the northeast (U.S. Geological Survey [USGS] 2012). Based on the topography, surface water on the Property infiltrates the ground surface or flows overland to the northeast.

### 4.1.2 Regional and Property Geology

The Property is in the Mojave Desert geomorphic province of California, which spans 25,000 square miles and is landlocked. The Mojave Desert is a wedge-shaped structural block that is enclosed to the southwest by the San Andreas Fault and the Traverse Ranges, while the north and northeast is enclosed by the Garlock Fault, the Tehachapi Mountains, and the Basin and Range. The Colorado River and the Nevada State Line form the eastern boundary of the province, and finally, the San Bernardino-Riverside County line forms the southern boundary. The desert itself is of Cenozoic nature and likely formed from the movements of the San Andreas and Garlock faults. The region is currently dominated by broad alluvial basins that are aggrading surfaces that receive nonmarine continental



Records Review December 4, 2019

deposits from the adjacent upland areas. The western portion of the province is riddled with north-west trending faults (San Andreas Fault being most predominant) and with east-west trending Garlock Fault.

The Property is underlain by Holocene or later Pleistocene sandy alluvium, which in turn overlies older, Plio-Pleistocene clayey alluvium.

#### 4.1.3 Regional and Property Hydrogeology

The Property is located within the Fremont Valley Groundwater Basin, which underlies Fremont Valley in eastern Kern County and northwestern San Bernardino County. The basin is bounded on the northwest by the Garlock fault zone against impermeable crystalline rocks of the El Paso Mountains and the Sierra Nevada. This basin is bounded on the east by crystalline rocks of the Summit Range, Red Mountain, Lava Mountains, Rand Mountains, Castle Butte, Bissel Hills, and Rosamond Hills. The basin is bounded on the southwest by the Antelope Valley Groundwater Basin along a groundwater divide approximated by a line connecting the mouth of Oak Creek through Middle Butte to exposed basement rock near Gem Hill. Both Quaternary alluvium and lacustrine deposits are water-bearing; however, the alluvium is the most important water-bearing material in the basin (California Department of Water Resources 2004).

Due to the wide range in topography across the Property, the depth to groundwater is expected to vary. The EDR DataMap™ Well Search records indicated the depth to water in nearby water wells ranges between 190 feet bgs to more than 300 feet bgs. Location-specific groundwater direction and elevations are not known.

### 4.2 FEDERAL, STATE AND TRIBAL ENVIRONMENTAL RECORDS

A regulatory agency database search report was obtained from EDR, a third-party environmental database search firm. A complete copy of the database search report, including the date the report was prepared, the date the information was last updated, and the definition of databases searched, is provided in Appendix D.

Stantec evaluated the information listed within the database relative to potential impact to the Property, assessing the potential for impacts based in part on the physical setting. As part of this process, inferences have been made regarding the likely groundwater flow direction at or near the Property. The inferred groundwater flow direction is likely to be to northeast. Observations about the Property and surrounding properties made during the Property reconnaissance are provided in more detail in Section 5, Site Reconnaissance.

#### 4.2.1 Listings for Property

The Property was not identified in the environmental database report.

#### 4.2.2 Listings for Nearby Sites with Potential to Impact Property

Stantec assessed data presented in the environmental agency database search report to evaluate the potential for conditions on adjacent and nearby sites to pose a REC, CREC, or HREC for the Property. The evaluation included an opinion of the potential for contamination by hazardous substances or petroleum products to migrate to the Property from a nearby property, including by vapor migration or encroachment (i.e., potential for a vapor encroachment condition).



Records Review December 4, 2019

Stantec considers the listings in the database search report provided in Appendix C to not constitute a potential REC for the Property.

### 4.3 LOCAL/REGIONAL ENVIRONMENTAL RECORDS

Stantec checked the following sources to obtain information pertaining to Property use and/or indications of RECs in connection with the Property:

#### 4.3.1 Kern County Department of Environmental Health

| Agency Name<br>Contact Information  | Finding   |
|---|---|
| Kern County Department of Environmental<br>Health<br>1800 Mt. Vernon Avenue<br>Bakersfield, CA 93306<br>(661) 321-3000<br>September 5, 2019 | Stantec submitted a request to the Kern County Department of Environmental Health to research whether any documents were on file for the Property. At the time of this report, Stantec has not been notified by the department with any information pertaining to the Property. If files become available at a later date, Stantec would issue an addendum to this report with a summary of findings. However, based on its review of other sources, Stantec considers it unlikely that any records from this agency would alter the conclusions or recommendations of this report. |

### 4.3.2 Regional Water Quality Control Board (RWQCB)

| Agency Name<br>Contact Information           | Finding  |
|--|--|
| Regional Water Quality Control Board (RWQCB) | Stantec searched for available files for the Site and nearby properties on the RWQCB Geotracker website (https://geotracker.waterboards.ca.gov). |
| Lahontan RWQCB Region 6V                     | According to the Geotracker website, no documents associated with the Property or adjoining properties are available.                            |
| 15095 Amargosa Road, Bldg. 2,<br>Ste 210     |  |
| Victorville, CA 92394                        |  |
| Researched: September 5, 2019                |  |

### 4.3.3 Department of Toxic Substances Control (DTSC)

| Agency Name<br>Contact Information  | Finding   |
|---|---|
| Department of Toxic Substances Control (DTSC) 8800 Cal Center Drive Sacramento, CA 95826 Online database: | Stantec searched for available files for the Site and nearby properties on the Department of Toxic Substances Control's Envirostor website (https://geotracker.waterboards.ca.gov). According to the Envirostor website, no documents associated with the Site are available. |
| https://www.envirostor.dtsc.ca.gov/<br>researched September 5, 2019                                       |   |



Records Review December 4, 2019

### 4.3.4 California City Building Department

| Agency Name, Contact Information  | Findings  |
|---|---|
| California City Building Department<br>21000 Hacienda Blvd.<br>California City, CA 93505<br>(760) 373-7140<br>September 5, 2019 | Stantec contacted the California City Building Department to research whether any documents were on file for the Property. At the time of this report, Stantec has not been notified by the department with any information pertaining to the Property. If files become available at a later date, Stantec would issue an addendum to this report with a summary of findings. However, based on its review of other sources, Stantec considers it unlikely that any records from this agency would alter the conclusions or recommendations of this report. |

### 4.3.5 California Division of Oil, Gas, and Geothermal Resources (DOGGR)

| Agency Name, Contact Information   | Findings   |
|--|--|
| DOGGR<br>4800 Stockdale Hwy., Suite 100<br>Bakersfield, CA 93309-0279<br>(661) 322-4031<br>September 9, 2019 | Stantec reviewed DOGGR's Well Finder online database to review potential oil wells at the Property or in the vicinity. According to the well finder, and as confirmed by measurements provided in the records, there are two oil wells at the Property, as discussed below.  |
|  | Lease by National Security Oil Co. "1" (API: 0402932491) is listed on the DOGGR Well Finder as a plugged dry hole. The well record available through the Well Finder database contains only two pages of information from the early 1920s—one that indicates its location and proposed operations, and the other is a letter indicating that the well was drilled to 111 feet. The location reported in the record is not clearly written but appears to indicate that it is 1,020 feet (or potentially 1,520 feet) east and 200 feet south of the northwest corner of Section 11, Township S2S, RS7E in Kern County. Either of the two probable locations specified in the record indicates that the well is in the northern portion of APN: 302-32-101, as shown on Figure 2.  |
|  | Childs-Wall "1" (API: 0402932490) is listed on the DOGGR Well Finder as a plugged dry hole. The well record indicates that the well was drilled in1945 to a depth of 2,232 feet. The record from 1946/1947 indicates that there is no casing in the hole and that it is a square wood conductor box that was cemented in place. The well was "closed" with a board nailed to the conductor box so the property owner could potentially convert it to a water well at a later date. According to the locational information provided in the well record, this well is located in the northwest portion of APN: 302-020-14. This location conflicts slightly with the DOGGR online map, which plots it near the adjoining boundary between APN: 302-020-15 and APN: 302-020-18. However, plotted well locations on the Well Finder have been acknowledged by DOGGR to occasionally be incorrect and that it is more reliable to use the well location specified in the original well record. |
|  | Based on a review of available well records, the wells do not have any casing and therefore would not be able to be located using geophysical survey methods. Given the proposed use of the Property as a solar farm, the wells are considered unlikely to represent an environmental concern. However, if these wells are encountered during Property redevelopment, Stantec recommends that work be  |



Records Review December 4, 2019

| Agency Name, Contact Information | Findings  |
|----------------------------------|---|
|                                  | stopped in the area and DOGGR be contacted for evaluation and determination as to any further requirements. |

#### 4.4 HISTORICAL RECORDS REVIEW

#### 4.4.1 Land Title Records/Deeds

Land title records, deeds, environmental liens, and activity and use limitation documentation was not provided by the User, and public records were not searched by Stantec.

#### 4.4.2 Aerial Photographs

Stantec reviewed historical aerial photographs provided by EDR. Copies of the aerial photographs are included in Appendix D. The general type of activity on a property and land use changes can often be discerned from the type and layout of structures visible in the photographs. However, specific elements of a facility's operation usually cannot be discerned from aerial photographs alone. The following table summarizes Stantec's observations of the reviewed historical aerial photographs.

| Year      | Observations, Property and Adjoining Properties   |  |
|-----------|---|--|
| 1952      | The Property is undeveloped desert land with native vegetation consisting predominantly of low-lying shrubs. There are a few spots on the Property where there are small circular areas (~5,000 square feet) that are void of vegetation. However, there is no indication of activities in these areas. Natural drainages trend southwest-northeast across the Property and surrounding properties. |  |
| 1972      | The Property and surrounding area appear the same as the previous photograph except that farming operations are visible offsite on a parcel to the northeast of the intersection of Yucaipa Street and Phillips Road.   |  |
| 1977      | The Property and surrounding area appear similar to the previous photographs.   |  |
| 1985-1986 | The Property and surrounding area appear similar to the previous photographs except that an approximate 2,200-square-foot dark surface feature appears in the northwest corner of APN: 302-34-201. As indicated below, this feature is not present in any of the other aerial photographs.  |  |
| 1994      | The Property and surrounding area appear similar to the previous photographs.   |  |
| 2005      | The Property and surrounding area appear similar to the previous photographs.   |  |
| 2009      | The Property and surrounding area appear similar to the previous photographs.   |  |
| 2012      | The Property and surrounding area appear similar to the previous photographs.   |  |
| 2016      | The Property and surrounding area appear similar to the previous photographs.   |  |

Former agricultural use was not identified at the Property. Additionally, no commercial use or other developed use was identified at the Property that would be considered an environmental concern.



4.5

Records Review December 4, 2019

#### 4.4.3 Historical Fire Insurance Maps

Fire insurance maps were developed for use by insurance companies to depict facilities, properties, and their uses for many locations throughout the United States. These maps provide information on the history of prior land use and are useful in assessing whether there may be potential environmental contamination on or near the Property. These maps, which have been periodically updated since the late 19th century, often provide valuable insight into historical Property uses.

Stantec requested fire insurance maps from EDR; however, no coverage exists for the Property. The Sanborn® Map Search Report indicating "no coverage" is presented in Appendix D.

### 4.4.4 Historical Topographic Maps

Stantec reviewed historical USGS 7.5-minute topographic maps of the Mojave NE, California City North, Cinco, Cantil, Castle Butte, Salt Dale, and Cross Mountain Quadrangles to help identify past Property usage and areas of potential environmental concern.

No RECs were noted during our review of the topographic maps. Copies of the historical maps are provided in Appendix D. The following table summarizes the maps reviewed and our observations.

| Year | Scale     | Observations, Property and Adjoining Properties   |
|------|-----------|---|
| 1915 | 1:125,000 | Only the southwest portion of the Property was available. A portion of the Southern Pacific Railroad passes through the western portion of the Property. There are no other improvements within the Property boundaries.  |
| 1943 | 1:63,500  | All of the Property is illustrated on this map, but there are no structures on the Property. Only dirt roads are depicted, and an area in the western portion of the Property is labeled as Neuralia.   |
| 1947 | 1:50,000  | The Property and surrounding area appear similar to the previous map.   |
| 1956 | 1:62,500  | The Property and surrounding area appear similar to the previous map except that several "wells" and a "water tank" are depicted. Only one of the wells is within the Property boundary along a proposed gen-tie line in the eastern portion of the Property. The remaining wells and water tank are offsite. |
| 1973 | 1:24,000  | The Property and surrounding area appear similar to the previous map.   |
| 1980 | 1:24,000  | This map shows the west half of the Property. The Property and surrounding area appear similar to the previous map.   |
| 1994 | 1:24,000  | This map shows the west ¾ of the Property. The Property and surrounding area appear similar to the previous map.  |
| 2012 | 1:24,000  | The entire Property is shown and appears the same as the previous map.  |

#### 4.4.5 Other Historical Sources

Stantec Consulting Services, Inc (Stantec), 2017. Phase I Environmental Site Assessment, Eland 1 Solar Farm, Unincorporated Area of Kern County, California, November 14.



4.6

Records Review December 4, 2019

This report is a Phase 1 ESA that was prepared for the Eland 1 Solar Farm proposed in the surrounding area. The Phase 1 concluded that potential impacts from total petroleum hydrocarbons, metals, and pesticides may be present in soils from aboveground fuel tanks and agricultural activities. The Property is not adjacent to areas of this parcel where the tanks and former agricultural uses were noted and are therefore not considered an environmental concern.



Site Reconnaissance December 4, 2019

#### 5.0 SITE RECONNAISSANCE

A visit to the Property and its vicinity was Mr. Nicholas Drachenberg, Stantec Environmental Scientist, and Ms. Sarah Toback, Stantec Staff Biologist, on August 12, 2019. Mr. Drachenberg and Ms. Toback were unaccompanied during the Property visit. Access to the Property was coordinated through the User. Figure 2 provides information about the Property and adjoining properties and the location of potential areas of environmental concern. Photographs collected during the Property visit are included in Appendix A.

#### 5.1 SITE RECONNAISSANCE METHODOLOGY

The site reconnaissance focused on observation of current conditions and observable indications of past uses and conditions of the Property that may indicate the presence of RECs. The reconnaissance of the Property was conducted on foot, and Stantec used the following methodology to observe the Property:

- Traverse the outer Property boundary.
- Traverse transects across the Property.

Weather conditions during the visit to the Property were clear and sunny. There were no weather-related Property access restrictions encountered during the site reconnaissance visit.

### 5.2 GENERAL DESCRIPTION

| Property and Area Description:                                | The Property is located in portions of unincorporated Kern County and California City, north of the California City Municipal Airport. It consists of 72 parcels totaling 1,965.95 acres of predominantly vacant and undeveloped land in unincorporated Kern County and California City. The User has proposed the construction and operation of an up to 500 MW-AC utility-scale solar farm with energy storage, known as the Kudu Solar Farm.  The Property is adjacent to the proposed/approved Eland 1 Solar Farm, south of the existing Springbok 1 & 2 Solar Farms and southeast of the LADWP Beacon Solar facility. |
|---|--|
| Property Operations.  | Most of the Property is currently vacant and undeveloped. However, the northeast corner of APN: 469-17-010 overlaps with a portion of the neighboring residential property to the east/northeast.  |
| Structures, Roads, Other Improvements:                        | There are no structures or improvements at the Property other than dirt or asphalt paved roads.  |
| Property Size (acres):  | 1,965.95 acres   |
| Estimated % of Property Covered by Buildings and/or Pavement: | <1%  |
| Observed Current Property Use/Operations:                     | Vacant, desert land  |
| Observed Evidence of Past Property Use(s):                    | Vacant, desert land  |



5.1

Site Reconnaissance December 4, 2019

| Sewage Disposal Method (and age): | Unknown/undeveloped |
|-----------------------------------|---------------------|
| Potable Water Source:             | Unknown/undeveloped |
| Electric Utility:                 | Unknown/undeveloped |

### 5.3 HAZARDOUS SUBSTANCES AND PETROLEUM PRODUCTS

The following table summarizes Stantec's observations during the Property reconnaissance.

| Observations   | Description/Location  |
|--|---|
| Hazardous Substances and Petroleum Products as Defined by CERCLA 42 U.S.C. § 9601(14): | None observed   |
| Drums (≥ 5 gallons):   | None observed   |
| Strong, Pungent, or Noxious Odors:   | None observed   |
| Pools of Liquid:   | None observed   |
| Unidentified Substance Containers:   | None observed   |
| Polychlorinated Biphenyl-Containing Equipment:   | None observed   |
| Other Observed Evidence of Hazardous Substances or Petroleum Products:                 | Four discarded cans of paint were observed in the western portion of APN:302-34-219 that ranged from 1 to 5 gallons. No staining or evidence of a release was observed on the surrounding soil. |

#### 5.4 INTERIOR OBSERVATIONS

The Property is undeveloped with no interior areas to inspect.

#### 5.5 EXTERIOR OBSERVATIONS

Stantec made the following observations during the site reconnaissance of exterior areas of the Property and/or identified the following information during the interview or records review portions of the assessment:

| Observations                              | Description   |
|---|---|
| On-site Pits, Ponds, or Lagoons:          | None observed   |
| Stained Soil or Pavement:                 | None observed   |
| Stressed Vegetation:                      | None observed   |
| Waste Streams and Waste Collection Areas: | None observed   |
| Solid Waste Disposal:                     | None observed other than discarded wood and occasional trash.   |
| Potential Areas of Fill Placement:        | No mounds, piles, or depressions suggesting the placement of fill material were observed on the Property. |



Site Reconnaissance December 4, 2019

| Observations                 | Description   |  |
|------------------------------|---|--|
| Wastewater:                  | No exterior wastewater discharge was observed.  |  |
| Stormwater:                  | There are no engineered stormwater structures or channels. Stormwater would follow overland following the topographic gradient the northeast.   |  |
| Wells:                       | Suspect water wells were observed during the field reconnaissance near the Property boundaries. Stantec recommends that all known and unknown (those encountered during proposed development activities) irrigation/water wells be abandoned in accordance with applicable regulations unless the wells would be used by the Project. |  |
| Septic Systems:              | No visible evidence of the existence of a septic system was observed.   |  |
| Other Exterior Observations: | None  |  |

### 5.6 UNDERGROUND STORAGE TANKS/STRUCTURES

| Existing<br>Underground<br>Storage Tanks<br>(USTs): | No visible evidence (fill pipes, vent pipes, dispensers, surface patches), which would indicate the presence of USTs, was discovered during the site reconnaissance.         |
|---|--|
| Former USTs:  | No visible evidence (fill pipes, vent pipes, dispensers, surface patches), reports, or other evidence of the former presence of USTs was discovered during this Phase I ESA. |
| Other<br>Underground<br>Structures:                 | None observed  |

#### 5.7 ABOVEGROUND STORAGE TANKS

| Existing<br>Aboveground<br>Storage Tanks<br>(ASTs): | No visible evidence (fill pipes, vent pipes, dispensers, surface stains), which would indicate the presence of ASTs, was discovered during the site reconnaissance.         |
|---|---|
| Former ASTs:  | No visible evidence (fill pipes, vent pipes, dispensers, surface stains), reports, or other evidence of the former presence of ASTs was discovered during this Phase I ESA. |

#### 5.8 ADJOINING PROPERTIES

#### 5.8.1 Current Uses of Adjoining Properties

As viewed from the Property and/or from public rights-of-way, adjoining properties mostly consist of undeveloped land. However, a railroad easement crosses through the Property, but a buffer of undeveloped land that is approximately 75 feet or more is present between the boundary and the railroad tracks. The one exception to this is in areas where the proposed gen-tie lines would cross the railroad tracks. Given the distance from the Property boundary to the railroad tracks, no further assessment is recommended. However, if subsurface work is proposed for the installation of gen-tie lines or poles in areas that are within 20 feet of the railroad tracks, Stantec would



Site Reconnaissance December 4, 2019

recommend evaluation of soil samples to determine whether metals concentrations in soil are above California hazardous waste levels or regulatory thresholds that may pose a risk to future onsite construction workers.

The California City Municipal Airport is located adjacent to the south of the Property. Residential properties are located adjacent to some of the proposed gen-tie line locations. A residential property is adjacent to APN 469-17-010 in the northeast portion of the Property. The rear yard of this residential property overlaps the northeast corner of Property parcel but appears to only be used for equipment storage.

#### 5.8.2 Observed Evidence of Past Uses of Adjoining Properties

Observations of adjoining properties providing indications of past use and activities, if any, are described below.

| NORTH | None observed   |
|-------|---|
| EAST  | None observed   |
| SOUTH | None observed   |
| WEST  | The properties appear predominantly undeveloped except for remnant row crops to the west of the southernmost Property parcel. |

#### 5.8.3 Pits, Ponds or Lagoons on Adjoining Properties

As viewed from the Property and/or from public rights-of-way, Stantec made the following observations about the presence of pits, ponds, and lagoons on adjoining properties:

| NORTH | None observed |
|-------|---------------|
| EAST  | None observed |
| SOUTH | None observed |
| WEST  | None observed |

#### 5.9 OBSERVED PHYSICAL SETTING

| Topography of the Property | Property topography slopes to the northeast at elevations ranging from |
|----------------------------|--|
| and Surrounding Area:      | approximately 2,440 feet amsl to approximately 2,280 feet amsl         |

**(** 

5.4

Interviews December 4, 2019

### 6.0 INTERVIEWS

The AAI final rule requires that a site interview be conducted with the property owner or site occupant that is most familiar with the site. The landowner representatives of the parcels associated with the Property were not available for interview. However, given that the Property consists of undeveloped vacant land, the lack of an interview is not considered a significant data gap.



Evaluation December 4, 2019

### 7.0 EVALUATION

This section provides a summary overview of or findings, opinions, and conclusions.

#### 7.1 FINDINGS AND OPINIONS

Information gathered from reviews of existing data and a property inspection was evaluated to determine if RECs are present in connection with the Property. Based on this information, Stantec made the following findings and developed the following opinions.

- Suspect water wells were observed during the field reconnaissance near the Property boundaries.
  - Stantec recommends that all known and unknown (those encountered during proposed development activities) irrigation/water wells be abandoned in accordance with applicable regulations unless the wells would be used by the Project.
- Four discarded cans of paint were observed in the western portion of APN:302-34-219 that ranged from 1 to 5 gallons. No staining or evidence of a release was observed on the surrounding soil.
- An environmental records search was performed and identified sites within their respective ASTM E 1527-13 search radii of the Property that may represent RECs, HRECs, or *de minimis* conditions.
  - Based on distance from the Property, position of sites with respect to assumed groundwater flow direction, the native soils, and/or regulatory status, none of the sites identified in the in the environmental records search report are expected to affect soil or groundwater quality at the Property. The environmental records search identified no RECs, HRECs or *de minimis* conditions at or near the Property.
- A railroad easement crosses through the Property, but a buffer of undeveloped land that is approximately 75 feet
  or more is present between the boundary and the railroad tracks. The one exception to this is in areas where the
  proposed gen-tie lines will cross the railroad tracks.
  - Given the distance from the Property boundary to the railroad tracks, no further assessment is recommended. However, if subsurface work is proposed for the installation of gen-tie lines or poles in areas that are within 20 feet of the railroad tracks, Stantec would recommend evaluation of soil samples to determine whether metals concentrations in soil are above California hazardous waste levels or regulatory thresholds that may pose a risk to future onsite construction workers.
- Stantec reviewed DOGGR's Well Finder online database to review potential oil wells at the Property or in the
  vicinity. According to the well finder, and as confirmed by measurements provided in the records, there are two
  oil wells at the Property.
  - Based on Stantec's review of the records, the wells do not have any casing, and one of the wells reportedly consists of a square wood conductor box that was cemented in place. Given the lack of casing in these wells, they would not be able to be located using geophysical survey methods. Due to the proposed use of the Property



Evaluation December 4, 2019

as a solar farm, the wells are considered unlikely to represent an environmental concern since access could be made to the well locations of record in the future since the solar panels would not be permanent structures. However, if these wells are encountered during Property redevelopment, Stantec recommends that work be stopped in the area and DOGGR be contacted for evaluation and determination regarding any further requirements.

#### 7.2 DATA GAPS

The federal AAI final rule [40 CFR 312.10(a)] and ASTM E1527-13 identify a "data gap" as the lack or inability to obtain information required by the standards and practices of the rule despite good faith efforts by the EP or the User.

Any data gaps resulting from the Phase I ESA described in this report are listed and discussed below.

| Gap   | Discussion   |  |
|---|--|--|
| Deletions or Exceptions from<br>Scope of Work Referenced in<br>Section 1.4: | None   |  |
| Weather-Related Restrictions to Site Reconnaissance:                        | None   |  |
| Facility Access Restrictions to Site Reconnaissance:                        | It was not within our scope to walk the entire Property. Stantec drove through the Property and observed the vicinity from high elevations, where possible.  |  |
| Other Site Reconnaissance Restrictions:                                     | None   |  |
| Data Gaps from Environmental Records Review:                                | None   |  |
| Data Gaps from Historical Records Review:                                   | None   |  |
| Data Gaps from Interviews:  | The landowner representatives of the parcels associated with the Property were not available for interview. However, given that the Property consists of undeveloped vacant land, the lack of an interview is not considered a significant data gap. |  |
| Other Data Gaps:  | A completed user questionnaire was not provided. Given the historical documents available for the Property, the lack of a completed user questionnaire is not considered a significant data gap.   |  |

#### 7.3 CONCLUSIONS

We have performed a Phase I ESA in conformance with the scope and limitations of ASTM Practice E1527 for the Property. Any exceptions to or deletions from this practice are described in Section 7.2, Data Gaps. This assessment has revealed no evidence of RECs in connection with the Property. No further investigation appears to be warranted at this time.

However, the following items of note were identified during this ESA:



Evaluation December 4, 2019

• Oil Wells. Based on Stantec's review of DOGGR's Well Finder online database and as confirmed by measurements provided in the individual well records, there are two oil wells on the Property. The wells are identified as National Security Oil Co. "1" (API: 0402932491) and Childs-Wall "1" (API: 0402932490). According to the records, National Security Oil Co. "1" was drilled in the early 1920s to 111 feet bgs and deemed a dry hole. The handwritten location in the record is not clearly written so there are two potential locations for the well, but both would fall in the northern portion of APN: 302-32-101, as shown on Figure 2.

The Childs-Wall "1" well was drilled in 1945 to a depth of 2,232 feet bgs and found to be a dry hole. The records indicate that there is no casing in the hole and that it is a square wood conductor box that was cemented in place. The well was "closed" with a board nailed to the conductor box so the property owner could potentially convert it to a water well at a later date. According to the locational information provided in the well record, this well is located in the northwest portion of APN: 302-020-14.

Based on a review of available well records, the wells do not have any casing and therefore would not be able to be located using geophysical survey methods. Given that the wells were determined to by "dry holes" and because of the proposed use of the Property as a solar farm, the wells are not considered a REC, but it should be noted that they may be encountered during development. If these wells are encountered during grading/development, Stantec recommends that work be stopped in the area and DOGGR be contacted for evaluation and determination for any further requirements.

Adjacent Railroad Easement. A railroad easement crosses through the Property, but a buffer of undeveloped
land that is approximately 75 feet or more is present between the boundary and the railroad tracks. The one
exception to this is in areas where the proposed gen-tie lines would cross the railroad tracks.

Given the distance from the Property boundary to the railroad tracks, no further assessment is recommended. However, if subsurface work is proposed for the installation of gen-tie lines or poles in areas that are within 20 feet of the railroad tracks, Stantec recommends the evaluation of soil samples to determine whether metals concentrations in soil are above California hazardous waste levels or regulatory thresholds that may pose a risk to future onsite construction workers.

Potential Water Wells. Suspect water wells were observed during the field reconnaissance near the Property
boundaries. Stantec recommends that all known and unknown (those encountered during proposed development
activities) water wells be abandoned in accordance with applicable regulations unless the wells will be used by
the Project.



Non-Scope Considerations December 4, 2019

#### 8.0 NON-SCOPE CONSIDERATIONS

The following ASTM E1527-13 non-scope services were performed as part of this Phase I ESA:

#### 8.1 LEAD-BASED PAINT

Concern for lead-based paint (LBP) is primarily related to residential structures. The EPA's Final Rule on Disclosure of Lead-Based Paint in Housing (40 CFR Part 745) defines LBP as paint or other surface coatings that contain lead equal to or in excess of 1.0 milligram per square centimeter or 0.5 percent by weight.

The risk of lead toxicity in LBP varies based upon the condition of the paint and the year of its application. The U.S. Department of Housing and Urban Development has identified the following risk factors:

- The age of the dwelling as follows: maximum risk is from paint applied before 1950.
- There is severe risk from paint applied before 1960.
- There is moderate risk from deteriorated paint applied before 1970.
- There is slight risk from the paint that is intact but applied before 1977.
- The condition of the painted surfaces.
- The presence of children and certain types of households in the building.
- Previously reported cases of lead poisoning in the building or area.

Given that there are no structures on the Property, LBP is not considered an environmental concern to the Property.

#### 8.2 ASBESTOS

Asbestos can be found in many applications, including sprayed-on or blanket-type insulation, pipe wraps, mastics, floor and ceiling tiles, wallboard, mortar, roofing materials, and a variety of other materials commonly used in construction. The greatest asbestos-related human health risks are associated with friable asbestos, which is an asbestos-containing material (ACM) that can be reduced to powder by hand pressure. Friable asbestos can become airborne and inhaled, which has been associated with specific types of respiratory disease. The manufacturing and use of asbestos in most building products was curtailed during the late 1970s.

Stantec makes no warranty as to the possible existence or absence of inaccessible materials or to their evaluation with respect to asbestos content. Samples of suspect ACM should be collected for laboratory analysis of asbestos prior to any renovation or building demolition to be compliant with, EPA National Emission Standard for Hazardous Air Pollutants regulations.

Given that there are no structures on the Property, ACMs are not considered an environmental concern to the Property.

#### 8.3 RADON

Radon is a colorless, tasteless radioactive gas with an EPA-specified action level of 4.0 PicoCuries per liter of air (pCi/L) for residential properties. Radon gas has a very short half-life of 3.8 days. The health risk potential of radon is



Non-Scope Considerations December 4, 2019

primarily associated with its rate of accumulation within confined areas near or in the ground, such as basements, where vapors can readily transfer to indoor air from the ground through foundation cracks or other pathways. Large, adequately ventilated rooms generally present limited risk for radon exposure. The radon concentrations in buildings and homes depend on many factors, including soil types, temperature, barometric pressure, and building construction (EPA 2019).

Stantec reviewed regional data published by the EPA on average indoor radon concentrations in the vicinity of the Property (http://www.epa.gov/radon/zonemap.html).

| EPA Radon Zones (w/Average Measured Indoor Radon concentrations) |                                     |                            |  |
|--|-------------------------------------|----------------------------|--|
| Zone 1 – High<br>(>4.0 pCi/L)                                    | Zone 2 – Moderate<br>(2 to 4 pCi/L) | Zone 3 – Low<br>(<2 pCi/L) |  |
|  | X                                   |                            |  |

The Property is located in Zone 2 and is considered to have medium potential for radon. To determine Property-specific radon levels, a radon survey would have to be conducted. The EDR report indicates that one site tested in zip code 93505 was 0.200 pCi/L. Therefore, further investigation of indoor radon issues is not warranted.



References December 4, 2019

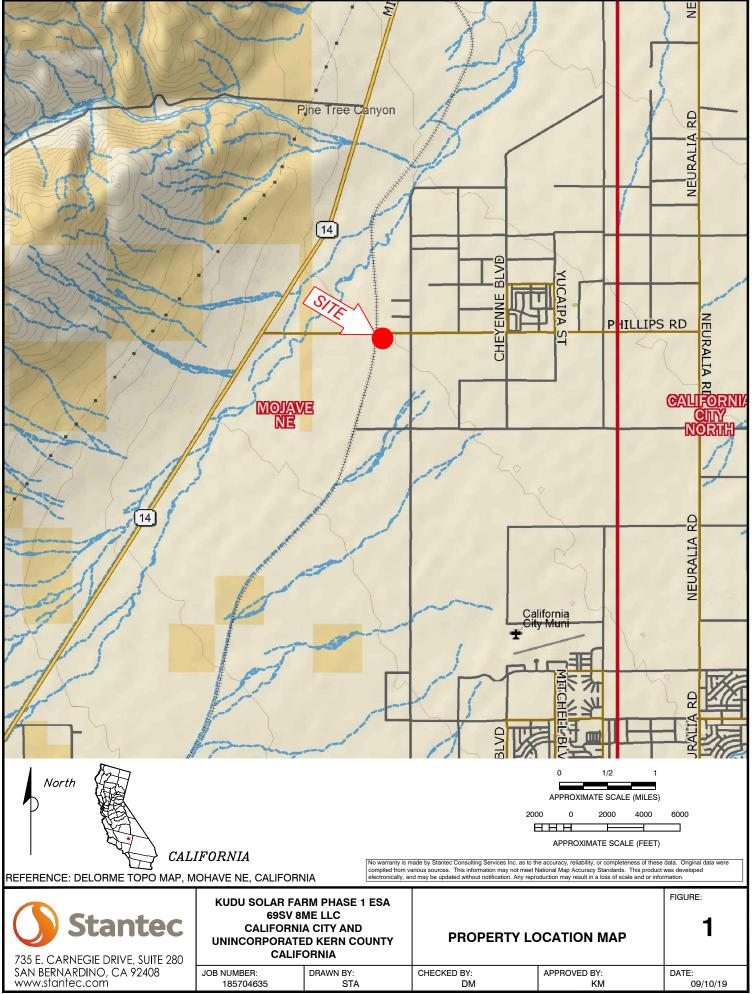
#### 9.0 REFERENCES

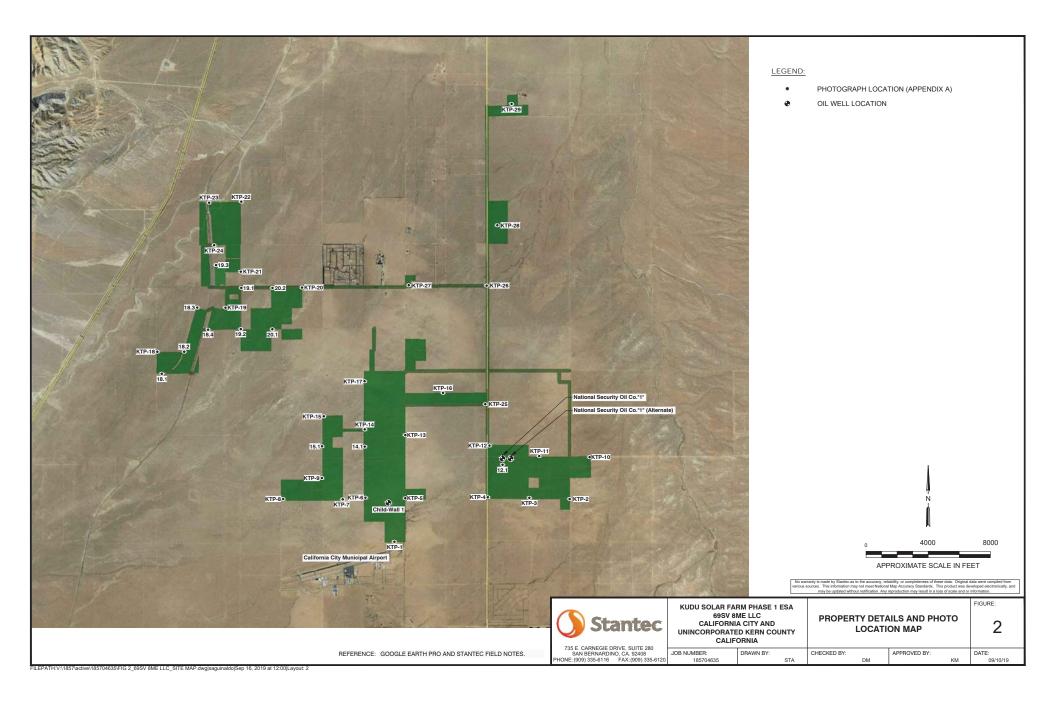
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  - https://water.ca.gov/LegacyFiles/pubs/groundwater/bulletin\_118/california's\_groundwater\_\_bulletin\_118\_-\_update\_2003\_/bulletin118\_9-sl.pdf > Last updated February 24, 2002. Accessed September 5, 2019.
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# **FIGURES**







# **APPENDICES**



Appendix A Photographs of the Property and Vicinity December 4, 2019

Appendix A Photographs of the Property and Vicinity







Client: 8minutenergy Project: Phase I ESA
Site Name: Kudu Site Location: California City, CA

Photograph ID: 1

**Photo Location:** 

KTP-1

**Direction:** North

**Survey Date:** 8/21/2019

**Comments:** Property area



Photograph ID: 2

**Photo Location:** 

KTP-1

Direction:

West

Survey Date:

8/21/2019

Comments:





Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA

Photograph ID: 3

**Photo Location:** 

KTP-1

**Direction:** 

East

**Survey Date:** 8/21/2019

Comments:

Property area



Photograph ID: 4

**Photo Location:** 

KTP-1

Direction:

South

**Survey Date:** 8/21/2019

Comments:

Possible well





Client: 8minutenergy Project: Phase I ESA
Site Name: Kudu Site Location: California City, CA

**Photograph ID:** 5

Photo Location:

KTP-1

**Direction:** North

**Survey Date:** 8/21/2019

Comments: Possible well



Photograph ID: 6

**Photo Location:** 

KTP-1

Direction:

West

Survey Date:

8/21/2019

Comments:

Abandoned structures





Client: 8minutenergy Project: Phase I ESA Site Name: Kudu Site Location: California City, CA Photograph ID: 7 **Photo Location:** KTP-2 Direction: South **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 8 **Photo Location:** KTP-2 Direction: West Survey Date: 8/21/2019 Comments: Property area





Client: 8minutenergy Project: Phase I ESA
Site Name: Kudu Site Location: California City, CA

Photograph ID: 9

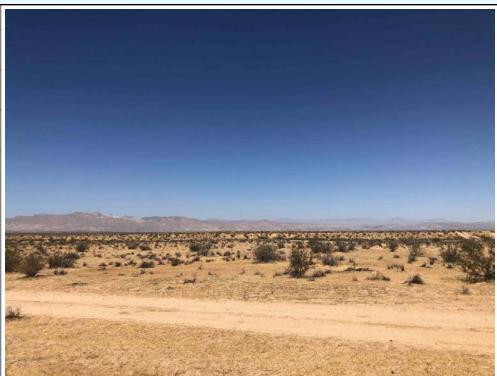
**Photo Location:** 

KTP-2

**Direction:** North

**Survey Date:** 8/21/2019

**Comments:** Property area



Photograph ID: 10

**Photo Location:** 

KTP-3

Direction:

East

**Survey Date:** 8/21/2019

Comments:







Client: 8minutenergy Project: Phase I ESA
Site Name: Kudu Site Location: California City, CA

Photograph ID: 11

**Photo Location:** 

KTP-3

**Direction:** South

**Survey Date:** 8/21/2019

**Comments:** Property area



Photograph ID: 12

**Photo Location:** 

KTP-3

Direction:

West

Survey Date:

8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy

Site Name: Kudu Site Location: California City, CA

Photograph ID: 13

**Photo Location:** 

KTP-3

Direction: North

**Survey Date:** 8/21/2019

Comments:

Property area



Photograph ID: 14

**Photo Location:** 

KTP-4

Direction:

North

Survey Date:

8/21/2019

Comments:

Property area - Neuralia Blvd. pictured







Client: 8minutenergy Project: Phase I ESA Site Name: Kudu Site Location: California City, CA

Photograph ID: 15

**Photo Location:** 

KTP-4

Direction:

East

**Survey Date:** 8/21/2019

Comments: Property area



Photograph ID: 16

**Photo Location:** 

KTP-4

Direction:

South

**Survey Date:** 8/21/2019

Comments:







Client: 8minutenergy Project: Phase I ESA

Site Name: Kudu Site Location: California City, CA

Photograph ID: 17

**Photo Location:** 

KTP-5

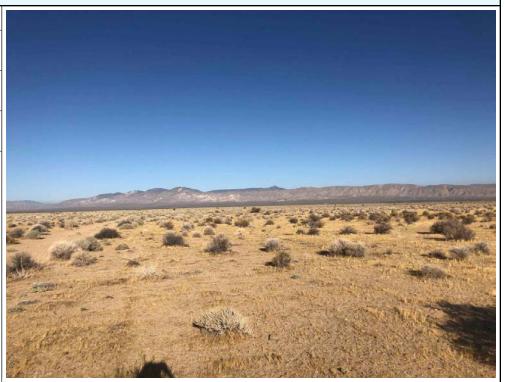
Direction:

West

**Survey Date:** 8/21/2019

Comments:

Property area



Photograph ID: 18

**Photo Location:** 

KTP-5

Direction:

North

Survey Date:

8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy

Site Name: Kudu Site Location: California City, CA

Photograph ID: 19

**Photo Location:** 

KTP-5

Direction:

East

**Survey Date:** 8/21/2019

Comments: Property area



Photograph ID: 20

**Photo Location:** 

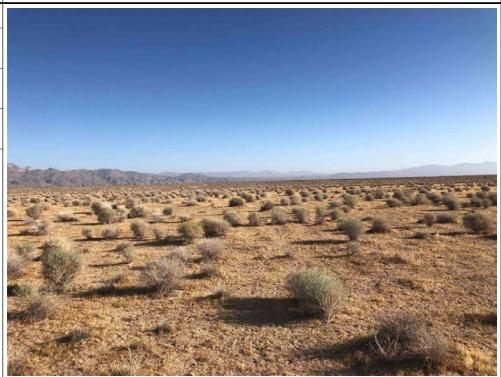
KTP-6

Direction:

North

**Survey Date:** 8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 21 **Photo Location:** KTP-6 Direction: East **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 22 **Photo Location:** KTP-6 Direction: South Survey Date: 8/21/2019 Comments: Property area





Phase I ESA Client: 8minutenergy Project: Site Name: Kudu Site Location: California City, CA

Photograph ID: 23

**Photo Location:** 

KTP-6

Direction:

West

**Survey Date:** 8/21/2019

Comments: Property area



Photograph ID: 24

**Photo Location:** 

KTP-7

Direction:

North

Survey Date:

8/21/2019

Comments:







Client: 8minutenergy Project: Phase I ESA

Site Name: Kudu Site Location: California City, CA

Photograph ID: 25

**Photo Location:** 

KTP-7

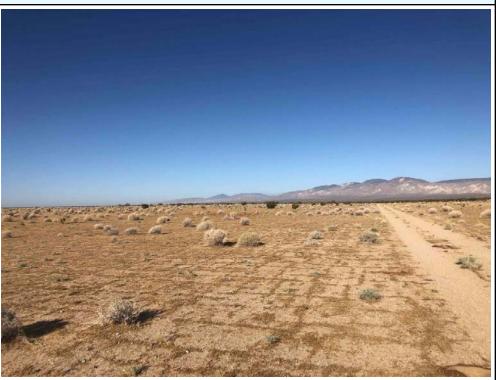
Direction:

West

**Survey Date:** 

8/21/2019

**Comments:** Property area



Photograph ID: 26

**Photo Location:** 

KTP-8

Direction:

North

**Survey Date:** 

8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 27 **Photo Location:** KTP-8 Direction: East **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 28 **Photo Location:** 

KTP-9

Direction: North

**Survey Date:** 8/21/2019

Comments: Property area







Photograph ID: 29

**Photo Location:** 

KTP-9

Direction:

East

**Survey Date:** 8/21/2019

0/21/2019

**Comments:** Property area



Photograph ID: 30

**Photo Location:** 

KTP-9

Direction:

South

**Survey Date:** 

8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 31 **Photo Location:** KTP-10 Direction: South **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 32 **Photo Location:** KTP-10 Direction: West **Survey Date:** 8/21/2019 Comments: Property area





Client: 8minutenergy Project: Phase I ESA Site Name: Kudu Site Location: California City, CA Photograph ID: 33 **Photo Location:** KTP-11 Direction: South **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 34 **Photo Location:** KTP-11 Direction: West **Survey Date:** 8/21/2019 Comments: Property area





Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 35 **Photo Location:** KTP-12 Direction: East **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 36 **Photo Location:** KTP-12 Direction: South **Survey Date:** 8/21/2019 Comments: Property area





Phase I ESA Client: 8minutenergy Project:

Site Name: Kudu Site Location: California City, CA

Photograph ID: 37

**Photo Location:** 

KTP-12.1

Direction:

East

**Survey Date:** 8/21/2019

Comments:

Paint cans



Photograph ID: 38

**Photo Location:** 

KTP-13

Direction:

North

**Survey Date:** 8/21/2019

Comments:







Photograph ID: 39

**Photo Location:** 

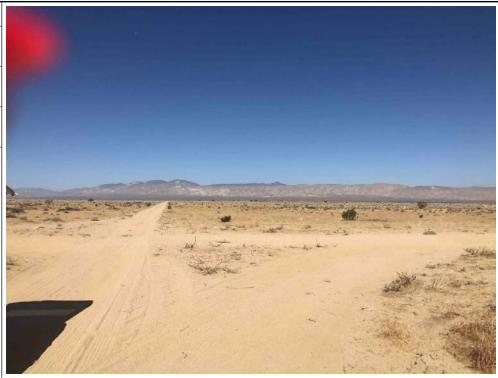
KTP-13

Direction:

West

**Survey Date:** 8/21/2019

**Comments:** Property area



Photograph ID: 40

**Photo Location:** 

KTP-13

Direction:

South

Survey Date:

8/21/2019

Comments:







Client: 8minutenergy Project: Phase I ESA

Site Name: Kudu Site Location: California City, CA

Photograph ID: 41

**Photo Location:** 

KTP-13

Direction:

East

**Survey Date:** 8/21/2019

Comments:

Property area



Photograph ID: 42

**Photo Location:** 

KTP-14

Direction:

North

**Survey Date:** 8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 43 **Photo Location:** KTP-14 Direction: East **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 44 **Photo Location:** KTP-14 Direction: South **Survey Date:** 8/21/2019 Comments: Property area





Photograph ID: 45

**Photo Location:** 

KTP-14.1

Direction:

West

**Survey Date:** 8/21/2019

Comments:

Possible abandoned water

well



Photograph ID: 46

**Photo Location:** 

KTP-15

Direction:

East

Survey Date:

8/21/2019

Comments:





Client: Project: Phase I ESA 8minutenergy

Site Name: Kudu Site Location: California City, CA

Photograph ID: 47

**Photo Location:** 

KTP-15

Direction:

South

**Survey Date:** 8/21/2019

Comments:

Property area



Photograph ID: 48

**Photo Location:** 

KTP-15.1

Direction:

North

**Survey Date:** 

8/21/2019

Comments:

Abandoned containers bucket and paint cans







Client: Project: Phase I ESA 8minutenergy

Site Name: Kudu Site Location: California City, CA

Photograph ID: 49

**Photo Location:** 

KTP-15.1

Direction:

North

**Survey Date:** 8/21/2019

Comments:

Abandoned containers bucket and paint cans



Photograph ID: 50

**Photo Location:** 

KTP-16

Direction:

South

**Survey Date:** 

8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 51 **Photo Location:** KTP-16 Direction: West **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 52 **Photo Location:** 

Photo Location:
KTP-16

Direction:
North

Survey Date:
8/21/2019

Comments:
Property area



Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 53 **Photo Location:** KTP-17 Direction: East **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 54 **Photo Location:** KTP-17 Direction: South **Survey Date:** 8/21/2019 Comments: Property area





Photograph ID: 55

**Photo Location:** 

KTP-17

Direction:

West

**Survey Date:** 

8/21/2019

Comments:

Property area



Photograph ID: 56

**Photo Location:** 

KTP-18

Direction:

South

**Survey Date:** 

8/21/2019

Comments:







Client: 8minutenergy Project: Phase I ESA Site Name: Kudu Site Location: California City, CA Photograph ID: 57 **Photo Location:** KTP-18 Direction: East **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 58 **Photo Location:** KTP-18 Direction: North Survey Date: 8/21/2019 Comments: Property area





Photograph ID: 59

Photo Location: KTP-18.1

Direction:

East

**Survey Date:** 8/21/2019

**Comments:** Property area



Photograph ID: 60

**Photo Location:** 

KTP-18.1

Direction:

North

**Survey Date:** 8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA

Photograph ID: 61

**Photo Location:** 

KTP-18.1

Direction:

West

**Survey Date:** 8/21/2019

Comments: Property area



Photograph ID: 62

**Photo Location:** 

KTP-18.2

Direction:

East

**Survey Date:** 

8/21/2019

Comments:





Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 63 **Photo Location:** KTP-18.2 Direction: South **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 64 **Photo Location:** KTP-18.2 Direction: North **Survey Date:** 8/21/2019 Comments: Property area





Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 65 **Photo Location:** KTP-18.3 Direction: East **Survey Date:** 8/21/2019 Comments: Property area

Photograph ID: 66

**Photo Location:** 

KTP-18.3

Direction:

South

**Survey Date:** 

8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA

Photograph ID: 67

**Photo Location:** 

KTP-18.3

Direction:

West

**Survey Date:** 8/21/2019

Comments: Property area



Photograph ID: 68

**Photo Location:** 

KTP-18.3

Direction:

North

**Survey Date:** 

8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 69

**Photo Location:** KTP-18.4

Direction: South

**Survey Date:** 8/21/2019

Comments: Property area



Photograph ID: 70

**Photo Location:** 

KTP-18.4

Direction: West

**Survey Date:** 8/21/2019

Comments:





Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 71 **Photo Location:** KTP-19 Direction: South **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 72 **Photo Location:** KTP-19 Direction: West **Survey Date:** 8/21/2019 Comments: Property area



Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 73 **Photo Location:** KTP-19 Direction: SW **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 74 **Photo Location:** KTP-19.1 Direction: South **Survey Date:** 8/21/2019 Comments: Property area





Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 75 **Photo Location:** KTP-19.1 Direction: South East **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 76 **Photo Location:** KTP-19.1 Direction: East **Survey Date:** 8/21/2019 Comments: Property area



Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 77 **Photo Location:** KTP-19.1 Direction: South West **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 78 **Photo Location:** KTP-19.2 Direction: South East Survey Date: 8/21/2019 Comments: Property area





Photograph ID: 79

**Photo Location:** 

KTP-19.2

**Direction:**South West

**Survey Date:** 8/21/2019

**Comments:** Property area



Photograph ID: 80

**Photo Location:** 

KTP-19.2

Direction:

North West

**Survey Date:** 8/21/2019

Comments:







Project: Phase I ESA Client: 8minutenergy

Site Name: Kudu Site Location: California City, CA

Photograph ID: 81

**Photo Location:** 

KTP-19.3

Direction:

East

**Survey Date:** 8/21/2019

Comments:

Property area - adjacent

railroad tracks



Photograph ID: 82

**Photo Location:** 

KTP-19.3

Direction:

South

**Survey Date:** 

8/21/2019

Comments:

Property area - adjacent

railroad tracks







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 83 **Photo Location:** KTP-19.3 Direction: South East **Survey Date:** 8/21/2019 Comments: Property area - adjacent railroad tracks Photograph ID: 84 **Photo Location:** KTP-20 Direction: South **Survey Date:** 8/21/2019 Comments: Property area





Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 85 **Photo Location:** KTP-20 Direction: West **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 86 **Photo Location:** KTP-20 Direction: South West Survey Date: 8/21/2019 Comments: Property area





Client: 8minutenergy Project: Phase I ESA

Site Name: Kudu Site Location: California City, CA

Photograph ID: 87

**Photo Location:** 

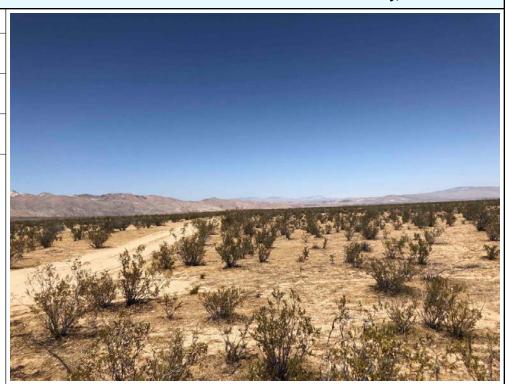
KTP-20.1

Direction:

North

**Survey Date:** 8/21/2019

Comments: Property area



Photograph ID: 88

**Photo Location:** 

KTP-20.1

Direction:

West

Survey Date:

8/21/2019

Comments:







Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 89 **Photo Location:** KTP-20.1 Direction: South East **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 90 **Photo Location:** KTP-20.2 Direction: East **Survey Date:** 8/21/2019 Comments: Property area





Client: 8minutenergy Project: Phase I ESA Site Name: Kudu Site Location: California City, CA Photograph ID: 91 **Photo Location:** KTP-20.2 Direction: South **Survey Date:** 8/21/2019 Comments: Property area Photograph ID: 92 **Photo Location:** KTP-21 Direction: West **Survey Date:** 8/23/2019 Comments: Property area





Client: 8minutenergy Project: Phase I ESA Site Name: Kudu Site Location: California City, CA Photograph ID: 93 **Photo Location:** KTP-21 Direction: South West **Survey Date:** 8/23/2019 Comments: Property area Photograph ID: 94 **Photo Location:** KTP-21 Direction: South **Survey Date:** 8/23/2019 Comments: Property area





Client: 8minutenergy Project: Phase I ESA

Site Name: Kudu Site Location: California City, CA

Photograph ID: 95

**Photo Location:** 

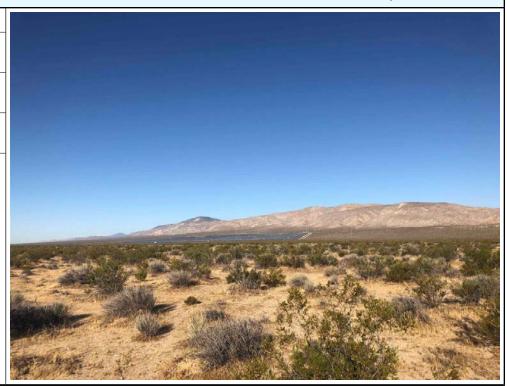
KTP-22

Direction:

East

**Survey Date:** 8/23/2019

**Comments:** Property area



Photograph ID: 96

**Photo Location:** 

KTP-22

Direction:

West

Survey Date:

8/23/2019

Comments:







Photograph ID: 97

**Photo Location:** 

KTP-22

**Direction:**South West

**Survey Date:** 8/23/2019

**Comments:** Property area



Photograph ID: 98

**Photo Location:** 

KTP-22

Direction:

South

Survey Date:

8/23/2019

Comments:







Photograph ID: 99

**Photo Location:** 

KTP-23

Direction:

East

**Survey Date:** 8/23/2019

Comments:

Property area



Photograph ID: 100

**Photo Location:** 

KTP-23

Direction:

South East

**Survey Date:** 

8/23/2019

Comments:







Client: 8minutenergy Project: Phase I ESA Site Name: Kudu Site Location: California City, CA Photograph ID: 101 **Photo Location:** KTP-23 Direction: South **Survey Date:** 8/23/2019 Comments: Property area Photograph ID: 102 **Photo Location:** KTP-24 Direction: North **Survey Date:** 8/23/2019 Comments: Property area





Client: 8minutenergy Project: Phase I ESA
Site Name: Kudu Site Location: California City, CA

Photograph ID: 103

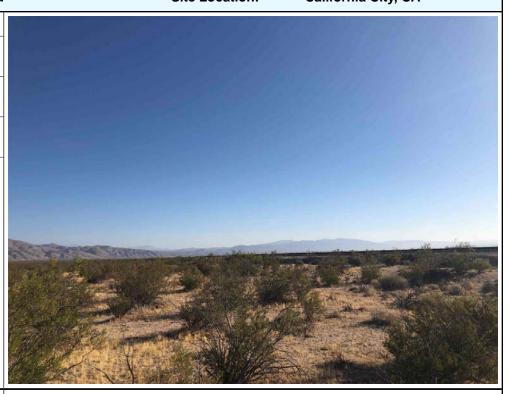
**Photo Location:** 

KTP-24

**Direction:** North East

**Survey Date:** 8/23/2019

**Comments:** Property area



Photograph ID: 104

**Photo Location:** 

KTP-24

Direction:

East

**Survey Date:** 8/23/2019

Comments:

Property area - adjacent railroad tracks





Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 105 **Photo Location:** KTP-25 Direction: North **Survey Date:** 9/13/2019 Comments: Gen-tie line path - North on Neuralia Rd. Photograph ID: 106 **Photo Location:** KTP-26 Direction: North Survey Date: 9/13/2019 Comments: Gen-tie line path - North on Neuralia Rd.



Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 107 **Photo Location:** KTP-26 Direction: West **Survey Date:** 9/13/2019 Comments: Gen-tie line path - West on Neuralia Rd. at Phillips Rd. Photograph ID: 108 **Photo Location:** KTP-27 Direction: West Survey Date: 9/13/2019 Comments: Gen-tie line path - West on Phillips Rd.



Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 109 **Photo Location:** KTP-27 Direction: North West **Survey Date:** 9/13/2019 Comments: Phillips Rd. looking at lot of future sub-station Photograph ID: 110 **Photo Location:** KTP-28 Direction: North **Survey Date:** 9/13/2019 Comments: Property area



Phase I ESA Client: Project: 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 111 **Photo Location:** KTP-28 Direction: West **Survey Date:** 9/13/2019 Comments: Property area Photograph ID: 112 **Photo Location:** KTP-28 Direction: East Survey Date: 9/13/2019 Comments: Property area





Client: Project: Phase I ESA 8minutenergy Site Name: Kudu Site Location: California City, CA Photograph ID: 113 **Photo Location:** KTP-29 Direction: North **Survey Date:** 9/13/2019 Comments: Miscellaneous trash at northern border of property area Photograph ID: 114 **Photo Location:** KTP-29 Direction: East Survey Date: 9/13/2019 Comments: Property area

## KUDU SOLAR FARM PHASE I ENVIRONMENTAL SITE ASSESSMENT

Appendix B Stantec Resumes December 4, 2019

**Appendix B STANTEC RESUMES** 



Managing Principal Geologist



Kyle has more than 28 years of professional experience—17 of those years with Stantec—providing geotechnical and environmental consulting. During the course of his experience, he has been involved with a wide variety of geological and engineering projects. He has been in direct charge of quality control/quality assurance (QA/QC) work for Stantec and previous firms for geological, engineering geological, and environmental services primarily in California. Additionally, Kyle has been a primary contact for Stantec with many different clients (including multi-party actions) and regulatory bodies involving contracting, workplan approvals, site assessments and closures, permitting, remedial action, and litigation support. With regard to litigation services, Kyle has extensive experience providing expert witness testimony, second-party review, and litigation support and analysis.

Kyle's extensive experience includes assessment and remediation of property-specific and regional issues involving soil and groundwater contaminated with petroleum hydrocarbons, chlorinated solvents, heavy metals, pesticides, and PCBs.

He currently serves as the managing principal geologist in Stantec's Redlands, California office.

#### **EDUCATION**

Engineering Geology/Hydrogeology, California State University, Los Angeles, California, 1984

AS, General Science, Crafton Hills College, Yucaipa, California, 1975

BS, Geological Sciences, California State University, Long Beach, California, 1982

#### **REGISTRATIONS**

Certified Engineering Geologist #1271, State of California

Professional Geologist #4066, State of California

#### PROJECT EXPERIENCE

#### **Bioremediation**

Excavation and Treatment of Petroleum-Contaminated Soil

Kyle designed the excavation and treatment of 45,000 cubic yards of petroleum-contaminated soil. Soil treatment included utilizing vapor extraction, combined with bioremediation.

#### **Chemicals & Polymers**

Assessments and Remediation, Vernon, California *Mr*. Emerson was part of the team for conducting Phase I and Phase II Environmental Site Assessments (ESA) and developing remedial action plans for two former chemical plant sites with 80-year industrial histories. Phase I ESAs used historical files, maps, aerial photographs, available documents, and data from public agencies and historical directories for identifying recognized environmental concerns. Extensive Phase II ESA survey activities aided in identifying below-grade structures such as vaults/USTs, as well as assessing the extent of influence and nature of the contamination. These investigations confirmed the presence of heavy metals, petroleum hydrocarbons, volatile organic compounds, polychlorinated biphenyls, radioactive materials, semi-volatile organic compounds, and polycyclic aromatic compounds in the soils for these sites. Specific areas of concern included former settling ponds, a bone yard, maintenance areas, transformer and substations, wastewater treatment facilities, and above-ground storage tank farms. A conceptual mode was developedl for use in a health risk assessment and developed risk-based corrective actions to address potential health and environmental concerns. He assisted with the development and implementation of a remedial action plan, combined administrative controls, engineering controls, and active remediation; this resulted in the cost-effective return of one site to active use, and is reducing health risks to occupants and the public at the second site.

Two Former Chemical Plants, Environmental Site

<sup>\*</sup> denotes projects completed with other firms

## CONFIDENTIAL: Aerospace Adhesives and Coatings Plant, Glendale, California

Mr. Emerson was part of the team that conducted feasibility studies to evaluate remedial alternatives for remediation of chlorinated VOCs, 1,4 dioxane, and hexavalent chromium (CrVI) in soil, soil vapor, and groundwater. Feasibility studies included groundwater pump testing, benchscale column testing to evaluate in situ alternatives for reducing CrVI to the less mobile CrIII valence state, soil vapor extraction, capping, and excavation. Field pilot studies were performed to evaluate the efficiency of various CrVI reductants including the use of ferrous sulfate, calcium polysulfide, emulsified oil, and fructose. Extensive multi-depth soil vapor testing was conducted to evaluate the distribution of VOCs in the subsurface and to support vapor intrusion risk assessment. Feasibility studies were completed in 2008. Remedial actions are expected to be completed in 2011.

#### **Condition Assessments**

## Assessment and Mitigation of Manufacturing Facility

Kyle managed the assessment and mitigation of an ammunition manufacturing facility covering 1,100 acres in a complex geologic environment. The contaminates involved red and white phosphorous, TNT, chlorinated solvents, solid wastes, and live ordinance.

## Soil Contamination Assessment Supervision and Management

Kyle managed and supervised soil contamination assessment and in-situ remediation of heavy metals involving chromium, cadmium, nickel and zinc by chemical fixation to depths in excess of 40 feet below ground surface beneath existing structures within several manufacturing facilities.

#### Litigation Support and Expert Testimony

Kyle provided litigation support and expert testimony on more than 20 separate projects involving service stations, chlorinated solvent cases, heavy metal, and semi-volatile releases.

#### Corporate / Office

#### CT Realty Environmental Remediation of Former Dry Cleaners, El Centro, California

Mr. Emerson was responsible for assessments and remediation at this former dry cleaners which released the dry cleaning chemical tetrachloroethene (PCE) to the ground and underlying groundwater. The work included initial site assessment, agency interaction and negotiations with the California Regional Water Quality Control Board (CRWQCB), and Colorado Basin Region human health risk assessment (HHRA), design and implementation of remedial investigations, feasibility studies, remedial action plans, and implementation of remediation in mitigating chlorinated solvent contamination in vadose and saturated zones at concentrations indicative of DNAPL. The results of the completed remediation, as well as continued confirmation sampling and monitoring, allowed the CRWQCB to issue site closure in 2008. The site has since been redeveloped into a new commercial development.

#### **Environmental Assessments**

#### Sitina Studies

Kyle performed initial siting studies for potential Class I, II, and III landfills. The project included detailed geologic mapping, hydrogeological studies, and permeability studies of caps and liners.

#### **Environmental Site Remediation**

## Assessment and Remedial Design, California (Project Supervisor)

Kyle supervised the assessment and remedial design of a system to eliminate salt brine contamination in shallow perched water horizons in the Yucaipa, San Bernardino, and Riverside areas of southern California.

#### Design and Installation of Recovery Systems\*

Kyle designed and installed numerous free-product recovery systems that successfully recovered product. One of the sites contained product up to 11-feet thick covering more than three city blocks. The dissolved phase had affected a multi-aquifer system and a public drinking water system.

#### Geophysical Characterizations\*

Kyle performed and supervised numerous geophysical characterizations to determine the extent of old landfills. He provided classification studies, landfill gas monitoring, removal verification during grading, methane collection and mitigation plans, permitting, and closure plans.

<sup>\*</sup> denotes projects completed with other firms

Managing Principal Geologist

#### Domestic Landfill Development\*

Kyle designed and supervised the dynamic consolidation of a domestic landfill for development. He used this process to minimize expected settlement to overlying structures. Kyle designed commercial developments on closed landfills that involved complex methane collection and monitoring systems and building settlement controls.

#### Clay Borrow Site Studies

Kyle performed more than 10 separate clay borrow site studies for determining sources of material to cap landfills; ranged from a 20-acre dry lakebed to a 450-acre parcel in complex folded marine sediments.

#### Assessment, Clean Up, and Regulatory Support Management, Santa, Monica (Project Manager)

Kyle managed the assessment, clean up, and complex regulatory support of a PRP site in an MTBE case (Charnock subbasin). His work involved more than 20 environmental professionals working full time for two years to complete the assessment and clean up mandated by the regulatory agencies.

#### **Hazardous Waste**

# San Gabriel Valley Superfund Site, Remediation & Closure of Multiple Source Areas, Industry, California

Mr. Emerson performed feasibility studies to evaluate appropriate and relevant remedial alternatives to mitigate constituents of concern in five AOCs contaminated with chlorinated hydrocarbons, heavy metals, petroleum fuel, and cutting oils. Ultimately, a combination of remedial alternatives was implemented that included large-diameter auger excavation to 45 feet to minimize impacts on facility operations, vapor extraction, vapor intrusion risk assessment, deed restriction, and monitored natural attenuation. At the completion of remedial actions, confirmation soil, soil vapor, and groundwater sampling were conducted and followed with risk assessment to demonstrate that remedial objectives had been achieved. No further action was recently granted by the US EPA and Los Angeles Regional Water Quality Control Board.

#### Mixed-Use

#### Port of San Diego Rohr Facility, Chula Vista, California

Mr. Enerson assisted in a detailed subsurface assessment of the Rohr facility. The intent of the assessment was to evaluate the 40-acre former aircraft part manufacturing facility for acquisition by the Port of San Diego for redevelopment into a business park and entertainment complex. The assessment identified the presence of soil, soil vapor, and groundwater impacts by petroleum hydrocarbons, VOCs, heavy metals, PCBs, and semi-volatile organic compounds. He utilized many sampling techniques to assess the limits and concentrations of contaminants in the subsurface. Ultimately, the team was able to develop a cost estimate for potential remedial action cost associated to corrective action to allow redevelopment.

#### Master Planned Commercial/Residential Redevelopment Project, Whittier, California (Project Manager)

Kyle oversaw the assessment of 26 contiguous properties that are part of a 21-acre master planned commercial/residential redevelopment project. The properties included industrial facilities, platting lines, fuel USTs, and metal processing plants, among others. The estimated cleanup costs are approximately \$2 million.

#### Multi-Unit / Family Residential

## Residential Development Assessment, Ventura, California (Project Director)

Kyle directed an assessment of a 40-acre former agricultural property proposed for residential development. Pesticides were identified above hazardous waste levels and preliminary remediation goals established by the U.S. Environmental Protection Agency. Through corrective grading methods and onsite placement of the pesticide impacted soils, all material were re-used on site without offsite disposal. The over all cost savings for the client was more than \$1 million. Total cost was less than \$250,000 for all necessary activities.

#### Oil & Gas

#### Oil Field Site Assessments\*

Kyle performed site assessments at oil field leases involving refineries, bulk storage areas, piping systems and wellhead, and drilling mud pit contamination.

<sup>\*</sup> denotes projects completed with other firms

Managing Principal Geologist

#### Environmental Protection Agency Superfund Action, Culver City, California (Project Manager)

Kyle served as the project manager representing a major oil company in the assessment, remedial action, and litigation support in a multi-party contamination case affecting a City water supply. The assessment involved more than 250 continuous core borings up to 100 feet, as well as extensive remedial actions. The total cost for all related activities was \$22 million. The case is settled and the closure of the site is pending.

#### **Project Management**

#### Liability and Property Management Consulting Services

Kyle is providing liability and property management consulting services to more than 10 medium to large property development firms in the US. His work involves property transaction assessments, contract review, acquisition guideline development, liability management evaluation, insurance acquisition, and strategic planning.

#### **Residential Development**

## Environmental Development Management and Review (Project Manager)

Kyle manages and reviews environmental development issues for a large residential developer specializing in development of contaminated industrial properties by providing innovative solutions in developing contaminated properties for residential use through risk assessment, engineering, and administrative and property development controls.

#### Site Management and Remediation

## Design and Implementation of Biodegradation Programs\*, California

Kyle designed and implemented one of the first in-situ biodegradation programs in California; it involved 50,000 cubic yards of diesel-contaminated soils, and groundwater to depths of 70 feet below ground surface.

#### Soil and Groundwater Remediation Systems

## Soil and Groundwater Contamination Assessments and Mitigation\*, California (Project Manger)

Kyle managed numerous chlorinated solvent soil and groundwater contamination assessments and mitigation programs in southern California. The projects involved releases that impacted soil and groundwater to depth of groundwater more than 700 feet in multi-aquifer systems. One case involved with plume dimensions more than 1 mile from the source affecting residential properties.

## Soil and Groundwater Assessment and Remediation Programs\*

Implemented hundreds of soil and groundwater assessment and remediation programs at various service station facilities in Southern and Northern California, and Nevada. Work involved assessment, remedial design, installation, maintenance and monitoring. Closure has been received on a majority of these sites.

#### Assessment and Remediation Management\*

Kyle managed the assessment and remediation of soil and groundwater manufacturing at dry cleaning facilities contaminated with chlorinated solvents.

#### Warehouse / Light Industrial

#### Glendale Redevelopment Project, Glendale, California (Project Manager)

Kyle managed the assessment and remedial actions during the redevelopment of and industrial property. The project involved the demolition of a historic manufacturing facility and a commercial dry cleaner. Each of these facilities were associated with releases of solvents and petroleum hydrocarbons. Remedial actions involved excavation by pattern drilling and off site disposal along with removal of former USTs. The total cost of remediation and assessment was \$450,000.00.

<sup>\*</sup> denotes projects completed with other firms

Managing Principal Geologist

#### Compton Redevelopment Project, Compton, California (Project Manager)

Kyle is serving as project manager for the assessment and remedial actions for a large redevelopment project. The project involves the redevelopment of a historic manufacturing facility and a former dry cleaner. Each of these facilities were associated with releases of solvents and petroleum hydrocarbons. The industrial facility was also associated with significant volumes of buried waste that required removal and disposal. These wastes also included the chemical referenced above, as well as PCBs and heavy metals. Remediation has included excavation, vapor extraction, and chemical fixation. The total cost of this project has been \$2.8 million to date.

<sup>\*</sup> denotes projects completed with other firms

Managing Principal Geologist

#### **PUBLICATIONS**

In-Situ Bioremediation of an Underground Diesel Fuel Spill: A Case Study. *Environmental* Management, 1989.

### Dion Monge

**Project Scientist** 



Dion has extensive knowledge of underground storage tank investigations, Phase I and II environmental site assessment, groundwater monitoring and reporting, soil, soil vapor, and groundwater quality assessments, and testing for asbestos and lead based paint. His project experience is extensive and wide ranging and includes many types of soil, soil vapor, and groundwater assessment and monitoring for planned, existing, and former sites. Dion also has experience in testing fill soils placed on grading sites.

He has experience on redevelopment of former oil field sites that include submittal of construction site review plans, oil well mitigation (venting and casing alterations), abandonment of oil wells, and remedial investigations and remediation involving soil contamination.

Dion also has experience working with 1166 AQMD air monitoring on projects ranging from limited access dry cleaner excavations, solvent excavations, and petroleum excavations related to underground storage tank releases. Included in this type of monitoring is the assessment of a safe work environment for the contractors involved with this type of work.

He has considerable knowledge in asbestos and lead based paint sampling as a building inspector and lead sampling technician. Asbestos and lead based paint surveys have ranged from large office buildings to sampling highway bridges.

#### **EDUCATION**

BS, Soil Science, California Polytechnic University, Pomona, Pomona, California, 2004

Health & Safety Certification (29 CFR 1910.120),, 40-Hour OSHA Health & Safety Certification, Redlands, California, 2005

Health & Safety Annual Update Certification, 8-Hour OSHA, Redlands, California, 2009

First Aid/CPR, American Red Cross, Redlands, California, 2009

Certified Building Inspector, AHERA 8-Hour Refresher, Redlands, California, 2009

#### PROJECT EXPERIENCE

#### Asbestos, Lead Based Paint, and Hazardous Material Management

Haller Wash Bridge No. 54-0891R&L, San Bernardino County, California (Asbestos and Lead-Based Paint Sampling Assistant)

Dion conducted asbestos and lead based paint survey on highway bridge. He assisted with planning field operations, measuring bridge dimensions, and collecting samples. Tasks included sample collection, bridge measurements, and documentation.

#### **Project Management Oversight**

Magnolia Plaza, Fountain Valley, California

Dion is providing project management of soil, soil vapor, and quarterly groundwater sampling related to a solvent release at a former dry cleaning facility. Tasks include preparation of work plans for approval by the Regional Water Quality Control Board and oversight of field sampling, including lithologic logging, for soil and soil vapor investigations performed within a multi-tenant strip center. Additional tasks include preparation of investigative reports and quarterly groundwater monitoring reports. The site remains an open case and preparation of a work plan to use electrical resistive heating ("ERH") will be prepared in the coming weeks.

### Dion Monge

**Project Scientist** 

#### Former Superb Dry Cleaners, Anaheim, California

Dion performed field oversight, direction, and confirmation soil sampling of a limited access excavation within a former dry cleaner unit. Post excavation field activities included application of a barrier type floor sealant along with post excavation indoor air sampling. Remedial work led to regulatory closure being granted from the local agency.

#### Site Assessment

#### Proposed Friends Christian High School, Yorba Linda, California

Dion prepared preliminary site assessment (PSA) report for future private school site to identify recognized environmental conditions ("RECs") related to past property usage as an oil field with 21 oil wells abandoned prior to 1990. Completion of the PSA led to his management of the project through site closure. Field investigations and reporting by Dion included Phase II investigations, methane survey, oil well leak testing and venting, backfill and compaction (including soils testing), DOGGR Construction Site Review, and excavation and onsite management of more than 5,000 cubic yards of petroleum impacted soils.

#### SR-58 Widening, San Bernardino County, California

Dion performed Initial Site Assessment (ISA) for Caltran at Kramer Junction for the proposed widening of State Route 58. The ISA was performed in accordance with guidelines promulgated by the American Society for Testing and Materials (ASTM) and included historical research and coordination of permit/file reviews with local building/planning departments and environmental agencies. Dion's role included the field visit, observation documentation, agency reviews, and reporting.

#### Soil Sampling

#### Caltrans I-15, Task Order 28, Hesperia, California

Dion conducted a soil investigation for metals analysis alongside I-15 for disposal recommendations during construction of mortar-lined channels at several locations. He assisted with planning field operations and collected soil samples. Tasks included sample collection, preservation, and documentation.

<sup>\*</sup> denotes projects completed with other firms

## KUDU SOLAR FARM PHASE I ENVIRONMENTAL SITE ASSESSMENT

Appendix C Environmental Agency Database Search Report December 4, 2019

Appendix C ENVIRONMENTAL AGENCY DATABASE SEARCH REPORT



Kudo

Kudo California City, CA 93505

Inquiry Number: 5759392.2s

August 21, 2019

# **EDR Area / Corridor Report**



#### **TABLE OF CONTENTS**

| SECTION  | PAGE |
|--|------|
| Executive Summary.                                 | ES1  |
| Mapped Sites Summary                               |      |
| Key Map  |      |
| Map Findings Summary                               |      |
| Focus Maps   | 7    |
| Map Findings                                       |      |
| Orphan Summary                                     | OR-1 |
| Government Records Searched/Data Currency Tracking | GR-1 |

Thank you for your business.
Please contact EDR at 1-800-352-0050
with any questions or comments.

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#### **EXECUTIVE SUMMARY**

A search of available environmental records was conducted by Environmental Data Resources, Inc (EDR). The report was designed to assist parties seeking to meet the search requirements of EPA's Standards and Practices for All Appropriate Inquiries (40 CFR Part 312), the ASTM Standard Practice for Environmental Site Assessments (E 1527-13), the ASTM Standard Practice for Environmental Site Assessments for Forestland or Rural Property (E 2247-16), the ASTM Standard Practice for Limited Environmental Due Diligence: Transaction Screen Process (E 1528-14) or custom requirements developed for the evaluation of environmental risk associated with a parcel of real estate.

#### SUBJECT PROPERTY INFORMATION

#### **ADDRESS**

KUDO CALIFORNIA CITY, CA 93505

#### TARGET PROPERTY SEARCH RESULTS

The Target Property was identified in the following databases.

Page Numbers and Map Identifications refer to the EDR Area/Corridor Report where detailed data on individual sites can be reviewed.

Sites listed in **bold italics** are in multiple databases.

#### SURROUNDING SITES: SEARCH RESULTS

Surrounding sites were not identified.

Unmappable (orphan) sites are not considered in the foregoing analysis.

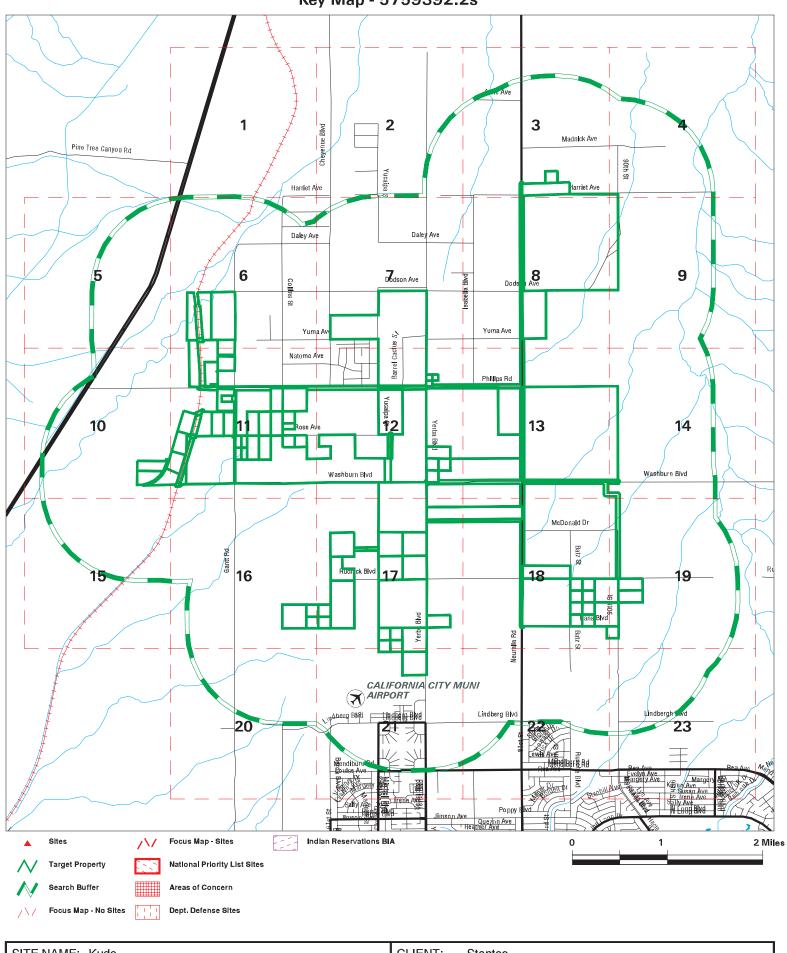
#### MAPPED SITES SUMMARY

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.) FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

NO MAPPED SITES FOUND

Key Map - 5759392.2s



SITE NAME: Kudo ADDRESS: Kudo

CITY/STATE: California City CA ZIP: 93505 CLIENT: Stantec CONTACT: Alicia Jansen

INQUIRY #: 5759392.2s DATE: 08/21/19

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3:23 PM

| Database   | Search<br>Distance<br>(Miles) | Target<br>Property | < 1/8       | 1/8 - 1/4   | 1/4 - 1/2      | 1/2 - 1        | > 1            | Total<br>Plotted |  |
|--|-------------------------------|--------------------|-------------|-------------|----------------|----------------|----------------|------------------|--|
| STANDARD ENVIRONME   | NTAL RECORDS                  | <u>s</u>           |             |             |                |                |                |                  |  |
| Federal NPL site list  |                               |                    |             |             |                |                |                |                  |  |
| NPL<br>Proposed NPL<br>NPL LIENS                                 | 1.000<br>1.000<br>1.000       |                    | 0<br>0<br>0 | 0<br>0<br>0 | 0<br>0<br>0    | 0<br>0<br>0    | NR<br>NR<br>NR | 0<br>0<br>0      |  |
| Federal Delisted NPL sit   | e list                        |                    |             |             |                |                |                |                  |  |
| Delisted NPL   | 1.000                         |                    | 0           | 0           | 0              | 0              | NR             | 0                |  |
| Federal CERCLIS list   |                               |                    |             |             |                |                |                |                  |  |
| FEDERAL FACILITY<br>SEMS   | 0.500<br>0.500                |                    | 0<br>0      | 0<br>0      | 0<br>0         | NR<br>NR       | NR<br>NR       | 0<br>0           |  |
| Federal CERCLIS NFRA   | P site list                   |                    |             |             |                |                |                |                  |  |
| SEMS-ARCHIVE   | 0.500                         |                    | 0           | 0           | 0              | NR             | NR             | 0                |  |
| Federal RCRA CORRACTS facilities list                            |                               |                    |             |             |                |                |                |                  |  |
| CORRACTS   | 1.000                         |                    | 0           | 0           | 0              | 0              | NR             | 0                |  |
| Federal RCRA non-COR   | RACTS TSD f                   | acilities list     |             |             |                |                |                |                  |  |
| RCRA-TSDF  | 0.500                         |                    | 0           | 0           | 0              | NR             | NR             | 0                |  |
| Federal RCRA generator   | rs list                       |                    |             |             |                |                |                |                  |  |
| RCRA-LQG<br>RCRA-SQG<br>RCRA-CESQG                               | 0.250<br>0.250<br>0.250       |                    | 0<br>0<br>0 | 0<br>0<br>0 | NR<br>NR<br>NR | NR<br>NR<br>NR | NR<br>NR<br>NR | 0<br>0<br>0      |  |
| Federal institutional controls / engineering controls registries |                               |                    |             |             |                |                |                |                  |  |
| LUCIS<br>US ENG CONTROLS<br>US INST CONTROL                      | 0.500<br>0.500<br>0.500       |                    | 0<br>0<br>0 | 0<br>0<br>0 | 0<br>0<br>0    | NR<br>NR<br>NR | NR<br>NR<br>NR | 0<br>0<br>0      |  |
| Federal ERNS list  |                               |                    |             |             |                |                |                |                  |  |
| ERNS   | TP                            |                    | NR          | NR          | NR             | NR             | NR             | 0                |  |
| State- and tribal - equiva                                       | alent NPL                     |                    |             |             |                |                |                |                  |  |
| RESPONSE   | 1.000                         |                    | 0           | 0           | 0              | 0              | NR             | 0                |  |
| State- and tribal - equiva                                       | alent CERCLIS                 | 5                  |             |             |                |                |                |                  |  |
| ENVIROSTOR   | 1.000                         |                    | 0           | 0           | 0              | 0              | NR             | 0                |  |
| State and tribal landfill and/or solid waste disposal site lists |                               |                    |             |             |                |                |                |                  |  |
| SWF/LF   | 0.500                         |                    | 0           | 0           | 0              | NR             | NR             | 0                |  |
| State and tribal leaking   | storage tank l                | ists               |             |             |                |                |                |                  |  |
| LUST   | 0.500                         |                    | 0           | 0           | 0              | NR             | NR             | 0                |  |

| Database   | Search<br>Distance<br>(Miles)                               | Target<br>Property | < 1/8                                   | 1/8 - 1/4                               | 1/4 - 1/2                                 | 1/2 - 1                                    | > 1                                    | Total<br>Plotted           |  |
|--|---|--------------------|---|---|---|--|--|----------------------------|--|
| INDIAN LUST<br>CPS-SLIC  | 0.500<br>0.500  |                    | 0                                       | 0<br>0                                  | 0<br>0                                    | NR<br>NR                                   | NR<br>NR                               | 0<br>0                     |  |
| State and tribal registered storage tank lists   |   |                    |   |   |   |  |  |                            |  |
| FEMA UST<br>UST<br>AST<br>INDIAN UST   | 0.250<br>0.250<br>0.250<br>0.250                            |                    | 0<br>0<br>0<br>0                        | 0<br>0<br>0<br>0                        | NR<br>NR<br>NR<br>NR                      | NR<br>NR<br>NR<br>NR                       | NR<br>NR<br>NR<br>NR                   | 0<br>0<br>0<br>0           |  |
| State and tribal voluntary   | y cleanup site  | es                 |   |   |   |  |  |                            |  |
| INDIAN VCP<br>VCP  | 0.500<br>0.500  |                    | 0                                       | 0<br>0                                  | 0<br>0                                    | NR<br>NR                                   | NR<br>NR                               | 0<br>0                     |  |
| State and tribal Brownfie  | elds sites  |                    |   |   |   |  |  |                            |  |
| BROWNFIELDS  | 0.500   |                    | 0                                       | 0                                       | 0   | NR   | NR                                     | 0                          |  |
| ADDITIONAL ENVIRONMENTAL RECORDS   |   |                    |   |   |   |  |  |                            |  |
| Local Brownfield lists   |   |                    |   |   |   |  |  |                            |  |
| US BROWNFIELDS   | 0.500   |                    | 0                                       | 0                                       | 0   | NR   | NR                                     | 0                          |  |
| Local Lists of Landfill / S<br>Waste Disposal Sites                                      | Solid   |                    |   |   |   |  |  |                            |  |
| WMUDS/SWAT<br>SWRCY<br>HAULERS<br>INDIAN ODI<br>ODI<br>DEBRIS REGION 9<br>IHS OPEN DUMPS | 0.500<br>0.500<br>TP<br>0.500<br>0.500<br>0.500<br>0.500    |                    | 0<br>0<br>NR<br>0<br>0<br>0             | 0<br>0<br>NR<br>0<br>0<br>0             | 0<br>0<br>NR<br>0<br>0<br>0               | NR<br>NR<br>NR<br>NR<br>NR<br>NR           | NR<br>NR<br>NR<br>NR<br>NR<br>NR       | 0<br>0<br>0<br>0<br>0<br>0 |  |
| Local Lists of Hazardous waste / Contaminated Sites                                      |   |                    |   |   |   |  |  |                            |  |
| US HIST CDL HIST Cal-Sites SCH CDL Toxic Pits CERS HAZ WASTE US CDL PFAS                 | TP<br>1.000<br>0.250<br>TP<br>1.000<br>0.250<br>TP<br>0.500 |                    | NR<br>0<br>0<br>NR<br>0<br>0<br>NR<br>0 | NR<br>0<br>0<br>NR<br>0<br>0<br>NR<br>0 | NR<br>0<br>NR<br>NR<br>0<br>NR<br>NR<br>0 | NR<br>0<br>NR<br>NR<br>0<br>NR<br>NR<br>NR | NR<br>NR<br>NR<br>NR<br>NR<br>NR<br>NR | 0<br>0<br>0<br>0<br>0<br>0 |  |
| Local Lists of Registered  | d Storage Tan   | ıks                |   |   |   |  |  |                            |  |
| SWEEPS UST<br>HIST UST<br>CERS TANKS<br>CA FID UST                                       | 0.250<br>0.250<br>0.250<br>0.250                            |                    | 0<br>0<br>0                             | 0<br>0<br>0<br>0                        | NR<br>NR<br>NR<br>NR                      | NR<br>NR<br>NR<br>NR                       | NR<br>NR<br>NR<br>NR                   | 0<br>0<br>0<br>0           |  |
| Local Land Records   |   |                    |   |   |   |  |  |                            |  |
| LIENS  | TP  |                    | NR                                      | NR                                      | NR  | NR   | NR                                     | 0                          |  |

| Database   | Search<br>Distance<br>(Miles)  | Target<br>Property | < 1/8                                       | 1/8 - 1/4   | 1/4 - 1/2                            | 1/2 - 1                                 | > 1                                   | Total<br>Plotted |
|--|--|--------------------|---|---|--------------------------------------|---|---------------------------------------|------------------|
| LIENS 2<br>DEED  | TP<br>0.500  |                    | NR<br>0                                     | NR<br>0   | NR<br>0                              | NR<br>NR                                | NR<br>NR                              | 0<br>0           |
| Records of Emergency F   | Release Repo   | rts                |   |   |                                      |   |                                       |                  |
| HMIRS<br>CHMIRS<br>LDS<br>MCS<br>SPILLS 90   | TP<br>TP<br>TP<br>TP<br>TP   |                    | NR<br>NR<br>NR<br>NR<br>NR                  | NR<br>NR<br>NR<br>NR<br>NR                                      | NR<br>NR<br>NR<br>NR<br>NR           | NR<br>NR<br>NR<br>NR<br>NR              | NR<br>NR<br>NR<br>NR<br>NR            | 0<br>0<br>0<br>0 |
| Other Ascertainable Rec  | ords   |                    |   |   |                                      |   |                                       |                  |
| RCRA NonGen / NLR FUDS DOD SCRD DRYCLEANERS US FIN ASSUR EPA WATCH LIST 2020 COR ACTION TSCA TRIS SSTS ROD RMP RAATS PRP PADS ICIS FTTS MLTS COAL ASH DOE COAL ASH EPA PCB TRANSFORMER RADINFO HIST FTTS DOT OPS CONSENT INDIAN RESERV FUSRAP UMTRA LEAD SMELTERS US AIRS US MINES ABANDONED MINES FINDS DOCKET HWC ECHO | 0.250 1.000 1.000 0.500 TP TP TP 0.250 TP TP TP 1.000 TP |                    | 0 0 0 0 RR 0 RR RR RR RR RR O RR RR O O O O | 0 0 0 0 RR O RR O RR SKRRRRRRR O RR O O O O RR O O RR KRRRRRRRR | NOOORRRR ORRRRRRRR ORRR OOOORRRRRRRR | N O O R R R R R R R R R R R R R R R R R | R R R R R R R R R R R R R R R R R R R |                  |
| UXO FUELS PROGRAM CA BOND EXP. PLAN Cortese CUPA Listings  | 1.000<br>0.250<br>1.000<br>0.500<br>0.250  |                    | 0<br>0<br>0<br>0                            | 0<br>0<br>0<br>0  | 0<br>NR<br>0<br>0<br>NR              | 0<br>NR<br>0<br>NR<br>NR                | NR<br>NR<br>NR<br>NR<br>NR            | 0<br>0<br>0<br>0 |

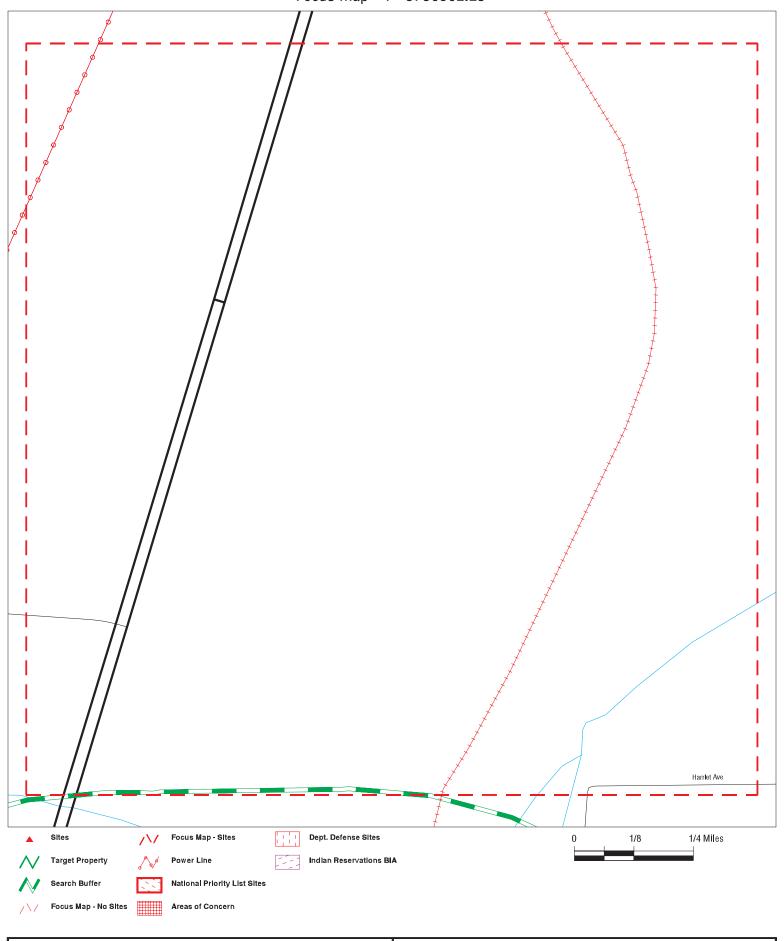
| Database               | Search<br>Distance<br>(Miles) | Target<br>Property | < 1/8  | 1/8 - 1/4 | 1/4 - 1/2 | 1/2 - 1  | > 1      | Total<br>Plotted |
|------------------------|-------------------------------|--------------------|--------|-----------|-----------|----------|----------|------------------|
| DRYCLEANERS            | 0.250                         |                    | 0      | 0         | NR        | NR       | NR       | 0                |
| EMI                    | TP                            |                    | NR     | NR        | NR        | NR       | NR       | Ō                |
| ENF                    | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| Financial Assurance    | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| HAZNET                 | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| ICE                    | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| HIST CORTESE           | 0.500                         |                    | 0      | 0         | 0         | NR       | NR       | 0                |
| HWP                    | 1.000                         |                    | 0      | 0         | 0         | 0        | NR       | 0                |
| HWT                    | 0.250                         |                    | 0      | 0         | NR        | NR       | NR       | 0                |
| MINES                  | 0.250                         |                    | 0      | 0         | NR        | NR       | NR       | 0                |
| MWMP                   | 0.250                         |                    | 0      | 0         | NR        | NR       | NR       | 0                |
| NPDES                  | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| PEST LIC<br>PROC       | TP<br>0.500                   |                    | NR     | NR        | NR<br>0   | NR<br>NR | NR<br>NR | 0<br>0           |
| Notify 65              | 1.000                         |                    | 0<br>0 | 0<br>0    | 0         | 0        | NR       | 0                |
| UIC                    | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| UIC GEO                | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| WASTEWATER PITS        | 0.500                         |                    | 0      | 0         | 0         | NR       | NR       | 0                |
| WDS                    | TP                            |                    | NR     | NR        | NR        | NR       | NR       | Ő                |
| WIP                    | 0.250                         |                    | 0      | 0         | NR        | NR       | NR       | Ö                |
| MILITARY PRIV SITES    | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| PROJECT                | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| WDR                    | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| CIWQS                  | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| CERS                   | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| NON-CASE INFO          | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| OTHER OIL GAS          | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| PROD WATER PONDS       | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| SAMPLING POINT         | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| WELL STIM PROJ         | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| EDR HIGH RISK HISTORIC | AL RECORDS                    |                    |        |           |           |          |          |                  |
| EDR Exclusive Records  |                               |                    |        |           |           |          |          |                  |
| EDR MGP                | 1.000                         |                    | 0      | 0         | 0         | 0        | NR       | 0                |
| EDR Hist Auto          | 0.125                         |                    | 0      | NR        | NR        | NR       | NR       | 0                |
| EDR Hist Cleaner       | 0.125                         |                    | 0      | NR        | NR        | NR       | NR       | 0                |
| EDR RECOVERED GOVER    | NMENT ARCH                    | IVES               |        |           |           |          |          |                  |
| Exclusive Recovered Go | vt. Archives                  |                    |        |           |           |          |          |                  |
| RGA LF                 | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
| RGA LUST               | TP                            |                    | NR     | NR        | NR        | NR       | NR       | 0                |
|                        |                               |                    |        |           |           |          |          |                  |
| - Totals               |                               | 0                  | 0      | 0         | 0         | 0        | 0        | 0                |

#### NOTES:

TP = Target Property

NR = Not Requested at this Search Distance

Sites may be listed in more than one database



SITE NAME: Kudo ADDRESS: Kudo CITY/STATE: California City CA ZIP: 93505

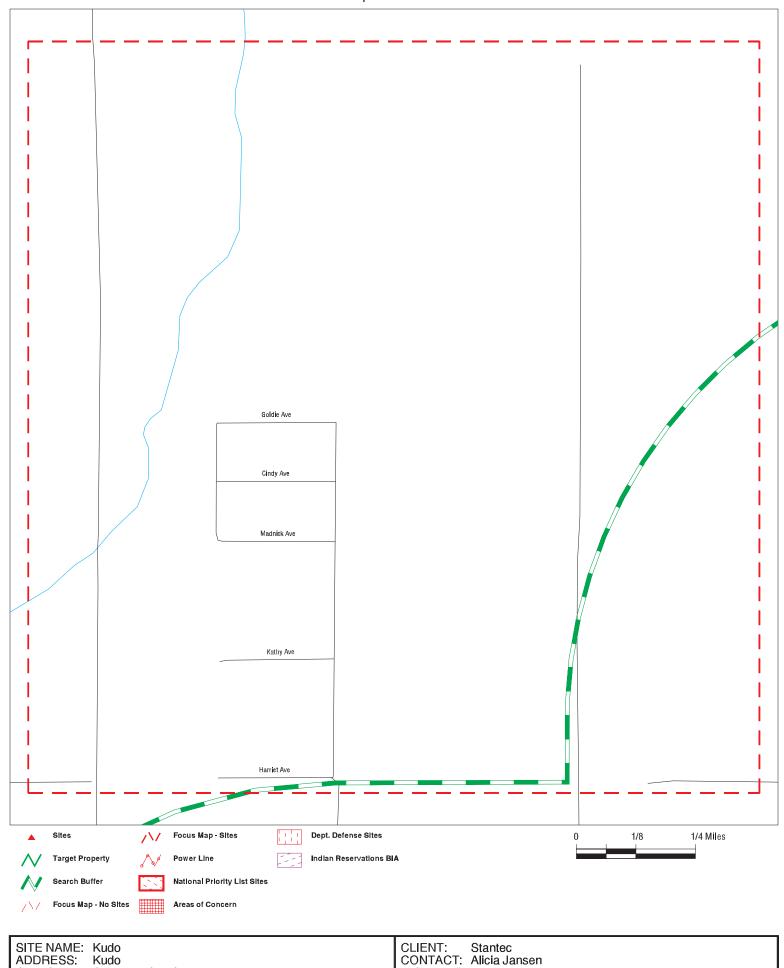
CLIENT: Stantec CONTACT: Alicia Jansen INQUIRY#: 5759392.2s DATE: 08/21/19

#### MAPPED SITES SUMMARY - FOCUS MAP 1

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.) FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

NO MAPPED SITES FOUND



CITY/STATE: California City CA ZIP: 93505

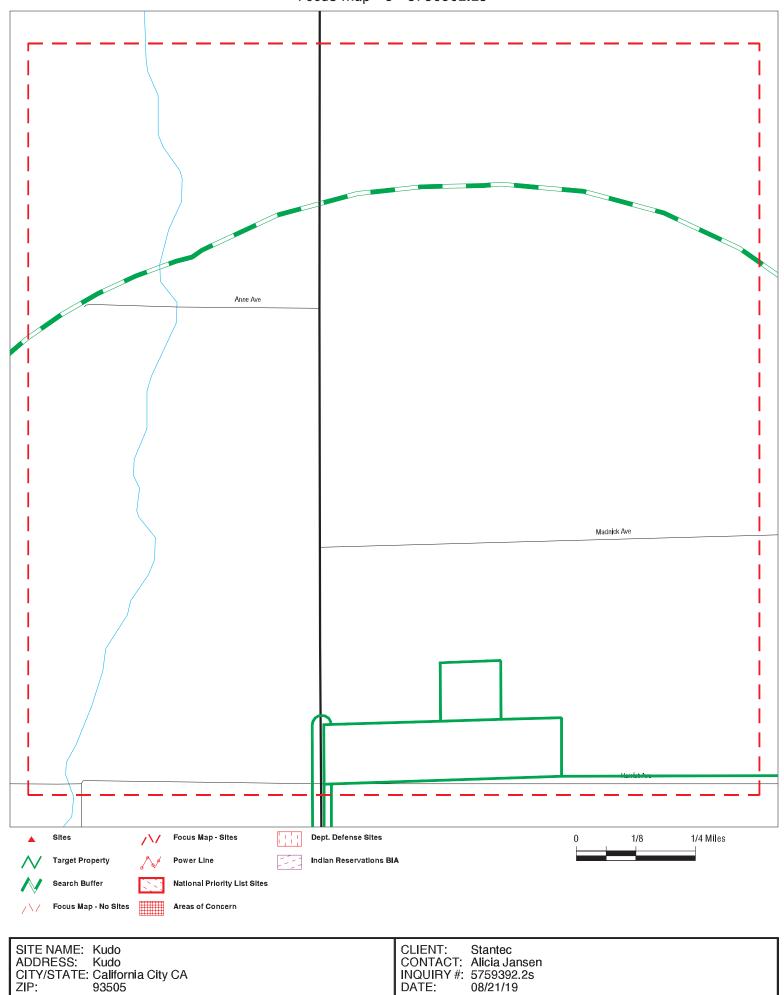
CLIENT: Stantec CONTACT: Alicia Jansen INQUIRY#: 5759392.2s DATE: 08/21/19

#### MAPPED SITES SUMMARY - FOCUS MAP 2

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

NO MAPPED SITES FOUND



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08/21/19

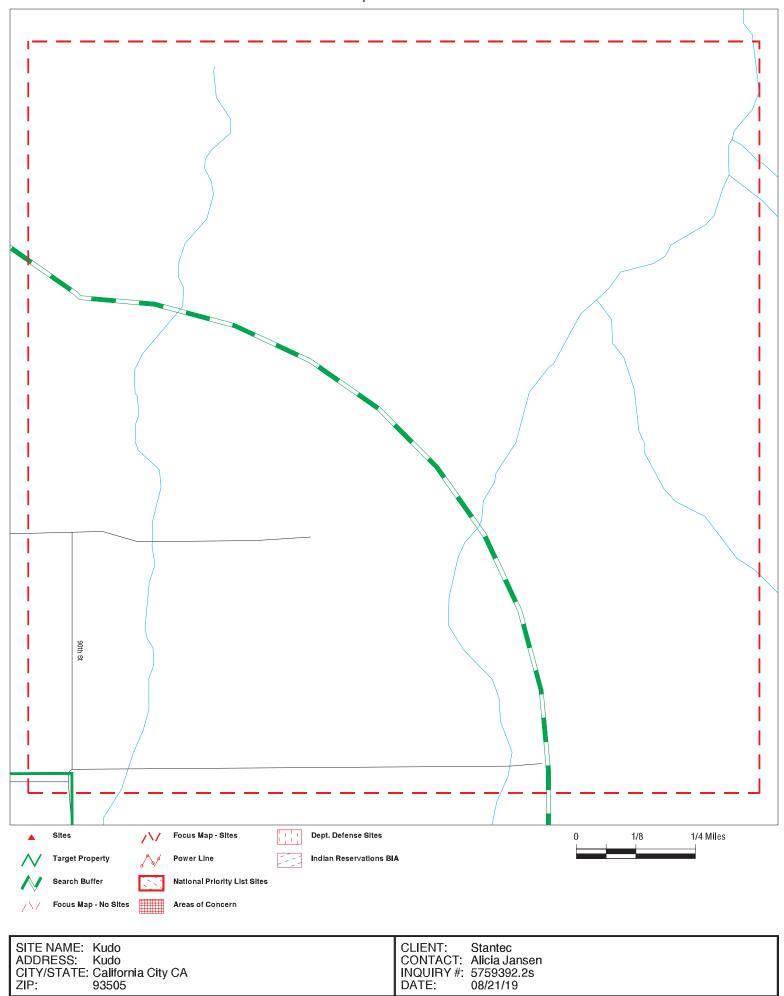
DATE:

#### MAPPED SITES SUMMARY - FOCUS MAP 3

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

NO MAPPED SITES FOUND



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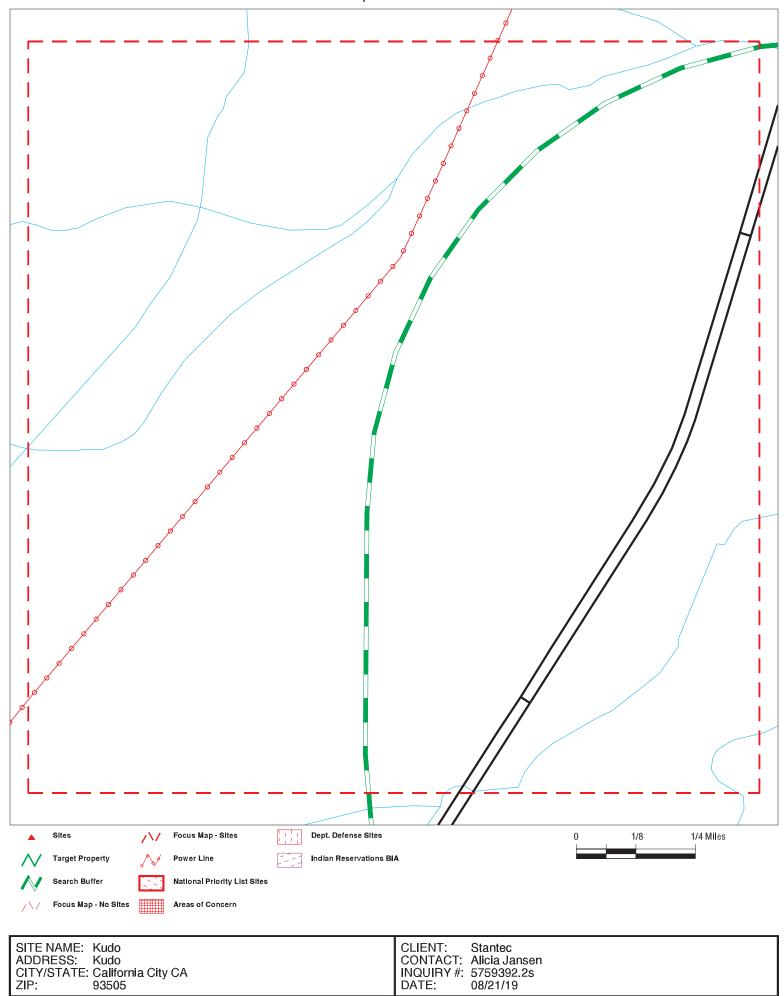
DATE:

#### MAPPED SITES SUMMARY - FOCUS MAP 4

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

NO MAPPED SITES FOUND



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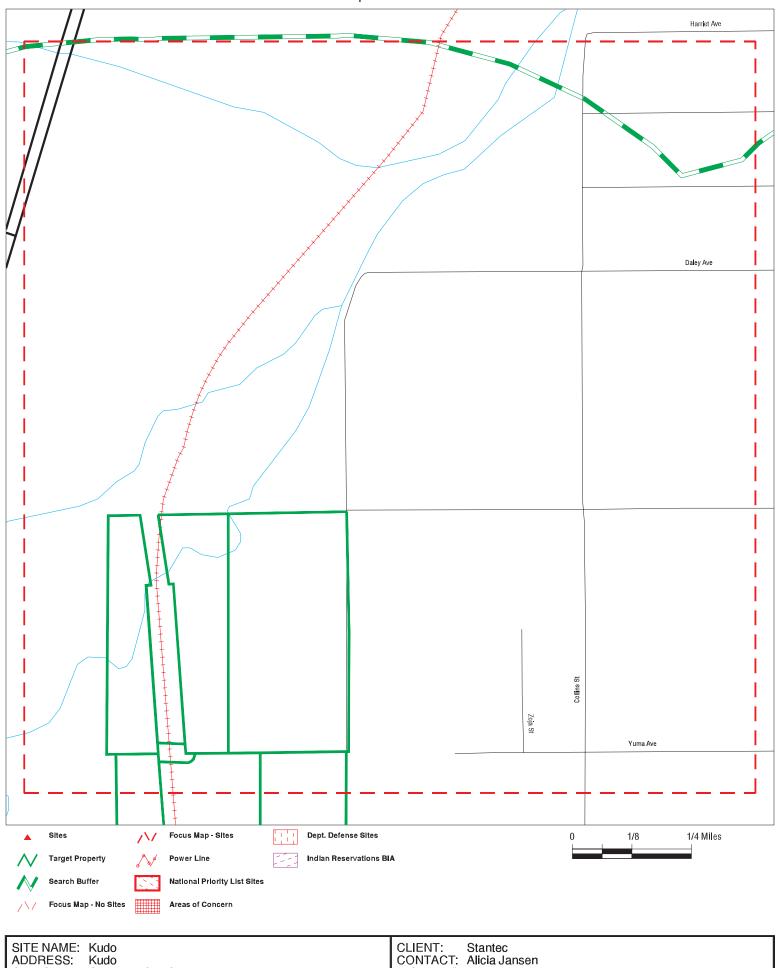
#### MAPPED SITES SUMMARY - FOCUS MAP 5

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

NO MAPPED SITES FOUND

Focus Map - 6 - 5759392.2s



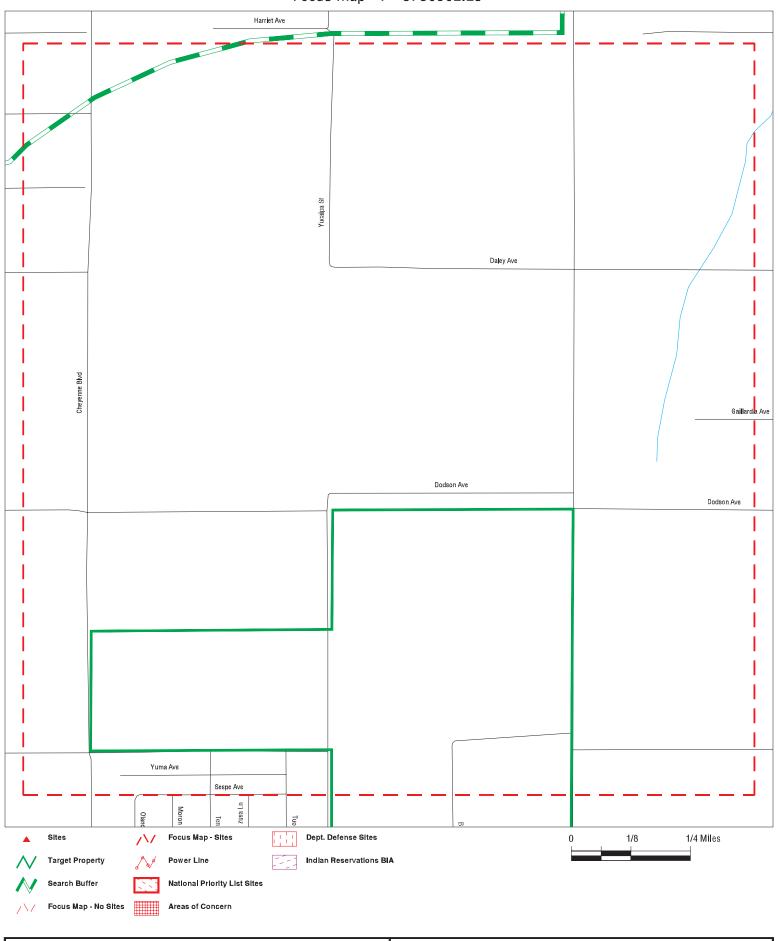
CITY/STATE: California City CA ZIP: 93505

CLIENT: Stantec CONTACT: Alicia Jansen INQUIRY#: 5759392.2s DATE: 08/21/19

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

# Focus Map - 7 - 5759392.2s



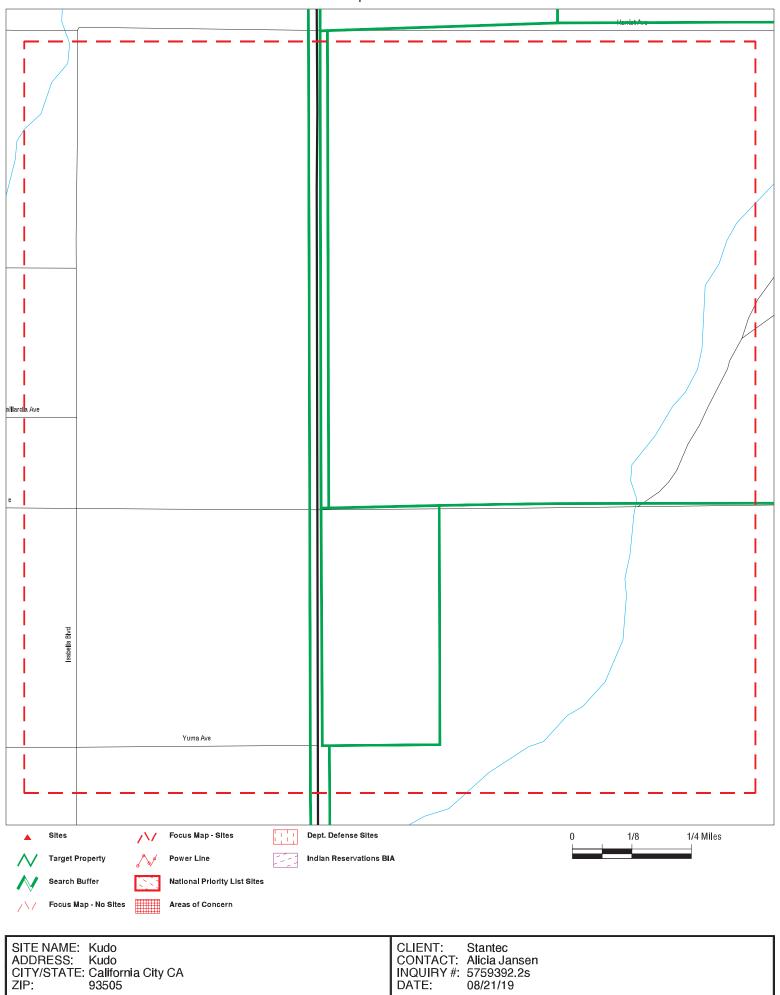
SITE NAME: Kudo ADDRESS: Kudo

CITY/STATE: California City CA ZIP: 93505 CLIENT: Stantec CONTACT: Alicia Jansen INQUIRY#: 5759392.2s DATE: 08/21/19

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.) FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

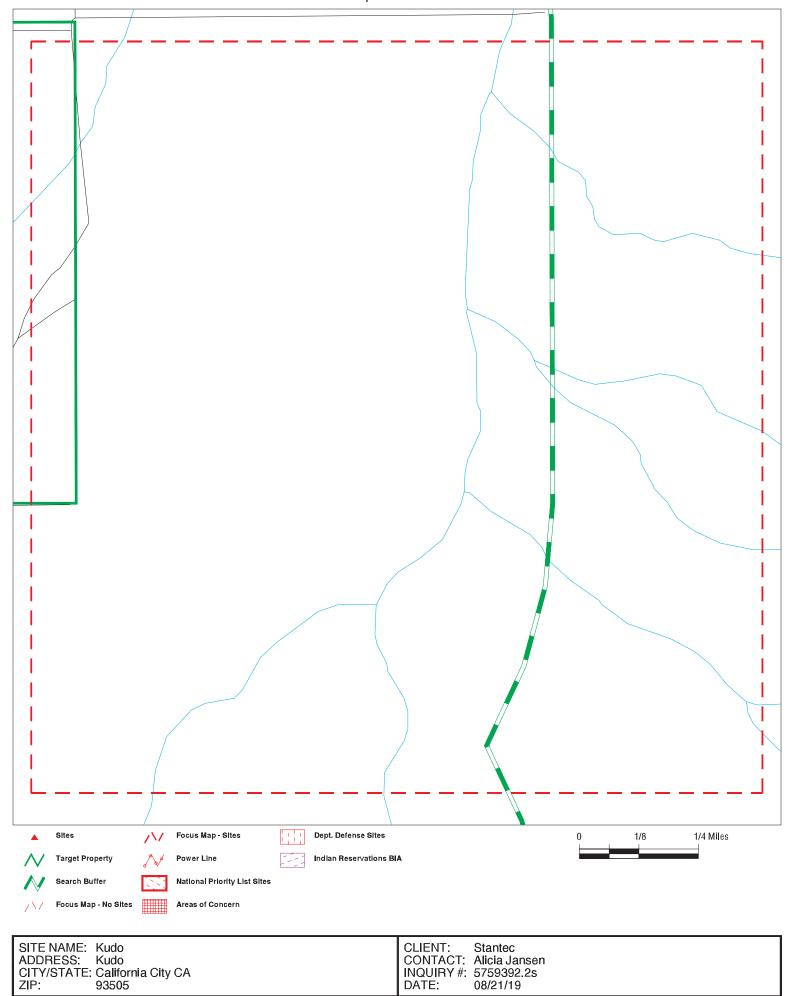
Focus Map - 8 - 5759392.2s



CLIENT: Stantec CONTACT: Alicia Jansen INQUIRY#: 5759392.2s DATE: 08/21/19

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION



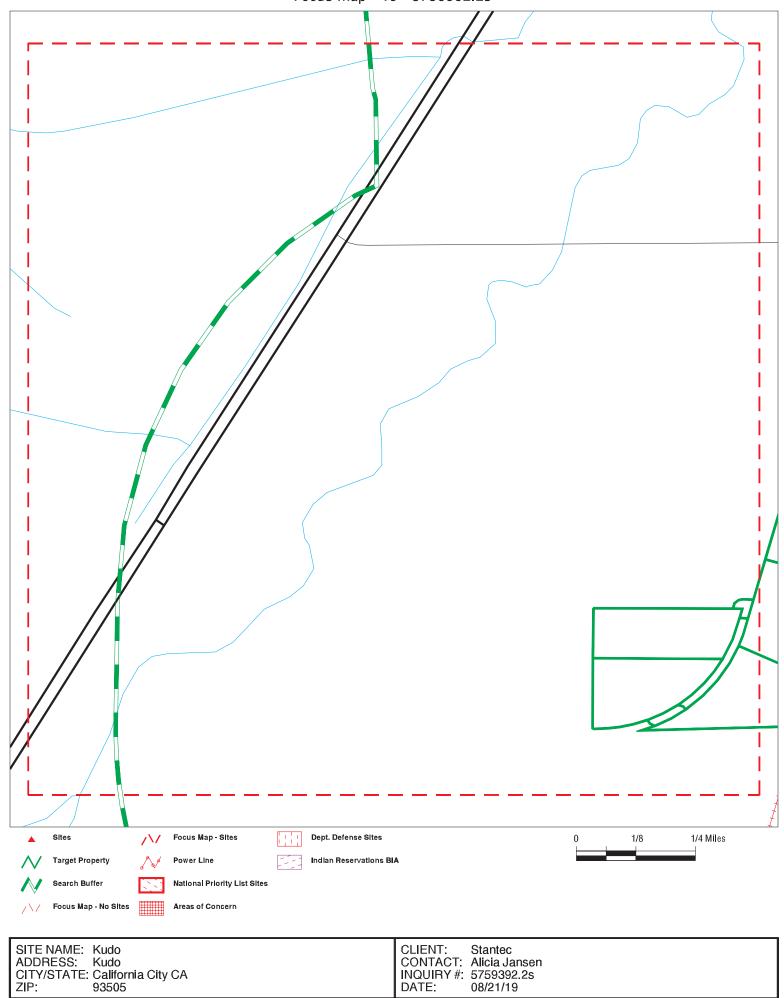
Copyright © 2019 EDR, Inc. © 2015 TomTom Rel. 2015.

08/21/19

DATE:

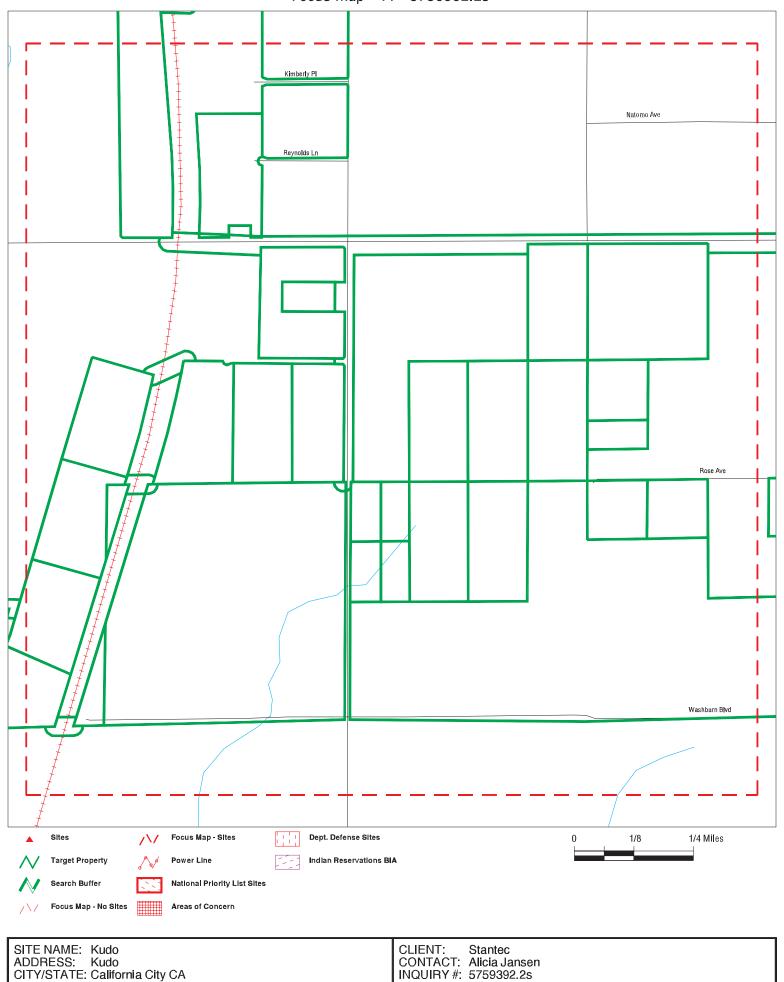
Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION



Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION



93505

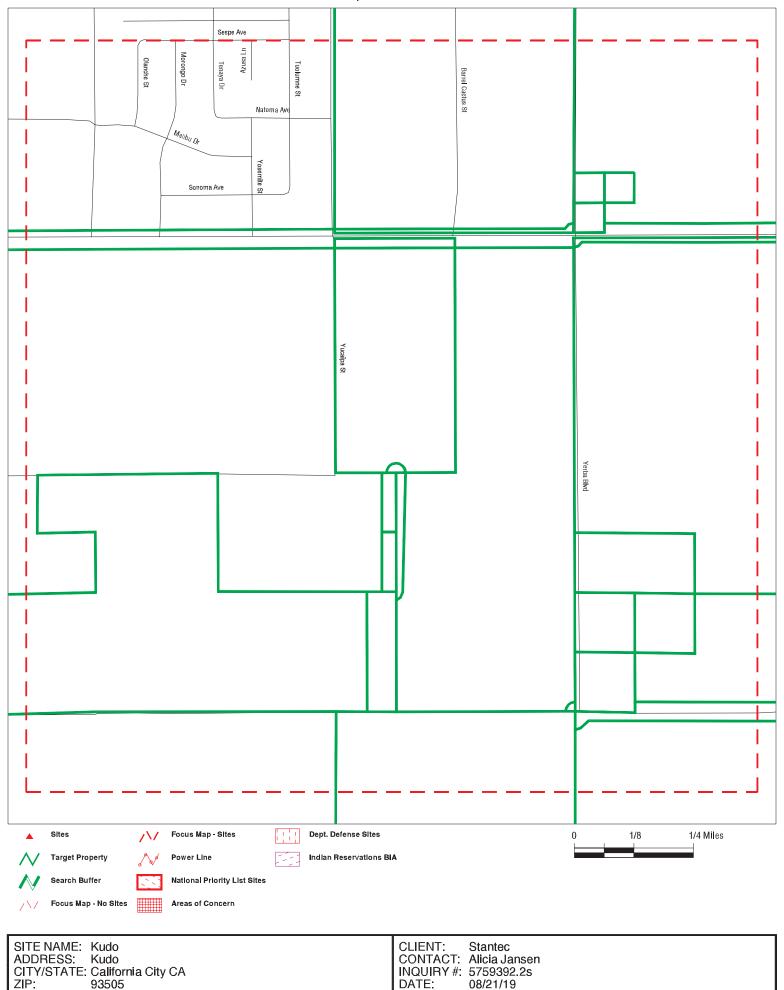
08/21/19
Copyright © 2019 EDR, Inc. © 2015 TomTom Rel. 2015.

DATE:

Target Property: KUDO CALIFORNIA CITY, CA 93505

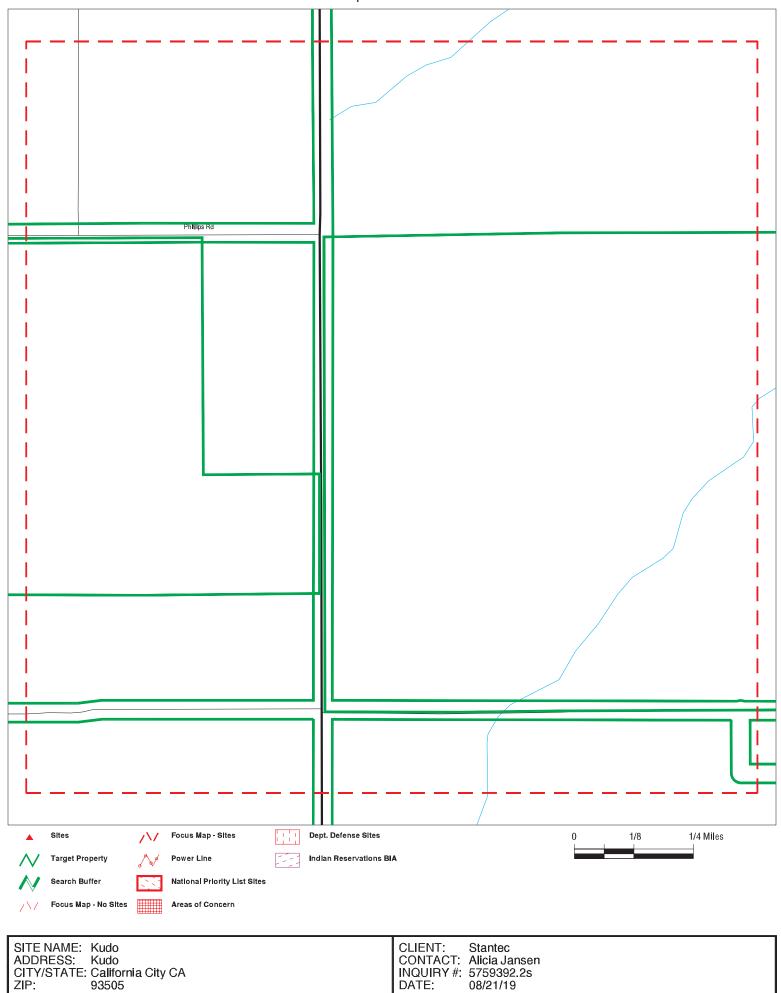
MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

# Focus Map - 12 - 5759392.2s



Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

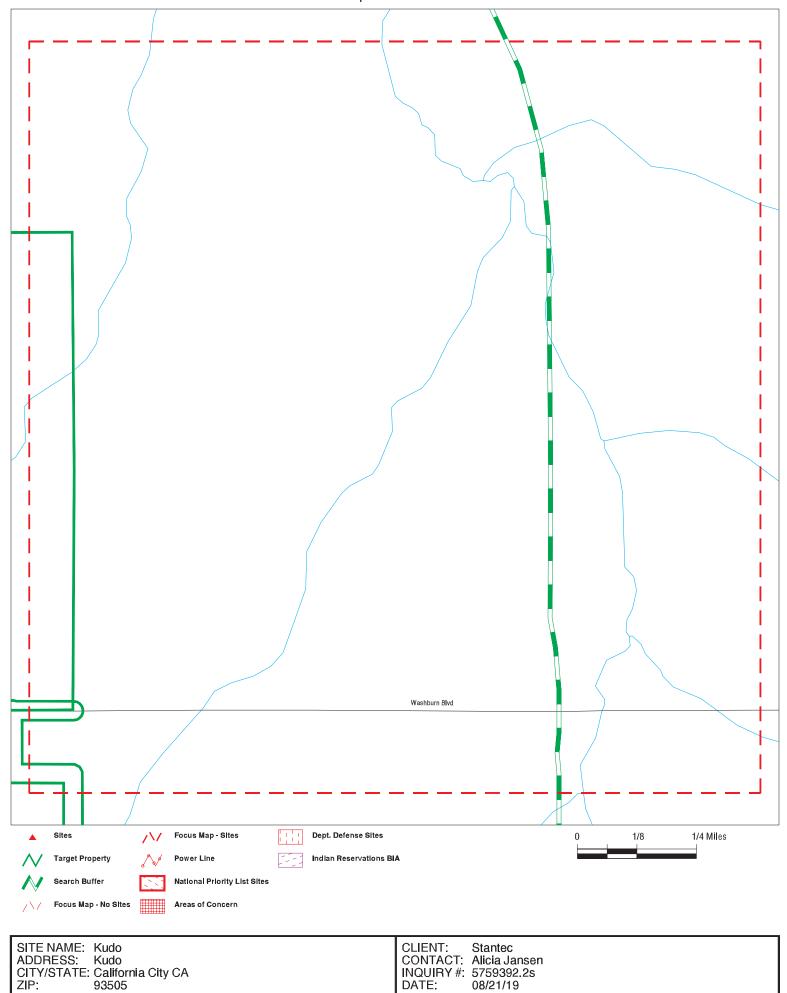


08/21/19

DATE:

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.) FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

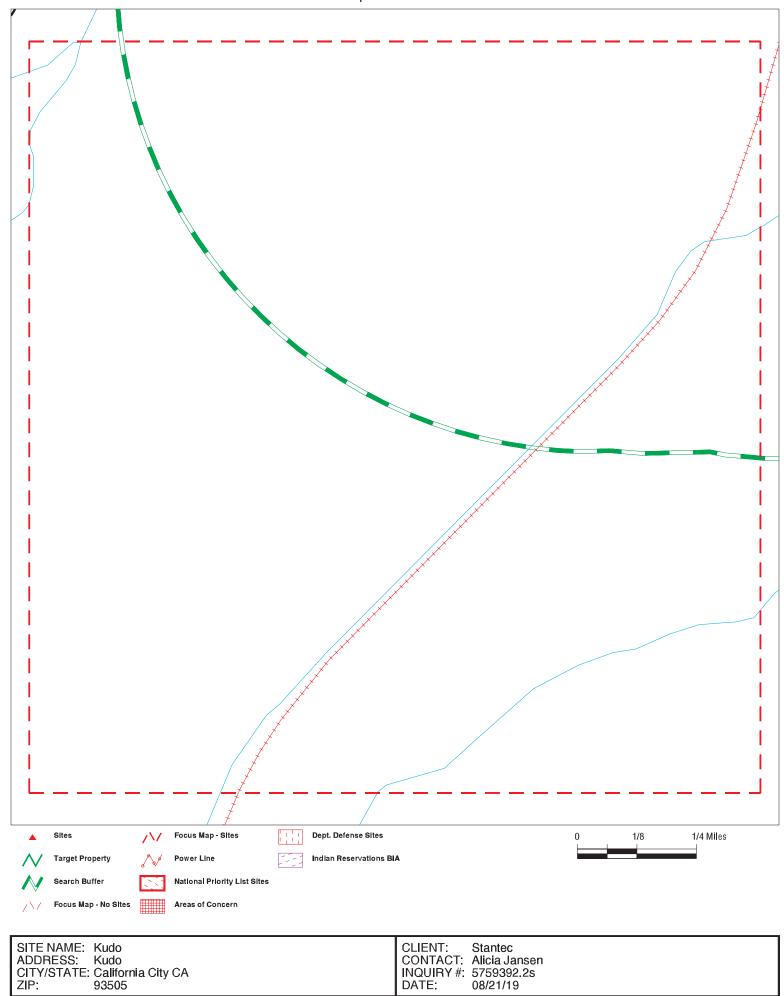


DATE: 08/21/19

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Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION



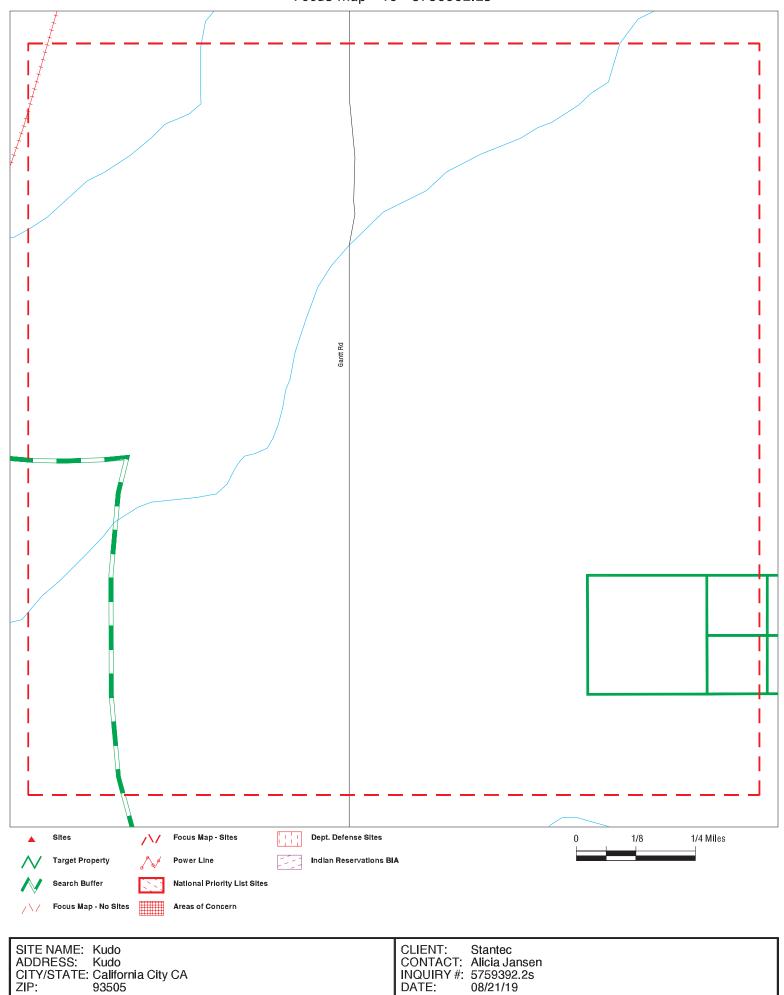
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08/21/19

DATE:

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

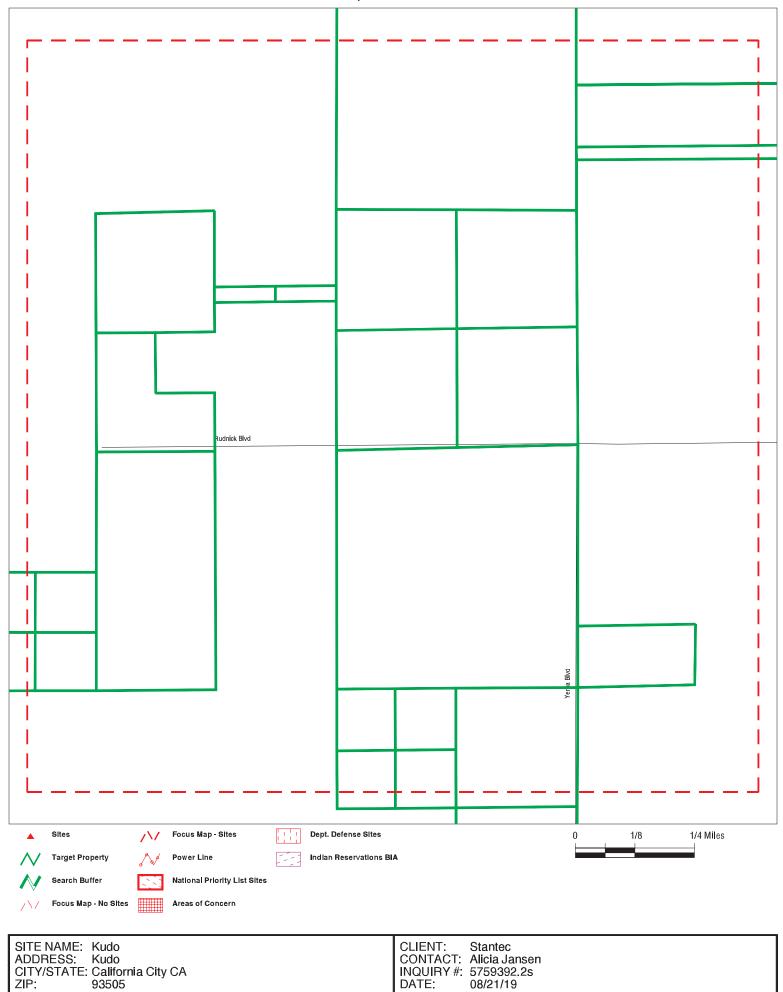


08/21/19

DATE:

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION



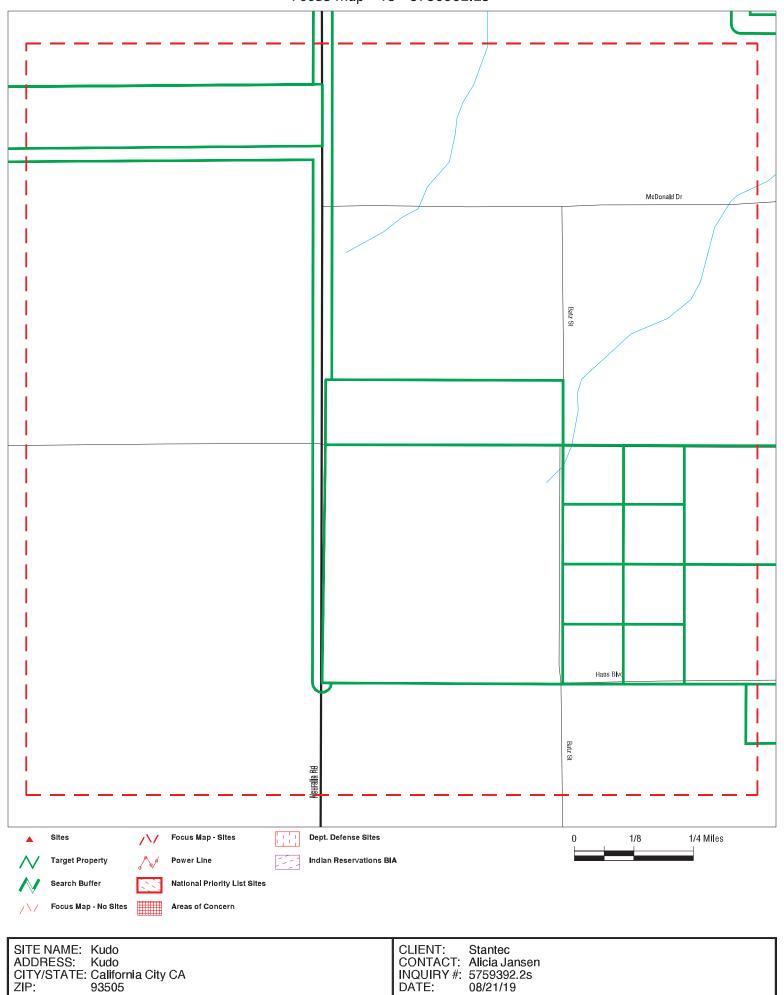
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08/21/19

DATE:

Target Property: KUDO CALIFORNIA CITY, CA 93505

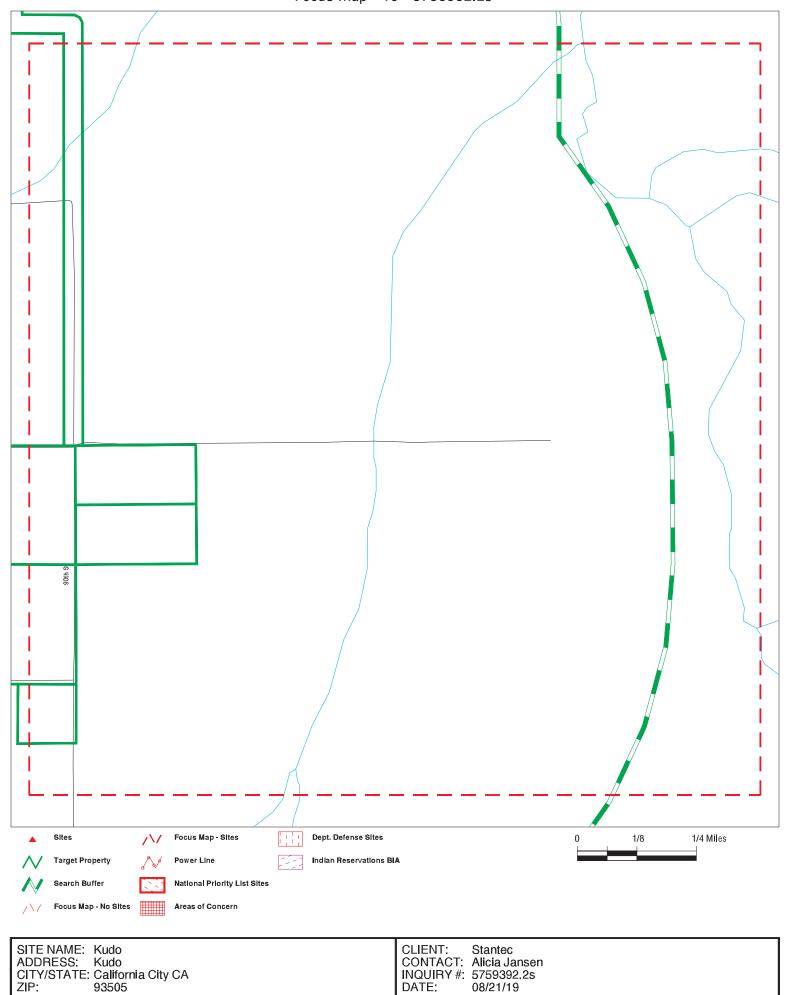
MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION



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Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

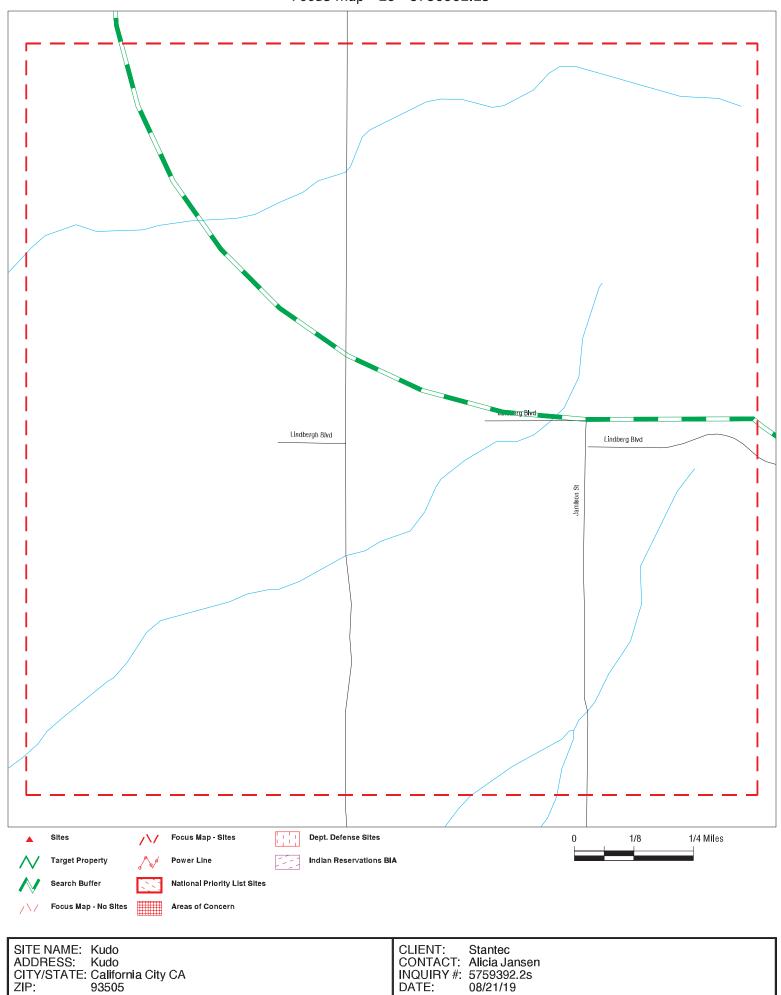


DATE: 08/21/19

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Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION



DATE: 08/21/19 Copyright © 2019 EDR, Inc. © 2015 TomTom Rel. 2015.

INQUIRY#: 5759392.2s

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.) FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

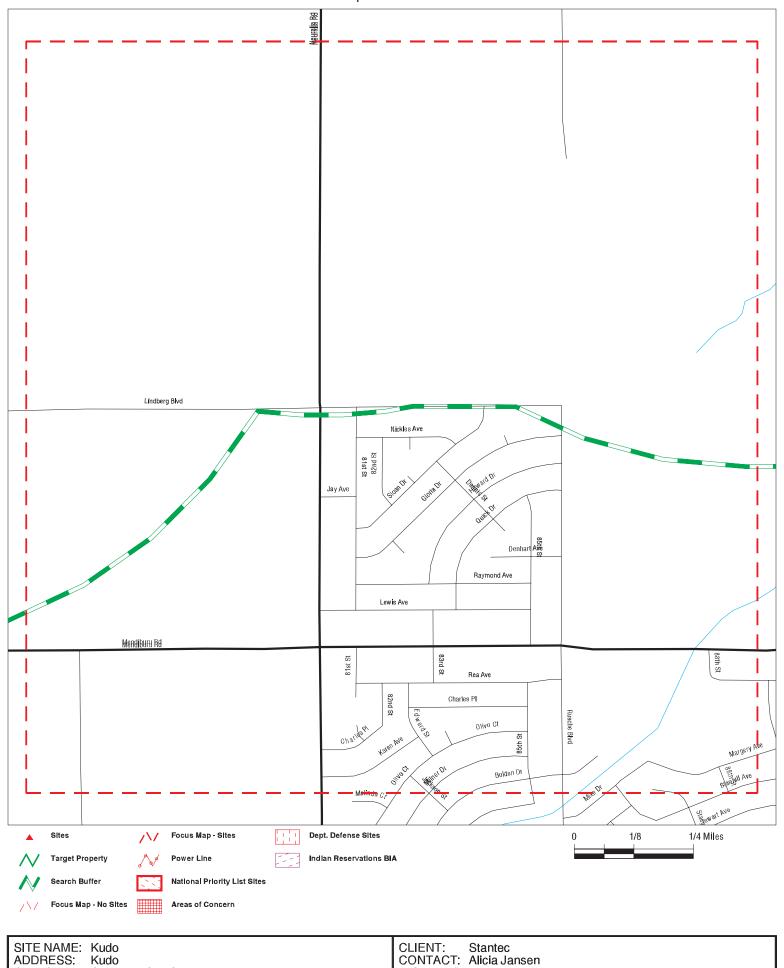


SITE NAME: Kudo ADDRESS: Kudo

CITY/STATE: California City CA ZIP: 93505 CLIENT: Stantec CONTACT: Alicia Jansen INQUIRY#: 5759392.2s DATE: 08/21/19

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

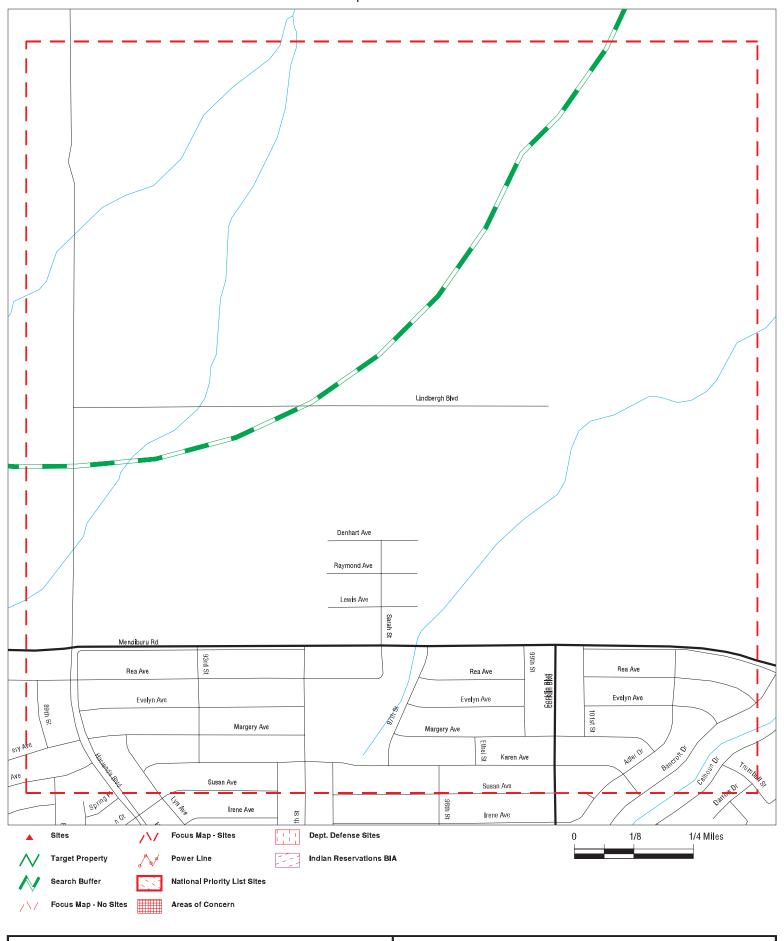


93505 DATE. 00/21/19

CITY/STATE: California City CA ZIP: 93505 CONTACT: Alicia Jansen INQUIRY #: 5759392.2s DATE: 08/21/19

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.) FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION



SITE NAME: Kudo ADDRESS: Kudo

CITY/STATE: California City CA ZIP: 93505 CLIENT: Stantec CONTACT: Alicia Jansen INQUIRY#: 5759392.2s DATE: 08/21/19

Target Property: KUDO CALIFORNIA CITY, CA 93505

MAP ID / DIST (ft. & mi.)
FOCUS MAP SITE NAME ADDRESS DATABASE ACRONYMS DIRECTION

| Map ID         | MAP FINDINGS |             |               |
|----------------|--------------|-------------|---------------|
| Direction      |              |             |               |
| Distance       |              |             | EDR ID Number |
| Elevation Site |              | Database(s) | EPA ID Number |

NO SITES FOUND

| ERN COUNTY 901704  ERN COUNTY 9164674  ERN COUNTY S105637059  ERN COUNTY S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OJAVE OJAVE S106389830 OIL FIELD OJAVE S106389830 TILLOW SPRINGS RD. A S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS   | City  CALIFORNIA CITY CALIFORNIA CITY CALIFORNIA CITY CALIFORNIA CITY CANTIL | S114001219<br>S105647245<br>S123302467<br>S123302467<br>S123654065<br>S123654065<br>A100417087<br>1024788890<br>1017391655<br>1023240651<br>1023375763<br>1023375763<br>1023375763<br>S118210096<br>S118210096<br>S123616932<br>S123592772 | Site Name  MJ UNLIMITED  MENDIBURU RD CAL CITY HIGH SCHOOL  AMERICAN HONDA MOTOR CO, INC  AMERICAN HONDA MOTOR CO INC  AMERICAN HONDA MOTOR CO, INC  AMERICAN HONDA MOTOR CO, INC  AMERICAN HONDA MOTOR CO, INC  ARCIERO RANCHES  SPRINGBOK 1 SOLAR FARM  SPRINGBOK 2 SOLAR FARM  AMERICAN HONDA MOTOR CO, INC.  AMERICAN HONDA MOTOR CO, INC.  AMERICAN HONDA MOTOR CO, INC. |  | Site Address  NORTH LOOP BLVD BETWEEN HACIENDA AND 90TH STREETS 90TH CALIFORNIA CITY BLVD  MARIAN WAY AND COLLINS BLVD  MENDIBURU RD FROM YERBA BLVD TO RUSCHE B 30216 NEURALIA RD 30216 NEURALIA RD 30216 NEURALIA RD 30216 NEURALIA RD 2999 NEURALIA RD 29977 NEURALIA RD 30216 NEURALIA RD | A BLVD HA  |
|---|---|--|---|--|---|--|
| S121655061 MENDIBURU RD CAL CITY HIGH SCHOOL 1016954065 AMERICAN HONDA MOTOR CO, INC A100417087 AMERICAN HONDA MOTOR CO, INC. 1024788890 AMERICAN HONDA MOTOR CO INC 1017391655 AMERICAN HONDA MOTOR CO, INC 1023240651 AMERICAN HONDA MOTOR CO, INC. 102339926 ARCIERO RANCHES 1023375763 SPRINGBOK 1 SOLAR FARM 1023375763 SPRINGBOK 2 SOLAR FARM S118210096 AMERICAN HONDA MOTOR CO,, INC. S123616932 AMERICAN HONDA MOTOR CO INC S123592772 AMERICAN HONDA MOTOR CO,, INC. 901704 9164674 S105637059 S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OIL FIELD S106389830 S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS |   | S114001219<br>S105647245<br>S123302467   | •   | NORTH LOOP BLVI 90TH CALIFORNIA                          | LVD A   | N HACIENDA AND 90TH STREETS 93505<br>93505<br>93505<br>93505 |
| S12165961 MENDBURU RD CAL CITY HIGH SCHOOL 1016954065 AMERICAN HONDA MOTOR CO, INC A100417087 AMERICAN HONDA MOTOR CO, INC. 1024788890 AMERICAN HONDA MOTOR CO, INC 107391655 AMERICAN HONDA MOTOR CO, INC 1023240651 AMERICAN HONDA MOTOR CO, INC 102339926 ARCIERO RANCHES 1023375763 SPRINGBOK 1 SOLAR FARM 1023354486 SPRINGBOK 2 SOLAR FARM 5118210096 AMERICAN HONDA MOTOR CO., INC. S123616932 AMERICAN HONDA MOTOR CO INC S123582772 AMERICAN HONDA MOTOR CO, INC. 901704 9164674 S106389830 S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS   |   | S123302467   | •   | MARIAN WAY AND   | COLLINS BLVD  | 93505  |
| A100417087 AMERICAN HONDA MOTOR CO., INC. 1024788890 AMERICAN HONDA MOTOR CO INC 1017391655 AMERICAN HONDA MOTOR CO, INC 1023240651 AMERICAN HONDA MOTOR CO.NA INC. 102339926 ARCIERO RANCHES 1023375763 SPRINGBOK 1 SOLAR FARM 1023354486 SPRINGBOK 2 SOLAR FARM S118210096 AMERICAN HONDA MOTOR CO., INC. S123616932 AMERICAN HONDA MOTOR CO INC S123592772 AMERICAN HONDA MOTOR CO., INC. 901704 9164674 S105637059 S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OIL FIELD S106389830 S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS   |   | S121655061<br>1016954065   |   | MENDIBURU RD FF  | OM YERBA BL\  | DM YERBA BLVD TO RUSCHE B 93505<br>93519                     |
| 1024788890 AMERICAN HONDA MOTOR CO INC 1017391655 AMERICAN HONDA MOTOR CO, INC 1023240651 AMERICAN HONDA MOTOR CO.NA INC. 1023309926 ARCIERO RANCHES 1023375763 SPRINGBOK 1 SOLAR FARM 1023354486 SPRINGBOK 2 SOLAR FARM S118210096 AMERICAN HONDA MOTOR CO., INC. S123616932 AMERICAN HONDA MOTOR CO INC S123592772 AMERICAN HONDA MOTOR CO., INC. 901704 9164674 S105637059 S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OIL FIELD S106389830 S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS  |   | A100417087   | ' AMERICAN HONDA MOTOR CO., INC.  | 30216 NEURALIA R   | D   | 93519  |
| 1017391655 AMERICAN HONDA MOTOR CO, INC 1023240651 AMERICAN HONDA MOTOR CO.NA INC. 1023309926 ARCIERO RANCHES 1023375763 SPRINGBOK 1 SOLAR FARM 1023354486 SPRINGBOK 2 SOLAR FARM S118210096 AMERICAN HONDA MOTOR CO., INC. S123616932 AMERICAN HONDA MOTOR CO INC S123592772 AMERICAN HONDA MOTOR CO., INC. 901704 9164674 S105637059 S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OIL FIELD S106389830 S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS   |   | 1024788890   | AMERICAN HONDA MOTOR CO INC   | 30216 NEURALIA RI  | O   | 93519  |
| 1023240651 AMERICAN HONDA MOTOR CO.NA INC. 1023309926 ARCIERO RANCHES 1023375763 SPRINGBOK 1 SOLAR FARM 1023354486 SPRINGBOK 2 SOLAR FARM S118210096 AMERICAN HONDA MOTOR CO., INC. S123616932 AMERICAN HONDA MOTOR CO INC S123592772 AMERICAN HONDA MOTOR CO., INC. 20UNTY 901704 20UNTY 9164674 20UNTY S105637059 S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OUNTY S16389830 V SPRINGS RD. A S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS   | F   | 1017391655   |   | 30216 NEURALIA RD  |   | _  |
| 1023309926 ARCIERO RANCHES 1023375763 SPRINGBOK 1 SOLAR FARM 1023354486 SPRINGBOK 2 SOLAR FARM S118210096 AMERICAN HONDA MOTOR CO., INC. S123616932 AMERICAN HONDA MOTOR CO INC S123592772 AMERICAN HONDA MOTOR CO., INC. 20UNTY 901704 20UNTY 9164674 20UNTY S105637059 S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OUNTY S16389830 V SPRINGS RD. A S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS  | ANTIL   | 1023240651   | AMERICAN HONDA MOTOR CO.NA INC.   | 30216 NEURALIA RD  |   | _  |
| 1023375763 SPRINGBOK 1 SOLAR FARM 1023354486 SPRINGBOK 2 SOLAR FARM S118210096 AMERICAN HONDA MOTOR CO., INC. S123616932 AMERICAN HONDA MOTOR CO INC S123592772 AMERICAN HONDA MOTOR CO., INC. OUNTY 901704 OUNTY 9164674 COUNTY S105637059 SOUNTY S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OUNTY VSPRINGS RD. A S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS   | ANTIL   | 1023309926   |   | 1200 NEURALIA  |   | w  |
| 1023354486 SPRINGBOK 2 SOLAR FARM S118210096 AMERICAN HONDA MOTOR CO., INC. S123616932 AMERICAN HONDA MOTOR CO INC S123592772 AMERICAN HONDA MOTOR CO., INC. COUNTY 901704 COUNTY 9164674 COUNTY S105637059 SOUNTY S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OUNTY V SPRINGS RD. A S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS  | ANTIL   | 1023375763   |   | 29999 NEURALIA RD  |   | 93519  |
| \$118210096 AMERICAN HONDA MOTOR CO., INC. \$123616932 AMERICAN HONDA MOTOR CO INC \$123592772 AMERICAN HONDA MOTOR CO., INC. \$20UNTY 901704 \$20UNTY 9164674 \$20UNTY \$105637059 \$20UNTY \$120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OIL FIELD E \$106389830 V \$PRINGS RD. A \$123729997 1X SIGITAS F. AND DANUTE S. BABUSIS   | ANTIL   | 1023354486   |   | 29977 NEURALIA RD  |   | 9  |
| S123616932 AMERICAN HONDA MOTOR CO INC S123592772 AMERICAN HONDA MOTOR CO., INC.  DUNTY 901704 9164674  DUNTY S105637059 S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OIL FIELD S106389830 SPRINGS RD. A S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS   | CANTIL  | S118210096   |   | 30216 NEURALIA RO  | )AD   | 93519  |
| \$123592772 AMERICAN HONDA MOTOR CO., INC.  DUNTY 901704  DUNTY 9164674  S105637059  S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OIL FIELD  \$106389830  SPRINGS RD. A \$123729997 1X SIGITAS F. AND DANUTE S. BABUSIS   | CANTIL  | S123616932   |   | 30216 NEURALIA RI  | O   | 93519  |
| DUNTY       901704         DUNTY       9164674         DUNTY       \$105637059         DUNTY       \$120028234       E&B, DRILLING SUMPS, MCDONALD ANTICLINE         OIL FIELD       \$106389830         SPRINGS RD. A       \$123729997       1X SIGITAS F. AND DANUTE S. BABUSIS  | CANTIL  | S123592772   |   | 30216 NEURALIA R   | OAD   | 93519  |
| DUNTY       9164674         DUNTY       \$105637059         DUNTY       \$120028234       E&B, DRILLING SUMPS, MCDONALD ANTICLINE         OIL FIELD       \$106389830         SPRINGS RD. A       \$123729997       1X SIGITAS F. AND DANUTE S. BABUSIS   | KERN COUNTY   | 901704   |   | SOUTH OF BUTE LA ROSE ON                                 | A ROSE ON   | A ROSE ON ERNS   |
| DUNTY       \$105637059         DUNTY       \$120028234       E&B, DRILLING SUMPS, MCDONALD ANTICLINE         OIL FIELD       \$106389830         SPRINGS RD. A       \$123729997       1X SIGITAS F. AND DANUTE S. BABUSIS   | KERN COUNTY   | 9164674  |   | MOBIL ROSE STATION                                       | TION  | TION ERNS  |
| SUNTY S120028234 E&B, DRILLING SUMPS, MCDONALD ANTICLINE OIL FIELD S106389830 SPRINGS RD. A S123729997 1X SIGITAS F. AND DANUTE S. BABUSIS  | KERN COUNTY   | S105637059   |   | PHILLIPS LAB SEV   | PHILLIPS LAB SEWAGE PLANT EDWARDS AFB   | VAGE PLANT EDWARDS AFB                                       |
| \$106389830<br>SPRINGS RD. A \$123729997 1X SIGITAS F. AND DANUTE S. BABUSIS  | KERN COUNTY   | S120028234   |   | MCDONALD ANTICLINE OIL FIELD                             | LINE OIL FIELD  | LINE OIL FIELD   |
|   | MOJAVE<br>WILLOW SPRINGS RD. A  |  |   | KERN CO AQUA DUCT,BETWEEN OFF OF 90TH WEST, 2 MI. NO. OF | UCT,BETWEEN CAL CITY ISABELLA AND MOJAVE<br>ST, 2 MI. NO. OF  |  |

To maintain currency of the following federal and state databases, EDR contacts the appropriate governmental agency on a monthly or quarterly basis, as required.

**Number of Days to Update:** Provides confirmation that EDR is reporting records that have been updated within 90 days from the date the government agency made the information available to the public.

NPL: National Priority List

National Priorities List (Superfund). The NPL is a subset of CERCLIS and identifies over 1,200 sites for priority cleanup under the Superfund Program. NPL sites may encompass relatively large areas. As such, EDR provides polygon coverage for over 1,000 NPL site boundaries produced by EPA's Environmental Photographic Interpretation Center (EPIC) and regional EPA offices.

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/18/2019 Date Made Active in Reports: 05/14/2019

Number of Days to Update: 26

Source: EPA
Telephone: N/A

Last EDR Contact: 07/02/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Quarterly

**NPL Site Boundaries** 

Sources:

EPA's Environmental Photographic Interpretation Center (EPIC)

Telephone: 202-564-7333

EPA Region 1 EPA Region 6

Telephone 617-918-1143 Telephone: 214-655-6659

EPA Region 3 EPA Region 7

Telephone 215-814-5418 Telephone: 913-551-7247

EPA Region 4 EPA Region 8

Telephone 404-562-8033 Telephone: 303-312-6774

EPA Region 5 EPA Region 9

Telephone 312-886-6686 Telephone: 415-947-4246

EPA Region 10

Telephone 206-553-8665

Proposed NPL: Proposed National Priority List Sites

A site that has been proposed for listing on the National Priorities List through the issuance of a proposed rule in the Federal Register. EPA then accepts public comments on the site, responds to the comments, and places on the NPL those sites that continue to meet the requirements for listing.

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/18/2019 Date Made Active in Reports: 05/14/2019

Number of Days to Update: 26

Source: EPA Telephone: N/A

Last EDR Contact: 07/02/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Quarterly

NPL LIENS: Federal Superfund Liens

Federal Superfund Liens. Under the authority granted the USEPA by CERCLA of 1980, the USEPA has the authority to file liens against real property in order to recover remedial action expenditures or when the property owner received notification of potential liability. USEPA compiles a listing of filed notices of Superfund Liens.

Date of Government Version: 10/15/1991 Date Data Arrived at EDR: 02/02/1994 Date Made Active in Reports: 03/30/1994

Number of Days to Update: 56

Source: EPA Telephone: 202-564-4267 Last EDR Contact: 08/15/2011

Next Scheduled EDR Contact: 11/28/2011 Data Release Frequency: No Update Planned

Delisted NPL: National Priority List Deletions

The National Oil and Hazardous Substances Pollution Contingency Plan (NCP) establishes the criteria that the EPA uses to delete sites from the NPL. In accordance with 40 CFR 300.425.(e), sites may be deleted from the NPL where no further response is appropriate.

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/18/2019 Date Made Active in Reports: 05/14/2019

Number of Days to Update: 26

Source: EPA Telephone: N/A

Last EDR Contact: 07/02/2019 Next Scheduled EDR Contact: 10/14/2019

Next Scheduled EDR Contact: 10/14/201
Data Release Frequency: Quarterly

FEDERAL FACILITY: Federal Facility Site Information listing

A listing of National Priority List (NPL) and Base Realignment and Closure (BRAC) sites found in the Comprehensive Environmental Response, Compensation and Liability Information System (CERCLIS) Database where EPA Federal Facilities Restoration and Reuse Office is involved in cleanup activities.

Date of Government Version: 04/03/2019
Date Data Arrived at EDR: 04/05/2019
Date Made Active in Reports: 05/14/2019

Number of Days to Update: 39

Source: Environmental Protection Agency

Telephone: 703-603-8704 Last EDR Contact: 07/03/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Varies

SEMS: Superfund Enterprise Management System

SEMS (Superfund Enterprise Management System) tracks hazardous waste sites, potentially hazardous waste sites, and remedial activities performed in support of EPA's Superfund Program across the United States. The list was formerly know as CERCLIS, renamed to SEMS by the EPA in 2015. The list contains data on potentially hazardous waste sites that have been reported to the USEPA by states, municipalities, private companies and private persons, pursuant to Section 103 of the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA). This dataset also contains sites which are either proposed to or on the National Priorities List (NPL) and the sites which are in the screening and assessment phase for possible inclusion on the NPL.

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/18/2019 Date Made Active in Reports: 05/23/2019

Number of Days to Update: 35

Source: EPA

Telephone: 800-424-9346 Last EDR Contact: 07/02/2019

Next Scheduled EDR Contact: 10/28/2019 Data Release Frequency: Quarterly

SEMS-ARCHIVE: Superfund Enterprise Management System Archive

SEMS-ARCHIVE (Superfund Enterprise Management System Archive) tracks sites that have no further interest under the Federal Superfund Program based on available information. The list was formerly known as the CERCLIS-NFRAP, renamed to SEMS ARCHIVE by the EPA in 2015. EPA may perform a minimal level of assessment work at a site while it is archived if site conditions change and/or new information becomes available. Archived sites have been removed and archived from the inventory of SEMS sites. Archived status indicates that, to the best of EPA's knowledge, assessment at a site has been completed and that EPA has determined no further steps will be taken to list the site on the National Priorities List (NPL), unless information indicates this decision was not appropriate or other considerations require a recommendation for listing at a later time. The decision does not necessarily mean that there is no hazard associated with a given site; it only means that. based upon available information, the location is not judged to be potential NPL site.

Date of Government Version: 04/11/2019
Date Data Arrived at EDR: 04/18/2019
Date Made Active in Reports: 05/23/2019

Number of Days to Update: 35

Source: EPA

Telephone: 800-424-9346 Last EDR Contact: 07/02/2019

Next Scheduled EDR Contact: 10/28/2019 Data Release Frequency: Quarterly

CORRACTS: Corrective Action Report

CORRACTS identifies hazardous waste handlers with RCRA corrective action activity.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/27/2019 Date Made Active in Reports: 04/17/2019

Number of Days to Update: 21

Source: EPA

Telephone: 800-424-9346 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

#### RCRA-TSDF: RCRA - Treatment, Storage and Disposal

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Transporters are individuals or entities that move hazardous waste from the generator offsite to a facility that can recycle, treat, store, or dispose of the waste. TSDFs treat, store, or dispose of the waste.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/27/2019 Date Made Active in Reports: 04/17/2019

Number of Days to Update: 21

Source: Environmental Protection Agency

Telephone: (415) 495-8895 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

### RCRA-LQG: RCRA - Large Quantity Generators

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Large quantity generators (LQGs) generate over 1,000 kilograms (kg) of hazardous waste, or over 1 kg of acutely hazardous waste per month.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/27/2019 Date Made Active in Reports: 04/17/2019

Number of Days to Update: 21

Source: Environmental Protection Agency

Telephone: (415) 495-8895 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

#### RCRA-SQG: RCRA - Small Quantity Generators

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Small quantity generators (SQGs) generate between 100 kg and 1,000 kg of hazardous waste per month.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/27/2019 Date Made Active in Reports: 04/17/2019

Number of Days to Update: 21

Source: Environmental Protection Agency

Telephone: (415) 495-8895 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

### RCRA-CESQG: RCRA - Conditionally Exempt Small Quantity Generators

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Conditionally exempt small quantity generators (CESQGs) generate less than 100 kg of hazardous waste, or less than 1 kg of acutely hazardous waste per month.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/27/2019 Date Made Active in Reports: 04/17/2019

Number of Days to Update: 21

Source: Environmental Protection Agency

Telephone: (415) 495-8895 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

### LUCIS: Land Use Control Information System

LUCIS contains records of land use control information pertaining to the former Navy Base Realignment and Closure properties.

Date of Government Version: 02/22/2019 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 04/17/2019

Number of Days to Update: 41

Source: Department of the Navy Telephone: 843-820-7326 Last EDR Contact: 05/10/2019

Next Scheduled EDR Contact: 08/26/2019 Data Release Frequency: Varies

#### US ENG CONTROLS: Engineering Controls Sites List

A listing of sites with engineering controls in place. Engineering controls include various forms of caps, building foundations, liners, and treatment methods to create pathway elimination for regulated substances to enter environmental media or effect human health.

Date of Government Version: 01/31/2019 Date Data Arrived at EDR: 02/04/2019 Date Made Active in Reports: 03/08/2019

Number of Days to Update: 32

Source: Environmental Protection Agency

Telephone: 703-603-0695 Last EDR Contact: 05/29/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: Varies

#### US INST CONTROL: Sites with Institutional Controls

A listing of sites with institutional controls in place. Institutional controls include administrative measures, such as groundwater use restrictions, construction restrictions, property use restrictions, and post remediation care requirements intended to prevent exposure to contaminants remaining on site. Deed restrictions are generally required as part of the institutional controls.

Date of Government Version: 01/31/2019 Date Data Arrived at EDR: 02/04/2019 Date Made Active in Reports: 03/08/2019

Number of Days to Update: 32

Source: Environmental Protection Agency

Telephone: 703-603-0695 Last EDR Contact: 05/29/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: Varies

### ERNS: Emergency Response Notification System

Emergency Response Notification System. ERNS records and stores information on reported releases of oil and hazardous substances.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/26/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 36

Source: National Response Center, United States Coast Guard

Telephone: 202-267-2180 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

#### STANDARD ENVIRONMENTAL RECORDS

#### State- and tribal - equivalent NPL

### CA RESPONSE: State Response Sites

Identifies confirmed release sites where DTSC is involved in remediation, either in a lead or oversight capacity. These confirmed release sites are generally high-priority and high potential risk.

Date of Government Version: 04/29/2019 Date Data Arrived at EDR: 04/30/2019 Date Made Active in Reports: 06/27/2019

Number of Days to Update: 58

Source: Department of Toxic Substances Control

Telephone: 916-323-3400 Last EDR Contact: 04/30/2019

Next Scheduled EDR Contact: 08/12/2019
Data Release Frequency: Quarterly

### State- and tribal - equivalent CERCLIS

### CA ENVIROSTOR: EnviroStor Database

The Department of Toxic Substances Control's (DTSC's) Site Mitigation and Brownfields Reuse Program's (SMBRP's) EnviroStor database identifes sites that have known contamination or sites for which there may be reasons to investigate further. The database includes the following site types: Federal Superfund sites (National Priorities List (NPL)); State Response, including Military Facilities and State Superfund; Voluntary Cleanup; and School sites. EnviroStor provides similar information to the information that was available in CalSites, and provides additional site information, including, but not limited to, identification of formerly-contaminated properties that have been released for reuse, properties where environmental deed restrictions have been recorded to prevent inappropriate land uses, and risk characterization information that is used to assess potential impacts to public health and the environment at contaminated sites.

Date of Government Version: 04/29/2019 Date Data Arrived at EDR: 04/30/2019 Date Made Active in Reports: 06/27/2019

Number of Days to Update: 58

Source: Department of Toxic Substances Control

Telephone: 916-323-3400 Last EDR Contact: 04/30/2019

Next Scheduled EDR Contact: 08/12/2019 Data Release Frequency: Quarterly

#### State and tribal landfill and/or solid waste disposal site lists

CA SWF/LF (SWIS): Solid Waste Information System

Active, Closed and Inactive Landfills. SWF/LF records typically contain an inventory of solid waste disposal facilities or landfills. These may be active or inactive facilities or open dumps that failed to meet RCRA Section 4004 criteria for solid waste landfills or disposal sites.

Date of Government Version: 05/13/2019 Date Data Arrived at EDR: 05/14/2019 Date Made Active in Reports: 07/17/2019

Number of Days to Update: 64

Source: Department of Resources Recycling and Recovery

Telephone: 916-341-6320 Last EDR Contact: 05/14/2019

Next Scheduled EDR Contact: 08/26/2019 Data Release Frequency: Quarterly

#### State and tribal leaking storage tank lists

CA LUST REG 6L: Leaking Underground Storage Tank Case Listing

For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 09/09/2003 Date Data Arrived at EDR: 09/10/2003 Date Made Active in Reports: 10/07/2003

Number of Days to Update: 27

Source: California Regional Water Quality Control Board Lahontan Region (6)

Telephone: 530-542-5572 Last EDR Contact: 09/12/2011

Next Scheduled EDR Contact: 12/26/2011
Data Release Frequency: No Update Planned

CA LUST REG 7: Leaking Underground Storage Tank Case Listing

Leaking Underground Storage Tank locations. Imperial, Riverside, San Diego, Santa Barbara counties.

Date of Government Version: 02/26/2004 Date Data Arrived at EDR: 02/26/2004 Date Made Active in Reports: 03/24/2004

Number of Days to Update: 27

Source: California Regional Water Quality Control Board Colorado River Basin Region (7)

Telephone: 760-776-8943 Last EDR Contact: 08/01/2011

Next Scheduled EDR Contact: 11/14/2011 Data Release Frequency: No Update Planned

CA LUST REG 8: Leaking Underground Storage Tanks

California Regional Water Quality Control Board Santa Ana Region (8). For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 02/14/2005 Date Data Arrived at EDR: 02/15/2005 Date Made Active in Reports: 03/28/2005

Number of Days to Update: 41

Source: California Regional Water Quality Control Board Santa Ana Region (8)

Telephone: 909-782-4496 Last EDR Contact: 08/15/2011

Next Scheduled EDR Contact: 11/28/2011 Data Release Frequency: No Update Planned

CA LUST REG 5: Leaking Underground Storage Tank Database

Leaking Underground Storage Tank locations. Alameda, Alpine, Amador, Butte, Colusa, Contra Costa, Calveras, El Dorado, Fresno, Glenn, Kern, Kings, Lake, Lassen, Madera, Mariposa, Merced, Modoc, Napa, Nevada, Placer, Plumas, Sacramento, San Joaquin, Shasta, Solano, Stanislaus, Sutter, Tehama, Tulare, Tuolumne, Yolo, Yuba counties.

Date of Government Version: 07/01/2008 Date Data Arrived at EDR: 07/22/2008 Date Made Active in Reports: 07/31/2008

Number of Days to Update: 9

Source: California Regional Water Quality Control Board Central Valley Region (5)

Telephone: 916-464-4834 Last EDR Contact: 07/01/2011

Next Scheduled EDR Contact: 10/17/2011 Data Release Frequency: No Update Planned

#### CA LUST REG 4: Underground Storage Tank Leak List

Los Angeles, Ventura counties. For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 09/07/2004 Date Data Arrived at EDR: 09/07/2004 Date Made Active in Reports: 10/12/2004

Number of Days to Update: 35

Source: California Regional Water Quality Control Board Los Angeles Region (4)

Telephone: 213-576-6710 Last EDR Contact: 09/06/2011

Next Scheduled EDR Contact: 12/19/2011 Data Release Frequency: No Update Planned

#### CA LUST REG 3: Leaking Underground Storage Tank Database

Leaking Underground Storage Tank locations. Monterey, San Benito, San Luis Obispo, Santa Barbara, Santa Cruz counties.

Date of Government Version: 05/19/2003 Date Data Arrived at EDR: 05/19/2003 Date Made Active in Reports: 06/02/2003

Number of Days to Update: 14

Source: California Regional Water Quality Control Board Central Coast Region (3) Telephone: 805-542-4786

Last EDR Contact: 07/18/2011

Next Scheduled EDR Contact: 10/31/2011 Data Release Frequency: No Update Planned

### CA LUST: Leaking Underground Fuel Tank Report (GEOTRACKER)

Leaking Underground Storage Tank (LUST) Sites included in GeoTracker. GeoTracker is the Water Boards data management system for sites that impact, or have the potential to impact, water quality in California, with emphasis on groundwater.

Date of Government Version: 12/10/2018 Date Data Arrived at EDR: 12/11/2018 Date Made Active in Reports: 01/15/2019

Number of Days to Update: 35

Source: State Water Resources Control Board

Telephone: see region list Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Quarterly

#### CA LUST REG 6V: Leaking Underground Storage Tank Case Listing

Leaking Underground Storage Tank locations. Inyo, Kern, Los Angeles, Mono, San Bernardino counties.

Date of Government Version: 06/07/2005 Date Data Arrived at EDR: 06/07/2005 Date Made Active in Reports: 06/29/2005

Number of Days to Update: 22

Source: California Regional Water Quality Control Board Victorville Branch Office (6)

Telephone: 760-241-7365 Last EDR Contact: 09/12/2011

Next Scheduled EDR Contact: 12/26/2011 Data Release Frequency: No Update Planned

### CA LUST REG 1: Active Toxic Site Investigation

Del Norte, Humboldt, Lake, Mendocino, Modoc, Siskiyou, Sonoma, Trinity counties. For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 02/01/2001 Date Data Arrived at EDR: 02/28/2001 Date Made Active in Reports: 03/29/2001

Number of Days to Update: 29

Source: California Regional Water Quality Control Board North Coast (1)

Telephone: 707-570-3769 Last EDR Contact: 08/01/2011

Next Scheduled EDR Contact: 11/14/2011 Data Release Frequency: No Update Planned

#### CA LUST REG 2: Fuel Leak List

Leaking Underground Storage Tank locations. Alameda, Contra Costa, Marin, Napa, San Francisco, San Mateo, Santa Clara, Solano, Sonoma counties.

Date of Government Version: 09/30/2004 Date Data Arrived at EDR: 10/20/2004 Date Made Active in Reports: 11/19/2004

Number of Days to Update: 30

Source: California Regional Water Quality Control Board San Francisco Bay Region (2)

Telephone: 510-622-2433 Last EDR Contact: 09/19/2011

Next Scheduled EDR Contact: 01/02/2012 Data Release Frequency: No Update Planned

### CA LUST REG 9: Leaking Underground Storage Tank Report

Orange, Riverside, San Diego counties. For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 03/01/2001 Date Data Arrived at EDR: 04/23/2001 Date Made Active in Reports: 05/21/2001

Number of Days to Update: 28

Source: California Regional Water Quality Control Board San Diego Region (9)

Telephone: 858-637-5595 Last EDR Contact: 09/26/2011

Next Scheduled EDR Contact: 01/09/2012 Data Release Frequency: No Update Planned

INDIAN LUST R10: Leaking Underground Storage Tanks on Indian Land A listing of leaking underground storage tank locations on Indian Land.

Date of Government Version: 10/13/2018 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 55

Source: EPA Region 1 Telephone: 617-918-1313 Last EDR Contact: 07/24/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN LUST R9: Leaking Underground Storage Tanks on Indian Land
A listing of leaking underground storage tank locations on Indian Land.

Date of Government Version: 10/13/2018 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 55

Source: EPA Region 1 Telephone: 617-918-1313 Last EDR Contact: 07/24/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN LUST R8: Leaking Underground Storage Tanks on Indian Land
A listing of leaking underground storage tank locations on Indian Land.

Date of Government Version: 10/13/2018 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 55

Source: EPA Region 1 Telephone: 617-918-1313 Last EDR Contact: 07/24/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN LUST R7: Leaking Underground Storage Tanks on Indian Land A listing of leaking underground storage tank locations on Indian Land.

Date of Government Version: 10/13/2018 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 55

Source: EPA Region 1 Telephone: 617-918-1313 Last EDR Contact: 07/24/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN LUST R6: Leaking Underground Storage Tanks on Indian Land A listing of leaking underground storage tank locations on Indian Land.

Date of Government Version: 10/13/2018 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 55

Source: EPA Region 1 Telephone: 617-918-1313 Last EDR Contact: 07/24/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN LUST R4: Leaking Underground Storage Tanks on Indian Land A listing of leaking underground storage tank locations on Indian Land.

Date of Government Version: 10/13/2018 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 55

Source: EPA Region 1 Telephone: 617-918-1313 Last EDR Contact: 07/24/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN LUST R1: Leaking Underground Storage Tanks on Indian Land
A listing of leaking underground storage tank locations on Indian Land.

Date of Government Version: 10/13/2018 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 55

Source: EPA Region 1 Telephone: 617-918-1313 Last EDR Contact: 07/24/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN LUST R5: Leaking Underground Storage Tanks on Indian Land
A listing of leaking underground storage tank locations on Indian Land.

Date of Government Version: 10/13/2018 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 55

Source: EPA Region 1 Telephone: 617-918-1313 Last EDR Contact: 07/24/2019

Next Scheduled EDR Contact: 11/04/2019

Data Release Frequency: Varies

CA CPS-SLIC: Statewide SLIC Cases (GEOTRACKER)

Cleanup Program Sites (CPS; also known as Site Cleanups [SC] and formerly known as Spills, Leaks, Investigations, and Cleanups [SLIC] sites) included in GeoTracker. GeoTracker is the Water Boards data management system for sites that impact, or have the potential to impact, water quality in California, with emphasis on groundwater.

Date of Government Version: 12/10/2018 Date Data Arrived at EDR: 12/11/2018 Date Made Active in Reports: 01/15/2019

Number of Days to Update: 35

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019

Data Release Frequency: Varies

CA SLIC REG 1: Active Toxic Site Investigations

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality

from spills, leaks, and similar discharges.

Date of Government Version: 04/03/2003

Date Data Arrived at EDR: 04/07/2003 Date Made Active in Reports: 04/25/2003

Number of Days to Update: 18

Source: California Regional Water Quality Control Board, North Coast Region (1)

Telephone: 707-576-2220 Last EDR Contact: 08/01/2011

Next Scheduled EDR Contact: 11/14/2011 Data Release Frequency: No Update Planned

CA SLIC REG 2: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality

from spills, leaks, and similar discharges.

Date of Government Version: 09/30/2004 Date Data Arrived at EDR: 10/20/2004 Date Made Active in Reports: 11/19/2004

Number of Days to Update: 30

Source: Regional Water Quality Control Board San Francisco Bay Region (2)

Telephone: 510-286-0457 Last EDR Contact: 09/19/2011

Next Scheduled EDR Contact: 01/02/2012 Data Release Frequency: No Update Planned

CA SLIC REG 3: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality from spills, leaks, and similar discharges.

Date of Government Version: 05/18/2006 Date Data Arrived at EDR: 05/18/2006 Date Made Active in Reports: 06/15/2006

Number of Days to Update: 28

Source: California Regional Water Quality Control Board Central Coast Region (3)

Telephone: 805-549-3147 Last EDR Contact: 07/18/2011

Next Scheduled EDR Contact: 10/31/2011
Data Release Frequency: No Update Planned

CA SLIC REG 4: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality

from spills, leaks, and similar discharges.

Date of Government Version: 11/17/2004 Date Data Arrived at EDR: 11/18/2004 Date Made Active in Reports: 01/04/2005

Number of Days to Update: 47

Source: Region Water Quality Control Board Los Angeles Region (4)

Telephone: 213-576-6600 Last EDR Contact: 07/01/2011

Next Scheduled EDR Contact: 10/17/2011 Data Release Frequency: No Update Planned

CA SLIC REG 5: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality

from spills, leaks, and similar discharges.

Date of Government Version: 04/01/2005 Date Data Arrived at EDR: 04/05/2005 Date Made Active in Reports: 04/21/2005

Number of Days to Update: 16

Source: Regional Water Quality Control Board Central Valley Region (5)

Telephone: 916-464-3291 Last EDR Contact: 09/12/2011

Next Scheduled EDR Contact: 12/26/2011 Data Release Frequency: No Update Planned

CA SLIC REG 6V: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality

from spills, leaks, and similar discharges.

Date of Government Version: 05/24/2005 Date Data Arrived at EDR: 05/25/2005 Date Made Active in Reports: 06/16/2005

Number of Days to Update: 22

Source: Regional Water Quality Control Board, Victorville Branch

Telephone: 619-241-6583 Last EDR Contact: 08/15/2011

Next Scheduled EDR Contact: 11/28/2011 Data Release Frequency: No Update Planned

CA SLIC REG 6L: SLIC Sites

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality

from spills, leaks, and similar discharges.

Date of Government Version: 09/07/2004 Date Data Arrived at EDR: 09/07/2004 Date Made Active in Reports: 10/12/2004

Number of Days to Update: 35

Source: California Regional Water Quality Control Board, Lahontan Region

Telephone: 530-542-5574 Last EDR Contact: 08/15/2011

Next Scheduled EDR Contact: 11/28/2011
Data Release Frequency: No Update Planned

CA SLIC REG 7: SLIC List

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality

from spills, leaks, and similar discharges.

Date of Government Version: 11/24/2004 Date Data Arrived at EDR: 11/29/2004 Date Made Active in Reports: 01/04/2005

Number of Days to Update: 36

Source: California Regional Quality Control Board, Colorado River Basin Region

Telephone: 760-346-7491 Last EDR Contact: 08/01/2011

Next Scheduled EDR Contact: 11/14/2011 Data Release Frequency: No Update Planned

CA SLIC REG 8: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality

from spills, leaks, and similar discharges.

Date of Government Version: 04/03/2008 Date Data Arrived at EDR: 04/03/2008 Date Made Active in Reports: 04/14/2008

Number of Days to Update: 11

Source: California Region Water Quality Control Board Santa Ana Region (8)

Telephone: 951-782-3298 Last EDR Contact: 09/12/2011

Next Scheduled EDR Contact: 12/26/2011 Data Release Frequency: No Update Planned

CA SLIC REG 9: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing

The SLIC (Spills, Leaks, Investigations and Cleanup) program is designed to protect and restore water quality

from spills, leaks, and similar discharges.

Date of Government Version: 09/10/2007 Date Data Arrived at EDR: 09/11/2007 Date Made Active in Reports: 09/28/2007

Number of Days to Update: 17

Source: California Regional Water Quality Control Board San Diego Region (9)

Telephone: 858-467-2980 Last EDR Contact: 08/08/2011

Next Scheduled EDR Contact: 11/21/2011 Data Release Frequency: No Update Planned

FEMA UST: Underground Storage Tank Listing

A listing of all FEMA owned underground storage tanks.

Date of Government Version: 05/15/2017 Date Data Arrived at EDR: 05/30/2017 Date Made Active in Reports: 10/13/2017

Number of Days to Update: 136

Source: FEMA

Telephone: 202-646-5797 Last EDR Contact: 07/10/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Varies

#### State and tribal registered storage tank lists

CA MILITARY UST SITES: Military UST Sites (GEOTRACKER)

Military ust sites

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

CA UST CLOSURE: Proposed Closure of Underground Storage Tank (UST) Cases

UST cases that are being considered for closure by either the State Water Resources Control Board or the Executive Director have been posted for a 60-day public comment period. UST Case Closures being proposed for consideration by the State Water Resources Control Board. These are primarily UST cases that meet closure criteria under the decisional framework in State Water Board Resolution No. 92-49 and other Board orders. UST Case Closures proposed for consideration by the Executive Director pursuant to State Water Board Resolution No. 2012-0061. These are cases that meet the criteria of the Low-Threat UST Case Closure Policy. UST Case Closure Review Denials and Approved Orders

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/12/2019 Date Made Active in Reports: 07/23/2019

Number of Days to Update: 41

Source: State Water Resources Control Board

Telephone: 916-327-7844 Last EDR Contact: 06/12/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

CA UST: Active UST Facilities

Active UST facilities gathered from the local regulatory agencies

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/23/2019

Number of Days to Update: 42

Source: SWRCB Telephone: 916-341-5851 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Semi-Annually

CA AST: Aboveground Petroleum Storage Tank Facilities

A listing of aboveground storage tank petroleum storage tank locations.

Date of Government Version: 07/06/2016 Date Data Arrived at EDR: 07/12/2016 Date Made Active in Reports: 09/19/2016

Number of Days to Update: 69

Source: California Environmental Protection Agency

Telephone: 916-327-5092 Last EDR Contact: 06/17/2019

Next Scheduled EDR Contact: 09/30/2019 Data Release Frequency: Varies

INDIAN UST R1: Underground Storage Tanks on Indian Land

Date of Government Version: 04/06/2016 Date Data Arrived at EDR: 03/02/2017 Date Made Active in Reports: 04/07/2017

Number of Days to Update: 36

Source: N/A Telephone: N/A

Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN UST R10: Underground Storage Tanks on Indian Land

Date of Government Version: 04/06/2016 Date Data Arrived at EDR: 03/02/2017 Date Made Active in Reports: 04/07/2017

Number of Days to Update: 36

Source: N/A Telephone: N/A

Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN UST R9: Underground Storage Tanks on Indian Land

Date of Government Version: 04/06/2016 Date Data Arrived at EDR: 03/02/2017 Date Made Active in Reports: 04/07/2017

Number of Days to Update: 36

Source: N/A Telephone: N/A

Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN UST R8: Underground Storage Tanks on Indian Land

Date of Government Version: 04/06/2016 Date Data Arrived at EDR: 03/02/2017 Date Made Active in Reports: 04/07/2017

Number of Days to Update: 36

Source: N/A Telephone: N/A

Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN UST R4: Underground Storage Tanks on Indian Land

Date of Government Version: 04/06/2016 Date Data Arrived at EDR: 03/02/2017 Date Made Active in Reports: 04/07/2017

Number of Days to Update: 36

Source: N/A Telephone: N/A

Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN UST R5: Underground Storage Tanks on Indian Land

Date of Government Version: 04/06/2016 Date Data Arrived at EDR: 03/02/2017 Date Made Active in Reports: 04/07/2017

Number of Days to Update: 36

Source: N/A Telephone: N/A

Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN UST R6: Underground Storage Tanks on Indian Land

Date of Government Version: 04/06/2016 Date Data Arrived at EDR: 03/02/2017 Date Made Active in Reports: 04/07/2017

Number of Days to Update: 36

Source: N/A Telephone: N/A

Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INDIAN UST R7: Underground Storage Tanks on Indian Land

Date of Government Version: 04/06/2016 Date Data Arrived at EDR: 03/02/2017 Date Made Active in Reports: 04/07/2017

Number of Days to Update: 36

Source: N/A Telephone: N/A

Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

#### State and tribal voluntary cleanup sites

CA VCP: Voluntary Cleanup Program Properties

Contains low threat level properties with either confirmed or unconfirmed releases and the project proponents have request that DTSC oversee investigation and/or cleanup activities and have agreed to provide coverage for DTSC's costs.

Date of Government Version: 04/29/2019 Date Data Arrived at EDR: 04/30/2019 Date Made Active in Reports: 06/27/2019

Number of Days to Update: 58

Source: Department of Toxic Substances Control

Telephone: 916-323-3400 Last EDR Contact: 04/30/2019

Next Scheduled EDR Contact: 08/12/2019 Data Release Frequency: Quarterly

INDIAN VCP R7: Voluntary Cleanup Priority Lisitng

A listing of voluntary cleanup priority sites located on Indian Land located in Region 7.

Date of Government Version: 03/20/2008 Date Data Arrived at EDR: 04/22/2008 Date Made Active in Reports: 05/19/2008

Number of Days to Update: 27

Source: EPA, Region 7 Telephone: 913-551-7365 Last EDR Contact: 04/20/2009

Next Scheduled EDR Contact: 07/20/2009

Data Release Frequency: Varies

INDIAN VCP R1: Voluntary Cleanup Priority Lisitng

A listing of voluntary cleanup priority sites located on Indian Land located in Region 7.

Date of Government Version: 03/20/2008 Date Data Arrived at EDR: 04/22/2008 Date Made Active in Reports: 05/19/2008

Number of Days to Update: 27

Source: EPA, Region 7 Telephone: 913-551-7365 Last EDR Contact: 04/20/2009

Next Scheduled EDR Contact: 07/20/2009

Data Release Frequency: Varies

#### State and tribal Brownfields sites

CA BROWNFIELDS: Considered Brownfieds Sites Listing

A listing of sites the SWRCB considers to be Brownfields since these are sites have come to them through the MOA Process.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/26/2019 Date Made Active in Reports: 04/29/2019

Number of Days to Update: 34

Source: State Water Resources Control Board

Telephone: 916-323-7905 Last EDR Contact: 06/25/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

### US BROWNFIELDS: A Listing of Brownfields Sites

Brownfields are real property, the expansion, redevelopment, or reuse of which may be complicated by the presence or potential presence of a hazardous substance, pollutant, or contaminant. Cleaning up and reinvesting in these properties takes development pressures off of undeveloped, open land, and both improves and protects the environment. Assessment, Cleanup and Redevelopment Exchange System (ACRES) stores information reported by EPA Brownfields grant recipients on brownfields properties assessed or cleaned up with grant funding as well as information on Targeted Brownfields Assessments performed by EPA Regions. A listing of ACRES Brownfield sites is obtained from Cleanups in My Community. Cleanups in My Community provides information on Brownfields properties for which information is reported back to EPA, as well as areas served by Brownfields grant programs.

Date of Government Version: 12/17/2018 Date Data Arrived at EDR: 12/18/2018 Date Made Active in Reports: 01/11/2019

Number of Days to Update: 24

Source: Environmental Protection Agency

Telephone: 202-566-2777 Last EDR Contact: 06/04/2019

Next Scheduled EDR Contact: 09/30/2019 Data Release Frequency: Semi-Annually

#### ADDITIONAL ENVIRONMENTAL RECORDS

#### Local Lists of Landfill / Solid Waste Disposal Sites

CA WMUDS/SWAT: Waste Management Unit Database

Waste Management Unit Database System. WMUDS is used by the State Water Resources Control Board staff and the Regional Water Quality Control Boards for program tracking and inventory of waste management units. WMUDS is composed of the following databases: Facility Information, Scheduled Inspections Information, Waste Management Unit Information, SWAT Program Information, SWAT Report Summary Information, SWAT Report Summary Data, Chapter 15 (formerly Subchapter 15) Information, Chapter 15 Monitoring Parameters, TPCA Program Information, RCRA Program Information, Closure Information, and Interested Parties Information.

Date of Government Version: 04/01/2000 Date Data Arrived at EDR: 04/10/2000 Date Made Active in Reports: 05/10/2000

Number of Days to Update: 30

Source: State Water Resources Control Board

Telephone: 916-227-4448 Last EDR Contact: 04/25/2019

Next Scheduled EDR Contact: 08/12/2019
Data Release Frequency: No Update Planned

CA SWRCY: Recycler Database

A listing of recycling facilities in California.

Date of Government Version: 03/11/2019 Date Data Arrived at EDR: 03/13/2019 Date Made Active in Reports: 04/30/2019

Number of Days to Update: 48

Source: Department of Conservation

Telephone: 916-323-3836 Last EDR Contact: 06/12/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Quarterly

CA HAULERS: Registered Waste Tire Haulers Listing

A listing of registered waste tire haulers.

Date of Government Version: 03/26/2019 Date Data Arrived at EDR: 03/27/2019 Date Made Active in Reports: 04/30/2019

Number of Days to Update: 34

Source: Integrated Waste Management Board

Telephone: 916-341-6422 Last EDR Contact: 05/09/2019

Next Scheduled EDR Contact: 08/26/2019 Data Release Frequency: Varies

INDIAN ODI: Report on the Status of Open Dumps on Indian Lands

Location of open dumps on Indian land.

Date of Government Version: 12/31/1998 Date Data Arrived at EDR: 12/03/2007 Date Made Active in Reports: 01/24/2008

Number of Days to Update: 52

Source: Environmental Protection Agency

Telephone: 703-308-8245 Last EDR Contact: 04/26/2019

Next Scheduled EDR Contact: 08/12/2019 Data Release Frequency: Varies

DEBRIS REGION 9: Torres Martinez Reservation Illegal Dump Site Locations

A listing of illegal dump sites location on the Torres Martinez Indian Reservation located in eastern Riverside County and northern Imperial County, California.

Date of Government Version: 01/12/2009 Date Data Arrived at EDR: 05/07/2009 Date Made Active in Reports: 09/21/2009

Number of Days to Update: 137

Source: EPA, Region 9 Telephone: 415-947-4219 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: No Update Planned

ODI: Open Dump Inventory

An open dump is defined as a disposal facility that does not comply with one or more of the Part 257 or Part 258 Subtitle D Criteria.

Date of Government Version: 06/30/1985 Date Data Arrived at EDR: 08/09/2004 Date Made Active in Reports: 09/17/2004

Number of Days to Update: 39

Source: Environmental Protection Agency

Telephone: 800-424-9346 Last EDR Contact: 06/09/2004 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

IHS OPEN DUMPS: Open Dumps on Indian Land

A listing of all open dumps located on Indian Land in the United States

Date of Government Version: 04/01/2014 Date Data Arrived at EDR: 08/06/2014 Date Made Active in Reports: 01/29/2015

Telephone: 301-443-1452 Last EDR Contact: 04/23/2019

Number of Days to Update: 176

Next Scheduled EDR Contact: 08/12/2019 Data Release Frequency: Varies

Source: Department of Health & Human Serivces, Indian Health Service

US HIST CDL: National Clandestine Laboratory Register

A listing of clandestine drug lab locations that have been removed from the DEAs National Clandestine Laboratory Register.

Date of Government Version: 02/24/2019 Date Data Arrived at EDR: 02/26/2019 Date Made Active in Reports: 04/17/2019 Source: Drug Enforcement Administration

Telephone: 202-307-1000 Last EDR Contact: 05/24/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: No Update Planned

#### Local Lists of Hazardous waste / Contaminated Sites

CA HIST CAL-SITES: Calsites Database

Number of Days to Update: 50

The Calsites database contains potential or confirmed hazardous substance release properties. In 1996, California EPA reevaluated and significantly reduced the number of sites in the Calsites database. No longer updated by the state agency. It has been replaced by ENVIROSTOR.

Date of Government Version: 08/08/2005 Date Data Arrived at EDR: 08/03/2006

Source: Department of Toxic Substance Control

Date Made Active in Reports: 08/24/2006

Telephone: 916-323-3400 Last EDR Contact: 02/23/2009

Number of Days to Update: 21

Next Scheduled EDR Contact: 05/25/2009 Data Release Frequency: No Update Planned

CA SCH: School Property Evaluation Program

This category contains proposed and existing school sites that are being evaluated by DTSC for possible hazardous materials contamination. In some cases, these properties may be listed in the CalSites category depending on the level of threat to public health and safety or the environment they pose.

Date of Government Version: 04/29/2019 Date Data Arrived at EDR: 04/30/2019

Source: Department of Toxic Substances Control

Date Made Active in Reports: 06/27/2019

Telephone: 916-323-3400 Last EDR Contact: 04/30/2019

Number of Days to Update: 58

Next Scheduled EDR Contact: 08/12/2019 Data Release Frequency: Quarterly

CA CDL: Clandestine Drug Labs

A listing of drug lab locations. Listing of a location in this database does not indicate that any illegal drug lab materials were or were not present there, and does not constitute a determination that the location either requires or does not require additional cleanup work.

Date of Government Version: 12/31/2017 Date Data Arrived at EDR: 06/12/2018

Source: Department of Toxic Substances Control

Date Made Active in Reports: 08/06/2018

Telephone: 916-255-6504 Last EDR Contact: 07/08/2019

Number of Days to Update: 55

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Varies

CA CERS HAZ WASTE: CERS HAZ WASTE

List of sites in the California Environmental Protection Agency (CalEPA) Regulated Site Portal which fall under the Hazardous Chemical Management, Hazardous Waste Onsite Treatment, Household Hazardous Waste Collection, Hazardous Waste Generator, and RCRA LQ HW Generator programs.

Date of Government Version: 04/09/2019 Date Data Arrived at EDR: 04/11/2019 Date Made Active in Reports: 05/08/2019

Number of Days to Update: 27

Source: CalEPA

Telephone: 916-323-2514 Last EDR Contact: 07/23/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Quarterly

CA TOXIC PITS: Toxic Pits Cleanup Act Sites

Toxic PITS Cleanup Act Sites. TOXIC PITS identifies sites suspected of containing hazardous substances where cleanup

has not yet been completed.

Date of Government Version: 07/01/1995 Date Data Arrived at EDR: 08/30/1995 Date Made Active in Reports: 09/26/1995

Number of Days to Update: 27

Source: State Water Resources Control Board

Telephone: 916-227-4364 Last EDR Contact: 01/26/2009

Next Scheduled EDR Contact: 04/27/2009

Data Release Frequency: No Update Planned

US CDL: Clandestine Drug Labs

A listing of clandestine drug lab locations. The U.S. Department of Justice ("the Department") provides this web site as a public service. It contains addresses of some locations where law enforcement agencies reported they found chemicals or other items that indicated the presence of either clandestine drug laboratories or dumpsites. In most cases, the source of the entries is not the Department, and the Department has not verified the entry and does not guarantee its accuracy. Members of the public must verify the accuracy of all entries by, for example, contacting local law enforcement and local health departments.

Date of Government Version: 02/24/2019 Date Data Arrived at EDR: 02/26/2019 Date Made Active in Reports: 04/17/2019

Number of Days to Update: 50

Source: Drug Enforcement Administration

Telephone: 202-307-1000 Last EDR Contact: 05/24/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: Quarterly

CA PFAS: PFAS Contamination Site Location Listing

A listing of PFAS contaminated sites included in the GeoTracker database.

Date of Government Version: 06/28/2019 Date Data Arrived at EDR: 06/28/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 26

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/28/2019

Next Scheduled EDR Contact: 09/23/2019

Data Release Frequency: Varies

#### Local Lists of Registered Storage Tanks

CA SWEEPS UST: SWEEPS UST Listing

Statewide Environmental Evaluation and Planning System. This underground storage tank listing was updated and maintained by a company contacted by the SWRCB in the early 1990's. The listing is no longer updated or maintained. The local agency is the contact for more information on a site on the SWEEPS list.

Date of Government Version: 06/01/1994 Date Data Arrived at EDR: 07/07/2005 Date Made Active in Reports: 08/11/2005

Number of Days to Update: 35

Source: State Water Resources Control Board

Telephone: N/A

Last EDR Contact: 06/03/2005 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

CA UST MENDOCINO: Mendocino County UST Database

A listing of underground storage tank locations in Mendocino County.

Date of Government Version: 12/04/2018
Date Data Arrived at EDR: 12/06/2018
Date Made Active in Reports: 12/14/2018

Number of Days to Update: 8

Source: Department of Public Health Telephone: 707-463-4466

Last EDR Contact: 05/24/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: Annually

CA HIST UST: Hazardous Substance Storage Container Database

The Hazardous Substance Storage Container Database is a historical listing of UST sites. Refer to local/county source for current data.

Date of Government Version: 10/15/1990 Date Data Arrived at EDR: 01/25/1991 Date Made Active in Reports: 02/12/1991

Number of Days to Update: 18

Source: State Water Resources Control Board

Telephone: 916-341-5851 Last EDR Contact: 07/26/2001 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

CA SAN FRANCISCO AST: Aboveground Storage Tank Site Listing

Aboveground storage tank sites

Date of Government Version: 09/11/2018 Date Data Arrived at EDR: 09/12/2018 Date Made Active in Reports: 10/11/2018

Number of Days to Update: 29

Source: San Francisco County Department of Public Health

Telephone: 415-252-3896 Last EDR Contact: 05/02/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Varies

CA CERS TANKS: California Environmental Reporting System (CERS) Tanks

List of sites in the California Environmental Protection Agency (CalEPA) Regulated Site Portal which fall under the Aboveground Petroleum Storage and Underground Storage Tank regulatory programs.

Date of Government Version: 04/09/2019 Date Data Arrived at EDR: 04/11/2019 Date Made Active in Reports: 05/08/2019

Number of Days to Update: 27

Source: California Environmental Protection Agency

Telephone: 916-323-2514 Last EDR Contact: 07/23/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Quarterly

CA FID UST: Facility Inventory Database

The Facility Inventory Database (FID) contains a historical listing of active and inactive underground storage tank locations from the State Water Resource Control Board. Refer to local/county source for current data.

Date of Government Version: 10/31/1994 Date Data Arrived at EDR: 09/05/1995 Date Made Active in Reports: 09/29/1995

Number of Days to Update: 24

Source: California Environmental Protection Agency

Telephone: 916-341-5851 Last EDR Contact: 12/28/1998 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

### Local Land Records

CA LIENS: Environmental Liens Listing

A listing of property locations with environmental liens for California where DTSC is a lien holder.

Date of Government Version: 02/28/2019 Date Data Arrived at EDR: 03/01/2019 Date Made Active in Reports: 04/02/2019

Number of Days to Update: 32

Source: Department of Toxic Substances Control

Telephone: 916-323-3400 Last EDR Contact: 06/03/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Varies

LIENS 2: CERCLA Lien Information

A Federal CERCLA ('Superfund') lien can exist by operation of law at any site or property at which EPA has spent Superfund monies. These monies are spent to investigate and address releases and threatened releases of contamination. CERCLIS provides information as to the identity of these sites and properties.

Date of Government Version: 04/11/2019
Date Data Arrived at EDR: 04/18/2019
Date Made Active in Reports: 05/23/2019

Number of Days to Update: 35

Source: Environmental Protection Agency Telephone: 202-564-6023 Last EDR Contact: 07/02/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Semi-Annually

#### CA DEED: Deed Restriction Listing

Site Mitigation and Brownfields Reuse Program Facility Sites with Deed Restrictions & Hazardous Waste Management Program Facility Sites with Deed / Land Use Restriction. The DTSC Site Mitigation and Brownfields Reuse Program (SMBRP) list includes sites cleaned up under the program's oversight and generally does not include current or former hazardous waste facilities that required a hazardous waste facility permit. The list represents deed restrictions that are active. Some sites have multiple deed restrictions. The DTSC Hazardous Waste Management Program (HWMP) has developed a list of current or former hazardous waste facilities that have a recorded land use restriction at the local county recorder's office. The land use restrictions on this list were required by the DTSC HWMP as a result of the presence of hazardous substances that remain on site after the facility (or part of the facility) has been closed or cleaned up. The types of land use restriction include deed notice, deed restriction, or a land use restriction that binds current and future owners.

Date of Government Version: 03/04/2019 Date Data Arrived at EDR: 03/05/2019 Date Made Active in Reports: 04/01/2019

Number of Days to Update: 27

Source: DTSC and SWRCB Telephone: 916-323-3400 Last EDR Contact: 06/04/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Semi-Annually

### HMIRS: Hazardous Materials Information Reporting System

Hazardous Materials Incident Report System. HMIRS contains hazardous material spill incidents reported to DOT.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/26/2019 Date Made Active in Reports: 05/14/2019

Number of Days to Update: 49

Source: U.S. Department of Transportation

Telephone: 202-366-4555 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

#### Records of Emergency Release Reports

### CA CHMIRS: California Hazardous Material Incident Report System

California Hazardous Material Incident Reporting System. CHMIRS contains information on reported hazardous material incidents (accidental releases or spills).

Date of Government Version: 10/24/2018 Date Data Arrived at EDR: 01/24/2019 Date Made Active in Reports: 03/05/2019

Number of Days to Update: 40

Source: Office of Emergency Services

Telephone: 916-845-8400 Last EDR Contact: 06/24/2019

Next Scheduled EDR Contact: 08/05/2019 Data Release Frequency: Semi-Annually

#### CA LDS: Land Disposal Sites Listing (GEOTRACKER)

Land Disposal sites (Landfills) included in GeoTracker. GeoTracker is the Water Boards data management system for sites that impact, or have the potential to impact, water quality in California, with emphasis on groundwater.

Date of Government Version: 12/10/2018 Date Data Arrived at EDR: 12/11/2018 Date Made Active in Reports: 01/15/2019

Number of Days to Update: 35

Source: State Water Quality Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Quarterly

#### CA MCS: Military Cleanup Sites Listing (GEOTRACKER)

Military sites (consisting of: Military UST sites; Military Privatized sites; and Military Cleanup sites [formerly known as DoD non UST]) included in GeoTracker. GeoTracker is the Water Boards data management system for sites that impact, or have the potential to impact, water quality in California, with emphasis on groundwater.

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Quarterly

#### CA SPILLS 90: SPILLS 90 data from FirstSearch

Spills 90 includes those spill and release records available exclusively from FirstSearch databases. Typically, they may include chemical, oil and/or hazardous substance spills recorded after 1990. Duplicate records that are already included in EDR incident and release records are not included in Spills 90.

Date of Government Version: 06/06/2012 Date Data Arrived at EDR: 01/03/2013 Date Made Active in Reports: 02/22/2013

Number of Days to Update: 50

Source: FirstSearch Telephone: N/A

Last EDR Contact: 01/03/2013 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

#### RCRA NonGen / NLR: RCRA - Non Generators / No Longer Regulated

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Non-Generators do not presently generate hazardous waste.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/27/2019 Date Made Active in Reports: 04/17/2019

Number of Days to Update: 21

Source: Environmental Protection Agency

Telephone: (415) 495-8895 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

### FUDS: Formerly Used Defense Sites

The listing includes locations of Formerly Used Defense Sites properties where the US Army Corps of Engineers is actively working or will take necessary cleanup actions.

Date of Government Version: 03/07/2019 Date Data Arrived at EDR: 04/03/2019 Date Made Active in Reports: 05/23/2019

Number of Days to Update: 50

Source: U.S. Army Corps of Engineers

Telephone: 202-528-4285 Last EDR Contact: 05/21/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Varies

#### DOD: Department of Defense Sites

This data set consists of federally owned or administered lands, administered by the Department of Defense, that have any area equal to or greater than 640 acres of the United States, Puerto Rico, and the U.S. Virgin Islands.

Date of Government Version: 12/31/2005 Date Data Arrived at EDR: 11/10/2006 Date Made Active in Reports: 01/11/2007

Number of Days to Update: 62

Source: USGS

Telephone: 888-275-8747 Last EDR Contact: 07/09/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Semi-Annually

#### FEDLAND: Federal and Indian Lands

Federally and Indian administrated lands of the United States. Lands included are administrated by: Army Corps of Engineers, Bureau of Reclamation, National Wild and Scenic River, National Wildlife Refuge, Public Domain Land, Wilderness, Wilderness Study Area, Wildlife Management Area, Bureau of Indian Affairs, Bureau of Land Management, Department of Justice, Forest Service, Fish and Wildlife Service, National Park Service.

Date of Government Version: 12/31/2005 Date Data Arrived at EDR: 02/06/2006 Date Made Active in Reports: 01/11/2007

Number of Days to Update: 339

Source: U.S. Geological Survey Telephone: 888-275-8747 Last EDR Contact: 07/10/2019

Next Scheduled EDR Contact: 10/21/2019

Data Release Frequency: N/A

#### SCRD DRYCLEANERS: State Coalition for Remediation of Drycleaners Listing

The State Coalition for Remediation of Drycleaners was established in 1998, with support from the U.S. EPA Office of Superfund Remediation and Technology Innovation. It is comprised of representatives of states with established drycleaner remediation programs. Currently the member states are Alabama, Connecticut, Florida, Illinois, Kansas, Minnesota, Missouri, North Carolina, Oregon, South Carolina, Tennessee, Texas, and Wisconsin.

Date of Government Version: 01/01/2017 Date Data Arrived at EDR: 02/03/2017 Date Made Active in Reports: 04/07/2017

Number of Days to Update: 63

Source: Environmental Protection Agency

Telephone: 615-532-8599 Last EDR Contact: 05/13/2019

Next Scheduled EDR Contact: 08/26/2019 Data Release Frequency: Varies

#### US FIN ASSUR: Financial Assurance Information

All owners and operators of facilities that treat, store, or dispose of hazardous waste are required to provide proof that they will have sufficient funds to pay for the clean up, closure, and post-closure care of their facilities.

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/26/2019 Date Made Active in Reports: 05/07/2019

Number of Days to Update: 42

Source: Environmental Protection Agency

Telephone: 202-566-1917 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

#### EPA WATCH LIST: EPA WATCH LIST

EPA maintains a "Watch List" to facilitate dialogue between EPA, state and local environmental agencies on enforcement matters relating to facilities with alleged violations identified as either significant or high priority. Being on the Watch List does not mean that the facility has actually violated the law only that an investigation by EPA or a state or local environmental agency has led those organizations to allege that an unproven violation has in fact occurred. Being on the Watch List does not represent a higher level of concern regarding the alleged violations that were detected, but instead indicates cases requiring additional dialogue between EPA, state and local agencies - primarily because of the length of time the alleged violation has gone unaddressed or unresolved.

Date of Government Version: 08/30/2013 Date Data Arrived at EDR: 03/21/2014 Date Made Active in Reports: 06/17/2014

Number of Days to Update: 88

Source: Environmental Protection Agency

Telephone: 617-520-3000 Last EDR Contact: 05/06/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Quarterly

### 2020 COR ACTION: 2020 Corrective Action Program List

The EPA has set ambitious goals for the RCRA Corrective Action program by creating the 2020 Corrective Action Universe. This RCRA cleanup baseline includes facilities expected to need corrective action. The 2020 universe contains a wide variety of sites. Some properties are heavily contaminated while others were contaminated but have since been cleaned up. Still others have not been fully investigated yet, and may require little or no remediation. Inclusion in the 2020 Universe does not necessarily imply failure on the part of a facility to meet its RCRA obligations.

Date of Government Version: 09/30/2017 Date Data Arrived at EDR: 05/08/2018 Date Made Active in Reports: 07/20/2018

Number of Days to Update: 73

Source: Environmental Protection Agency

Telephone: 703-308-4044 Last EDR Contact: 05/10/2019

Next Scheduled EDR Contact: 08/19/2019

Data Release Frequency: Varies

#### TSCA: Toxic Substances Control Act

Toxic Substances Control Act. TSCA identifies manufacturers and importers of chemical substances included on the TSCA Chemical Substance Inventory list. It includes data on the production volume of these substances by plant site.

Date of Government Version: 12/31/2016
Date Data Arrived at EDR: 06/21/2017
Date Made Active in Reports: 01/05/2018

Number of Days to Update: 198

Source: EPA

Telephone: 202-260-5521 Last EDR Contact: 06/18/2019

Next Scheduled EDR Contact: 09/30/2019 Data Release Frequency: Every 4 Years

### TRIS: Toxic Chemical Release Inventory System

Toxic Release Inventory System. TRIS identifies facilities which release toxic chemicals to the air, water and land in reportable quantities under SARA Title III Section 313.

Date of Government Version: 12/31/2016 Date Data Arrived at EDR: 01/10/2018 Date Made Active in Reports: 01/12/2018

Number of Days to Update: 2

Source: EPA

Telephone: 202-566-0250 Last EDR Contact: 05/24/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Annually

#### SSTS: Section 7 Tracking Systems

Section 7 of the Federal Insecticide, Fungicide and Rodenticide Act, as amended (92 Stat. 829) requires all registered pesticide-producing establishments to submit a report to the Environmental Protection Agency by March 1st each year. Each establishment must report the types and amounts of pesticides, active ingredients and devices being produced, and those having been produced and sold or distributed in the past year.

Date of Government Version: 12/31/2009 Date Data Arrived at EDR: 12/10/2010 Date Made Active in Reports: 02/25/2011

Number of Days to Update: 77

Source: EPA Telephone: 202-564-4203 Last EDR Contact: 04/24/2019

Next Scheduled EDR Contact: 08/05/2019 Data Release Frequency: Annually

#### ROD: Records Of Decision

Record of Decision. ROD documents mandate a permanent remedy at an NPL (Superfund) site containing technical and health information to aid in the cleanup.

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/18/2019 Date Made Active in Reports: 05/23/2019

Number of Days to Update: 35

Source: EPA

Telephone: 703-416-0223 Last EDR Contact: 07/01/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Annually

#### RMP: Risk Management Plans

When Congress passed the Clean Air Act Amendments of 1990, it required EPA to publish regulations and guidance for chemical accident prevention at facilities using extremely hazardous substances. The Risk Management Program Rule (RMP Rule) was written to implement Section 112(r) of these amendments. The rule, which built upon existing industry codes and standards, requires companies of all sizes that use certain flammable and toxic substances to develop a Risk Management Program, which includes a(n): Hazard assessment that details the potential effects of an accidental release, an accident history of the last five years, and an evaluation of worst-case and alternative accidental releases; Prevention program that includes safety precautions and maintenance, monitoring, and employee training measures; and Emergency response program that spells out emergency health care, employee training measures and procedures for informing the public and response agencies (e.g the fire department) should an accident occur.

Date of Government Version: 04/25/2019 Date Data Arrived at EDR: 05/02/2019 Date Made Active in Reports: 05/23/2019

Number of Days to Update: 21

Source: Environmental Protection Agency Telephone: 202-564-8600

Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

### RAATS: RCRA Administrative Action Tracking System

RCRA Administration Action Tracking System. RAATS contains records based on enforcement actions issued under RCRA pertaining to major violators and includes administrative and civil actions brought by the EPA. For administration actions after September 30, 1995, data entry in the RAATS database was discontinued. EPA will retain a copy of the database for historical records. It was necessary to terminate RAATS because a decrease in agency resources made it impossible to continue to update the information contained in the database.

Date of Government Version: 04/17/1995 Date Data Arrived at EDR: 07/03/1995 Date Made Active in Reports: 08/07/1995

Number of Days to Update: 35

Source: EPA

Telephone: 202-564-4104 Last EDR Contact: 06/02/2008

Next Scheduled EDR Contact: 09/01/2008 Data Release Frequency: No Update Planned

PRP: Potentially Responsible Parties

A listing of verified Potentially Responsible Parties

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/18/2019 Date Made Active in Reports: 05/23/2019

Number of Days to Update: 35

Source: EPA

Telephone: 202-564-6023 Last EDR Contact: 07/01/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Quarterly

PADS: PCB Activity Database System

PCB Activity Database. PADS Identifies generators, transporters, commercial storers and/or brokers and disposers of PCB's who are required to notify the EPA of such activities.

Date of Government Version: 03/20/2019 Date Data Arrived at EDR: 04/10/2019 Date Made Active in Reports: 05/14/2019

Number of Days to Update: 34

Source: EPA

Telephone: 202-566-0500 Last EDR Contact: 07/12/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Annually

ICIS: Integrated Compliance Information System

The Integrated Compliance Information System (ICIS) supports the information needs of the national enforcement and compliance program as well as the unique needs of the National Pollutant Discharge Elimination System (NPDES) program.

Date of Government Version: 11/18/2016 Date Data Arrived at EDR: 11/23/2016 Date Made Active in Reports: 02/10/2017

Number of Days to Update: 79

Source: Environmental Protection Agency

Telephone: 202-564-2501 Last EDR Contact: 07/03/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Quarterly

FTTS: FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide Act)/TSCA (Toxic Substances Control Act) FTTS tracks administrative cases and pesticide enforcement actions and compliance activities related to FIFRA,

TSCA and EPCRA (Emergency Planning and Community Right-to-Know Act). To maintain currency, EDR contacts the

Agency on a quarterly basis.

Date of Government Version: 04/09/2009 Date Data Arrived at EDR: 04/16/2009 Date Made Active in Reports: 05/11/2009

Number of Days to Update: 25

Source: EPA/Office of Prevention, Pesticides and Toxic Substances

Telephone: 202-566-1667 Last EDR Contact: 08/18/2017

Next Scheduled EDR Contact: 12/04/2017 Data Release Frequency: No Update Planned

FTTS INSP: FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide Act)/TSCA (Toxic Substances Control Act)

FTTS tracks administrative cases and pesticide enforcement actions and compliance activities related to FIFRA, TSCA and EPCRA (Emergency Planning and Community Right-to-Know Act). To maintain currency, EDR contacts the Agency on a quarterly basis.

Date of Government Version: 04/09/2009 Date Data Arrived at EDR: 04/16/2009 Date Made Active in Reports: 05/11/2009

Number of Days to Update: 25

Source: EPA/Office of Prevention, Pesticides and Toxic Substances

Telephone: 202-566-1667 Last EDR Contact: 08/18/2017

Next Scheduled EDR Contact: 12/04/2017
Data Release Frequency: No Update Planned

MLTS: Material Licensing Tracking System

MLTS is maintained by the Nuclear Regulatory Commission and contains a list of approximately 8,100 sites which possess or use radioactive materials and which are subject to NRC licensing requirements. To maintain currency,

EDR contacts the Agency on a quarterly basis.

Date of Government Version: 08/30/2016 Date Data Arrived at EDR: 09/08/2016 Date Made Active in Reports: 10/21/2016

Number of Days to Update: 43

Source: Nuclear Regulatory Commission

Telephone: 301-415-7169 Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Quarterly

COAL ASH DOE: Steam-Electric Plant Operation Data
A listing of power plants that store ash in surface ponds.

Date of Government Version: 12/31/2005 Date Data Arrived at EDR: 08/07/2009 Date Made Active in Reports: 10/22/2009

Number of Days to Update: 76

Source: Department of Energy Telephone: 202-586-8719 Last EDR Contact: 06/07/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Varies

COAL ASH EPA: Coal Combustion Residues Surface Impoundments List

A listing of coal combustion residues surface impoundments with high hazard potential ratings.

Date of Government Version: 07/01/2014 Date Data Arrived at EDR: 09/10/2014 Date Made Active in Reports: 10/20/2014

Number of Days to Update: 40

Source: Environmental Protection Agency

Telephone: N/A

Last EDR Contact: 06/07/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Varies

PCB TRANSFORMER: PCB Transformer Registration Database

The database of PCB transformer registrations that includes all PCB registration submittals.

Date of Government Version: 05/24/2017 Date Data Arrived at EDR: 11/30/2017 Date Made Active in Reports: 12/15/2017

Number of Days to Update: 15

Source: Environmental Protection Agency

Telephone: 202-566-0517 Last EDR Contact: 04/26/2019

Next Scheduled EDR Contact: 08/05/2019

Data Release Frequency: Varies

RADINFO: Radiation Information Database

The Radiation Information Database (RADINFO) contains information about facilities that are regulated by U.S. Environmental Protection Agency (EPA) regulations for radiation and radioactivity.

Date of Government Version: 04/02/2019 Date Data Arrived at EDR: 04/02/2019 Date Made Active in Reports: 05/14/2019

Number of Days to Update: 42

Source: Environmental Protection Agency

Telephone: 202-343-9775 Last EDR Contact: 07/01/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Quarterly

HIST FTTS: FIFRA/TSCA Tracking System Inspection & Enforcement Case Listing

A complete inspection and enforcement case listing from the FIFRA/TSCA Tracking System (FTTS) for all ten EPA regions. The information was obtained from the National Compliance Database (NCDB). NCDB supports the implementation of FIFRA (Federal Insecticide, Fungicide, and Rodenticide Act) and TSCA (Toxic Substances Control Act). Some EPA regions are now closing out records. Because of that, and the fact that some EPA regions are not providing EPA Headquarters with updated records, it was decided to create a HIST FTTS database. It included records that may not be included in the newer FTTS database updates. This database is no longer updated.

Date of Government Version: 10/19/2006 Date Data Arrived at EDR: 03/01/2007 Date Made Active in Reports: 04/10/2007

Number of Days to Update: 40

Source: Environmental Protection Agency

Telephone: 202-564-2501 Last EDR Contact: 12/17/2008

Next Scheduled EDR Contact: 03/17/2008

Data Release Frequency: No Update Planned

HIST FTTS INSP: FIFRA/TSCA Tracking System Inspection & Enforcement Case Listing

A complete inspection and enforcement case listing from the FIFRA/TSCA Tracking System (FTTS) for all ten EPA regions. The information was obtained from the National Compliance Database (NCDB). NCDB supports the implementation of FIFRA (Federal Insecticide, Fungicide, and Rodenticide Act) and TSCA (Toxic Substances Control Act). Some EPA regions are now closing out records. Because of that, and the fact that some EPA regions are not providing EPA Headquarters with updated records, it was decided to create a HIST FTTS database. It included records that may not be included in the newer FTTS database updates. This database is no longer updated.

Date of Government Version: 10/19/2006 Date Data Arrived at EDR: 03/01/2007 Date Made Active in Reports: 04/10/2007

Number of Days to Update: 40

Source: Environmental Protection Agency

Telephone: 202-564-2501 Last EDR Contact: 12/17/2008

Next Scheduled EDR Contact: 03/17/2008 Data Release Frequency: No Update Planned

DOT OPS: Incident and Accident Data

Department of Transporation, Office of Pipeline Safety Incident and Accident data.

Date of Government Version: 12/03/2018 Date Data Arrived at EDR: 01/29/2019 Date Made Active in Reports: 03/21/2019

Number of Days to Update: 51

Source: Department of Transporation, Office of Pipeline Safety

Telephone: 202-366-4595 Last EDR Contact: 04/30/2019

Next Scheduled EDR Contact: 08/12/2019 Data Release Frequency: Quarterly

CONSENT: Superfund (CERCLA) Consent Decrees

Major legal settlements that establish responsibility and standards for cleanup at NPL (Superfund) sites. Released periodically by United States District Courts after settlement by parties to litigation matters.

Date of Government Version: 03/31/2019 Date Data Arrived at EDR: 04/23/2019 Date Made Active in Reports: 05/23/2019

Number of Days to Update: 30

Source: Department of Justice, Consent Decree Library

Telephone: Varies

Last EDR Contact: 07/08/2019

Next Scheduled EDR Contact: 10/21/2019

Data Release Frequency: Varies

BRS: Biennial Reporting System

The Biennial Reporting System is a national system administered by the EPA that collects data on the generation and management of hazardous waste. BRS captures detailed data from two groups: Large Quantity Generators (LQG) and Treatment, Storage, and Disposal Facilities.

Date of Government Version: 12/31/2015 Date Data Arrived at EDR: 02/22/2017 Date Made Active in Reports: 09/28/2017

Number of Days to Update: 218

Source: EPA/NTIS Telephone: 800-424-9346 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Biennially

INDIAN RESERV: Indian Reservations

This map layer portrays Indian administered lands of the United States that have any area equal to or greater than 640 acres.

Date of Government Version: 12/31/2014 Date Data Arrived at EDR: 07/14/2015 Date Made Active in Reports: 01/10/2017

Number of Days to Update: 546

Source: USGS

Telephone: 202-208-3710 Last EDR Contact: 07/10/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Semi-Annually

FUSRAP: Formerly Utilized Sites Remedial Action Program

DOE established the Formerly Utilized Sites Remedial Action Program (FUSRAP) in 1974 to remediate sites where radioactive contamination remained from Manhattan Project and early U.S. Atomic Energy Commission (AEC) operations.

Date of Government Version: 08/08/2017 Date Data Arrived at EDR: 09/11/2018 Date Made Active in Reports: 09/14/2018

Number of Days to Update: 3

Source: Department of Energy Telephone: 202-586-3559 Last EDR Contact: 05/02/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Varies

UMTRA: Uranium Mill Tailings Sites

Uranium ore was mined by private companies for federal government use in national defense programs. When the mills shut down, large piles of the sand-like material (mill tailings) remain after uranium has been extracted from the ore. Levels of human exposure to radioactive materials from the piles are low; however, in some cases tailings were used as construction materials before the potential health hazards of the tailings were recognized.

Date of Government Version: 06/23/2017 Date Data Arrived at EDR: 10/11/2017 Date Made Active in Reports: 11/03/2017

Number of Days to Update: 23

Source: Department of Energy Telephone: 505-845-0011 Last EDR Contact: 05/24/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Varies

LEAD SMELTER 1: Lead Smelter Sites

A listing of former lead smelter site locations.

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/18/2019 Date Made Active in Reports: 05/14/2019

Number of Days to Update: 26

Source: Environmental Protection Agency

Telephone: 703-603-8787 Last EDR Contact: 07/01/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Varies

LEAD SMELTER 2: Lead Smelter Sites

A listing of former lead smelter site locations.

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/18/2019 Date Made Active in Reports: 05/14/2019

Number of Days to Update: 26

Source: Environmental Protection Agency

Telephone: 703-603-8787 Last EDR Contact: 07/01/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Varies

US AIRS (AFS): Aerometric Information Retrieval System Facility Subsystem

Date of Government Version: 10/27/2009 Date Data Arrived at EDR: 11/10/2009 Date Made Active in Reports: 12/08/2009

Number of Days to Update: 28

Source: N/A Telephone: N/A

Last EDR Contact: 11/12/1996 Next Scheduled EDR Contact: N/A Data Release Frequency: Annually

US AIRS MINOR: Aerometric Information Retrieval System Facility Subsystem

Date of Government Version: 10/27/2009
Date Data Arrived at EDR: 11/10/2009
Date Made Active in Penerte: 12/08/2009

Date Made Active in Reports: 12/08/2009

Number of Days to Update: 28

Source: N/A Telephone: N/A

Last EDR Contact: 11/12/1996 Next Scheduled EDR Contact: N/A Data Release Frequency: Annually

US MINES: Active Mines & Mineral Plants Database Listing

Active Mines and Mineral Processing Plant operations for commodities monitored by the Minerals Information Team of the USGS.

Date of Government Version: 04/14/2011 Date Data Arrived at EDR: 06/08/2011

Date Made Active in Reports: 09/13/2011 Number of Days to Update: 97 Source: USGS

Telephone: 703-648-7709 Last EDR Contact: 05/31/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: Varies

US MINES 2: Active Mines & Mineral Plants Database Listing

Active Mines and Mineral Processing Plant operations for commodities monitored by the Minerals Information Team of the USGS.

Date of Government Version: 04/14/2011 Date Data Arrived at EDR: 06/08/2011 Date Made Active in Reports: 09/13/2011

Number of Days to Update: 97

Source: USGS

Telephone: 703-648-7709 Last EDR Contact: 05/31/2019

Next Scheduled EDR Contact: 09/09/2019

Data Release Frequency: Varies

#### US MINES 3: Active Mines & Mineral Plants Database Listing

Active Mines and Mineral Processing Plant operations for commodities monitored by the Minerals Information Team of the USGS.

Date of Government Version: 04/14/2011 Date Data Arrived at EDR: 06/08/2011 Date Made Active in Reports: 09/13/2011

Number of Days to Update: 97

Source: USGS

Telephone: 703-648-7709 Last EDR Contact: 05/31/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: Varies

#### ABANDONED MINES: Abandoned Mines

An inventory of land and water impacted by past mining (primarily coal mining) is maintained by OSMRE to provide information needed to implement the Surface Mining Control and Reclamation Act of 1977 (SMCRA). The inventory contains information on the location, type, and extent of AML impacts, as well as, information on the cost associated with the reclamation of those problems. The inventory is based upon field surveys by State, Tribal, and OSMRE program officials. It is dynamic to the extent that it is modified as new problems are identified and existing problems are reclaimed.

Date of Government Version: 03/27/2019 Date Data Arrived at EDR: 03/28/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 34

Source: Department of Interior Telephone: 202-208-2609 Last EDR Contact: 06/19/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Quarterly

#### FINDS: Facility Index System/Facility Registry System

Facility Index System. FINDS contains both facility information and 'pointers' to other sources that contain more detail. EDR includes the following FINDS databases in this report: PCS (Permit Compliance System), AIRS (Aerometric Information Retrieval System), DOCKET (Enforcement Docket used to manage and track information on civil judicial enforcement cases for all environmental statutes), FURS (Federal Underground Injection Control), C-DOCKET (Criminal Docket System used to track criminal enforcement actions for all environmental statutes), FFIS (Federal Facilities Information System), STATE (State Environmental Laws and Statutes), and PADS (PCB Activity Data System).

Date of Government Version: 02/15/2019 Date Data Arrived at EDR: 03/05/2019 Date Made Active in Reports: 03/15/2019

Number of Days to Update: 10

Source: EPA Telephone: (415) 947-8000 Last EDR Contact: 06/05/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Quarterly

#### DOCKET HWC: Hazardous Waste Compliance Docket Listing

A complete list of the Federal Agency Hazardous Waste Compliance Docket Facilities.

Date of Government Version: 05/31/2018 Date Data Arrived at EDR: 07/26/2018 Date Made Active in Reports: 10/05/2018

Number of Days to Update: 71

Source: Environmental Protection Agency

Telephone: 202-564-0527 Last EDR Contact: 05/24/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: Varies

### ECHO: Enforcement & Compliance History Information

ECHO provides integrated compliance and enforcement information for about 800,000 regulated facilities nationwide.

Date of Government Version: 04/07/2019 Date Data Arrived at EDR: 04/09/2019 Date Made Active in Reports: 05/23/2019

Number of Days to Update: 44

Source: Environmental Protection Agency

Telephone: 202-564-2280 Last EDR Contact: 07/09/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Quarterly

**UXO: Unexploded Ordnance Sites** 

A listing of unexploded ordnance site locations

Date of Government Version: 12/31/2017 Date Data Arrived at EDR: 01/17/2019 Date Made Active in Reports: 04/01/2019

Number of Days to Update: 74

Source: Department of Defense Telephone: 703-704-1564 Last EDR Contact: 07/15/2019

Next Scheduled EDR Contact: 10/28/2019 Data Release Frequency: Varies

FUELS PROGRAM: EPA Fuels Program Registered Listing

This listing includes facilities that are registered under the Part 80 (Code of Federal Regulations) EPA Fuels Programs. All companies now are required to submit new and updated registrations.

Date of Government Version: 02/19/2019 Date Data Arrived at EDR: 02/21/2019 Date Made Active in Reports: 04/01/2019

Number of Days to Update: 39

Source: EPA

Telephone: 800-385-6164 Last EDR Contact: 05/21/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Quarterly

#### Other Ascertainable Records

CA BOND EXP. PLAN: Bond Expenditure Plan

Department of Health Services developed a site-specific expenditure plan as the basis for an appropriation of Hazardous Substance Cleanup Bond Act funds. It is not updated.

Date of Government Version: 01/01/1989 Date Data Arrived at EDR: 07/27/1994 Date Made Active in Reports: 08/02/1994

Number of Days to Update: 6

Source: Department of Health Services

Telephone: 916-255-2118 Last EDR Contact: 05/31/1994 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

CA CORTESE: "Cortese" Hazardous Waste & Substances Sites List

The sites for the list are designated by the State Water Resource Control Board (LUST), the Integrated Waste Board (SWF/LS), and the Department of Toxic Substances Control (Cal-Sites).

Date of Government Version: 03/25/2019 Date Data Arrived at EDR: 03/26/2019 Date Made Active in Reports: 05/01/2019

Number of Days to Update: 36

Source: CAL EPA/Office of Emergency Information

Telephone: 916-323-3400 Last EDR Contact: 06/25/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

CA CUPA LIVERMORE-PLEASANTON: CUPA Facility Listing

list of facilities associated with the various CUPA programs in Livermore-Pleasanton

Date of Government Version: 05/01/2019 Date Data Arrived at EDR: 05/14/2019 Date Made Active in Reports: 07/17/2019

Number of Days to Update: 64

Source: Livermore-Pleasanton Fire Department

Telephone: 925-454-2361 Last EDR Contact: 05/14/2019

Next Scheduled EDR Contact: 08/26/2019 Data Release Frequency: Varies

CA CUPA SAN FRANCISCO CO: CUPA Facility Listing

Cupa facilities

Date of Government Version: 04/18/2019 Date Data Arrived at EDR: 04/19/2019 Date Made Active in Reports: 04/30/2019

Number of Days to Update: 11

Source: San Francisco County Department of Environmental Health

Telephone: 415-252-3896 Last EDR Contact: 04/18/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Varies

CA DRYCLEANERS: Cleaner Facilities

A list of drycleaner related facilities that have EPA ID numbers. These are facilities with certain SIC codes: power laundries, family and commercial; garment pressing and cleaner's agents; linen supply; coin-operated laundries and cleaning; drycleaning plants, except rugs; carpet and upholster cleaning; industrial launderers; laundry and garment services.

Date of Government Version: 03/01/2019 Date Data Arrived at EDR: 04/25/2019 Date Made Active in Reports: 05/30/2019

Number of Days to Update: 35

Source: Department of Toxic Substance Control

Telephone: 916-327-4498 Last EDR Contact: 06/03/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Annually

CA DRYCLEAN AVAQMD: Antelope Valley Air Quality Management District Drycleaner Listing

A listing of dry cleaners in the Antelope Valley Air Quality Management District.

Date of Government Version: 02/27/2019 Date Data Arrived at EDR: 02/28/2019 Date Made Active in Reports: 04/01/2019

Number of Days to Update: 32

Source: Antelope Valley Air Quality Management District

Telephone: 661-723-8070 Last EDR Contact: 06/03/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Varies

CA DRYCLEAN SOUTH COAST: South Coast Air Quality Management District Drycleaner Listing

A listing of dry cleaners in the South Coast Air Quality Management District

Date of Government Version: 03/19/2019 Date Data Arrived at EDR: 03/22/2019 Date Made Active in Reports: 04/09/2019

Number of Days to Update: 18

Source: South Coast Air Quality Management District

Telephone: 909-396-3211 Last EDR Contact: 05/23/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: Varies

CA EMI: Emissions Inventory Data

Toxics and criteria pollutant emissions data collected by the ARB and local air pollution agencies.

Date of Government Version: 12/31/2017 Date Data Arrived at EDR: 06/20/2018 Date Made Active in Reports: 08/06/2018

Number of Days to Update: 47

Source: California Air Resources Board

Telephone: 916-322-2990 Last EDR Contact: 06/24/2019

Next Scheduled EDR Contact: 09/30/2019 Data Release Frequency: Varies

CA ENF: Enforcement Action Listing

A listing of Water Board Enforcement Actions. Formal is everything except Oral/Verbal Communication, Notice of Violation, Expedited Payment Letter, and Staff Enforcement Letter.

Date of Government Version: 11/01/2018 Date Data Arrived at EDR: 11/02/2018 Date Made Active in Reports: 12/13/2018

Number of Days to Update: 41

Source: State Water Resoruces Control Board

Telephone: 916-445-9379 Last EDR Contact: 07/18/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

CA Financial Assurance 1: Financial Assurance Information Listing

Financial Assurance information

Date of Government Version: 04/22/2019 Date Data Arrived at EDR: 04/23/2019 Date Made Active in Reports: 06/26/2019

Number of Days to Update: 64

Source: Department of Toxic Substances Control

Telephone: 916-255-3628 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

CA Financial Assurance 2: Financial Assurance Information Listing

A listing of financial assurance information for solid waste facilities. Financial assurance is intended to ensure that resources are available to pay for the cost of closure, post-closure care, and corrective measures if the owner or operator of a regulated facility is unable or unwilling to pay.

Date of Government Version: 05/15/2019 Date Data Arrived at EDR: 05/16/2019 Date Made Active in Reports: 07/18/2019 Number of Days to Update: 63 Source: California Integrated Waste Management Board

Telephone: 916-341-6066 Last EDR Contact: 05/09/2019

Next Scheduled EDR Contact: 08/26/2019 Data Release Frequency: Varies

#### CA HAZNET: Facility and Manifest Data

Facility and Manifest Data. The data is extracted from the copies of hazardous waste manifests received each year by the DTSC. The annual volume of manifests is typically 700,000 - 1,000,000 annually, representing approximately 350,000 - 500,000 shipments. Data are from the manifests submitted without correction, and therefore many contain some invalid values for data elements such as generator ID, TSD ID, waste category, and disposal method. This database begins with calendar year 1993.

Date of Government Version: 12/31/2017 Date Data Arrived at EDR: 05/29/2019 Date Made Active in Reports: 07/22/2019

Number of Days to Update: 54

Source: California Environmental Protection Agency

Telephone: 916-255-1136 Last EDR Contact: 07/12/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Annually

#### CA ICE: ICE

Contains data pertaining to the Permitted Facilities with Inspections / Enforcements sites tracked in Envirostor.

Date of Government Version: 05/20/2019 Date Data Arrived at EDR: 05/21/2019 Date Made Active in Reports: 07/18/2019

Number of Days to Update: 58

Source: Department of Toxic Subsances Control

Telephone: 877-786-9427 Last EDR Contact: 05/21/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Quarterly

#### CA HIST CORTESE: Hazardous Waste & Substance Site List

The sites for the list are designated by the State Water Resource Control Board [LUST], the Integrated Waste Board [SWF/LS], and the Department of Toxic Substances Control [CALSITES]. This listing is no longer updated by the state agency.

Date of Government Version: 04/01/2001 Date Data Arrived at EDR: 01/22/2009 Date Made Active in Reports: 04/08/2009

Number of Days to Update: 76

Source: Department of Toxic Substances Control

Telephone: 916-323-3400 Last EDR Contact: 01/22/2009 Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

#### CA HWP: EnviroStor Permitted Facilities Listing

Detailed information on permitted hazardous waste facilities and corrective action ("cleanups") tracked in EnviroStor.

Date of Government Version: 05/20/2019 Date Data Arrived at EDR: 05/21/2019 Date Made Active in Reports: 07/18/2019

Number of Days to Update: 58

Source: Department of Toxic Substances Control

Telephone: 916-323-3400 Last EDR Contact: 05/21/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Quarterly

### CA HWT: Registered Hazardous Waste Transporter Database

A listing of hazardous waste transporters. In California, unless specifically exempted, it is unlawful for any person to transport hazardous wastes unless the person holds a valid registration issued by DTSC. A hazardous waste transporter registration is valid for one year and is assigned a unique registration number.

Date of Government Version: 04/08/2019 Date Data Arrived at EDR: 04/09/2019 Date Made Active in Reports: 05/30/2019

Number of Days to Update: 51

Source: Department of Toxic Substances Control

Telephone: 916-440-7145 Last EDR Contact: 07/09/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Quarterly

### CA MINES: Mines Site Location Listing

A listing of mine site locations from the Office of Mine Reclamation.

Date of Government Version: 12/10/2018 Date Data Arrived at EDR: 12/12/2018 Date Made Active in Reports: 01/15/2019

Number of Days to Update: 34

Source: Department of Conservation

Telephone: 916-322-1080 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Quarterly

CA MWMP: Medical Waste Management Program Listing

The Medical Waste Management Program (MWMP) ensures the proper handling and disposal of medical waste by permitting and inspecting medical waste Offsite Treatment Facilities (PDF) and Transfer Stations (PDF) throughout the state. MWMP also oversees all Medical Waste Transporters.

Date of Government Version: 02/20/2019 Date Data Arrived at EDR: 03/05/2019 Date Made Active in Reports: 04/02/2019

Number of Days to Update: 28

Source: Department of Public Health Telephone: 916-558-1784 Last EDR Contact: 06/04/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Varies

CA NPDES: NPDES Permits Listing

A listing of NPDES permits, including stormwater.

Date of Government Version: 05/13/2019 Date Data Arrived at EDR: 05/14/2019 Date Made Active in Reports: 07/17/2019

Number of Days to Update: 64

Source: State Water Resources Control Board

Telephone: 916-445-9379 Last EDR Contact: 05/14/2019

Next Scheduled EDR Contact: 08/26/2019 Data Release Frequency: Quarterly

CA PEST LIC: Pesticide Regulation Licenses Listing

A listing of licenses and certificates issued by the Department of Pesticide Regulation. The DPR issues licenses and/or certificates to: Persons and businesses that apply or sell pesticides; Pest control dealers and brokers; Persons who advise on agricultural pesticide applications.

Date of Government Version: 03/04/2019 Date Data Arrived at EDR: 03/05/2019 Date Made Active in Reports: 04/05/2019

Number of Days to Update: 31

Source: Department of Pesticide Regulation

Telephone: 916-445-4038 Last EDR Contact: 06/04/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Quarterly

CA PROC: Certified Processors Database A listing of certified processors.

Date of Government Version: 03/11/2019 Date Data Arrived at EDR: 03/13/2019 Date Made Active in Reports: 04/29/2019

Number of Days to Update: 47

Source: Department of Conservation Telephone: 916-323-3836

Last EDR Contact: 06/12/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Quarterly

CA NOTIFY 65: Proposition 65 Records

Listings of all Proposition 65 incidents reported to counties by the State Water Resources Control Board and the Regional Water Quality Control Board. This database is no longer updated by the reporting agency.

Date of Government Version: 03/18/2019 Date Data Arrived at EDR: 03/19/2019 Date Made Active in Reports: 04/29/2019

Number of Days to Update: 41

Source: State Water Resources Control Board

Telephone: 916-445-3846 Last EDR Contact: 06/17/2019

Next Scheduled EDR Contact: 09/30/2019
Data Release Frequency: No Update Planned

CA UIC: UIC Listing

A listing of wells identified as underground injection wells, in the California Oil and Gas Wells database.

Date of Government Version: 04/27/2018 Date Data Arrived at EDR: 06/13/2018 Date Made Active in Reports: 07/17/2018

Number of Days to Update: 34

Source: Deaprtment of Conservation Telephone: 916-445-2408 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

CA UIC GEO: Underground Injection Control Sites (GEOTRACKER)

Underground control injection sites

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resource Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

CA WASTEWATER PITS: Oil Wastewater Pits Listing

Water officials discovered that oil producers have been dumping chemical-laden wastewater into hundreds of unlined pits that are operating without proper permits. Inspections completed by the Central Valley Regional Water Quality Control Board revealed the existence of previously unidentified waste sites. The water boards review found that more than one-third of the region's active disposal pits are operating without permission.

Date of Government Version: 05/08/2018 Date Data Arrived at EDR: 07/11/2018 Date Made Active in Reports: 09/13/2018

Number of Days to Update: 64

Source: RWQCB, Central Valley Region

Telephone: 559-445-5577 Last EDR Contact: 07/12/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Varies

CA WDS: Waste Discharge System

Sites which have been issued waste discharge requirements.

Date of Government Version: 06/19/2007 Date Data Arrived at EDR: 06/20/2007 Date Made Active in Reports: 06/29/2007

Number of Days to Update: 9

Source: State Water Resources Control Board

Telephone: 916-341-5227 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019
Data Release Frequency: No Update Planned

CA WIP: Well Investigation Program Case List

Well Investigation Program case in the San Gabriel and San Fernando Valley area.

Date of Government Version: 07/03/2009 Date Data Arrived at EDR: 07/21/2009 Date Made Active in Reports: 08/03/2009

Number of Days to Update: 13

Source: Los Angeles Water Quality Control Board

Telephone: 213-576-6726 Last EDR Contact: 06/19/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: No Update Planned

CA MILITARY PRIV SITES: Military Privatized Sites (GEOTRACKER)

Military privatized sites

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

CA PROJECT: Project Sites (GEOTRACKER)

Projects sites

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

CA WDR: Waste Discharge Requirements Listing

In general, the Waste Discharge Requirements (WDRs) Program (sometimes also referred to as the "Non Chapter 15 (Non 15) Program") regulates point discharges that are exempt pursuant to Subsection 20090 of Title 27 and not subject to the Federal Water Pollution Control Act. Exemptions from Title 27 may be granted for nine categories of discharges (e.g., sewage, wastewater, etc.) that meet, and continue to meet, the preconditions listed for each specific exemption. The scope of the WDRs Program also includes the discharge of wastes classified as inert, pursuant to section 20230 of Title 27.

Date of Government Version: 03/11/2019 Date Data Arrived at EDR: 03/13/2019 Date Made Active in Reports: 04/29/2019

Number of Days to Update: 47

Source: State Water Resources Control Board

Telephone: 916-341-5810 Last EDR Contact: 06/12/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Quarterly

#### CA CIWQS: California Integrated Water Quality System

The California Integrated Water Quality System (CIWQS) is a computer system used by the State and Regional Water Quality Control Boards to track information about places of environmental interest, manage permits and other orders, track inspections, and manage violations and enforcement activities.

Date of Government Version: 03/05/2019 Date Data Arrived at EDR: 03/05/2019 Date Made Active in Reports: 04/02/2019

Number of Days to Update: 28

Source: State Water Resources Control Board

Telephone: 866-794-4977 Last EDR Contact: 06/04/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Varies

#### CA CERS: CalEPA Regulated Site Portal Data

The CalEPA Regulated Site Portal database combines data about environmentally regulated sites and facilities in California into a single database. It combines data from a variety of state and federal databases, and provides an overview of regulated activities across the spectrum of environmental programs for any given location in California. These activities include hazardous materials and waste, state and federal cleanups, impacted ground and surface waters, and toxic materials

Date of Government Version: 04/09/2019 Date Data Arrived at EDR: 04/11/2019 Date Made Active in Reports: 05/08/2019

Number of Days to Update: 27

Source: California Environmental Protection Agency

Telephone: 916-323-2514 Last EDR Contact: 07/23/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

#### CA NON-CASE INFO: Non-Case Information Sites (GEOTRACKER)

Non-Case Information sites

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

### CA OTHER OIL GAS: Other Oil & Gas Projects Sites (GEOTRACKER)

Other Oil & Gas Projects sites

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

### CA PROD WATER PONDS: Produced Water Ponds Sites (GEOTRACKER)

Produced water ponds sites

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

CA SAMPLING POINT: Sampling Point? Public Sites (GEOTRACKER)

Sampling point - public sites

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

#### CA WELL STIM PROJ: Well Stimulation Project (GEOTRACKER)

Includes areas of groundwater monitoring plans, a depiction of the monitoring network, and the facilities, boundaries, and subsurface characteristics of the oilfield and the features (oil and gas wells, produced water ponds, UIC wells, water supply wells, etc?) being monitored

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/11/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 43

Source: State Water Resources Control Board

Telephone: 866-480-1028 Last EDR Contact: 06/11/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Varies

### EDR MGP: EDR Proprietary Manufactured Gas Plants

The EDR Proprietary Manufactured Gas Plant Database includes records of coal gas plants (manufactured gas plants) compiled by EDR's researchers. Manufactured gas sites were used in the United States from the 1800's to 1950's to produce a gas that could be distributed and used as fuel. These plants used whale oil, rosin, coal, or a mixture of coal, oil, and water that also produced a significant amount of waste. Many of the byproducts of the gas production, such as coal tar (oily waste containing volatile and non-volatile chemicals), sludges, oils and other compounds are potentially hazardous to human health and the environment. The byproduct from this process was frequently disposed of directly at the plant site and can remain or spread slowly, serving as a continuous source of soil and groundwater contamination.

Date of Government Version: N/A Date Data Arrived at EDR: N/A Date Made Active in Reports: N/A Number of Days to Update: N/A Source: EDR, Inc. Telephone: N/A Last EDR Contact: N/A

Next Scheduled EDR Contact: N/A

Data Release Frequency: No Update Planned

### EDR Hist Auto: EDR Exclusive Historical Auto Stations

EDR has searched selected national collections of business directories and has collected listings of potential gas station/filling station/service station sites that were available to EDR researchers. EDR's review was limited to those categories of sources that might, in EDR's opinion, include gas station/filling station/service station establishments. The categories reviewed included, but were not limited to gas, gas station, gasoline station, filling station, auto, automobile repair, auto service station, service station, etc. This database falls within a category of information EDR classifies as "High Risk Historical Records", or HRHR. EDR's HRHR effort presents unique and sometimes proprietary data about past sites and operations that typically create environmental concerns, but may not show up in current government records searches.

Date of Government Version: N/A Date Data Arrived at EDR: N/A Date Made Active in Reports: N/A

Number of Days to Update: N/A

Source: EDR, Inc. Telephone: N/A Last EDR Contact: N/A

Next Scheduled EDR Contact: N/A Data Release Frequency: Varies

### EDR Hist Cleaner: EDR Exclusive Historical Cleaners

EDR has searched selected national collections of business directories and has collected listings of potential dry cleaner sites that were available to EDR researchers. EDR's review was limited to those categories of sources that might, in EDR's opinion, include dry cleaning establishments. The categories reviewed included, but were not limited to dry cleaners, cleaners, laundry, laundromat, cleaning/laundry, wash & dry etc. This database falls within a category of information EDR classifies as "High Risk Historical Records", or HRHR. EDR's HRHR effort presents unique and sometimes proprietary data about past sites and operations that typically create environmental concerns, but may not show up in current government records searches.

Date of Government Version: N/A Date Data Arrived at EDR: N/A Date Made Active in Reports: N/A Number of Days to Update: N/A Source: EDR, Inc.
Telephone: N/A
Last EDR Contact: N/A

Next Scheduled EDR Contact: N/A Data Release Frequency: Varies

#### **EDR RECOVERED GOVERNMENT ARCHIVES**

#### **Exclusive Recovered Govt. Archives**

CA RGA LF: Recovered Government Archive Solid Waste Facilities List

The EDR Recovered Government Archive Landfill database provides a list of landfills derived from historical databases and includes many records that no longer appear in current government lists. Compiled from Records formerly available from the Department of Resources Recycling and Recovery in California.

Date of Government Version: N/A
Date Data Arrived at EDR: 07/01/2013
Date Made Active in Reports: 01/13/2014
Number of Days to Update: 196

Source: Department of Resources Recycling and Recovery Telephone:  $\ensuremath{\mathsf{N}/\mathsf{A}}$ 

Last EDR Contact: 06/01/2012 Next Scheduled EDR Contact: N/A Data Release Frequency: Varies

CA RGA LUST: Recovered Government Archive Leaking Underground Storage Tank

The EDR Recovered Government Archive Leaking Underground Storage Tank database provides a list of LUST incidents derived from historical databases and includes many records that no longer appear in current government lists. Compiled from Records formerly available from the State Water Resources Control Board in California.

Date of Government Version: N/A
Date Data Arrived at EDR: 07/01/2013
Date Made Active in Reports: 12/30/2013
Number of Days to Update: 182

Source: State Water Resources Control Board Telephone: N/A

Last EDR Contact: 06/01/2012 Next Scheduled EDR Contact: N/A Data Release Frequency: Varies

### **COUNTY RECORDS**

### ALAMEDA COUNTY:

#### Contaminated Sites

A listing of contaminated sites overseen by the Toxic Release Program (oil and groundwater contamination from chemical releases and spills) and the Leaking Underground Storage Tank Program (soil and ground water contamination from leaking petroleum USTs).

Date of Government Version: 01/09/2019 Date Data Arrived at EDR: 01/11/2019 Date Made Active in Reports: 03/05/2019

Source: Alameda County Environmental Health Services

Source: Alameda County Environmental Health Services

Telephone: 510-567-6700 Last EDR Contact: 07/08/2019

Number of Days to Update: 53

Next Scheduled EDR Contact: 10/21/2019

Data Release Frequency: Semi-Annually

#### **Underground Tanks**

Underground storage tank sites located in Alameda county.

Date of Government Version: 04/10/2019 Date Data Arrived at EDR: 04/11/2019 Date Made Active in Reports: 06/20/2019

Telephone: 510-567-6700

Last EDR Contact: 07/19/2019

Number of Days to Update: 70

Next Scheduled EDR Contact: 04/24/2047 Data Release Frequency: Semi-Annually

### AMADOR COUNTY:

**CUPA Facility List** 

Cupa Facility List

Date of Government Version: 06/27/2019 Date Data Arrived at EDR: 06/28/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 26

Source: Amador County Environmental Health

Telephone: 209-223-6439 Last EDR Contact: 06/17/2019

Next Scheduled EDR Contact: 09/16/2019

Data Release Frequency: Varies

**BUTTE COUNTY:** 

CUPA Facility Listing

Cupa facility list.

Date of Government Version: 04/21/2017 Date Data Arrived at EDR: 04/25/2017 Date Made Active in Reports: 08/09/2017

Number of Days to Update: 106

Source: Public Health Department Telephone: 530-538-7149 Last EDR Contact: 07/08/2019

Next Scheduled EDR Contact: 10/21/2019
Data Release Frequency: No Update Planned

**CALVERAS COUNTY:** 

CUPA Facility Listing

Cupa Facility Listing

Date of Government Version: 05/01/2019 Date Data Arrived at EDR: 05/02/2019 Date Made Active in Reports: 05/29/2019

Number of Days to Update: 27

Source: Calveras County Environmental Health

Telephone: 209-754-6399 Last EDR Contact: 06/24/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

COLUSA COUNTY:

**CUPA Facility List** 

Cupa facility list.

Date of Government Version: 05/17/2019 Date Data Arrived at EDR: 05/21/2019 Date Made Active in Reports: 07/18/2019

Number of Days to Update: 58

Source: Health & Human Services Telephone: 530-458-0396 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Semi-Annually

CONTRA COSTA COUNTY:

Site List

List includes sites from the underground tank, hazardous waste generator and business plan/2185 programs.

Date of Government Version: 05/22/2019 Date Data Arrived at EDR: 05/23/2019 Date Made Active in Reports: 07/18/2019

Number of Days to Update: 56

Source: Contra Costa Health Services Department

Telephone: 925-646-2286 Last EDR Contact: 04/29/2019

Next Scheduled EDR Contact: 08/12/2019 Data Release Frequency: Semi-Annually

DEL NORTE COUNTY:

**CUPA Facility List** 

Cupa Facility list

Date of Government Version: 02/20/2019 Date Data Arrived at EDR: 05/01/2019 Date Made Active in Reports: 05/30/2019

Number of Days to Update: 29

Source: Del Norte County Environmental Health Division

Telephone: 707-465-0426 Last EDR Contact: 04/25/2019

Next Scheduled EDR Contact: 08/12/2019

Data Release Frequency: Varies

#### EL DORADO COUNTY:

**CUPA Facility List** 

CUPA facility list.

Date of Government Version: 06/05/2019 Date Data Arrived at EDR: 06/06/2019 Date Made Active in Reports: 07/23/2019

Number of Days to Update: 47

Source: El Dorado County Environmental Management Department

Telephone: 530-621-6623 Last EDR Contact: 04/29/2019

Next Scheduled EDR Contact: 08/12/2019

Data Release Frequency: Varies

#### FRESNO COUNTY:

## **CUPA Resources List**

Certified Unified Program Agency. CUPA's are responsible for implementing a unified hazardous materials and hazardous waste management regulatory program. The agency provides oversight of businesses that deal with hazardous materials, operate underground storage tanks or aboveground storage tanks.

Date of Government Version: 04/10/2019 Date Data Arrived at EDR: 04/11/2019 Date Made Active in Reports: 04/30/2019

Number of Days to Update: 19

Source: Dept. of Community Health Telephone: 559-445-3271 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Semi-Annually

## GLENN COUNTY:

CUPA Facility List

Cupa facility list

Date of Government Version: 01/22/2018 Date Data Arrived at EDR: 01/24/2018 Date Made Active in Reports: 03/14/2018

Number of Days to Update: 49

Source: Glenn County Air Pollution Control District

Telephone: 830-934-6500 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019
Data Release Frequency: No Update Planned

## HUMBOLDT COUNTY:

CUPA Facility List

CUPA facility list.

Date of Government Version: 12/11/2018 Date Data Arrived at EDR: 12/13/2018 Date Made Active in Reports: 01/15/2019

Number of Days to Update: 33

Source: Humboldt County Environmental Health

Telephone: N/A

Last EDR Contact: 05/20/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Semi-Annually

## IMPERIAL COUNTY:

**CUPA Facility List** 

Cupa facility list.

Date of Government Version: 04/24/2019 Date Data Arrived at EDR: 04/25/2019 Date Made Active in Reports: 06/27/2019

Number of Days to Update: 63

Source: San Diego Border Field Office

Telephone: 760-339-2777 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

INYO COUNTY:

CUPA Facility List
Cupa facility list.

Date of Government Version: 04/02/2018 Date Data Arrived at EDR: 04/03/2018 Date Made Active in Reports: 06/14/2018

Number of Days to Update: 72

Source: Inyo County Environmental Health Services

Telephone: 760-878-0238 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019

Data Release Frequency: Varies

KERN COUNTY:

Underground Storage Tank Sites & Tank Listing Kern County Sites and Tanks Listing.

Date of Government Version: 05/06/2019 Date Data Arrived at EDR: 05/07/2019 Date Made Active in Reports: 07/16/2019

Number of Days to Update: 70

Source: Kern County Environment Health Services Department

Telephone: 661-862-8700 Last EDR Contact: 05/02/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Quarterly

KINGS COUNTY:

**CUPA Facility List** 

A listing of sites included in the county's Certified Unified Program Agency database. California's Secretary for Environmental Protection established the unified hazardous materials and hazardous waste regulatory program as required by chapter 6.11 of the California Health and Safety Code. The Unified Program consolidates the administration, permits, inspections, and enforcement activities.

Date of Government Version: 05/16/2019 Date Data Arrived at EDR: 05/17/2019 Date Made Active in Reports: 05/30/2019

Number of Days to Update: 13

Source: Kings County Department of Public Health

Telephone: 559-584-1411 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Varies

LAKE COUNTY:

CUPA Facility List Cupa facility list

> Date of Government Version: 05/30/2019 Date Data Arrived at EDR: 05/31/2019 Date Made Active in Reports: 07/23/2019

Number of Days to Update: 53

Source: Lake County Environmental Health

Telephone: 707-263-1164 Last EDR Contact: 07/15/2019

Next Scheduled EDR Contact: 10/28/2019 Data Release Frequency: Varies

LASSEN COUNTY:

**CUPA Facility List** 

Cupa facility list

Date of Government Version: 01/17/2019 Date Data Arrived at EDR: 01/18/2019 Date Made Active in Reports: 03/05/2019

Number of Days to Update: 46

Source: Lassen County Environmental Health

Telephone: 530-251-8528 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

LOS ANGELES COUNTY:

Key Areas of Concerns in Los Angeles County

San Gabriel Valley areas where VOC contamination is at or above the MCL as designated by region 9 EPA office. Date of Government Version: 3/30/2009 Exide Site area is a cleanup plan of lead-impacted soil surrounding the former

Exide Facility as designated by the DTSC. Date of Government Version: 7/17/2017

Date of Government Version: 03/30/2009 Date Data Arrived at EDR: 03/31/2009 Date Made Active in Reports: 10/23/2009

Number of Days to Update: 206

Source: N/A Telephone: N/A

Last EDR Contact: 06/17/2019

Next Scheduled EDR Contact: 09/30/2019 Data Release Frequency: No Update Planned

**HMS: Street Number List** 

Industrial Waste and Underground Storage Tank Sites.

Date of Government Version: 05/13/2019 Date Data Arrived at EDR: 05/16/2019 Date Made Active in Reports: 07/18/2019

Number of Days to Update: 63

Source: Department of Public Works

Telephone: 626-458-3517 Last EDR Contact: 07/08/2019

Next Scheduled EDR Contact: 10/21/2019 Data Release Frequency: Semi-Annually

List of Solid Waste Facilities

Solid Waste Facilities in Los Angeles County.

Date of Government Version: 04/15/2019 Date Data Arrived at EDR: 04/16/2019 Date Made Active in Reports: 06/21/2019

Number of Days to Update: 66

Source: La County Department of Public Works

Telephone: 818-458-5185 Last EDR Contact: 07/17/2019

Next Scheduled EDR Contact: 10/28/2019

Data Release Frequency: Varies

City of Los Angeles Landfills

Landfills owned and maintained by the City of Los Angeles.

Date of Government Version: 01/01/2019 Date Data Arrived at EDR: 01/15/2019 Date Made Active in Reports: 03/07/2019

Number of Days to Update: 51

Source: Engineering & Construction Division

Telephone: 213-473-7869 Last EDR Contact: 07/12/2019

Next Scheduled EDR Contact: 10/28/2019 Data Release Frequency: Varies

Active & Inactive AST Inventory

A listing of active & inactive above ground petroleum storage tank site locations, located in the City of Los Angeles.

Date of Government Version: 01/01/2019 Date Data Arrived at EDR: 04/05/2019 Date Made Active in Reports: 05/29/2019

Number of Days to Update: 54

Source: Los Angeles Fire Department

Telephone: 213-978-3800 Last EDR Contact: 06/25/2019

Next Scheduled EDR Contact: 10/07/2019

Data Release Frequency: Varies

## Methane Producing Landfills

This data was created on April 30, 2012 to represent known disposal sites in Los Angeles County that may produce and emanate methane gas. The shapefile contains disposal sites within Los Angeles County that once accepted degradable refuse material. Information used to create this data was extracted from a landfill survey performed by County Engineers (Major Waste System Map, 1973) as well as historical records from CalRecycle, Regional Water Quality Control Board, and Los Angeles County Department of Public Health

Date of Government Version: 04/30/2012 Date Data Arrived at EDR: 04/17/2019 Date Made Active in Reports: 05/29/2019

Number of Days to Update: 42

Source: Los Angeles County Department of Public Works

Telephone: 626-458-6973 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 10/28/2019
Data Release Frequency: No Update Planned

#### Active & Inactive Hazardous Materials Inventory

A listing of active & inactive hazardous materials facility locations, located in the City of Los Angeles.

Date of Government Version: 01/01/2019 Date Data Arrived at EDR: 04/05/2019 Date Made Active in Reports: 05/29/2019

Number of Days to Update: 54

Source: Los Angeles Fire Department

Telephone: 213-978-3800 Last EDR Contact: 06/25/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Varies

#### Active & Inactive UST Inventory

A listing of active & inactive underground storage tank site locations and underground storage tank historical sites, located in the City of Los Angeles.

Date of Government Version: 01/01/2019 Date Data Arrived at EDR: 04/05/2019 Date Made Active in Reports: 05/29/2019

Number of Days to Update: 54

Source: Los Angeles Fire Department

Telephone: 213-978-3800 Last EDR Contact: 06/25/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Varies

## Site Mitigation List

Industrial sites that have had some sort of spill or complaint.

Date of Government Version: 04/08/2019 Date Data Arrived at EDR: 04/16/2019 Date Made Active in Reports: 06/21/2019

Number of Days to Update: 66

Source: Community Health Services Telephone: 323-890-7806 Last EDR Contact: 07/17/2019

Next Scheduled EDR Contact: 10/28/2019 Data Release Frequency: Annually

## City of El Segundo Underground Storage Tank

Underground storage tank sites located in El Segundo city.

Date of Government Version: 01/21/2017 Date Data Arrived at EDR: 04/19/2017 Date Made Active in Reports: 05/10/2017

Number of Days to Update: 21

Source: City of El Segundo Fire Department Telephone: 310-524-2236

Last EDR Contact: 07/12/2019

Next Scheduled EDR Contact: 10/28/2019 Data Release Frequency: No Update Planned

## City of Long Beach Underground Storage Tank

Underground storage tank sites located in the city of Long Beach.

Date of Government Version: 04/22/2019 Date Data Arrived at EDR: 04/23/2019 Date Made Active in Reports: 06/27/2019

Number of Days to Update: 65

Source: City of Long Beach Fire Department Telephone: 562-570-2563

Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019

Data Release Frequency: Varies

City of Torrance Underground Storage Tank

Underground storage tank sites located in the city of Torrance.

Date of Government Version: 04/04/2019 Date Data Arrived at EDR: 04/23/2019 Date Made Active in Reports: 06/27/2019

Number of Days to Update: 65

Source: City of Torrance Fire Department

Telephone: 310-618-2973 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Semi-Annually

#### MADERA COUNTY:

## **CUPA Facility List**

A listing of sites included in the county's Certified Unified Program Agency database. California's Secretary for Environmental Protection established the unified hazardous materials and hazardous waste regulatory program as required by chapter 6.11 of the California Health and Safety Code. The Unified Program consolidates the administration, permits, inspections, and enforcement activities.

Date of Government Version: 02/20/2019 Date Data Arrived at EDR: 02/22/2019 Date Made Active in Reports: 03/07/2019

Number of Days to Update: 13

Source: Madera County Environmental Health

Telephone: 559-675-7823 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Varies

## MARIN COUNTY:

Underground Storage Tank Sites

Currently permitted USTs in Marin County.

Date of Government Version: 09/26/2018 Date Data Arrived at EDR: 10/04/2018 Date Made Active in Reports: 11/02/2018

Number of Days to Update: 29

Source: Public Works Department Waste Management

Telephone: 415-473-6647 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Semi-Annually

## MERCED COUNTY:

CUPA Facility List CUPA facility list.

> Date of Government Version: 05/29/2019 Date Data Arrived at EDR: 05/30/2019 Date Made Active in Reports: 07/22/2019

Number of Days to Update: 53

Source: Merced County Environmental Health

Telephone: 209-381-1094 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Varies

## MONO COUNTY:

CUPA Facility List CUPA Facility List

> Date of Government Version: 05/23/2019 Date Data Arrived at EDR: 05/30/2019 Date Made Active in Reports: 07/22/2019

Number of Days to Update: 53

Source: Mono County Health Department

Telephone: 760-932-5580 Last EDR Contact: 05/23/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: Varies

#### MONTEREY COUNTY:

**CUPA Facility Listing** 

CUPA Program listing from the Environmental Health Division.

Date of Government Version: 02/05/2019 Date Data Arrived at EDR: 02/07/2019 Date Made Active in Reports: 03/05/2019

Number of Days to Update: 26

Source: Monterey County Health Department

Telephone: 831-796-1297 Last EDR Contact: 06/28/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Varies

NAPA COUNTY:

Sites With Reported Contamination

A listing of leaking underground storage tank sites located in Napa county.

Date of Government Version: 01/09/2017 Date Data Arrived at EDR: 01/11/2017 Date Made Active in Reports: 03/02/2017

Number of Days to Update: 50

Telephone: 707-253-4269 Last EDR Contact: 05/24/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: No Update Planned

Closed and Operating Underground Storage Tank Sites

Underground storage tank sites located in Napa county.

Date of Government Version: 02/21/2019 Date Data Arrived at EDR: 02/22/2019 Date Made Active in Reports: 03/08/2019

Number of Days to Update: 14

Source: Napa County Department of Environmental Management

Source: Napa County Department of Environmental Management

Telephone: 707-253-4269 Last EDR Contact: 05/24/2019

Next Scheduled EDR Contact: 09/09/2019 Data Release Frequency: No Update Planned

**NEVADA COUNTY:** 

**CUPA Facility List** 

CUPA facility list.

Date of Government Version: 05/20/2019 Date Data Arrived at EDR: 05/21/2019 Date Made Active in Reports: 05/30/2019

Number of Days to Update: 9

Source: Community Development Agency

Telephone: 530-265-1467 Last EDR Contact: 05/13/2019

Next Scheduled EDR Contact: 08/12/2019 Data Release Frequency: Varies

**ORANGE COUNTY:** 

List of Industrial Site Cleanups

Petroleum and non-petroleum spills.

Date of Government Version: 05/01/2019 Date Data Arrived at EDR: 05/09/2019 Date Made Active in Reports: 05/30/2019

Number of Days to Update: 21

Source: Health Care Agency Telephone: 714-834-3446 Last EDR Contact: 05/06/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Annually

List of Underground Storage Tank Cleanups

Orange County Underground Storage Tank Cleanups (LUST).

Date of Government Version: 05/01/2019 Date Data Arrived at EDR: 05/09/2019 Date Made Active in Reports: 05/30/2019

Number of Days to Update: 21

Source: Health Care Agency Telephone: 714-834-3446 Last EDR Contact: 05/06/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Quarterly

List of Underground Storage Tank Facilities

Orange County Underground Storage Tank Facilities (UST).

Date of Government Version: 04/02/2019 Date Data Arrived at EDR: 05/07/2019 Date Made Active in Reports: 07/16/2019

Number of Days to Update: 70

Source: Health Care Agency Telephone: 714-834-3446 Last EDR Contact: 05/07/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Quarterly

#### PLACER COUNTY:

Master List of Facilities

List includes aboveground tanks, underground tanks and cleanup sites.

Date of Government Version: 02/28/2019 Date Data Arrived at EDR: 03/01/2019 Date Made Active in Reports: 04/12/2019

Number of Days to Update: 42

Source: Placer County Health and Human Services

Telephone: 530-745-2363 Last EDR Contact: 06/03/2019

Next Scheduled EDR Contact: 06/17/2019 Data Release Frequency: Semi-Annually

#### PLUMAS COUNTY:

**CUPA Facility List** 

Plumas County CUPA Program facilities.

Date of Government Version: 03/31/2019 Date Data Arrived at EDR: 04/23/2019 Date Made Active in Reports: 06/26/2019

Number of Days to Update: 64

Source: Plumas County Environmental Health

Telephone: 530-283-6355 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019

Data Release Frequency: Varies

#### RIVERSIDE COUNTY:

Listing of Underground Tank Cleanup Sites

Riverside County Underground Storage Tank Cleanup Sites (LUST).

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/12/2019 Date Made Active in Reports: 04/30/2019

Number of Days to Update: 18

Source: Department of Environmental Health

Telephone: 951-358-5055 Last EDR Contact: 06/17/2019

Next Scheduled EDR Contact: 09/30/2019 Data Release Frequency: Quarterly

Underground Storage Tank Tank List

Underground storage tank sites located in Riverside county.

Date of Government Version: 04/11/2019 Date Data Arrived at EDR: 04/12/2019 Date Made Active in Reports: 06/20/2019

Number of Days to Update: 69

Source: Department of Environmental Health

Telephone: 951-358-5055 Last EDR Contact: 06/17/2019

Next Scheduled EDR Contact: 09/30/2019 Data Release Frequency: Quarterly

## SACRAMENTO COUNTY:

Toxic Site Clean-Up List

List of sites where unauthorized releases of potentially hazardous materials have occurred.

Date of Government Version: 02/05/2019 Date Data Arrived at EDR: 04/02/2019 Date Made Active in Reports: 06/18/2019

Number of Days to Update: 77

Source: Sacramento County Environmental Management

Telephone: 916-875-8406 Last EDR Contact: 06/28/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Quarterly

## Master Hazardous Materials Facility List

Any business that has hazardous materials on site - hazardous material storage sites, underground storage tanks, waste generators.

Date of Government Version: 02/06/2019 Date Data Arrived at EDR: 04/02/2019 Date Made Active in Reports: 06/20/2019

Number of Days to Update: 79

Source: Sacramento County Environmental Management

Telephone: 916-875-8406 Last EDR Contact: 06/28/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Quarterly

## SAN BENITO COUNTY:

CUPA Facility List Cupa facility list

> Date of Government Version: 03/11/2019 Date Data Arrived at EDR: 03/13/2019 Date Made Active in Reports: 04/30/2019

Number of Days to Update: 48

Source: San Benito County Environmental Health

Telephone: N/A

Last EDR Contact: 07/16/2019

Next Scheduled EDR Contact: 08/19/2019

Data Release Frequency: Varies

## SAN BERNARDINO COUNTY:

## **Hazardous Material Permits**

This listing includes underground storage tanks, medical waste handlers/generators, hazardous materials handlers, hazardous waste generators, and waste oil generators/handlers.

Date of Government Version: 05/31/2019 Date Data Arrived at EDR: 05/31/2019 Date Made Active in Reports: 07/22/2019

Number of Days to Update: 52

Source: San Bernardino County Fire Department Hazardous Materials Division

Telephone: 909-387-3041 Last EDR Contact: 05/06/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Quarterly

## SAN DIEGO COUNTY:

## Hazardous Materials Management Division Database

The database includes: HE58 - This report contains the business name, site address, business phone number, establishment 'H' permit number, type of permit, and the business status. HE17 - In addition to providing the same information provided in the HE58 listing, HE17 provides inspection dates, violations received by the establishment, hazardous waste generated, the quantity, method of storage, treatment/disposal of waste and the hauler, and information on underground storage tanks. Unauthorized Release List - Includes a summary of environmental contamination cases in San Diego County (underground tank cases, non-tank cases, groundwater contamination, and soil contamination are included.)

Date of Government Version: 03/04/2019 Date Data Arrived at EDR: 03/05/2019 Date Made Active in Reports: 04/02/2019

Number of Days to Update: 28

Source: Hazardous Materials Management Division

Telephone: 619-338-2268 Last EDR Contact: 06/04/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Quarterly

#### Solid Waste Facilities

San Diego County Solid Waste Facilities.

Date of Government Version: 04/18/2018 Date Data Arrived at EDR: 04/24/2018 Date Made Active in Reports: 06/19/2018

Number of Days to Update: 56

Source: Department of Health Services

Telephone: 619-338-2209 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

#### Local Oversight Program Listing

A listing of all LOP release sites that are or were under the County of San Diego's jurisdiction. Included are closed or transferred cases, open cases, and cases that did not have a case type indicated. The cases without a case type are mostly complaints; however, some of them could be LOP cases.

Date of Government Version: 04/24/2019 Date Data Arrived at EDR: 04/25/2019 Date Made Active in Reports: 06/27/2019

Number of Days to Update: 63

Source: Department of Environmental Health

Telephone: 858-505-6874 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Varies

## **Environmental Case Listing**

The listing contains all underground tank release cases and projects pertaining to properties contaminated with hazardous substances that are actively under review by the Site Assessment and Mitigation Program.

Date of Government Version: 03/23/2010 Date Data Arrived at EDR: 06/15/2010 Date Made Active in Reports: 07/09/2010

Number of Days to Update: 24

Source: San Diego County Department of Environmental Health

Telephone: 619-338-2371 Last EDR Contact: 06/03/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: No Update Planned

## SAN FRANCISCO COUNTY:

#### Local Oversite Facilities

A listing of leaking underground storage tank sites located in San Francisco county.

Date of Government Version: 09/19/2008 Date Data Arrived at EDR: 09/19/2008 Date Made Active in Reports: 09/29/2008

Number of Days to Update: 10

Source: Department Of Public Health San Francisco County

Telephone: 415-252-3920 Last EDR Contact: 05/02/2019

Next Scheduled EDR Contact: 08/19/2019
Data Release Frequency: No Update Planned

## Underground Storage Tank Information

Underground storage tank sites located in San Francisco county.

Date of Government Version: 11/05/2018 Date Data Arrived at EDR: 11/06/2018 Date Made Active in Reports: 12/14/2018

Number of Days to Update: 38

Source: Department of Public Health

Telephone: 415-252-3920 Last EDR Contact: 05/02/2019

Next Scheduled EDR Contact: 08/19/2019
Data Release Frequency: Quarterly

## SAN JOAQUIN COUNTY:

## San Joaquin Co. UST

A listing of underground storage tank locations in San Joaquin county.

Date of Government Version: 06/22/2018 Date Data Arrived at EDR: 06/26/2018 Date Made Active in Reports: 07/11/2018

Number of Days to Update: 15

Source: Environmental Health Department

Telephone: N/A

Last EDR Contact: 06/17/2019

Next Scheduled EDR Contact: 09/30/2019 Data Release Frequency: Semi-Annually

## SAN LUIS OBISPO COUNTY:

**CUPA Facility List** 

Cupa Facility List.

Date of Government Version: 05/20/2019 Date Data Arrived at EDR: 05/21/2019 Date Made Active in Reports: 07/18/2019

Number of Days to Update: 58

Source: San Luis Obispo County Public Health Department

Telephone: 805-781-5596 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Varies

SAN MATEO COUNTY:

**Business Inventory** 

List includes Hazardous Materials Business Plan, hazardous waste generators, and underground storage tanks.

Date of Government Version: 03/04/2019 Date Data Arrived at EDR: 03/13/2019 Date Made Active in Reports: 04/29/2019

Number of Days to Update: 47

Source: San Mateo County Environmental Health Services Division

Telephone: 650-363-1921 Last EDR Contact: 06/12/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Annually

Fuel Leak List

A listing of leaking underground storage tank sites located in San Mateo county.

Date of Government Version: 03/29/2019 Date Data Arrived at EDR: 03/29/2019 Date Made Active in Reports: 05/29/2019

Number of Days to Update: 61

Source: San Mateo County Environmental Health Services Division

Telephone: 650-363-1921 Last EDR Contact: 06/10/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Semi-Annually

SANTA BARBARA COUNTY:

**CUPA Facility Listing** 

CUPA Program Listing from the Environmental Health Services division.

Date of Government Version: 09/08/2011 Date Data Arrived at EDR: 09/09/2011 Date Made Active in Reports: 10/07/2011

Number of Days to Update: 28

Source: Santa Barbara County Public Health Department

Telephone: 805-686-8167 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: No Update Planned

SANTA CLARA COUNTY:

Cupa Facility List

Cupa facility list

Date of Government Version: 05/16/2019 Date Data Arrived at EDR: 05/23/2019 Date Made Active in Reports: 07/18/2019

Number of Days to Update: 56

Source: Department of Environmental Health

Telephone: 408-918-1973 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019

Data Release Frequency: Varies

HIST LUST - Fuel Leak Site Activity Report

A listing of open and closed leaking underground storage tanks. This listing is no longer updated by the county. Leaking underground storage tanks are now handled by the Department of Environmental Health.

Date of Government Version: 03/29/2005 Date Data Arrived at EDR: 03/30/2005 Date Made Active in Reports: 04/21/2005

Number of Days to Update: 22

Source: Santa Clara Valley Water District

Telephone: 408-265-2600 Last EDR Contact: 03/23/2009

Next Scheduled EDR Contact: 06/22/2009 Data Release Frequency: No Update Planned

#### LOP Listing

A listing of leaking underground storage tanks located in Santa Clara county.

Date of Government Version: 03/03/2014 Date Data Arrived at EDR: 03/05/2014 Date Made Active in Reports: 03/18/2014

Number of Days to Update: 13

Source: Department of Environmental Health

Telephone: 408-918-3417 Last EDR Contact: 05/24/2019

Next Scheduled EDR Contact: 09/09/2019
Data Release Frequency: No Update Planned

#### Hazardous Material Facilities

Hazardous material facilities, including underground storage tank sites.

Date of Government Version: 05/19/2019 Date Data Arrived at EDR: 05/23/2019 Date Made Active in Reports: 07/22/2019

Number of Days to Update: 60

Source: City of San Jose Fire Department

Telephone: 408-535-7694 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Annually

## SANTA CRUZ COUNTY:

**CUPA Facility List** 

CUPA facility listing.

Date of Government Version: 01/21/2017 Date Data Arrived at EDR: 02/22/2017 Date Made Active in Reports: 05/23/2017

Number of Days to Update: 90

Source: Santa Cruz County Environmental Health

Telephone: 831-464-2761 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Varies

## SHASTA COUNTY:

**CUPA Facility List** 

Cupa Facility List.

Date of Government Version: 06/15/2017 Date Data Arrived at EDR: 06/19/2017 Date Made Active in Reports: 08/09/2017

Number of Days to Update: 51

Source: Shasta County Department of Resource Management

Telephone: 530-225-5789 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 09/02/2019 Data Release Frequency: Varies

## SOLANO COUNTY:

Leaking Underground Storage Tanks

A listing of leaking underground storage tank sites located in Solano county.

Date of Government Version: 03/05/2019 Date Data Arrived at EDR: 03/07/2019 Date Made Active in Reports: 04/29/2019

Number of Days to Update: 53

Source: Solano County Department of Environmental Management

Telephone: 707-784-6770 Last EDR Contact: 06/03/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Quarterly

## **Underground Storage Tanks**

Underground storage tank sites located in Solano county.

Date of Government Version: 06/04/2019 Date Data Arrived at EDR: 06/06/2019 Date Made Active in Reports: 07/23/2019

Number of Days to Update: 47

Source: Solano County Department of Environmental Management

Telephone: 707-784-6770 Last EDR Contact: 06/03/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Quarterly

## SONOMA COUNTY:

Cupa Facility List

Cupa Facility list

Date of Government Version: 06/18/2019 Date Data Arrived at EDR: 06/25/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 29

Source: County of Sonoma Fire & Emergency Services Department

Telephone: 707-565-1174 Last EDR Contact: 06/19/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Varies

Leaking Underground Storage Tank Sites

A listing of leaking underground storage tank sites located in Sonoma county.

Date of Government Version: 04/03/2019 Date Data Arrived at EDR: 04/11/2019 Date Made Active in Reports: 04/30/2019

Number of Days to Update: 19

Source: Department of Health Services

Telephone: 707-565-6565 Last EDR Contact: 06/19/2019

Next Scheduled EDR Contact: 10/07/2019 Data Release Frequency: Quarterly

STANISLAUS COUNTY:

CUPA Facility List Cupa facility list

> Date of Government Version: 12/11/2018 Date Data Arrived at EDR: 12/13/2018 Date Made Active in Reports: 01/15/2019

Number of Days to Update: 33

Source: Stanislaus County Department of Ennvironmental Protection

Telephone: 209-525-6751 Last EDR Contact: 07/15/2019

Next Scheduled EDR Contact: 10/28/2019 Data Release Frequency: Varies

SUTTER COUNTY:

**Underground Storage Tanks** 

Underground storage tank sites located in Sutter county.

Date of Government Version: 06/03/2019 Date Data Arrived at EDR: 06/04/2019 Date Made Active in Reports: 07/23/2019

Number of Days to Update: 49

Source: Sutter County Environmental Health Services

Telephone: 530-822-7500 Last EDR Contact: 06/03/2019

Next Scheduled EDR Contact: 09/16/2019 Data Release Frequency: Semi-Annually

TEHAMA COUNTY:

CUPA Facility List Cupa facilities

> Date of Government Version: 05/20/2019 Date Data Arrived at EDR: 05/21/2019 Date Made Active in Reports: 07/18/2019

Number of Days to Update: 58

Source: Tehama County Department of Environmental Health

Telephone: 530-527-8020 Last EDR Contact: 05/16/2019

Next Scheduled EDR Contact: 08/19/2019 Data Release Frequency: Varies

TRINITY COUNTY:

CUPA Facility List Cupa facility list

Date of Government Version: 04/24/2019 Date Data Arrived at EDR: 04/25/2019 Date Made Active in Reports: 06/28/2019

Number of Days to Update: 64

Source: Department of Toxic Substances Control

Telephone: 760-352-0381 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019

Data Release Frequency: Varies

## TULARE COUNTY:

**CUPA Facility List** 

Cupa program facilities

Date of Government Version: 05/09/2019 Date Data Arrived at EDR: 05/10/2019 Date Made Active in Reports: 07/17/2019

Number of Days to Update: 68

Source: Tulare County Environmental Health Services Division

Telephone: 559-624-7400 Last EDR Contact: 05/06/2019

Next Scheduled EDR Contact: 08/19/2019

Data Release Frequency: Varies

## TUOLUMNE COUNTY:

CUPA Facility List

Cupa facility list

Date of Government Version: 04/23/2018 Date Data Arrived at EDR: 04/25/2018 Date Made Active in Reports: 06/25/2018

Number of Days to Update: 61

Source: Divison of Environmental Health

Telephone: 209-533-5633 Last EDR Contact: 07/19/2019

Next Scheduled EDR Contact: 11/04/2019

Data Release Frequency: Varies

## **VENTURA COUNTY:**

Business Plan, Hazardous Waste Producers, and Operating Underground Tanks

The BWT list indicates by site address whether the Environmental Health Division has Business Plan (B), Waste Producer (W), and/or Underground Tank (T) information.

Date of Government Version: 03/26/2019 Date Data Arrived at EDR: 04/25/2019 Date Made Active in Reports: 06/27/2019

Number of Days to Update: 63

Source: Ventura County Environmental Health Division

Telephone: 805-654-2813 Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Quarterly

#### Inventory of Illegal Abandoned and Inactive Sites

Ventura County Inventory of Closed, Illegal Abandoned, and Inactive Sites.

Date of Government Version: 12/01/2011 Date Data Arrived at EDR: 12/01/2011 Date Made Active in Reports: 01/19/2012

Number of Days to Update: 49

Source: Environmental Health Division

Telephone: 805-654-2813 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/14/2019
Data Release Frequency: No Update Planned

## Listing of Underground Tank Cleanup Sites

Ventura County Underground Storage Tank Cleanup Sites (LUST).

Date of Government Version: 05/29/2008 Date Data Arrived at EDR: 06/24/2008 Date Made Active in Reports: 07/31/2008

Number of Days to Update: 37

Source: Environmental Health Division

Telephone: 805-654-2813 Last EDR Contact: 05/09/2019

Next Scheduled EDR Contact: 08/26/2019
Data Release Frequency: No Update Planned

## Medical Waste Program List

To protect public health and safety and the environment from potential exposure to disease causing agents, the Environmental Health Division Medical Waste Program regulates the generation, handling, storage, treatment and disposal of medical waste throughout the County.

Date of Government Version: 03/26/2019 Date Data Arrived at EDR: 04/25/2019 Date Made Active in Reports: 05/30/2019

Number of Days to Update: 35

Source: Ventura County Resource Management Agency

Telephone: 805-654-2813 Last EDR Contact: 07/22/2019

Next Scheduled EDR Contact: 11/04/2019 Data Release Frequency: Quarterly

#### Underground Tank Closed Sites List

Ventura County Operating Underground Storage Tank Sites (UST)/Underground Tank Closed Sites List.

Date of Government Version: 06/10/2019 Date Data Arrived at EDR: 06/12/2019 Date Made Active in Reports: 07/24/2019

Number of Days to Update: 42

Source: Environmental Health Division

Telephone: 805-654-2813 Last EDR Contact: 06/12/2019

Next Scheduled EDR Contact: 09/23/2019 Data Release Frequency: Quarterly

#### YOLO COUNTY:

Underground Storage Tank Comprehensive Facility Report
Underground storage tank sites located in Yolo county.

Date of Government Version: 03/29/2019 Date Data Arrived at EDR: 04/05/2019 Date Made Active in Reports: 06/20/2019

Number of Days to Update: 76

Source: Yolo County Department of Health

Telephone: 530-666-8646 Last EDR Contact: 06/26/2019

Next Scheduled EDR Contact: 10/14/2019 Data Release Frequency: Annually

## YUBA COUNTY:

## **CUPA Facility List**

CUPA facility listing for Yuba County.

Date of Government Version: 05/03/2019 Date Data Arrived at EDR: 05/07/2019 Date Made Active in Reports: 07/16/2019

Number of Days to Update: 70

Source: Yuba County Environmental Health Department

Telephone: 530-749-7523 Last EDR Contact: 04/25/2019

Next Scheduled EDR Contact: 08/12/2019

Data Release Frequency: Varies

## OTHER DATABASE(S)

Depending on the geographic area covered by this report, the data provided in these specialty databases may or may not be complete. For example, the existence of wetlands information data in a specific report does not mean that all wetlands in the area covered by the report are included. Moreover, the absence of any reported wetlands information does not necessarily mean that wetlands do not exist in the area covered by the report.

## Oil/Gas Pipelines

Source: PennWell Corporation

Petroleum Bundle (Crude Oil, Refined Products, Petrochemicals, Gas Liquids (LPG/NGL), and Specialty Gases (Miscellaneous)) N = Natural Gas Bundle (Natural Gas, Gas Liquids (LPG/NGL), and Specialty Gases (Miscellaneous)). This map includes information copyrighted by PennWell Corporation. This information is provided on a best effort basis and PennWell Corporation does not guarantee its accuracy nor warrant its fitness for any particular purpose. Such information has been reprinted with the permission of PennWell.

#### Electric Power Transmission Line Data

Source: PennWell Corporation

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Sensitive Receptors: There are individuals deemed sensitive receptors due to their fragile immune systems and special sensitivity to environmental discharges. These sensitive receptors typically include the elderly, the sick, and children. While the location of all sensitive receptors cannot be determined, EDR indicates those buildings and facilities - schools, daycares, hospitals, medical centers, and nursing homes - where individuals who are sensitive receptors are likely to be located.

#### AHA Hospitals:

Source: American Hospital Association, Inc.

Telephone: 312-280-5991

The database includes a listing of hospitals based on the American Hospital Association's annual survey of hospitals.

Medical Centers: Provider of Services Listing

Source: Centers for Medicare & Medicaid Services

Telephone: 410-786-3000

A listing of hospitals with Medicare provider number, produced by Centers of Medicare & Medicaid Services,

a federal agency within the U.S. Department of Health and Human Services.

Nursing Homes

Source: National Institutes of Health

Telephone: 301-594-6248

Information on Medicare and Medicaid certified nursing homes in the United States.

Public Schools

Source: National Center for Education Statistics

Telephone: 202-502-7300

The National Center for Education Statistics' primary database on elementary

and secondary public education in the United States. It is a comprehensive, annual, national statistical database of all public elementary and secondary schools and school districts, which contains data that are comparable across all states.

**Private Schools** 

Source: National Center for Education Statistics

Telephone: 202-502-7300

The National Center for Education Statistics' primary database on private school locations in the United States.

Daycare Centers: Licensed Facilities Source: Department of Social Services

Telephone: 916-657-4041

Flood Zone Data: This data was obtained from the Federal Emergency Management Agency (FEMA). It depicts 100-year and 500-year flood zones as defined by FEMA. It includes the National Flood Hazard Layer (NFHL) which incorporates Flood Insurance Rate Map (FIRM) data and Q3 data from FEMA in areas not covered by NFHL.

Source: FEMA

Telephone: 877-336-2627

Date of Government Version: 2003, 2015

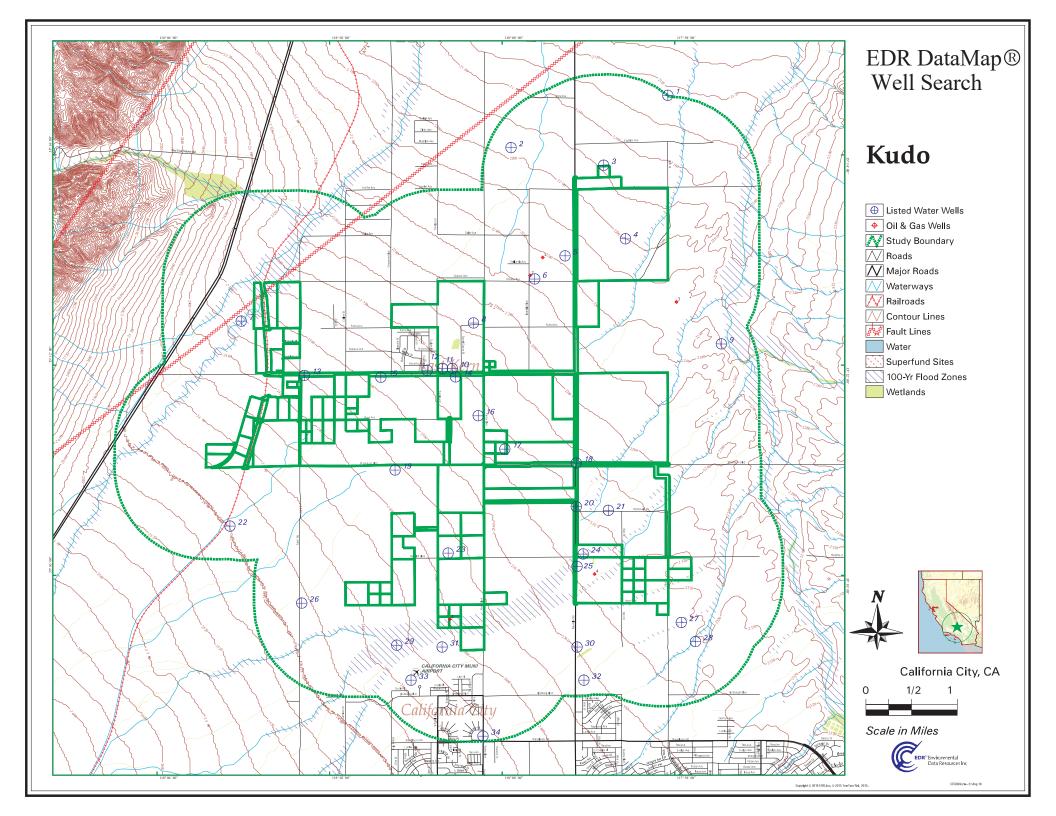
NWI: National Wetlands Inventory. This data, available in select counties across the country, was obtained by EDR in 2002, 2005 and 2010 from the U.S. Fish and Wildlife Service.

State Wetlands Data: Wetland Inventory Source: Department of Fish & Game

Telephone: 916-445-0411

## STREET AND ADDRESS INFORMATION

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**Kudo** California City, CA 93505

Inquiry Number: 5759392.2w

August 21, 2019

# **EDR DataMap™ Well Search Report**



Thank you for your business.
Please contact EDR at 1-800-352-0050
with any questions or comments.

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# GEOCHECK VERSION 2.1 SUMMARY

## FEDERAL DATABASE WELL INFORMATION

| ID  | MAP | WELL            |
|---|-----|-----------------|
| 3 USG\$40000161611 4 USG\$40000161498 5 USG\$40000161484 5 USG\$40000161470 6 USG\$40000161434 7 USG\$40000161363 8 USG\$40000161360 9 USG\$40000161309 12 USG\$40000161309 12 USG\$40000161304 13 USG\$40000161304 14 USG\$40000161295 15 USG\$40000161295 16 USG\$40000161297 17 USG\$40000161177 19 USG\$40000161177 20 USG\$40000161177 20 USG\$40000161136 21 USG\$40000161132 22 USG\$40000161132 23 USG\$40000161100 24 USG\$40000161100   | ID  | ID              |
| 3 USG\$40000161611 4 USG\$40000161498 5 USG\$40000161484 5 USG\$40000161470 6 USG\$40000161434 7 USG\$40000161363 8 USG\$40000161360 9 USG\$40000161309 12 USG\$40000161309 12 USG\$40000161304 13 USG\$40000161304 14 USG\$40000161295 15 USG\$40000161295 16 USG\$40000161297 17 USG\$40000161177 19 USG\$40000161177 20 USG\$40000161177 20 USG\$40000161136 21 USG\$40000161132 22 USG\$40000161132 23 USG\$40000161100 24 USG\$40000161100   |     |                 |
| 4 USG\$40000161498 5 USG\$40000161484 5 USG\$40000161484 7 USG\$40000161434 7 USG\$40000161363 8 USG\$40000161360 9 USG\$40000161309 12 USG\$40000161304 13 USG\$40000161300 14 USG\$40000161295 15 USG\$40000161295 16 USG\$40000161296 16 USG\$40000161177 19 USG\$40000161177 20 USG\$40000161177 20 USG\$40000161132 21 USG\$40000161132 22 USG\$40000161100 24 USG\$40000161100  |     |                 |
| 5         USGS40000161484           5         USGS40000161470           6         USGS40000161434           7         USGS40000161363           8         USGS40000161344           10         USGS40000161309           12         USGS40000161304           13         USGS40000161300           14         USGS40000161295           15         USGS40000161296           16         USGS40000161234           17         USGS40000161194           18         USGS40000161179           19         USGS40000161177           20         USGS40000161136           21         USGS40000161132           22         USGS40000161102           23         USGS40000161100           24         USGS40000161096 | -   |                 |
| 5       USGS40000161470         6       USGS40000161434         7       USGS40000161363         8       USGS40000161360         9       USGS40000161309         12       USGS40000161304         13       USGS40000161300         14       USGS40000161295         15       USGS40000161296         16       USGS40000161234         17       USGS40000161194         18       USGS40000161179         19       USGS40000161177         20       USGS40000161136         21       USGS40000161132         22       USGS40000161122         23       USGS40000161100         24       USGS40000161096  | =   |                 |
| 6 USG\$40000161434 7 USG\$40000161363 8 USG\$40000161360 9 USG\$40000161344 10 USG\$40000161309 12 USG\$40000161304 13 USG\$40000161300 14 USG\$40000161295 15 USG\$40000161295 16 USG\$40000161294 17 USG\$40000161194 18 USG\$40000161177 19 USG\$40000161177 20 USG\$40000161177 20 USG\$40000161132 21 USG\$40000161132 22 USG\$40000161100 24 USG\$40000161100   | -   |                 |
| 7 USGS40000161363 8 USGS40000161360 9 USGS40000161344 10 USGS40000161309 12 USGS40000161304 13 USGS40000161300 14 USGS40000161295 15 USGS40000161295 16 USGS40000161294 17 USGS40000161194 18 USGS40000161177 19 USGS40000161177 20 USGS40000161177 20 USGS40000161132 21 USGS40000161132 22 USGS40000161100 24 USGS40000161100   | -   |                 |
| 8 USG\$40000161360 9 USG\$40000161344 10 USG\$40000161309 12 USG\$40000161300 14 USG\$40000161295 15 USG\$40000161296 16 USG\$40000161234 17 USG\$40000161194 18 USG\$40000161177 19 USG\$40000161177 20 USG\$40000161177 20 USG\$40000161132 21 USG\$40000161132 22 USG\$40000161100 24 USG\$40000161096   | -   |                 |
| 9 USG\$40000161344 10 USG\$40000161309 12 USG\$40000161300 13 USG\$40000161300 14 USG\$40000161295 15 USG\$40000161296 16 USG\$40000161234 17 USG\$40000161194 18 USG\$40000161177 19 USG\$40000161177 20 USG\$40000161177 20 USG\$40000161132 21 USG\$40000161132 22 USG\$40000161100 24 USG\$40000161096  | •   |                 |
| 10 USG\$40000161309 12 USG\$40000161304 13 USG\$40000161300 14 USG\$40000161295 15 USG\$40000161296 16 USG\$40000161234 17 USG\$40000161194 18 USG\$40000161179 19 USG\$40000161177 20 USG\$40000161177 20 USG\$40000161132 21 USG\$40000161132 22 USG\$40000161100 24 USG\$40000161096   | -   |                 |
| 12 USG\$40000161304 13 USG\$40000161300 14 USG\$40000161295 15 USG\$40000161296 16 USG\$40000161234 17 USG\$40000161194 18 USG\$40000161179 19 USG\$40000161177 20 USG\$40000161177 20 USG\$40000161132 21 USG\$40000161132 22 USG\$40000161100 24 USG\$40000161096   | -   |                 |
| 13 USGS40000161300 14 USGS40000161295 15 USGS40000161296 16 USGS40000161234 17 USGS40000161194 18 USGS40000161179 19 USGS40000161176 19 USGS40000161177 20 USGS40000161136 21 USGS40000161132 22 USGS40000161132 23 USGS40000161100 24 USGS40000161096  | . • |                 |
| 14 USG\$40000161295 15 USG\$40000161296 16 USG\$40000161234 17 USG\$40000161194 18 USG\$40000161179 19 USG\$40000161176 19 USG\$40000161177 20 USG\$40000161136 21 USG\$40000161132 22 USG\$40000161132 23 USG\$40000161100 24 USG\$40000161096   |     | USGS40000161304 |
| 15 USGS40000161296<br>16 USGS40000161234<br>17 USGS40000161194<br>18 USGS40000161179<br>19 USGS40000161176<br>19 USGS40000161177<br>20 USGS40000161136<br>21 USGS40000161132<br>22 USGS40000161122<br>23 USGS40000161100<br>24 USGS40000161096  | 13  | USGS40000161300 |
| 16 USGS40000161234 17 USGS40000161194 18 USGS40000161179 19 USGS40000161176 19 USGS40000161177 20 USGS40000161136 21 USGS40000161132 22 USGS40000161122 23 USGS40000161100 24 USGS40000161096   | 14  | USGS40000161295 |
| 17 USGS40000161194 18 USGS40000161179 19 USGS40000161176 19 USGS40000161177 20 USGS40000161136 21 USGS40000161132 22 USGS40000161122 23 USGS40000161100 24 USGS40000161096  | 15  | USGS40000161296 |
| 18 USGS40000161179 19 USGS40000161176 19 USGS40000161177 20 USGS40000161136 21 USGS40000161132 22 USGS40000161122 23 USGS40000161100 24 USGS40000161096   | 16  | USGS40000161234 |
| 19 USGS40000161176<br>19 USGS40000161177<br>20 USGS40000161136<br>21 USGS40000161132<br>22 USGS40000161122<br>23 USGS40000161100<br>24 USGS40000161096  | 17  | USGS40000161194 |
| 19 USGS40000161177<br>20 USGS40000161136<br>21 USGS40000161132<br>22 USGS40000161122<br>23 USGS40000161100<br>24 USGS40000161096  | 18  | USGS40000161179 |
| 20 USGS40000161136<br>21 USGS40000161132<br>22 USGS40000161122<br>23 USGS40000161100<br>24 USGS40000161096  | 19  | USGS40000161176 |
| 21 USGS40000161132<br>22 USGS40000161122<br>23 USGS40000161100<br>24 USGS40000161096  | 19  | USGS40000161177 |
| 22 USGS40000161122<br>23 USGS40000161100<br>24 USGS40000161096  | 20  | USGS40000161136 |
| 23 USGS40000161100<br>24 USGS40000161096  | 21  | USGS40000161132 |
| 24 USGS40000161096  | 22  | USGS40000161122 |
|   | 23  | USGS40000161100 |
| 23 USGS40000161097  | 24  | USGS40000161096 |
|   | 23  | USGS40000161097 |
| 23 USGS40000161098  | 23  | USGS40000161098 |
| 25 USGS40000161086  | 25  | USGS40000161086 |
| 26 USGS40000161057  | 26  | USGS40000161057 |
| 27 USGS40000161036  | 27  | USGS40000161036 |
| 28 USGS40000161015  | 28  |                 |
| 29 USGS40000161014  | 29  |                 |
| 30 USGS40000161011  |     |                 |
| 31 USGS40000161012  | 31  |                 |
| 34 USGS40000160917  | 34  | USGS40000160917 |

## STATE WATER WELL INFORMATION

| MAP<br>ID | WELL<br><u>ID</u> |
|-----------|-------------------|
| 1         | CADWR8000016949   |
| 2         | CADWR8000016908   |
| 3         | CADWR8000016895   |
| 6         | CADWR8000016784   |
| 7         | CADWR8000016733   |
| 8         | CADWR8000016730   |
| 9         | CADWR8000016721   |
| 11        | 17892             |
| 10        | CADWR8000016688   |
| 12        | CADWR8000016686   |
| 13        | CADWR8000016684   |
| 14        | CADWR8000016681   |
| 15        | CADWR8000016679   |
| 16        | CADWR8000016633   |

## GEOCHECK VERSION 2.1 SUMMARY

## STATE WATER WELL INFORMATION

| MAP<br>ID | WELL<br><u>ID</u> |
|-----------|-------------------|
| 17        | CADWR8000016601   |
| 18        | CADWR8000016588   |
| 19        | CADWR8000016586   |
| 20        | CADWR8000016562   |
| 21        | CADWR8000016560   |
| 23        | CADWR8000016535   |
| 23        | CADWR8000016534   |
| 24        | CADWR8000016533   |
| 25        | CADWR8000016526   |
| 26        | CADWR8000016504   |
| 27        | CADWR8000016492   |
| 28        | CADWR8000016478   |
| 31        | CADWR8000016476   |
| 30        | CADWR8000016475   |
| 32        | 18194             |
| 33        | 18195             |
| 34        | CADWR8000016395   |

## STATE OIL/GAS WELL INFORMATION

| MAP       | WELL            |
|-----------|-----------------|
| <u>ID</u> | <u>ID</u>       |
| 1         | CAOG13000002552 |
| 2         | CAOG13000002553 |
| 3         | CAOG13000002554 |
| 4         | CAOG13000002879 |
| 5         | CAOG13000002878 |

## PUBLIC WATER SUPPLY SYSTEM INFORMATION

NO WELLS FOUND

## **USGS TOPOGRAPHIC MAP(S)**

35117-B8 CALIFORNIA CITY NORTH, CA 35118-B1 MOJAVE NE, CA

## AREA RADON INFORMATION

Federal Area Radon Information for Zip Code: 93505

Number of sites tested: 1

| Area                    | Average Activity | % <4 pCi/L   | % 4-20 pCi/L | % >20 pCi/L  |
|-------------------------|------------------|--------------|--------------|--------------|
| Living Area - 1st Floor | 0.200 pCi/L      | 100%         | 0%           | 0%           |
| Living Area - 2nd Floor | Not Reported     | Not Reported | Not Reported | Not Reported |
| Basement                | Not Reported     | Not Reported | Not Reported | Not Reported |

Federal EPA Radon Zone for KERN County: 2

Note: Zone 1 indoor average level > 4 pCi/L.

: Zone 2 indoor average level >= 2 pCi/L and <= 4 pCi/L.

: Zone 3 indoor average level < 2 pCi/L.

## GEOCHECK VERSION 2.1 SUMMARY

## AREA RADON INFORMATION

Federal Area Radon Information for KERN COUNTY, CA

Number of sites tested: 94

Area Average Activity % <4 pCi/L % 4-20 pCi/L % >20 pCi/L

Living Area - 1st Floor 1.422 pCi/L 98% 2% 0%

Living Area - 2nd Floor Not Reported Not Reported

#### Water Well Information:

Map ID: 2

Well Hole Depth Units:

Feet below surface:

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 031S037E15L001M Well Type: Description: HUC: 18090206 Not Reported Drainage Area: Not Reported **Drainage Area Units:** Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date:19800508Well Depth:350Well Depth Units:ftWell Hole Depth:350

Ground water levels, Number of Measurements: 2 Level reading date: 1980-05-08

Feet to sea level:

Not Reported

Note: Not Reported

ft

237

Level reading date: 1980-05-08 Feet below surface: 237

Feet to sea level: Not Reported Note: Not Reported

Map ID: 3

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 031S037E14L001M Well Type: Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Central Valley aquifer system

Formation Type: Not Reported Aquifer Type: Not Reported Construction Date: 19140101 Well Depth: Not Reported Well Depth Units: Not Reported Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 2 Level reading date: 1953-01-22 Feet below surface: 196.60 Feet to sea level: Not Reported

Note: Not Reported

Level reading date: 1929-10-01 Feet below surface: 184.50
Feet to sea level: Not Reported Note: Not Reported

TC5759392.2w Page 1 of 54

Map ID:

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center Monitor Location: 031S037E23K001M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Contrib Drainage Area Unts: Not Reported Not Reported

Aquifer:

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: 19530101 Well Depth: 205

Basin and Range basin-fill aquifers

Well Hole Depth: Well Depth Units: Not Reported

Well Hole Depth Units: Not Reported

Map ID: 5

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center Monitor Location: 031S037E22J001M Well Type: HUC: Description: Not Reported 18090206 Not Reported Drainage Area: Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth:

Well Depth Units: Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Map ID: 5

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 031S037E22R001M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer:

Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth:

Well Depth Units: Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Map ID: 6

USGS-CA Organization ID:

Organization Name: USGS California Water Science Center Monitor Location: 031S037E22Q001M Well Type: Description: Not Reported 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Contrib Drainage Area Unts: Not Reported Not Reported

Basin and Range basin-fill aquifers Aquifer:

Formation Type: Not Reported Aquifer Type: Not Reported Construction Date: 19140101 Well Depth: Not Reported Well Depth Units: Not Reported Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 15 Level reading date: 1960-03-02 Feet below surface: Not Reported Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Level reading date: 1959-12-02 Feet below surface: 298.21
Feet to sea level: Not Reported Note: Not Reported

Total out to the following the

Level reading date: 1959-03-10 Feet below surface: 274.83
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1958-11-05 Feet below surface: 273.73
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1957-11-22 Feet below surface: 269.32

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1957-11-01 Feet below surface: 269.00

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1957-03-06 Feet below surface: 268.97

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1956-11-27 Feet below surface: 267.91

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1956-03-22 Feet below surface: 265.99
Feet to sea level: Not Reported Note: Not Reported

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Level reading date: 1955-11-15 Feet below surface: 265.09

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1955-03-02 Feet below surface: 262.93

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1954-12-03 Feet below surface: 262.14

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1954-03-15 Feet below surface: 260.15

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1953-01-22 Feet below surface: 257.77

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1929-09-30 Feet below surface: 253.00

Feet to sea level: Not Reported Note: Not Reported

Map ID: 7

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center

Monitor Location: 031S037E30F001M Well Type: Description: Not Reported HUC: 18090206 Drainage Area Units: Drainage Area: Not Reported Not Reported Contrib Drainage Area Unts: Contrib Drainage Area: Not Reported Not Reported

Aquifer: Basin and Range basin-fill aquifers

Not Reported Formation Type: Not Reported Aquifer Type:

Well Depth: Construction Date: Not Reported 331

Well Depth Units: Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

21 1978-03-28 Ground water levels, Number of Measurements: Level reading date:

Feet below surface: Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1976-03-08 Feet below surface: 322.90

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1975-10-16 Feet below surface: 322.12

Feet to sea level: Not Reported Note: Not Reported

Feet below surface: Level reading date: 1975-02-06 321.42

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1974-10-23 Feet below surface: 321.79

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1974-02-12 Feet below surface: 320.95

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1973-10-02 Feet below surface: 324.25

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1973-02-15 Feet below surface: 325.65

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1972-10-12 Feet below surface: 327.40

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1972-03-15 Feet below surface: 319.99 Note:

Feet to sea level: Not Reported Not Reported

Level reading date: 1971-10-27 Feet below surface: 319.58

Feet to sea level: Not Reported Not Reported Note:

Level reading date: 1971-03-17 Feet below surface: 318.87

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1970-10-21 Feet below surface: 318.82

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1970-03-17 Feet below surface: 318.86

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1969-04-15 Feet below surface: 321.50

Not Reported Feet to sea level: Not Reported Note:

Level reading date: 1968-03-20 Feet below surface: 327.82

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1967-01-04 Feet below surface: 313.64 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1958-01-28 Feet below surface: 307.20 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1930-03-05 Feet below surface: 300.50

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1929-10-03 Feet below surface: 300.80

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1917-10-03 Feet below surface: 304.00

Feet to sea level: Not Reported Note: Not Reported

Map ID: 8

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center

Monitor Location: 031S037E28H001M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported **Drainage Area Units:** Not Reported Contrib Drainage Area Unts: Contrib Drainage Area: Not Reported Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth: 585

Well Depth Units: ft Well Hole Depth:

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 12 Level reading date: 1965-07-26 Feet below surface: 239.40 Feet to sea level: Not Reported

Note: Not Reported

Level reading date: 1965-06-03 Feet below surface: 239.29
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1965-05-05 Feet below surface: 237.01

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1965-04-01 Feet below surface: 234.95
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1965-02-14 Feet below surface: 233.37
Feet to sea level: Not Reported Note: Not Reporte

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1965-01-14 Feet below surface: 233.40
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1964-12-15 Feet below surface: 233.08
Feet to sea level: Not Reported Note: Not Report

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1964-11-11 Feet below surface: 232.96
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1964-10-13 Feet below surface: 234.50 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1964-09-11 Feet below surface: 233.67

Not Reported

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1964-08-12 Feet below surface: 235.61

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1964-06-11 Feet below surface: 233.87

Feet to sea level: Not Reported Note: Not Reported

Map ID: 9

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 031S037E26K001M Well Type: Description: Not Reported 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported Construction Date: Not Reported Well Depth: Not Reported Well Depth Units: Not Reported Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 6 Level reading date: 1958-01-30

Feet below surface: 244.36 Feet to sea level: Not Reported

Note: Not Reported

Level reading date: 1958-01-01 Feet below surface: 244.00
Feet to sea level: Not Reported Note: Not Reported

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Level reading date: 1956-08-16 Feet below surface: 237.75 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1930-03-05 Feet below surface: 231.40
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1929-09-30 Feet below surface: 231.00

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1918-02-06 Feet below surface: 233.00

Feet to sea level: Not Reported Note: Not Reported

Map ID: 10

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center

Monitor Location: 031S037E28Q001M Well Type: Description: HUC: 18090206 Not Reported Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: 19560101 Well Depth: 600

Well Depth Units: ft Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements:
1 Level reading date: 1958-01-28
Feet below surface: 243.43 Feet to sea level: Not Reported

Note: Not Reported

Map ID: 12

Organization ID: USGS-CA

USGS California Water Science Center Organization Name: Monitor Location: 031S037E28P001M Well Type: Description: Not Reported HUC: 18090206 Drainage Area: Not Reported **Drainage Area Units:** Not Reported Contrib Drainage Area: Contrib Drainage Area Unts: Not Reported Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported Construction Date: 19570101 Well Depth: Not Reported Well Depth Units: Not Reported Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 1 Level reading date: 1958-01-28 Feet below surface: 266.33 Feet to sea level: Not Reported

Note: Not Reported

Map ID: 13

Organization ID: USGS-CA

USGS California Water Science Center Organization Name: Monitor Location: 031S037E32Z001M Well Type: Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Not Reported Contrib Drainage Area: Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth: 349
Well Depth Units: ft Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 1 Level reading date: 1917-10-03
Feet below surface: 307.00 Feet to sea level: Not Reported

Note: Not Reported

Map ID: 14

Organization ID: USGS-CA
Organization Name: USGS California Water Science Center

Monitor Location: 031S037E33Z001M Type: Well
Description: Not Reported HUC: 18090206
Drainage Area: Not Reported Drainage Area Units: Not Reported
Contrib Drainage Area: Not Reported Contrib Drainage Area Units: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported Construction Date: Not Reported Well Depth: Not Reported

Well Depth Units: Not Reported Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 2 Level reading date: 1930-03-05 Feet below surface: 256.18 Feet to sea level: Not Reported

Note: Not Reported

Level reading date: 1929-09-30 Feet below surface: 255.78

Feet to sea level: Not Reported Note: Not Reported

Map ID: 15

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center

Monitor Location: 031S037E32A001M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Not Reported Drainage Area Units: Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth: 349

Well Depth Units: ft Well Hole Depth:

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 5 Level reading date: 1960-03-05 Feet below surface: 276.40 Feet to sea level: Not Reported

Note: Not Reported

Level reading date: 1953-01-23 Feet below surface: Not Reported

Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Level reading date: 1930-03-05 Feet below surface: 276.40
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1929-10-01 Feet below surface: 276.20

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1917 Feet below surface: 274.00

Feet to sea level: Not Reported Note: Not Reported

Map ID: 16

Organization ID: USGS-CA
Organization Name: USGS California Water Science Center

Monitor Location: 031S037E33H001M Type: Well
Description: Not Reported HUC: 18090206
Drainage Area: Not Reported Drainage Area Units: Not Reported
Contrib Drainage Area: Not Reported Contrib Drainage Area Units: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth: 535

Well Depth Units: ft Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Not Reported

| Ground water levels, Number of M<br>Feet below surface:<br>Note: | Measurements:<br>276.04<br>Not Reported | 150 | Level reading date:<br>Feet to sea level: | 2004-09-15<br>Not Reported |
|--|---|-----|---|----------------------------|
| Level reading date:  | 2004-09-15                              |     | Feet below surface:                       | 276.04                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2004-03-30                              |     | Feet below surface:                       | 275.28                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2004-03-30                              |     | Feet below surface:                       | 275.28                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2003-09-16                              |     | Feet below surface:                       | 275.61                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2003-09-16                              |     | Feet below surface:                       | 275.61                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2003-03-25                              |     | Feet below surface:                       | 275.24                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2003-03-25                              |     | Feet below surface:                       | 275.24                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2002-09-17                              |     | Feet below surface:                       | 275.62                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2002-09-17                              |     | Feet below surface:                       | 275.62                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2002-03-27                              |     | Feet below surface:                       | 275.09                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2002-03-27                              |     | Feet below surface:                       | 275.09                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2001-09-11                              |     | Feet below surface:                       | 275.75                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2001-09-11                              |     | Feet below surface:                       | 275.75                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2001-03-22                              |     | Feet below surface:                       | 275.10                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2001-03-22                              |     | Feet below surface:                       | 275.10                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2000-09-13                              |     | Feet below surface:                       | 275.72                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2000-09-13                              |     | Feet below surface:                       | 275.72                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2000-03-22                              |     | Feet below surface:                       | 275.35                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 2000-03-22                              |     | Feet below surface:                       | 275.35                     |
| Feet to sea level:   | Not Reported                            |     | Note:                                     | Not Reported               |
| Level reading date:  | 1999-11-17                              |     | Feet below surface:                       | 275.87                     |

| Feet to sea level:  | Not Reported | Note:               | Not Reported |
|---------------------|--------------|---------------------|--------------|
| Level reading date: | 1999-11-17   | Feet below surface: | 275.87       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1999-03-17   | Feet below surface: | 274.96       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1999-03-17   | Feet below surface: | 274.96       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1998-11-04   | Feet below surface: | 275.36       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1998-11-04   | Feet below surface: | 275.36       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1998-03-18   | Feet below surface: | 274.86       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1998-03-18   | Feet below surface: | 274.86       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1997-11-17   | Feet below surface: | 275.69       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1997-11-17   | Feet below surface: | 275.69       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1997-03-05   | Feet below surface: | 275.30       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1997-03-05   | Feet below surface: | 275.30       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1996-11-14   | Feet below surface: | 275.64       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1996-11-14   | Feet below surface: | 275.64       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1996-04-15   | Feet below surface: | 275.59       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1996-04-15   | Feet below surface: | 275.59       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1995-12-06   | Feet below surface: | 275.97       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1995-12-06   | Feet below surface: | 275.97       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1995-04-17   | Feet below surface: | 275.88       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1995-04-17   | Feet below surface: | 275.88       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1994-10-27   | Feet below surface: | 276.69       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

| Level reading date: | 1994-10-27   | Feet below surface: | 276.69       |
|---------------------|--------------|---------------------|--------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1994-04-13   | Feet below surface: | 276.97       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1994-04-13   | Feet below surface: | 276.97       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1993-11-18   | Feet below surface: | 277.80       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1993-11-18   | Feet below surface: | 277.80       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1993-04-21   | Feet below surface: | 277.04       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1993-04-21   | Feet below surface: | 277.04       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1992-11-04   | Feet below surface: | 278.61       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1992-11-04   | Feet below surface: | 278.61       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1992-04-16   | Feet below surface: | 277.09       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1992-04-16   | Feet below surface: | 277.09       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1991-10-22   | Feet below surface: | 278.27       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1991-10-22   | Feet below surface: | 278.27       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1991-03-22   | Feet below surface: | 278.50       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1991-03-22   | Feet below surface: | 278.50       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1990-10-15   | Feet below surface: | 282.18       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1990-10-15   | Feet below surface: | 282.18       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1990-03-14   | Feet below surface: | 278.98       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1990-03-14   | Feet below surface: | 278.98       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1989-10-18   | Feet below surface: | 280.77       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1989-10-18   | Feet below surface: | 280.77       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

| Level reading date:                       | 1989-03-21                 | Feet below surface:          | 278.24                 |
|---|----------------------------|------------------------------|------------------------|
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1989-03-21                 | Feet below surface:          | 278.24                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1988-03-29                 | Feet below surface:          | 280.30                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1988-03-29                 | Feet below surface:          | 280.30                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1987-11-04                 | Feet below surface:          | 280.20                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:<br>Feet to sea level: | 1987-11-04<br>Not Reported | Feet below surface:<br>Note: | 280.20<br>Not Reported |
| Level reading date: Feet to sea level:    | 1987-02-23                 | Feet below surface:          | 276.82                 |
|   | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1987-02-23                 | Feet below surface:          | 276.82                 |
| Feet to sea level:  Level reading date:   | Not Reported<br>1986-10-23 | Note: Feet below surface:    | Not Reported 280.15    |
| Feet to sea level:  Level reading date:   | Not Reported<br>1986-10-23 | Note: Feet below surface:    | Not Reported 280.15    |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1986-03-26                 | Feet below surface:          | 277.74                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1986-03-26                 | Feet below surface:          | 277.74                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1985-10-31                 | Feet below surface:          | 278.42                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1985-10-31                 | Feet below surface:          | 278.42                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1985-05-16                 | Feet below surface:          | 278.19                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1985-05-16                 | Feet below surface:          | 278.19                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1984-10-30                 | Feet below surface:          | 278.50                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1984-10-30                 | Feet below surface:          | 278.50                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1984-03-07                 | Feet below surface:          | 276.17                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1984-03-07                 | Feet below surface:          | 276.17                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |
| Level reading date:                       | 1983-10-27                 | Feet below surface:          | 278.19                 |
| Feet to sea level:                        | Not Reported               | Note:                        | Not Reported           |

| Level reading date: | 1983-10-27   | Feet below surface: | 278.19       |
|---------------------|--------------|---------------------|--------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1983-04-14   | Feet below surface: | 277.28       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1983-04-14   | Feet below surface: | 277.28       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1982-10-07   | Feet below surface: | 279.13       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1982-10-07   | Feet below surface: | 279.13       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1982-02-11   | Feet below surface: | 274.14       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1982-02-11   | Feet below surface: | 274.14       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1981-11-19   | Feet below surface: | 279.40       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1981-11-19   | Feet below surface: | 279.40       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1981-04-16   | Feet below surface: | 278.85       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1981-04-16   | Feet below surface: | 278.85       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1980-10-15   | Feet below surface: | 281.05       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1980-10-15   | Feet below surface: | 281.05       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1980-04-16   | Feet below surface: | 279.91       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1980-04-16   | Feet below surface: | 279.91       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1979-10-24   | Feet below surface: | 279.39       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1979-10-24   | Feet below surface: | 279.39       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1979-02-13   | Feet below surface: | 275.26       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1979-02-13   | Feet below surface: | 275.26       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1978-03-28   | Feet below surface: | 277.40       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1978-03-28   | Feet below surface: | 277.40       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

| Level reading date: | 1977-03-08   | Feet below surface: | 279.05       |
|---------------------|--------------|---------------------|--------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1977-03-08   | Feet below surface: | 279.05       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1976-02-12   | Feet below surface: | 276.78       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1976-02-12   | Feet below surface: | 276.78       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1976-01-06   | Feet below surface: | 275.19       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1976-01-06   | Feet below surface: | 275.19       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1975-02-05   | Feet below surface: | 273.70       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1975-02-05   | Feet below surface: | 273.70       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1974-02-12   | Feet below surface: | 275.16       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1974-02-12   | Feet below surface: | 275.16       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1973-02-15   | Feet below surface: | 272.73       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1973-02-15   | Feet below surface: | 272.73       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1972-03-15   | Feet below surface: | 280.31       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1972-03-15   | Feet below surface: | 280.31       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-10-28   | Feet below surface: | 277.25       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-10-28   | Feet below surface: | 277.25       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-03-17   | Feet below surface: | 279.30       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-03-17   | Feet below surface: | 279.30       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1970-10-22   | Feet below surface: | 278.79       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1970-10-22   | Feet below surface: | 278.79       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1970-03-17   | Feet below surface: | 279.10       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

| Level reading date: | 1970-03-17   | Feet below surface: | 279.10       |
|---------------------|--------------|---------------------|--------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1969-04-15   | Feet below surface: | 277.59       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1969-04-15   | Feet below surface: | 277.59       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1968-03-21   | Feet below surface: | 277.83       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1968-03-21   | Feet below surface: | 277.83       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-01-04   | Feet below surface: | 269.34       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-01-04   | Feet below surface: | 269.34       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1965-04-01   | Feet below surface: | 268.50       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1965-04-01   | Feet below surface: | 268.50       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1965-01-14   | Feet below surface: | 267.61       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1965-01-14   | Feet below surface: | 267.61       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1964-12-15   | Feet below surface: | 267.52       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1964-12-15   | Feet below surface: | 267.52       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1964-10-13   | Feet below surface: | 268.23       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1964-10-13   | Feet below surface: | 268.23       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1964-09-11   | Feet below surface: | 268.17       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1964-09-11   | Feet below surface: | 268.17       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1961-07-26   | Feet below surface: | 274.75       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1961-07-26   | Feet below surface: | 274.75       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1959-02-04   | Feet below surface: | 270.00       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1959-02-04   | Feet below surface: | 270.00       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

Level reading date: 1958-01-28 Feet below surface: 274.48
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1958-01-28 Feet below surface: 274.48
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1956-06-19 Feet below surface: 230.00 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1956-06-19 Feet below surface: 230.00

Feet to sea level: Not Reported Note: Not Reported

Map ID: 17

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center
Monitor Location: 031S037E34A001M Type:

Description:Not ReportedHUC:18090206Drainage Area:Not ReportedDrainage Area Units:Not ReportedContrib Drainage Area:Not ReportedContrib Drainage Area Units:Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: 19140101 Well Depth: 205

Well Depth Units: ft Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 8 Level reading date: 1958-01-29 Feet below surface: Not Reported Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Level reading date: 1958-01-29 Feet below surface: Not Reported

Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Level reading date: 1953-01-22 Feet below surface: 200.95
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1953-01-22 Feet below surface: 200.95

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1930-03-05 Feet below surface: 201.11
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1930-03-05 Feet below surface: 201.11

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1929-10-01 Feet below surface: 200.61

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1929-10-01 Feet below surface: 200.61

Feet to sea level: Not Reported Note: Not Reported

Well

Map ID: 18

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center

Monitor Location: 031S037E35N001M Well Type: Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area Unts: Contrib Drainage Area: Not Reported Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported Construction Date: 19520101 Well Depth: 405.25 Well Depth Units: tt Well Hole Depth: 444

Well Hole Depth Units: ft

Ground water levels, Number of Measurements: 97 Level reading date: 2004-09-15

Feet below surface: 254.16 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2004-03-30 Feet below surface: 253.75

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2003-09-16 Feet below surface: 254.02

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2003-03-25 Feet below surface: 254.06

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2002-09-17 Feet below surface: 254.31

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2002-03-27 Feet below surface: 253.94

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2001-09-11 Feet below surface: 254.39

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2001-03-22 Feet below surface: 253.81

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2000-09-13 Feet below surface: 254.32

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2000-03-22 Feet below surface: 254.52

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1999-11-17 Feet below surface: 254.95

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1999-03-17 Feet below surface: 253.76

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1998-11-04 Feet below surface: 254.10

Feet to sea level: Not Reported Note: Not Reported

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Level reading date: 1998-03-18 Feet below surface: 254.11
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1997-11-17 Feet below surface: 254.66

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1997-03-05 Feet below surface: 254.60

Feet to sea level: Not Reported Note: Not Reported

| Level reading date: | 1996-11-14   | Feet below surface: | 254.86       |
|---------------------|--------------|---------------------|--------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1996-04-15   | Feet below surface: | 255.24       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1995-12-06   | Feet below surface: | 255.85       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1995-04-17   | Feet below surface: | 256.16       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1994-10-27   | Feet below surface: | 256.75       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1994-04-13   | Feet below surface: | 257.44       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1993-11-18   | Feet below surface: | 257.46       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1993-04-21   | Feet below surface: | 257.54       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1992-11-04   | Feet below surface: | 258.09       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1992-04-16   | Feet below surface: | 256.53       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1991-10-22   | Feet below surface: | 257.39       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1991-04-18   | Feet below surface: | 257.64       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1990-10-15   | Feet below surface: | 259.60       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1990-03-14   | Feet below surface: | 258.69       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1989-10-18   | Feet below surface: | 258.19       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1989-03-21   | Feet below surface: | 257.72       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1988-03-29   | Feet below surface: | 257.74       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1987-11-04   | Feet below surface: | 258.13       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1987-02-23   | Feet below surface: | 255.76       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1986-10-23   | Feet below surface: | 257.32       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1986-03-26   | Feet below surface: | 255.35       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

| Level reading date: | 1985-10-31   | Feet below surface: | 256.36       |
|---------------------|--------------|---------------------|--------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1985-05-16   | Feet below surface: | 256.70       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1984-10-30   | Feet below surface: | 256.39       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1984-03-07   | Feet below surface: | 256.04       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1983-10-27   | Feet below surface: | 256.04       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1983-04-14   | Feet below surface: | 256.03       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1982-10-07   | Feet below surface: | 256.66       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1982-02-11   | Feet below surface: | 254.84       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1981-11-19   | Feet below surface: | 255.90       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1981-04-16   | Feet below surface: | 256.72       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1980-10-15   | Feet below surface: | 257.13       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1980-04-16   | Feet below surface: | 258.98       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1979-10-24   | Feet below surface: | 261.91       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1979-02-13   | Feet below surface: | 255.37       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1978-10-16   | Feet below surface: | 255.89       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1978-03-28   | Feet below surface: | 254.20       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1977-10-12   | Feet below surface: | 256.00       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1977-03-08   | Feet below surface: | 256.98       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1976-11-03   | Feet below surface: | 254.89       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1976-02-12   | Feet below surface: | 254.98       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1975-10-16   | Feet below surface: | 255.45       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

| Level reading date: | 1975-02-05   | Feet below surface: | 251.40       |
|---------------------|--------------|---------------------|--------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1974-10-23   | Feet below surface: | 253.18       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1974-02-12   | Feet below surface: | 251.60       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1973-10-02   | Feet below surface: | 254.01       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1973-02-14   | Feet below surface: | 253.25       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1972-10-12   | Feet below surface: | 254.09       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1972-03-15   | Feet below surface: | 253.28       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-10-28   | Feet below surface: | 253.48       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-03-17   | Feet below surface: | 252.25       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1970-10-22   | Feet below surface: | 250.65       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1970-03-17   | Feet below surface: | 249.90       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1969-09-18   | Feet below surface: | 255.80       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1969-04-15   | Feet below surface: | 267.04       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1968-10-31   | Feet below surface: | 249.30       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1968-03-21   | Feet below surface: | 248.17       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-10-11   | Feet below surface: | 248.12       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-04-12   | Feet below surface: | 247.33       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-01-04   | Feet below surface: | 247.00       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1966-10-17   | Feet below surface: | 246.37       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1966-03-09   | Feet below surface: | 244.09       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1965-10-18   | Feet below surface: | 244.00       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

| Level reading date: | 1965-03-16   | Feet below surface: | 242.54                     |
|---------------------|--------------|---------------------|----------------------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1964-10-07   | Feet below surface: | 242.68                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1964-03-04   | Feet below surface: | 244.49                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1963-11-07   | Feet below surface: | 244.41                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1963-03-13   | Feet below surface: | 244.82                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1962-11-09   | Feet below surface: | 243.73                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1962-03-15   | Feet below surface: | 245.18                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1961-11-14   | Feet below surface: | 245.49                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1961-02-27   | Feet below surface: | 246.20                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1960-11-10   | Feet below surface: | 245.60                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1960-03-02   | Feet below surface: | 247.38                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1959-12-02   | Feet below surface: | 247.92                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1959-03-10   | Feet below surface: | 246.04                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1958-03-04   | Feet below surface: | 243.72                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1958-03-01   | Feet below surface: | 244.00                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1958-01-30   | Feet below surface: | 244.08                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1953-04-14   | Feet below surface: | 292.50                     |
| Feet to sea level:  | Not Reported | Note:               | The site was being pumped. |
| Level reading date: | 1953-01-22   | Feet below surface: | 230.79                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |

Map ID: 19

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 032S037E04D001M Type: Well HUC: Description: Not Reported 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area Unts: Contrib Drainage Area: Not Reported Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: 19520101 Well Depth: 650

Well Depth Units: ft Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 6 Level reading date: 1967-01-04 Feet below surface: Not Reported Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Level reading date: 1961-07-26 Feet below surface: 312.16
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1959-02-04 Feet below surface: 323.00 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1958-01-28 Feet below surface: 335.19
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1953-04-17 Feet below surface: 365.00

Feet to sea level: Not Reported Note: The site was being pumped.

Level reading date: 1953-01-23 Feet below surface: 301.06
Feet to sea level: Not Reported Note: Not Reported

Map ID: 19

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 032S037E04D002M Type: Well HUC: Description: Not Reported 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported Construction Date: Not Reported Well Depth: Not Reported Well Depth: Not Reported Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Map ID: 20

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 032S037E02E001M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Well Hole Depth:

Well Hole Depth:

Not Reported

Not Reported

Construction Date: Not Reported Well Depth:

Well Depth Units:

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 3 Level reading date: 1930-02-25 Feet to sea level: Not Reported

Feet below surface: 242.63

Not Reported Note:

Level reading date: 1929-09-30 Feet below surface: 251.40

Feet to sea level: Not Reported

Note: The site had been pumped recently.

Level reading date: 1917 Feet below surface: 244.00

Feet to sea level: Not Reported Note: Not Reported

Map ID: 21

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center

Monitor Location: 032S037E02F001M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Not Reported **Drainage Area Units:** Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Not Reported Formation Type: Not Reported Aguifer Type:

Construction Date: Not Reported Well Depth: 206

Well Depth Units: ft

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 2 Level reading date: 1958-01-30 Feet below surface: Not Reported Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Level reading date: 1953-02-09 Feet below surface: 232.41

Feet to sea level: Not Reported Not Reported Note:

Map ID: 22

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center Monitor Location: 032S037E06L001M Type: Well Description: Not Reported HUC: 18090206 Not Reported Drainage Area Units: Drainage Area: Not Reported Contrib Drainage Area Unts: Contrib Drainage Area: Not Reported Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Well Depth: Construction Date: Not Reported 85

Well Depth Units: Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Map ID: 23

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 032S037E04Q001M Well Type: Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Contrib Drainage Area Unts: Not Reported Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth: 427

Well Depth Units: ft Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 8 Level reading date: 1957-03-06 Feet below surface: Not Reported Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Level reading date: 1956-11-27 Feet below surface: Not Reported

Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Level reading date: 1956-03-22 Feet below surface: 317.87

Feet to sea level: Not Reported Note:

Level reading date: 1955-03-02 Feet below surface: 310.64

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1954-03-15 Feet below surface: 315.55

Feet to sea level: Not Reported

Note: A nearby site that taps the same aquifer was being pumped.

Level reading date: 1953-01-23 Feet below surface: 302.98

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1930-02-25 Feet below surface: 304.30

Feet to sea level: Not Reported Note:

Level reading date: 1929-09-30 Feet below surface: 303.20

Feet to sea level: Not Reported Note: Not Reported

Map ID: 24

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 032S037E01N001M Well Type: Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported Construction Date: Not Reported Well Depth: Not Reported Well Depth Units: Not Reported Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 18 Level reading date: 1967-01-04 Feet below surface: Not Reported Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Not Reported

Not Reported

| Level reading date:<br>Feet to sea level:<br>Note: | 1961-02-27<br>Not Reported<br>The site was dry (no water level recor | Feet below surface: ded). | Not Reported |
|--|--|---------------------------|--------------|
| Level reading date:                                | 1960-11-10   | Feet below surface:       | 230.30       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1960-03-02   | Feet below surface:       | 230.83       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1959-12-02   | Feet below surface:       | 231.14       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1959-03-10   | Feet below surface:       | 230.49       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1958-11-05   | Feet below surface:       | 231.20       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1958-02-03   | Feet below surface:       | 229.71       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1958-02-01   | Feet below surface:       | 230.00       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1957-11-22   | Feet below surface:       | 230.11       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1957-03-06   | Feet below surface:       | 229.98       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1956-11-27   | Feet below surface:       | 227.72       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1956-03-22   | Feet below surface:       | 225.28       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1955-11-15   | Feet below surface:       | 225.43       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1955-03-02   | Feet below surface:       | 225.16       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1954-12-03   | Feet below surface:       | 226.03       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1954-03-15   | Feet below surface:       | 226.48       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |
| Level reading date:                                | 1953-02-09   | Feet below surface:       | 223.59       |
| Feet to sea level:                                 | Not Reported   | Note:                     | Not Reported |

Map ID: 23

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 032S037E04P001M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area Unts: Contrib Drainage Area: Not Reported Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth: 800

Well Depth Units: ft Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 4 Level reading date: 1976-09-06

Feet below surface: 326.24 Feet to sea level: Not Reported

Note: Not Reported

Level reading date: 1961-07-26 Feet below surface: 318.58 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1958-01-28 Feet below surface: 339.90

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1952-01-01 Feet below surface: 265.00 Feet to sea level: Not Reported Note: Not Reported

Map ID: 23

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center Monitor Location: 032S037E04P002M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported **Drainage Area Units:** Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth: 812
Well Depth Units: ft Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Map ID: 25

Organization ID: USGS-CA

USGS California Water Science Center Organization Name: Monitor Location: 032S037E02N001M Well Type: Description: 18090206 Not Reported HUC: Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth: 90

Well Depth Units: Not Reported Well Hole Depth: Not Reported

Well Depth Units: Not Reported

Well Hole Depth Units: Not Reported

1953-01-22 Ground water levels, Number of Measurements: 3 Level reading date: Feet below surface: Not Reported Feet to sea level: Not Reported

Note: The site was dry (no water level recorded).

Level reading date: 1930-02-25 Feet below surface: 252.32 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1929-09-30 Feet below surface: 251.82 Not Reported

Feet to sea level: Not Reported Note:

26 Map ID:

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center Monitor Location: 032S037E08E001M Well Type: Description: HUC: 18090206 Not Reported Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: Not Reported Well Depth: 410 Well Hole Depth: Not Reported

Well Depth Units:

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 3 Level reading date: 1952-09-18 Feet to sea level: Feet below surface: Not Reported Not Reported

The site was dry (no water level recorded). Note:

Level reading date: Feet below surface: 370.00 1917-01-01 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1917 Feet below surface: 370.00 Feet to sea level: Not Reported Note: Not Reported

Map ID: 27

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center

Monitor Location: 032S037E12M001M Well Type: Description: Not Reported HUC: 18090206 Not Reported Drainage Area: Not Reported Drainage Area Units: Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Not Reported Formation Type: Not Reported Aquifer Type: Well Depth: Construction Date: 1957 430.82 Well Depth Units: Well Hole Depth: Not Reported ft

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 41 Level reading date: 2004-03-30 Feet below surface: 249.36 Feet to sea level: Not Reported

Note: Not Reported

Level reading date: 2003-03-26 Feet below surface: 249.52 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2002-03-27 Feet below surface: 249.04 Feet to sea level: Not Reported Note: Not Reported Level reading date: 2001-03-23 Feet below surface: 249.00 Feet to sea level: Not Reported Note: Not Reported Level reading date: 2000-03-22 Feet below surface: 248.64 Feet to sea level: Not Reported Note: Not Reported 1999-03-16 Level reading date: Feet below surface: Not Reported Feet to sea level: Not Reported An obstruction was encountered in the well above the water surface (no water level recorded). Note: Level reading date: 1998-03-18 Feet below surface: 248.22 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1997-03-07 Feet below surface: 248.07 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1996-04-15 Feet below surface: 247.85 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1995-04-18 Feet below surface: 247.53 Feet to sea level: Not Reported Not Reported Note: Level reading date: 1994-04-13 Feet below surface: 247.72 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1993-04-22 Feet below surface: 247.35 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1992-04-16 Feet below surface: 247.10 Feet to sea level: Not Reported Not Reported Note: Level reading date: 1991-04-19 Feet below surface: 246.70 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1990-03-14 Feet below surface: 246.60 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1989-03-24 Feet below surface: 245.87 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1988-03-30 Feet below surface: 245.74 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1987-02-23 Feet below surface: 244.87 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1986-03-26 Feet below surface: 245.31 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1985-05-16 Feet below surface: 245.01 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1984-03-07 Feet below surface: 244.76 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1983-04-14 Feet below surface: 244.50 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1982-02-11 Feet below surface: 244.37

| Feet to sea level:  | Not Reported | Note:               | Not Reported |
|---------------------|--------------|---------------------|--------------|
| Level reading date: | 1981-04-16   | Feet below surface: | 244.32       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1980-04-16   | Feet below surface: | 244.17       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1979-02-13   | Feet below surface: | 244.06       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1978-03-28   | Feet below surface: | 243.33       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1977-03-07   | Feet below surface: | 243.29       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1976-02-12   | Feet below surface: | 243.05       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1975-02-05   | Feet below surface: | 242.82       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1974-02-12   | Feet below surface: | 242.35       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1973-02-14   | Feet below surface: | 242.45       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1972-03-16   | Feet below surface: | 242.40       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-10-28   | Feet below surface: | 244.33       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-03-18   | Feet below surface: | 242.28       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1970-10-22   | Feet below surface: | 242.30       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1970-03-17   | Feet below surface: | 242.00       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1969-04-15   | Feet below surface: | 242.13       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1968-03-20   | Feet below surface: | 242.72       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-01-04   | Feet below surface: | 243.22       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-01-01   | Feet below surface: | 243.00       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

Map ID: 28

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center Monitor Location: 032S037E12P001M Type: Well HUC: Description: Not Reported 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area Unts: Contrib Drainage Area: Not Reported Not Reported

Aquifer: Basin and Range basin-fill aquifers

Not Reported Formation Type: Not Reported Aquifer Type: Well Depth: Not Reported Construction Date: Not Reported Well Hole Depth: Well Depth Units: Not Reported Not Reported

Well Hole Depth Units: Not Reported

1967-04-01 Ground water levels, Number of Measurements: Level reading date: 1 Feet below surface: 279.00 Feet to sea level: Not Reported

Note: Not Reported

Map ID: 29

**USGS-CA** Organization ID:

Organization Name: USGS California Water Science Center Monitor Location: 032S037E09Z001M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Not Reported **Drainage Area Units:** Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Aquifer Type: Not Reported Formation Type: Not Reported

Construction Date: Not Reported Well Depth: 2232

Well Hole Depth: Well Depth Units: Not Reported ft

Well Hole Depth Units: Not Reported

Map ID: 30

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center Monitor Location: 032S037E11N001M Type: Well Description: Not Reported HUC: 18090206 Drainage Area: Not Reported Drainage Area Units: Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer:

Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: 19520101 Well Depth: 600

Well Hole Depth: Well Depth Units: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: Level reading date: 2004-03-30 66 Feet below surface: 295.48 Feet to sea level: Not Reported

Note: Not Reported

Level reading date: 2003-03-26 Feet below surface: 295.14 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 2002-03-27 Feet below surface: 294.52

| Feet to sea level:  | Not Reported | Note:               | Not Reported |
|---------------------|--------------|---------------------|--------------|
| Level reading date: | 2001-03-23   | Feet below surface: | 294.20       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 2000-03-22   | Feet below surface: | 293.86       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1999-03-17   | Feet below surface: | 293.54       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1998-03-18   | Feet below surface: | 292.91       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1997-03-07   | Feet below surface: | 292.79       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1996-04-15   | Feet below surface: | 292.40       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1995-04-18   | Feet below surface: | 291.88       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1994-04-13   | Feet below surface: | 291.66       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1993-04-21   | Feet below surface: | 291.27       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1992-04-16   | Feet below surface: | 297.36       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1991-04-19   | Feet below surface: | 286.28       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1990-03-14   | Feet below surface: | 293.86       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1989-03-21   | Feet below surface: | 292.96       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1988-03-30   | Feet below surface: | 293.24       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1987-02-23   | Feet below surface: | 292.38       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1986-03-26   | Feet below surface: | 291.68       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1985-05-16   | Feet below surface: | 287.26       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1984-03-07   | Feet below surface: | 286.31       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1983-04-14   | Feet below surface: | 286.16       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1982-02-11   | Feet below surface: | 285.91       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

| Level reading date: | 1981-04-16   | Feet below surface: | 285.78       |
|---------------------|--------------|---------------------|--------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1980-04-16   | Feet below surface: | 289.40       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1978-03-28   | Feet below surface: | 287.19       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1977-03-07   | Feet below surface: | 284.15       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1976-02-12   | Feet below surface: | 283.90       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1975-02-05   | Feet below surface: | 283.17       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1974-02-12   | Feet below surface: | 282.26       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1973-02-14   | Feet below surface: | 281.79       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1972-03-15   | Feet below surface: | 281.38       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-10-28   | Feet below surface: | 281.54       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1971-03-17   | Feet below surface: | 280.68       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1970-10-22   | Feet below surface: | 281.06       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1970-03-17   | Feet below surface: | 280.19       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1969-09-18   | Feet below surface: | 280.88       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1969-04-15   | Feet below surface: | 279.95       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1968-10-31   | Feet below surface: | 280.27       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1968-03-21   | Feet below surface: | 279.86       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-10-11   | Feet below surface: | 279.70       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-04-12   | Feet below surface: | 279.48       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1967-01-04   | Feet below surface: | 279.48       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |
| Level reading date: | 1966-10-17   | Feet below surface: | 279.66       |
| Feet to sea level:  | Not Reported | Note:               | Not Reported |

| Level reading date: | 1966-03-09   | Feet below surface: | 279.32                     |
|---------------------|--------------|---------------------|----------------------------|
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1965-10-18   | Feet below surface: | 279.61                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1965-03-16   | Feet below surface: | 279.47                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1964-10-07   | Feet below surface: | 279.79                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1964-03-04   | Feet below surface: | 279.67                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1963-11-08   | Feet below surface: | 279.97                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1963-03-13   | Feet below surface: | 280.96                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1962-11-09   | Feet below surface: | 279.88                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1962-03-15   | Feet below surface: | 280.02                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1961-11-14   | Feet below surface: | 280.32                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1961-07-26   | Feet below surface: | 275.58                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1961-02-27   | Feet below surface: | 280.51                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1960-11-10   | Feet below surface: | 280.74                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1960-03-02   | Feet below surface: | 281.29                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1959-12-02   | Feet below surface: | 281.63                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1959-03-10   | Feet below surface: | 281.91                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1958-11-05   | Feet below surface: | 280.77                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1958-03-04   | Feet below surface: | 279.08                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1958-03-01   | Feet below surface: | 279.00                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1958-01-30   | Feet below surface: | 280.18                     |
| Feet to sea level:  | Not Reported | Note:               | Not Reported               |
| Level reading date: | 1953-05-01   | Feet below surface: | 389.00                     |
| Feet to sea level:  | Not Reported | Note:               | The site was being pumped. |

Level reading date: 1953-01-22 Feet below surface: 268.09 Feet to sea level: Not Reported Note: Not Reported

Map ID: 31

Organization ID: **USGS-CA** 

Organization Name: USGS California Water Science Center Monitor Location: 032S037E09Q001M Type: Well Description: HUC: 18090206 Not Reported Drainage Area: Not Reported **Drainage Area Units:** Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Not Reported Aquifer Type:

Construction Date: Not Reported Well Depth: Not Reported

Well Hole Depth: Well Depth Units: ft Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 28 Level reading date: 1993-06-10

Feet below surface: Not Reported Feet to sea level: Note: The site was dry (no water level recorded).

Level reading date: 1988-03-29 Feet below surface: 341.69

Feet to sea level: Not Reported Note: Not Reported 337.90

Level reading date: 1987-02-23 Feet below surface: Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1986-04-23 Feet below surface: 341.00 Not Reported

Feet to sea level: Not Reported Note:

Level reading date: 1984-03-07 Feet below surface: 335.79 Not Reported

Feet to sea level: Not Reported Note:

Level reading date: 1983-04-14 Feet below surface: 335.45

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1982-02-11 Feet below surface: 335.70

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1981-04-16 Feet below surface: 336.07 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1980-04-16 Feet below surface: 337.80

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1979-02-14 Feet below surface: 335.87

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1978-03-28 Feet below surface: 335.30

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1977-03-08 Feet below surface: 334.45

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1976-02-12 Feet below surface: 333.65

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1975-02-05 Feet below surface: 333.25

Not Reported

Feet to sea level: Not Reported Note: Not Reported Level reading date: 1974-02-12 Feet below surface: 332.95 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1973-02-14 Feet below surface: 331.45 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1972-03-16 Feet below surface: 331.59 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1971-10-28 Feet below surface: 332.44 Feet to sea level: Not Reported Note: Not Reported Feet below surface: Level reading date: 1971-03-18 332.10 Feet to sea level: Not Reported Note: Not Reported 1970-10-22 Feet below surface: 330.76 Level reading date: Feet to sea level: Not Reported Note: Not Reported Level reading date: 1970-03-17 Feet below surface: 328.96 Not Reported Feet to sea level: Not Reported Note: Feet below surface: Level reading date: 1969-04-15 328.72 Feet to sea level: Note: Not Reported Not Reported Level reading date: 1968-03-21 Feet below surface: 327.90 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1967-01-03 Feet below surface: 328.81 Feet to sea level: Not Reported Note: Not Reported Feet below surface: 1961-07-26 Level reading date: 327.91 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1958-01-28 Feet below surface: 364.67 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1956-06-19 Feet below surface: 275.00 Feet to sea level: Not Reported Note: Not Reported Level reading date: 1953-04-15 Feet below surface: 275.00 Feet to sea level: Not Reported Note: Not Reported

Map ID: 34

Organization ID: USGS-CA

Organization Name: USGS California Water Science Center

032S037E16R001M Well Monitor Location: Type: Not Reported Description: HUC: 18090206 Drainage Area: Drainage Area Units: Not Reported Not Reported Contrib Drainage Area: Not Reported Contrib Drainage Area Unts: Not Reported

Aquifer: Basin and Range basin-fill aquifers

Formation Type: Not Reported Aquifer Type: Not Reported

Construction Date: 19520101 Well Depth: 686

Well Depth Units: 19520101 Well Hole Depth: Not Reported

Well Hole Depth Units: Not Reported

Ground water levels, Number of Measurements: 18 Level reading date: 2004-08-11 Feet below surface: Not Reported Feet to sea level: Not Reported

Note: The site was being pumped.

Level reading date: 2004-08-11 Feet below surface: Not Reported

Feet to sea level: Not Reported Note: The site was being pumped.

Level reading date: 2003-08-27 Feet below surface: Not Reported

Feet to sea level: Not Reported Note: The site was being pumped.

Level reading date: 2003-08-27 Feet below surface: Not Reported

Feet to sea level: Not Reported Note: The site was being pumped.

Level reading date: 1965-10-28 Feet below surface: 345.70
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1965-10-28 Feet below surface: 345.70 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1963-06-03 Feet below surface: 339.00

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1963-06-03 Feet below surface: 339.00 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1961-07-26 Feet below surface: 347.12
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1961-07-26 Feet below surface: 347.12
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1959-02-04 Feet below surface: 358.00
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1959-02-04 Feet below surface: 358.00
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1958-01-28 Feet below surface: 385.59
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1958-01-28 Feet below surface: 385.59
Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1956-06-19 Feet below surface: 390.00 Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1956-06-19 Feet below surface: 390.00 Feet to sea level: Not Reported Note: Not Reported

Feet to sea level: Not Reported Note: Not Reported

Level reading date: 1953-04-30 Feet below surface: 390.00 Feet to sea level: Not Reported Note: Not Reported

Level reading date:1953-04-30Feet below surface:390.00Feet to sea level:Not ReportedNote:Not Reported

#### Water Well Information:

| Map ID:   | 1 |  |
|-----------|---|--|
| iviap ID. | I |  |

State Well #: 31S37E12N001M Station ID: 24180 Well Name: Not Reported Well Use: Unknown Well Type: Unknown Well Depth:

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

Map ID: 2

State Well #: 31S37E15L001M Station ID: 38461 Well Name: Well Use: Unknown Not Reported Well Depth: Well Type: Unknown

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

Map ID: 3

State Well #: 31S37E14L001M Station ID: 24183 Well Name: Not Reported Well Use: Unknown

Well Depth: Well Type: Unknown 0

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

Map ID:

State Well #: 31S37E22Q001M Station ID: 24184 Well Name: Not Reported Well Use: Unknown Well Type: Unknown Well Depth:

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

Map ID: 7

31S37E30F001M State Well #: Station ID: 24187 Well Use: Well Name: Not Reported Unknown Well Depth:

Well Type: Unknown Well Completion Rpt #: Basin Name: Fremont Valley Not Reported

Map ID: 8

State Well #: 31S37E28H001M Station ID: 24185 Well Name: Not Reported Well Use: Unknown

Well Type: Unknown Well Depth:

Not Reported Basin Name: Fremont Valley Well Completion Rpt #:

Map ID: 9 State Well #: 31S37E26K001M Station ID: 38521

Well Name: Not Reported Well Use: Unknown Unknown Well Type: Well Depth:

Well Completion Rpt #: Basin Name: Fremont Valley Not Reported

17892 31S/37E-28P02 M Seq: Prim sta c:

Frds no: 1500333001 County: 15 District: User id: CYA Water type: System no: 1500333 G

WELL 01 - TREATED WELL/AMBNT/MUN/INTAKE Source nam: Station ty:

Latitude: 351158.9 Longitude: 1180038.2 Precision: Status: Comment 1: 500' N OF PHILLIPS RD, 325' W OF YUCAIPA ON SANOMA ST IN FREEMONT VALLEY CA Comment 3: Not Reported Comment 2: Not Reported Not Reported Comment 4: Comment 5: Not Reported Not Reported Comment 6: Comment 7:

System no: 1500333 System nam: ANTELOPE VALLEY WATER COMPANY

PHILLIPS RD & HWY 14 Hqname: Not Reported Address:

MOJAVE State: CA City:

93501 Zip: Zip ext: Not Reported

Pop serv: 200 Connection: 71

Area serve: Not Reported

Sample date: 25-APR-17 Finding: 0.512 Chemical: NITRATE (AS N) Report units: MG/L

DIr: 0.4

12-APR-16 0.655 Sample date: Finding: Chemical: NITRATE (AS N) Report units: MG/L

DIr: 0.4

Sample date: 08-MAR-16 450. Finding: Chemical: TOTAL DISSOLVED SOLIDS Report units: MG/L

DIr:

Sample date: 08-MAR-16 Finding: 0.17 Chemical: FLUORIDE (F) (NATURAL-SOURCE) Report units: MG/L

0.1 DIr:

Sample date: 08-MAR-16 Finding: 100. Chemical: **SULFATE** Report units: MG/L

DIr: 0.5

Sample date: 08-MAR-16 Finding: 76. CHLORIDE Report units: MG/L

Chemical: DIr: 0.

08-MAR-16 Sample date: Finding: 4.1 Report units: MG/L

Chemical: **POTASSIUM** DIr:

Finding: Sample date: 08-MAR-16 87.

SODIUM Chemical: Report units: MG/L

DIr:

Sample date: 08-MAR-16 Finding: 12. Chemical: **MAGNESIUM** Report units: MG/L

DIr:

08-MAR-16 Sample date: Finding: 52. Report units: Chemical: **CALCIUM** MG/L

DIr: 0.

Sample date: 08-MAR-16 Finding: 180.

Report units: Chemical: HARDNESS (TOTAL) AS CACO3 MG/L 0.

DIr:

08-MAR-16 0.48 Sample date: Finding: Chemical: NITRATE (AS N) Report units: MG/L DIr: Sample date: 08-MAR-16 Finding: 190. **BICARBONATE ALKALINITY** Chemical: Report units: MG/L DIr: Finding: Sample date: 08-MAR-16 160. ALKALINITY (TOTAL) AS CACO3 Chemical: Report units: MG/L DIr: Sample date: 08-MAR-16 Finding: 7.2 Chemical: PH, LABORATORY Report units: Not Reported DIr: Sample date: 08-MAR-16 Finding: 730. SPECIFIC CONDUCTANCE Report units: US Chemical: DIr: Sample date: 08-MAR-16 7.24 Finding: Chemical: PH, FIELD Report units: Not Reported DIr: 0. Sample date: 08-MAR-16 Finding: 25. Chemical: SOURCE TEMPERATURE C Report units: С DIr: Sample date: 08-MAR-16 Finding: 130.6 Chemical: **IRON** Report units: UG/L DIr: 100. 08-MAR-16 Sample date: 508.2 Finding: Chemical: **BORON** Report units: UG/L DIr: 100. Sample date: 08-MAR-16 Finding: 4.115 Report units: Chemical: **POTASSIUM** MG/L DIr: 0. Sample date: 08-MAR-16 Finding: 83.97 Chemical: SODIUM Report units: MG/L DIr: 0. Sample date: 08-MAR-16 Finding: 12.67 Chemical: MAGNESIUM Report units: MG/L DIr: 08-MAR-16 Sample date: Finding: 53.53 Chemical: **CALCIUM** Report units: MG/L DIr: 0. Sample date: 08-MAR-16 Finding: 0.48 Chemical: TURBIDITY, LABORATORY Report units: NTU 0.1 Sample date: 08-MAR-16 Finding: 12. AGGRSSIVE INDEX (CORROSIVITY) Chemical: Report units: Not Reported

Sample date:

Chemical:

14-JUL-15

SOURCE TEMPERATURE C

27.4

С

Finding:

Report units:

Finding:

Report units:

7.69

27.2

7.33

27.3

С

С

Not Reported

Not Reported

Not Reported

Not Reported

26.

0.63

PCI/L

Not Reported

7.

26.

С

2.9

0.4

PCI/L

С

DIr: 0.

Sample date: 14-JUL-15 Chemical: PH, FIELD

DIr:

Sample date: 09-JUN-15

Chemical: SOURCE TEMPERATURE C

0.

Dlr:

Sample date: 09-JUN-15

Chemical: PH, FIELD

Dlr: 0

Sample date: 12-MAY-15

Chemical: SOURCE TEMPERATURE C

DIr:

Sample date: 12-MAY-15

Chemical: PH, FIELD

DIr: 0.

Sample date: 21-APR-15

Chemical: PH, FIELD

DIr: 0.

Sample date: 21-APR-15

Chemical: SOURCE TEMPERATURE C

DIr:

Sample date: 21-APR-15

Chemical: RADIUM 228 MDA95

DIr: 0

Sample date: 21-APR-15

Chemical: PH, FIELD

Dlr: 0.

Sample date: 21-APR-15

Chemical: SOURCE TEMPERATURE C

Dlr: 0.

Sample date: 21-APR-15

Chemical: GROSS ALPHA COUNTING ERROR

DIr:

Sample date: 21-APR-15

Chemical: GROSS ALPHA MDA95 Report units: PCI/L

DIr:

Sample date: 21-APR-15

Chemical: RADIUM 226 MDA95 Report units: PCI/L

DIr: 0

Sample date: 14-APR-15 Finding: 5.074 Chemical: URANIUM (PCI/L) Report units: PCI/L

Dlr: 1.

Sample date: 14-APR-15 Finding: 27.4

Chemical: SOURCE TEMPERATURE C Report units: C

DIr: 0.

14-APR-15 Sample date: Finding: 7.2 Chemical: PH, FIELD Report units: Not Reported DIr: 07-APR-15 Sample date: Finding: 2.017 Chemical: NITRATE (AS NO3) Report units: MG/L DIr: Finding: Sample date: 10-MAR-15 7.64 Chemical: PH, FIELD Report units: Not Reported DIr: Sample date: 10-MAR-15 Finding: 27.2 SOURCE TEMPERATURE C Chemical: Report units: С DIr: 10-FEB-15 Sample date: Finding: 26.3 SOURCE TEMPERATURE C Report units: Chemical: С DIr: Sample date: 10-FEB-15 Finding: 7.7 Chemical: PH, FIELD Report units: Not Reported DIr: 0. Sample date: 13-JAN-15 Finding: 7.2 Chemical: PH, FIELD Report units: Not Reported DIr: Sample date: 13-JAN-15 Finding: 25.2 Chemical: SOURCE TEMPERATURE C Report units: С DIr: 09-DEC-14 Sample date: 26.1 Finding: Chemical: SOURCE TEMPERATURE C Report units: С DIr: Sample date: 09-DEC-14 Finding: 7.6 Chemical: PH, FIELD Report units: Not Reported DIr: 0. Sample date: 13-NOV-14 Finding: 26.1 SOURCE TEMPERATURE C Chemical: Report units: С DIr: 0. Sample date: 13-NOV-14 Finding: Chemical: PH, FIELD Report units: Not Reported DIr: 14-OCT-14 Sample date: Finding: 7.9 Chemical: PH, FIELD Report units: Not Reported DIr: 0. 14-OCT-14 Sample date: Finding: 28.3 Chemical: SOURCE TEMPERATURE C Report units: С 13-OCT-14 Sample date: Finding: 2. Chemical: CHROMIUM, HEXAVALENT Report units: UG/L

16-SEP-14

PH, FIELD

Sample date:

Chemical:

Not Reported

7.8

Finding:

Report units:

Dlr: 0.

16-SEP-14 Sample date: Finding: 28.3 SOURCE TEMPERATURE C Report units: Chemical: С

DIr:

Sample date: 09-SEP-14 Finding: 7.7

Chemical: PH, FIELD Report units: Not Reported

DIr:

25-AUG-14 27.5 Sample date: Finding: Chemical: SOURCE TEMPERATURE C Report units:

DIr:

25-AUG-14 Sample date: Finding: 7.3

PH, FIELD Chemical: Report units: Not Reported

DIr:

19-AUG-14 Sample date: Finding: 7.4

Chemical: PH, FIELD Report units: Not Reported

DIr: 0.

19-AUG-14 Sample date: Finding: 27.7

SOURCE TEMPERATURE C Report units: Chemical: С

DIr:

12-AUG-14 Sample date: Finding: 7.5

PH, FIELD Chemical: Report units: Not Reported

DIr:

Sample date: 08-JUL-14 Finding: 7.6

Chemical: PH, FIELD Report units: Not Reported

DIr: 0.

Sample date: 10-JUN-14 Finding: 7.6

Chemical: PH, FIELD Report units: Not Reported

DIr: 0.

13-MAY-14 Sample date: Finding: 7.6

Chemical: PH, FIELD Report units: Not Reported

DIr: 0.

01-APR-14 Sample date: Finding: 1.8

CHROMIUM, HEXAVALENT Report units: UG/L Chemical:

DIr:

01-APR-14 Sample date: Finding: 2.021 Chemical: NITRATE (AS NO3) Report units: MG/L

DIr:

Sample date: 11-MAR-14 Finding: 7.7

Chemical: PH, FIELD Report units: Not Reported

DIr: 0.

Sample date: 11-FEB-14 Finding: 7.8

Chemical: PH, FIELD Report units: Not Reported

DIr: 0.

Sample date: 14-JAN-14 Finding: 7.6

PH, FIELD Report units: Chemical: Not Reported

DIr: 0.

17-DEC-13

Sample date: Finding: Chemical: URANIUM (PCI/L) Report units: PCI/L DIr: 10-DEC-13 Sample date: Finding: 7.8 Chemical: PH, FIELD Report units: Not Reported DIr: 0. Finding: Sample date: 12-NOV-13 7.8 Chemical: PH, FIELD Report units: Not Reported DIr: Sample date: 15-OCT-13 Finding: 2.2 Chemical: CHROMIUM, HEXAVALENT Report units: UG/L DIr: Sample date: 08-OCT-13 Finding: 7.8 PH, FIELD Report units: Not Reported Chemical: DIr: Sample date: 10-SEP-13 Finding: 7.4 Chemical: PH, FIELD Report units: Not Reported DIr: 0. Sample date: 13-AUG-13 Finding: 7.3 Chemical: PH, FIELD Report units: Not Reported DIr: Sample date: 09-JUL-13 Finding: 7.8 Chemical: PH. FIELD Report units: Not Reported DIr: 11-JUN-13 Sample date: Finding: 7.8 PH, FIELD Report units: Not Reported Chemical: DIr: 0. Sample date: 14-MAY-13 Finding: Report units: Chemical: PH, FIELD Not Reported DIr: 0. Sample date: 16-APR-13 Finding: ODOR THRESHOLD @ 60 C TON Chemical: Report units: DIr: 1.

Sample date: 09-APR-13 Chemical: PH, FIELD

DIr:

Sample date: 09-APR-13 Chemical: NITRATE (AS NO3)

DIr:

Sample date: 13-MAR-13

Chemical: AGGRSSIVE INDEX (CORROSIVITY)

Sample date: 13-MAR-13 Finding: 2.9 Chemical: NITRATE (AS NO3) Report units: MG/L

Finding:

Finding:

Finding:

Report units:

Report units:

Report units:

Sample date: 13-MAR-13 Finding: 0.56 Chemical: LANGELIER INDEX @ 60 C Report units: Not Reported

Not Reported

Not Reported

2.389

MG/L

13.

4.744

Dlr:

0.

Sample date: 13-MAR-13 Finding: 470. TOTAL DISSOLVED SOLIDS Report units: Chemical: MG/L DIr: 0. Sample date: 13-MAR-13 Finding: 0.17 Chemical: FLUORIDE (F) (NATURAL-SOURCE) Report units: MG/L DIr: 0.1 13-MAR-13 80. Sample date: Finding: Chemical: **CHLORIDE** Report units: MG/L DIr: Sample date: 13-MAR-13 Finding: 4.2 **POTASSIUM** Chemical: Report units: MG/L DIr: 13-MAR-13 Sample date: Finding: 85. SODIUM Chemical: Report units: MG/L DIr: Sample date: 13-MAR-13 Finding: 12. **MAGNESIUM** Report units: Chemical: MG/L DIr: 13-MAR-13 52. Sample date: Finding: Chemical: **CALCIUM** Report units: MG/L DIr: Sample date: 13-MAR-13 Finding: 180. Chemical: HARDNESS (TOTAL) AS CACO3 Report units: MG/L DIr:

Sample date: 13-MAR-13 Finding: 190.
Chemical: BICARBONATE ALKALINITY Report units: MG/L
DIr: 0.

Sample date: 13-MAR-13 Finding: 160.
Chemical: ALKALINITY (TOTAL) AS CACO3 Report units: MG/L
DIr: 0.

Sample date: 13-MAR-13 Finding: 8.2
Chemical: PH, LABORATORY Report units: Not Reported

Dir: 0.

Sample date: 13-MAR-13 Finding: 750.
Chemical: SPECIFIC CONDUCTANCE Report units: US
DIr: 0.

Sample date: 13-MAR-13 Finding: 8.4

Chemical: PH, FIELD Report units: Not Reported DIr: 0.

Sample date: 13-MAR-13 Finding: 27.1

Chemical: SOURCE TEMPERATURE C Report units: C
DIr: 0.

Sample date: 13-MAR-13 Finding: 8.4
Chemical: PH, FIELD Report units: Not Reported

Dir: O. Report units: Not Reported

| Sample date:<br>Chemical:<br>Dlr: | 13-MAR-13<br>SOURCE TEMPERATURE C<br>0. | Finding:<br>Report units: | 27.1<br>C           |
|-----------------------------------|---|---------------------------|---------------------|
| Sample date:<br>Chemical:<br>Dlr: | 13-MAR-13<br>SULFATE<br>0.5             | Finding:<br>Report units: | 110.<br>MG/L        |
| Sample date:<br>Chemical:<br>Dlr: | 12-MAR-13<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 8.3<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 12-MAR-13<br>BORON<br>100.              | Finding:<br>Report units: | 550.<br>UG/L        |
| Sample date:<br>Chemical:<br>Dlr: | 08-JAN-13<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.7<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 11-DEC-12<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.5<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 13-NOV-12<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.6<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 09-OCT-12<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.8<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 11-SEP-12<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.9<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 14-AUG-12<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.9<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 10-JUL-12<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.7<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 12-JUN-12<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.7<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 08-MAY-12<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.7<br>Not Reported |
| Sample date:<br>Chemical:<br>Dlr: | 01-MAY-12<br>NITRATE (AS NO3)<br>2.     | Finding:<br>Report units: | 2.275<br>MG/L       |
| Sample date:<br>Chemical:<br>Dlr: | 10-APR-12<br>PH, FIELD<br>0.            | Finding:<br>Report units: | 7.8<br>Not Reported |
| Sample date:<br>Chemical:         | 13-MAR-12<br>PH, FIELD                  | Finding:<br>Report units: | 7.4<br>Not Reported |

Dir: 0.

Sample date: 14-FEB-12 Finding: 7.9

Chemical: PH, FIELD Report units: Not Reported

Dlr: 0.

Sample date: 10-JAN-12 Finding: 7.5

Chemical: PH, FIELD Report units: Not Reported

DIr: 0.

Map ID: 10

State Well #: 31S37E28Q001M Station ID: 38522
Well Name: Not Reported Well Use: Unknown

Well Type: Unknown Well Depth: 0

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

Map ID: 12

 State Well #:
 31S37E28P001M
 Station ID:
 24186

 Well Name:
 Not Reported
 Well Use:
 Unknown

Well Type: Unknown Well Depth: 0

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

Map ID: 13

 State Well #:
 31S37E32Z001M
 Station ID:
 24188

 Well Name:
 Not Reported
 Well Use:
 Unknown

Well Type: Unknown Well Depth: 0

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

Map ID: 14

 State Well #:
 31S37E33Z001M
 Station ID:
 24189

 Well Name:
 Not Reported
 Well Use:
 Unknown

Well Type: Unknown Well Depth: 0

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

Map ID: 15

 State Well #:
 31S37E32A001M
 Station ID:
 38523

 Well Name:
 Not Reported
 Well Use:
 Unknown

Well Type: Unknown Well Depth: 0

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

Map ID: 16

 State Well #:
 31S37E33H001M
 Station ID:
 38524

 Well Name:
 Not Reported
 Well Use:
 Unknown

Well Type: Unknown Well Depth: 0

Basin Name: Fremont Valley Well Completion Rpt #: Not Reported

| State Well #:<br>Well Name:<br>Well Type:<br>Basin Name:            | 1      | 31S37E34A001M<br>Not Reported<br>Jnknown<br>Fremont Valley | Station ID: Well Use: Well Depth: Well Completion Rpt #:          | 24190<br>Unknown<br>0<br>Not Reported |
|---|--------|--|---|---------------------------------------|
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 1<br>J | 31S37E35N001M<br>Not Reported<br>Jnknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 38525<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 1      | 32S37E04D001M<br>Not Reported<br>Jnknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 37260<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 1      | 32S37E02E001M<br>Not Reported<br>Jnknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 21571<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 1<br>J | 32S37E02F001M<br>Not Reported<br>Jnknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 37259<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 1      | 32S37E04Q001M<br>Not Reported<br>Jnknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 21574<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 1      | 32S37E04P001M<br>Not Reported<br>Jnknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 21573<br>Unknown<br>0<br>Not Reported |
|   |        |  |   |                                       |

Map ID:

24

| State Well #:<br>Well Name:<br>Well Type:<br>Basin Name:            |    | 32S37E01N001M<br>Not Reported<br>Unknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 37258<br>Unknown<br>0<br>Not Reported |
|---|----|--|---|---------------------------------------|
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 25 | 32S37E02N001M<br>Not Reported<br>Unknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 21572<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 26 | 32S37E08E001M<br>Not Reported<br>Unknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 37261<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 27 | 32S37E12M001M<br>Not Reported<br>Unknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 21576<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 28 | 32S37E12P001M<br>Not Reported<br>Unknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 21577<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 31 | 32S37E09Q001M<br>Not Reported<br>Unknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 21575<br>Unknown<br>0<br>Not Reported |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type:<br>Basin Name: | 30 | 32S37E11N001M<br>Not Reported<br>Unknown<br>Fremont Valley | Station ID:<br>Well Use:<br>Well Depth:<br>Well Completion Rpt #: | 37262<br>Unknown<br>0<br>Not Reported |

Map ID:

32

18194 32S/37E-14N01 M Seq: Prim sta c:

Frds no: 1510032004 County: 15 District: User id: CYA System no: 1510032 Water type: G

WELL/AMBNT/MUN/INTAKE/SUPPLY WELL 04 - DESTROYED Source nam: Station ty:

Latitude: 350900.0 Longitude: 1175900.0 Precision: Status: DS

Comment 1: Not Reported Comment 2: Not Reported Not Reported Comment 4: Not Reported Comment 3:

Not Reported Not Reported Comment 5: Comment 6: Not Reported Comment 7:

System no: 1510032 System nam: CALIFORNIA CITY, CITY OF 21000 HACIENDA BLVD Not Reported Address:

Hqname: **CALIFORNIA CITY** State: City: CA

Zip: 93505 Zip ext: Not Reported

Pop serv: 10000 Connection: 2992

**CALIFORNIA CITY** Area serve:

Map ID: 33

Seq: 18195 Prim sta c: 32S/37E-16N01 M

1510032006 Frds no: County: 15 District: User id: CYA 12 Water type: System no: 1510032

WELL 14 - CHLORINATION WELL/AMBNT/MUN/INTAKE/SUPPLY Source nam: Station ty:

350900.0 Longitude: 1180100.0 Latitude: Precision: Status: ΑТ Not Reported Not Reported Comment 1: Comment 2:

Not Reported Not Reported Comment 3: Comment 4: Not Reported Comment 5: Comment 6: Not Reported Comment 7: Not Reported

System no: 1510032 System nam: CALIFORNIA CITY, CITY OF Hqname: Not Reported Address: 21000 HACIENDA BLVD

**CALIFORNIA CITY** State: City: CA

Not Reported Zip: 93505 Zip ext:

Pop serv: 10000 Connection: 2992

Sample date: 25-JAN-18 Finding: 0.59

**CALIFORNIA CITY** 

Area serve:

Chemical: NITRATE (AS N) Report units: MG/L

DIr: 0.4

Sample date: 01-AUG-17 Finding: 210.

**BICARBONATE ALKALINITY** Chemical: Report units: MG/L DIr:

Sample date: 01-AUG-17 Finding: 1.06

**GROSS ALPHA MDA95** Report units: Chemical: PCI/L

DIr:

Sample date: 01-AUG-17 0.572 Finding: Chemical: **GROSS ALPHA COUNTING ERROR** Report units: PCI/L

DIr:

Sample date: 01-AUG-17 0.19 Finding:

Chemical: TURBIDITY, LABORATORY Report units: NTU

DIr: 0.1

Sample date: 01-AUG-17 Finding: 470.

Chemical: TOTAL DISSOLVED SOLIDS Report units: MG/L

Dlr: 0.

Sample date: 01-AUG-17 Finding: 7.3 Chemical: URANIUM (PCI/L) Report units: PCI/L

Dlr: 1

Sample date: 01-AUG-17 Finding: 25. Chemical: BARIUM Report units: UG/L

Dlr: 100.

Sample date: 01-AUG-17 Finding: 4.4 Chemical: ARSENIC Report units: UG/L

Dlr: 2.

Sample date: 01-AUG-17 Finding: 0.297

Chemical: RADIUM 228 COUNTING ERROR Report units: PCI/L

DIr: 0.

Sample date: 01-AUG-17 Finding: 0.672

Chemical: RADIUM 228 MDA95 Report units: PCI/L

Dlr: 0.

Sample date: 01-AUG-17 Finding: 1. Chemical: COLOR Report units: UNITS

Dlr: 0.

Sample date: 01-AUG-17 Finding: 789. Chemical: SPECIFIC CONDUCTANCE Report units: US

Dir: 0.

Sample date: 01-AUG-17 Finding: 8.09

Chemical: PH, LABORATORY Report units: Not Reported

Dlr: 0.

Sample date: 01-AUG-17 Finding: 180.

Chemical: ALKALINITY (TOTAL) AS CACO3 Report units: MG/L DIr: 0.

Sample date: 01-AUG-17 Finding: 0.6
Chemical: NITRATE (AS N) Report units: MG/L

Dir: 0.4

Sample date: 01-AUG-17 Finding: 130.

Chemical: HARDNESS (TOTAL) AS CACO3 Report units: MG/L

Sample date: 01-AUG-17 Finding: 36.

Chemical: CALCIUM Report units: MG/L DIr: 0.

Sample date: 01-AUG-17 Finding: 9.9

Chemical: MAGNESIUM Report units: MG/L DIr: 0.

Sample date: 01-AUG-17 Finding: 140.

Chemical: SODIUM Report units: MG/L DIr: 0.

Sample date: 01-AUG-17 Finding: 3.1

Chemical: POTASSIUM Report units: MG/L DIr: 0.

| Sample date:<br>Chemical:<br>Dlr: | 01-AUG-17<br>CHLORIDE<br>0.                       | Finding:<br>Report units: | 81.<br>MG/L    |
|-----------------------------------|---|---------------------------|----------------|
| Sample date:<br>Chemical:<br>Dlr: | 01-AUG-17<br>SULFATE<br>0.5                       | Finding:<br>Report units: | 93.<br>MG/L    |
| Sample date:<br>Chemical:<br>Dlr: | 01-AUG-17<br>FLUORIDE (F) (NATURAL-SOURCE)<br>0.1 | Finding:<br>Report units: | 1.1<br>MG/L    |
| Sample date:<br>Chemical:<br>Dlr: | 16-MAR-17<br>NITRATE (AS N)<br>0.4                | Finding:<br>Report units: | 0.79<br>MG/L   |
| Sample date:<br>Chemical:<br>Dlr: | 02-JUN-16<br>RADIUM 226 COUNTING ERROR<br>0.      | Finding:<br>Report units: | 0.423<br>PCI/L |
| Sample date:<br>Chemical:<br>Dlr: | 02-JUN-16<br>RADIUM 228 COUNTING ERROR<br>0.      | Finding:<br>Report units: | 0.498<br>PCI/L |
| Sample date:<br>Chemical:<br>Dlr: | 29-MAR-16<br>NITRATE (AS N)<br>0.4                | Finding:<br>Report units: | 0.58<br>MG/L   |
| Sample date:<br>Chemical:<br>Dlr: | 27-AUG-15<br>RADIUM 226 COUNTING ERROR<br>0.      | Finding:<br>Report units: | 1.02<br>PCI/L  |
| Sample date:<br>Chemical:<br>Dlr: | 27-AUG-15<br>RADIUM 228 COUNTING ERROR<br>0.      | Finding:<br>Report units: | 0.41<br>PCI/L  |
| Sample date:<br>Chemical:<br>Dlr: | 27-AUG-15<br>RADIUM 226<br>1.                     | Finding:<br>Report units: | 1.28<br>PCI/L  |
| Sample date:<br>Chemical:<br>DIr: | 26-AUG-15<br>URANIUM (PCI/L)<br>1.                | Finding:<br>Report units: | 7.1<br>PCI/L   |
| Sample date:<br>Chemical:<br>DIr: | 07-MAY-15<br>URANIUM (PCI/L)<br>1.                | Finding:<br>Report units: | 6.9<br>PCI/L   |
| Sample date:<br>Chemical:<br>DIr: | 27-MAR-15<br>NITRATE (AS NO3)<br>2.               | Finding:<br>Report units: | 3.<br>MG/L     |
| Sample date:<br>Chemical:<br>Dlr: | 23-FEB-15<br>CHROMIUM, HEXAVALENT<br>1.           | Finding:<br>Report units: | 2.5<br>UG/L    |
| Sample date:<br>Chemical:<br>Dlr: | 25-AUG-14<br>FLUORIDE (F) (NATURAL-SOURCE)<br>0.1 | Finding:<br>Report units: | 1.3<br>MG/L    |
| Sample date:<br>Chemical:         | 25-AUG-14<br>GROSS ALPHA MDA95                    | Finding:<br>Report units: | 1.16<br>PCI/L  |

## GEOCHECK VERSION 2.1 STATE DATABASE WELL INFORMATION

DIr: 0.

Sample date: 25-AUG-14 Finding: 0.381
Chemical: GROSS ALPHA COUNTING ERROR Report units: PCI/L

Dlr: 0.

Sample date: 25-AUG-14 Finding: 6.07 Chemical: GROSS ALPHA Report units: PCI/L

Dlr: 3

Sample date: 25-AUG-14 Finding: 2.1 Chemical: TOTAL TRIHALOMETHANES Report units: UG/L

Dlr: 0.

Sample date: 25-AUG-14 Finding: 2.9

Chemical: TURBIDITY, LABORATORY Report units: NTU DIr: 0.1

Sample date: 25-AUG-14 Finding: 1.
Chemical: COLOR Report units: UNITS

Dir: 0.

Sample date: 25-AUG-14 Finding: 803. Chemical: SPECIFIC CONDUCTANCE Report units: US

Chemical: SPECIFIC CONDUCTANCE Report units: U

Dir: 0.

Sample date: 25-AUG-14 Finding: 8.18

Chemical: PH, LABORATORY Report units: Not Reported

Dlr: 0.

Sample date: 25-AUG-14 Finding: 180.

Chemical: ALKALINITY (TOTAL) AS CACO3 Report units: MG/L

Dlr: 0.

0.

DIr:

DIr:

Sample date: 25-AUG-14 Finding: 220.
Chemical: BICARBONATE ALKALINITY Report units: MG/L

Dir: 0.

Sample date: 25-AUG-14 Finding: 110.

Chemical: HARDNESS (TOTAL) AS CACO3 Report units: MG/L

Sample date: 25-AUG-14 Finding: 30.

Chemical: CALCIUM Report units: MG/L DIr: 0.

Sample date: 25-AUG-14 Finding: 8.6 Chemical: MAGNESIUM Report units: MG/L

Chemical: MAGNESIUM Report units: MG/L
DIr: 0.

Sample date: 25-AUG-14 Finding: 140.
Chemical: SODIUM Report units: MG/L

Sample date: 25-AUG-14 Finding: 3.1

Chemical: POTASSIUM Report units: MG/L Dlr: 0.

Sample date: 25-AUG-14 Finding: 80.

Chemical: CHLORIDE Report units: MG/L DIr: 0.

#### GEOCHECK VERSION 2.1 STATE DATABASE WELL INFORMATION

| Sample date:<br>Chemical:<br>Dlr:                    | 25-AUG-14<br>SULFATE<br>0.5                    | Finding:<br>Report units:               | 94.<br>MG/L           |
|--|--|---|-----------------------|
| Sample date:<br>Chemical:<br>Dlr:                    | 25-AUG-14<br>ARSENIC<br>2.                     | Finding:<br>Report units:               | 4.4<br>UG/L           |
| Sample date:<br>Chemical:<br>Dlr:                    | 25-AUG-14<br>BARIUM<br>100.                    | Finding:<br>Report units:               | 25.<br>UG/L           |
| Sample date:<br>Chemical:<br>Dlr:                    | 25-AUG-14<br>CHROMIUM (TOTAL)<br>10.           | Finding:<br>Report units:               | 14.<br>UG/L           |
| Sample date:<br>Chemical:<br>Dlr:                    | 25-AUG-14<br>IRON<br>100.                      | Finding:<br>Report units:               | 1000.<br>UG/L         |
| Sample date:<br>Chemical:<br>Dlr:                    | 25-AUG-14<br>BROMOFORM (THM)<br>1.             | Finding:<br>Report units:               | 1.7<br>UG/L           |
| Sample date:<br>Chemical:<br>Dlr:                    | 25-AUG-14<br>TOTAL DISSOLVED SOLIDS<br>0.      | Finding:<br>Report units:               | 570.<br>MG/L          |
| Sample date:<br>Chemical:<br>Dlr:                    | 25-AUG-14<br>NITRATE (AS NO3)<br>2.            | Finding:<br>Report units:               | 2.2<br>MG/L           |
| Sample date:<br>Chemical:<br>Dlr:                    | 30-MAY-14<br>NITRATE (AS NO3)<br>2.            | Finding:<br>Report units:               | 2.1<br>MG/L           |
| Sample date:<br>Chemical:<br>Dlr:                    | 01-OCT-13<br>NITRATE (AS NO3)<br>2.            | Finding:<br>Report units:               | 2.7<br>MG/L           |
| Sample date:<br>Chemical:<br>Dlr:                    | 23-AUG-12<br>GROSS ALPHA<br>3.                 | Finding:<br>Report units:               | 9.97<br>PCI/L         |
| Sample date:<br>Chemical:<br>Dlr:                    | 23-AUG-12<br>GROSS ALPHA COUNTING ERROR<br>0.  | Finding:<br>Report units:               | 0.492<br>PCI/L        |
| Sample date:<br>Chemical:<br>Dlr:                    | 23-AUG-12<br>GROSS ALPHA MDA95<br>0.           | Finding:<br>Report units:               | 1.64<br>PCI/L         |
| Sample date:<br>Chemical:<br>Dlr:                    | 23-MAR-12<br>NITRATE (AS NO3)<br>2.            | Finding:<br>Report units:               | 3.1<br>MG/L           |
| Map ID:<br>State Well #:<br>Well Name:<br>Well Type: | 34<br>32S37E16R001M<br>Not Reported<br>Unknown | Station ID:<br>Well Use:<br>Well Depth: | 21578<br>Unknown<br>0 |

## GEOCHECK VERSION 2.1 STATE DATABASE WELL INFORMATION

Fremont Valley Well Completion Rpt #: Not Reported Basin Name: Map ID: 1 API#: 0402932416 Well #: 1 Well Status: Plugged Well Type: DΗ Thos. M. Blake Operator Name: Lease Name: Cinco Field Name: Any Field Area Name: Any Area Confidential Well: GIS Source: hud Directionally Drilled: Ν SPUD Date: Not Reported Map ID: 2 API#: 0402932417 Well #: Well Status: Well Type: DH Plugged Operator Name: Cinco Development Co., Inc Lease Name: Field Name: Any Field Hix Area Name: Any Area GIS Source: hud Confidential Well: Directionally Drilled: Ν Ν SPUD Date: Not Reported Map ID: 3 API#: 0402932418 Well #: 1 Well Status: Plugged Well Type: DΗ Operator Name: T. L. Park Lease Name: Dove Field Name: Any Field Area Name: Any Area GIS Source: Confidential Well: hud Directionally Drilled: Ν SPUD Date: Not Reported Map ID: API#: 0402932491 Well #: Well Status: Well Type: DH Plugged Operator Name: National Security Oil Co. Lease Name: Lease by National Security Oil Co. Field Name: Any Field Area Name: Any Area GIS Source: hud Confidential Well: Directionally Drilled: Ν SPUD Date: Not Reported Map ID: 5 API#: 0402932490 Well #: Well Status: Plugged Well Type: DH Childs-Wall Operator Name: J. S. & L. Co. Lease Name: Field Name: Any Field Area Name: Any Area GIS Source: Confidential Well: hud SPUD Date: Directionally Drilled: Ν Not Reported

#### CALIFORNIA GOVERNMENT WELL RECORDS SEARCHED

PWS: Public Water Systems

Source: EPA/Office of Drinking Water

Telephone: 202-564-3750

Public Water System data from the Federal Reporting Data System. A PWS is any water system which provides water to at

least 25 people for at least 60 days annually. PWSs provide water from wells, rivers and other sources.

PWS ENF: Public Water Systems Violation and Enforcement Data

Source: EPA/Office of Drinking Water

Telephone: 202-564-3750

Violation and Enforcement data for Public Water Systems from the Safe Drinking Water Information System (SDWIS) after

August 1995. Prior to August 1995, the data came from the Federal Reporting Data System (FRDS).

USGS Water Wells: USGS National Water Inventory System (NWIS)

This database contains descriptive information on sites where the USGS collects or has collected data on surface water and/or groundwater. The groundwater data includes information on wells, springs, and other sources of groundwater.

State Wetlands Data: Wetland Inventory Source: Department of Fish and Wildlife

Telephone: 916-445-0411

Water Well Database

Source: Department of Water Resources

Telephone: 916-651-9648

California Drinking Water Quality Database Source: Department of Public Health

Telephone: 916-324-2319

The database includes all drinking water compliance and special studies monitoring for the state of California since 1984. It consists of over 3,200,000 individual analyses along with well and water system information.

California Oil and Gas Well Locations Source: Department of Conservation

Telephone: 916-323-1779

Oil and Gas well locations in the state.

#### California Earthquake Fault Lines

Source: California Division of Mines and Geology

The fault lines displayed on EDR's Topographic map are digitized quaternary fault lines prepared in 1975 by the United State Geological Survey. Additional information (also from 1975) regarding activity at specific fault lines comes from California's Preliminary Fault Activity Map prepared by the California Division of Mines and Geology.

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## KUDU SOLAR FARM PHASE I ENVIRONMENTAL SITE ASSESSMENT

Appendix D Historical Records December 4, 2019

## Appendix D HISTORICAL RECORDS



Kudo Kudo California City, CA 93505

Inquiry Number: 5759392.6

August 20, 2019

# **Certified Sanborn® Map Report**



#### **Certified Sanborn® Map Report**

08/20/19

Site Name: Client Name:

Kudo Stantec

Kudo 735 E. Carnegie Drive, Suite 280 California City, CA 93505 SAN BERNARDINO, CA 92408

EDR Inquiry # 5759392.6 Contact: Alicia Jansen



The Sanborn Library has been searched by EDR and maps covering the target property location as provided by Stantec were identified for the years listed below. The Sanborn Library is the largest, most complete collection of fire insurance maps. The collection includes maps from Sanborn, Bromley, Perris & Browne, Hopkins, Barlow, and others. Only Environmental Data Resources Inc. (EDR) is authorized to grant rights for commercial reproduction of maps by the Sanborn Library LLC, the copyright holder for the collection. Results can be authenticated by visiting www.edrnet.com/sanborn.

The Sanborn Library is continually enhanced with newly identified map archives. This report accesses all maps in the collection as of the day this report was generated.

#### Certified Sanborn Results:

Certification # FF32-44CD-A229

PO # NA
Project NA

#### **UNMAPPED PROPERTY**

This report certifies that the complete holdings of the Sanborn Library, LLC collection have been searched based on client supplied target property information, and fire insurance maps covering the target property were not found.



Sanborn® Library search results

Certification #: FF32-44CD-A229

The Sanborn Library includes more than 1.2 million fire insurance maps from Sanborn, Bromley, Perris & Browne, Hopkins, Barlow and others which track historical property usage in approximately 12,000 American cities and towns. Collections searched:

✓ Library of Congress

University Publications of America

▼ EDR Private Collection

The Sanborn Library LLC Since 1866™

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Kudo Kudo California City, CA 93505

Inquiry Number: 5759392.5

August 21, 2019

# **EDR Historical Topo Map Report**

with QuadMatch™



#### **EDR Historical Topo Map Report**

08/21/19

Site Name: Client Name:

Kudo Stantec

Kudo 735 E. Carnegie Drive, Suite 280 California City, CA 93505 SAN BERNARDINO, CA 92408

EDR Inquiry # 5759392.5 Contact: Alicia Jansen



EDR Topographic Map Library has been searched by EDR and maps covering the target property location as provided by Stantec were identified for the years listed below. EDR's Historical Topo Map Report is designed to assist professionals in evaluating potential liability on a target property resulting from past activities. EDRs Historical Topo Map Report includes a search of a collection of public and private color historical topographic maps, dating back to the late 1800s.

| Search Results: |      | Coordinates:  | Coordinates:                |  |
|-----------------|------|---------------|-----------------------------|--|
| P.O.#           | NA   | Latitude:     | 35.179582 35° 10' 46" North |  |
| Project:        | NA   | Longitude:    | -118.0083 -118° 0' 30" West |  |
| -               |      | UTM Zone:     | Zone 11 North               |  |
|                 |      | UTM X Meters: | 408190.82                   |  |
|                 |      | UTM Y Meters: | 3893423.78                  |  |
|                 |      | Elevation:    | 2367.81' above sea level    |  |
| Maps Provid     | ded: |               |                             |  |
| 2012            | 1915 |               |                             |  |

#### 1994 1980 1973 1967 1956

1947 1943

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#### Topo Sheet Key

This EDR Topo Map Report is based upon the following USGS topographic map sheets.

#### 2012 Source Sheets



Mojave NE 2012 7.5-minute, 24000



California City North 2012 7.5-minute, 24000



Cinco 2012 7.5-minute, 24000



Cantil 2012 7.5-minute, 24000

#### 1994 Source Sheets



Mojave NE 1994 7.5-minute, 24000 Aerial Photo Revised 1972



MOJAVE NE 1994 7.5-minute, 24000

#### 1980 Source Sheets



Mojave NE 1980 7.5-minute, 24000 Aerial Photo Revised 1972



MOJAVE NE 1980 7.5-minute, 24000

#### 1973 Source Sheets



Mojave NE 1973 7.5-minute, 24000 Aerial Photo Revised 1972



California City North 1973 7.5-minute, 24000 Aerial Photo Revised 1972



Cantil 1973 7.5-minute, 24000 Aerial Photo Revised 1965

#### Topo Sheet Key

This EDR Topo Map Report is based upon the following USGS topographic map sheets.

#### 1967 Source Sheets



Cantil 1967 7.5-minute, 24000 Aerial Photo Revised 1965

#### 1956 Source Sheets



Castle Butte 1956 15-minute, 62500 Aerial Photo Revised 1943



Mojave 1956 15-minute, 62500 Aerial Photo Revised 1943

#### 1947 Source Sheets



MOJAVE 1947 15-minute, 50000



Castle Butte 1947 15-minute, 50000 Aerial Photo Revised 1943



SALTDALE 1947 15-minute, 50000



CROSS MOUNTAIN 1947 15-minute, 50000

#### 1943 Source Sheets



Saltdale 1943 15-minute, 62500 Aerial Photo Revised 1943



Castle Butte 1943 15-minute, 62500 Aerial Photo Revised 1943



Mojave 1943 15-minute, 62500 Aerial Photo Revised 1943



Cross Mountain 1943 15-minute, 62500 Aerial Photo Revised 1943

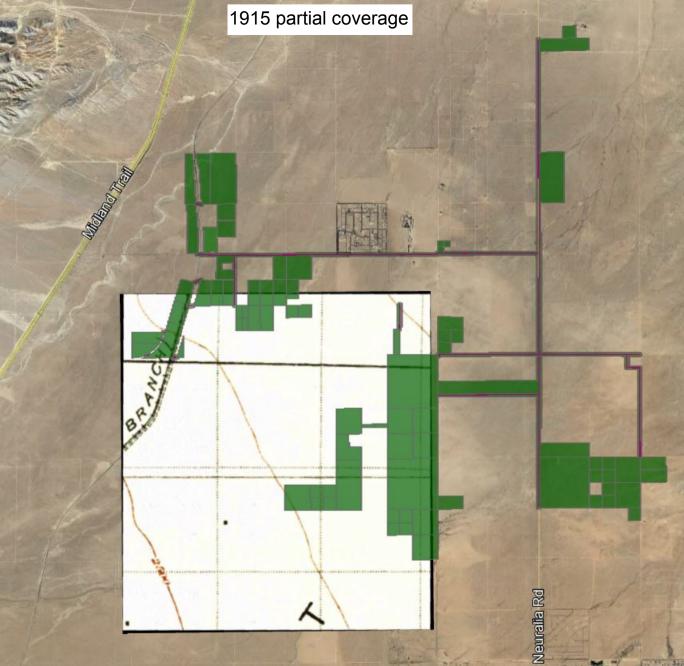
#### Topo Sheet Key

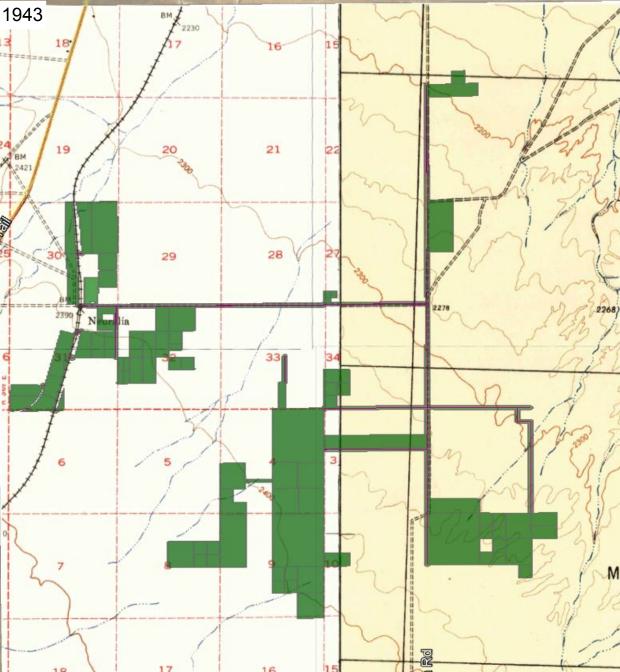
This EDR Topo Map Report is based upon the following USGS topographic map sheets.

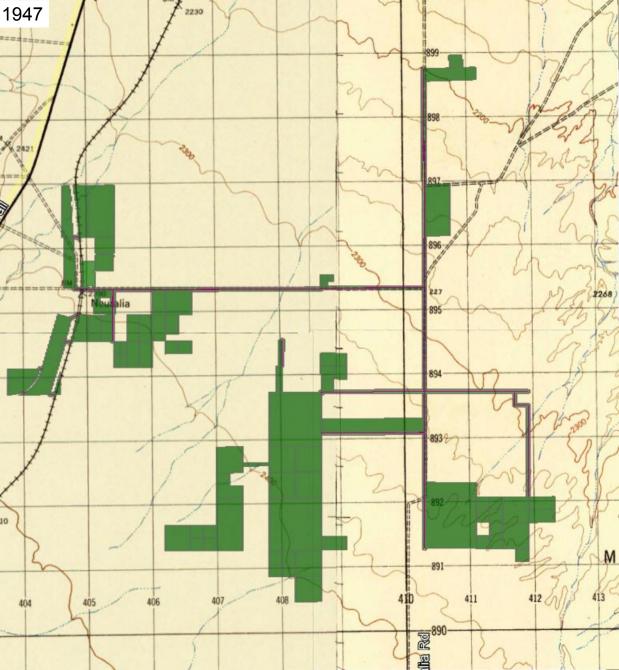
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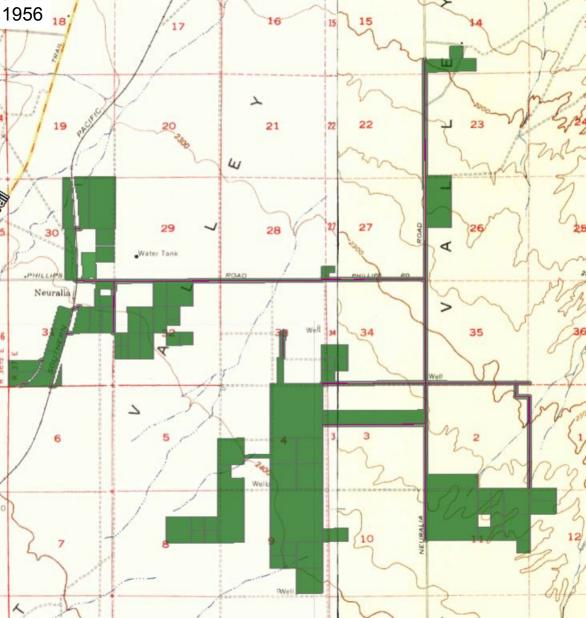


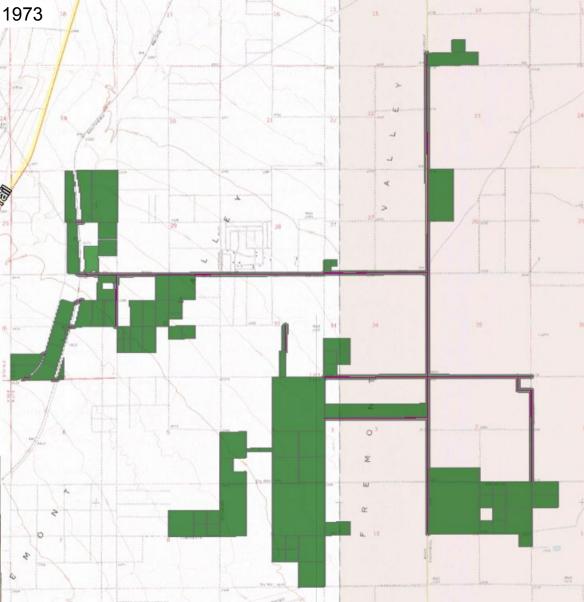
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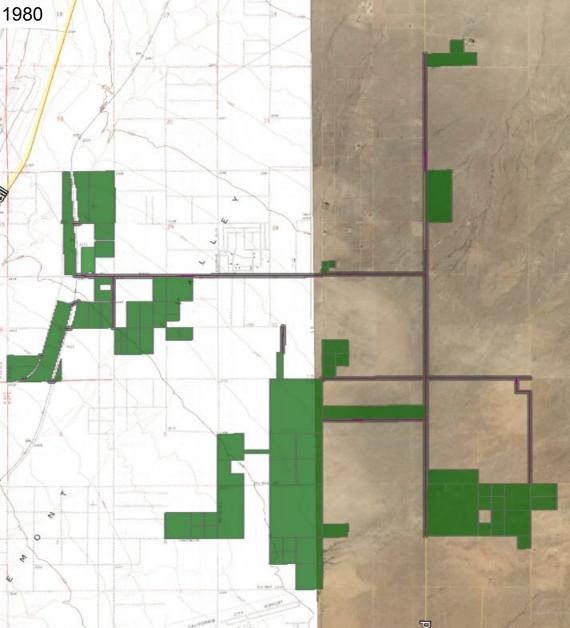


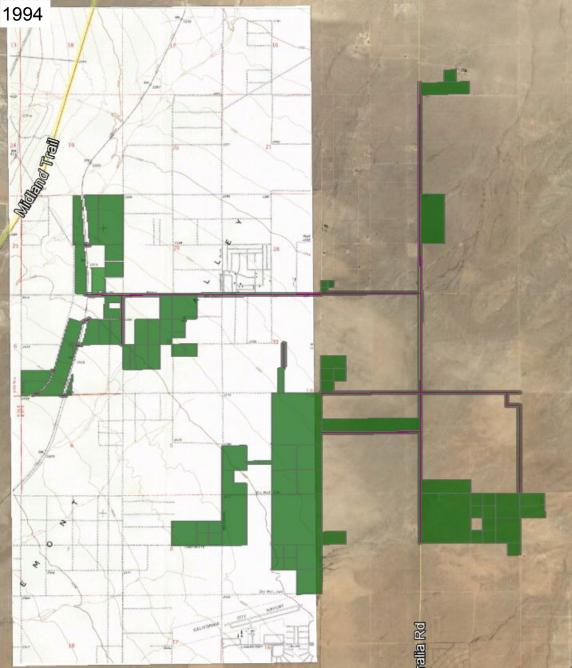


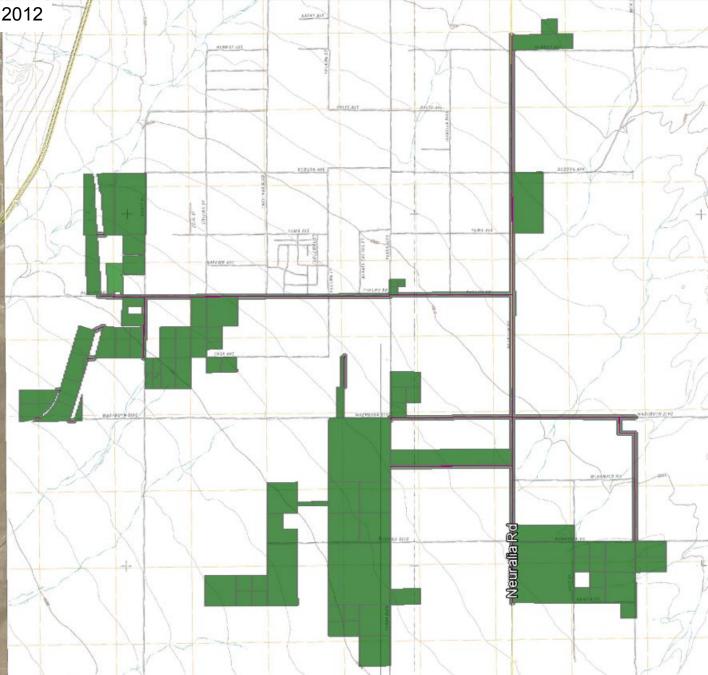












#### Kudo

Kudo

California City, CA 93505

Inquiry Number: 5759392.8

August 26, 2019

## The EDR Aerial Photo Decade Package



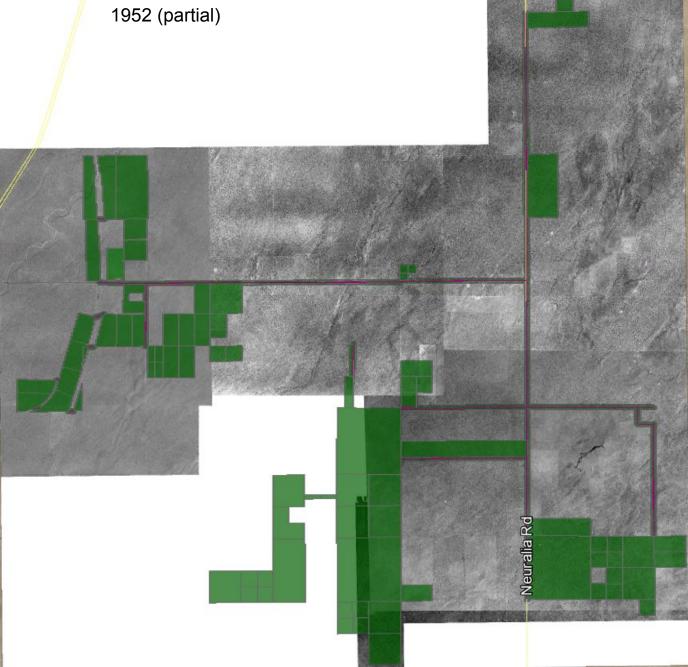
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Aerial Photography August 26, 2019

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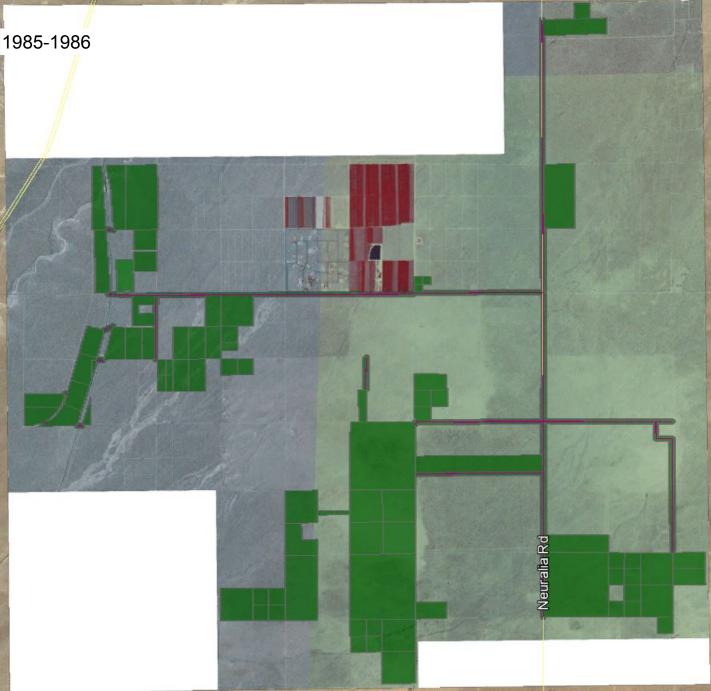
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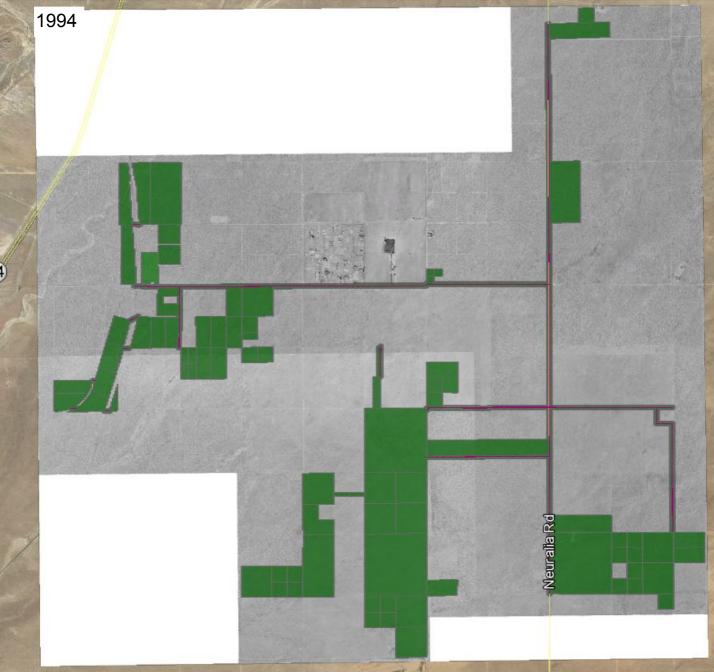
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| 1985-1986           | Aerial Photograph. Scale:       | Flight Year: 1985-1986              | USDA                  |
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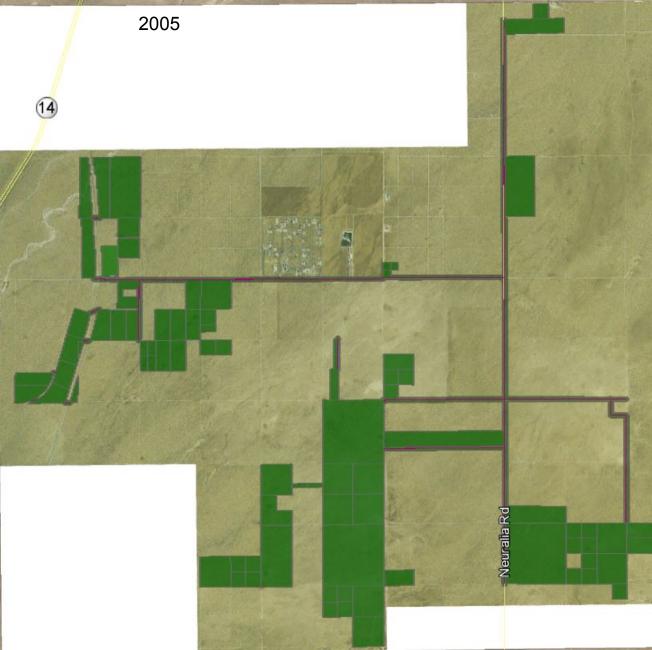


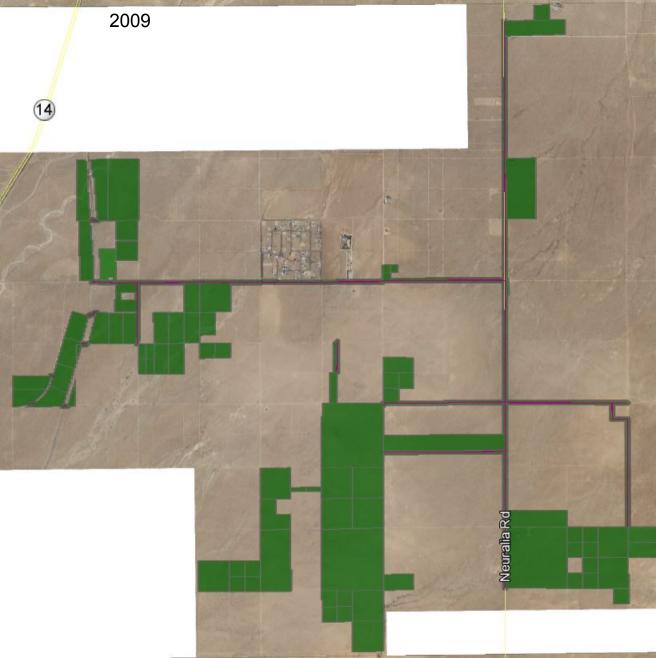


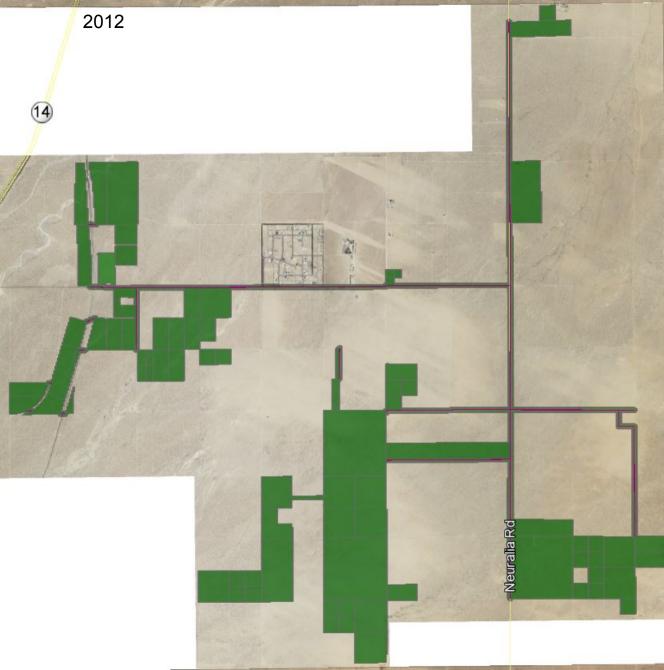


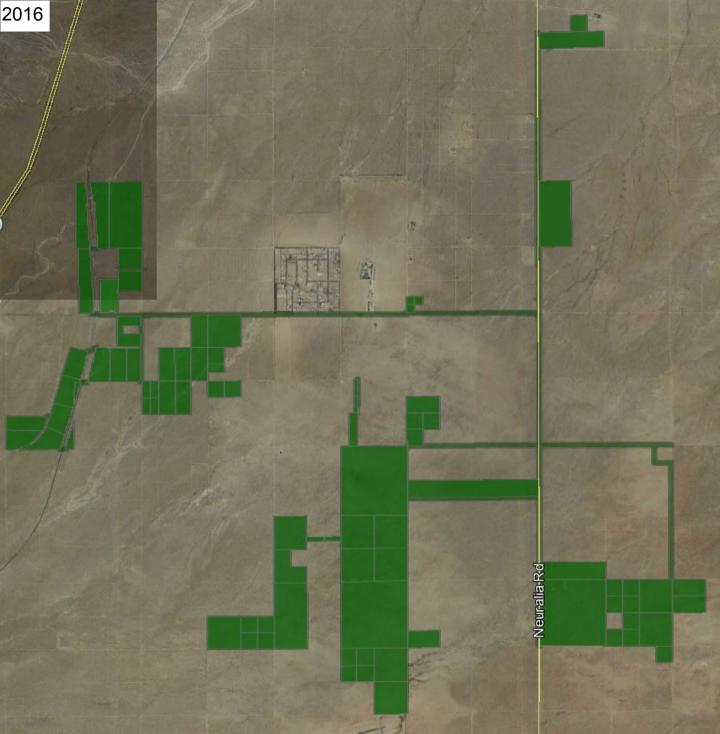












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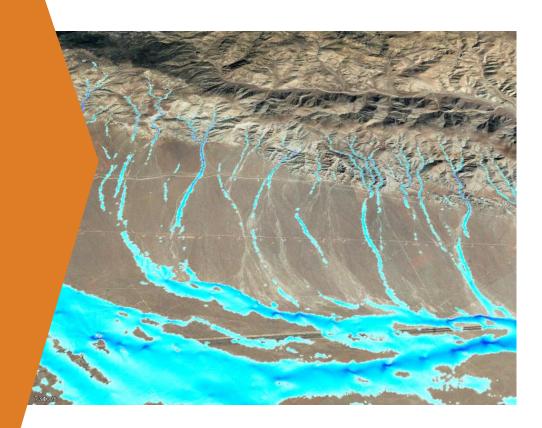
# **Appendix I**Hydrology Study

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## Westwood

Hydrology Study **Kudu Solar Project** 

Kern County, CA August 2019 (*Revised August 2020*)



Prepared For:

SOLAR ENERGY

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#### Westwood

#### Hydrology Study for

### **Kudu Solar Project**

#### Prepared for:

8minutenergy Renewables, LLC 211 Sutter Street San Francisco, CA 94108



#### Prepared by:

Chris Carda, PE Westwood Professional Services 12701 Whitewater Drive, Suite 300 Minnetonka, MN 55343

Project Number: 0023948.00

Date: 8/27/2019 (Revised 08/24/2020)

#### **CONTENTS**

| List of Exhibits               | ji |
|--------------------------------|----|
| List of Appendices             | ii |
|                                |    |
| OVERVIEW                       | 1  |
| DATA SOURCES                   | 2  |
| PROJECT HYDROLOGY              |    |
| Kern County Hydrology (CivilD) | 3  |
| FLO-2D MODELING                | 3  |
| ON-SITE RETENTION REQUIREMENTS | 4  |
| RESULTS AND DESIGN INFORMATION | 5  |
| NEXT STEPS                     | 6  |
| REFERENCES                     | 7  |
|                                |    |

#### **EXHIBITS**

Exhibit 1: Location Map

Exhibit 2: Base Hydrology Map

Exhibit 3: Soils Map

Exhibit 4: Landcover Map

Exhibit 5: Curve Number and Topographic Source Map

Exhibit 6: 100-Year Max Water Depth Map (Entire Modeled Area)

Exhibit 6A: 100-Year Max Water Depth Map (Project Area)

Exhibit 7: 100-Year Peak Velocity Map (Entire Modeled Area) Exhibit 7A: 100-Year Peak Velocity Map (Project Area)

Exhibit 8: 100-Scour Depth Map (Project Area)

Exhibit 9: Kern County Hydrology Map

#### **APPENDICES**

Appendix A: CivilD Printouts (Kern County Hydrology Manual)

Appendix B: Kern County Curve Number Table

Appendix C: Atlas 14 Rainfall Data

Appendix D: Kern County Hydrology Manual Excerpts

Appendix E: Kern County Development Standards: Standards for Drainage

Appendix F: Pre-Post Water Balance Calculation Sheets

Appendix G: Inflow Rates

Appendix H: FEMA FIRM Panels

#### **OVERVIEW**

The purpose of the study is to describe the hydrology of the proposed Kudu Solar Project ("the project") and any impacts that the hydrology may play in the design of the solar array and for use in Kern County permitting. The study is an expansion of the Eland Solar Project that was previously conducted. No new modeling was included in this study.

The project includes developing approximately 4,000 acres in Kern County, CA in the area around California City, CA (Exhibit 1). The project consists of numerous parcels and landowners scattered throughout the area. The main area of parcels is between Highway 14 to the west, Phillips Rd to the north and Neuralia Rd to the east. At the time of this report, the project consists of solar panels, an inverter and an access road. Runoff generated from the solar panels will flow to the edge of the panels and be allowed to drip onto the existing pervious surface below and allowed to disperse and infiltrate below the panels across the site.

With the project being located within Kern County the stormwater requirements for Kern County were researched and applicable regulations were followed.

The project site generally slopes to the northeast. The watershed area encompasses approximately 407 square miles and is part of a watershed that commences southwest of the project. The project area is on a mild slope of around 1%.

The project area is within FEMA FIRM panels 06029C2925E, 06029C2930E, 06029C2920E, and 06029C2940E (Appendix H). A FEMA designated 1% annual chance flood hazard area for Zone A (undetermined flood depth) runs through a portion of the project area (Exhibit 2).

The hydrologic modeling in this report was created using FLO-2D modeling software. Because of the complex and distributary/alluvial nature of flow paths upstream and through the project site, FLO-2D hydrologic/hydraulic modeling software was utilized to determine flow depths and velocities throughout the site.

Overall, the analysis shows low water depths and velocities (Exhibits 6 and 7) across the majority of the site. During a 100 year storm the flood depths across the majority of the project area are less than 0.5 feet with velocities less than 1 foot/second. See Exhibits 6 and 7 for areas within the project with higher flood depths and velocities. Based on experience on other similar projects, the site is suitable for the planned development by avoiding areas of high flood depths and velocities in channelized flow areas.

The new solar array will require retention to mitigate the runoff from the new impervious surfaces. The design volume for the onsite retention basin is calculated per Section 408-1 of the Kern County Development Standards (KCDS). The calculation is based on an initial assumption of the impervious area added by the project. The runoff volume from the ISDD five-day storm is calculated at 10.67 acrefeet.

Hydrology Study 1 Kudu Solar Project

#### **DATA SOURCES**

The models and methods for this project utilize a combination of public and private data as shown in Table 1.

Table 1: Data Sources

| Data Type       | Format             | Source             | Use                  |
|-----------------|--------------------|--------------------|----------------------|
| Elevation       | Photogrammetry     | Westwood           | Site FLO-2D Model    |
|                 |                    |                    | Elevations           |
| Elevation       | 10-Meter Digital   | USGS 10-Meter      | Watershed FLO-2D     |
|                 | Elevation Model    | National Elevation | Model Elevations     |
|                 |                    | Dataset            |                      |
| Crop Data       | Shapefile          | USDA 2013 Crop     | Landcover            |
|                 |                    | Data Layer         |                      |
| Soils           | Shapefile          | USGS SSURGO        | Curve Numbers        |
|                 |                    | Dataset            |                      |
| Precipitation   | PDF File           | NOAA Atlas 14      | Design storms        |
|                 |                    | Website            |                      |
| HUC-12 Drainage | Shapefile          | USGS               | Define Model Extents |
| Boundary        |                    |                    |                      |
| Site Boundary   | Shapefile          | 8minutenergy       | Define Model Extents |
|                 |                    | Renewables, LLC.   |                      |
| 2015 Aerial     | ArcGIS Map Service | USDA FSA           | Reference            |
| Photography     |                    |                    |                      |

Hydrology Study 2 Kudu Solar Project

#### PROJECT HYDROLOGY

The project area is located in the south-central California, in the area surrounding California City, CA. The project site generally slopes to the northeast. The previously modeled watershed area encompasses approximately 407 square miles and is part of a watershed that commences southwest of the project. The project area is on a mild slope of 1%. The potential hydrologic issues in this general landscape are flooding and erosive velocities.

Because of the complex and distributary/alluvial nature of flow paths upstream and through the project site, a FLO-2D model was utilized to determine flow depths and velocities throughout the site. This FLO-2D model was calibrated to the Kern County Hydrology Manual and used to model the site hydrology.

#### **Kern County Hydrology (CivilD)**

CivilD modeling software was used to calculate flow rates and confirm that the FLO-2D model was providing results consistent with the Kern County methods (Appendix D). A point (Exhibit 9) was selected to calibrate the results of the FLO-2D model. This location works reasonably well as a calibration point because it is similar to watersheds that contribute to the project site and is relatively concentrated. Inputs to CivilD were calculated following guidance in the KCHM and modeling inputs/outputs can be found in Appendix A. The peak flow rate for the calibration watershed using CivilD was 611.02 cfs. Table 2 below shows the inputs into the CivilD model.

| Table 2: | CivilD | Calibration | Watershed | Inputs |
|----------|--------|-------------|-----------|--------|
|----------|--------|-------------|-----------|--------|

| Table 21 Civil Calibration Waterened Inpate |                             |            |       |  |  |
|---|-----------------------------|------------|-------|--|--|
| Description                                 | Equation                    | Unit       | Value |  |  |
| Watershed Area                              | Calculated in GIS           | Square Mi. | 0.90  |  |  |
| Watershed Area                              | Conversion                  | Acres      | 573   |  |  |
| 100-year Aerial Reduction                   | Figure E-4                  | Unitless   | 1.0   |  |  |
| Watershed Area with Reduction               | Aerial Reduction*Area       | Acres      | 573   |  |  |
| Equation                                    | Lag=24n(I*lca/sqrt(s))^0.38 | Hours      | 0.43  |  |  |
| Basin Factor                                | KCHM Page 156 (n)           | Unitless   | .05   |  |  |
| Longest Watercourse                         | Calculated in GIS (I)       | Miles      | 1.98  |  |  |
| Length to Centroid                          | Calculated in GIS (Ica)     | Miles      | 1.05  |  |  |
| Upstream Elevation                          | From 10-m offsite DTM       | Feet       | 5,633 |  |  |
| Elevation at Concentration                  | From 10-m offsite DTM       | Feet       | 3,729 |  |  |
| Difference in Elevation                     | Upstream – Downstream (H)   | Feet       | 1904  |  |  |
| Slope along Watercourse                     | Slope (s)                   | FT/Mi.     | 962   |  |  |
| Average CN for watershed (Appendix B)       | CN=                         | Unitless   | 91.0  |  |  |

#### **FLO-2D MODELING**

FLO-2D is a physical process model that routes rainfall runoff and flood hydrographs over flow surfaces or in channels using the dynamic wave approximation to the momentum equation. FLO-2D offers advantages over 1-D models and unit hydrograph methods by allowing for breakout flows and visualization of flows across a potential site. This is particularly useful on a moderately sloped distributed area such as the project site. The primary inputs are a DTM (elevation data), curve numbers, and precipitation. A grid system is set up within the FLO-2D software and based upon the large watershed size the FLO-2D grid cells were optimized at 50'. Four inflow locations were input into the model to reduce the size, these inflows were based on the FEMA FIS and Streamstats with inflows of 8,060 cfs, 11,600 cfs, 8,000 cfs and 7,800 cfs respectively. Culverts were input into the model along the railroad.

Precipitation data downloaded from NOAA Atlas 14 (Appendix C) for the 100 year rain events in the project watershed were 3.71" of rainfall. By using the 100-year rainfall event for design purposes it allows

Hydrology Study 3 Kudu Solar Project

for the best initial analysis in order to determine the worst areas of flooding and erosion. The 100-year rainfall depth was distributed based on a nested distribution of Atlas-14 point precipitation estimates and input into FLO-2D.

There is a railroad located to the west of the project boundary. Due to this section of the model using 10-meter elevation data the railroad was not distinguishable in the elevation data. To account for any influence the railroad may have on the hydrology of the site, adjustments were made in the FLO-2D model. The elevation along a portion of the railroad was raised an elevation of 3 feet to account for the railroad berm based on anecdotal information from the client. Culverts were then input into the FLO-2D model in locations along the railroad determined from Google Earth (Exhibit 2). Culverts sizes were estimated based on Google Earth imagery. Prior to final design the railroad and culvert locations should be surveyed along with proper culvert dimensions determined.

The elevation data input into the FLO-2D model was 1-meter flown LiDAR data and USGS 10-meter elevation incorporated into the DTM using the export to xyz file function in Global Mapper. These XYZ files are read directly into FLO-2D.

USDA-NRCS SSURGO soil data provides soil types within the project boundary and full coverage of the contributing watershed. Soils in the area are primarily classified as hydrologic group A & B (Exhibit 3). Land cover was obtained from the Kern County Hydrology Manual. Exhibit 4 displays the Land Cover Classes for the entire watershed. The majority of land in this area is assumed to be chaparral, narrowleaf. With the majority of the land being undeveloped the soil conditions assumed in the model were poor soil in order to take the most conservative approach. This raises the curve number of the model because the soil conditions do not have as much plant growth on them. Curve numbers were applied to each grid cell in the FLO-2D model based on intersecting the grid with the fallow soil and land cover data (Exhibit 5). The majority of the project area has a curve number between 60 and 90. Areas with a higher curve number will have more runoff and areas with a lower curve number will have less runoff. This is based on the type of soils, "A" soils have the highest infiltration rates and "D" soils have the lowest infiltration rates, along with the landcover of the area, dense vegetation will have less runoff and fallow farm fields and impervious areas will have more runoff.

The FLO-2D model was calibrated to CivilD by increasing the Manning's and curve number values of the FLO-2D model. The Manning's values were applied to each grid cell in the FLO-2D model based on intersecting the grid with the soils. The peak flow model results from FLO-2D matched closely (<3%) the Kern County results providing assurances that the FLO-2D software was performing adequately (Table 3).

Table 3: Comparison of modeling methods at calibration point

|                 | CivilD (Kern County) | FLO-2D |
|-----------------|----------------------|--------|
| Volume (ac-ft)  | 134.75               | 163.46 |
| Peak Flow (cfs) | 611.02               | 599.06 |

#### **ON-SITE RETENTION REQUIREMENTS**

The proposed solar project development will require retention to mitigate the runoff from the new impervious surfaces, primarily piles. Due to the spacing of the piles and parcels, it is not feasible to direct runoff from all array locations to a common basin. Therefore the proposed basin will not retain runoff from the entire site, but will be located in a common discharge point for as many piles as possible and will include the required capacity to offset the increased runoff from all of the piles. Runoff generated from

Hydrology Study 4 Kudu Solar Project

the piles and access roads will be allowed to disperse and infiltrate across the site in existing flow patterns.

The site layout and facilities have not yet been finalized but future basins will be placed throughout the project to meet the retention volume required when design is finalized. Table 4 below summarizes the proposed impervious areas and retention volumes provided as of 08/27/2019 based on Kern County retention requirements (Appendix E). The added piles to the site were assumed be 1% impervious cover of the site, however the onsite requirements and imperviousness will be updated during final design to ensure that it meets all the storage requirements. Additionally, pre-post State Water Balance Calculation sheets have been provided in Appendix F. The State Water Balance Calculator showsthe need for permanent drainage facilities but since the Kern County storage requirements are greater, the kern County method will be used for basin sizing.

| Table 4: Pro | posed Impervious | Areas and Kern ( | County Retention | Calculations |
|--------------|------------------|------------------|------------------|--------------|
|              |                  |                  |                  |              |

| Site          | 10-yr, 5-day | Impervious | Drainage    | Retention     | Retention     |
|---------------|--------------|------------|-------------|---------------|---------------|
|               | Rainfall     | Cover (%)* | Area (ac)** | Volume        | Volume        |
|               | Depth (in)   |            |             | Required (ac- | Provided (ac- |
|               |              |            |             | ft)           | ft)           |
| Solar Project | 3.20         | 1.00       | 4,000       | 10.67         | TBD during    |
| Development   |              |            |             |               | Final Design  |
| Total         |              |            | 4,000       | 10.67         | TBD           |

<sup>\*</sup>The impervious cover calculations are the added impervious piles at the panel locations.

The design volume for the retention basins is calculated Engineering Bulletin 11-02 of the Kern County Development Standards (KCDS). The runoff volume form the ISDD five-day storm is calculated as:

Retention Basin Volume (ac-ft) =  $[(\mathbf{D}_{10yr-5day})/12](\mathbf{a} \mathbf{i})(\mathbf{Area}) = 10.67 \text{ ac-ft}$ 

Where,

 $\mathbf{D}_{10} = 10$ -yr, 5-day depth of rainfall (in) = 3.20 inches

**a** i=average percentage of impervious area = 1%

**Area**= Drainage area of total development = 4,000 acres

#### RESULTS AND DESIGN INFORMATION

Overall, the analysis shows low water depths and velocities (Exhibits 6 and 7) across the majority of the site (with the exception of the channelized flows throughout the center of project boundary). Due to the moderately sloped landscape in the area many channelized areas have depths over 1' and velocities >1fps. These areas of the site should be avoided. During a 100 year storm the flood depths across the majority of the project area are less than 0.5 feet with velocities less than 1 foot/second. Also due to the moderate slopes adjacent to the streams there are areas with erosion and velocity issues which should also be avoided. FEMA has completed a study to determine flood hazard for the selected location; therefore, a flood map has been published. There are FEMA flood hazards that affect the project area. The flood hazards should be avoided during final site placement and cover approximately 315 acres.

The Kern County requirements had to be met for the modeling criteria. The State of CA requires the state water balance calculator to be completed. The Kern County requirements are controlling.

Based on experience on other similar projects, the overall site is suitable for the planned development by avoiding areas of high flood depths and velocities.

Hydrology Study 5 Kudu Solar Project

<sup>\*\*</sup>The drainage area is the area that is within the total temporary disturbance of the project.

#### **NEXT STEPS**

- 1. Final design should account for flood depths, velocities, and scour presented in Exhibits 6, 7 and 8 to protect infrastructure and meets Kern County Development Standards for construction in floodplains.
- Crossing types (low water crossing or culvert) should be determined for each crossing location as determined based on field conditions.
- 3. The retention basin(s) should be located on the downstream sides of the properties and be no more than 18" deep to ensure that the basin infiltrates in 72 hours. If the basin is deeper than 18", freeboard and fencing requirements will be triggered. (408-3, 408-4 KCDS) Chapter VIII of the KCDS should be reviewed prior to final design to ensure that all construction criteria are being met.
- 4. The proposed project is not expected to cause more than 1 foot of water surface rise and discharges the 100-year storm in a manner similar to the existing flow pattern. (404-1 KCDS).
- 5. All electrical equipment will be set at least 2 feet above grade.
- 6. Scour calculations are shown on Exhibit 8 and are applicable for a W6x9 pile. If pile size is different from the assumed, scour should be recalculated.
- 7. The railroad though the FLO-2D boundary should be surveyed for accurate embankment height, along with accurate culvert sizes, locations, and elevations. This assumption has a large impact on the flooding on site and needs to be revised prior to final design.

Hydrology Study 6 Kudu Solar Project

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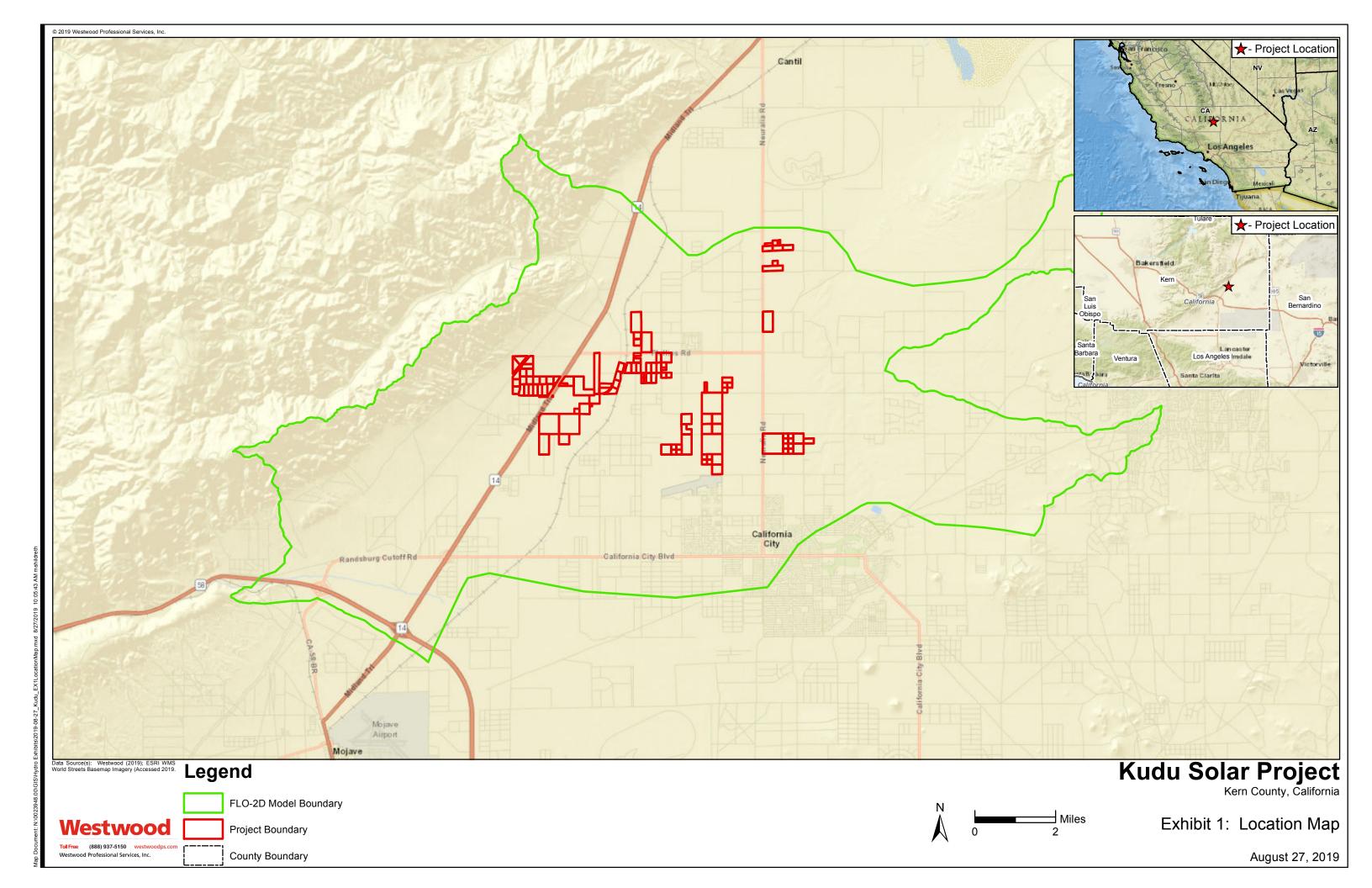
Kern County Development Standards (August 1995) Downloaded 6/3/2014 from http://esps.kerndsa.com/engineering/development-standards

Hydrology Study 7 Kudu Solar Project

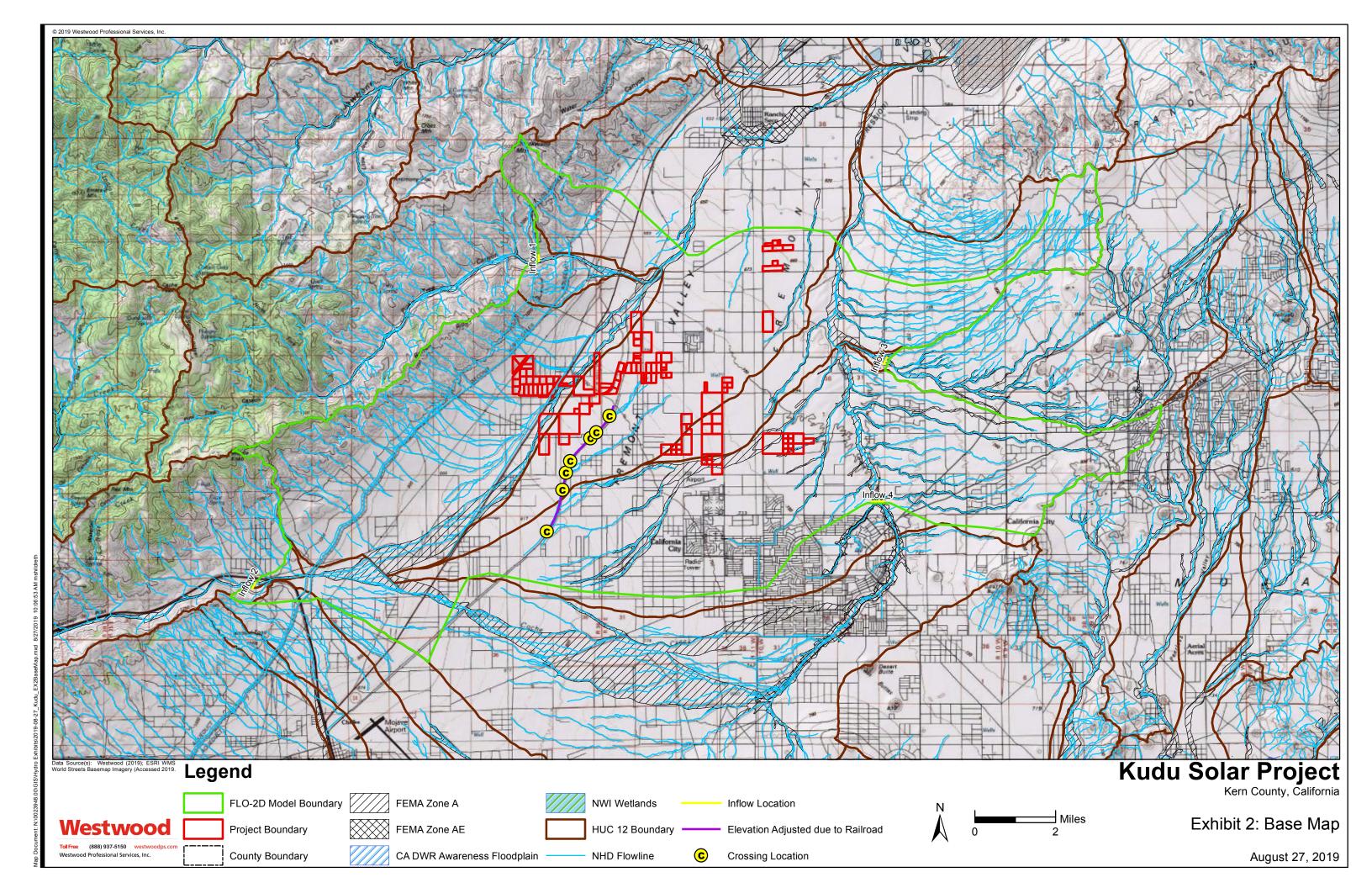
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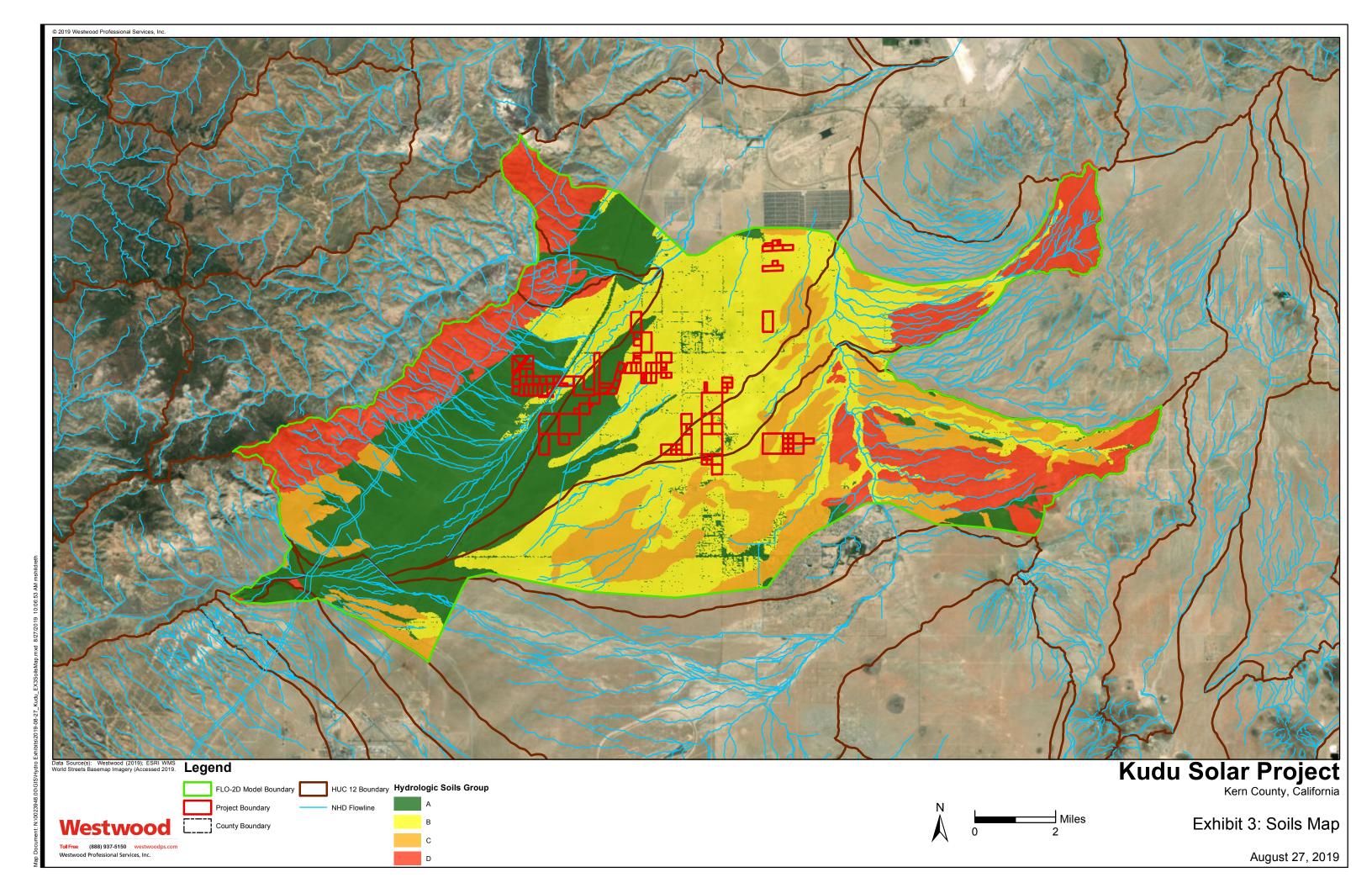
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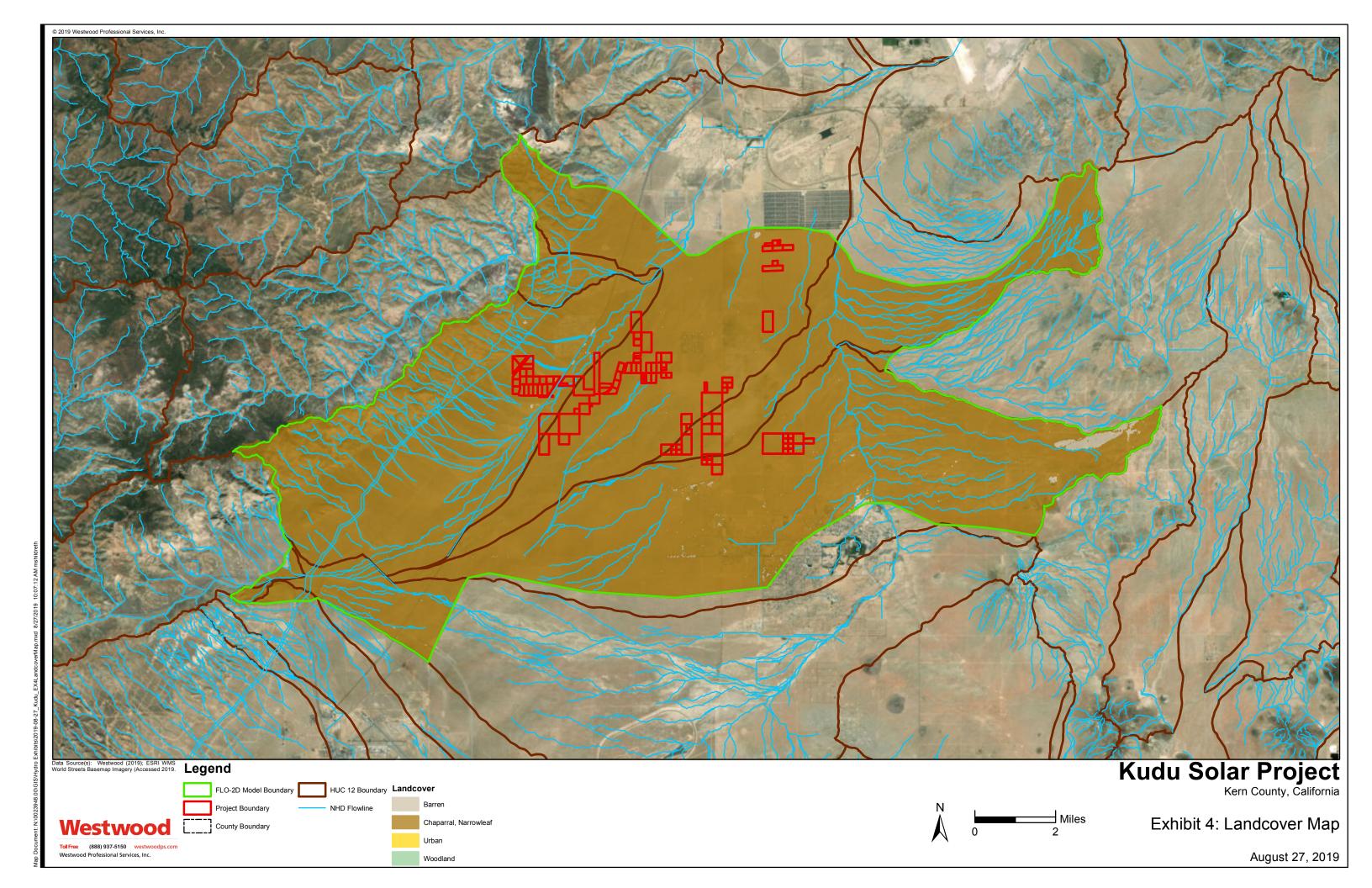




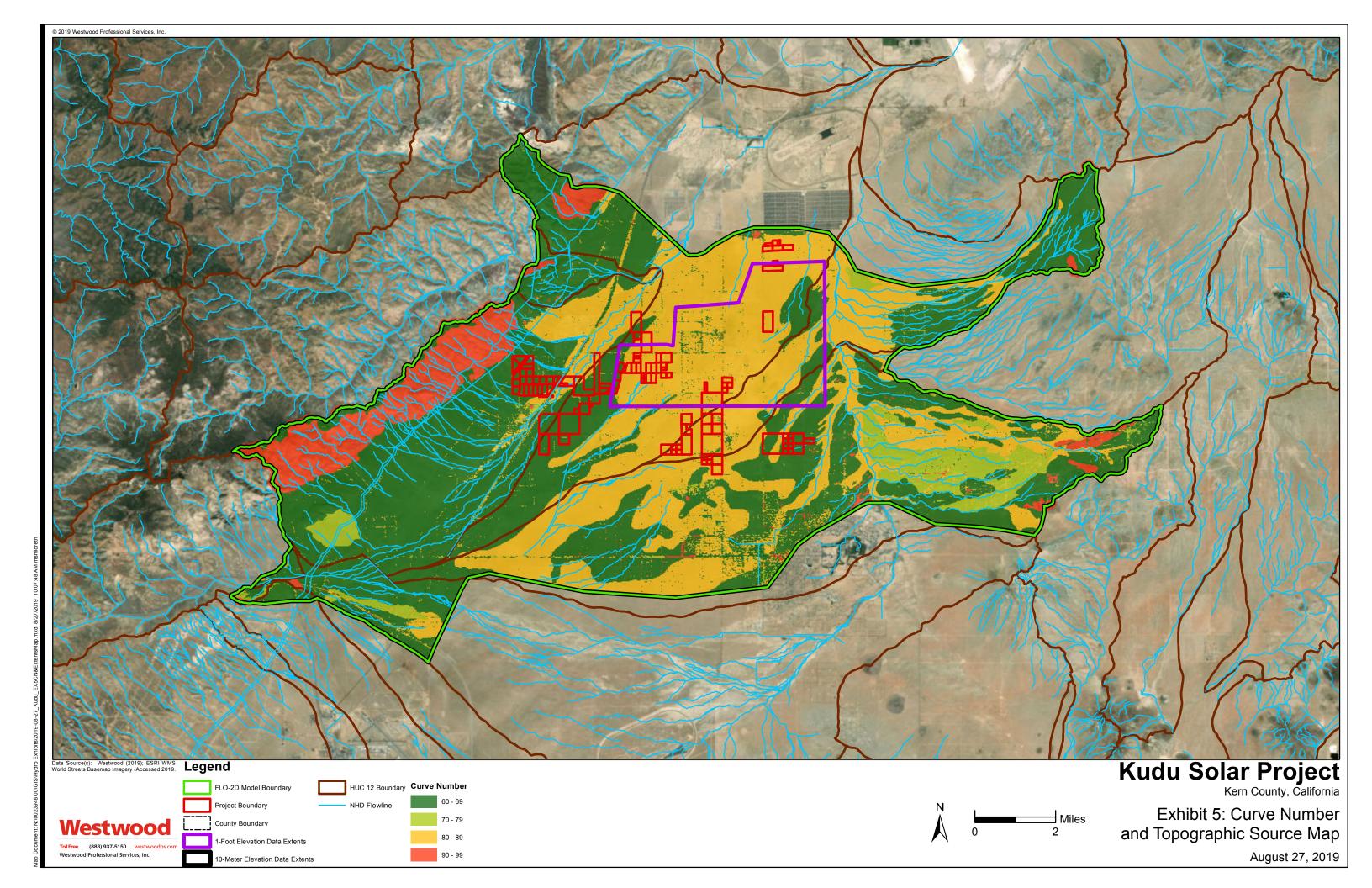




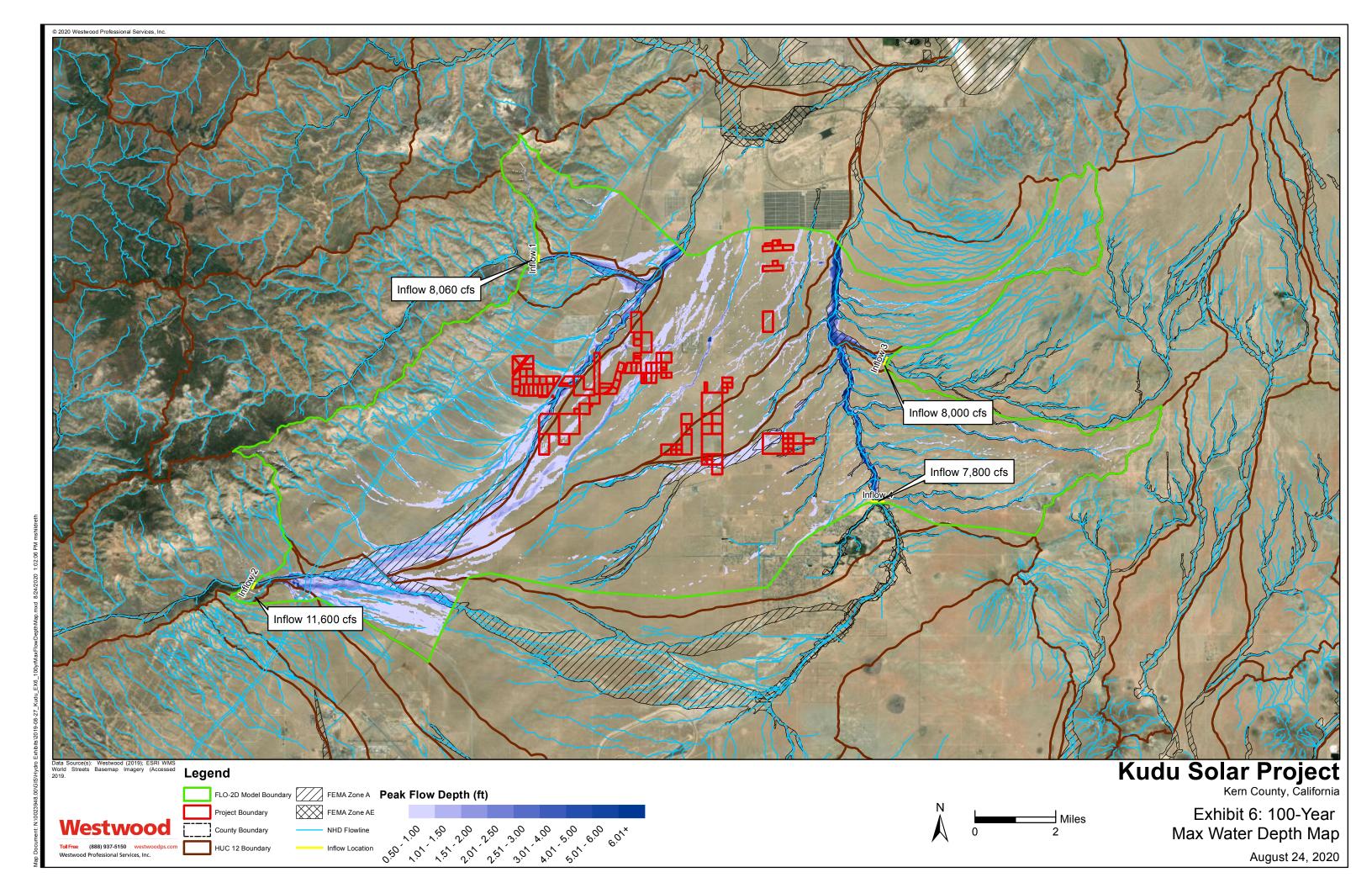




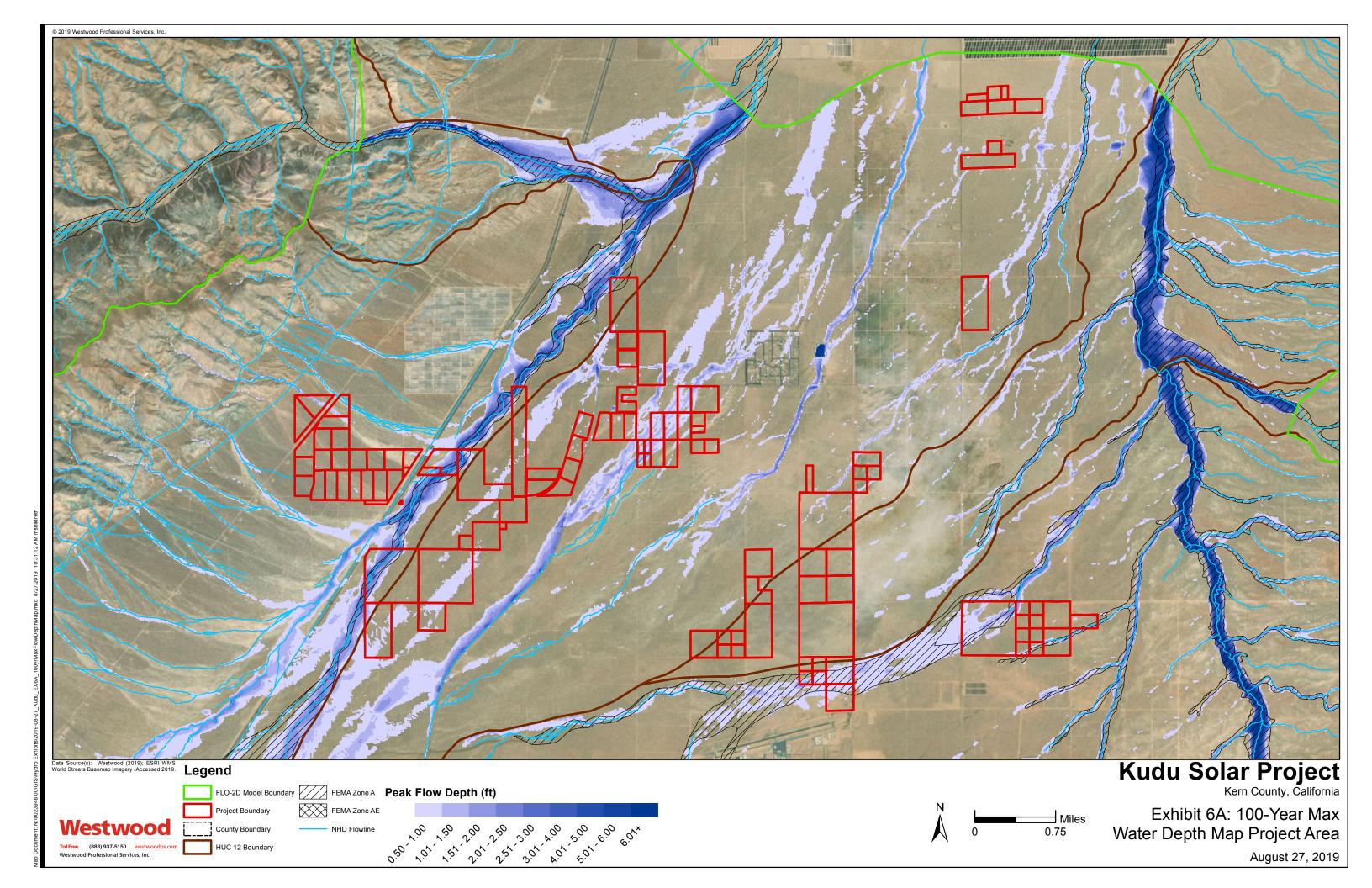




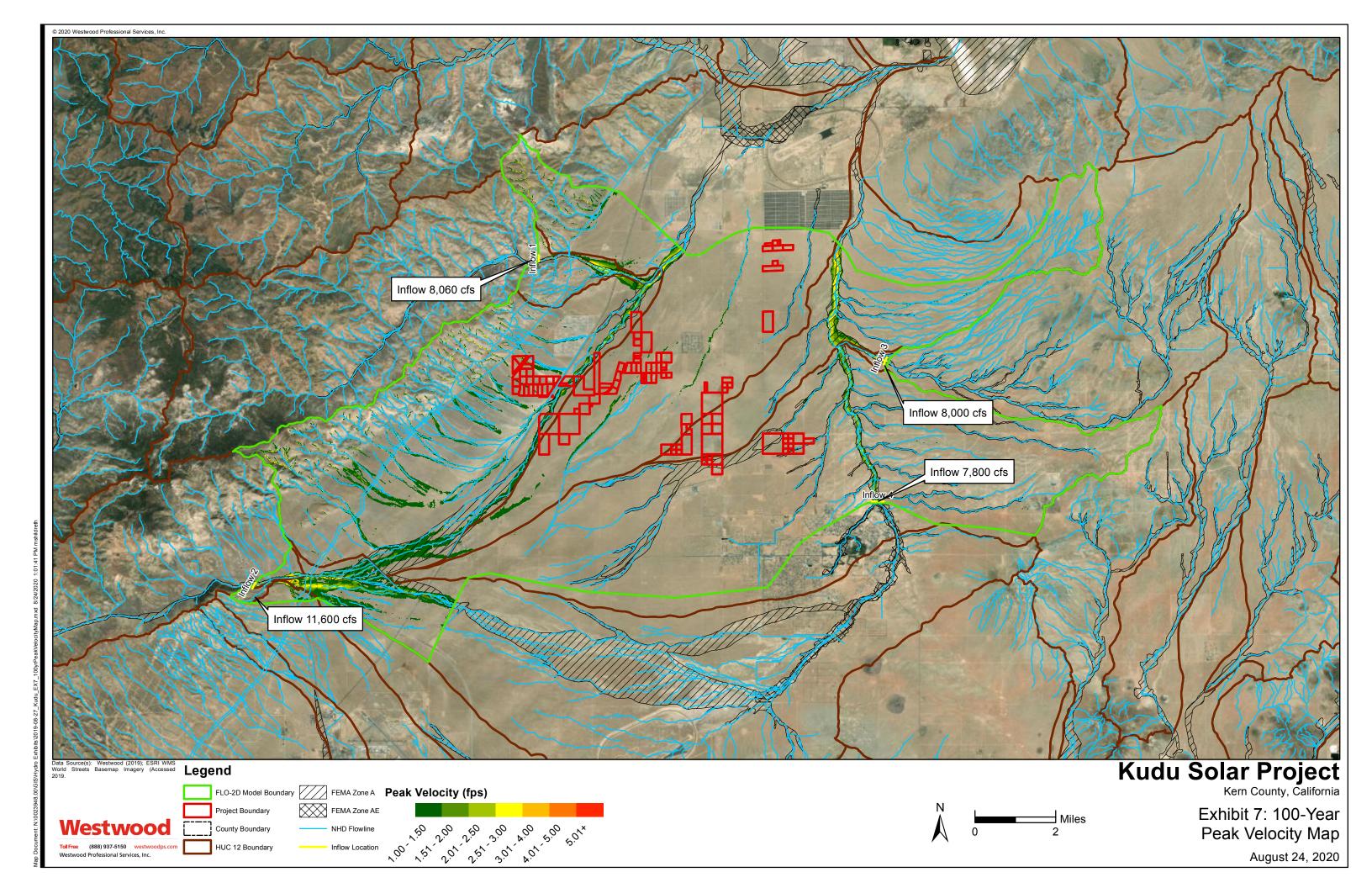




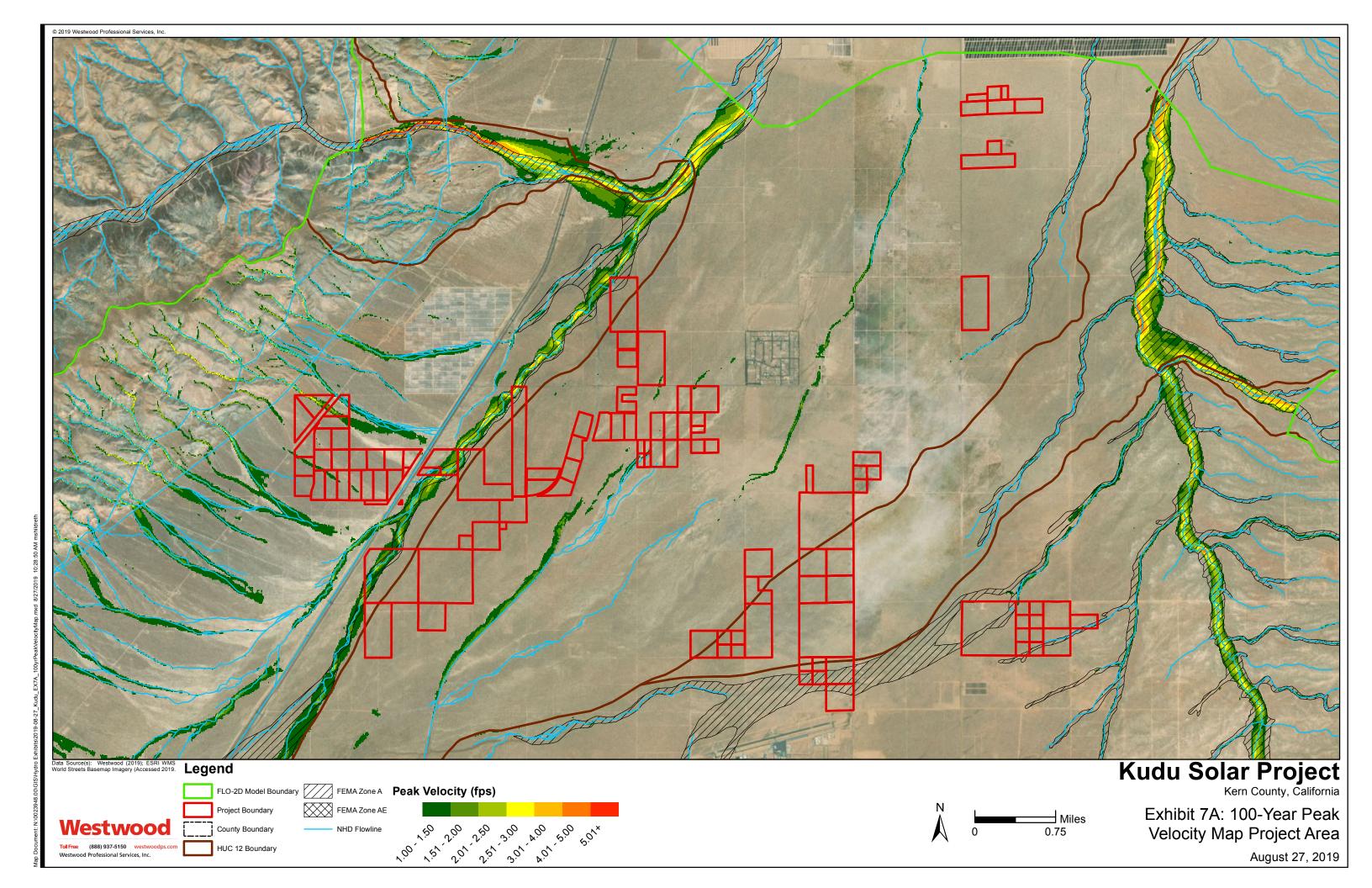




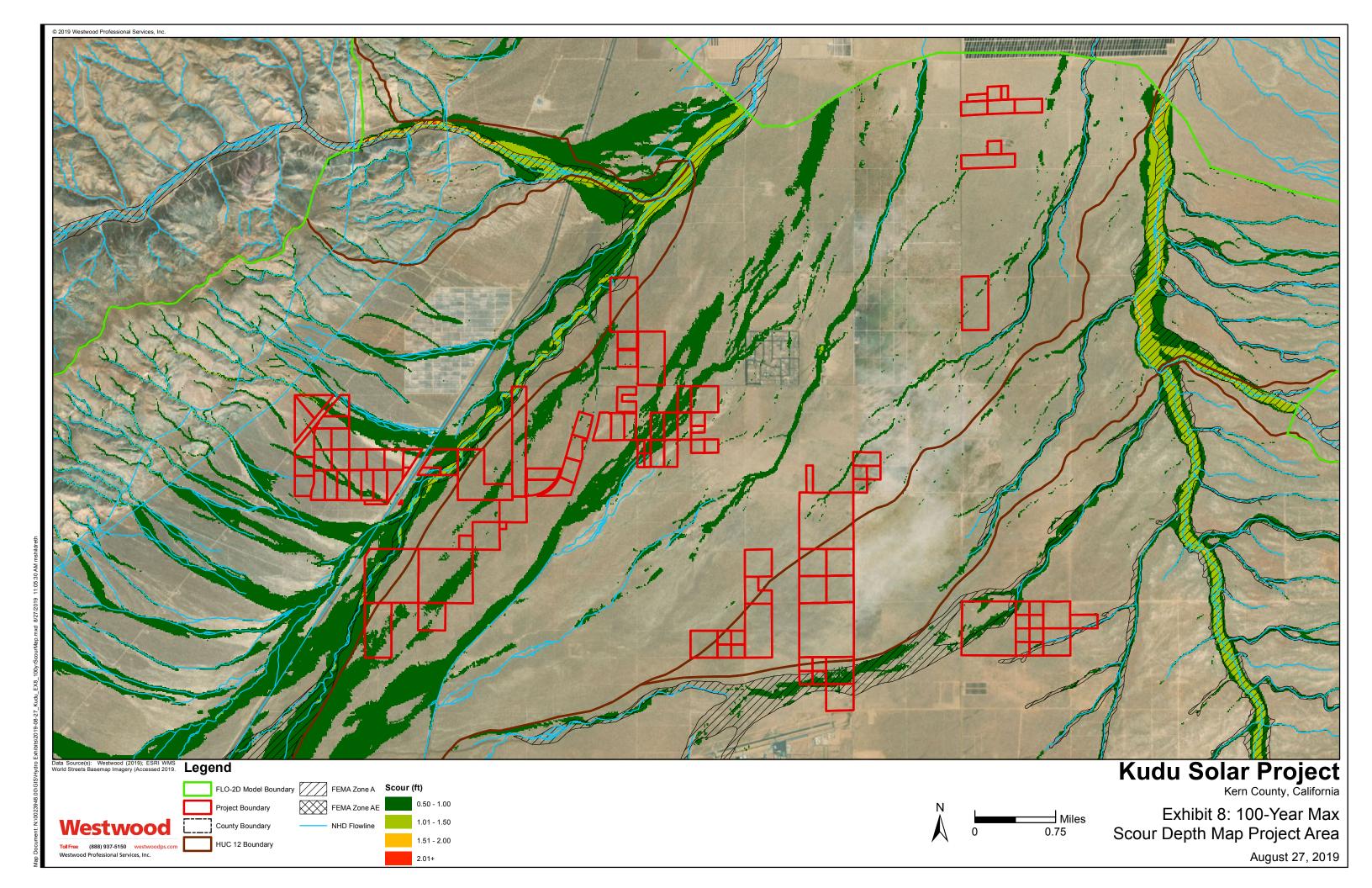




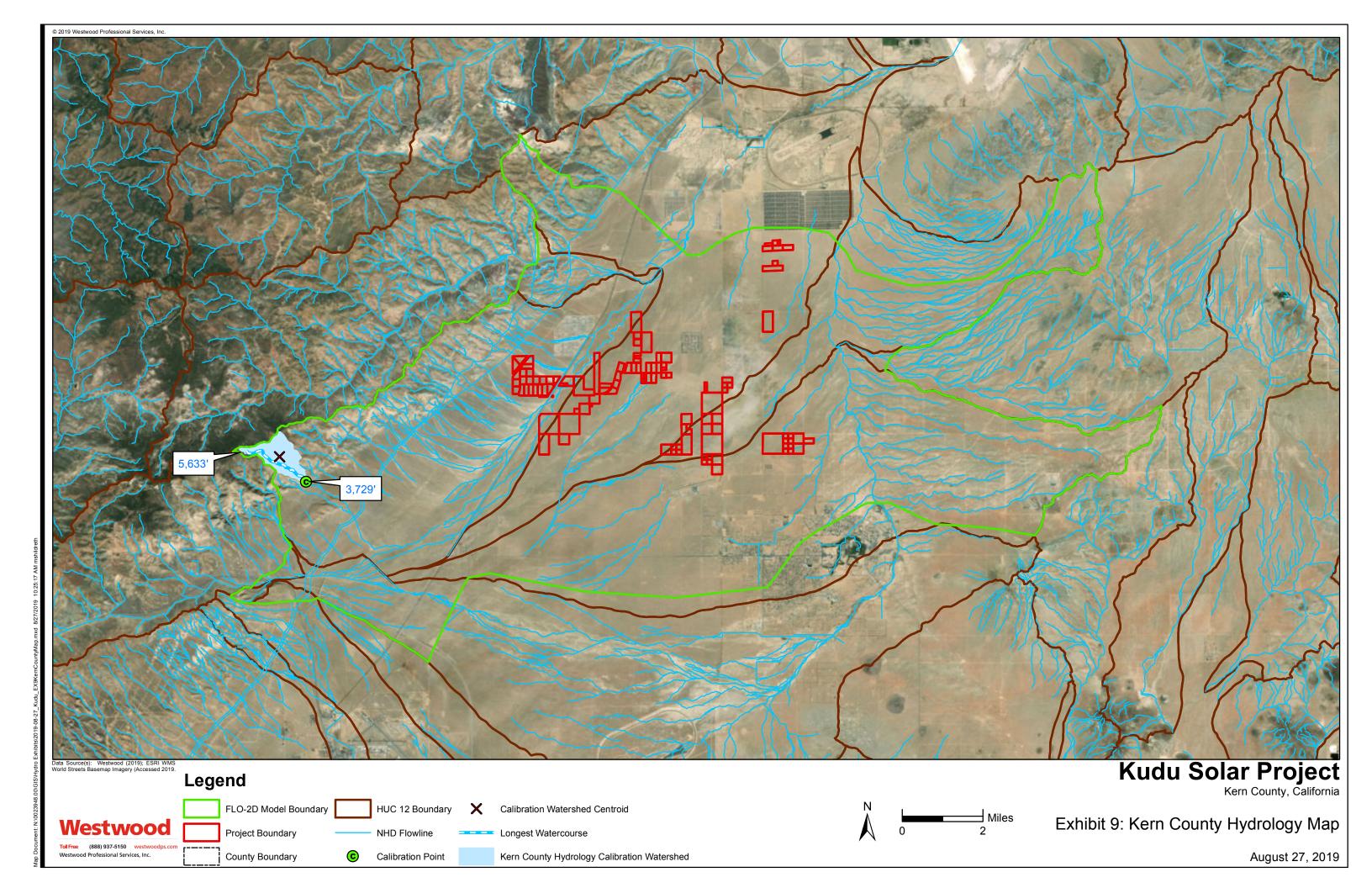














# Appendix A CivilD Printouts (Kern County Hydrology Manual)

## Unit Hydrograph Analysis Copyright (c) CIVILCADD/CIVILDESIGN, 2004, Version 7.0 Study date 04/18/19

| ++++- |                            | -+++++++++                    | -++++++          | ++++++++++++                                |        |
|-------|----------------------------|-------------------------------|------------------|---|--------|
|       |                            |                               |                  |   |        |
|       | Kern Count                 | ty Synthetic I<br>Manual date |                  | raph Hydrology                              | Method |
|       | Program Li                 | cense Serial                  |                  | 6   |        |
|       | Kudu Solar                 | :                             |                  |   |        |
|       |                            |                               |                  |   |        |
|       | Stor                       | rm Event Year                 | = 100            |   |        |
|       | English (                  | in-lb) Input                  | Units Used       | l   |        |
|       | English F                  | Rainfall Data                 | (Inches) I       | nput Values Use                             | ed     |
|       | English (                  | Jnits used in                 | output for       | rmat  |        |
|       |                            | DATA INPUT:<br>Intensity-Dura | ation Curve      | e Slope = 0.600                             |        |
|       | Zone Desig                 | gnation: Deser                | rt Region        | Latitude =                                  | 35.21  |
|       | Sub-<br>(Ac.<br>Rainfall d | -Area I                       | Ouration (hours) | isohyetal data<br>Isohyetal<br>(In)<br>0.75 |        |
|       |                            | data for year<br>573.00       |                  | 1.27  |        |
|       |                            | data for year<br>573.00       | 100              | 2.00  |        |
|       |                            | lata for year<br>573.00       | 100              | 3.71  |        |

```
++
     DESERT REGION area of study
     Log-Log Rainfall Intensity Slope = 0.60
     _____
     ****** Area-averaged max loss rate, Fm ******
     SCS curve
                Area
                          Area
                                    Fр
                                           Αр
     Number
                                                  (In/Hr)
                 (Ac.)
                        Fraction (In/Hr) (dec.)
                                           1.000
     91.0
                573.00
                         1.000
                                   0.180
                                                  0.180
     Area-averaged adjusted loss rate Fm (In/Hr) = 0.180
     ****** Area-Averaged low loss rate fraction, Yb *******
                          SCS CN
                                      S
                                           Pervious
              Area
                           (AMC2)
                                           Yield Fr
      (Ac.)
              Fract
       573.00 1.000
                           91.0
                                      0.99
                                               0.739
     Area-averaged catchment yield fraction, Y = 0.739
     Area-averaged low loss fraction, Yb = 0.261
     Watercourse length =
                        10454.00(Ft.)
     Length from concentration point to centroid = 5544.00(Ft.)
     Elevation difference along watercourse = 1904.00(Ft.)
     Mannings friction factor along watercourse = 0.050
     Watershed area = 573.00(Ac.)
     Catchment Lag time = 0.430 hours
     Unit interval = 5.000 minutes
     Unit interval percentage of lag time = 19.3924
     Hydrograph baseflow = 0.00(CFS)
     Average maximum watershed loss rate(Fm) = 0.180(In/Hr)
     Average low loss rate fraction (Yb) = 0.261 (decimal)
     DESERT S-Graph Selected
     Computed peak 5-minute rainfall = 0.434(In)
     Computed peak 30-minute rainfall = 0.889(In)
     Specified peak 1-hour rainfall = 1.173(In)
     Computed peak 3-hour rainfall = 1.627(In)
     Specified peak 6-hour rainfall = 2.000(In)
     Specified peak 24-hour rainfall = 3.710(In)
     Note: User specified rainfall values used.
     Computed peak 5-minute rainfall = 0.290(In)
     Computed peak 30-minute rainfall = 0.691(In)
     Specified peak 1-hour rainfall = 0.960(In)
     Computed peak 3-hour rainfall = 1.520(In)
     Specified peak 6-hour rainfall = 2.000(In)
     Specified peak 24-hour rainfall = 3.710(In)
     Rainfall depth area reduction factors:
     Using a total area of 573.00(Ac.) (Ref: fig. E-4)
```

```
5-minute factor = 0.974 Adjusted rainfall = 0.283(In)
30-minute factor = 0.974 Adjusted rainfall = 0.673(In)
1-hour factor = 0.974 Adjusted rainfall = 0.935(In)
3-hour factor = 0.996 Adjusted rainfall = 1.514(In)
6-hour factor = 0.998 Adjusted rainfall = 1.996(In)
24-hour factor = 0.999 Adjusted rainfall = 3.706(In)
                     Unit Hydrograph
Unit Hydrograph ((CFS))
                    'S' Graph
Interval
Number
                   Mean values
              (K = 6929.72 (CFS))
                                                74.903
                     1.081
  2
                                              215.541
                     4.191
  3
                    10.407
                                              430.752
                    23.999
                                               941.878
  5
                    42.270
                                             1266.132
  6
                    53.241
                                               760.224
  7
                    61.480
                                               570.933
  8
                    67.344
                                               406.400
  9
                    71.911
                                               316.462
 10
                    75.632
                                               257.893
                     78.653
                                                209.299
 11
 12
                    81.322
                                               184.996
 13
                    83.581
                                                156.532
 14
                     85.433
                                                128.305
 15
                     87.055
                                                112.434
                                               100.395
 16
                     88.504
 17
                    89.786
                                                88.812
 18
                     90.909
                                                 77.870
                    91.966
                                                73.213
 19
 20
                    92.891
                                                64.100
 21
                    93.782
                                                61.755
 22
                    94.467
                                                47.456
 23
                     95.073
                                                41.995
 24
                     95.679
                                                41.995
 25
                     96.160
                                                33.329
                     96.500
                                                23.584
 26
 27
                     96.840
                                                23.576
 28
                     97.181
                                                23.576
 29
                     97.521
                                                23.576
 30
                     97.860
                                                23.534
 31
                     98.115
                                                17.623
                    98.309
 32
                                                13.438
 33
                    98.503
                                                13.438
 34
                    98.696
                                                 13.438
 35
                    98.890
                                                 13.438
 36
                    99.084
                                                 13.438
 37
                    99.278
                                                13.438
 38
                    99.472
                                                13.438
 39
                    99.666
                                                13.438
 40
                   100.000
                                                23.139
```

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| Dainfall      | 11                        | .]           |              | int            |
|---------------|---------------------------|--------------|--------------|----------------|
| Peak Rainfall | values calcu<br>Intensity | Depth        | Adjusted     | Unit Rainfall  |
| Unit Number   | Incensicy                 | Deptii       | Adjusted     | (In)           |
| 1             | 3.48                      | 0.29         | 0.28         | 0.283          |
| 2             | 2.43                      | 0.29         | 0.40         | 0.203          |
| 3             | 1.98                      | 0.49         | 0.48         | 0.086          |
| 4             | 1.70                      | 0.57         | 0.55         | 0.072          |
| 5             | 1.52                      | 0.63         | 0.62         | 0.063          |
| 6             | 1.38                      | 0.69         | 0.67         | 0.057          |
| 7             | 1.27                      | 0.74         | 0.72         | 0.051          |
| 8             | 1.19                      | 0.79         | 0.77         | 0.047          |
| 9             | 1.12                      | 0.84         | 0.82         | 0.044          |
| 10            | 1.06                      | 0.88         | 0.86         | 0.042          |
| 11            | 1.00                      | 0.92         | 0.90         | 0.040          |
| 12            | 0.96                      | 0.96         | 0.94         | 0.038          |
| 13            | 0.92                      | 0.99         | 0.97         | 0.033          |
| 14            | 0.88                      | 1.02         | 1.00         | 0.032          |
| 15            | 0.84                      | 1.05         | 1.03         | 0.031          |
| 16            | 0.81                      | 1.08         | 1.06         | 0.030          |
| 17            | 0.78                      | 1.11         | 1.09         | 0.029          |
| 18            | 0.76                      | 1.14         | 1.12         | 0.028          |
| 19            | 0.73                      | 1.16         | 1.14         | 0.027          |
| 20            | 0.71                      | 1.19         | 1.17         | 0.026          |
| 21            | 0.69                      | 1.21         | 1.20         | 0.025          |
| 22            | 0.67                      | 1.24         | 1.22         | 0.025          |
| 23            | 0.66                      | 1.26         | 1.24         | 0.024          |
| 24            | 0.64                      | 1.28         | 1.27         | 0.023          |
| 25            | 0.63                      | 1.30         | 1.29         | 0.023          |
| 26            | 0.61                      | 1.33         | 1.31         | 0.022          |
| 27            | 0.60                      | 1.35         | 1.33         | 0.022          |
| 28            | 0.59                      | 1.37         | 1.36         | 0.021          |
| 29            | 0.57                      | 1.39         | 1.38         | 0.021          |
| 30            | 0.56                      | 1.41         | 1.40         | 0.021          |
| 31            | 0.55                      | 1.43         | 1.42         | 0.020          |
| 32            | 0.54                      | 1.45         | 1.44         | 0.020          |
| 33            | 0.53                      | 1.47         | 1.46         | 0.020          |
| 34            | 0.52                      | 1.48         | 1.48         | 0.019          |
| 35            | 0.52                      | 1.50         | 1.50         | 0.019          |
| 36<br>37      | 0.51                      | 1.52<br>1.54 | 1.51<br>1.53 | 0.019<br>0.017 |
| 38            | 0.50<br>0.49              | 1.55         | 1.55         | 0.017          |
| 39            | 0.49                      | 1.57         | 1.56         | 0.016          |
| 40            | 0.48                      | 1.58         | 1.58         | 0.016          |
| 41            | 0.47                      | 1.60         | 1.59         | 0.016          |
| 42            | 0.46                      | 1.62         | 1.61         | 0.015          |
| 43            | 0.46                      | 1.63         | 1.63         | 0.015          |
| 44            | 0.45                      | 1.65         | 1.64         | 0.015          |
| 45            | 0.44                      | 1.66         | 1.66         | 0.015          |
| 46            | 0.44                      | 1.67         | 1.67         | 0.015          |
| 47            | 0.43                      | 1.69         | 1.68         | 0.014          |
| 48            | 0.43                      | 1.70         | 1.70         | 0.014          |
| 49            | 0.42                      | 1.72         | 1.71         | 0.014          |
| 50            | 0.42                      | 1.73         | 1.73         | 0.014          |
| 51            | 0.41                      | 1.74         | 1.74         | 0.014          |
| 52            | 0.41                      | 1.76         | 1.75         | 0.014          |
| 53            | 0.40                      | 1.77         | 1.77         | 0.013          |
| 54            | 0.40                      | 1.78         | 1.78         | 0.013          |
| 55            | 0.39                      | 1.80         | 1.79         | 0.013          |
| 56            | 0.39                      | 1.81         | 1.81         | 0.013          |
| 57            | 0.38                      | 1.82         | 1.82         | 0.013          |

| Γ0         | 0 20         | 1 04         | 1 02         | 0 012          |
|------------|--------------|--------------|--------------|----------------|
| 58<br>59   | 0.38<br>0.38 | 1.84<br>1.85 | 1.83<br>1.84 | 0.013<br>0.013 |
| 60         | 0.37         | 1.86         | 1.86         | 0.012          |
| 61         | 0.37         | 1.87         | 1.87         | 0.012          |
| 62<br>63   | 0.36<br>0.36 | 1.89<br>1.90 | 1.88<br>1.89 | 0.012<br>0.012 |
| 64         | 0.36         | 1.91         | 1.90         | 0.012          |
| 65         | 0.35         | 1.92         | 1.92         | 0.012          |
| 66         | 0.35         | 1.93         | 1.93         | 0.012          |
| 67<br>68   | 0.35<br>0.35 | 1.94<br>1.96 | 1.94<br>1.95 | 0.012<br>0.011 |
| 69         | 0.35         | 1.96         | 1.96         | 0.011          |
| 70         | 0.34         | 1.98         | 1.97         | 0.011          |
| 71         | 0.34         | 1.99         | 1.99         | 0.011          |
| 72<br>73   | 0.33<br>0.33 | 2.00         | 2.00         | 0.011          |
| 73<br>74   | 0.33         | 2.01<br>2.02 | 2.01<br>2.02 | 0.012<br>0.012 |
| 75         | 0.33         | 2.03         | 2.03         | 0.012          |
| 76         | 0.32         | 2.05         | 2.04         | 0.012          |
| 77         | 0.32         | 2.06         | 2.06         | 0.012          |
| 78<br>79   | 0.32<br>0.32 | 2.07<br>2.08 | 2.07<br>2.08 | 0.012<br>0.012 |
| 80         | 0.31         | 2.09         | 2.09         | 0.012          |
| 81         | 0.31         | 2.11         | 2.10         | 0.012          |
| 82         | 0.31         | 2.12         | 2.12         | 0.012          |
| 83<br>84   | 0.31<br>0.31 | 2.13<br>2.14 | 2.13<br>2.14 | 0.011<br>0.011 |
| 85         | 0.30         | 2.15         | 2.15         | 0.011          |
| 86         | 0.30         | 2.16         | 2.16         | 0.011          |
| 87         | 0.30         | 2.17         | 2.17         | 0.011          |
| 88<br>89   | 0.30<br>0.30 | 2.18<br>2.20 | 2.18<br>2.19 | 0.011<br>0.011 |
| 90         | 0.30         | 2.20         | 2.19         | 0.011          |
| 91         | 0.29         | 2.22         | 2.22         | 0.011          |
| 92         | 0.29         | 2.23         | 2.23         | 0.011          |
| 93<br>94   | 0.29<br>0.29 | 2.24<br>2.25 | 2.24<br>2.25 | 0.011<br>0.011 |
| 95         | 0.29         | 2.26         | 2.26         | 0.011          |
| 96         | 0.28         | 2.27         | 2.27         | 0.011          |
| 97         | 0.28         | 2.28         | 2.28         | 0.011          |
| 98<br>99   | 0.28<br>0.28 | 2.29<br>2.30 | 2.29<br>2.30 | 0.010<br>0.010 |
| 100        | 0.28         | 2.31         | 2.31         | 0.010          |
| 101        | 0.28         | 2.32         | 2.32         | 0.010          |
| 102        | 0.27         | 2.33         | 2.33         | 0.010          |
| 103<br>104 | 0.27<br>0.27 | 2.34<br>2.35 | 2.34<br>2.35 | 0.010<br>0.010 |
| 105        | 0.27         | 2.36         | 2.36         | 0.010          |
| 106        | 0.27         | 2.37         | 2.37         | 0.010          |
| 107        | 0.27         | 2.38         | 2.38         | 0.010          |
| 108<br>109 | 0.27<br>0.26 | 2.39<br>2.40 | 2.39<br>2.40 | 0.010<br>0.010 |
| 110        | 0.26         | 2.40         | 2.40         | 0.010          |
| 111        | 0.26         | 2.42         | 2.42         | 0.010          |
| 112        | 0.26         | 2.43         | 2.43         | 0.010          |
| 113<br>114 | 0.26<br>0.26 | 2.44<br>2.45 | 2.44<br>2.45 | 0.010<br>0.010 |
| 115        | 0.26         | 2.45         | 2.45         | 0.010          |
| 116        | 0.26         | 2.47         | 2.47         | 0.010          |
| 117        | 0.25         | 2.48         | 2.48         | 0.009          |

| 118<br>119<br>120<br>121<br>122<br>123<br>124<br>125<br>126<br>127<br>128<br>129 | 0.25<br>0.25<br>0.25<br>0.25<br>0.25<br>0.25<br>0.25<br>0.25 | 2.49<br>2.50<br>2.51<br>2.52<br>2.53<br>2.54<br>2.55<br>2.55<br>2.56<br>2.57<br>2.58<br>2.59<br>2.60 | 2.49<br>2.50<br>2.51<br>2.52<br>2.53<br>2.54<br>2.54<br>2.55<br>2.56<br>2.57<br>2.58<br>2.59<br>2.60 | 0.009<br>0.009<br>0.009<br>0.009<br>0.009<br>0.009<br>0.009<br>0.009<br>0.009 |
|--|--|--|--|---|
| 131<br>132   | 0.24   | 2.61<br>2.62   | 2.61<br>2.62   | 0.009   |
| 133  | 0.24   | 2.63   | 2.63   | 0.009   |
| 134<br>135   | 0.24<br>0.24   | 2.64<br>2.64   | 2.63<br>2.64   | 0.009<br>0.009  |
| 136  | 0.23   | 2.65   | 2.65   | 0.009   |
| 137  | 0.23   | 2.66   | 2.66   | 0.009   |
| 138<br>139   | 0.23<br>0.23   | 2.67<br>2.68   | 2.67<br>2.68   | 0.009<br>0.009  |
| 140  | 0.23   | 2.69   | 2.69   | 0.009   |
| 141<br>142   | 0.23<br>0.23   | 2.70<br>2.70   | 2.69<br>2.70   | 0.009<br>0.009  |
| 143  | 0.23   | 2.70   | 2.70   | 0.003   |
| 144  | 0.23   | 2.72   | 2.72   | 0.008   |
| 145<br>146   | 0.23<br>0.23   | 2.73<br>2.74   | 2.73<br>2.74   | 0.008   |
| 147  | 0.22   | 2.75   | 2.74   | 0.008   |
| 148  | 0.22   | 2.75   | 2.75   | 0.008   |
| 149<br>150   | 0.22<br>0.22   | 2.76<br>2.77   | 2.76<br>2.77   | 0.008<br>0.008  |
| 151  | 0.22   | 2.78   | 2.78   | 0.008   |
| 152<br>153   | 0.22<br>0.22   | 2.79<br>2.80   | 2.79<br>2.79   | 0.008<br>0.008  |
| 154  | 0.22   | 2.80   | 2.80   | 0.008   |
| 155  | 0.22   | 2.81   | 2.81   | 0.008   |
| 156<br>157   | 0.22<br>0.22   | 2.82<br>2.83   | 2.82<br>2.83   | 0.008<br>0.008  |
| 158  | 0.22   | 2.84   | 2.83   | 0.008   |
| 159<br>160   | 0.21<br>0.21   | 2.84<br>2.85   | 2.84<br>2.85   | 0.008<br>0.008  |
| 161  | 0.21   | 2.86   | 2.86   | 0.008   |
| 162  | 0.21   | 2.87   | 2.87   | 0.008   |
| 163<br>164   | 0.21<br>0.21   | 2.88<br>2.88   | 2.87<br>2.88   | 0.008   |
| 165  | 0.21   | 2.89   | 2.89   | 0.008   |
| 166<br>167   | 0.21<br>0.21   | 2.90<br>2.91   | 2.90<br>2.91   | 0.008   |
| 168  | 0.21   | 2.91   | 2.91   | 0.008<br>0.008  |
| 169  | 0.21   | 2.92   | 2.92   | 0.008   |
| 170<br>171   | 0.21<br>0.21   | 2.93<br>2.94   | 2.93<br>2.94   | 0.008<br>0.008  |
| 172  | 0.21   | 2.95   | 2.94   | 0.008   |
| 173  | 0.20   | 2.95   | 2.95   | 0.008   |
| 174<br>175   | 0.20<br>0.20   | 2.96<br>2.97   | 2.96<br>2.97   | 0.008<br>0.008  |
| 176  | 0.20   | 2.98   | 2.97   | 0.008   |
| 177  | 0.20   | 2.98   | 2.98   | 0.008   |

| 178<br>179<br>180<br>181<br>182<br>183<br>184<br>185               | 0.20<br>0.20<br>0.20<br>0.20<br>0.20<br>0.20<br>0.20<br>0.20         | 2.99 3.00 3.01 3.01 3.02 3.03 3.04 3.04 3.05                                 | 2.99 3.00 3.00 3.01 3.02 3.03 3.03 3.04 3.05                                 | 0.008<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007          |
|--|--|--|--|--|
| 187<br>188<br>189<br>190<br>191<br>192<br>193                      | 0.20<br>0.20<br>0.20<br>0.19<br>0.19<br>0.19<br>0.19                 | 3.06<br>3.06<br>3.07<br>3.08<br>3.09<br>3.09<br>3.10<br>3.11                 | 3.06<br>3.06<br>3.07<br>3.08<br>3.09<br>3.09<br>3.10<br>3.11                 | 0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007          |
| 195<br>196<br>197<br>198<br>199<br>200<br>201                      | 0.19<br>0.19<br>0.19<br>0.19<br>0.19<br>0.19<br>0.19                 | 3.12<br>3.12<br>3.13<br>3.14<br>3.14<br>3.15<br>3.16<br>3.16                 | 3.11<br>3.12<br>3.13<br>3.14<br>3.14<br>3.15<br>3.16<br>3.16                 | 0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007          |
| 203<br>204<br>205<br>206<br>207<br>208<br>209<br>210               | 0.19<br>0.19<br>0.19<br>0.19<br>0.19<br>0.18<br>0.18                 | 3.17<br>3.18<br>3.19<br>3.19<br>3.20<br>3.21<br>3.21<br>3.22                 | 3.17<br>3.18<br>3.18<br>3.19<br>3.20<br>3.20<br>3.21<br>3.22                 | 0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007          |
| 211<br>212<br>213<br>214<br>215<br>216<br>217<br>218               | 0.18<br>0.18<br>0.18<br>0.18<br>0.18<br>0.18<br>0.18                 | 3.23<br>3.23<br>3.24<br>3.25<br>3.25<br>3.26<br>3.27<br>3.27                 | 3.23<br>3.23<br>3.24<br>3.25<br>3.25<br>3.26<br>3.27<br>3.27                 | 0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007          |
| 219<br>220<br>221<br>222<br>223<br>224<br>225<br>226<br>227        | 0.18<br>0.18<br>0.18<br>0.18<br>0.18<br>0.18<br>0.18<br>0.18         | 3.28<br>3.29<br>3.29<br>3.30<br>3.31<br>3.31<br>3.32<br>3.33<br>3.33         | 3.28<br>3.29<br>3.29<br>3.30<br>3.31<br>3.31<br>3.32<br>3.33<br>3.33         | 0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007<br>0.007 |
| 228<br>229<br>230<br>231<br>232<br>233<br>234<br>235<br>236<br>237 | 0.18<br>0.18<br>0.17<br>0.17<br>0.17<br>0.17<br>0.17<br>0.17<br>0.17 | 3.34<br>3.35<br>3.35<br>3.36<br>3.37<br>3.37<br>3.38<br>3.39<br>3.39<br>3.40 | 3.34<br>3.35<br>3.35<br>3.36<br>3.36<br>3.37<br>3.38<br>3.38<br>3.39<br>3.40 | 0.007<br>0.007<br>0.007<br>0.006<br>0.006<br>0.006<br>0.006<br>0.006 |

| 238        | 0 17         | 2 40         |      | 2 40         |   | 0 006          |  |
|------------|--------------|--------------|------|--------------|---|----------------|--|
| 239        | 0.17<br>0.17 | 3.40<br>3.41 |      | 3.40<br>3.41 |   | 0.006          |  |
| 240        | 0.17         | 3.42         |      | 3.42         |   | 0.006          |  |
| 241        | 0.17         | 3.42         |      | 3.42         |   | 0.006          |  |
| 242        | 0.17         | 3.43         |      | 3.43         |   | 0.006          |  |
| 243        | 0.17         | 3.44         |      | 3.44         |   | 0.006          |  |
| 244        | 0.17         | 3.44         |      | 3.44         |   | 0.006          |  |
| 245        | 0.17         | 3.45         |      | 3.45         |   | 0.006          |  |
| 246        | 0.17         | 3.45         |      | 3.45         |   | 0.006          |  |
| 247        | 0.17         | 3.46         |      | 3.46         |   | 0.006          |  |
| 248        | 0.17         | 3.47         |      | 3.47         |   | 0.006          |  |
| 249<br>250 | 0.17<br>0.17 | 3.47<br>3.48 |      | 3.47<br>3.48 |   | 0.006<br>0.006 |  |
| 251        | 0.17         | 3.49         |      | 3.49         |   | 0.006          |  |
| 252        | 0.17         | 3.49         |      | 3.49         |   | 0.006          |  |
| 253        | 0.17         | 3.50         |      | 3.50         |   | 0.006          |  |
| 254        | 0.17         | 3.50         |      | 3.50         |   | 0.006          |  |
| 255        | 0.17         | 3.51         |      | 3.51         |   | 0.006          |  |
| 256        | 0.16         | 3.52         |      | 3.52         |   | 0.006          |  |
| 257        | 0.16         | 3.52         |      | 3.52         |   | 0.006          |  |
| 258        | 0.16         | 3.53         |      | 3.53         |   | 0.006          |  |
| 259        | 0.16         | 3.54         |      | 3.53         |   | 0.006          |  |
| 260<br>261 | 0.16<br>0.16 | 3.54<br>3.55 |      | 3.54<br>3.55 |   | 0.006          |  |
| 262        | 0.16         | 3.55         |      | 3.55         |   | 0.006<br>0.006 |  |
| 263        | 0.16         | 3.56         |      | 3.56         |   | 0.006          |  |
| 264        | 0.16         | 3.57         |      | 3.56         |   | 0.006          |  |
| 265        | 0.16         | 3.57         |      | 3.57         |   | 0.006          |  |
| 266        | 0.16         | 3.58         |      | 3.58         |   | 0.006          |  |
| 267        | 0.16         | 3.58         |      | 3.58         |   | 0.006          |  |
| 268        | 0.16         | 3.59         |      | 3.59         |   | 0.006          |  |
| 269        | 0.16         | 3.60         |      | 3.59         |   | 0.006          |  |
| 270        | 0.16         | 3.60         |      | 3.60<br>3.61 |   | 0.006          |  |
| 271<br>272 | 0.16<br>0.16 | 3.61<br>3.61 |      | 3.61         |   | 0.006<br>0.006 |  |
| 272        | 0.16         | 3.62         |      | 3.62         |   | 0.006          |  |
| 274        | 0.16         | 3.62         |      | 3.62         |   | 0.006          |  |
| 275        | 0.16         | 3.63         |      | 3.63         |   | 0.006          |  |
| 276        | 0.16         | 3.64         |      | 3.64         |   | 0.006          |  |
| 277        | 0.16         | 3.64         |      | 3.64         |   | 0.006          |  |
| 278        | 0.16         | 3.65         |      | 3.65         |   | 0.006          |  |
| 279        | 0.16         | 3.65         |      | 3.65         |   | 0.006          |  |
| 280        | 0.16         | 3.66         |      | 3.66         |   | 0.006          |  |
| 281<br>282 | 0.16<br>0.16 | 3.67<br>3.67 |      | 3.67<br>3.67 |   | 0.006          |  |
| 283        | 0.16         | 3.68         |      | 3.68         |   | 0.006          |  |
| 284        | 0.16         | 3.68         |      | 3.68         |   | 0.006          |  |
| 285        | 0.16         | 3.69         |      | 3.69         |   | 0.006          |  |
| 286        | 0.16         | 3.69         |      | 3.69         |   | 0.006          |  |
| 287        | 0.15         | 3.70         |      | 3.70         |   | 0.006          |  |
| 288        | 0.15         | 3.71         |      | 3.71         |   | 0.006          |  |
| Time =     | 24.00 Hours  | Total        | unit | rainfall     | = | 3.71(In)       |  |
|            |              | <br>         |      |              |   |                |  |
|            |              |              |      |              |   |                |  |

| Unit     | Unit     | Unit      | Effective |
|----------|----------|-----------|-----------|
| Period   | Rainfall | Soil-Loss | Rainfall  |
| (number) | (In)     | (In)      | (In)      |
|          |          |           |           |

1

| 2  | 0 0050 | 0 0015 | 0 0043 |
|----|--------|--------|--------|
| 2  | 0.0058 | 0.0015 | 0.0043 |
| 3  | 0.0058 | 0.0015 | 0.0043 |
| 4  | 0.0058 | 0.0015 | 0.0043 |
| 5  | 0.0058 | 0.0015 | 0.0043 |
| 6  | 0.0058 | 0.0015 | 0.0043 |
| 7  | 0.0058 | 0.0015 | 0.0043 |
|    |        |        |        |
| 8  | 0.0059 | 0.0015 | 0.0043 |
| 9  | 0.0059 | 0.0015 | 0.0043 |
| 10 | 0.0059 | 0.0015 | 0.0044 |
| 11 | 0.0059 | 0.0015 | 0.0044 |
| 12 | 0.0059 | 0.0016 | 0.0044 |
| 13 | 0.0060 | 0.0016 | 0.0044 |
| 14 | 0.0060 | 0.0016 | 0.0044 |
|    |        |        |        |
| 15 | 0.0060 | 0.0016 | 0.0044 |
| 16 | 0.0060 | 0.0016 | 0.0044 |
| 17 | 0.0060 | 0.0016 | 0.0045 |
| 18 | 0.0060 | 0.0016 | 0.0045 |
| 19 | 0.0061 | 0.0016 | 0.0045 |
| 20 | 0.0061 | 0.0016 | 0.0045 |
|    | 0.0061 |        |        |
| 21 |        | 0.0016 | 0.0045 |
| 22 | 0.0061 | 0.0016 | 0.0045 |
| 23 | 0.0061 | 0.0016 | 0.0045 |
| 24 | 0.0062 | 0.0016 | 0.0046 |
| 25 | 0.0062 | 0.0016 | 0.0046 |
| 26 | 0.0062 | 0.0016 | 0.0046 |
| 27 | 0.0062 | 0.0016 | 0.0046 |
|    |        |        |        |
| 28 | 0.0062 | 0.0016 | 0.0046 |
| 29 | 0.0063 | 0.0016 | 0.0046 |
| 30 | 0.0063 | 0.0016 | 0.0046 |
| 31 | 0.0063 | 0.0017 | 0.0047 |
| 32 | 0.0063 | 0.0017 | 0.0047 |
| 33 | 0.0064 | 0.0017 | 0.0047 |
| 34 | 0.0064 | 0.0017 | 0.0047 |
|    |        |        |        |
| 35 | 0.0064 | 0.0017 | 0.0047 |
| 36 | 0.0064 | 0.0017 | 0.0047 |
| 37 | 0.0064 | 0.0017 | 0.0048 |
| 38 | 0.0065 | 0.0017 | 0.0048 |
| 39 | 0.0065 | 0.0017 | 0.0048 |
| 40 | 0.0065 | 0.0017 | 0.0048 |
| 41 | 0.0065 | 0.0017 | 0.0048 |
| 42 | 0.0066 | 0.0017 | 0.0048 |
|    |        |        |        |
| 43 | 0.0066 | 0.0017 | 0.0049 |
| 44 | 0.0066 | 0.0017 | 0.0049 |
| 45 | 0.0066 | 0.0017 | 0.0049 |
| 46 | 0.0067 | 0.0017 | 0.0049 |
| 47 | 0.0067 | 0.0017 | 0.0049 |
| 48 | 0.0067 | 0.0018 | 0.0050 |
| 49 | 0.0067 | 0.0018 | 0.0050 |
| 50 |        | 0.0018 | 0.0050 |
|    | 0.0068 |        |        |
| 51 | 0.0068 | 0.0018 | 0.0050 |
| 52 | 0.0068 | 0.0018 | 0.0050 |
| 53 | 0.0068 | 0.0018 | 0.0051 |
| 54 | 0.0069 | 0.0018 | 0.0051 |
| 55 | 0.0069 | 0.0018 | 0.0051 |
| 56 | 0.0069 | 0.0018 | 0.0051 |
| 57 | 0.0070 | 0.0018 | 0.0051 |
|    |        |        |        |
| 58 | 0.0070 | 0.0018 | 0.0052 |
| 59 | 0.0070 | 0.0018 | 0.0052 |
| 60 | 0.0070 | 0.0018 | 0.0052 |
| 61 | 0.0071 | 0.0018 | 0.0052 |
|    |        |        |        |

| 66 0.0072 0.0019<br>67 0.0073 0.0019<br>68 0.0073 0.0019  | 0.0054   |
|---|--|
| 69       0.0073       0.0019         70       0.0073       0.0019         71       0.0074       0.0019         72       0.0074       0.0019         73       0.0075       0.0019         74       0.0075       0.0020         75       0.0075       0.0020  | 0.0054<br>0.0054<br>0.0055<br>0.0055<br>0.0055<br>0.0055                     |
| 76       0.0076       0.0020         77       0.0076       0.0020         78       0.0076       0.0020         79       0.0077       0.0020         80       0.0077       0.0020         81       0.0078       0.0020         82       0.0078       0.0020         83       0.0078       0.0020   | 0.0056<br>0.0056<br>0.0057<br>0.0057<br>0.0057<br>0.0057<br>0.0057           |
| 84       0.0079       0.0021         85       0.0079       0.0021         86       0.0079       0.0021         87       0.0080       0.0021         88       0.0080       0.0021         89       0.0081       0.0021         90       0.0081       0.0021  | 0.0058<br>0.0058<br>0.0059<br>0.0059<br>0.0059<br>0.0060                     |
| 91       0.0082       0.0021         92       0.0082       0.0021         93       0.0083       0.0022         94       0.0083       0.0022         95       0.0083       0.0022         96       0.0084       0.0022         97       0.0084       0.0022         00       0.0022       0.0032   | 0.0060<br>0.0061<br>0.0061<br>0.0061<br>0.0062<br>0.0062                     |
| 98       0.0085       0.0022         99       0.0085       0.0022         100       0.0086       0.0022         101       0.0086       0.0023         102       0.0087       0.0023         103       0.0088       0.0023         104       0.0088       0.0023         105       0.0089       0.0023   | 0.0063<br>0.0063<br>0.0064<br>0.0064<br>0.0065<br>0.0065                     |
| 106       0.0089       0.0023         107       0.0090       0.0023         108       0.0090       0.0024         109       0.0091       0.0024         110       0.0091       0.0024         111       0.0092       0.0024         112       0.0093       0.0024   | 0.0066<br>0.0066<br>0.0067<br>0.0067<br>0.0067<br>0.0068                     |
| 113       0.0093       0.0024         114       0.0094       0.0025         115       0.0095       0.0025         116       0.0095       0.0025         117       0.0096       0.0025         118       0.0097       0.0025         119       0.0098       0.0026         120       0.0098       0.0026         121       0.0099       0.0026 | 0.0069<br>0.0069<br>0.0070<br>0.0070<br>0.0071<br>0.0071<br>0.0072<br>0.0072 |

| 1 2 2 | 0.0100 | 0 0026 | 0 0074 |
|-------|--------|--------|--------|
| 122   | 0.0100 | 0.0026 | 0.0074 |
| 123   | 0.0101 | 0.0026 | 0.0074 |
| 124   | 0.0101 | 0.0026 | 0.0075 |
| 125   | 0.0102 | 0.0027 | 0.0076 |
|       |        |        |        |
| 126   | 0.0103 | 0.0027 | 0.0076 |
| 127   | 0.0104 | 0.0027 | 0.0077 |
| 128   | 0.0105 | 0.0027 | 0.0077 |
| 129   | 0.0106 | 0.0028 | 0.0078 |
|       |        |        |        |
| 130   | 0.0106 | 0.0028 | 0.0079 |
| 131   | 0.0108 | 0.0028 | 0.0080 |
| 132   | 0.0108 | 0.0028 | 0.0080 |
| 133   | 0.0110 | 0.0029 | 0.0081 |
| 134   |        |        | 0.0082 |
|       | 0.0110 | 0.0029 |        |
| 135   | 0.0112 | 0.0029 | 0.0083 |
| 136   | 0.0112 | 0.0029 | 0.0083 |
| 137   | 0.0114 | 0.0030 | 0.0084 |
| 138   | 0.0115 | 0.0030 | 0.0085 |
|       |        |        |        |
| 139   | 0.0116 | 0.0030 | 0.0086 |
| 140   | 0.0117 | 0.0031 | 0.0087 |
| 141   | 0.0119 | 0.0031 | 0.0088 |
| 142   | 0.0120 | 0.0031 | 0.0088 |
|       |        |        |        |
| 143   | 0.0121 | 0.0032 | 0.0090 |
| 144   | 0.0122 | 0.0032 | 0.0090 |
| 145   | 0.0111 | 0.0029 | 0.0082 |
| 146   | 0.0112 | 0.0029 | 0.0083 |
|       |        |        | 0.0084 |
| 147   | 0.0114 | 0.0030 |        |
| 148   | 0.0115 | 0.0030 | 0.0085 |
| 149   | 0.0117 | 0.0031 | 0.0086 |
| 150   | 0.0118 | 0.0031 | 0.0087 |
| 151   | 0.0120 | 0.0031 | 0.0089 |
|       |        |        |        |
| 152   | 0.0122 | 0.0032 | 0.0090 |
| 153   | 0.0124 | 0.0032 | 0.0092 |
| 154   | 0.0125 | 0.0033 | 0.0093 |
| 155   | 0.0128 | 0.0033 | 0.0094 |
| 156   |        |        |        |
|       | 0.0129 | 0.0034 | 0.0095 |
| 157   | 0.0132 | 0.0035 | 0.0098 |
| 158   | 0.0134 | 0.0035 | 0.0099 |
| 159   | 0.0137 | 0.0036 | 0.0101 |
| 160   | 0.0138 | 0.0036 | 0.0102 |
| 161   |        |        |        |
|       | 0.0142 | 0.0037 | 0.0105 |
| 162   | 0.0144 | 0.0038 | 0.0106 |
| 163   | 0.0148 | 0.0039 | 0.0109 |
| 164   | 0.0150 | 0.0039 | 0.0111 |
| 165   | 0.0154 | 0.0040 | 0.0114 |
|       |        |        |        |
| 166   | 0.0156 | 0.0041 | 0.0115 |
| 167   | 0.0161 | 0.0042 | 0.0119 |
| 168   | 0.0164 | 0.0043 | 0.0121 |
| 169   | 0.0186 | 0.0049 | 0.0137 |
|       |        | 0.0049 |        |
| 170   | 0.0189 |        | 0.0139 |
| 171   | 0.0195 | 0.0051 | 0.0144 |
| 172   | 0.0199 | 0.0052 | 0.0147 |
| 173   | 0.0206 | 0.0054 | 0.0152 |
| 174   | 0.0210 | 0.0055 | 0.0155 |
|       |        |        |        |
| 175   | 0.0219 | 0.0057 | 0.0162 |
| 176   | 0.0224 | 0.0058 | 0.0165 |
| 177   | 0.0234 | 0.0061 | 0.0173 |
| 178   | 0.0240 | 0.0063 | 0.0177 |
| 179   | 0.0253 | 0.0066 | 0.0187 |
|       |        |        |        |
| 180   | 0.0260 | 0.0068 | 0.0192 |
| 181   | 0.0277 | 0.0072 | 0.0204 |
|       |        |        |        |

| 182 | 0.0286 | 0.0075  | 0.0211 |
|-----|--------|---------|--------|
| 183 | 0.0307 | 0.0080  | 0.0227 |
| 184 | 0.0320 | 0.0084  | 0.0236 |
| 185 | 0.0378 | 0.0099  | 0.0279 |
| 186 | 0.0370 | 0.0104  | 0.0293 |
| 187 | 0.0357 | 0.0104  | 0.0328 |
|     |        |         |        |
| 188 | 0.0474 | 0.0124  | 0.0350 |
| 189 | 0.0569 | 0.0149  | 0.0421 |
| 190 | 0.0632 | 0.0150* | 0.0482 |
| 191 | 0.0858 | 0.0150* | 0.0708 |
| 192 | 0.1128 | 0.0150* | 0.0978 |
| 193 | 0.2826 | 0.0150* | 0.2676 |
| 194 | 0.0720 | 0.0150* | 0.0570 |
| 195 | 0.0511 | 0.0133  | 0.0377 |
| 196 | 0.0418 | 0.0109  | 0.0309 |
| 197 | 0.0334 | 0.0087  | 0.0247 |
| 198 | 0.0296 | 0.0077  | 0.0219 |
| 199 | 0.0268 | 0.0070  | 0.0198 |
| 200 | 0.0246 | 0.0064  | 0.0182 |
| 201 | 0.0229 | 0.0060  | 0.0169 |
| 202 | 0.0215 | 0.0056  | 0.0158 |
| 203 | 0.0202 | 0.0053  | 0.0149 |
| 204 | 0.0192 | 0.0050  | 0.0142 |
| 205 | 0.0166 | 0.0043  | 0.0123 |
| 206 | 0.0159 | 0.0041  | 0.0117 |
| 207 | 0.0152 | 0.0040  | 0.0112 |
| 208 | 0.0146 | 0.0038  | 0.0108 |
| 209 | 0.0140 | 0.0037  | 0.0104 |
| 210 | 0.0135 | 0.0035  | 0.0100 |
| 211 | 0.0133 | 0.0034  | 0.0097 |
| 212 | 0.0131 | 0.0033  | 0.0093 |
| 213 | 0.0127 | 0.0033  | 0.0091 |
| 214 | 0.0123 | 0.0032  | 0.0088 |
| 214 | 0.0119 | 0.0031  | 0.0086 |
| 216 | 0.0113 | 0.0030  | 0.0083 |
| 217 | 0.0123 | 0.0030  | 0.0083 |
|     |        |         |        |
| 218 | 0.0121 | 0.0031  | 0.0089 |
| 219 | 0.0118 | 0.0031  | 0.0087 |
| 220 | 0.0116 | 0.0030  | 0.0085 |
| 221 | 0.0113 | 0.0030  | 0.0084 |
| 222 | 0.0111 | 0.0029  | 0.0082 |
| 223 | 0.0109 | 0.0028  | 0.0081 |
| 224 | 0.0107 | 0.0028  | 0.0079 |
| 225 | 0.0105 | 0.0027  | 0.0078 |
| 226 | 0.0103 | 0.0027  | 0.0076 |
| 227 | 0.0102 | 0.0027  | 0.0075 |
| 228 | 0.0100 | 0.0026  | 0.0074 |
| 229 | 0.0099 | 0.0026  | 0.0073 |
| 230 | 0.0097 | 0.0025  | 0.0072 |
| 231 | 0.0096 | 0.0025  | 0.0071 |
| 232 | 0.0094 | 0.0025  | 0.0070 |
| 233 | 0.0093 | 0.0024  | 0.0069 |
| 234 | 0.0092 | 0.0024  | 0.0068 |
| 235 | 0.0091 | 0.0024  | 0.0067 |
| 236 | 0.0089 | 0.0023  | 0.0066 |
| 237 | 0.0088 | 0.0023  | 0.0065 |
| 238 | 0.0087 | 0.0023  | 0.0064 |
| 239 | 0.0086 | 0.0023  | 0.0064 |
| 240 | 0.0085 | 0.0022  | 0.0063 |
| 241 | 0.0084 | 0.0022  | 0.0062 |
|     |        |         |        |

```
0.0022
              0.0083
                                               0.0061
243
              0.0082
                             0.0021
                                               0.0061
244
              0.0081
                             0.0021
                                               0.0060
                             0.0021
245
              0.0080
                                               0.0059
246
              0.0080
                             0.0021
                                               0.0059
              0.0079
                             0.0021
247
                                               0.0058
              0.0078
                             0.0020
248
                                               0.0058
              0.0077
                             0.0020
249
                                                0.0057
              0.0077
                             0.0020
250
                                                0.0057
              0.0077
0.0076
0.0075
0.0074
                             0.0020
251
                                                0.0056
                             0.0020
252
                                                0.0055
253
                             0.0019
                                                0.0055
              0.0074
0.0073
0.0072
254
                             0.0019
                                                0.0054
                             0.0019
                                               0.0054
255
256
                             0.0019
                                               0.0053
              0.0072
0.0071
                             0.0019
257
                                               0.0053
                             0.0019
                                               0.0053
258
              0.0071
                             0.0018
                                               0.0052
259
260
              0.0070
                             0.0018
                                               0.0052
261
              0.0069
                             0.0018
                                               0.0051
262
              0.0069
                             0.0018
                                               0.0051
              0.0068
                             0.0018
                                               0.0050
263
264
              0.0068
                             0.0018
                                               0.0050
265
              0.0067
                             0.0018
                                               0.0050
              0.0067
                             0.0017
                                               0.0049
266
                             0.0017
                                               0.0049
267
              0.0066
                             0.0017
              0.0066
                                               0.0049
268
                             0.0017
269
               0.0065
                                               0.0048
               0.0065
                             0.0017
                                               0.0048
270
                             0.0017
               0.0064
                                               0.0048
271
                             0.0017
272
               0.0064
                                               0.0047
                             0.0017
273
               0.0063
                           0.0017
0.0016
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0.0016
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0.0015
0.0015
                                                0.0047
               0.0063
274
                                               0.0047
               0.0063
275
                                               0.0046
              0.0062
276
                                               0.0046
              0.0062
                                               0.0046
277
              0.0061
                                               0.0045
278
              0.0061
279
                                               0.0045
              0.0061
280
                                               0.0045
              0.0060
                                               0.0044
281
282
              0.0060
                                               0.0044
283
              0.0059
                                               0.0044
              0.0059
                                               0.0044
              0.0059
285
                                               0.0043
              0.0058
286
                                               0.0043
287
              0.0058
                             0.0015
                                               0.0043
              0.0058 0.0015
288
                                               0.0043
               3.7057
                              0.8823
                                                2.8234
______
Total soil rain loss = 0.88(In)
Total effective rainfall = 2.82(In)
Peak flow rate in flood hydrograph = 611.02(CFS)
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# 24 - HOUR STORM Runoff Hydrograph

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| _         | Hydrogr      | aph in | 5    | Minute inter | rvals ((CF: | 5))   |
|-----------|--------------|--------|------|--------------|-------------|-------|
| Time(h+m) | Volume Ac.Ft | Q(CFS  | 3) 0 | 175.0        | 350.0       | 525.0 |
| 0+ 5      | 0.0022       | 0.32   | Q    |              |             |       |
| 0+10      | 0.0107       | 1.23   | Q    |              |             |       |
| 0+15      | 0.0318       | 3.07   | Q    |              |             |       |
| 0+20      | 0.0805       | 7.07   | Q    |              |             |       |
| 0+25      | 0.1664       | 12.47  | Q    |              |             |       |
| 0+30      | 0.2747       | 15.73  | Q    |              |             |       |
| 0+35      | 0.4000       | 18.20  | VQ   |              |             |       |
| 0+40      | 0.5376       | 19.97  | VQ   |              |             |       |
| 0+45      | 0.6848       | 21.38  | VQ   |              |             |       |
| 0+50      | 0.8400       | 22.53  | VQ   |              |             |       |
| 0+55      | 1.0017       | 23.49  | VQ   |              |             |       |
| 1+ 0      | 1.1694       | 24.34  | VQ   |              |             |       |
| 1+ 5      | 1.3421       | 25.08  | VQ   |              |             |       |
| 1+10      | 1.5191       | 25.70  | VQ   |              |             |       |
| 1+15      | 1.6999       | 26.26  | VQ   |              |             |       |
| 1+20      | 1.8842       | 26.76  | VQ   |              |             |       |
| 1+25      | 2.0717       | 27.22  | VQ   |              |             |       |
| 1+30      | 2.2620       | 27.63  | VQ   |              |             |       |
| 1+35      | 2.4550       | 28.03  | VQ   |              |             |       |
| 1+40      | 2.6505       | 28.39  | VQ   |              |             |       |
| 1+45      | 2.8484       | 28.74  | VQ   |              |             |       |
| 1+50      | 3.0484       | 29.03  | VQ   |              |             |       |
| 1+55      | 3.2501       | 29.30  | VQ   |              |             |       |
| 2+ 0      | 3.4538       | 29.57  | Q    |              |             |       |
|           |              |        |      |              |             |       |

| 2+ 5 | 3.6591  | 29.80 | Q  |   | 1 | 1 |  |
|------|---------|-------|----|---|---|---|--|
| 2+10 | 3.8657  | 30.00 | Q  |   |   | 1 |  |
| 2+15 | 4.0736  | 30.20 | Q  |   |   | 1 |  |
| 2+20 | 4.2829  | 30.39 | Q  |   |   |   |  |
| 2+25 | 4.4936  | 30.59 | Q  |   |   |   |  |
| 2+30 | 4.7057  | 30.79 | Q  |   |   |   |  |
| 2+35 | 4.9190  | 30.97 | Q  |   |   | 1 |  |
| 2+40 | 5.1333  | 31.13 | Q  |   |   |   |  |
| 2+45 | 5.3488  | 31.29 | Q  |   |   |   |  |
| 2+50 | 5.5654  | 31.45 | Q  |   |   | 1 |  |
| 2+55 | 5.7831  | 31.61 | Q  |   |   | 1 |  |
| 3+ 0 | 6.0019  | 31.77 | Q  |   |   | 1 |  |
| 3+ 5 | 6.2219  | 31.94 | Q  |   |   |   |  |
| 3+10 | 6.4430  | 32.10 | Q  |   |   | 1 |  |
| 3+15 | 6.6652  | 32.27 | Q  |   |   |   |  |
| 3+20 | 6.8889  | 32.48 | QV |   |   |   |  |
| 3+25 | 7.1134  | 32.60 | QV |   |   |   |  |
| 3+30 | 7.3387  | 32.71 | QV |   |   |   |  |
| 3+35 | 7.5648  | 32.82 | QV |   |   |   |  |
| 3+40 | 7.7916  | 32.94 | QV |   |   |   |  |
| 3+45 | 8.0193  | 33.06 | QV |   |   |   |  |
| 3+50 | 8.2478  | 33.18 | QV |   |   |   |  |
| 3+55 | 8.4771  | 33.30 | QV |   |   |   |  |
| 4+ 0 | 8.7072  | 33.42 | QV |   |   |   |  |
| 4+ 5 | 8.9382  | 33.54 | QV | 1 |   |   |  |
| 4+10 | 9.1701  | 33.66 | QV | 1 |   |   |  |
| 4+15 | 9.4028  | 33.79 | QV |   |   |   |  |
| 4+20 | 9.6363  | 33.91 | QV |   |   |   |  |
| 4+25 | 9.8708  | 34.04 | QV |   |   |   |  |
| 4+30 | 10.1061 | 34.17 | QV |   | I |   |  |
|      |         |       |    |   |   |   |  |

|   | 4+35 | 10.3424 | 34.30 | Q V |   | 1 |  |
|---|------|---------|-------|-----|---|---|--|
| l | 4+40 | 10.5795 | 34.43 | Q V |   | 1 |  |
|   | 4+45 | 10.8175 | 34.57 | Q V |   | 1 |  |
|   | 4+50 | 11.0565 | 34.70 | Q V |   | 1 |  |
|   | 4+55 | 11.2964 | 34.84 | Q V |   | 1 |  |
|   | 5+ 0 | 11.5373 | 34.97 | Q V |   | 1 |  |
|   | 5+ 5 | 11.7791 | 35.11 | QV  |   | 1 |  |
|   | 5+10 | 12.0219 | 35.25 | QV  |   | 1 |  |
|   | 5+15 | 12.2657 | 35.40 | QV  |   | 1 |  |
|   | 5+20 | 12.5104 | 35.54 | QV  |   | 1 |  |
|   | 5+25 | 12.7562 | 35.69 | QV  | 1 | 1 |  |
| l | 5+30 | 13.0030 | 35.83 | QV  |   |   |  |
|   | 5+35 | 13.2508 | 35.98 | QV  | 1 | 1 |  |
| ı | 5+40 | 13.4996 | 36.13 | Q V |   | 1 |  |
| ı | 5+45 | 13.7495 | 36.28 | Q V | 1 | 1 |  |
| ı | 5+50 | 14.0005 | 36.44 | Q V | 1 | 1 |  |
| ı | 5+55 | 14.2525 | 36.60 | Q V |   | 1 |  |
| ı | 6+ 0 | 14.5056 | 36.75 | Q V | 1 | 1 |  |
| ı | 6+ 5 | 14.7598 | 36.91 | Q V | 1 | 1 |  |
| ı | 6+10 | 15.0152 | 37.07 | Q V | 1 | 1 |  |
| ı | 6+15 | 15.2716 | 37.24 | Q V | 1 | 1 |  |
| ı | 6+20 | 15.5292 | 37.40 | Q V | 1 | 1 |  |
| ı | 6+25 | 15.7880 | 37.57 | Q V | 1 | 1 |  |
| ı | 6+30 | 16.0479 | 37.74 | Q V | 1 | 1 |  |
| ı | 6+35 | 16.3090 | 37.92 | Q V | 1 | 1 |  |
| ı | 6+40 | 16.5714 | 38.09 | Q V |   | 1 |  |
| ı | 6+45 | 16.8349 | 38.27 | Q V | 1 | 1 |  |
| 1 | 6+50 | 17.0997 | 38.44 | Q V |   | 1 |  |
| 1 | 6+55 | 17.3657 | 38.63 | Q V |   | 1 |  |
| I | 7+ 0 | 17.6330 | 38.81 | Q V |   |   |  |
|   |      |         |       |     |   |   |  |

| 1      |      |         |       |   |   |   |   |
|--------|------|---------|-------|---|---|---|---|
|        | 7+ 5 | 17.9016 | 39.00 | Q | V |   |   |
|        | 7+10 | 18.1715 | 39.19 | Q | V |   |   |
| 1      | 7+15 | 18.4427 | 39.38 | Q | V |   |   |
| 1      | 7+20 | 18.7152 | 39.57 | Q | V |   |   |
|        | 7+25 | 18.9891 | 39.77 | Q | V |   |   |
| 1      | 7+30 | 19.2644 | 39.97 | Q | V |   | 1 |
|        | 7+35 | 19.5411 | 40.17 | Q | V |   | 1 |
| 1      | 7+40 | 19.8192 | 40.38 | Q | V |   |   |
| 1      | 7+45 | 20.0987 | 40.59 | Q | V |   | 1 |
| 1      | 7+50 | 20.3797 | 40.80 | Q | V |   |   |
| 1      | 7+55 | 20.6622 | 41.01 | Q | V |   | 1 |
|        | 8+ 0 | 20.9461 | 41.23 | Q | V |   |   |
| 1      | 8+ 5 | 21.2316 | 41.45 | Q | V |   | 1 |
| 1      | 8+10 | 21.5186 | 41.68 | Q | V |   |   |
| 1      | 8+15 | 21.8073 | 41.91 | Q | V |   | 1 |
| 1      | 8+20 | 22.0975 | 42.14 | Q | V |   |   |
| 1      | 8+25 | 22.3893 | 42.37 | Q | V |   |   |
| ı      | 8+30 | 22.6828 | 42.61 | Q | V |   | 1 |
| 1      | 8+35 | 22.9779 | 42.86 | Q | V |   |   |
| 1      | 8+40 | 23.2748 | 43.10 | Q | V |   | 1 |
| ı      | 8+45 | 23.5734 | 43.35 | Q | V |   | 1 |
| ı      | 8+50 | 23.8737 | 43.61 | Q | V |   | 1 |
| 1      | 8+55 | 24.1758 | 43.87 | Q | V |   |   |
| 1      | 9+ 0 | 24.4797 | 44.13 | Q | V |   |   |
| 1      | 9+ 5 | 24.7855 | 44.40 | Q | V |   |   |
| l<br>I | 9+10 | 25.0932 | 44.67 | Q | V |   |   |
| l<br>I | 9+15 | 25.4028 | 44.95 | Q | V |   |   |
| 1      | 9+20 | 25.7143 | 45.23 | Q | V |   |   |
| 1      | 9+25 | 26.0278 | 45.52 | Q | V | 1 |   |
| 1      | 9+30 | 26.3433 | 45.81 | Q | V |   |   |
|        |      |         |       |   |   |   |   |

|        | 9+35  | 26.6609 | 46.11 |   | Q | v | I | 1 |  |
|--------|-------|---------|-------|---|---|---|---|---|--|
|        | 9+40  | 26.9806 | 46.42 | 1 | Q | v |   | 1 |  |
|        | 9+45  | 27.3024 | 46.73 | 1 | Q | v |   | 1 |  |
|        | 9+50  | 27.6264 | 47.04 | 1 | Q | v |   | 1 |  |
|        | 9+55  | 27.9526 | 47.37 | - | Q | v |   | 1 |  |
|        | 10+ 0 | 28.2810 | 47.69 | 1 | Q | v |   | 1 |  |
|        | 10+ 5 | 28.6118 | 48.03 |   | Q | v |   | 1 |  |
|        | 10+10 | 28.9449 | 48.37 | 1 | Q | v |   | 1 |  |
|        | 10+15 | 29.2804 | 48.72 | 1 | Q | v |   | 1 |  |
|        | 10+20 | 29.6184 | 49.07 |   | Q | v |   | 1 |  |
|        | 10+25 | 29.9588 | 49.43 |   | Q | v |   | 1 |  |
|        | 10+30 | 30.3018 | 49.80 |   | Q | v |   | 1 |  |
|        | 10+35 | 30.6474 | 50.18 |   | Q | v |   | 1 |  |
|        | 10+40 | 30.9956 | 50.57 |   | Q | v |   | 1 |  |
|        | 10+45 | 31.3466 | 50.96 |   | Q | v |   | 1 |  |
|        | 10+50 | 31.7004 | 51.36 |   | Q | v |   | 1 |  |
|        | 10+55 | 32.0570 | 51.78 |   | Q | v |   | 1 |  |
|        | 11+ 0 | 32.4165 | 52.20 |   | Q | v |   | 1 |  |
|        | 11+ 5 | 32.7790 | 52.64 |   | Q | V |   | 1 |  |
|        | 11+10 | 33.1445 | 53.07 |   | Q | v |   | 1 |  |
| 1      | 11+15 | 33.5132 | 53.53 |   | Q | v |   | 1 |  |
| <br>   | 11+20 | 33.8850 | 53.99 |   | Q | V |   | 1 |  |
| 1      | 11+25 | 34.2602 | 54.47 |   | Q | V |   | 1 |  |
| 1      | 11+30 | 34.6386 | 54.95 |   | Q | V |   | 1 |  |
| 1      | 11+35 | 35.0206 | 55.46 |   | Q | V |   | 1 |  |
| 1      | 11+40 | 35.4060 | 55.97 |   | Q | V |   | 1 |  |
| 1      | 11+45 | 35.7952 | 56.50 |   | Q | V |   | 1 |  |
| l<br>I | 11+50 | 36.1880 | 57.04 |   | Q | V |   | 1 |  |
| <br>   | 11+55 | 36.5847 | 57.60 |   | Q | V |   | 1 |  |
| ı      | 12+ 0 | 36.9852 | 58.16 |   | Q | V |   | 1 |  |
|        |       |         |       |   |   |   |   |   |  |

|      | 12+ 5 | 37.3894 | 58.69 | Q | V   | 1 |
|------|-------|---------|-------|---|-----|---|
|      | 12+10 | 37.7963 | 59.08 | Q | V   | 1 |
|      | 12+15 | 38.2046 | 59.28 | Q | V   | 1 |
|      | 12+20 | 38.6109 | 59.00 | Q | V   | 1 |
|      | 12+25 | 39.0133 | 58.43 | Q | V   | 1 |
|      | 12+30 | 39.4152 | 58.36 | Q | V   | 1 |
|      | 12+35 | 39.8181 | 58.50 | Q | V   | 1 |
| 1    | 12+40 | 40.2232 | 58.81 | Q | V   | 1 |
| l    | 12+45 | 40.6313 | 59.25 | Q | V   |   |
|      | 12+50 | 41.0428 | 59.76 | Q | V   |   |
|      | 12+55 | 41.4585 | 60.35 | Q | V   | 1 |
| 1    | 13+ 0 | 41.8785 | 60.98 | Q | V   | 1 |
| 1    | 13+ 5 | 42.3033 | 61.69 | Q | V   | 1 |
| 1    | 13+10 | 42.7333 | 62.44 | Q | V   | 1 |
| 1    | 13+15 | 43.1689 | 63.25 | Q | V   |   |
| 1    | 13+20 | 43.6104 | 64.10 | Q | V   |   |
| 1    | 13+25 | 44.0582 | 65.02 | Q | l v |   |
| ı    | 13+30 | 44.5126 | 65.97 | Q | V   |   |
| ı    | 13+35 | 44.9740 | 67.00 | Q | V   |   |
| ı    | 13+40 | 45.4427 | 68.06 | Q | V   | 1 |
| ı    | 13+45 | 45.9192 | 69.19 | Q | V   | 1 |
| ı    | 13+50 | 46.4039 | 70.38 | Q | V   | 1 |
| ı    | 13+55 | 46.8975 | 71.66 | Q | V   | 1 |
| ı    | 14+ 0 | 47.4001 | 72.98 | Q | V   | 1 |
| ı    | 14+ 5 | 47.9132 | 74.51 | Q | V   | 1 |
| <br> | 14+10 | 48.4385 | 76.27 | Q | V   | 1 |
| ı    | 14+15 | 48.9786 | 78.42 | Q | V   | 1 |
| <br> | 14+20 | 49.5383 | 81.27 | Q | V   | 1 |
| <br> | 14+25 | 50.1214 | 84.67 | Q | V   | 1 |
| ı    | 14+30 | 50.7243 | 87.54 | Q | l v | 1 |
|      |       |         |       |   |     |   |

| ı     |         |        |   |   |   |          |     |   |
|-------|---------|--------|---|---|---|----------|-----|---|
| 14+35 | 51.3466 | 90.36  | Q | , | V |          |     |   |
| 14+40 | 51.9877 | 93.10  | Q | , | V |          |     |   |
| 14+45 | 52.6485 | 95.94  | Q |   | V |          |     |   |
| 14+50 | 53.3293 | 98.85  | Q |   | V |          |     |   |
| 14+55 | 54.0316 | 101.98 | Q |   | V |          |     |   |
| 15+ 0 | 54.7567 | 105.27 | Q |   | V |          |     |   |
| 15+ 5 | 55.5065 | 108.88 | Q |   | V |          |     |   |
| 15+10 | 56.2829 | 112.73 | Q |   | V |          |     |   |
| 15+15 | 57.0889 | 117.03 | Q |   | V |          |     |   |
| 15+20 | 57.9271 | 121.70 | Q |   | V |          |     |   |
| 15+25 | 58.8032 | 127.21 | Q |   | V |          |     |   |
| 15+30 | 59.7234 | 133.62 | Q |   | V |          |     |   |
| 15+35 | 60.6979 | 141.50 | Q |   | V |          |     |   |
| 15+40 | 61.7411 | 151.48 | Q |   | V |          |     |   |
| 15+45 | 62.8705 | 163.98 | Q |   | V |          |     |   |
| 15+50 | 64.0946 | 177.74 | Q |   | 7 | <i>7</i> |     |   |
| 15+55 | 65.4432 | 195.82 | 1 | Q | 7 | <i>7</i> |     |   |
| 16+ 0 | 66.9701 | 221.71 | 1 | Q | 7 | <i>7</i> |     |   |
| 16+ 5 | 68.8417 | 271.75 |   |   | Q | V        |     |   |
| 16+10 | 71.2117 | 344.12 |   |   | Ç | V   C    |     |   |
| 16+15 | 74.2250 | 437.54 |   |   |   | V        | Q   |   |
| 16+20 | 78.1054 | 563.43 | I |   |   | 7        | J   | Q |
| 16+25 | 82.3135 | 611.02 |   |   |   |          | V   | Q |
| 16+30 | 85.6317 | 481.80 | I |   |   |          | V Q |   |
| 16+35 | 88.4404 | 407.83 |   |   |   | (        | Q V |   |
| 16+40 | 90.8136 | 344.59 | I |   | Ç | 2        | V   |   |
| 16+45 | 92.8821 | 300.34 | 1 |   | Q | 1        | V   |   |
| 16+50 | 94.7257 | 267.69 | 1 |   | Q | 1        | V   |   |
| 16+55 | 96.3845 | 240.86 | I | Q |   | 1        | V   |   |
| 17+ 0 | 97.9075 | 221.14 | I | Q |   | 1        | V   |   |
|       |         |        |   |   |   |          |     |   |

| ı    |       |          |        |  |   |   |   |     |
|------|-------|----------|--------|--|---|---|---|-----|
| <br> | 17+ 5 | 99.3020  | 202.48 |  |   | Q | 1 | v   |
| <br> | 17+10 | 100.5794 | 185.48 |  |   | Q | 1 | v   |
| 1    | 17+15 | 101.7649 | 172.13 |  | ( | Q | 1 | V   |
| <br> | 17+20 | 102.8673 | 160.07 |  | ( | 2 |   | V   |
| 1    | 17+25 | 103.8909 | 148.63 |  | Q |   | 1 | V   |
| <br> | 17+30 | 104.8467 | 138.78 |  | Q |   | 1 | V   |
| 1    | 17+35 | 105.7486 | 130.96 |  | Q |   | 1 | V   |
| <br> | 17+40 | 106.5956 | 122.98 |  | Q |   | 1 | V   |
| <br> | 17+45 | 107.3982 | 116.54 |  | Q |   | 1 | V   |
| <br> | 17+50 | 108.1454 | 108.49 |  | Q |   | 1 | V   |
|      | 17+55 | 108.8523 | 102.65 |  | Q |   | 1 | V   |
| ı    | 18+ 0 | 109.5278 | 98.07  |  | Q |   | 1 | V   |
| ı    | 18+ 5 | 110.1629 | 92.23  |  | Q |   | 1 | V   |
|      | 18+10 | 110.7621 | 86.99  |  | Q |   | 1 | V   |
|      | 18+15 | 111.3429 | 84.34  |  | Q |   | 1 | V   |
|      | 18+20 | 111.9114 | 82.54  |  | Q |   | 1 | V   |
|      | 18+25 | 112.4702 | 81.14  |  | Q |   | 1 | V   |
|      | 18+30 | 113.0155 | 79.18  |  | Q |   | 1 | V   |
|      | 18+35 | 113.5392 | 76.05  |  | Q |   | 1 | V   |
|      | 18+40 | 114.0449 | 73.43  |  | Q |   | 1 | V   |
|      | 18+45 | 114.5390 | 71.74  |  | Q |   | 1 | l v |
|      | 18+50 | 115.0227 | 70.22  |  | Q |   | 1 | l v |
|      | 18+55 | 115.4961 | 68.74  |  | Q |   | 1 | l v |
|      | 19+ 0 | 115.9600 | 67.36  |  | Q |   | 1 | l v |
|      | 19+ 5 | 116.4142 | 65.95  |  | Q |   | 1 | l v |
|      | 19+10 | 116.8595 | 64.66  |  | Q |   | 1 | v   |
|      | 19+15 | 117.2945 | 63.16  |  | Q |   | 1 | v   |
|      | 19+20 | 117.7265 | 62.73  |  | Q |   | 1 | v   |
|      | 19+25 | 118.1147 | 56.36  |  | Q |   | 1 | l v |
|      | 19+30 | 118.4915 | 54.71  |  | Q |   | 1 | l v |
|      |       |          |        |  |   |   |   |     |

| 1 |       |          |       |   |   |   |   |
|---|-------|----------|-------|---|---|---|---|
| 1 | 19+35 | 118.8598 | 53.48 | Q |   | 1 | V |
|   | 19+40 | 119.2206 | 52.39 | Q |   |   | V |
|   | 19+45 | 119.5749 | 51.44 | Q | 1 | 1 | V |
|   | 19+50 | 119.9230 | 50.55 | Q | 1 | 1 | V |
|   | 19+55 | 120.2655 | 49.72 | Q |   |   | V |
| 1 | 20+ 0 | 120.6026 | 48.94 | Q |   | 1 | V |
| 1 | 20+ 5 | 120.9345 | 48.20 | Q |   |   | V |
| 1 | 20+10 | 121.2616 | 47.48 | Q | 1 | 1 | V |
| 1 | 20+15 | 121.5839 | 46.80 | Q | 1 | 1 | V |
| 1 | 20+20 | 121.9017 | 46.14 | Q | 1 | 1 | V |
| 1 | 20+25 | 122.2153 | 45.54 | Q |   | 1 | V |
| 1 | 20+30 | 122.5250 | 44.96 | Q |   | 1 | V |
| 1 | 20+35 | 122.8308 | 44.40 | Q |   | 1 | V |
| 1 | 20+40 | 123.1328 | 43.86 | Q | 1 | 1 | V |
| 1 | 20+45 | 123.4313 | 43.34 | Q |   | 1 | V |
| 1 | 20+50 | 123.7263 | 42.83 | Q |   | 1 | V |
| 1 | 20+55 | 124.0179 | 42.35 | Q |   | 1 | V |
| 1 | 21+ 0 | 124.3064 | 41.88 | Q |   | 1 | V |
| 1 | 21+ 5 | 124.5917 | 41.43 | Q |   | 1 | V |
| 1 | 21+10 | 124.8740 | 40.99 | Q |   | 1 | V |
| 1 | 21+15 | 125.1534 | 40.57 | Q |   | 1 | V |
| 1 | 21+20 | 125.4301 | 40.17 | Q |   | 1 | V |
| 1 | 21+25 | 125.7039 | 39.76 | Q |   | 1 | V |
| 1 | 21+30 | 125.9750 | 39.36 | Q |   | 1 | V |
| 1 | 21+35 | 126.2434 | 38.97 | Q |   | 1 | V |
| 1 | 21+40 | 126.5092 | 38.60 | Q |   | 1 | V |
| 1 | 21+45 | 126.7725 | 38.23 | Q |   | 1 | V |
| 1 | 21+50 | 127.0334 | 37.88 | Q |   | 1 | V |
| 1 | 21+55 | 127.2918 | 37.53 | Q |   | 1 | V |
| ı | 22+ 0 | 127.5480 | 37.19 | Q |   | 1 | V |
|   |       |          |       |   |   |   |   |

|         | 22+ 5 | 127.8019 | 36.86 | Q | 1 |   | V |
|---------|-------|----------|-------|---|---|---|---|
|         | 22+10 | 128.0535 | 36.54 | Q | 1 | 1 | V |
|         | 22+15 | 128.3030 | 36.23 | Q |   |   | V |
|         | 22+20 | 128.5504 | 35.92 | Q |   |   | V |
|         | 22+25 | 128.7958 | 35.63 | Q |   |   | V |
| 1       | 22+30 | 129.0391 | 35.33 | Q |   |   | V |
| 1       | 22+35 | 129.2805 | 35.05 | Q |   |   | V |
| 1       | 22+40 | 129.5200 | 34.77 | Q |   |   | V |
| 1       | 22+45 | 129.7576 | 34.50 | Q |   |   | V |
| 1       | 22+50 | 129.9934 | 34.23 | Q |   |   | V |
| 1       | 22+55 | 130.2274 | 33.97 | Q |   |   | V |
| 1       | 23+ 0 | 130.4596 | 33.72 | Q |   |   | V |
| 1       | 23+ 5 | 130.6901 | 33.47 | Q |   |   | V |
| 1       | 23+10 | 130.9190 | 33.23 | Q |   |   | V |
| 1       | 23+15 | 131.1462 | 32.99 | Q |   |   | V |
| 1       | 23+20 | 131.3718 | 32.75 | Q |   |   | V |
| ν       | 23+25 | 131.5958 | 32.53 | Q |   |   |   |
|         | 23+30 | 131.8182 | 32.30 | Q |   |   |   |
| V       | 23+35 | 132.0392 | 32.08 | Q |   |   |   |
| V       | 23+40 | 132.2586 | 31.86 | Q | 1 |   |   |
| V       | 23+45 | 132.4766 | 31.65 | Q |   |   |   |
| V       | 23+50 | 132.6931 | 31.44 | Q |   |   |   |
| V       | 23+55 | 132.9083 | 31.24 | Q |   |   |   |
| V       | 24+ 0 | 133.1220 | 31.04 | Q |   |   |   |
| v <br>v | 24+ 5 | 133.3323 | 30.52 | Q |   |   |   |
|         | 24+10 | 133.5349 | 29.42 | Q |   |   |   |
| V       | 24+15 | 133.7236 | 27.41 | Q |   |   |   |
| V       | 24+20 | 133.8838 | 23.25 | Q |   |   |   |
| V       | 24+25 | 134.0059 | 17.74 | Q | 1 |   |   |
| V       | 24+30 | 134.1052 | 14.41 | Q |   |   |   |
|         |       |          |       |   |   |   |   |

| V        |       |          |       |   |   |   |
|----------|-------|----------|-------|---|---|---|
| v  <br>V | 24+35 | 134.1871 | 11.90 | Q | 1 |   |
|          | 24+40 | 134.2567 | 10.10 | Q | 1 |   |
| V        | 24+45 | 134.3166 | 8.70  | Q | 1 |   |
| V        | 24+50 | 134.3686 | 7.55  | Q | 1 | 1 |
| V        | 24+55 | 134.4141 | 6.61  | Q | 1 | 1 |
| V        | 25+ 0 | 134.4540 | 5.79  | Q | 1 | 1 |
| V        | 25+ 5 | 134.4890 | 5.09  | Q | 1 |   |
| V        | 25+10 | 134.5201 | 4.51  | Q | 1 | 1 |
| V        | 25+15 | 134.5477 | 4.01  | Q | 1 | 1 |
| V        | 25+20 | 134.5722 | 3.56  | Q | 1 | 1 |
| V        | 25+25 | 134.5939 | 3.16  | Q | 1 |   |
| V        | 25+30 | 134.6133 | 2.81  | Q | 1 |   |
| V        | 25+35 | 134.6304 | 2.48  | Q | 1 | 1 |
| V        | 25+40 | 134.6455 | 2.19  | Q | 1 | 1 |
| V        | 25+45 | 134.6587 | 1.92  | Q | 1 | 1 |
| V        | 25+50 | 134.6704 | 1.70  | Q | 1 | 1 |
| V        | 25+55 | 134.6809 | 1.52  | Q | 1 | 1 |
| V        | 26+ 0 | 134.6900 | 1.33  | Q | 1 | 1 |
| V        | 26+ 5 | 134.6981 | 1.18  | Q | 1 | 1 |
| V        | 26+10 | 134.7055 | 1.07  | Q | 1 | [ |
| V        | 26+15 | 134.7122 | 0.97  | Q | 1 | [ |
| v <br>v  | 26+20 | 134.7181 | 0.86  | Q | 1 | [ |
| v  <br>V | 26+25 | 134.7233 | 0.75  | Q | 1 |   |
| v  <br>V | 26+30 | 134.7278 | 0.65  | Q | 1 |   |
|          | 26+35 | 134.7317 | 0.57  | Q | 1 |   |
| V        | 26+40 | 134.7352 | 0.51  | Q | 1 |   |
| V        | 26+45 | 134.7383 | 0.45  | Q | 1 | 1 |
| V        | 26+50 | 134.7410 | 0.39  | Q |   | [ |
| V        | 26+55 | 134.7433 | 0.33  | Q |   | I |
| V        | 27+ 0 | 134.7452 | 0.27  | Q |   | [ |
|          |       |          |       |   |   |   |

| ٧l      |       |          |      |   |   |   |   |
|---------|-------|----------|------|---|---|---|---|
| 1       | 27+ 5 | 134.7467 | 0.21 | Q |   |   |   |
| v <br>v | 27+10 | 134.7477 | 0.16 | Q | 1 |   | 1 |
| V       | 27+15 | 134.7484 | 0.10 | Q | I | 1 |   |
|         |       |          |      |   |   |   |   |

# Appendix B Kern County Curve Number Table

Residential Landscaping (Lawn, Shrubs, etc.) - The pervious portions of commercial establishments, single and multiple family dwellings, trailer parks and schools where the predominant land cover is lawn, shrubbery and trees.

Row Crops - Lettuce, tomatoes, beets, tulips or any field crop planted in rows far enough apart that most of the soil surface is exposed to rainfall impact throughout the growing season. At plowing, planting and harvest times it is equivalent to fallow.

<u>Small Grain</u> - Wheat, oats, barley, flax, etc. planted in rows close enough that the soil surface is not exposed except during planting and shortly thereafter.

<u>Legumes</u> - Alfalfa, sweetclover, timothy, etc. and combinations are either planted in close rows or broadcast.

Fallow - Fallow land is land plowed but not yet seeded or tilled.

Woodland - grass - Areas with an open cover of broadleaf or coniferous trees usually live oak and pines, with the intervening ground space occupied by annual grasses or weeds. The trees may occur singly or in small clumps. Canopy density, the amount of ground surface shaded at high noon, is from 20 to 50 percent.

<u>Woodland</u> - Areas on which coniferous or broadleaf trees predominate. The canopy density is at least 50 percent. Open areas may have a cover of annual or perennial grasses or of brush. Herbaceous plant cover under the trees is usually sparse because of leaf or needle litter accumulation.

<u>Chaparral</u> - Land on which the principal vegetation consists of evergreen shrubs with broad, hard, stiff leaves such as manzonita, ceanothus and scrub oak. The brush cover is usually dense or moderately dense. Diffusely branched evergreen shrubs with fine needle-like leaves, such as chamise and redchank, with dense high growth are also included in this soil cover.

Annual Grass - Land on which the principal vegetation consists of annual grasses and weeds such as annual bromes, wild barley, soft chess, ryegrass and filaree.

<u>Irrigated Pasture</u> - Irrigated land planted to perennial grasses and legumes for production of forage and which is cultivated only to establish or renew the stand of plants. Dry land pasture is considered as annual grass.

Meadow - Land areas with seasonally high water table, locally called cienegas. Principal vegetation consists of sod-forming grasses interspersed with other plants.

Orchard (Deciduous) - Land planted to such deciduous trees as apples, apricots, pears, walnuts, and almonds.

Orchard (Evergreen) - Land planted to evergreen trees which include citrus and avocados and coniferous plantings.

Turf - Golf courses, parks and similar lands where the predominant cover is irrigated mowed close-grown turf grass. Parks in which trees are dense may be classified as woodland.

# KERN COUNTY

HYDROLOGY MANUAL

S C S COVER TYPE DESCRIPTIONS

(A 40/E)

|   | 12                   |                  |                |                |                |
|---|----------------------|------------------|----------------|----------------|----------------|
| Curve (1) Numbers of Hydrologic Soil-Cover Complex  | es For Pervic        | us Ar            | eas-A          | MC I           | Ī              |
|   | Quality of           |                  |                | l Gro          | up             |
| Cover Type (3)  | Cover (2)            | A                | В              | С              | D              |
| NATURAL COVERS -  |                      |                  |                |                |                |
| Barren<br>(Rockland, eroded and graded land)  |                      | 77               | 86             | 91             | 94             |
| Chaparral, Broadleaf<br>(Manzonita, ceanothus and scrub oak)  | Poor<br>Fair<br>Good | 53<br>40<br>31   | 70<br>63<br>57 | 80<br>75<br>71 | 85<br>81<br>78 |
| Chaparral, Narrowleaf<br>(Chamise and Redskank)   | Poor<br>Fair         | 7 <b>1</b><br>55 | 82<br>72       | 88<br>81       | 91<br>86       |
| Grass, Annual or Perennial  | Poor<br>Fair<br>Good | 68<br>49<br>39   | 79<br>69<br>61 | 86<br>79<br>74 | 89<br>84<br>80 |
| Meadows or Cienagas (Areas with seasonally high water table, principal vegatation is sod forming grass) | Poor<br>Fair<br>Good | 63<br>51<br>30   | 77<br>70<br>58 | 85<br>80<br>71 | 88<br>84<br>78 |
| Open Brush (Soft wood shrubs-buckwheat, sage, etc.)   | Poor<br>Fair<br>Good | 62<br>46<br>41   | 76<br>66<br>63 | 84<br>77<br>75 | 88<br>83<br>81 |
| Woodland (4)  (Coniferous or broadleaf trees  predominate. Canopy density is at  least 50 percent)      | Poor<br>Fair<br>Good | 45<br>36<br>30   | 66<br>60<br>55 | 77<br>73<br>70 | 83<br>79<br>77 |
| Woodland, Grass (Coniferous or broadleaf trees with canopy density from 20 to 50 percent)               | Poor<br>Fair<br>Good | 57<br>43<br>32   | 73<br>65<br>58 | 82<br>76<br>72 | 86<br>82<br>79 |
| URBAN COVERS -  |                      |                  |                |                |                |
| Residential or Commercial Landscaping (Lawns, shrubs, etc.)   | Good                 | 39               | 61             | 74             | 80             |
| Turf<br>(Irrigated and mowed grass)   | Poor<br>Fair<br>Good | 68<br>49<br>39   | 79<br>69<br>61 | 86<br>79<br>74 | 89<br>84<br>80 |

KERN COUNTY Hydrology Manual CURVE NUMBERS
FOR
PERVIOUS AREAS

Curve (1) Numbers of Hydrologic Soil-Cover Complexes For Pervious Areas-AMC II

|  | Quality of           |                | Soi            | L Gro          | up             |
|--|----------------------|----------------|----------------|----------------|----------------|
| Cover Type (3)   | Cover (2)            | A              | В              | С              | D              |
| AGRICULTURAL COVERS -                                      |                      |                |                |                |                |
| Fallow<br>(Bare Soil)                                      |                      | 77             | 86             | 91             | 94             |
| Close Seeded (alfalfa, sweetclover, timothy, etc.)         | Poor<br>Good         | 66<br>58       | 77<br>72       | 85<br>81       | 89<br>85       |
| Orchards, Evergreen<br>(Citrus, avacodos, etc.)            | Poor<br>Fair<br>Good | 57<br>43<br>32 | 73<br>65<br>58 | 82<br>76<br>72 | 86<br>82<br>79 |
| Pasture (Grassland or range, continuos forage for grazing) | Poor<br>Fair<br>Good | 68<br>49<br>39 | 79<br>69<br>61 | 86<br>79<br>74 | 89<br>84<br>80 |
| Row Crops<br>(Straight row, non-contoured)                 | Poor<br>Good         | 72<br>67       | 81<br>78       | 88<br>85       | 91<br>89       |
| Small Grain<br>(Straight row, non-contoured)               | Poor<br>Good         | 65<br>63       | 76<br>75       | 84<br>83       | 88<br>87       |

#### Notes:

1. Average runoff condition, Ia = 0.2(S)

2. Poor: Heavily grazed, regularly burned areas, or areas of high burn potential. Less than 50 percent of the ground surface is

protected by plant cover or brush and tree canopy.

Fair: Moderate cover with 50 percent to 75 percent of the ground surface protected. In wooded areas the woods are grazed but not

burned, and some forest litter covers the soil.

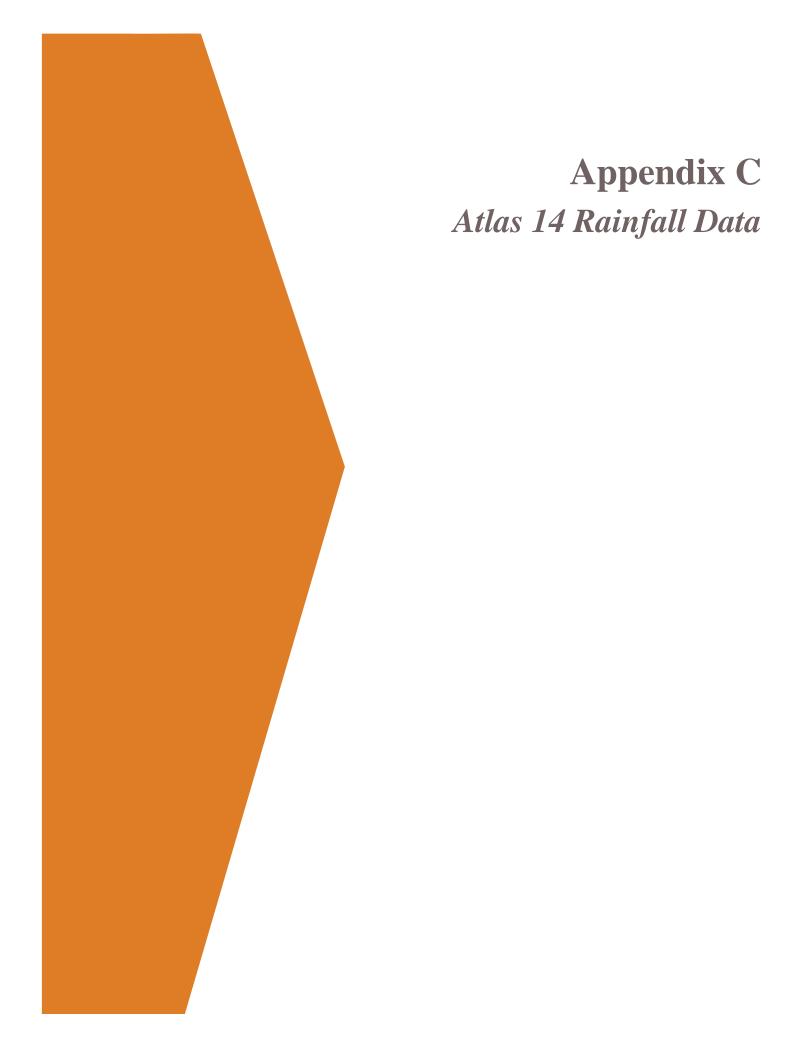
Good: Heavy or dense cover with more than 75 percent of the ground

surface protected. In wooded areas the woods are protected from

grazing, litter and brush adequately cover soil.

3. See Figure C-1 for definition of cover types.

KERN COUNTY Hydrology Manual CURVE NUMBERS
FOR
PERVIOUS AREAS





#### NOAA Atlas 14, Volume 6, Version 2 Location name: Mojave, California, USA\* Latitude: 35.2017°, Longitude: -118.0103° Elevation: 2317.59 ft\*\*

\* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

| PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup> |                                     |                               |                               |                               |                               |                               |                               |                               |                               |                            |
|--|-------------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|----------------------------|
| Duration   | Average recurrence interval (years) |                               |                               |                               |                               |                               |                               |                               |                               |                            |
|  | 1                                   | 2                             | 5                             | 10                            | 25                            | 50                            | 100                           | 200                           | 500                           | 1000                       |
| 5-min  | <b>0.071</b> (0.058-0.088)          | <b>0.096</b> (0.079-0.119)    | <b>0.131</b> (0.107-0.163)    | <b>0.162</b> (0.131-0.203)    | <b>0.209</b><br>(0.164-0.269) | <b>0.247</b><br>(0.190-0.325) | <b>0.290</b><br>(0.218-0.391) | <b>0.338</b><br>(0.247-0.467) | <b>0.409</b><br>(0.287-0.589) | <b>0.472</b> (0.320-0.703) |
| 10-min   | <b>0.102</b><br>(0.084-0.126)       | <b>0.138</b> (0.113-0.170)    | <b>0.188</b> (0.154-0.233)    | <b>0.233</b> (0.188-0.290)    | <b>0.299</b><br>(0.234-0.385) | <b>0.355</b><br>(0.273-0.466) | <b>0.416</b> (0.312-0.560)    | <b>0.484</b> (0.354-0.669)    | <b>0.587</b><br>(0.412-0.844) | <b>0.677</b> (0.459-1.01)  |
| 15-min   | <b>0.124</b> (0.101-0.153)          | <b>0.166</b><br>(0.136-0.206) | <b>0.228</b> (0.186-0.282)    | <b>0.282</b> (0.228-0.351)    | <b>0.362</b> (0.283-0.466)    | <b>0.429</b><br>(0.330-0.564) | <b>0.503</b><br>(0.377-0.677) | <b>0.585</b> (0.428-0.810)    | <b>0.709</b> (0.498-1.02)     | <b>0.818</b> (0.555-1.22)  |
| 30-min   | <b>0.170</b> (0.139-0.210)          | <b>0.229</b> (0.187-0.282)    | <b>0.313</b> (0.255-0.387)    | <b>0.387</b> (0.313-0.483)    | <b>0.497</b><br>(0.390-0.640) | <b>0.589</b> (0.453-0.775)    | <b>0.691</b> (0.519-0.930)    | <b>0.804</b> (0.588-1.11)     | <b>0.975</b> (0.684-1.40)     | <b>1.13</b> (0.763-1.67)   |
| 60-min   | <b>0.236</b> (0.194-0.291)          | <b>0.318</b> (0.260-0.392)    | <b>0.435</b> (0.355-0.538)    | <b>0.537</b> (0.435-0.670)    | <b>0.690</b> (0.541-0.889)    | <b>0.819</b> (0.629-1.08)     | <b>0.960</b> (0.720-1.29)     | <b>1.12</b> (0.816-1.55)      | <b>1.35</b> (0.950-1.95)      | <b>1.56</b> (1.06-2.32)    |
| 2-hr   | <b>0.350</b> (0.286-0.431)          | <b>0.460</b><br>(0.376-0.568) | <b>0.615</b> (0.502-0.761)    | <b>0.749</b><br>(0.606-0.934) | <b>0.944</b> (0.740-1.22)     | <b>1.10</b> (0.848-1.45)      | <b>1.28</b> (0.958-1.72)      | <b>1.46</b> (1.07-2.02)       | <b>1.73</b> (1.22-2.50)       | <b>1.96</b> (1.33-2.92)    |
| 3-hr   | <b>0.428</b><br>(0.350-0.527)       | <b>0.560</b><br>(0.458-0.692) | <b>0.745</b><br>(0.608-0.922) | <b>0.903</b> (0.731-1.13)     | <b>1.13</b> (0.887-1.46)      | <b>1.32</b> (1.01-1.73)       | <b>1.52</b> (1.14-2.04)       | <b>1.73</b> (1.26-2.39)       | <b>2.03</b> (1.43-2.93)       | <b>2.28</b> (1.55-3.40)    |
| 6-hr   | <b>0.571</b> (0.467-0.704)          | <b>0.752</b> (0.615-0.929)    | <b>1.00</b> (0.816-1.24)      | <b>1.21</b> (0.981-1.51)      | <b>1.51</b> (1.18-1.95)       | <b>1.75</b> (1.35-2.30)       | <b>2.00</b> (1.50-2.70)       | <b>2.27</b> (1.66-3.14)       | <b>2.65</b> (1.86-3.82)       | <b>2.96</b> (2.01-4.40)    |
| 12-hr  | <b>0.706</b> (0.578-0.870)          | <b>0.964</b> (0.789-1.19)     | <b>1.31</b> (1.07-1.63)       | <b>1.61</b> (1.30-2.00)       | <b>2.01</b> (1.58-2.59)       | <b>2.34</b> (1.79-3.07)       | <b>2.67</b> (2.00-3.59)       | <b>3.02</b> (2.21-4.18)       | <b>3.51</b> (2.46-5.05)       | <b>3.90</b> (2.65-5.80)    |
| 24-hr  | <b>0.895</b> (0.795-1.03)           | <b>1.27</b> (1.13-1.46)       | <b>1.78</b> (1.57-2.05)       | <b>2.20</b> (1.93-2.56)       | <b>2.78</b> (2.36-3.35)       | <b>3.24</b> (2.69-3.98)       | <b>3.71</b> (3.00-4.67)       | <b>4.20</b> (3.31-5.45)       | <b>4.89</b> (3.69-6.61)       | <b>5.42</b> (3.95-7.60)    |
| 2-day  | <b>1.06</b> (0.938-1.21)            | <b>1.51</b> (1.34-1.74)       | <b>2.14</b> (1.89-2.47)       | <b>2.66</b> (2.33-3.09)       | <b>3.38</b> (2.87-4.07)       | <b>3.96</b> (3.28-4.86)       | <b>4.55</b> (3.69-5.74)       | <b>5.18</b> (4.08-6.72)       | <b>6.06</b> (4.57-8.20)       | <b>6.75</b> (4.92-9.46)    |
| 3-day  | <b>1.15</b> (1.02-1.32)             | <b>1.65</b> (1.46-1.90)       | <b>2.34</b> (2.07-2.69)       | <b>2.91</b> (2.55-3.39)       | <b>3.72</b> (3.15-4.47)       | <b>4.36</b> (3.62-5.35)       | <b>5.02</b> (4.07-6.33)       | <b>5.73</b> (4.51-7.43)       | <b>6.72</b> (5.07-9.09)       | <b>7.52</b> (5.48-10.5)    |
| 4-day  | <b>1.22</b> (1.08-1.40)             | <b>1.75</b> (1.55-2.01)       | <b>2.48</b> (2.19-2.86)       | <b>3.09</b> (2.71-3.60)       | <b>3.95</b> (3.35-4.75)       | <b>4.63</b> (3.84-5.69)       | <b>5.34</b> (4.32-6.73)       | <b>6.09</b> (4.79-7.90)       | <b>7.14</b> (5.39-9.66)       | <b>7.98</b> (5.81-11.2)    |
| 7-day  | <b>1.34</b> (1.19-1.54)             | <b>1.92</b> (1.70-2.21)       | <b>2.72</b> (2.40-3.14)       | <b>3.38</b> (2.97-3.93)       | <b>4.31</b> (3.65-5.18)       | <b>5.03</b> (4.18-6.19)       | <b>5.78</b> (4.68-7.28)       | <b>6.56</b> (5.16-8.51)       | <b>7.64</b> (5.76-10.3)       | <b>8.48</b> (6.18-11.9)    |
| 10-day   | <b>1.39</b> (1.23-1.59)             | <b>1.99</b> (1.77-2.29)       | <b>2.82</b> (2.50-3.26)       | <b>3.51</b> (3.08-4.09)       | <b>4.47</b> (3.79-5.38)       | <b>5.22</b> (4.33-6.42)       | <b>5.99</b> (4.85-7.55)       | <b>6.79</b> (5.34-8.80)       | <b>7.89</b> (5.95-10.7)       | <b>8.74</b> (6.36-12.2)    |
| 20-day   | <b>1.61</b> (1.43-1.84)             | <b>2.34</b> (2.07-2.69)       | <b>3.34</b> (2.96-3.86)       | <b>4.19</b> (3.67-4.87)       | <b>5.38</b> (4.56-6.47)       | <b>6.31</b> (5.24-7.76)       | <b>7.27</b> (5.89-9.16)       | <b>8.27</b> (6.50-10.7)       | <b>9.61</b> (7.25-13.0)       | <b>10.7</b> (7.76-14.9)    |
| 30-day   | <b>1.81</b> (1.61-2.08)             | <b>2.65</b> (2.35-3.05)       | <b>3.82</b> (3.38-4.41)       | <b>4.81</b> (4.22-5.60)       | <b>6.23</b> (5.28-7.50)       | <b>7.35</b> (6.10-9.03)       | <b>8.49</b> (6.88-10.7)       | <b>9.69</b> (7.63-12.6)       | <b>11.3</b> (8.54-15.3)       | <b>12.6</b> (9.15-17.6)    |
| 45-day   | <b>2.10</b> (1.87-2.42)             | <b>3.09</b> (2.74-3.56)       | <b>4.49</b> (3.97-5.18)       | <b>5.69</b> (4.99-6.62)       | <b>7.42</b> (6.29-8.93)       | <b>8.82</b> (7.32-10.8)       | <b>10.3</b> (8.30-12.9)       | <b>11.8</b> (9.25-15.2)       | <b>13.8</b> (10.4-18.7)       | <b>15.4</b> (11.2-21.6)    |
| 60-day   | <b>2.32</b> (2.06-2.66)             | <b>3.41</b> (3.02-3.92)       | <b>4.97</b> (4.39-5.73)       | <b>6.33</b> (5.55-7.36)       | <b>8.29</b> (7.03-9.98)       | 9.89<br>(8.21-12.2)           | <b>11.6</b> (9.36-14.6)       | <b>13.3</b> (10.5-17.2)       | <b>15.7</b> (11.8-21.2)       | <b>17.5</b> (12.8-24.6)    |

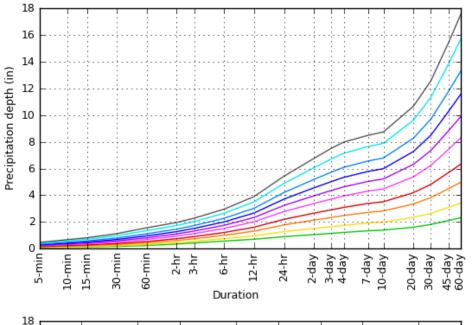
<sup>&</sup>lt;sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

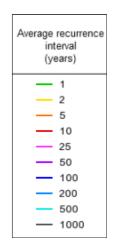
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

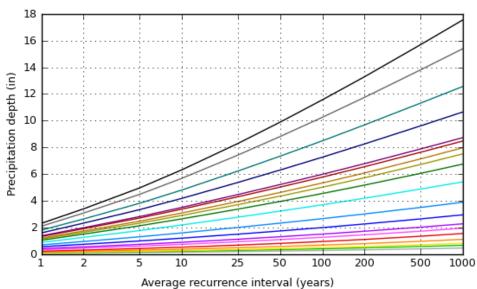
Please refer to NOAA Atlas 14 document for more information.

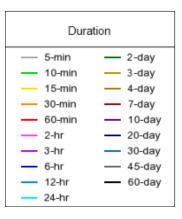
### PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 35.2017°, Longitude: -118.0103°









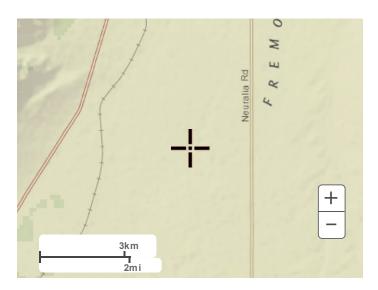
NOAA Atlas 14, Volume 6, Version 2

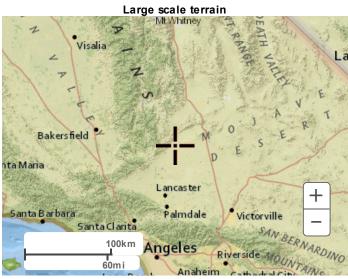
Created (GMT): Fri Mar 22 20:44:18 2019

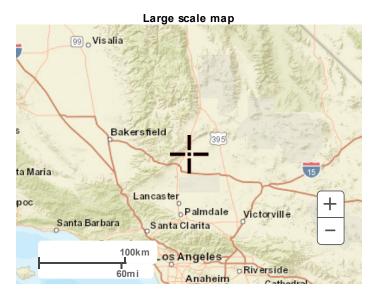
Back to Top

Maps & aerials

Small scale terrain







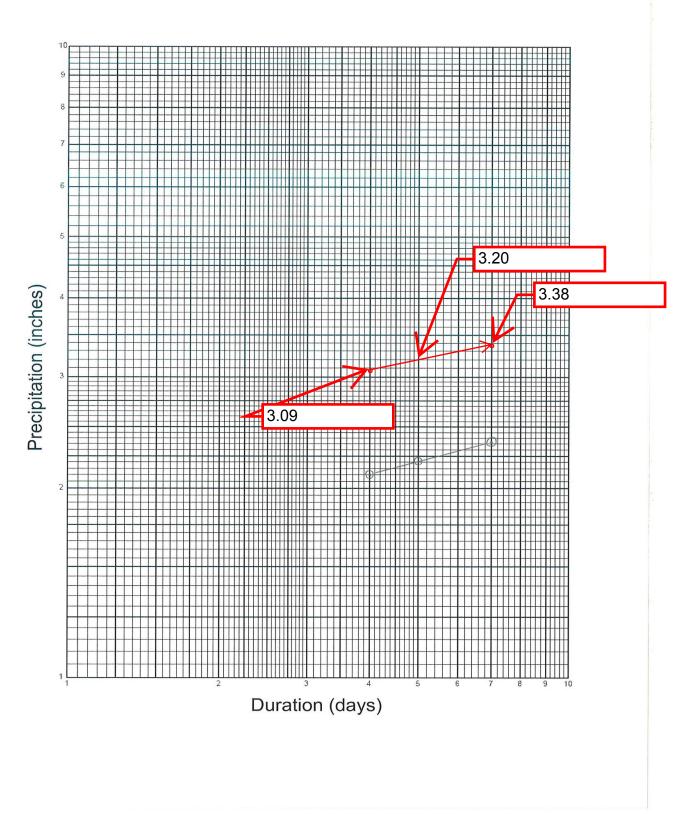
Large scale aerial



Back to Top

US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

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# Appendix D Kern County Hydrology Manual Excerpts

Residential Landscaping (Lawn, Shrubs, etc.) - The pervious portions of commercial establishments, single and multiple family dwellings, trailer parks and schools where the predominant land cover is lawn, shrubbery and trees.

Row Crops - Lettuce, tomatoes, beets, tulips or any field crop planted in rows far enough apart that most of the soil surface is exposed to rainfall impact throughout the growing season. At plowing, planting and harvest times it is equivalent to fallow.

<u>Small Grain</u> - Wheat, oats, barley, flax, etc. planted in rows close enough that the soil surface is not exposed except during planting and shortly thereafter.

<u>Legumes</u> - Alfalfa, sweetclover, timothy, etc. and combinations are either planted in close rows or broadcast.

Fallow - Fallow land is land plowed but not yet seeded or tilled.

Woodland - grass - Areas with an open cover of broadleaf or coniferous trees usually live oak and pines, with the intervening ground space occupied by annual grasses or weeds. The trees may occur singly or in small clumps. Canopy density, the amount of ground surface shaded at high noon, is from 20 to 50 percent.

<u>Woodland</u> - Areas on which coniferous or broadleaf trees predominate. The canopy density is at least 50 percent. Open areas may have a cover of annual or perennial grasses or of brush. Herbaceous plant cover under the trees is usually sparse because of leaf or needle litter accumulation.

<u>Chaparral</u> - Land on which the principal vegetation consists of evergreen shrubs with broad, hard, stiff leaves such as manzonita, ceanothus and scrub oak. The brush cover is usually dense or moderately dense. Diffusely branched evergreen shrubs with fine needle-like leaves, such as chamise and redchank, with dense high growth are also included in this soil cover.

Annual Grass - Land on which the principal vegetation consists of annual grasses and weeds such as annual bromes, wild barley, soft chess, ryegrass and filaree.

<u>Irrigated Pasture</u> - Irrigated land planted to perennial grasses and legumes for production of forage and which is cultivated only to establish or renew the stand of plants. Dry land pasture is considered as annual grass.

Meadow - Land areas with seasonally high water table, locally called cienegas. Principal vegetation consists of sod-forming grasses interspersed with other plants.

Orchard (Deciduous) - Land planted to such deciduous trees as apples, apricots, pears, walnuts, and almonds.

Orchard (Evergreen) - Land planted to evergreen trees which include citrus and avocados and coniferous plantings.

Turf - Golf courses, parks and similar lands where the predominant cover is irrigated mowed close-grown turf grass. Parks in which trees are dense may be classified as woodland.

# KERN COUNTY

HYDROLOGY MANUAL

S C S COVER TYPE DESCRIPTIONS

(A 40/E)

|   | 12                   |                  |                |                |                |
|---|----------------------|------------------|----------------|----------------|----------------|
| Curve (1) Numbers of Hydrologic Soil-Cover Complex  | es For Pervic        | us Ar            | eas-A          | MC I           | Ξ              |
|   | Quality of           |                  |                | l Gro          | up             |
| Cover Type (3)  | Cover (2)            | A                | В              | С              | D              |
| NATURAL COVERS -  |                      |                  |                |                |                |
| Barren<br>(Rockland, eroded and graded land)  |                      | 77               | 86             | 91             | 94             |
| Chaparral, Broadleaf<br>(Manzonita, ceanothus and scrub oak)  | Poor<br>Fair<br>Good | 53<br>40<br>31   | 70<br>63<br>57 | 80<br>75<br>71 | 85<br>81<br>78 |
| Chaparral, Narrowleaf<br>(Chamise and Redskank)   | Poor<br>Fair         | 7 <b>1</b><br>55 | 82<br>72       | 88<br>81       | 91<br>86       |
| Grass, Annual or Perennial  | Poor<br>Fair<br>Good | 68<br>49<br>39   | 79<br>69<br>61 | 86<br>79<br>74 | 89<br>84<br>80 |
| Meadows or Cienagas (Areas with seasonally high water table, principal vegatation is sod forming grass) | Poor<br>Fair<br>Good | 63<br>51<br>30   | 77<br>70<br>58 | 85<br>80<br>71 | 88<br>84<br>78 |
| Open Brush (Soft wood shrubs-buckwheat, sage, etc.)   | Poor<br>Fair<br>Good | 62<br>46<br>41   | 76<br>66<br>63 | 84<br>77<br>75 | 88<br>83<br>81 |
| Woodland (4)  (Coniferous or broadleaf trees  predominate. Canopy density is at least 50 percent)       | Poor<br>Fair<br>Good | 45<br>36<br>30   | 66<br>60<br>55 | 77<br>73<br>70 | 83<br>79<br>77 |
| Woodland, Grass (Coniferous or broadleaf trees with canopy density from 20 to 50 percent)               | Poor<br>Fair<br>Good | 57<br>43<br>32   | 73<br>65<br>58 | 82<br>76<br>72 | 86<br>82<br>79 |
| URBAN COVERS -  |                      |                  |                |                |                |
| Residential or Commercial Landscaping (Lawns, shrubs, etc.)   | Good                 | 39               | 61             | 74             | 80             |
| Turf<br>(Irrigated and mowed grass)   | Poor<br>Fair<br>Good | 68<br>49<br>39   | 79<br>69<br>61 | 86<br>79<br>74 | 89<br>84<br>80 |

KERN COUNTY Hydrology Manual CURVE NUMBERS
FOR
PERVIOUS AREAS

Curve (1) Numbers of Hydrologic Soil-Cover Complexes For Pervious Areas-AMC II

|  | Quality of           | Soil Group     |                | up             |                |
|--|----------------------|----------------|----------------|----------------|----------------|
| Cover Type (3)   | Cover (2)            | A              | В              | С              | D              |
| AGRICULTURAL COVERS -                                      |                      |                |                |                |                |
| Fallow<br>(Bare Soil)                                      |                      | 77             | 86             | 91             | 94             |
| Close Seeded (alfalfa, sweetclover, timothy, etc.)         | Poor<br>Good         | 66<br>58       | 77<br>72       | 85<br>81       | 89<br>85       |
| Orchards, Evergreen<br>(Citrus, avacodos, etc.)            | Poor<br>Fair<br>Good | 57<br>43<br>32 | 73<br>65<br>58 | 82<br>76<br>72 | 86<br>82<br>79 |
| Pasture (Grassland or range, continuos forage for grazing) | Poor<br>Fair<br>Good | 68<br>49<br>39 | 79<br>69<br>61 | 86<br>79<br>74 | 89<br>84<br>80 |
| Row Crops<br>(Straight row, non-contoured)                 | Poor<br>Good         | 72<br>67       | 81<br>78       | 88<br>85       | 91<br>89       |
| Small Grain<br>(Straight row, non-contoured)               | Poor<br>Good         | 65<br>63       | 76<br>75       | 84<br>83       | 88<br>87       |

#### Notes:

1. Average runoff condition, Ia = 0.2(S)

2. Poor: Heavily grazed, regularly burned areas, or areas of high burn potential. Less than 50 percent of the ground surface is

protected by plant cover or brush and tree canopy.

Fair: Moderate cover with 50 percent to 75 percent of the ground surface protected. In wooded areas the woods are grazed but not

burned, and some forest litter covers the soil.

Good: Heavy or dense cover with more than 75 percent of the ground

surface protected. In wooded areas the woods are protected from

grazing, litter and brush adequately cover soil.

3. See Figure C-1 for definition of cover types.

KERN COUNTY Hydrology Manual CURVE NUMBERS
FOR
PERVIOUS AREAS

| ACTUAL  | IMPERVIOUS COVER   | - ac   |
|---|--|--|
| Land Use  | Range-Percent  | Recommended Value<br>For Average<br>Conditions-Percent (1) |
| Natural or Agriculture  | 0 - 0  | 0  |
| Public Park   | 10 - 25  | 15   |
| School  | 30 - 50  | 40   |
| Single Family Residential: (2)  |  |  |
| 2.5 acre lots 1 acre lots 2-3 DU/acre 3-5 DU/acre 5-8 DU/acre 4-8 8-10 DU/acre MH More than 10 DU/acre Multiple Family Residential: | 5 - 15<br>10 - 25<br>20 - 40<br>30 - 50<br>35 - 55<br>50 - 70<br>65 - 90 | 10<br>20<br>30<br>21<br>40<br>50<br>22-23 60<br>80         |
| Condominiums<br>Apartments  | 45 - 70<br>65 - 90   | 65<br>80   |
| Mobile Home Parks  Commercial, Downtown  Business or Industrial   | 60 - 85<br>80 - 100  | 75<br>90   |

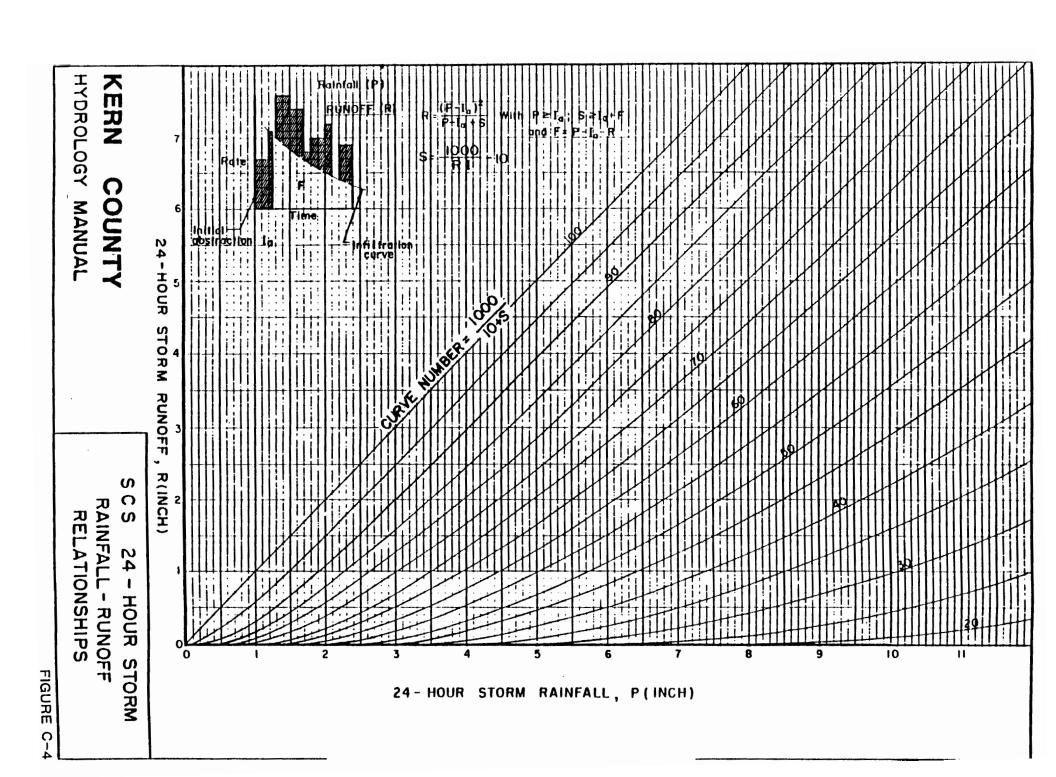
#### Notes:

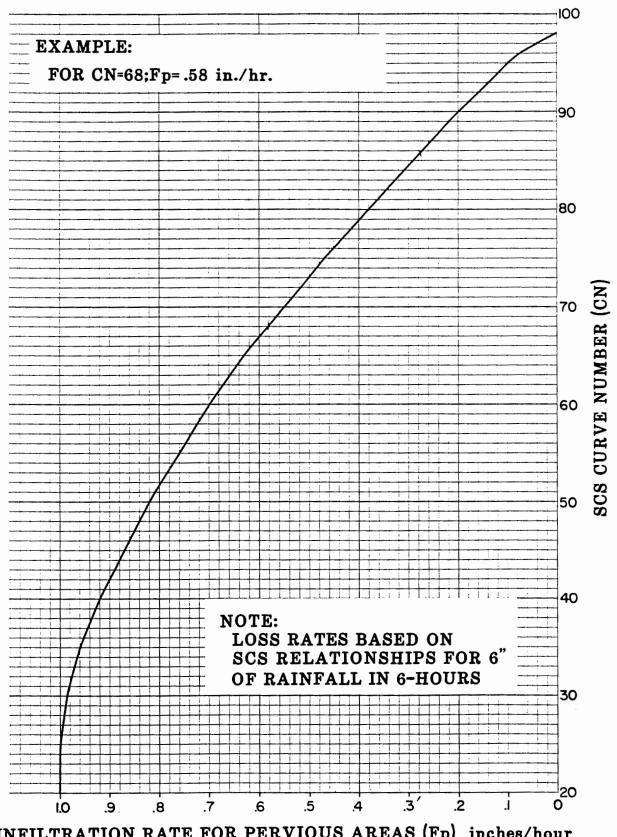
- 1) Recommended values are based on average conditions which may not apply to a particular study. The percentage impervious may vary greatly even on comparable study sized lots due to differences in in dwelling size, improvements, etc. Landscape practices should also be considered as it is common in some areas to use ornamental gravels underlain by impervious plastic materials in place of lawns and shrubs. A field investigation of a study area shall always be made, and a review of aerial photos, where available, may assist in estimating the percentage of impervious cover in developed areas.
- 2) For typical equestrian subdivisions increase impervious area 5% over the values recommended in the table above.

FOR DEVELOPED AREAS

ACTUAL IMPERVIOUS COVER

KERN COUNTY Hydrology Manual

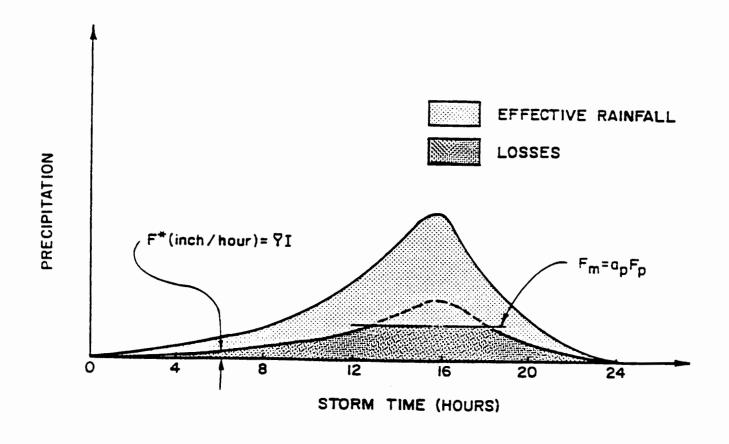




INFILTRATION RATE FOR PERVIOUS AREAS (Fp) inches/hour

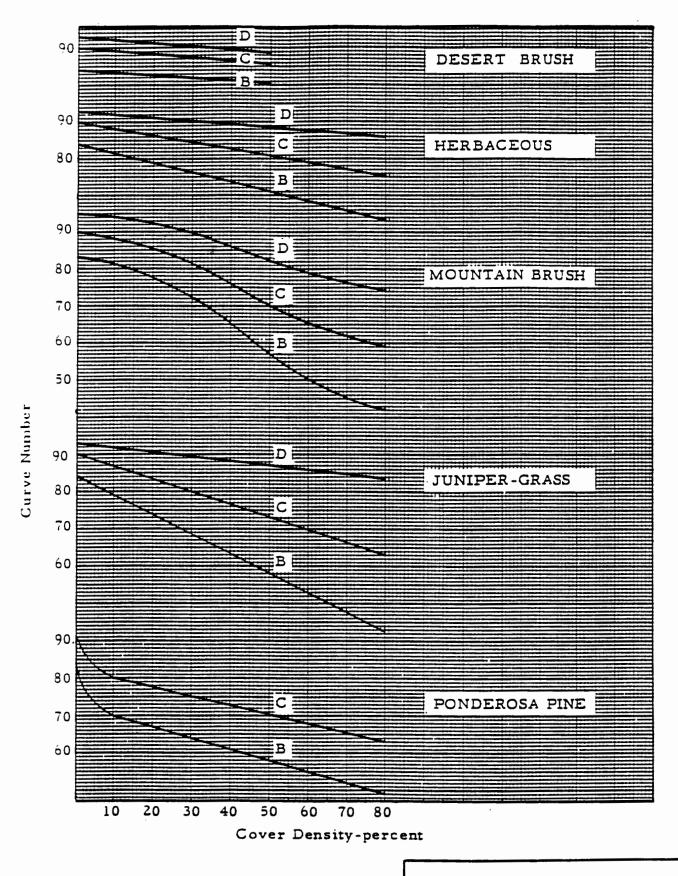
KERN COUNTY Hydrology Manual

INFILTRATION RATE FOR PERVIOUS AREAS VERSUS SCS CURVE NUMBERS



KERN COUNTY
HYDROLOGY MANUAL

DESIGN STORM LOSS FUNCTION



KERN COUNTY

HYDROLOGY MANUAL

HYDROLOGIC SOIL
COVER COMPLEXES AND
ASSOCIATED CURVE NUMBERS

# Section C **Equations**

# **List of Equations**

|              | <u> </u>                                  |                           |   |
|--------------|---|---------------------------|---|
| Equation No. | <b>Equation</b>                           |                           |   |
| C.1          | la  | =                         | 0.2S  |
| C.2          | $S = \frac{1000}{CN} -$                   | 10                        |   |
| C.3          | $Y_j = \frac{(P_{24})^2}{(P_{24} - 1)^2}$ | $\frac{-Ia)^2}{Ia+S)P_2}$ |   |
| C.4          | $Y = \frac{Y_1 A_1 +}{A_1 + A_2}$         | $\frac{+Y_mA_m}{++A_n}$   | <u>,                                     </u> |
| C.5          | $\overline{Y} = 1 - Y$                    |                           |   |
| C.6          | $F^* = \overline{Y} \cdot I$              |                           |   |
| C.7          | Fm  | =                         | $a_p F_p$                                     |
|              |   |                           |   |

# **Variables**

| la | Initial Abstraction (inches) |
|----|------------------------------|
| S  | Estimate soil capacity       |
| CN | Area Curve Number            |

 $\frac{\mathsf{Y}_{\mathsf{j}}}{\mathsf{Y}}$ Yield fraction for 24-hour storm runoff

Yield

Catchment low loss fraction

# Appendix E Kern County Development Standards: Standards for Drainage

## **DIVISION FOUR**

## STANDARDS FOR DRAINAGE

#### **CHAPTER I. GENERAL**

## Sec. 401-1 General Purpose

- 401-1.01 It is the general purpose of these standards that waters generated by storms, springs, or other sources be mitigated so as to provide reasonable levels of protection for life and property, and the maintenance of necessary access to property or passage of the traveling public on the public highways.
- To meet this general purpose, it is necessary that these standards reasonably protect life from the direct effects of flood waters, the indirect health effects associated with stagnating water, and the attractive nuisance provided by standing waters. It is necessary to reasonably protect property from the damaging effects of flood waters. Property access for the ingress and egress of emergency vehicles, or the general public should be reasonably provided. The passage of public vehicles on the public highways should also be reasonably ensured.
- In general, the mitigation measures for the protection of life and property, and the maintenance of emergency vehicle access are based upon the Capital Storm Design Discharge (CSDD). The issues related to property access (by the public) and passage on public highways, and local drainage facility design are based upon the Intermediate Storm Design Discharge (ISDD).
- The design standards in this section are to be deemed to be minimal, and shall not limit the design engineer from using higher standards based upon the engineer's assessment of the protection needs of the development. Alternatives are permissible which are determined by the Director to be of equal or higher quality.
- The Director may allow such exceptions as he may find to be reasonably required by the specific circumstances, to be in the public interest and in conformity with the general objectives of these standards.
- **401-1.06** Special circumstances may exist that require additional mitigation above and beyond these standards as determined by the Director.

Revision 5.21.10 193

## Sec. 401-2 <u>Maintenance</u>

- 401-2.01 All facilities intended for public maintenance shall be designed and constructed subject to the approval of the Director and the maintenance entity, or these standards, whichever is more conservative.
- All drainage facilities intended for private maintenance shall provide a maintenance plan, subject to the approval of the Director. All such facility maintenance plans shall include, but not be limited to: (a) schedule of cleaning (or clearing), (b) mosquito and vector abatement measures (if applicable), (c) pump maintenance schedule (if applicable), (d) notarized statement by the owner(s) acknowledging his/her/their responsibility and intent to maintain the proposed facility in accordance with the approved maintenance schedule.
- 401-2.03 Subdivisions with privately maintained streets shall have the drainage facilities maintained by a homeowners association or other entity which has the ability to assess fees for maintenance.

#### **CHAPTER II. DEFINITIONS**

## Sec. 402-1 <u>Definitions:</u>

- **402-1.01 AGENCY**: refers to the Department of the County of Kern with jurisdiction.
- **402.1.02 ALLUVIAL FAN**: is a landform originating at an apex and characterized by high-velocity flows; active processes of erosion, sediment transport, and deposition; and unpredictable flow paths.
- **402-1.03 APEX**: means a point on an alluvial fan or similar landform below which the flow path of the major stream that formed the fan becomes unpredictable and alluvial fan flooding can occur.
- **402-1.04 CAPITAL STORM DESIGN DISCHARGE (CSDD)**: is that flow determined based upon a precipitation event having a one percent probability of being equaled or exceeded in any given year, commonly referred to as the 100 year storm.
- **402-1.05 CLOSED CONDUIT**: is any system of underground drainage facilities, other than culverts.

- **402-1.06 COMPREHENSIVE DRAINAGE PLAN**: refers to a storm water runoff mitigation plan for multi-phase developments. Such a plan need not be adopted by the County, but will be kept on file by the Director.
- **402-1.07 CONSTRUCTED CHANNEL**: refers to the physical modification of natural channels or the construction of channels.
- **402-1.08 CONTROL FACILITY**: are those hydraulic structures which mitigate the effects of surface runoff resulting from development, flow pattern modification, or flood flows.
- **402-1.09 CULVERT**: is a hydraulically short conduit which conveys storm runoff flows through a roadway embankment or past some other type of flow obstruction.
- **402-1.10 DESIGN PONDING DEPTH**: is the depth to which the design volume will pond in a storm water basin.
- **402-1.11 DETENTION BASIN**: is a storm water facility designed to affect flood hydrograph peak attenuation.
- **402-1.12 EMBANKMENT AREA**: is an area of compacted fill material.
- **402-1.13 ENCROACHMENT:** refers to any change in land use that materially alters the lands flow conveyance potential.
- **402-1.14 FLOOD CONTROL PLAN**: is a plan for the mitigation of flood flows originating from off-site watersheds, or resulting from on-site development.
- **402-1.15 FLOOD FLOW**: shall be considered to be the CSDD for reference in these standards.
- **402-1.16 FLOW PATTERN**: refers to any physical tracing resultant from the historic or existing runoff of water.
- **402-1.17 INTERMEDIATE STORM DESIGN DISCHARGE (ISDD)**: is that flow determined based upon a precipitation event having a ten percent probability of being equaled or exceeded in any given year, commonly referred to as the ten-year storm.
- **LEVEE**: is an embankment whose primary purpose is to furnish drainage or flood protection from storm water runoff and which is, therefore, subject to water loading for periods of only a few days or weeks a year.

- **MASTER DRAINAGE PLAN**: refers to a comprehensive drainage plan or flood control plan adopted by the County which includes adopted funding mechanisms.
- **NATURAL CHANNEL**: is a flow pattern characterized by incised flow channelization with well defined banks and including the overbank flow areas.
- **NUISANCE FLOW**: shall be considered as those waters originating from within, or adjacent to, the development not resulting from storm runoff.
- **ONE PERCENT RISK FLOW**: is the flow on an alluvial fan based upon the joint probability of the flow distribution at the fan apex and the probability of occurring at the development site.
- **402-1.23 REASONABLE:** in the context of this section refers to the balancing of the utility of the facilities or circumstances described against the gravity of the potential for harm.
- **402-1.24 RETENTION BASIN**: is a terminal storm water facility for the storage of runoff. Commonly referred to as a sump.
- **402-1.25 RETARDATION BASIN**: Synonymous with Detention Basin.
- **SLOPE EASEMENT**: shall include the horizontal dimension from the top to toe of slope plus the setback requirements specified by the Grading Ordinance.
- **402-1.27 SOILS ENGINEER (GEOTECHNICAL ENGINEER):** shall mean an engineer experienced and knowledgeable in the practice of soils engineering (geotechnical engineering).
- 402-1.28 SOILS ENGINEERING (GEOTECHNICAL ENGINEERING): shall mean the application of the principles of soil mechanics in the investigation, evaluation and design of civil works involving the use of earth materials and the inspection and/or testing of the construction thereof.
- **STRESS AREA**: refers to those locations where the erosion potential is greater than a straight, uniform channel reach, and includes junctions, transitions, and curves.
- **402-1-30 WATERWAY**: refers to any natural channel, artificial channel or closed conduit, which provides a course for drainage water to flow.

# Sec. 402-2 Off-Site Capital Storm Design Discharge (CSDD) Mitigation

The CSDD flow determined from the off-site watershed shall consider the total area of the off-site watershed. The watershed development condition may be considered in its existing condition at the time of the proposed development if no control facilities mitigating surface runoff exist, and as undeveloped if adequate control facilities mitigating surface runoff exist.

The design of all structures within the development shall be protected to a minimum of one (1) foot above the water surface associated with the CSDD.

The CSDD flow shall be received into the development without diversion onto adjacent property or causing more than one foot rise in pre-development water surface, and shall be discharged in a manner as similar as possible to the existing condition downstream of the development.

## Sec. 402-3 Off-Site Intermediate Storm Design Discharge (ISDD) Mitigation

The ISDD flow shall be based upon the uncontrolled developed watershed proximate to the development when no defined flow pattern exists. When a flow pattern is defined, the ISDD flow determination shall include the total watershed contributing to the flow pattern.

The off-site ISDD shall be mitigated in conjunction with requirements for on-site ISDD flows.

# Sec. 402-4 <u>Hydrologic Flow Determinations</u>

The CSDD and ISDD flows shall be calculated in accordance with the current Kern County Hydrology Manual.

#### **CHAPTER III. DRAINAGE PLANS**

#### Sec. 403-1 Authority

#### **403-1.01** County Master Drainage Plans

The County administers master drainage plans (MDP) over some portions of the County. In these MDP areas, the design hydrology is governed by the assumption made and methodology used, in the development of the MDP or its most recent revision. Modifications to the MDP's assumed land uses may result in the requirement of additional permanent facilities being constructed to mitigate unanticipated runoff.

If MDP planned facilities have not been constructed at the time of site development, then temporary facilities will be required to be

constructed by the Developer. Such facilities may be abandoned upon completion of the MDP facilities intended to serve the site.

#### **403-1.02** Special Districts

Special Districts, such as Community Service Districts, may prepare comprehensive drainage and/or flood control plans for areas under their jurisdiction. Such plans are subject to the review and approval of the County.

If the Special Districts planned facilities have not been constructed at the time of site development, then temporary facilities will be required to be constructed. Such facilities may be abandoned upon completion of the planned facilities intended to serve the site.

County Service Areas are typically required to be formed for the maintenance of drainage facilities in the absence of another maintenance entity.

#### 403-1.03 Subdivisions

These standards shall apply to the drainage/floodplain management requirements specified for subdivisions improvements in the County's Land Division Ordinance.

If the subdivisions storm runoff mitigation measures are to be constructed as part of a comprehensive drainage plan, then each phase of the development shall be designed to function independently or in conjunction with completed development phases.

#### **403-1.04** Mobile Home/Recreational Vehicle Parks

These standards shall apply to the drainage/floodplain management review of Mobile Home/Recreational Vehicle Parks specified in the County's Zoning Ordinance.

## **403-1.05** Site Development

These standards shall apply to the drainage/floodplain management requirements specified for site development in the County's Building Code, Grading Code, Floodplain Management Ordinance, and all other pertinent County Ordinances.

## **CHAPTER IV. ALLUVIAL FAN DEVELOPMENT**

#### Sec. 404-1 Development Policy

Development upon an alluvial fan shall mitigate the effects of the flow at the site of development, which has a one-percent risk of being equaled or exceeded in any given year. Such mitigation shall ensure that the one-percent risk flow will be received into the development site, without causing more than one foot of water surface rise resulting from encroachment at the development site, and discharge the one percent risk flow in a manner, as close as possible, to the flow pattern existing prior to development of the site.

#### Sec. 404-2 Flood Control Facility Requirements

The design of structural flood control measures on alluvial fans shall demonstrate that the measures will effectively eliminate alluvial fan flood hazards from the area protected by such measures. The provided analyses must include, but are not limited to, the following:

- Engineering analyses that quantify the discharges and volumes of water, debris, and sediment movement associated with the flood that has a one percent probability of being exceeded in any year at the apex under current watershed conditions and under potential adverse conditions (e.g., deforestation of the watershed by fire). The potential for debris flow and sediment movement must be assessed using an engineering method acceptable to the Director and Federal Emergency Management Agency (FEMA). The assessment should consider the characteristics and availability of sediment in the drainage basin above the apex and on the alluvial fan.
- Engineering analyses showing that the measures will accommodate the estimated peak discharges and volumes of water, debris, and sediment, as determined in accordance with Section 404-2.01, and will withstand the associated hydrodynamic and hydrostatic forces.
- **404-2.03** Engineering analyses showing that the measures have been designed to withstand the potential erosion and scour associated with estimated discharges.
- 404-2.04 Engineering analyses or evidence showing that the measures will provide protection from hazards associated with the possible relocation of flow paths from other parts of the fan.
- 404-2.05 Engineering analyses that assess the effect of the project on flood hazards, including depth and velocity of floodwaters and scour and sediment deposition, on other areas of the fan.

404-2.06 Engineering analyses demonstrating that flooding from sources other than the fan apex, including local runoff, is either insignificant or has been accounted for in the design.

#### **CHAPTER V. STREET DRAINAGE**

#### Sec. 405-1 <u>Design Flow</u>

**405-1.01** The ISDD shall include the evaluation of both on-site and off-site watersheds when applicable.

#### **405-1.02** Street Conveyance

- 1. For Type "A" subdivisions, the ISDD may exceed the top of a six (6) inch curb by 0.10 feet.
- 2. For Type "B" subdivisions, the depth of flow contained within the road right of way shall not exceed 0.60 feet for the ISDD.
- 3. The depth of flow for the CSDD on major and secondary highways shall be maintained as not to prohibit reasonable access.
- 4. For mobile home/recreational vehicle parks, the depth of flow for the ISDD shall not exceed the carrying capacity of the travel way.
- 5. Where the discharge exceeds the above mentioned limits, a stormdrain or other facilities shall be provided to convey the excess flows.
- 6. The drainage system shall be free flowing and shall not allow the retention of more than one (1) foot of water measured at the flowline after the flows have subsided.

#### **405-1.03** Sedimentation

In areas suspected of significant sediment yield from an ISDD, the following shall apply:

- 1. The developer's engineer shall quantify any sediment yield from on-site or off-site properties based upon the ISDD.
- 2. Sediment yield shall be independent of the runoff event and is to be mitigated separate from the design discharge.

- 3. Sediment shall not be deposited on the roadway.
- 4. Higher levels of mitigation may be required in mudslidemudflow areas.

#### **405-1.04** Erosion

1. Erosion protection measures based on the ISDD shall be established upstream, downstream and through the project by the developer's engineer subject to approval by the Director.

# CHAPTER VI. CULVERTS, BRIDGES AND AT-GRADE-CROSSINGS

#### Sec. 406-1 General

- 406-1.01 All publicly maintained crossings of natural channels shall be bridged or culverted. The minimum length of any culvert shall be from toe-of-slope to toe-of-slope. Additional right-of-way may be required for maintenance of these facilities.
- **406-1.02** Roadways shall be required to bridge a floodway where encroachment of the floodway is prohibited.
- 406-1.03 Energy losses for bridge piers, interior walls for multiple box culverts, or other obstructions within the channel shall be predicated upon the obstruction width plus two (2) feet of debris allowance for each obstruction.

## Sec. 406-2 <u>Culverts</u>

- The ISDD for the total upstream watershed under existing conditions shall not exceed soffit of culvert.
- The CSDD for the total upstream watershed under existing conditions will be allowed to overtop the roadway until 2.0 feet of specific energy is obtained, at which point additional culverts will be required to meet these minimum requirements.
- The 2.0 feet of specific energy shall be calculated at the crown or high point of the traveled roadway.
- The minimum size of any culvert under a publicly maintained roadway shall be 18 inches. For private roads or public access, which are privately maintained, this requirement may be waived.
- **406-2.05** Culverts shall be designed to have a minimum useful life of 50 years.

## Sec. 406-3 Bridges

- The lowest portion of the bridge span shall be one foot or 0.2 times the specific energy (whichever is greater) above the water surface elevation when the normal depth of flow for the CSDD is subcritical.
- The lowest portion of the bridge span shall be one foot or 0.2 times the specific energy (whichever is greater) above the sequent flow depth when the normal depth of flow for the CSDD is supercritical.
- When levee conditions exist, the lowest portion of the bridge span shall also meet the minimum freeboard requirements of the levee.

# Sec. 406-4 <u>At-Grade-Crossings</u>

406-4.01 At-grade-crossings shall not be permitted on a publicly maintained roadway and shall not encroach upon a floodway.

## CHAPTER VII. CLOSED CONDUIT SYSTEMS, CATCH BASINS

#### Sec. 407-1 <u>Design</u>

- 407-1.01 Closed conduit system shall be designed for the total ISDD flow less allowable street flow. (see Chapter V Street Drainage)
- 407-1.02 A closed conduit system intended to serve on-site lot development shall be designed for the total ISDD originating on-site.
- 407-1.03 Closed conduit system shall be designed to have a minimum useful life of 50 years.
- The minimum size of a closed conduit system within the street right-of-way or intended for public maintenance shall be 18 inches.
- The minimum size of a closed conduit system outside of the street right-of-way and intended to be privately maintained shall be eight (8) inches.
- The minimum cover over any closed conduit system shall be 24 inches. The minimum cover required within the street right-of-way shall be 30 inches.
- 407-1.07 Closed conduit system shall be free flowing with no continuous standing water within the pipe.

- The designed pipe size shall not be allowed to decrease as the system progresses downstream.
- The minimum slope of any closed conduit system shall be .001(.10 percent) unless otherwise approved by the Director.
- **407-1.10** The hydrologic tie-in design criteria for the closed conduit system shall be based on equal recurrence.
- 407-1.11 Closed conduit system within the street right-of-way or intended for public maintenance shall be Class III reinforced concrete pipe with rubber gasket joints, or cast-in-place concrete pipe unless otherwise approved or required by the Director.
- The developer's engineer shall plot the hydraulic grade line and the energy grade line profiles for the closed conduit system either on a set of, or on the original, street improvement plans. All calculations and related data for these profiles shall be included with the street improvement plans when submitted.

#### Sec. 407-2 <u>Location</u>

- 407-2.01 A publicly maintained closed conduit system shall be placed within the road right-of-way or easement unless otherwise approved by the Director.
- The alignment of a publicly maintained closed conduit system shall be parallel or perpendicular with the centerline of the road unless otherwise approved by the Director.

#### Sec. 407-3 Freeboard

Within the closed conduit system, the hydraulic grade line shall be at least 0.5 feet below all inlet flowline elevations, and 0.5 feet below the top of non-pressure manholes.

#### Sec. 407-4 Manholes

- **407-4.01** Within the closed conduit system, manholes shall be provided at all junctions, bends, and at intervals prescribed below:
  - a. Manholes shall be provided at intervals no greater than 300 feet where the conduit diameter is less than or equal to 30 inches.

- b. Manholes shall be provided at intervals no greater than 400 feet where the conduit diameter is larger than 30 inches, but smaller than 48 inches.
- c. Manholes shall be provided at intervals no greater than 500 feet where the conduit diameter is 48 inches or larger.
- 407-4.02 A pressure manhole shaft and a pressure cover shall be installed in a closed conduit system whenever the energy grade line is less than 0.50 below the top of the manhole.

## Sec. 407-5 Losses

In addition to normal friction losses, energy losses due to entrance and exit conditions, bends, junctions, and transitions shall be computed. The engineer shall supply all data and reference material for calculated losses subject to review and approval by the Director.

## Sec. 407-6 <u>Erosion</u>

- Velocities within the closed conduit system should not exceed 20 feet per second with standard wall RCP, or 10 feet per second for plastic pipe. Where velocities exceed 20 feet per second for RCP, or 10 feet per second for plastic pipe, a special pipe shall be installed as approved by the Director.
- 407-6.02 Erosion protection against scour velocities shall be provided at the inlet and outlet of the closed conduit system. The engineer shall supply all data and reference material supporting his/her design, subject to approval by the Director.

#### Sec. 407-7 Catch Basins

- The inlet design at closed conduit systems (i.e., location, depression, capacity, structural, etc.) shall be subject to review and approval by the Director.
- 407-7.02 Grate type inlets to the closed conduit system within the street rightof-way shall be allowed only in conjunction with side curb openings and shall be bicycle safe.
- The minimum width of opening for any catch basin intended to be publicly maintained shall be three (3) feet and six (6) inches (3.5').

## Sec. 407-8 Rights-of-Way/Easements

- A right-of-way sufficient to contain the closed conduit and appurtenances plus a minimum of five feet on each side, measured from the edge of the conduit or drainage structure, shall be provided but in no case shall the right-of-way be less than 15-feet in width. Whenever possible, rights-of-way for conduits shall be adjacent to property lines and outside areas where structures are planned. Under no circumstances shall closed conduits and appurtenances be constructed less than 10-feet from any planned or existing structure.
- **407-8.02** Easements will be required on all closed conduit systems outside of the street right-of-way, which are intended for public maintenance.
- **407-8.3** Land rights shall be conveyed to the County in one of the following forms, whichever is appropriate:
  - 1. Separate parcel easement dedicated on a subdivision map.
  - 2. Easement dedicated on a subdivision map as part of adjacent lots.
  - 3. Fee simple or easement offered or granted by separate documents.

#### CHAPTER VIII. RETENTION BASIN DESIGN

#### Sec. 408-1 <u>Design Volume</u>

The design volume of storm water retention basins shall be based upon the runoff from the ISDD five-day storm event and a volume of nuisance water determined by the engineer. No runoff generated on site from the design storm or from nuisance flows will be allowed to leave the site unless downstream drainage disposal facilities exist to handle the flow. The retention of upstream off-site flows shall not be considered to reduce the size of the required on-site retention facilities or mitigate the runoff from the proposed development. An evaluation of the runoff volumes associated with the site in its existing condition shall not reduce the size of the required drainage facilities. The runoff volume from the ISDD five-day storm shall be calculated using the formula:

Runoff Volume =  $0.12 (D_{10})(a_i)(Area)$ 

 $D_{10}$  = 10 yr 24-hr. depth of rainfall (in.)

a<sub>i</sub> = average percentage of impervious area

Area = Drainage area of total development

 $0.12 = 1.44 \times 1/12$ 

1.44 = 5 day mass ratio (KC Hydrology Manual, Table B-1)

1/12 = Conversion of rainfall depth in inches to feet

## Sec. 408-2 <u>Hydraulic Design</u>

In the absence of a hydrologic volume routing analysis, the storm drain hydraulic grade line calculations shall assume that 50% of the design storm volume and 100% of the nuisance volume is in the basin when the peak flow rates occur.

#### Sec. 408-3 Freeboard

Freeboard shall be required for all retention basins having a design water depth exceeding 18 inches. Six (6) inches of freeboard will be required when the design ponding depth within the basin is four (4) feet or less. For basins with a design ponding depth greater than four (4) feet the amount of freeboard required shall be one (1) foot. Freeboard shall be measured from the lowest gutter inlet or top of bank, whichever is lower.

#### Sec. 408-4 Fencing

Retention basins shall be fenced and provided with gated access when the design ponding depth exceeds 18 inches. All retention basins, regardless of ponding depth, that are maintained by the County or an entity administered by the County shall be enclosed by a six (6) foot high masonry block wall. Exceptions may be made, subject to the Director's approval, for certain master planned facilities intended for multi-purpose use.

- The fence shall consist of a six (6) foot high chain link fence of 9 gage fabric with redwood slats or a six (6) foot masonry block wall or approved equal. Fence post footings shall have a minimum diameter of 12 inches and a minimum depth of 30 inches. Masonry block walls shall be designed in accordance with accepted engineering practices. Retaining walls used for basin fencing requirements shall have their design approved by the Director. See Plates R-77 thru R-82.
- **408-4.02** Fence setbacks measured from the top of slope shall provide a reasonable maintenance way for the equipment outlined in the maintenance plan. The following minimum setbacks shall apply:

| Design ponding depth     | Setback                   |
|--------------------------|---------------------------|
| ≤ 18 inches              | 2 feet                    |
| > 18 inches but ≤ 4 feet | 5 feet                    |
| > 4 feet                 | 10 feet                   |
| > 8 feet                 | 10 feet (or in accordance |
|                          | with an approved maint-   |
|                          | enance plan).             |

The basin access gate may be chain-link, wrought iron, or other as approved by the Director. The double gate is not to be attached directly to the masonry wall. The opening must be sufficient for the 14-foot double gate and anchor posts. If wrought iron is used, a metal

mesh privacy screen is to be securely attached to the double gate by rivets or equivalent as approved by the Director. Wrought iron double gates will also require a commercial grade latch or equivalent that can be locked with a County padlock (3/8" shackle diameter). See Plates D-11 for specific sizing and material requirements.

## Sec. 408-5 Access

An equipment access ramp to the bottom of the retention basin shall be provided when the design depth exceeds 18 inches or when the facility is intended for County maintenance.

The ramp shall be a minimum of 12 feet wide with a maximum slope of 15%. The gate to the access ramp shall be 14 feet wide.

Exception - When the design ponding depth is  $\leq$  4 feet, the maximum slope on the ramp may be increased to 20%.

- **408-5.02** Ramps shall not be designed to convey drainage water into the sump.
- 408-5.03 The ramp alignment shall be no more than 45 degrees from the center of the access gate to facilitate maintenance equipment ingress and egress. Other proposed alignments shall have their design approved by the Director.

# Sec. 408-6 Curbing and Rodent Barriers

- In conjunction with fencing, a six (6) inch wide, eighteen (18) inch deep continuous concrete curb shall be provided around the top of the sump. The top of the curb shall be 0.5 feet above the highest adjacent grade. When the sump is fronting on a street, the top of the curbing shall be a minimum of one (1) foot above the top of the street curb. Ramped access across the curb shall be provided at all gated access points to the sump.
- 408-6.02 Rodent barriers will be required on the sides of the sump in proximity to open space, agricultural areas or lot one (1) acre or larger. The bottom of the rodent barrier shall be a minimum of 42 inches below finish grade.

Exception - Rodent barriers may be omitted when the design water depth is 4 feet or less.

#### Sec. 408-7 <u>General Construction Requirements</u>

**408-7.01** General construction requirements for retention facilities shall be in accordance with Plates D-1, D-2, and D-3.

- **408-7.02** Retention facilities shall have the design volume contained entirely in cut.
- Slopes shall be designed no steeper than is safe and no steeper than two (2) horizontal to one (1) vertical. A slope stability analysis will be required when the design water depth exceeds eight (8) feet and side slopes are steeper than 3:1.
- 408-7.04 The minimum bottom dimension for retention basins with a design depth greater than four (4) feet shall be 20 feet. For design water depths 4 feet or less, the minimum bottom width shall be no less than that required for maintenance equipment specified in the maintenance plan.
- **408-7.05** The maintenance way shall be sloped away from the top of bank at a minimum 2%.
- **408-7.06** Drainage basins intended for County maintenance shall be located on a lot dedicated exclusively for drainage/recreational purposes.

#### Sec. 408-8 Testing

- 408-8.01 Retention basins shall not be permitted unless it can be demonstrated, to the satisfaction of the Director, that the basin will completely drain the design volume within seven (7) days.
- Testing of the proposed retention basin shall be provided by a Soils Engineer and shall include, but need not be limited to, an analysis of the soils boring logs and the establishment of the drainage rates of the soils encountered. A minimum of one (1) boring shall be logged within the proposed sump location. This boring shall be advanced below the invert of the basin to a depth equivalent to at least three (3) times the design ponding depth. Testing methods used to establish soil drainage rates shall be approved by the Director.

#### **CHAPTER IX. DETENTION BASIN DESIGN**

#### Sec. 409-1 Design Flow

The design flow into the basin shall be the ISDD five-day runoff hydrograph. Hydrograph design and mass ratios shall be in accordance with the Kern County Hydrology Manual. The out flow hydrograph shall not extend beyond five days from the end of the inflow hydrograph. Infiltration effects from the detention facility shall not be included in the calculation of the outflow hydrograph.

#### Sec. 409-2 <u>Facility Design</u>

Sizing and placement of detention facilities shall not aggravate the potential for downstream flooding.

Requirements for fencing, curbing, setbacks, access, and freeboard shall be in accordance with retention basin design.

- **409-2.01** Detention basins shall be provided with a concreted low flow bypass, or approved equivalent, for the conveyance of nuisance flows to the outlet.
- 409-2.02 An emergency spillway will be incorporated in the design of all detention basins.

#### Sec. 409-3 Sedimentation

Sediment yield shall be determined and mitigation provided by the developer's engineer.

#### Sec. 409-4 Duplex Pump Station (Wet Well) Design Specifications

Pumps used in conjunction with detention facilities shall have their design approved by the Director. Specific design criteria shall include the use of an automated duplex pump, and an alarm system. The pump system shall be designed to pass a minimum two (2) inch sphere and for reliability and low maintenance. Pump maintenance shall be included in the facility maintenance plan.

- Pump station shall be designed to drain the sump in 5 to 7 days with one (1) pump running. However, the minimum flow rate shall be 100 gpm.
- **409-4.02** Pump station shall be a duplex system which automatically alternates between pumps at the end of each cycle.
- The pump station shall either include a lag pump design or automatic controls, which will start the second pump if the first fails to pump.
- **409-4.04** Pumps shall be minimum one (1) HP.
- Pump station shall be designed to allow easy removal of pumps for maintenance, without requiring personnel to enter into a wet well or similar enclosed structure. A "cage" style pump system, where the pump is located in a cage structure at the bottom of the basin, will not be allowed.

- **409-4.06** Pumps and pump station inlet structure shall be screened to prohibit plugging by debris.
- 409-4.07 The pump station (including the electrical/control panel) shall be located next to the entrance of the basin.
- The receiver wet well shall consist of one 60" diameter concrete precast manhole sections with single offset R-3 rubber gasket joints per ASTM C-478, latest edition or approved equal. Duplex pump system shall be equipped with two 1HP (minimum), 115V, non-clog, explosion proof, sump pumps with alarm and alarm switch, check valves, ball valves, discharge line, pump lift out assembly, and electrical junction box. Include a 30" x 42" hatch with lockable, steel hinged access with safety grate.
- The lifting assembly shall be best suited for the pump arrangement. All cables, etc. are to be stainless steel nylon coated. All slide metal surfaces must be considered non-sparking, by URL, to prevent spark ignition in wet well.
- The valve vault shall consist of one 42" diameter concrete precast manhole section (conforming to ASTM C-478 with single offset R-3 gasket joints) with gate valves, swing check valves, and adjustable pipe supports or equivalent. Include a 24" x 24" hatch with lockable, hinged steel access door with safety grate.
- Sump pump wiring shall be connected to a waterproof electrical control panel in a NEMA 3 enclosure or equivalent.
- 409-4.12 A four inch (4") thick Class 2 concrete pad will be required to encompass the precast top slabs, manholes and control panel.
- 409-4.13 All electrical conduits and connectors shall be sealed water-tight and gas-tight using bitumastic paint.
- 409-4.14 All pipe or conduit wall penetrations shall be sealed with a neoprene seal.
- 409-4.15 All exposed steel (pipe, valves, flanges, elbows, and control box exterior) shall be primed with zinc-chromate primer and painted with an epoxy enamel finish. Color to be grey unless otherwise approved.

- A water level staff shall be placed in the sump. The staff may be either anchored to the sideslope of the sump or be attached to the outlet structure, as approved by the Director. The bottom portion of the staff shall be painted black and white, alternating at one-foot increments, to an elevation equivalent to the half full-depth of the sump. The top portion of the staff shall be painted red and white, alternating at one-foot increments, to one foot above design water surface.
- All controls shall be mounted in a NEMA (3) metal enclosure or equivalent. The control panel and all electrical components shall bear the Underwriter's Laboratory (UL) Label. All circuit breakers shall have operators extending through the control panel door. All motor starter overload resets, selector switches, push buttons and pilot lights shall be mounted on the control panel door. The control panel shall be enclosed in a vandal resistant enclosure with provisions for locking with a County's lock 3/8" shank pad lock or approved equal.
- The control for each pump shall include a thermal magnetic circuit breaker, rotary hand-off-automatic switch, and magnetic motor starter with ambient compensated overload relays and quicktrip heaters. The pump control circuit shall include a door interlock switch to denergize the control circuit when the control panel door is open, a control mounted transformer with fused 115 volt secondary, and a door mounted control circuit disconnect switch.
- Pump operation shall be controlled by three (3) bulb type liquid level sensors. An intrinsically safe pilot circuit shall be provided for each level sensor to reduce the power to the sensor to a level incapable of releasing sufficient electrical or thermal energy to ignite explosive gases.
- A fourth level sensor, with intrinsically safe circuit, shall be furnished for indication of high water alarm condition. High water alarm shall be indicated by a panel-mounted pilot light and external audible alarm with silence button.
- The controls shall provide for lead/lag sequencing of the pumps, an automatic alternator shall alternate the lead/lag duty on each succeeding pump cycle. An outer pump seal leakage detection system shall be included in the control enclosure. When the motor probes sense the presence of moisture in the oil seal chamber, a

relay coil will illuminate a panel mounted indicating alarm lamp to indicate possible outer motor seal failure and the alarm light.

- The pump station shall have a Hand-Off-Auto switch and an automatic low water shut-off, and have green (run) and red (alarm) indicator lights visible from the road/street.
- **409-4.23** Control panel shall contain hour meters for each pump.
- 409-4.24 Control panel shall contain a switched GFI 115 volt duplex electrical outlet.
- **409-4.25** Control panel shall include an emergency generator hook-up connection.
- System Testing—Installed pumps, controls and pipes shall be tested in accordance with recommendations of the manufacturer prior to acceptance by the Kern County Engineering, Surveying & permit Services Department.
- Prior to acceptance, two (2) complete operation and maintenance manuals, with wiring and interconnect diagrams for all equipment and controls, model and serial numbers of the sump pumps, and a set of as-built drawings on cronar shall be furnished to the County.

#### CHAPTER X. CONSTRUCTED CHANNEL DESIGN CRITERIA

#### Sec. 410-1 Design Flow

Constructed channels shall be designed to carry the CSDD plus freeboard.

#### Sec. 410-2 Freeboard

- The minimum freeboard between the design water surface, and the top of bank of the channel shall be 0.50 feet or 0.20 of the specific energy, whichever is greater.
- 410-2.02 If the designed water surface is within the embankment area, the design and construction of the channel shall be in accordance with the levee design criteria, including freeboard requirements.
- 410-2.03 The minimum freeboard requirements for bridges, culverts, and utility crossings which span open channels and which are existing, planned

or projected at the time of channel design shall be in accordance with the requirements specified in Sections 406-2 and 406-3.

410-2.04 Superelevation resultant from directional modification shall be considered prior to computing the required freeboard.

# Sec. 410-3 <u>Hydraulic Design</u>

- 410-3.01 Channels shall be designed with proper allowance for hydraulic losses for all planned and projected future crossings or other obstructions to maintain clearance and freeboard as required.
- 410-3.02 The water surface and the energy grade line profile shall be computed and plotted for all constructed channels and at locations where natural channels modifications are proposed.
- 410-3.03 Constructed channels shall not be designed with a slope in the range of  $\pm$  20% of critical slope unless freeboard equal to the height for instability waves is added.
- 410-3.04 A minimum velocity of two (2) feet per second shall be maintained for lined channels to prevent sedimentation.

# Sec. 410-4 <u>Structural Design</u>

- The minimum bottom width of constructed channels shall be ten (10) feet. A triangular channel may be permitted when the channel side slopes are four (4) to one (1) or flatter.
- The minimum centerline radii for curves in constructed channels shall be three (3) times the top width of the design water surface.
- Design of slopes shall be predicated upon results of an investigation by a Soil Engineer, subject to the approval of the Director.
- 410-4.04 Adequate bank protection and drop structures shall be provided where the slopes in the channel are steep and high velocities are present.
- 410-4.05 Bank protection shall be provided based on the design engineer's recommendations, subject to the approval of the Director. Stress area protection shall extend downstream from the end of the stress area a distance equal to ten (10) times the design water depth, unless the engineer can show that the erosion potential is not excessive.

- At drop structures or in other locations where a hydraulic jump may occur, bank protection shall be provided through the hydraulic jump for a minimum distance of six (6) times the sum of the sequent depth and the depth of freeboard. This protection shall cover the invert and extend to the height of the sequent depth plus the height of the freeboard. The protection material may be either concrete, concreted-rock slope protection, sacked concrete, air-blown mortar or other approved alternative.
- 410-4.07 All channel lining materials and methods shall be specified by the engineer and approved by the Director.
- 410-4.08 All appurtenant drainage facilities shall be constructed and areas adjacent to channels graded so that erosion will be prevented within the channel right-of-way.
- **410-4.09** Waterways shall enter the main channel at an angle not exceeding 25 degrees.

## Sec. 410-5 Erosion

The engineer shall provide recommendations on all necessary mitigation measures for erosion including bank protection and bottom stabilization of the channel, subject to the approval of the Director.

| Sec. | 410-6    | <u>Fencing</u>   |
|------|----------|--|
|      | 410-6.01 | Constructed channels with slopes steeper than four (4) to one (1) with specific energy, at any point, greater than 1.5 feet shall be fenced in its entirety. |
|      | 410-6.02 | A six (6) foot high nine (9) gage chain link fence fabric with tension wire shall be installed on each side of the right-of-way.                             |
|      | 410-6.03 | At all road intersections, fencing shall be installed to prevent public access to constructed channels.  |
|      | 410-6.04 | A 14 foot wide chain link drive gate shall be provided at all points of vehicular access.  |
| Sec. | 410-7    | Easements/Right-of Ways and Maintenance Ways   |
|      | 410-7.01 | Right-of-ways for constructed channels with side slopes steeper than four (4) to one (1) shall be provided as follows:                                       |

- a. The right-of-way for channels with top widths greater than 50 feet, as measured to the top of freeboard, shall include the top width of the channel, two maintenance ways (one on each side of the channel), slope easements (when applicable), and interceptor ditch area (when applicable). The maintenance ways shall be a minimum of 15 feet wide. Runoff from the maintenance ways shall be mitigated.
- b. The right-of-way for channels with top widths of 50 feet or less, as measured to the top of freeboard, shall include the top width of the channel, one maintenance way on either side of the channel, slope easements (when applicable), and interceptor ditch area (when applicable). The maintenance way shall be a minimum of 15 feet wide. Runoff from the maintenance way shall be mitigated.
- The right-of-way for constructed channels with side slopes four (4) to one (1) or flatter shall be sufficient to contain the top width of the channel (measured from top of freeboard) plus slope easements as needed. A minimum of five (5) feet on either side of the channel shall be provided for maintenance purposes.
- **410-7.03** Right-of-way for turn-around: Turn-around distance and radii:

At the terminus and at intervals not to exceed one channel mile, turn around areas shall be provided. The minimum inside radii for maintenance roads shall be 40 feet.

- Tributary waterways shall be conveyed under maintenance roads in closed conduits or culverts as applicable. Where open channel tributaries cross a maintenance road, a convenient turn-around area shall be provided for maintenance vehicles. The minimum diameter of a turn-around shall be 40 feet.
- At intersections of the channel with public roads, sufficient right-of-way shall be provided to permit access from the public road to the maintenance road as approved by the Director.

In the event that the channel right-of-way does not intersect a public road, a turn-around or a 15 foot wide access right-of-way shall be provided from a public road to the channel right-of-way at intervals not to exceed one (1) channel mile.

#### Sec. 410-8 <u>Sedimentation</u>

The determination of sediment yield and proposed mitigation measures of such shall be prepared and recommended by a qualified registered civil engineer, subject to the approval of the Director.

## **CHAPTER XI. LEVEE DESIGN**

#### Sec. 411-1 Design Flow

Levees shall be designed to accommodate for the CSDD plus freeboard.

## Sec. 411-2 <u>Freeboard</u>

- The minimum freeboard between the designed CSDD water surface and the levee's top of bank shall be three (3) feet or 0.20 times the specific energy plus one (1) foot, whichever is greater.
- An additional one (1) foot, above this minimum of freeboard, shall be required within 100 feet of either side of structures within the levee or whenever the flow is constricted, such as at bridges. An additional 0.50 foot above the minimum is also required at the upstream end, tapering to the minimum at the downstream end of the levee.

#### Sec. 411-3 <u>Hydraulic Design</u>

See Section 410-3 Hydraulic Design for details.

#### Sec. 411-4 <u>Structural Design</u>

Levees shall be designed in accordance with the latest revision of the Corps of Engineers Design and Construction of Levees, Engineer Manual, EM1110-2-1913.

#### Sec. 411-5 <u>Erosion</u>

Mitigation measure for erosion protection shall be prepared and recommended by a registered civil engineer, subject to the approval of the Director.

## Sec. 411-6 Fencing

Fencing requirements for levees shall be in accordance with the criteria contained in the constructed channel design, Section 410-6.

# Sec. 411-7 <u>Easements/Right-Of-Way</u>

Access, easements and right-of-way shall be in accordance with the requirements set forth in Section 410-7. (Constructed Channels).

#### Sec. 411-8 Sedimentation

Mitigation measures shall be prepared and recommended by a qualified, registered engineer, subject to the approval of the Director.

#### Sec. 411-9 <u>Maintenance</u>

A maintenance plan and an entity with taxing power to maintain levees shall be established, subject to the approval of the Director. Neither the County nor County Service Area will maintain a levee.

#### **CHAPTER XII. NATURAL CHANNELS**

#### Sec. 412-1 Delineation

All natural channels shall be identified and clearly delineated on the plans with the appropriate floodplain designation.

For defined natural channels, the Floodplain and Floodway Boundaries shall be delineated, subject to the approval of the Director.

#### Sec. 412-2 Setback

The minimum setback from the top of bank of a natural channel with side slopes steeper than two (2) horizontal to one (1) vertical, shall be a two (2) to one (1) slope plus a 10 foot wide buffer strip. The setback shall be measured from the toe of the slope. Where the slopes are flatter than two (2) to one (1), the required setback shall be a minimum of 10 feet from the Floodway limit.

#### Sec. 412-3 Tie-Ins

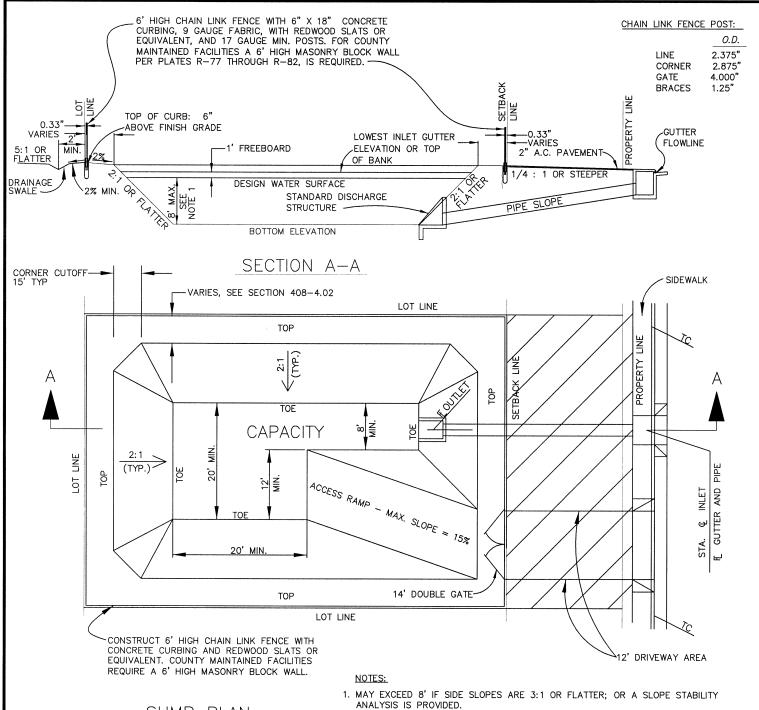
Where natural channels merge into constructed channels, the tie-ins shall be designed in a manner to dissipate energy and protect against erosion. The design for such tie-ins shall be in accordance with acceptable engineering practices and approved by the Director.

#### Sec. 412-4 Relocation

Should an existing natural channel be relocated, the channel shall be designed in accordance with the criteria specified herein for constructed channels.

# Sec. 412-5 <u>Use of Natural Facilities</u>

All applicable Federal and State permits and requirements shall be required for any operation that would discharge dredged or fill material in any waters of the United States (normally channels identified with blue lines on the U.S.G.S. maps).



# SUMP PLAN

#### LEGEND

TOP - TOP OF CURB

FG - FINISH GRADE

OG - ORIGINAL GROUND



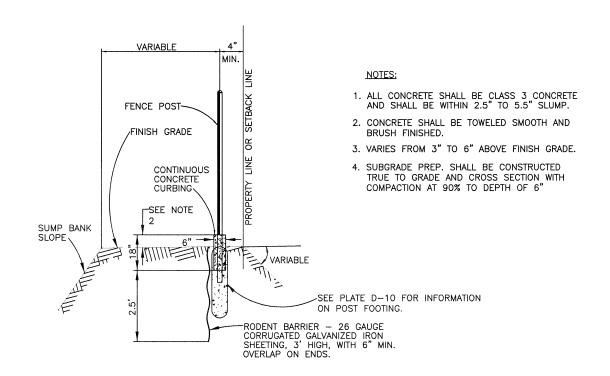
PLOTTED: 02/25/2010

INDICATES 2" A.C. OVER NATIVE SOIL WHICH HAS BEEN TREATED WITH A PERMANENT SOIL STERILANT SUBJECT TO THE APPROVAL OF THE DIRECTOR.

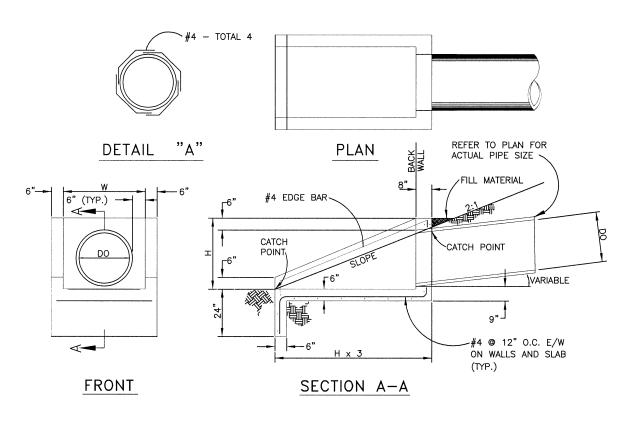
CHECKED BY:

- 2. VARIATIONS TO THE DIMENSION MAY BE APPROVED BY THE DIRECTOR.
- ADDITIONAL REQUIREMENTS MAY BE IMPOSED AS PART OF THE CONDITIONS ISSUED.
- 4. COMPACT O.G. TO 95% FOR MINIMUM OF SIX (6) INCHES UNDER 2" A.C.
- 5. WHEN FENCE IS SET ON FRONT R/W LINE SIDEWALK SHALL BE FULL WIDTH.
- 6. TACK WELD FABRIC AND HARDWARE TO POSTS.
- TREAT BLOCK WALL WITH ANTI-GRAFFITI PRODUCT SUBJECT TO APPROVAL OF THE DIRECTOR.
- 8. CONSTRUCT  $6" \times 18"$  CONCRETE CURB UNDER GATE W/ TWO (2) #4 REBAR TOP AND BOTTOM.

DATE: Revisions 8-18-1995 COUNTY OF KERN PLATE NO. Date Desc STATE OF CALIFORNIA 4/09 B.D.H DESIGNED BY: DEVELOPMENT SUMP DETAILS DRAWN BY: STANDARD D-1K.S.



### CURBING AND RODENT BARRIER DETAILS



### DISCHARGE STRUCTURE

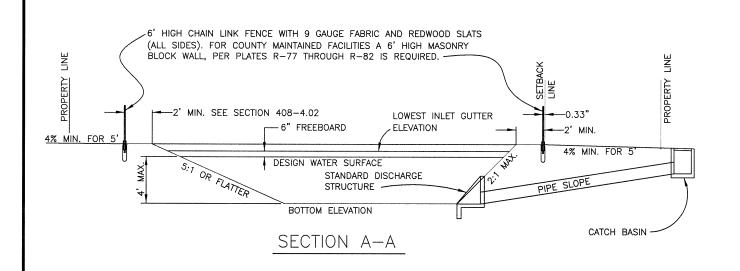
| PLOT          | TED: 02/25/2010 |                    |
|---------------|-----------------|--------------------|
| Revis<br>Date | sions<br>Desc   | DATE:<br>3-31-1995 |
| 4/09          | B HILL          | DESIGNED BY:       |
|               |                 | R.J.L.             |
|               |                 | DRAWN BY:<br>K.S   |
|               | •               | CHECKED BY:        |
|               |                 | C.L.               |

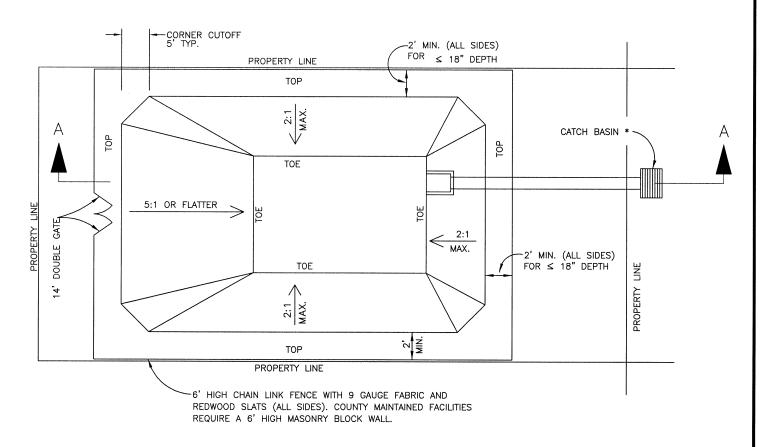
COUNTY OF KERN
STATE OF CALIFORNIA
DEVELOPMENT
STANDARD

CURBING, RODENT BARRIER, AND DISCHARGE STRUCTURE DETAILS PLATE NO.

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D-2





### SUMP PLAN

NO CURB AND GUTTER SHOWN

 $\ensuremath{\overline{\text{NOTE:}}}$  SEE ADDITIONAL NOTES AND REQUIREMENTS FOR CHAIN-LINK FENCES AND MASONRY WALLS ON PLATE D-1

| PLOT          | TED: 02/25/2010 |                        |
|---------------|-----------------|------------------------|
| Revis<br>Date | sions<br>Desc   | DATE:<br>8-18-1995     |
| 4/09          | B.D.H.          | DESIGNED BY:<br>R.J.L. |
| <u> </u>      | •               | DRAWN BY:              |
|               | •               | K.S                    |
|               |                 | CHECKED BY:            |
|               |                 | C.L.                   |

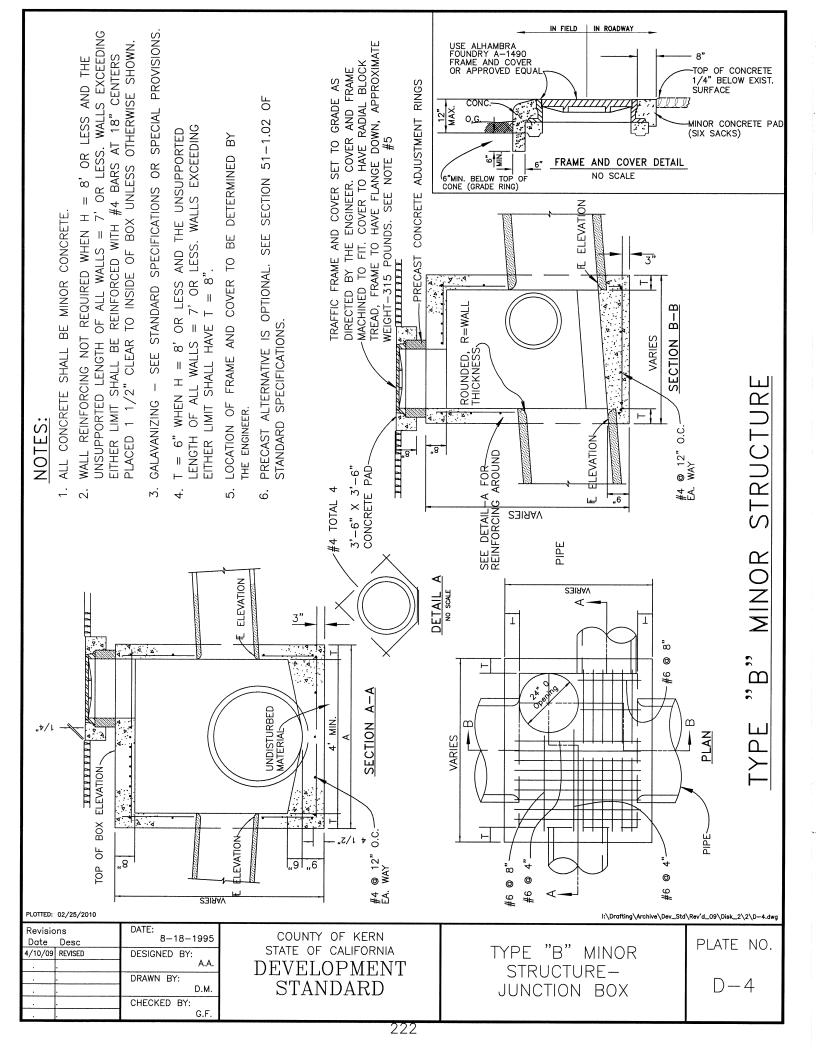
COUNTY OF KERN
STATE OF CALIFORNIA
DEVELOPMENT
STANDARD

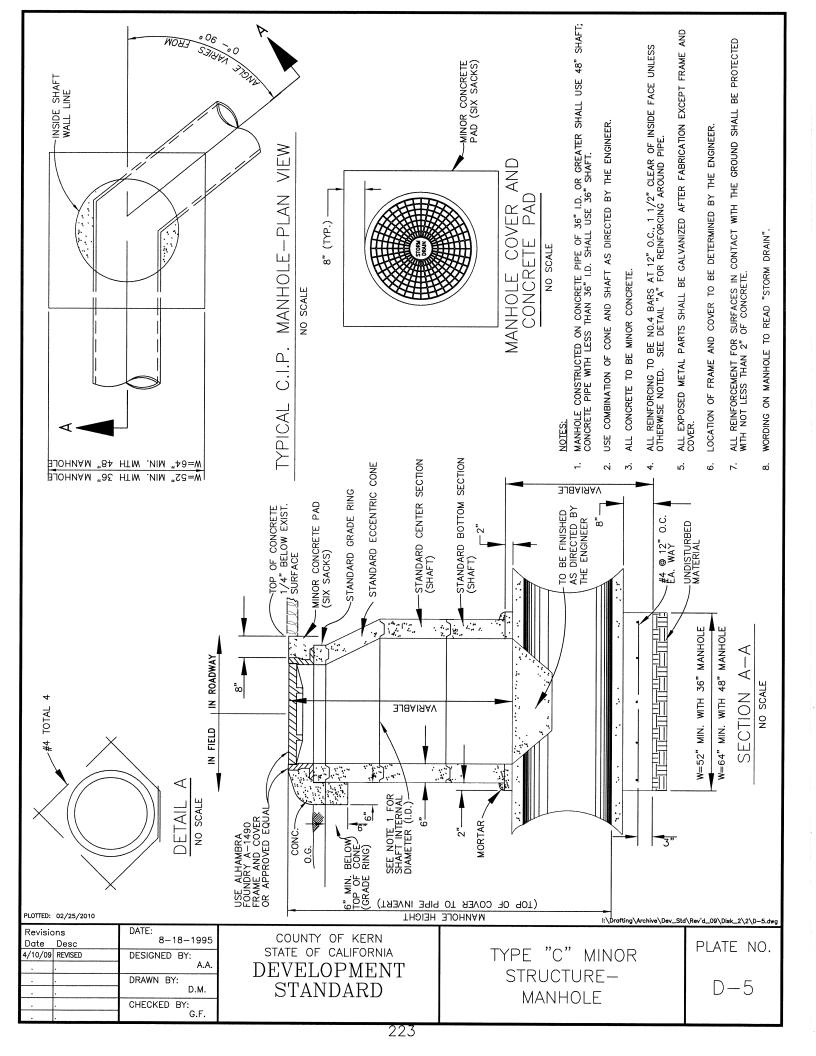
SHALLOW SUMP DETAILS

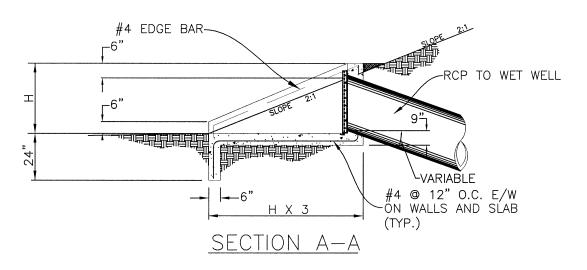
PLATE NO.

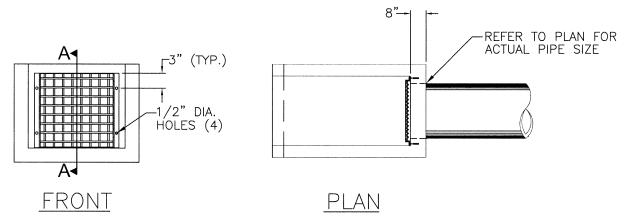
l:\Drafting\Archive\Dev\_Std\Rev'd\_09\Disk\_2\2\D-3 Shallow Sump.dwg

D-3









# INLET STRUCTURE

### **GRATE NOTES:**

- 1. GRATE FABRICATED OR EQUIVALENT SHELF ITEM— ALL PARTS & PRODUCTS GALVANIZED
- 2. FRAME CONSTRUCTED W/ 1/4" x 3/4" x 2" x LENGTH (VARIES TO PIPE SIZE ) ANGLE IRON
- 3. MIN. FOUR- 3/8"X 3" S.S. RED HEAD ANCHOR BOLTS FLAT LOCK WASHER, 2 EA PER VERTICAL ANGLE 3" FROM TOP & BOTTOM OF FRAME.
- 4. FOUR-1/2" DIA. HOLES IN FRAME
- 5. GRATE OPENING  $1\frac{3}{16}$ " x 2" O.C.
- 6. 1/4" DIA ROD WELDED TO FRAME ON ALL SIDES

### NOTES:

1. PIPE DETAIL REFER TO PLATE D-2.

PLOTTED: 02/25/2010

 Revisions
 4-30-2009

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 DESIGNED

 KL.H.
 K.L.H.

 DRAWN
 BY:

 B.D.H.
 CHECKED

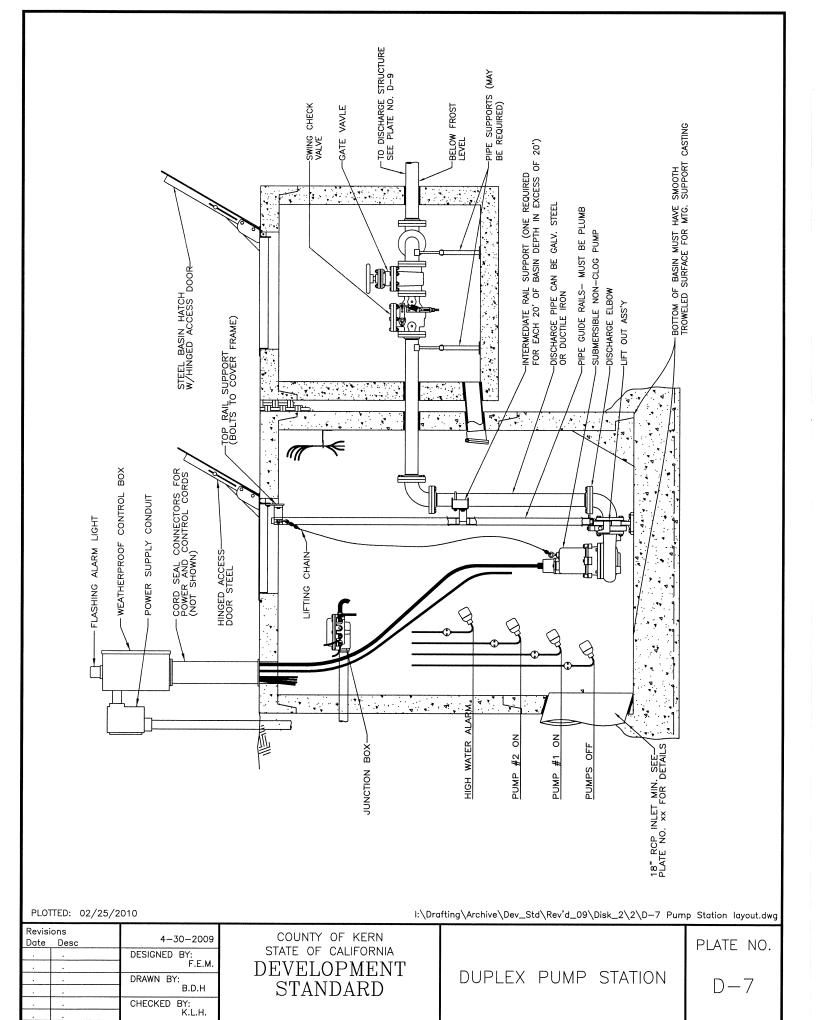
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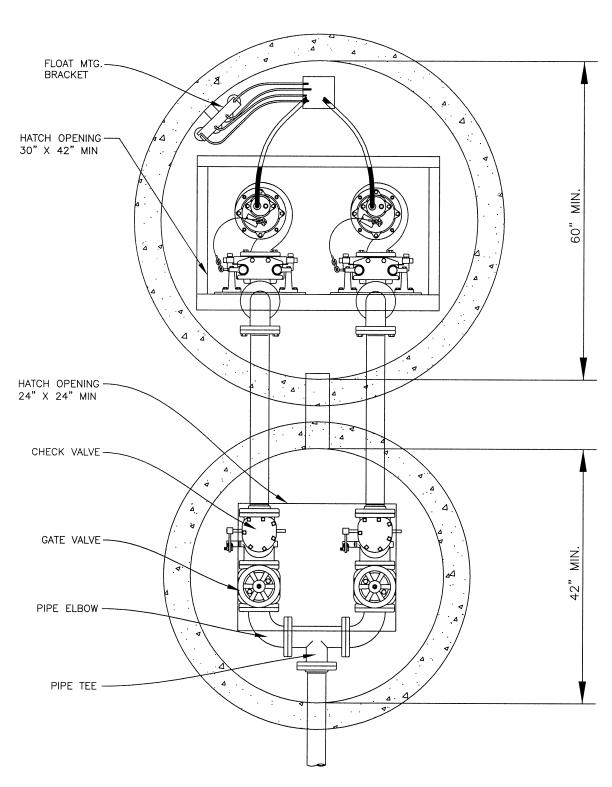
COUNTY OF KERN
STATE OF CALIFORNIA
DEVELOPMENT
STANDARD

PUMP STATION INLET STRUCTURE

PLATE NO.

D - 6





\*MODIFIED FROM <u>FEMyers.com</u> NON-CLOG, 3" DISCHARGE, DUPLEX PUMP INSTALLATION DRAWING ESS-2228b

CHECKED BY: K.L.H.

 Revisions
 4-30-2009

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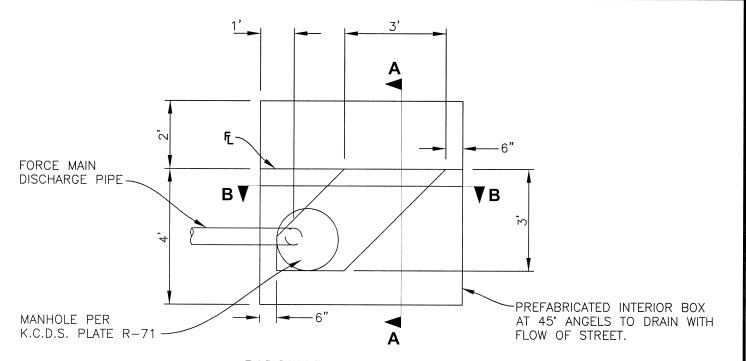
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COUNTY OF KERN STATE OF CALIFORNIA DEVELOPMENT STANDARD

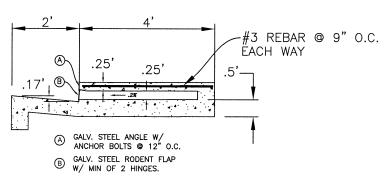
PLAN VIEW DUPLEX PUMPS

PLATE NO.

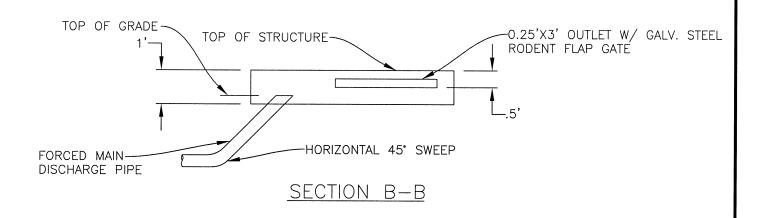
D-8



### DISCHARGE STRUCTURE



### SECTION A-A



| FLOI | ILD. | 02/ | 23/4 | 2010 |  |
|------|------|-----|------|------|--|
|      |      |     |      |      |  |
|      |      |     |      |      |  |

 Revisions Date
 Desc
 4-30-2009

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 DESIGNED BY: K.L.H.

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 DRAWN BY: B.D.H.
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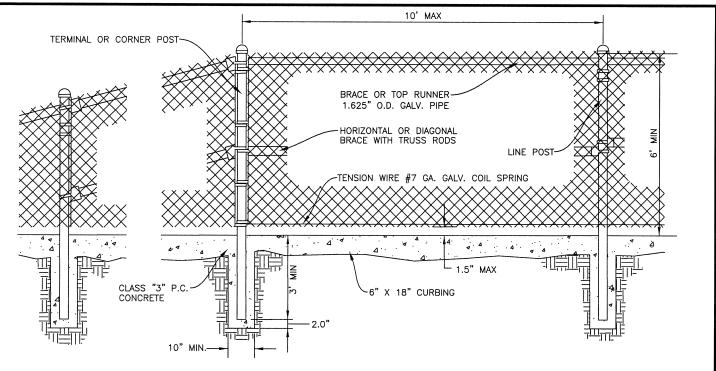
COUNTY OF KERN
STATE OF CALIFORNIA
DEVELOPMENT
STANDARD

PUMP STATION
DISCHARGE STRUCTURE

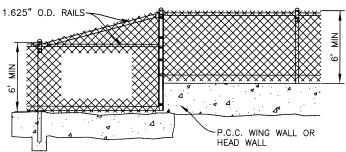
PLATE NO.

I:\Drafting\Archive\Dev\_Std\Rev'd\_09\Disk\_2\2\D-9 Discharge structure.dwg

D - 9



### TYPICAL CHAIN LINK FENCE DETAIL



# TYPICAL DETAIL AT CULVERT ENDWALLS

### NOTES:

- INSTALLATION OF FENCING AND GATES SHALL BE IN ACCORDANCE WITH THE REQUIREMENTS OF "STANDARD SPECIFICATION, STATE OF CALIFORNIA, DEPARTMENT OF TRANSPORTATION," APPROVED CURRENT EDITION.
- CONCRETE CURBING SHALL BE CONSTRUCTED UNDER ALL FENCES. CURBING SHALL BE 6" X 18", CLASS 3 CONCRETE.
- CORNER POST SHALL BE INSTALLED AT ALL ANGLES IN FENCE LINE IN EXCESS OF 10".
- 4. END, CORNER, AND GATE POSTS SHALL BE BRACED TO THE NEAREST LINE POST WITH GALV. DIAGONAL OR HORIZONTAL BRACES USED AS COMPRESSION MEMBERS AND GALV. 0.375" STEEL TRUSS RODS WITH TURNBUCKLES OR TRUSS TIGHTENER USED AS TENSION MEMBERS.
- 5. FABRIC SHALL BE FASTENED TO GATE POST, TERMINAL POST, OR CORNER POST WITH 3" X 3/4" STRETCHER BAR BONDS AT 8" ON CENTER.

### **FENCING SPECIFICATIONS:**

- FENCING FABRIC SHALL BE 9 GUAGE, 2" MESH, AFTER WEAVING, KNUCKLED TOP AND BOTTOM, 6' HIGH GALV.
- 2. CORNER POSTS SHALL BE 2-%" O.D. GALV. PIPE.
- 3. LINE POST 2-%" O.D. GALV. PIPE.
- 4. PRIVACY SLATS SHALL BE 2-3/6" X 1/4".
- FABRIC SHALL BE FASTENED TO LINE POST, LAST RUNNER, AND BOTTOM TENSION WIRES WITH FABRIC BONDS SPACED APPROX. 14" APART.
- 7. FABRIC SHALL CONFORM TO ASTM A-392, CLASS 1.
- 8. SUBGRADE PREPARATION SHALL BE CONSTRUCTED TRUE TO GRADE AND CROSS SECTION WITH COMPACTION OF 85% TO A DEPTH OF 0.5"
- 9. WHEN REDWOOD SUBURBAN SCREEN, OR EQUIVALENT IS REQUIRED IT SHALL BE CONSTRUCTED SO THAT THE SLATS ARE LOCKED INTO POSITION AND CAN ONLY BE REMOVED WITH TOOLS.
- 10. FENCE FABRIC IS TO BE TACK WELDED TO POSTS IN THREE PLACES (TOP, CENTER, AND BOTTOM). FENCE HARDWARE IS TO BE TACK WELDED AND GROUND SMOOTH. ALL EXPOSED METAL PARTS ARE TO BE GALV. PRIOR TO INSTALLATION.

PLOTTED: 02/25/2010

CHECKED BY:

CHAIN LINK FENCING SPECIFICATIONS

PLATE NO.

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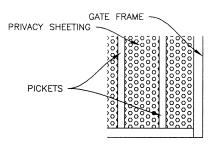
D - 10

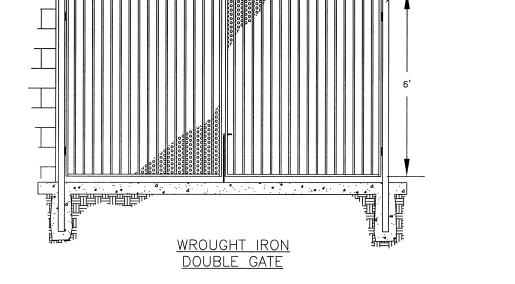
### WROUGHT IRON GATE SPECS:

1. HINGE POST SHALL BE A MIN. OF  $4x4x \frac{\pi}{6}$  SQ TUBING.

4" MAX.

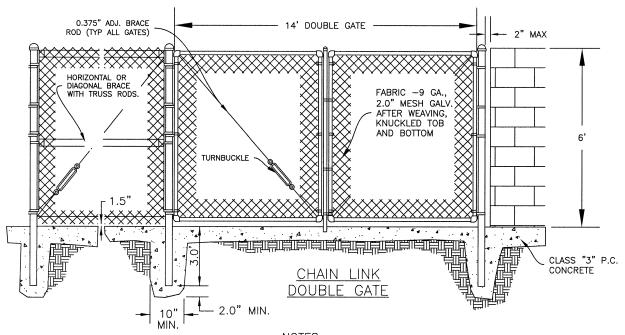
- GATE FRAME SHALL BE A MIN. 1-1/2" SQ. TUBING.
- 3. PICKETS SHALL BE A MIN.  $\frac{\pi}{4}$  SQ TUBING WITH 4" MAX CLEAR DIMENSION.
- 4. PRIVACY SHEETING SHALL BE PERFORATED SHEET METAL, 24 GAUGE, ¼6" DIM HOLE, ¼8" STAGGERED CENTER.
- 5. GATE SHALL BE A 14' DOUBLE GATE.
- 6. GATE LATCH SHALL HAVE COMMERCIAL GRADE LOCKING DEVICE FOR ¾" PADLOCK SHANK OR A LICKING DEVICE THAT CAN BE KEYED TO THE STANDARD K.C.E.S.S. KEY-CORE.





14' DOUBLE GATE

### PRIVACY SHEETING DETAIL



### NOTES:

### DOUBLE DRIVE GATE

WIDTH-14'
HEIGHT-6'
FRAME-1.875" O.D. GALV. PIPE 2.72LB/FT
COMMERCIAL LOCKING DEVICE WITH DROP ROD

- 1. CURBING AS SPECIFIED BY COUNTY OF KERN DEVELOPMENT STANDARDS, PLATE D-2.
- 2. END, CORNER, AND GATE POSTS SHALL BE BRACED TO THE NEAREST LINE POST WITH GALV. DIAGONAL OR HORIZONTAL BRACES USED AS COMPRESSION MEMBERS AND GALV. 0.375" STEEL TRUSS RODS WITH TURNBUCKLES OR TRUSS TIGHTENERS USED AS TENSION MEMBERS.
- 3. WHEN REDWOOD SUBURBAN SCREEN, OR EQUIVALENT, IS REQUIRED IT SHALL BE CONSTRUCTED SO THAT THE SLATS ARE LOCKED INTO POSITION AND CAN ONLY BE REMOVED WITH TOOLS.
- 4. FRAMES SHALL BE MADE WITH FITTINGS OR WELDS GROUND SMOOTH, AND GALVANIZED.
- 5. CHAIN LINK FENCE FABRIC SHALL CONFORM TO ASTM: A-392, CLASS 1, AND BE INSTALLED IN ACCORDANCE WITH THE REQUIREMENTS OF SECTION 80-4 OF THE "STANDARD SPECIFICATIONS, STATE OF CALIFORNIA, DEPARTMENT OF TRANSPORTATION", APPROVED CURRENT EDITION.

PLOTTED: 02/25/2010

COUNTY OF KERN

[ATE OF CALIFORNIA | DOLLD | F. OATE | PLATE NO.

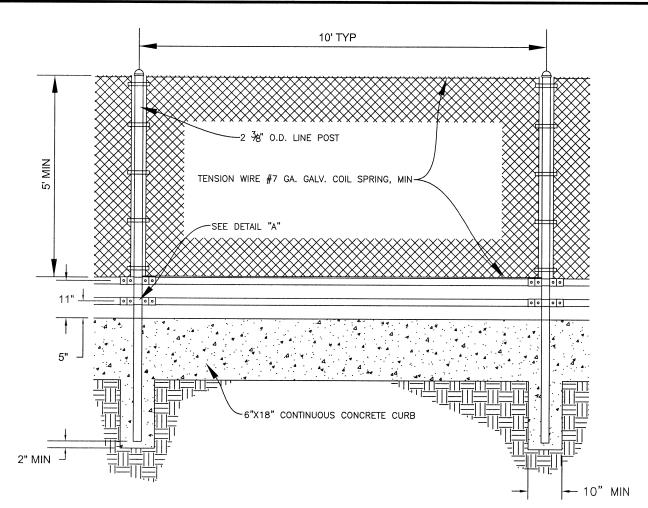
| Revis<br>Date | Desc | 6-6-2009     |
|---------------|------|--------------|
|               | •    | DESIGNED BY: |
|               |      | K.L.H.       |
|               | •    | DRAWN BY:    |
|               |      | B.D.H.       |
|               | •    | CHECKED BY:  |
|               |      | A.A.         |

STANDARD

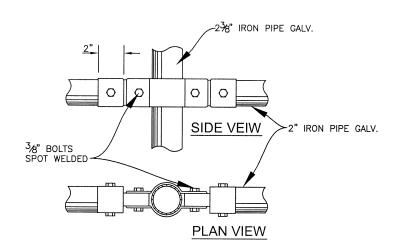
DOUBLE GATE SPECIFICATIONS

PLATE NO. D-11

HINGE POST



# TRANSVERSE PROTECTION BAR



### NOTES:

- 1. ALL CONCRETE SHALL BE CLASS 3.
- 2. SEE PLATE D-10 FOR ADDITIONAL FENCE DETAILS.
- 3. ALL EXPOSED METAL PARTS ARE TO BE GALV PRIOR TO INSTALLATION.
- HARDWARE IS TO BE TACK WELDED AND GROUND SMOOTH AND GALV.
- 5. SEE PLATE D-2 FOR RODENT BARRIER DETAILS.

### **DETAIL "A"**

| PLOTT         | ED: 02/26/2010 |              |
|---------------|----------------|--------------|
| Revis<br>Date | sions<br>Desc  | 6-5-2009     |
|               |                | DESIGNED BY: |
|               |                | K.L.H.       |
|               | •              | DRAWN BY:    |
|               | •              | B.D.H.       |
|               |                | CHECKED BY:  |
|               |                | A,J.L.       |

COUNTY OF KERN
STATE OF CALIFORNIA
DEVELOPMENT
STANDARD

FLOOD ZONE FENCING SPECIFICATIONS

PLATE NO.

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D - 12

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# Appendix F Pre-Post Water Balance Calculation Sheets

# Kudu Solar Project Post Construction Stormwater Calculation Worksheet

| is the project located within a permitted Phase I or Phase I Municipal Separate Storm Sewer System (MS4) area? Note: Non-traditional symal MS4s that lie within a Phase I or I MS4 area but are NOT destinated mus | is the project located within a permitted Phase I Municipal Separate Storm Sewer System (MS4) area? Mote: Ho no traditional small MS4s that lie within a Phase I or III MS5 area but are NOT designated must comply with the Construction General Permit post construction calculator. | lator.   | No 🔻       |
|--|--|--|------------|
| Will the project use an alternative method to calculate runoff   | Will the project use an alternative method to calculate runoff volume or use different site design measures than those listed in the GSP calculator?   |  | ▶ ON       |
| Will the project be subdivided into smaller sub-areas or drainage management areas?  | nage management areas?   |  | ► ON       |
| INPUT FOR WATERSHED: Enter watershed details and click on the Compute & Save button.   | click on the Compute & Save button.  |  |            |
| La. Name: Kudu Solar Project   |  |  |            |
| I.b. County: Kern ▼  |  |  |            |
| I.c. Closest Location: Mojave  |  |  |            |
| l.d. Size(acres): 4000   |  |  |            |
| Pre-Construction IMPUT   |  |  |            |
| Le. Dominant Soil Type:  | Group B Soils - Moderate infiltration. Silt loam or loam, Infiltration rate 0.15 to 0.3 inch/hr when wet.  |  |            |
| Lf. Existing Dominant Non-built Land Use Type:   | Natural Desert   |  |            |
| I.g. Existing rooftop impervious area(acres):  |  |  |            |
| I.h. Existing non-rooftop impervious area(acres):  |  |  |            |
| Post-Construction IMPUT  |  |  |            |
| I.i. Proposed Dominant Non-built Land Use Type:  | Natural Desert Landscape ▼   |  |            |
| I.j. Proposed rooftop impervious area(acres):  | 0  |  |            |
| I.k. Proposed non-rooftop impervious area(acres): 200  | 200  |  |            |
| Compute & Save   |  |  |            |
| OUTPUT:  |  |  |            |
| O.a. Existing Runoff Curve Number:   | 77   | O.d. Proposed Runoff Curve Number:             | 78.05      |
| O.b. Design Storm(inches):   | 0.5  | O.e. Net Credit of Volume Credits(Cubic feet): | 3329.99991 |
| O.c. Pre-project Runoff Volume(Cubic Feet):  | 0.00   | O.f. Post-project Runoff Volume(Cubic Feet):   | 0.00       |
| O.g. Post-project Runoff Volume minus Volume Credits(Cubic Feet):  | uits(Cubie -171.08   |  |            |
| ***Pre-project Runoff Volume >= Post-project Runoff Volume. No further calculation is necessary!   | . No further calculation is necessary!   |  |            |

# Appendix G Inflow Rates

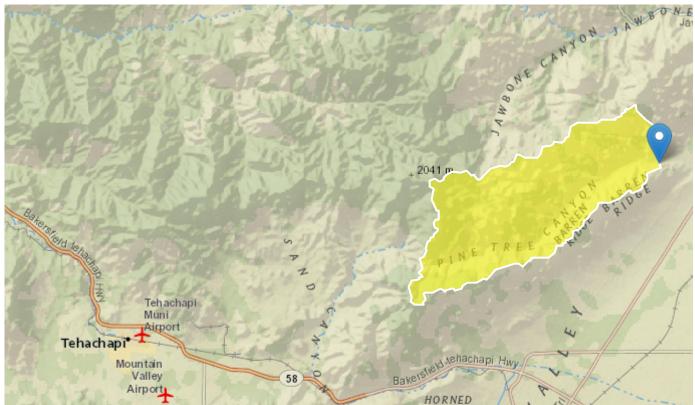
# **Inflow 1**

Region ID: CA

Workspace ID: CA20190326172345723000

Clicked Point (Latitude, Longitude): 35.23105, -118.08454

Time: 2019-03-26 11:24:00 -0600



| Basin Characteristics |   |       |              |
|-----------------------|---|-------|--------------|
| Parameter Code        | Parameter Description                   | Value | Unit         |
| DRNAREA               | Area that drains to a point on a stream | 34.2  | square miles |

| Peak-Flow Statistics Parameters [100 Percent (34.2 square miles) 2012 5113 Region 6 Dese | ertl |
|--|------|
|  |      |

| Parameter Code | Parameter Name | Value | Units        | Min Limit | Max Limit |
|----------------|----------------|-------|--------------|-----------|-----------|
| DRNAREA        | Drainage Area  | 34.2  | square miles | 0.04      | 173       |

Peak-Flow Statistics Flow Report [100 Percent (34.2 square miles) 2012 5113 Region 6 Desert]

PII: Prediction Interval-Lower, PIu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other -- see report)

| Statistic           | Value | Unit   | SEp |  |
|---------------------|-------|--------|-----|--|
| 2 Year Peak Flood   | 61.5  | ft^3/s | 214 |  |
| 5 Year Peak Flood   | 358   | ft^3/s | 226 |  |
| 10 Year Peak Flood  | 902   | ft^3/s | 248 |  |
| 25 Year Peak Flood  | 2410  | ft^3/s | 298 |  |
| 50 Year Peak Flood  | 4540  | ft^3/s | 357 |  |
| 100 Year Peak Flood | 8060  | ft^3/s | 444 |  |
| 200 Year Peak Flood | 13600 | ft^3/s | 575 |  |
| 500 Year Peak Flood | 25600 | ft^3/s | 856 |  |

### Peak-Flow Statistics Citations

Gotvald, A.J., Barth, N.A., Veilleux, A.G., and Parrett, Charles, 2012, Methods for determining magnitude and frequency of floods in California, based on data through water year 2006: U.S. Geological Survey Scientific Investigations Report 2012–5113, 38 p., 1 pl. (http://pubs.usgs.gov/sir/2012/5113/)

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Application Version: 4.3.0

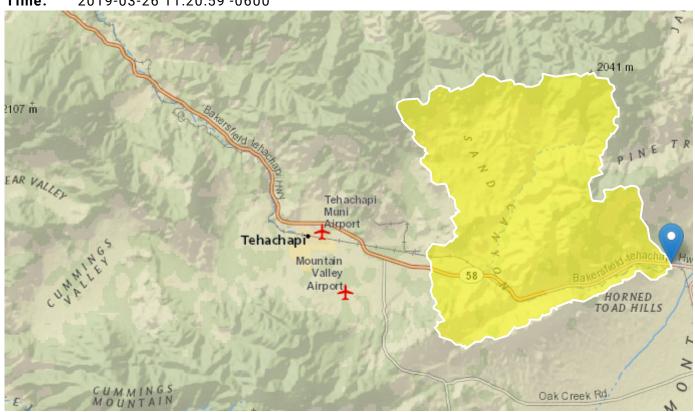
# Inflow 2

Region ID: CA

Workspace ID: CA20190326172044886000

Clicked Point (Latitude, Longitude): 35.11700, -118.19982

Time: 2019-03-26 11:20:59 -0600



| Basin Characteristics |   |       |              |
|-----------------------|---|-------|--------------|
| Parameter Code        | Parameter Description                   | Value | Unit         |
| DRNAREA               | Area that drains to a point on a stream | 69.9  | square miles |

| Parameter Code | Parameter Name | Value | Units        | Min Limit | Max Limit |
|----------------|----------------|-------|--------------|-----------|-----------|
| DRNAREA        | Drainage Area  | 69.9  | square miles | 0.04      | 173       |

Peak-Flow Statistics Flow Report [100 Percent (69.9 square miles) 2012 5113 Region 6 Desert]

Peak-Flow Statistics Parameters [100 Percent (69.9 square miles) 2012 5113 Region 6 Desert]

PII: Prediction Interval-Lower, PIu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other -- see report)

| Statistic           | Value | Unit   | SEp |
|---------------------|-------|--------|-----|
| 2 Year Peak Flood   | 88.3  | ft^3/s | 214 |
| 5 Year Peak Flood   | 515   | ft^3/s | 226 |
| 10 Year Peak Flood  | 1300  | ft^3/s | 248 |
| 25 Year Peak Flood  | 3460  | ft^3/s | 298 |
| 50 Year Peak Flood  | 6520  | ft^3/s | 357 |
| 100 Year Peak Flood | 11600 | ft^3/s | 444 |
| 200 Year Peak Flood | 19500 | ft^3/s | 575 |
| 500 Year Peak Flood | 36700 | ft^3/s | 856 |

### Peak-Flow Statistics Citations

Gotvald, A.J., Barth, N.A., Veilleux, A.G., and Parrett, Charles, 2012, Methods for determining magnitude and frequency of floods in California, based on data through water year 2006: U.S. Geological Survey Scientific Investigations Report 2012–5113, 38 p., 1 pl. (http://pubs.usgs.gov/sir/2012/5113/)

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Application Version: 4.3.0

# Inflow 3

Region ID: CA

Workspace ID: CA20190326172511217000

Clicked Point (Latitude, Longitude): 35.19725, -117.93514

Time: 2019-03-26 11:25:25 -0600



| Basin Characteristics |   |       |              |
|-----------------------|---|-------|--------------|
| Parameter Code        | Parameter Description                   | Value | Unit         |
| DRNAREA               | Area that drains to a point on a stream | 33.7  | square miles |

| Peak-Flow Statistics Parameters [2012 5113 Region 6 Desert] |                |       |              |           |           |
|---|----------------|-------|--------------|-----------|-----------|
| Parameter Code  | Parameter Name | Value | Units        | Min Limit | Max Limit |
| DRNAREA   | Drainage Area  | 33.7  | square miles | 0.04      | 173       |

Peak-Flow Statistics Flow Report [2012 5113 Region 6 Desert]

PII: Prediction Interval-Lower, PIu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other -- see report)

| Statistic           | Value | Unit   | SEp |
|---------------------|-------|--------|-----|
| 2 Year Peak Flood   | 61.1  | ft^3/s | 214 |
| 5 Year Peak Flood   | 356   | ft^3/s | 226 |
| 10 Year Peak Flood  | 895   | ft^3/s | 248 |
| 25 Year Peak Flood  | 2390  | ft^3/s | 298 |
| 50 Year Peak Flood  | 4510  | ft^3/s | 357 |
| 100 Year Peak Flood | 8000  | ft^3/s | 444 |
| 200 Year Peak Flood | 13500 | ft^3/s | 575 |
| 500 Year Peak Flood | 25400 | ft^3/s | 856 |

### Peak-Flow Statistics Citations

Gotvald, A.J., Barth, N.A., Veilleux, A.G., and Parrett, Charles, 2012, Methods for determining magnitude and frequency of floods in California, based on data through water year 2006: U.S. Geological Survey Scientific Investigations Report 2012–5113, 38 p., 1 pl. (http://pubs.usgs.gov/sir/2012/5113/)

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Application Version: 4.3.0

Table 5 - SUMMARY OF PEAK DISCHARGES

Peak Discharges (cfs)

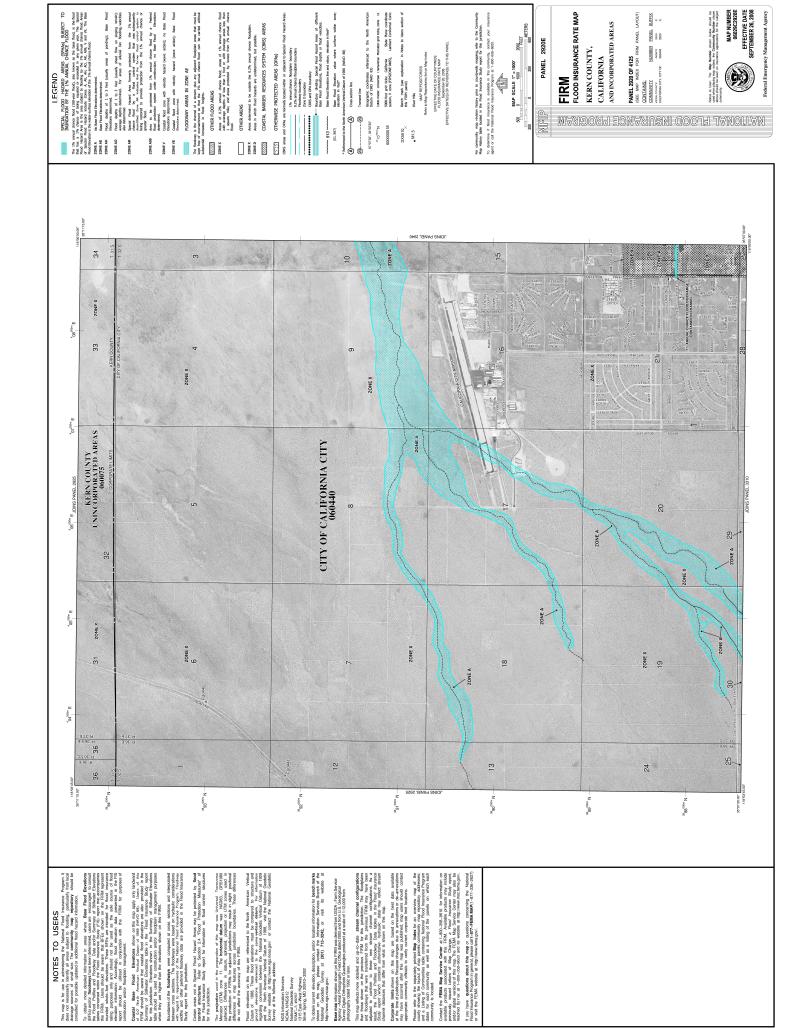
|                       | <u>ual-Chance</u>                     |   |  |                                  |                    |  |              |                 |             | 00                           |  |
|-----------------------|---------------------------------------|---|--|----------------------------------|--------------------|--|--------------|-----------------|-------------|------------------------------|--|
|                       | 0.2-Percent-Annual-Chance             | i   | ŀ  | ł                                |                    | 6,700  |              | 2,900           |             | 16,400                       |  |
|                       | 1-Percent-Annual-Chance               | 7,280   | 3,780  | 8,530                            |                    | 3,000  |              | 1,600           |             | 7,800                        |  |
| rean Discharges (C13) | 2-Percent-Annual-Chance               | f   | ł  | ł                                |                    | 2,000  |              | 1,200           |             | 5,300                        |  |
|                       | 10-Percent-Annual-Chance              | 1   | ;  | ;                                |                    | 580  |              | 520             |             | 1,900                        |  |
|                       | Drainage Area (sq. mi.)               | 14.2  | 7.7  | 16.8                             |                    | 3.6  |              | 14.0            |             | 163.4                        |  |
|                       | riodung source<br>and <u>Location</u> | 2,850 Feet above<br>Confluence with Kern<br>River | 11,000 Feet above<br>Confluence with Kern<br>River | At Confluence with Kern<br>River | Boron Avenue Creek | At Confluence with<br>Twenty Mule Team Creek | Breckenridge | At Fairfax Road | Cache Creek | At Downstream Limit of Study |  |

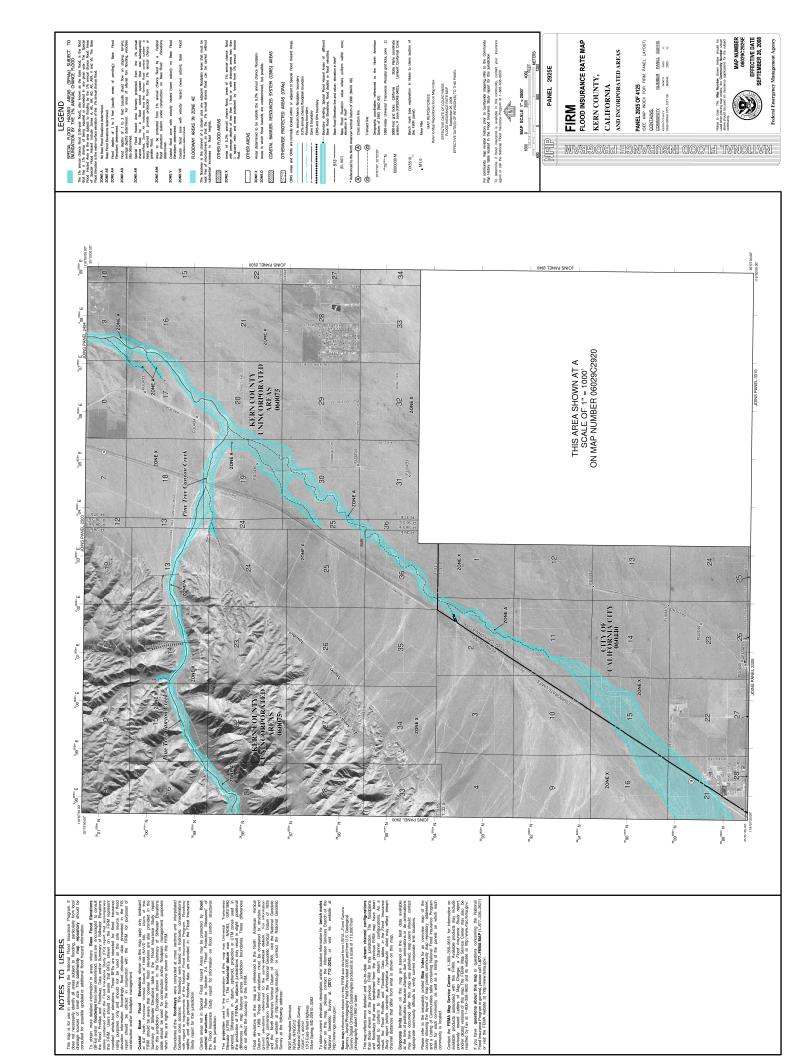
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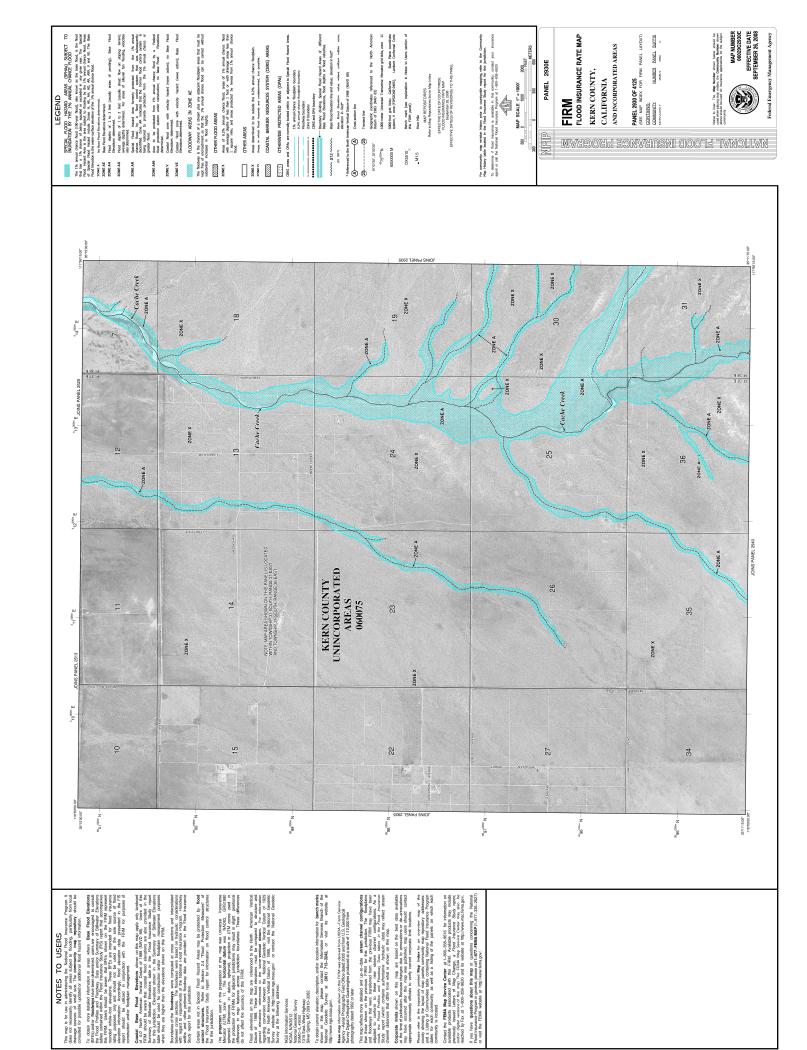
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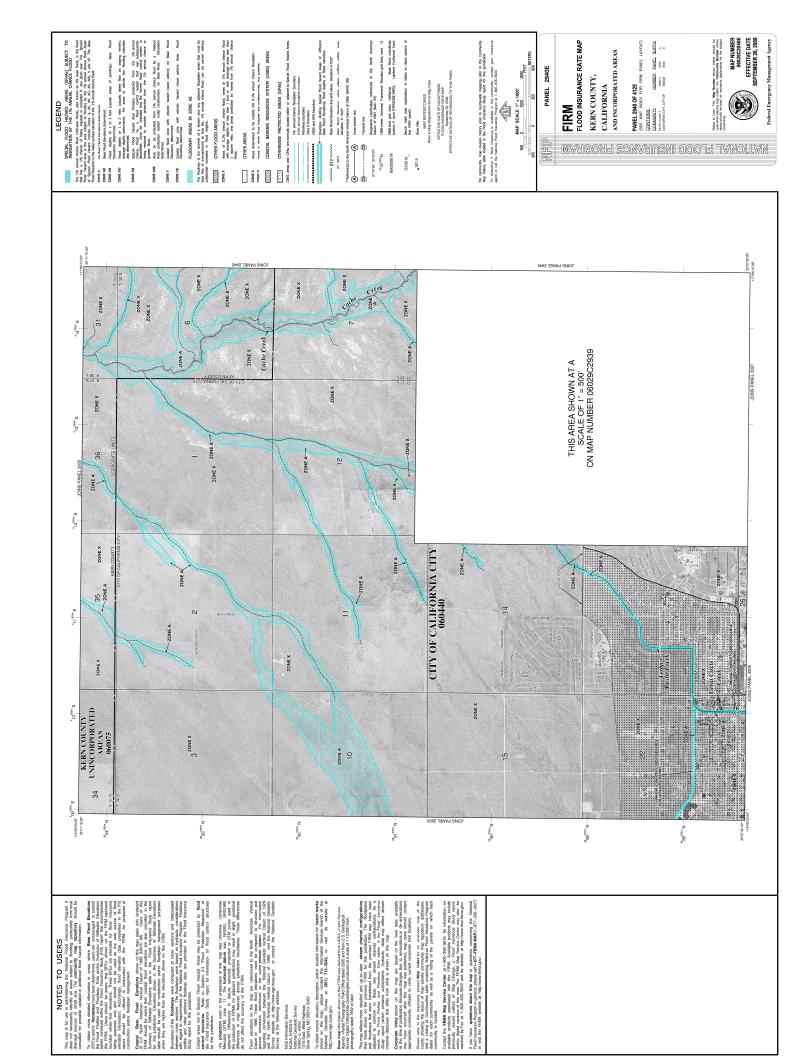
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# Appendix J Noise Study

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# Kudu Solar Farm Project

## Noise Study

prepared for

### 69SV 8me LLC

5455 Wilshire Boulevard, Suite 2010 Los Angeles, California 90036 Contact: Mr. Erec DeVost

### prepared by

Rincon Consultants, Inc. 449 15<sup>th</sup> Street, Suite 303 Oakland, California 94612

November 2021



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# **Table of Contents**

| 1  | Projec     | t Description  | 1  |  |  |
|----|------------|--|----|--|--|
|    | 1.1        | Introduction   | 1  |  |  |
|    | 1.2        | Project Site and Description   | 1  |  |  |
|    | 1.3        | Construction Activities  | 1  |  |  |
|    | 1.4        | Operational Activities   | 5  |  |  |
| 2  | Backgr     | ound   | 7  |  |  |
|    | 2.1        | Overview of Sound Measurement  | 7  |  |  |
|    | 2.2        | Vibration  |    |  |  |
|    | 2.3        | Existing Project Area Noise Levels   |    |  |  |
|    | 2.4        | Regulatory Setting   |    |  |  |
| 3  | Impac      | Analysis   | 16 |  |  |
|    | 3.1        | Methodology and Significance Thresholds  |    |  |  |
|    | 3.2        | Results  | 21 |  |  |
| 4  | Recom      | mendations   | 35 |  |  |
| 5  | Conclu     | sions  | 37 |  |  |
| 6  | References |  |    |  |  |
| Tc | ıbles      |  |    |  |  |
| Ta | ble 1      | Overall Project Construction Schedule  | 5  |  |  |
| Ta | ble 2      | Noise Monitoring Results in the Project Site Vicinity – Short Term               | 11 |  |  |
| Ta | ble 3      | Project Site Noise Monitoring Results – Long Term                                | 12 |  |  |
| Ta | ble 4      | California City Exterior Noise Standards   | 14 |  |  |
| Ta | ble 5      | Estimated Existing and Construction Vehicle Trips                                | 20 |  |  |
| Ta | ble 6      | Significance of Changes in Roadway Noise Exposure                                | 20 |  |  |
| Ta | ble 7      | Typical Construction Equipment Noise Levels                                      | 22 |  |  |
| Ta | ble 8      | Noise Levels at Various Distances from Construction at the Project Parcels       | 23 |  |  |
| Ta | ble 9      | Typical Construction Noise Levels at Various Distances from Gen-Tie Construction | 24 |  |  |
| Ta | ble 10     | Combined Construction Noise Levels for Worst-Case Scenario <sup>1</sup>          | 26 |  |  |
| Ta | ble 11     | Construction Traffic Noise   | 27 |  |  |
| Ta | ble 12     | Estimated Noise Rating for Equipment Utilized During Project Operations          | 28 |  |  |
| Ta | ble 13     | Operational Noise Levels at Nearest Sensitive Receivers                          | 29 |  |  |
|    |            |  |    |  |  |

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### Kudu Solar Farm Project

### Figures

| Figure 1 | Regional Location  | 3  |
|----------|--|----|
| _        | Project Location   |    |
| · ·      | Noise Measurement Locations                                    |    |
| Figure 4 | Locations of Noise-Sensitive Receptors Closest to Project Site | 18 |
| Figure 5 | Receiver Locations and Operational Noise Contours              | 31 |

### **Appendices**

Appendix A On-Site Noise Measurement Data

Appendix B Roadway Construction Noise Model (RCNM) Results

# 1 Project Description

### 1.1 Introduction

This study analyzes the potential noise impacts of the proposed Kudu Solar Farm Project (Project) located within the unincorporated Kern County and within California City. Rincon Consultants, Inc. (Rincon) prepared this study under contract to 8minute Solar Energy, LLC for use by Kern County, the lead agency. The study evaluates the short- and long-term impacts of the Project to noise-sensitive receivers.

### 1.2 Project Site and Description

The Project site is located in unincorporated Kern County and a northern section of the California City. The area is a relatively flat desert landscape. The majority of the Project is bisected by Washburn Boulevard (which is also the California City boundary) and Neuralia Road. The westernmost portion of the Project is located approximately one mile east of State Route 14 (SR 14); the southernmost portion of the Project is located approximately 500 feet north of the California City Municipal Airport; the easternmost portion of the Project is located just east of 90<sup>th</sup> Street in California City; and the northernmost portion of the Project is located just north of Harriet Avenue in Kern County. The Project includes 75 parcels totaling approximately 1,955 gross acres. Figure 1 and Figure 2 show the regional location and immediate vicinity of the Project site, respectively.

This Project description is abbreviated, focusing on elements of the proposed solar facility that are most relevant for the noise analysis. On the parcels, the Project would use solar photovoltaic (PV) panels or modules on mounting frameworks to convert sunlight directly into electricity. This electricity would be delivered from the panels to inverter stations, where the electricity would be converted from direct current (DC) to alternating current (AC). Each parcel may also include an operations and maintenance (O&M) building, substations, energy storage systems, and/or transmission facilities, as necessary. In addition to the solar PV sites, the Project would include a gentie corridor to deliver power from the solar facility to the electrical grid. This corridor would run to a dedicated Project substation, or to the Eland 1 Substation. The Project may also share the Eland 1 generation tie-line (gen-tie) facilities, or gen-tie rights-of-way. The Eland 1 substation and gen-tie line have gone through environmental analysis and subsequent approval by Kern County and are not part of the Project (Kern County 2018).

### 1.3 Construction Activities

Construction of all Project components would occur over approximately 12 to 18 months beginning as early as the fourth quarter of 2021 (i.e., October 1, 2021). Construction of the Project would include the following types of activities:<sup>1</sup>

Noise Study

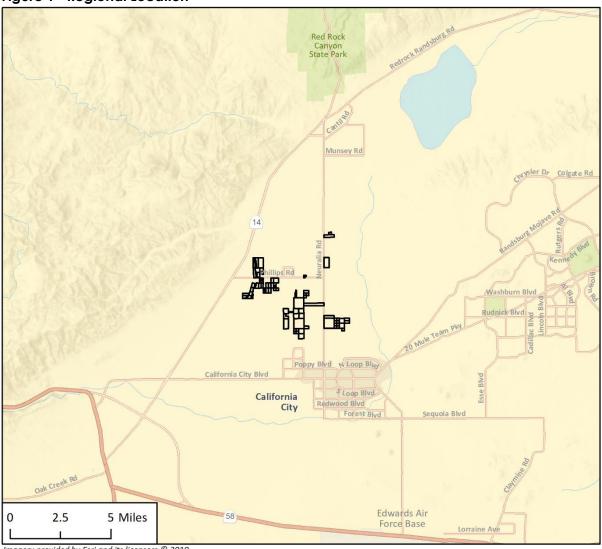
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<sup>&</sup>lt;sup>1</sup> This list of types of construction activities is presented without respect to the phasing of construction over time.

# 69SV 8me LLC Kudu Solar Farm Project

- Site preparation
- Grading and earthwork
- Concrete foundations

Figure 1 Regional Location

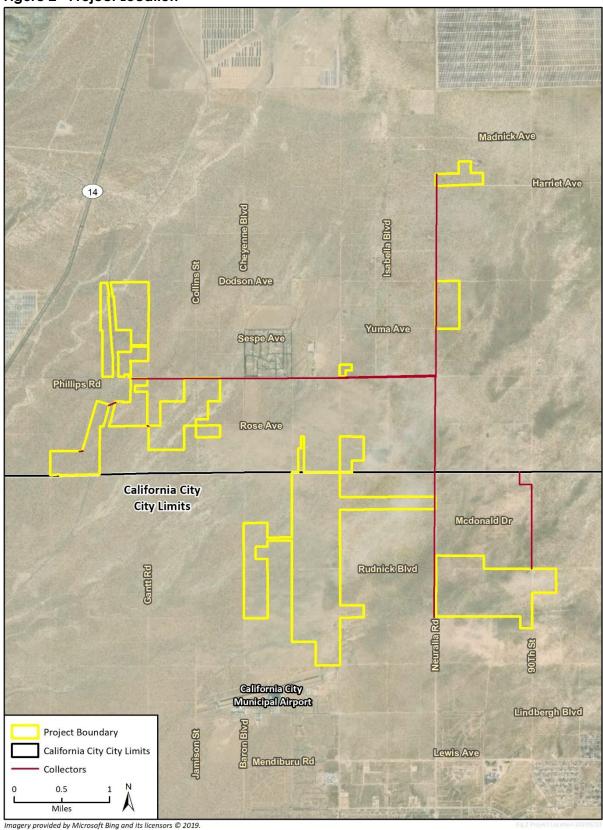


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Figure 2 Project Location



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- Structural steel work
- Electrical/instrumentation work
- Collector line installation
- Architecture and landscaping

Each Project parcel may be constructed simultaneously and phases of construction would overlap.

Table 1 shows the construction schedule, number of workdays, and overlapping phases that were assumed in the following analysis.

Table 1 Overall Project Construction Schedule

|                                      | WorkMonth |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |
|--------------------------------------|-----------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|
| Phase                                | Days      | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| Phase 1: Site preparation & Grading  | 86        |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |
| Phase 2: Tracker Foundations (Piles) | 150       |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |
| Phase 3: Underground Cabling         | 150       |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |
| Phase 4: Mechanical Installation     | 175       |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |
| Phase 5: Electrical Installation     | 200       |   |   |   |   |   |   |   |   |   |    |    |    |    |    |    |

Note: Construction schedule of 15 months is the average time estimated by the applicant for the construction period (i.e., 12 to 18 months).

Construction traffic would access the Project from Philips Road, Gantt Road, and Neuralia Road, or through the Eland 1 Project site. It is estimated that up to 1,000 workers per day (during peak construction periods) would be required during the construction of the Project. On-road traffic would consist of employee and vendor vehicle trips. The number of vehicle trips would vary by month depending on the construction activities.

Heavy construction is expected to occur between 6:00 AM and 5:00 PM, Monday through Friday. Additional hours may be necessary to make-up schedule deficiencies or to complete critical construction activities. Some activities may continue 24 hours per day, seven days per week. Nighttime activities could include, but are not limited to, refueling equipment, staging material for the following day's construction activities, quality assurance/control, and commissioning.

Materials and supplies would be delivered to the Project site by truck. Truck deliveries would normally occur during daylight hours. However, there could be offloading and/or transporting of materials to the Project site on weekends and during evening hours.

Earthmoving activities are expected to be limited to the construction of access roads, O&M buildings, substations, energy storage systems, and storm water protection or storage (detention) facilities. Final grading may include revegetation with low lying grass or applying earth-binding materials to disturbed areas.

# 1.4 Operational Activities

Once completed, the Project would generally be limited to the following maintenance activities:

- Cleaning PV panels
- Monitoring electricity generation

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#### Kudu Solar Farm Project

- Providing site security
- Maintaining the facility: replacing or repairing inverters, wiring, and PV modules

The Project would operate continuously, seven days a week, until the anticipated repowering or decommissioning of the Project in 30 to 40 years. It is expected that the Project would require an operational staff of up to 20 full-time employees. The Project may share an O&M, substation, and/or transmission facilities with one or more nearby energy projects, which could reduce the proposed Project's on-site operational staff. Maintenance activities may occur seven days a week, 24 hours a day to ensure PV panel output when solar energy is available.

# 2 Background

### 2.1 Overview of Sound Measurement

Sound is a vibratory disturbance created by a moving or vibrating source, which is capable of being detected by the hearing organs. Noise is defined as sound that is loud, unpleasant, unexpected, or undesired and may therefore be classified as a more specific group of sounds. The effects of noise on people can include general annoyance, interference with speech communication, sleep disturbance, and, in the extreme, hearing impairment (Caltrans 2013).

In technical terms, sound levels are described as either a "sound power level" or a "sound pressure level," which while easily confused are two distinct characteristics of sound. Both share the same unit of measure, the decibel (dB). However, the sound power level, expressed as L<sub>w</sub>, is the energy converted into sound by the source. As sound energy travels through the air, it creates a sound wave in the air that exerts pressure on receivers such as an eardrum or microphone, the SPL. Sound measurement instruments only measure SPL, and limits used in standards are generally SPL. Modeling uses the L<sub>w</sub> of equipment to calculate the SPL at a distance.

Noise levels are commonly measured in dB using the A-weighted sound pressure level (dBA). The A-weighting scale is an adjustment to the actual sound pressure levels so that they are consistent with the human hearing response, which is most sensitive to frequencies around 4,000 Hertz and less sensitive to frequencies around and below 100 Hertz (Kinsler, et. al. 1999). Decibels are measured on a logarithmic scale that quantifies sound intensity in a manner similar to the Richter scale used to measure earthquake magnitudes. A doubling of the energy of a noise source, such as doubling of traffic volume, would increase the noise level by 3 dB; dividing the energy in half would result in a 3 dB decrease (Crocker 2007).

Human perception of noise has no simple correlation with sound energy: the perception of sound is not linear in terms of dBA or in terms of sound energy. Two sources do not "sound twice as loud" as one source. It is widely accepted that the average healthy ear can barely perceive changes of 3 dBA, increase or decrease (i.e., twice the sound energy); that a change of 5 dBA is readily perceptible (8 times the sound energy); and that an increase (or decrease) of 10 dBA sounds twice (half) as loud ([10.5x the sound energy] Crocker 2007).

Sound changes in both level and frequency spectrum as it travels from the source to the receiver. The most obvious change is the decrease in level as the distance from the source increases. The manner by which noise reduces with distance depends on factors such as the type of sources (e.g., point or line, the path the sound will travel, site conditions, and obstructions). Noise levels from a point source typically attenuate, or drop off, at a rate of 6 dBA per doubling of distance (e.g., construction, industrial machinery, ventilation units). Noise from a line source (e.g., roadway, pipeline, railroad) typically attenuates at about 3 dBA per doubling of distance (Caltrans 2013). The propagation of noise is also affected by the intervening ground, known as ground absorption. A hard site, such as a parking lot or smooth body of water, receives no additional ground attenuation and the changes in noise levels with distance (drop-off rate) result from simply the geometric spreading of the source. An additional ground attenuation value of 1.5 dBA per doubling of distance applies to a soft site (e.g., soft dirt, grass, or scattered bushes and trees) (Caltrans 2013). Noise levels may also be reduced by intervening structures; the amount of attenuation provided by this "shielding" depends on the size of the object and the frequencies of the noise levels. Natural terrain features such as hills and dense

#### Kudu Solar Farm Project

woods, and man-made features such as buildings and walls, can significantly alter noise levels. Generally, any large structure blocking the line of sight will provide at least a 5-dBA reduction in source noise levels at the receiver (Federal Highway Administration [FHWA] 2017). Structures can substantially reduce exposure to noise as well. The FHWA's guidelines indicate that modern building construction generally provides an exterior-to-interior noise level reduction of 20 to 35 dBA with closed windows.

The impact of noise is not a function of loudness alone. The time of day when noise occurs and the duration of the noise are also important factors of Project noise impact. Most noise that lasts for more than a few seconds is variable in its intensity. Consequently, a variety of noise descriptors have been developed. One of the most frequently used noise metrics is the equivalent noise level ( $L_{eq}$ ); it considers both duration and sound power level.  $L_{eq}$  is defined as the single steady A-weighted level equivalent to the same amount of energy as that contained in the actual fluctuating levels over time. Typically,  $L_{eq}$  is summed over a one-hour period.  $L_{max}$  is the highest root mean squared (RMS) sound pressure level within the sampling period, and  $L_{min}$  is the lowest RMS sound pressure level within the measuring period (Crocker 2007).

Noise that occurs at night tends to be more disturbing than that occurring during the day. Community noise is usually measured using Day-Night Average Level ( $L_{dn}$ ), which is the 24-hour average noise level with a +10 dBA penalty for noise occurring during nighttime (10:00 PM to 7:00 AM) hours. The relationship between the peak-hour  $L_{eq}$  value and the  $L_{dn}$  depends on the distribution of traffic during the day, evening, and night.

### 2.2 Vibration

Groundborne vibration of concern in environmental analysis consists of the oscillatory waves that move from a source through the ground to adjacent structures. The number of cycles per second of oscillation makes up the vibration frequency, described in terms of Hz. The frequency of a vibrating object describes how rapidly it oscillates. The normal frequency range of most groundborne vibration that can be felt by the human body starts from a low frequency of less than 1 Hz and goes to a high of about 200 Hz (Crocker 2007).

While people have varying sensitivities to vibrations at different frequencies, in general they are most sensitive to low-frequency vibration. Vibration in buildings, such as from nearby construction activities, may cause windows, items on shelves, and pictures on walls to rattle. Vibration of building components can also take the form of an audible low-frequency rumbling noise, referred to as groundborne noise. Groundborne noise is usually only a problem when the originating vibration spectrum is dominated by frequencies in the upper end of the range (60 to 200 Hz), or when foundations or utilities, such as sewer and water pipes, physically connect the structure and the vibration source (Federal Transit Administration [FTA] 2018). Although groundborne vibration is sometimes noticeable in outdoor environments, it is almost never annoying to people who are outdoors. The primary concern from vibration is that it can be intrusive and annoying to building occupants and vibration-sensitive land uses.

Vibration energy spreads out as it travels through the ground, causing the vibration level to diminish with distance away from the source. High-frequency vibrations diminish much more rapidly than low frequencies, so low frequencies tend to dominate the spectrum at large distances from the source. Discontinuities in the soil strata can also cause diffractions or channeling effects that affect the propagation of vibration over long distances (Caltrans 2020). When a building is impacted by vibration, a ground-to-foundation coupling loss will usually reduce the overall vibration level.

However, under rare circumstances, the ground-to-foundation coupling may actually amplify the vibration level due to structural resonances of the floors and walls.

Vibration amplitudes are usually expressed in peak particle velocity (PPV) or root mean squared (RMS) vibration velocity. The PPV and RMS velocity are normally described in inches per second (in./sec.). PPV is defined as the maximum instantaneous positive or negative peak of a vibration signal. PPV is often used in monitoring of blasting vibration because it is related to the stresses that are experienced by buildings (Caltrans 2020).

## 2.3 Existing Project Area Noise Levels

The Project site is located in a rural desert environment with scattered rural residential uses. The primary sources of noise on-site and in the surrounding area include motor vehicles, wind, and fauna (birds, small mammals, etc.). The greatest vehicle noise would occur from vehicles on the main thoroughfares (SR 14, Philips Road, and Neuralia Road). Additional noise sources in the area include aircraft associated with the California City Municipal Airport.

To evaluate existing noise levels in the area, four 15-minute noise measurements (ST1 through ST4) and two 24-hour noise measurements (LT1 and LT2) were taken on and near the Project site on September 18 and 19, 2019, using an ANSI Type II integrating sound level meter. Figure 3 shows the locations of the noise measurements. The noise measurement locations were chosen to provide a representative range of ambient noise levels across the Project site and in the nearby area, especially near existing noise-sensitive residences and roadways. The short-term noise measurement results are shown in Table 2 and the long-term results are shown in Table 3. Detailed noise meter outputs are included in Appendix A.

Figure 3 Noise Measurement Locations

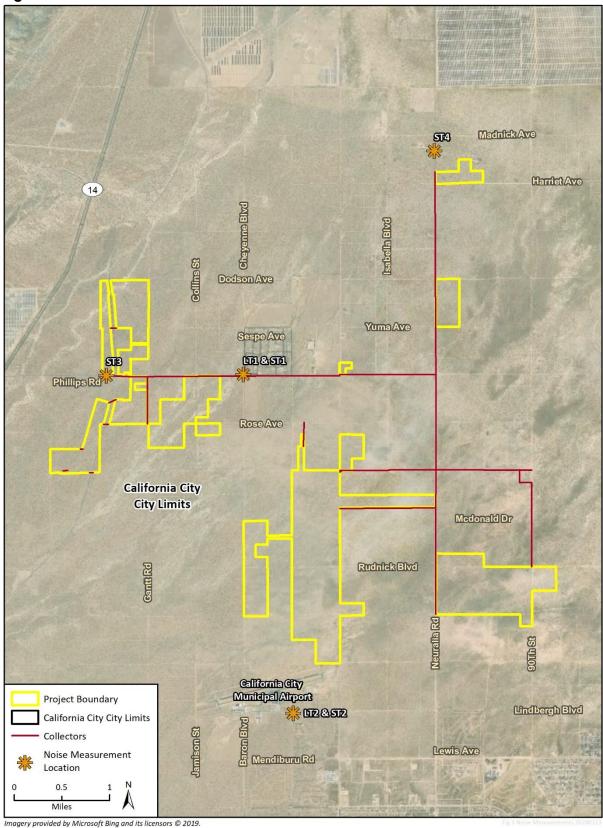


Table 2 Noise Monitoring Results in the Project Site Vicinity – Short Term

| Measurement<br>Number | Measurement Location  | Sample Times        | Approximate Distance to Primary Noise Source                         | Noise<br>Level<br>(dBA L <sub>eq</sub> ) <sup>1</sup> |
|-----------------------|---|---------------------|--|---|
| 1                     | Cheyenne Boulevard/Phillips Road in<br>Kern County (LT1 Location)         | 12:31 PM – 12:46 PM | 40 feet from<br>centerline of Phillips<br>Road                       | 51  |
| 2                     | Mitchell Boulevard/Lindbergh<br>Boulevard, California City (LT2 location) | 11:32 AM – 11:47 AM | 90 feet from<br>centerline of<br>Lindbergh Boulevard                 | 52  |
| 3                     | Phillips Road near Sage Street in Kern<br>County                          | 1:43 PM – 1:58 PM   | 25 feet from<br>centerline of from<br>centerline of Phillips<br>Road | 55  |
| 4                     | Neuralia Road and Esther Avenue   | 1:02 PM – 1:17 PM   | 30 feet from center of<br>Neuralia Road                              | 63  |

See Figure 3 for Noise Measurement Locations.

Source: Rincon Consultants, field measurements conducted on September 18, 2019, using ANSI Type II Integrating sound level meter. See Appendix A.

 $<sup>^1</sup>$  The equivalent noise level (Leq) is defined as the single steady A-weighted level that is equivalent to the same amount of energy as that contained in the actual fluctuating levels over a period of time (essentially, the average noise level). For these measurements, the Leq was over a 15-minute period.

Table 3 Project Site Noise Monitoring Results – Long Term

| Sample Time          | $dBA\;L_{eq}$              | Sample Time                               | dBA L <sub>eq</sub> |
|----------------------|----------------------------|---|---------------------|
| LT1 - Cheyenne Bou   | levard/Phillips Road in Ke | rn County, September 18-19, 2019          |                     |
| 12:28 PM             | 63                         | 12:28 AM                                  | 58                  |
| 1:28 PM              | 62                         | 1:28 AM                                   | 41                  |
| 2:28 PM              | 64                         | 2:28 AM                                   | 52                  |
| 3:28 PM              | 63                         | 3:28 AM                                   | 49                  |
| 4:28 PM              | 61                         | 4:28 AM                                   | 54                  |
| 5:28 PM              | 60                         | 5:28 AM                                   | 51                  |
| 6:28 PM              | 55                         | 6:28 AM                                   | 41                  |
| 7:28 PM              | 49                         | 7:28 AM                                   | 44                  |
| 8:28 PM              | 50                         | 8:28 AM                                   | 59                  |
| 9:28 PM              | 51                         | 9:28 AM                                   | 60                  |
| 10:28 PM             | 44                         | 10:28 AM                                  | 61                  |
| 11:28 PM             | 51                         | 11:28 AM                                  | 61                  |
|                      |                            | 24-hour Noise Level                       | 58                  |
| LT2 - Mitchell Boule | vard/Lindbergh Boulevard   | d, California City, September 18-19, 2019 |                     |
| 11:31 AM             | 51                         | 11:31 PM                                  | 56                  |
| 12:31 PM             | 51                         | 12:31 AM                                  | 52                  |
| 1:31 PM              | 51                         | 1:31 AM                                   | 32                  |
| 2:31 PM              | 52                         | 2:31 AM                                   | 31                  |
| 3:31 PM              | 49                         | 3:31 AM                                   | 35                  |
| 4:31 PM              | 54                         | 4:31 AM                                   | 41                  |
| 5:31 PM              | 49                         | 5:31 AM                                   | 55                  |
| 6:31 PM              | 47                         | 6:31 AM                                   | 44                  |
| 7:31 PM              | 51                         | 7:31 AM                                   | 60                  |
| 8:31 PM              | 47                         | 8:31 AM                                   | 54                  |
| 9:31 PM              | 46                         | 9:31 AM                                   | 57                  |
| 10:31 PM             | 48                         | 10:31 AM                                  | 52                  |
|                      |                            | 24-hour Noise Level                       | 52                  |

Source: Rincon Consultants, field measurements conducted on September 18 and 19, 2019, using ANSI Type II Integrating sound level meter. See Appendix A.

## 2.4 Regulatory Setting

### Kern County

The Noise Element of the Kern County General Plan, which was adopted in 2004 and last updated in 2009, sets goals and policies that guide the physical development of the unincorporated areas under the County's discretionary land use authority. These goals include ensuring residents of Kern County are protected from excessive noise, moderate levels of noise are maintained in the County, and ensuring the protection of the economic base of Kern County by preventing the encroachment of incompatible land uses near known noise producing roadways, industries, railroads, airports, oil and gas extraction, and other sources. To help achieve these goals, the Noise Element includes policy requirements for new noise-sensitive land uses, noise level criteria, and enforcing the State Noise Insulation Standards.

Implementation Measure F in the Noise Element, as follows, would apply the Project, limiting the exposure of sensitive land uses to exterior noise:

Require proposed commercial and industrial uses or operations to be designed or arranged so
that they will not subject residential or other noise sensitive land uses to exterior noise levels in
excess of 65 dB Ldn and interior noise levels in excess of 45 dB Ldn.

Pursuant to Policy 5, the exterior noise standard applies to outdoor activity areas at sensitive land uses:

- Prohibit new noise-sensitive land uses in noise-impacted areas unless effective mitigation measures are incorporated into the project design. Such mitigation shall be designed to reduce noise to the following levels:
  - a) 65 dB Ldn or less in outdoor activity areas;
  - b) 45 dB Ldn or less within interior living spaces or other noise sensitive interior spaces.

Operation of the proposed solar energy Project would be subject to these County standards.

Noise issues are also addressed in Chapter 8.36 of the Kern County Code. These include acceptable hours of construction and limitations on construction related noise impacts on adjacent sensitive receptors. Noise-producing construction activities that are audible to a person with average hearing ability at a distance of 150 feet from a construction site, if the site is within 1,000 feet of an occupied residential dwelling, are prohibited between the hours of 9:00 PM to 6:00 AM on weekdays, and 9:00 PM to 8:00 AM on weekends. However, the following exceptions are permitted:

- 1. The resource management director or his designated representative may for good cause exempt some construction work for a limited time.
- 2. Emergency work is exempt from this section.

Kern County has not adopted specific policies or standards pertaining to vibration.

### California City

Article 4, *Noise and Vibration*, of California City's Municipal Code contains operational noise limits for exterior and interior areas. Exterior noise standards are shown in Table 4. In addition to the exterior noise standards, the interior noise standard in California City is 55 dBA from 7:00 AM to 10:00 PM and 45 dBA from 10:00 PM to 7:00 AM.

Table 4 California City Exterior Noise Standards

|            |   | Allowable Exterior N | Noise Level (dBA L <sub>eq</sub> ) |
|------------|---|----------------------|------------------------------------|
| Noise Zone | Noise Zone Definition (Type of Land Use)  | 7:00 AM to 10:00 PM  | 10:00 PM to 7:00 AM                |
| I          | Single, double and multiple family residential properties located at a distance more than 600 feet from a major roadway             | 50                   | 45                                 |
| II         | Single, double and multiple family residential properties located at a distance equal to or less than 600 feet from a major roadway | 55                   | 50                                 |
| III        | Commercial properties   | 65                   | 60                                 |
| IV         | Manufacturing or industrial properties  | 70                   | 70                                 |

- No person shall create noise, or allow the creation of noise on property owned, leased, occupied or otherwise controlled by such person, which causes the noise level when measured on other property to exceed:
  - The noise standard for a cumulative period of more than thirty minutes in any hour; or
  - The noise standard plus 5 dBA for a cumulative period of more than fifteen minutes in any hour; or
  - The noise standard plus 10 dBA for a cumulative period of more than five minutes in any hour; or
  - The noise standard plus 15 dBA for a cumulative period of more than one minute in any hour; or
  - The noise standard plus 20 dBA for any period of time.
- If the ambient noise level exceeds any of the above five noise limit categories, the cumulative period applicable to the category shall be increased to reflect the noise level.
- Each of the noise limits specified above shall be reduced by 5 dBA for impact or simple tone noises, or for noises consisting of speech or music.
- If the measurement location is on a boundary between two different noise zones, the lower noise level standard applicable to the noise zone shall apply.
- If the intruding noise source is continuous and cannot reasonably be discontinued or stopped for a time period whereby the ambient noise level can be determined, the measured noise level obtained while the source is in operation shall be compared directly to the allowable noise level standards as specified respective to the measurement location's designated land use and for the time of day the noise level is measured.

Source: Section 5-1.405 of the California City Municipal Code

Per Section 5-1.407 of the California City Municipal Code, noise sources associated with or vibration created by construction, repair or remodeling of real property or during authorized seismic surveys are exempt from the above standards under the following conditions:

- The activities occur between the hours of 6:00 AM and 8:00 PM between May 15 and September 15 of each year or between the hours of 7:00 AM and 8:00 PM during the remainder of the year.
- The activities do not take place on Sundays or federal holidays.
- The noise level created by such activities does not exceed 60 dBA plus the limits specific herein as measured on residential property; and
- A vibration does not endanger the public health, welfare and safety.

Per Section 5-1.412 and 5.1-413 of the California City Municipal Code, if the generator of noise is unable to comply with the above standards (e.g., performing construction activities outside of the allowed hours), the owner or operator of a noise or vibration source may file an application with the Health Officer for a variance. The owner or operator shall set forth actions taken to comply with the reasons why immediate compliance cannot be achieved, a proposed method of achieving compliance, and a proposed time schedule for accomplishment. The application shall be accompanied by a fee in the amount established from time to time by resolution. A separate

application shall be filed for each noise source. Several mobile sources under common ownership, or several fixed sources on a single property may be combined into one application. Upon receipt of the application and fee, the Health Officer shall refer it with a recommendation within 30 days to the Planning Commission. The Planning Commission will consider the variance with the following:

- The magnitude of nuisance caused by the offensive noise;
- The uses of property within the area of impingement by the noise;
- The time factors related to study, design, financing and construction of remedial work;
- The economic factors related to age and useful life of the equipment; and
- The general public interest, welfare and safety.

Section 5-1.410 of the California City Municipal Code outlines the vibration standards, which states that no person shall create, maintain or cause ground vibration perceptible without instruments at any point on adjoining property. The perception threshold shall be presumed to be more than 0.05 in./sec. RMS vertical velocity.

# 3 Impact Analysis

# 3.1 Methodology and Significance Thresholds

To assess the potential for temporary construction and long-term operational noise impacts, noise-sensitive receivers closest to the Project site were identified. Figure 4 shows the general locations of noise-sensitive receivers used in the analysis. The Project parcels are generally located in a rural area, with nearby noise-sensitive receivers being single-family residences. The nearest residences in Kern County are approximately 50feet from Project parcels and the nearest residences in California City are approximately 3,250 feet from the southernmost Project parcel (see Table 5). Some of the proposed routes for the gen-tie corridor would run adjacent to noise-sensitive receivers in a single-family residential neighborhood north of Phillips Road. For the analysis, it is assumed that gen-tie corridor construction would occur within 50 feet of noise-sensitive receivers. Noise-sensitive receivers would be located no closer to the project site that the polygons used in Figure 4 to delineate the boundaries of the nearest receptors such as residences and parks. Receivers and distances are shown in Table 5.

Table 5 Modeled Distances of Noise-Sensitive Receivers to Project Site

| Receiver <sup>1</sup>          | Description                           | Jurisdiction    | Approximate Modeled Distance to<br>Project Site |
|--------------------------------|---------------------------------------|-----------------|---|
| R1                             | Esther Ave Residence                  | Kern County     | 1,700   |
| R2                             | Isabella Blvd Residence               | Kern County     | 3,300   |
| R3                             | Near Dodson Ave and Isabella Blvd     | Kern County     | 3,500   |
| R4                             | Yerba Blvd Residence                  | Kern County     | 1,300   |
| R5                             | Southeast Phillips Rd Residence       | Kern County     | 2,100   |
| R6                             | Southwestern Phillips Rd Residence    | Kern County     | 3,000   |
| R7                             | Residence south of Lindbergh          | California City | 3,250   |
| R8                             | Denhart Ave Residence                 | California City | 6,700   |
| R9                             | Possible Residence near Neuralia Road | Kern County     | 50  |
| R10                            | Possible Residence near Neuralia Road | Kern County     | 50  |
| <sup>1</sup> Receiver location | s shown in Figure 4.                  |                 |   |

Due to the large distance included in noise modeling between Project activities that generate noise and the nearest noise-sensitive receivers (e.g., located from 1,200 feet up to several miles from Project activities), the accuracy of the models compared to real world conditions is uncertain. This is because the models assume perfect travel of noise with standard atmospheric attenuation, while in the real world complicating variables would occur that the models are unable to or inaccurately able to capture (e.g., interference with other noise sources, curvature of the earth, complicated atmospheric or topographical conditions, etc.). Therefore, with the simplicity of the models and the complicated variables that come into play with large distances between a noise source and a receiver, the modeling results at these distances should be considered theoretical in nature.

Exposure of the proposed solar facility to ambient noise was not evaluated because the solar facility would not be a noise-sensitive land use.

### Construction and Decommissioning Noise

The FHWA's software program Roadway Construction Noise Model (RCNM) was used to estimate construction noise at nearby sensitive receptors. Construction noise modeling results are provided in Appendix B. The types of construction equipment that would be used on-site were provided by 8minute Solar Energy. RCNM provides reference noise levels at the standard distance of 50 feet and estimates noise levels at nearby sensitive receivers based on a standard noise attenuation rate of 6 dB per doubling of distance (line-of-sight method of sound attenuation for point sources of noise such as construction equipment). Although construction activity would typically take place in the interior of Project parcels, this analysis conservatively assumes that equipment may be used along the boundaries of Project parcels facing the nearest noise-sensitive receivers. In addition, RCNM does not consider topography or other environmental factors that attenuate noise. The average noise levels (Leq) from all combined equipment were modeled at the nearest noise-sensitive receivers. Noise levels were modeled from the use of equipment at individual Project parcels and the gen-tie corridor, as well as from multiple sites simultaneously under construction.

On-site construction noise would cause a significant impact if it occurs outside of the County's permitted hours of 6:00AM to 9:00 PM on weekdays and 8:00 AM to 9:00 PM on weekends, within 1,000 feet of an occupied residential dwelling, unless the applicant obtains an exemption to

Madnick Ave Harriet Ave 14 **Gheyenne Blyd** Isabella Blvd Yuma Ave Sespe Ave Rose Ave **California City City Limits** Mcdonald Dr Rudnick Blvd California City Municipal Airport Lindbergh Blvd JamisonSt Lewis Ave **Project Boundary** California City City Limits Collectors Sensitive Receiver Location 0.75 Miles

Figure 4 Locations of Noise-Sensitive Receptors Closest to Project Site

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prohibited nighttime construction noise pursuant to Chapter 8.36 of the Kern County Code and implements a noise control plan to reduce nighttime construction noise. On-site construction noise would also create a significant impact if it exceeds California City's 60 dBA construction noise limit. In addition, a significant impact may occur if daytime construction activity results in extremely high noise levels that could be detrimental to the health and safety of nearby residents.

As stated in Section 1.2, *Project Site and Description*, at the end of the Project's useful life (anticipated to be 30-40 years), the proposed solar facility and associated infrastructure would be decommissioned in accordance with then-current decommissioning practices. At this time, it is not possible to quantitatively evaluate potential noise that would result from Project decommissioning, due to the uncertainty of when decommissioning would occur and the technology or construction practices that would be available at that time. Therefore, based on current decommissioning practices and as a reasonable worst-case scenario, this analysis assumes that noise impacts generated during future decommissioning would be similar to noise impacts generated during the construction phase of the Project.

### **Construction Traffic Noise**

Noise levels from existing traffic and with-construction traffic along SR 14, Phillips Road, and Neuralia Road were estimated in terms of peak-hour L<sub>eq</sub> using the Traffic Noise Model, Version 2.5 (TNM 2.5) (FHWA 2004). The model calculations are based on estimates of existing vehicle trips collected by Kern Council of Governments in 2017, and from Caltrans traffic counts taken in 2017 for SR 14. Vehicle trips generated by Project construction activities are estimated by traffic volumes provided in the Aratina Solar Project Traffic Impact Analysis (EPD Solutions, Inc. 2019), a similar project in the region. The Aratina Solar Project also assumed up to 1,000 workers during peak construction periods; which would occur during the overlap of concrete foundations, structural steel work, and electrical/instrumentation work. A vehicle trip is defined as a one-direction vehicle movement. The total number of trips generated by the Project includes both inbound and outbound trips. The roadways were modeled conservatively using a straight-line analysis (i.e., assuming no attenuation from topography and a straight roadway). Loose soil was used as the default ground type; per FHWA's *Ground and Pavement Effects using FHWA's Traffic Noise Model 2.5* report, an example of loose soil ground can be dirt soil with sparse vegetation, similar to the environmental setting of the area (FHWA 2010).

Table 6 shows the estimated number of existing and construction-generated vehicle trips at the modeled roadway segments. The table also includes the estimated speeds for each roadway used in the model. The modal split of construction trips was assumed to be 95 percent passenger cars and 5 percent heavy trucks for construction on Project parcels, consistent with the Aratina Solar Project Traffic Impact Analysis (EPD Solutions, Inc. 2019). The modal split of existing trips was assumed to be a typical 94 percent passenger cars, 4 percent medium trucks, and 2 percent heavy trucks. Peak hour traffic was assumed to be 10 percent of daily traffic (a standard conversion rate between peak-hour and daily traffic). Construction trips were assumed to be split from SR 14 on to Phillips Road or Neuralia Road (8minute 2019, pers. comm.).

Table 6 Estimated Existing and Construction Vehicle Trips

| Roadway Segment | Speed Limit (mph)           | Existing Daily<br>Vehicle Trips <sup>1</sup> | Construction Daily<br>Vehicle Trips <sup>2</sup> | Existing + Construction Daily Vehicle Trips |
|-----------------|-----------------------------|--|--|---|
| SR 14           | 65 (55 for heavy<br>trucks) | 7,700  | 2,110  | 9,810                                       |
| Phillips Road   | 55                          | 214  | 1,055  | 1,552                                       |
| Neuralia Road   | 55                          | 720  | 1,055  | 1,775                                       |

<sup>&</sup>lt;sup>1</sup> Existing average daily vehicle trips obtained from 2017 traffic counts on local roadways (Kern Council of Governments 2019), and from Caltrans traffic counts taken in 2017 for SR 14 (Caltrans 2019).

For traffic-related noise, impacts are considered potentially significant if Project-generated traffic would result in exposure of sensitive receivers to an unacceptable increase in noise levels during construction and/or operational activities. Recommendations in the FTA's *Transit Noise and Vibration Impact Assessment Manual* were used to determine whether increases in traffic noise would be unacceptable (FTA 2018). Under these FTA criteria, as existing ambient noise increases, the "allowable" increase in noise exposure due to a project is reduced. Table 7 shows the FTA criteria considered when evaluating traffic noise generated by this Project. If sensitive receivers would be exposed to long-term traffic noise increases exceeding these criteria, impacts may be considered significant.

Table 7 Significance of Changes in Roadway Noise Exposure

| Existing Noise Exposure (dBA L <sub>dn</sub> or L <sub>eq</sub> ) | Allowable Noise Exposure Increase (dBA $L_{dn}$ or $L_{eq}$ ) |  |
|---|---|--|
| 40-45   | 10  |  |
| 45-50   | 7   |  |
| 50-55   | 5   |  |
| 55-60   | 3   |  |
| 60-65   | 2   |  |
| 65-74   | 1   |  |
| 75+   | 0   |  |
| Source: FTA 2018 (Figure 4-3 on                                   | page 30)  |  |

### **On-Site Operational Noise**

On-site operational noise sources were modeled with SoundPLAN. Propagation of modeled stationary noise sources was based on ISO Standard 9613-2, "Attenuation of Sound during Propagation Outdoors, Part 2: General Method of Calculation." The assessment methodology assumes that all receivers would be downwind of stationary sources. This is a worst-case assumption for total noise impacts, since, in reality, only some receivers would be downwind at any one time.

<sup>&</sup>lt;sup>2</sup> Daily vehicle trips generated by construction were estimated by Aratina Solar Project Traffic Impact Analysis (EPD Solutions, Inc. 2019), a similar project in the region that would also have 1,000 peak construction workers. Construction trips were assumed to be split from SR 14 on to Phillips Road or Neuralia Road (8minute 2019, pers. comm.).

Operational noise sources from the Project include PV solar arrays with associated electrical equipment (such as transformers and inverters), energy storage systems, substations, collector lines, and the operations and maintenance facility. Details of each source are provided under Section 3.2.

Operational noise would result in a significant impact if it would exceed Kern County's standard of 65 dBA  $L_{dn}$  for exterior noise at the nearest noise-sensitive receptors or California City's 50 dBA  $L_{eq}$  from 7:00 AM to 10:00 PM or 45 dBA  $L_{eq}$  from 10:00 PM to 7:00 AM noise limits for single- and multi-family residences.

### **Operational Traffic Noise**

Vehicle trips generated by Project operational activities are estimated by traffic volumes provided in the Aratina Solar Project Traffic Impact Analysis, a similar project in the region, which listed 22 trips for 5 employees (EPD Solutions, Inc. 2019) or 4.4 trips per employee. The Kudu Solar Farm Project is estimated to have 20 employees; therefore, Project operation is estimated to generate 88 trips per day.

The existing traffic volumes used in this analysis are shown in Table 6. These traffic volumes were compared with the expected increase in traffic volumes after construction of the Project. Modeling of traffic noise indicates that, in general, a 10 percent increase in traffic volume would raise traffic noise by approximately 0.4 dBA, a 20 percent increase would raise traffic noise by about 0.8 dBA, a 30 percent increase would result in an approximately 1.1 dBA increase in traffic noise, and a 40 percent increase would increase traffic noise by about 1.5 dBA. The significance of the Project's increase in traffic noise was determined using the FTA criteria shown in Table 7.

#### Vibration

Vibration associated with construction of the Project has the potential to be an annoyance to nearby land uses. The criteria used for California City is 0.05 in./sec. RMS, which is specified by California City's Municipal Code.

## 3.2 Results

### **Construction and Decommissioning Noise**

Construction and decommissioning of the Project would involve the use of noise-generating equipment during various phases, including transport of personnel and materials to the site, heavy machinery used in grading and clearing the site, pneumatic post drivers to install foundation supports for solar array modules, as well as equipment used during construction of the proposed solar arrays, infrastructure improvements, and related structures. Emergency diesel generators may be used during construction activities.

Table 8 shows the noise levels associated with heavy construction equipment at a reference distance of 50 feet from the source. As shown in this table, noise levels at this distance can range from about 74 to 85 dBA, depending upon the types of equipment in operation at any given time and phase of construction (FHWA 2006). The highest noise levels during construction would result from pneumatic post-driving of foundation support posts (similar to steel posts used in highway guard rails) for the solar array modules and from the use of auger drill rigs and scrapers.

Table 8 Typical Construction Equipment Noise Levels

| Equipment            | Acoustical Usage Factor (%)1 | Measured L <sub>max</sub> (dBA at 50 feet) |
|----------------------|------------------------------|--|
| Augur Drill Rig      | 20                           | 84   |
| Backhoe              | 40                           | 78   |
| Compactor (ground)   | 20                           | 83   |
| Concrete Mixer Truck | 40                           | 85   |
| Crane                | 16                           | 85   |
| Dozer                | 40                           | 82   |
| Dump Truck           | 40                           | 76   |
| Excavator            | 40                           | 81   |
| Flat Bed Truck       | 40                           | 74   |
| Front End Loader     | 40                           | 79   |
| Generator            | 50                           | 81   |
| Grader               | 40                           | 83   |
| Pickup Truck         | 40                           | 75   |
| Pneumatic Tools      | 50                           | 85   |
| Roller               | 20                           | 80   |
| Scraper              | 40                           | 84   |
| Warning Horn         | 5                            | 83   |
| Welder/Torch         | 40                           | 74   |

<sup>&</sup>lt;sup>1</sup> The average fraction of time each piece of construction equipment is operating at full power (i.e., its loudest condition) during a construction operation.

Source: FHWA 2006

Project components at all Project parcels and the gen-tie would be constructed over a 12- to 18-month period. This analysis makes a conservative assumption that all construction at a Project parcel and the gen-tie would occur simultaneously (i.e., modeling assumed all equipment listed in Table 8 would be operational at once). In practice, however, grading and site preparation would take place sequentially at the Project sites. When these activities are completed at one Project parcel, post driving would start in that area while grading equipment would begin operating at another Project parcel.

Construction activities would be subject to Kern County and California City policies and regulations. Heavy construction activities would normally occur on-site between the hours of 6:00 AM and 5:00 PM, which is between the acceptable hours for construction listed in Section 8.36.020(H) of the Kern County Code and Section 5-1.407 of the California City Municipal Code. However, additional hours may be necessary to make up schedule deficiencies or to complete critical construction activities. As a result, some construction activities may be required to continue 24 hours per day, seven days per week. Activities that generate relatively low amounts of noise, such as refueling equipment, staging material for the following day's construction activities, quality assurance/control, and commissioning, may potentially occur between the hours of 9:00 PM and 6:00 AM on weekdays and the hours of 9:00 PM and 8:00 AM on weekends. Per Section 8.36.020 of the Kern County Code, these activities would require approval from the development services agency director or his or her designated representative if audible to a person with average hearing ability at a distance of 150 feet from a construction site, if the site is within 1,000 feet of an occupied residential dwelling. Per Section 5-1.412 of the California City Municipal Code, a variance can be requested for construction work outside of allowed hours; this variance is reviewed by California City's Planning Commission that will consider the

magnitude, uses, time, economic factors, and general public interest of the construction activities in granting the waiver.

Noise-sensitive receivers near Project construction include single-family residences in Kern County and California City. These land uses would experience a temporary increase in noise during construction of the Project. The following subsections detail the impacts to noise-sensitive receivers in proximity to the Project parcels and the gen-tie corridor.

### Construction at Project Parcels

Table 9 shows the estimated average noise level from construction at the Project parcels at the nearest noise-sensitive land use areas, based on a standard noise attenuation rate of 6 dBA per doubling of distance for point sources of noise. Each noise-sensitive land use listed is the closest land use in that general area, and therefore noise-sensitive receivers in those general areas further away would experience lower noise levels.

Table 9 Noise Levels at Various Distances from Construction at the Project Parcels

| Receptor  | Distance from Construction<br>(feet) | Noise Level at Receptor<br>(dBA L <sub>eq</sub> ) |
|---|--------------------------------------|---|
| Reference Distance                                      | 50                                   | 89  |
| Potential residences off Neuralia Road <sup>1</sup>     | 50                                   | 89  |
| Single-family residence in California City <sup>2</sup> | 3,250                                | 53  |

See Appendix B

As shown in Table 9, although construction noise levels from simultaneous heavy equipment operation would reach 89 dBA L<sub>eq</sub> at the reference distance of 50 feet, due to the large distance between construction at the Project parcels and the nearest noise-sensitive receivers, construction noise levels under the conservative scenario analyzed would only reach as high as 61 dBA L<sub>eq</sub>. Most construction activities would occur in the body of each parcel, farther from nearby noise-sensitive receivers than analyzed, and would therefore result in lower noise levels, especially in later construction phases when equipment with the loudest equipment, such as pneumatic tools and graders, would no longer be used. Heavy construction activity involving pneumatic tools and graders also would not occur during nighttime hours.

Per Section 8.36.020 of the Kern County Code, construction activities outside of acceptable hours would require approval from the development services agency director or designated representative if audible to a person with average hearing ability at a distance of 150 feet from a construction site, if the site is within 1,000 feet of an occupied residential dwelling. Because sensitive receivers are closer than 1,000 feet away from construction, County approval and implementation of a noise control plan would be required unless nighttime construction noise is inaudible at nearby residences. In addition, daytime construction noise levels in excess of 70 dBA L<sub>eq</sub> could disturb nearby residents. Therefore, cumulative construction noise would have a potentially significant temporary impact. Section 4, *Recommendations*, provides measures to mitigate construction noise outside of permitted hours.

The closest California City residences are located further away and therefore would be subject to noise levels of 53 dBA  $L_{eq}$ . These noise levels would be below California City's 60 dBA construction noise limit. However, construction may occur outside of California City's allowed construction hours

<sup>&</sup>lt;sup>1</sup> Closest noise-sensitive land uses from different areas of the Project in Kern County; these are identified as R9 and R10 in Figure 4.

<sup>&</sup>lt;sup>2</sup> Closest noise-sensitive land use in California City; this are identified as R7 in Figure 4.

#### Kudu Solar Farm Project

(6:00 AM and 8:00 PM between May 15 and September 15 of each year or between the hours of 7:00 AM and 8:00 PM during the remainder of the year, and no construction on Sundays or federal holidays). Per Section 5-1.412 of the California City Municipal Code, a variance can be requested for construction work outside of allowed hours; this variance is reviewed by California City's Planning Commission that will consider the magnitude, uses, time, economic factors, and general public interest of the construction activities in granting the waiver. Construction during these hours may exceed California City's single-family residential exterior noise standard of 50 dBA Leq from 7:00 AM to 10:00 PM and 45 dBA Leq from 10:00 PM to 7:00 AM. Project parcel construction within 8,000 feet may exceed the 45 dBA Leq from 10:00 PM to 7:00 AM. In accordance with the requirements of Section 5-1.412 of the California City Municipal Code, the Project would obtain a variance if construction were to occur during the nighttime hours at these distances to California City residences. Therefore, impacts would be less than significant.

#### Gen-Tie

In connecting to a substation, the gen-tie corridor may be routed through Phillips Road adjacent to noise-sensitive receivers in the single-family residential neighborhood bordered by Yuma Street, Yucaipa Street, Cheyenne Boulevard, and Phillips Road in Kern County. Therefore, for the purposes of this analysis, at the closest point of construction, the gen-tie routes would be located approximately 50 feet from single-family residences. These are the nearest sensitive receivers to any of the gen-tie route alternatives, and they would experience a temporary increase in noise during construction of the Project. As modeled, construction of the gen-tie would potentially involve the use an auger drill rig, front end loader, grader, pickup truck, crane, and concrete mixer truck. Table 10 shows construction noise levels at various distances from gen-tie construction activity, including those of the nearest noise-sensitive receivers, based on a standard noise attenuation rate of 6 dBA per doubling of distance for point sources of noise.

Table 10 Typical Construction Noise Levels at Various Distances from Gen-Tie Construction

| Receptor  | Distance from Construction (feet) | Noise Level at Receptor (dBA $L_{eq}$ ) |
|---|-----------------------------------|---|
| Reference Distance                                      | 50                                | 84                                      |
| Single-family residence Kern County <sup>1</sup>        | 50                                | 84                                      |
| Single-family residence in California City <sup>2</sup> | 8,300                             | 40                                      |

See Appendix B

As shown in Table 10, simultaneous heavy equipment use during gen-tie construction would generate a noise level of up to 84 dBA L<sub>eq</sub> when within 50 feet of single-family residences in Kern County. Most construction activities would occur further from nearby noise receptors, and would, therefore, result in lower noise levels, especially in later construction phases when equipment with louder equipment, such as cranes and concrete mixer trucks, would no longer be used. Heavy construction activity involving cranes and concrete mixer trucks also would not occur during nighttime hours. Per Section 8.36.020 of the Kern County Code, construction activities outside of acceptable hours would require approval from the development services agency director or

<sup>&</sup>lt;sup>1</sup>Closest noise-sensitive land use in the Kern County single-family neighborhood bordered by Yuma Street, Yucaipa Street, Cheyenne Boulevard, and Phillips Road in Kern County.

<sup>&</sup>lt;sup>2</sup> Closest noise-sensitive land use in California City.

designated representative if audible to a person with average hearing ability at a distance of 150 feet from a construction site, if the site is within 1,000 feet of an occupied residential dwelling. Because sensitive receivers in Kern County are closer than 1,000 feet away from gen-tie construction, County approval and implementation of a noise control plan would be required unless nighttime construction noise is in compliance with County regulations. In addition, daytime construction noise levels in excess of 70 dBA Leq could disturb nearby residents. Therefore, combined construction noise would have a potentially significant temporary impact. Section 4, *Recommendations*, provides measures to mitigate construction noise outside of permitted hours. Gen-tie construction in Kern County would not be conducted within 1,000 feet of noise-sensitive receivers outside of the single-family neighborhood bordered by Yuma Street, Yucaipa Street, Cheyenne Boulevard, and Phillips Road.

The closest California City residences are located much further away and therefore would be subject to minor noise levels of 40 dBA  $L_{\rm eq}$ . These noise levels would be below California City's 60 dBA construction noise limit. Although construction of the gen-tie may occur outside of California City's allowed construction hours, a noise level of 40 dBA  $L_{\rm eq}$  would be below California City's nighttime exterior and interior noise standard of 45 dBA  $L_{\rm eq}$ . Therefore, noise generated by construction at California City sensitive receivers would not have a significant impact. Nevertheless, implementation of measures in Section 4, *Recommendations*, would reduce construction noise to the extent feasible.

#### Project Decommissioning

As stated in Section 1.2, *Project Site and Description*, at the end of the Project's useful life (anticipated to be 30-40 years), the solar facility and associated infrastructure may be decommissioned in accordance with then-current decommissioning practices. Given the Project's operating life cycle and distant timeframe for decommissioning activities, it is too speculative to quantify the potential noise impacts that could occur during decommissioning activities. On a rough basis, decommissioning would be similar to Project construction and be completed in 12 to 18 months. Assuming that the facility would be torn down and the materials present recycled or disposed, temporary noise associated with such actions are assumed to be generally similar to the noise levels that would result from Project construction. Similar to the noise generated during construction of the Project, decommissioning activities would be conducted in accordance with all applicable requirements in effect at the time of Project termination. Potential future environmental effects associated with Project decommissioning would be addressed at the time decommissioning is proposed consistent with regulations in effect at that time. A final decommissioning plan, based on then-current technology, site conditions, and regulations, would be prepared prior to actual decommissioning.

### Combined On-Site Construction Noise

As described in Section 1.2, *Project Site and Description*, Project components at all sites would be constructed over a 12- to 18-month period. This analysis makes a conservative assumption that construction at all Project parcels and the gen-tie would occur simultaneously. Concurrent construction activity at more than one parcel and the gen-tie line may expose nearby residences to combined noise impacts. This analysis of combined effects focuses on the effects of concurrent construction activities for the worst-case scenario (i.e., the closest residences which would be exposed to construction activities at multiple sites).

Some residences located in Kern County would be exposed to adjacent construction noise from gentie construction and more distant noise from Project parcels, specifically at the single-family

#### **Kudu Solar Farm Project**

neighborhood bordered by Yuma Street, Yucaipa Street, Cheyenne Boulevard, and Phillips Road. Because of these residences proximity to gen-tie construction (as close as 50 feet), combined noise levels are dominated by gen-tie construction noise. The single-family residence off Morongo Drive near Phillips Road in Kern County is the closest residence within 50 feet of gen-tie construction that is closest to parcel construction. These include parcels located at a distance of 2,000, 3,100, 3,500, 3,600, and 4,500 feet. This residence is representative of a reasonable worst-case scenario for combined project construction noise impacts, assuming concurrent construction of gen-tie corridor and the nearest Project parcels. Table 11 estimates the combined construction noise levels for this scenario, which could reach approximately 84 dBA L<sub>eq</sub>.

Table 11 Combined Construction Noise Levels for Worst-Case Scenario<sup>1</sup>

| Project Site         | Distance from Construction (feet) | Noise Level at Receptor (dBA $L_{eq}$ ) |  |
|----------------------|-----------------------------------|---|--|
| Gen-tie              | 50                                | 84                                      |  |
| Project Parcel       | 2,000                             | 52                                      |  |
| Project Parcel       | 3,100                             | 48                                      |  |
| Project Parcel       | 3,500                             | 47                                      |  |
| Project Parcel       | 3,600                             | 47                                      |  |
| Project Parcel       | 4,500                             | 45                                      |  |
| Combined Noise Level |                                   | 84                                      |  |

<sup>&</sup>lt;sup>1</sup> Worst-case scenario is for single-family residence off Morongo Drive near Phillips Road in Kern County, which is closest residence to the Project parcels that is adjacent to gen-tie construction.

Per Section 8.36.020 of the Kern County Code, construction activities outside of acceptable hours would require approval from the development services agency director or designated representative if audible to a person with average hearing ability at a distance of 150 feet from a construction site, if the site is within 1,000 feet of an occupied residential dwelling. Because sensitive receivers in Mojave are closer than 1,000 feet away from gen-tie construction, County approval and implementation of a noise control plan would be required unless nighttime construction noise is in compliance with County regulations. In addition, daytime construction noise levels in excess of 70 dBA L<sub>eq</sub> could disturb nearby residents. Therefore, combined construction noise would have a potentially significant temporary impact. Section 4, *Recommendations*, provides measures to mitigate construction noise outside of permitted hours.

### **Construction Traffic Noise**

Construction of the Project would increase traffic noise offsite from commuting construction workers and from haul trucks bringing materials to and from the Project site. As mentioned previously, Project components would be constructed simultaneously over a 12- to 18-month period. This could expose nearby residences to combined noise from construction traffic. This analysis of combined effects focuses on the effects of concurrent construction traffic for the worst-case scenario (i.e., traffic generated by the peak construction period). Table 6 in Section 3.1, *Methodology and Significance Thresholds*, compares existing daily traffic volumes on nearby road segments to anticipated traffic generated by Project construction. Based on these traffic volumes, Table 12 shows

modeled traffic noise levels at the nearest receivers under existing traffic conditions and with construction traffic.

**Table 12 Construction Traffic Noise** 

| Roadway       | Nearest<br>Sensitive<br>Receiver              | Distance from Roadway Centerline to Nearest Sensitive Receiver (feet) | Existing<br>Traffic<br>Noise<br>(dBA L <sub>eq</sub> ) | With-<br>Construction<br>Traffic Noise<br>(dBA L <sub>eq</sub> ) | Change in<br>Traffic<br>Noise<br>(dBA L <sub>eq</sub> ) | FTA Allowable Noise Exposure Increase (dBA L <sub>eq</sub> ) |
|---------------|---|---|--|--|---|--|
| SR 14         | Single-family<br>residences in<br>Kern County | 300   | 54   | 55   | 1   | 5  |
| Phillips Road | Single-family<br>residences in<br>Kern County | 80  | 53   | 58   | 5   | 5  |
| Neuralia Road | Single-family<br>residences in<br>Kern County | 105   | 52   | 57   | 5   | 5  |

As shown in Table 12, construction traffic would increase noise levels by up to 5 dBA  $L_{eq}$  at the nearest sensitive receivers from Project construction. However, none of the traffic noise increases would exceed the applicable FTA criteria. Therefore, the short-term increase in traffic noise from Project construction would be less than significant.

### **On-Site Operational Noise**

The Project would operate continuously, seven days a week, until the anticipated repowering or decommissioning of the Project in 30 to 40 years. Stationary noise sources during operation would include PV solar arrays with associated electrical equipment (such as transformers and inverters), energy storage systems, substations, collector lines, and the operations and maintenance facility. Electrical equipment produces a discrete low-frequency humming noise. The noise from transformers is produced by alternating current flux in the core, which causes it to vibrate.

Transformers would be located within the inverters, which would lie within an enclosed or canopied metal structure. Within enclosures, inverters typically produce a noise level of 58 dBA L<sub>eq</sub> at the source (Monterey County 2014). However, a fully enclosed metal structure would attenuate noise from inverter stations more effectively than would a canopy structure with open walls. It is unknown at this time whether the inverters/transformers would be enclosed or open. This would be determined during design once the inverter/transformer manufacturer has been selected. Open inverters would generate a noise level of approximately 52 dBA at a distance of 75 feet (*California Valley Solar Project Final EIR*, San Luis Obispo County 2011). If the inverters are enclosed, each inverter enclosure may also include heating, ventilation, and air conditioning (HVAC) systems mounted on the exterior of the inverter enclosure, which would generate a noise level of 58 dBA at a distance of 75 feet.

Table 13 lists representative noise levels of equipment used for similar solar projects that are assumed to be used on the Project site.

Table 13 Estimated Noise Rating for Equipment Utilized During Project Operations

| Equipment Type                | Reference Noise Level<br>(dBA L <sub>eq</sub> ) | Distance from Source<br>(feet) |  |
|-------------------------------|---|--------------------------------|--|
| Gen-Tie <sup>1</sup>          | 20  | 50                             |  |
| PV Panel                      | 44  | 50                             |  |
| 500+ kW Inverter (unenclosed) | 52  | 75                             |  |
| Transformer                   | 58  | 3.3                            |  |
| Inverter HVAC System          | 58  | 75                             |  |

<sup>&</sup>lt;sup>1</sup> Only applicable to the gen-tie transmission line.

Sources: U.S. Department of Energy 2011; San Luis Obispo County 2011; Illingworth and Rodkin 2009; Kern County 2014; Monterey County 2014

As shown in Table 13, it is expected that the loudest noise generated by on-site solar operations would come from the HVAC systems at 58 dBA L<sub>eq</sub> at a distance of 75 feet from the source. As the closed inverter would generate a higher noise level than an open inverter due to the inclusion of HVAC units, the enclosed inverters are conservatively used for this analysis. The combined noise levels from the HVAC systems and transformers, which would be anticipated to operate simultaneously, are analyzed below at the closest sensitive receivers through SoundPLAN modeling. Noise levels from the gen-tie transmission line, PV panels, and substations/energy storage systems are discussed separately, as these noise sources would be minor in comparison to the HVAC systems and transformers and were not modeled.

### Solar Array Noise

Sensitive receivers nearby the Project parcels include rural single-family residences in Kern County and single-family residences located in the northern neighborhoods of California City. Noise levels from the Project's solar array operations (transformers and inverters [HVAC]) are shown in Table 14, and noise level contours and receiver locations are shown in Figure 5.

Table 14 Operational Noise Levels at Nearest Sensitive Receivers

|          |                                       | Jurisdiction <sup>1</sup> | Noise Level at Receiver |                     | Exceed     |
|----------|---------------------------------------|---------------------------|-------------------------|---------------------|------------|
| Receiver | Receiver Description                  |                           | dBA L <sub>eq</sub>     | dBA L <sub>dn</sub> | Threshold? |
| R1       | Esther Ave Residence                  | Kern County               | 24                      | 30                  | No         |
| R2       | Isabella Blvd Residence               | Kern County               | 21                      | 27                  | No         |
| R3       | Near Dodson Ave and Isabella Blvd     | Kern County               | 21                      | 27                  | No         |
| R4       | Yerba Blvd Residence                  | Kern County               | 25                      | 31                  | No         |
| R5       | Southeast Phillips Rd Residence       | Kern County               | 27                      | 33                  | No         |
| R6       | Southwestern Phillips Rd Residence    | Kern County               | 28                      | 34                  | No         |
| R7       | Residence south of Lindbergh          | California City           | 23                      | 30                  | No         |
| R8       | Denhart Ave Residence                 | California City           | 18                      | 24                  | No         |
| R9       | Possible Residence near Neuralia Road | Kern County               | 34                      | 40                  | No         |
| R10      | Possible Residence near Neuralia Road | Kern County               | 34                      | 40                  | No         |

Note: Calculations completed in SoundPLAN; See Figure 5 for receiver locations.

As shown in Table 14, operational noise levels from the project site would reach up to 34 dBA  $L_{dn}$  at Kern County sensitive receivers and 24 dBA  $L_{eq}$  at California City sensitive receivers. These noise levels would be well below Kern County's standard of 65 dBA  $L_{dn}$  for exterior noise at the nearest noisesensitive receptors or California City's 50 dBA  $L_{eq}$  from 7:00 AM to 10:00 PM and 45 dBA  $L_{eq}$  from 10:00 PM to 7:00 AM noise limits for residences. The noise would likely not be audible over the existing ambient noise in the areas. Therefore, operational noise impacts from the Project would be less than significant.

#### Gen-Tie

The gen-tie transmission line would generate noise from the corona affect, which is a phenomenon associated with the electrical ionization of the air that occurs near the surface of the energized conductor and suspension hardware due to very high electric field strength. This is audible power line noise that is generated from electric corona discharge, which is usually experienced as a random crackling or hissing sound. The corona effect on the gen-tie transmission line would generate a noise level of approximately 20 dBA at a distance of 50 feet (*California Valley Solar Project Final EIR*, San Luis Obispo County 2011). This is the approximate distance to the nearest residences from the gentie route. As observed during a site visit to the area and transmission lines from existing solar farms in the area, noise levels from these transmissions lines were not detected over the existing ambient noise sources in the area (wind, vehicles, planes, and trains) just outside of the solar farm properties. Therefore, per site observations and the general low noise of transmissions lines, gen-tie noise would not exceed County's standard of 65 dBA L<sub>dn</sub> at the nearest residences, and impacts would be less than significant.

 $<sup>^1</sup>$  Operational noise would result in a significant impact depending on the jurisdiction it is location in; the Kern County standard is 65 dBA  $L_{dn}$  for exterior noise at the nearest noise-sensitive receptors, and the California City standard is 50 dBA  $L_{eq}$  from 7:00 AM to 10:00 PM or 45 dBA  $L_{eq}$  from 10:00 PM to 7:00 AM noise limits at single- and multi-family residences.

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### PV Panel

PV panel noise would come from the tracking motors. These systems involve the panels being driven by motors to make brief, incremental adjustments to track the arc of the sun to maximize the solar effect. While these motors may generate noise of up to 44 dBA at 50 feet, these motors would

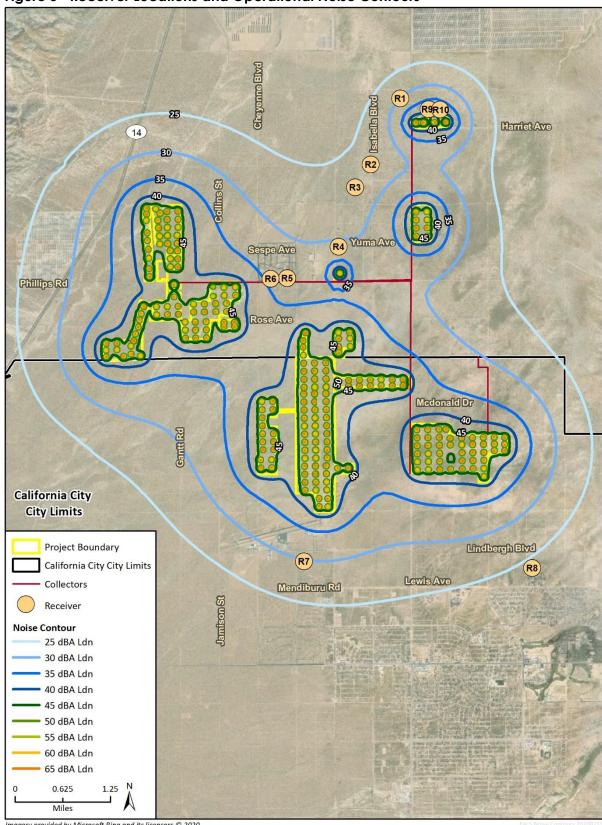


Figure 5 Receiver Locations and Operational Noise Contours

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#### Kudu Solar Farm Project

operate briefly throughout an hour (e.g., several minutes per hour) as the sun moves west across the sky, and then would reset at night to face the eastern sky. By operating only several minutes per hour, the hourly noise level would be negligible at the nearest sensitive receivers. In addition, as observed during a site visit to the area and viewing of existing solar farms in the area, noise levels from PV panel tracking were not detected over the existing ambient noise sources in the area (wind, vehicles, planes, and trains) just outside of the solar farm properties. Therefore, noise levels from the PV panels would be less than significant.

### Substation/Energy Storage System

The substation and energy storage systems would likely be constructed in a similar area of the Project. These facilities would collect, transmit, and store energy generated by the solar arrays. Noise generated by these facilities may include HVAC units. However, the transformers and inverters analyzed earlier in this section would include a much larger number of HVAC units for the inverters and additional noise from the transformers spread across the Project site that would be more prominent than the noise generated by the substation and energy storage system, which would be located in one area of the Project sites. In addition, as observed during a site visit to the area and viewing of existing solar farms in the area, noise levels from substations and energy storage systems were not detected over the existing ambient noise sources in the area (wind, vehicles, planes, and trains) just outside of the solar farm properties. Therefore, noise levels from the PV panels would be less than significant.

### **Operational Traffic Noise**

Once the Project is complete, vehicle trips to the Project site would be associated with operations and maintenance of the solar facility. In addition, the Project would require occasional nighttime activities, including deliveries, repairs, maintenance, office and administrative activities, security personnel, and emergency response.

As shown in Table 15, existing roadways would generate noise levels of 52 to 54 dBA  $L_{\rm eq}$  to the nearest single-family residences. Pursuant to the FTA criteria described in Table 7, a significant noise impact would occur if roadway noise would increase by more than 5 dBA. With the relatively minor increase in traffic volumes from Project operation (88 trips), Project operation would increase noise by or less than 1 dBA. This increase would be imperceptible to the nearest residents and would not exceed applicable FTA criteria. Therefore, the Project's noise increases from operational traffic would have a less than significant impact.

**Table 15 Operational Traffic Noise** 

| Roadway       | Nearest Sensitive<br>Receiver                 | Distance from<br>Roadway<br>Centerline to<br>Nearest Sensitive<br>Receiver (feet) | Existing<br>Traffic<br>Noise<br>(dBA L <sub>eq</sub> ) | With-<br>Operational<br>Traffic Noise<br>(dBA L <sub>eq</sub> ) | Change<br>in Traffic<br>Noise<br>(dBA L <sub>eq</sub> ) | FTA Allowable<br>Noise<br>Exposure<br>Increase<br>(dBA L <sub>eq</sub> ) |
|---------------|---|---|--|---|---|--|
| SR 14         | Single-family<br>residences in Kern<br>County | 300   | 54   | 54  | <1  | 5  |
| Phillips Road | Single-family<br>residences in Kern<br>County | 80  | 53   | 54  | 1   | 5  |
| Neuralia Road | Single-family<br>residences in Kern<br>County | 105   | 52   | 52  | <1  | 5  |

#### Vibration

### Construction at Project Parcels

Construction at the Project parcels may require post driving and vibratory rollers and has the potential to result in temporary vibration impacts on structures and humans. Based on the potential site locations, post driving activities could occur within 3,250 feet of the nearest residence (22362 Guynemer Court) in California City. As impact pile drivers have higher vibration levels than vibratory pile drivers, the potential vibration impact calculations assume that impact pile drivers will be used. Other construction activities are less intensive than pile driving and would have lower PPV than pile driving. Therefore, vibration levels from pile driving are considered worst case for construction at the Project parcels. Caltrans vibration guidance provides the following equation<sup>2</sup> to calculate PPV at sensitive receptors:

PPV Impact Pile Driver= PPV<sub>Ref</sub> (25/D)<sup>n</sup> x (E<sub>equip</sub>/E<sub>Ref</sub>)<sup>0.5</sup> (in./sec.)

Where:

PPV<sub>Ref</sub> = 0.65 in/sec for a reference pile driver at 25 feet

D = distance from pile driver to the receiver in feet

n = 1.1 is a value related to the vibration attenuation rate through ground

E<sub>equip</sub> is rated energy of impact pile driver in ft-lbs

E<sub>Ref</sub> is 36,000 ft-lb (rated energy of reference pile driver)

Using the referenced formula and an assumed 2,400 ft-lb rated energy<sup>3</sup> for the post driver and converting the in./sec. PPV values to in./sec. RMS, the Project would generate vibration levels of up to 0.0002 in./sec. RMS at the nearest California City residential structure, well below the 0.05 in./sec. RMS threshold. In addition, heavy construction activity involving pneumatic tools and graders also

<sup>&</sup>lt;sup>2</sup> Equation is provided in Section 7.1.1, Equation 9 of Caltrans 2020.

<sup>&</sup>lt;sup>3</sup> This would be a typical size for the type of post drivers that would be used to drive in the foundations for the arrays. An example is a Bradco Post Driver by Paladin with 2,400 ft-lb rated energy (<a href="https://www.paladinattachments.com/sites/default/files/prod">https://www.paladinattachments.com/sites/default/files/prod</a> lit/SS%20-%20BR%20-%20post%20driver.pdf)

#### **Kudu Solar Farm Project**

would not occur during nighttime hours. Therefore, vibration impacts associated with construction of the proposed Project would be less than significant.

Once constructed, the proposed PV facility would not have any components that would generate vibration levels. Thus, operation of the proposed Project would not result in any vibration and impacts would be less than significant.

#### Gen-tie Construction

Gen-tie construction may require the use of an auger drill rig that has the potential to result in temporary vibration impacts on structures and humans. Based on the potential site locations, auger drilling activities could occur within 8,300 feet of the nearest off-site residential structure in California City. Other than use of an auger drill rig, other construction activities at the gen-tie corridors are less intensive than auger drill rig and would have lower PPV than the auger drill rig. Therefore, vibration levels from the auger drill rig are considered worst case for the gen-tie construction. Caltrans vibration guidance provides the following equation to calculate PPV at sensitive receptors:

PPV Equipment = PPV<sub>Ref</sub> (25/D)<sup>n</sup> (in./sec.) <sup>4</sup>

Where:

PPV<sub>Ref</sub> = Equipment reference vibration level at 25 feet

D = distance from equipment to the receiver in feet

n = 1.1 is a value related to the vibration attenuation rate through ground

Caltrans vibration guidelines do not provide vibration levels specifically for an auger drill rig; however, the guidelines do provide vibration levels for caisson drilling of 0.089 in./sec. PPV. A caisson drill would typically drill a much larger hole than the type of bore performed for a solar foundation post (e.g., a caisson drill would be used to drill a bridge pier). Although a caisson drill is a more intensive activity that would result in greater vibration than an auger drill, it was used as a conservative reference for this analysis. Using the referenced formula and converting the in./sec. PPV values to in./sec. RMS, the Project would generate vibration levels of up to 0.00004 in./sec. RMS at the nearest California City residential structure, well below the 0.05 in./sec. PPV threshold. In addition, heavy construction activity involving drilling would not occur during nighttime hours. Therefore, vibration impacts associated with construction of the proposed Project would be less than significant.

#### Operation

Once constructed, the proposed PV facility would not have any components that would generate vibration levels. Thus, operation of the proposed Project would not result in any vibration and impacts would be less than significant.

<sup>&</sup>lt;sup>4</sup> Equation is provided in Section 7.2, Equation 12 of Caltrans 2020.

# 4 Recommendations

Construction of the Project would temporarily increase ambient noise levels at noise-sensitive receptors near the Project site. The following recommendations would reduce noise impacts from the Project's construction activities. Measure 1 is recommended because although not necessary to comply with construction noise standards, it would prevent the physical environmental impact of exposing sensitive receptors to potentially disruptive noise levels during permitted construction hours. Measure 2 is necessary for nighttime construction activity to comply with Section 8.36.020 of the Kern County Code.

#### N-1 Construction Noise Reduction Measures

The applicant shall apply the following measures during active construction work of the Project occurring within 1,000 feet of an occupied, offsite noise-sensitive receptor.

### Mufflers

Construction equipment shall be properly maintained and all internal combustion engine driven machinery with intake and exhaust mufflers and engine shrouds, as applicable, shall be in good condition and appropriate for the equipment. During construction, all equipment, fixed or mobile, shall be operated with closed engine doors and shall be equipped with properly operating and maintained mufflers, consistent with manufacturers' standards.

#### Equipment Staging

All stationary equipment shall be staged as far away from noise-sensitive receptors as feasible.

#### Equipment Idling

Diesel-powered construction vehicles and equipment shall not be left idling for longer than five minutes when not in use, consistent with California Code of Regulations Title 13, Section 2485.

### N-2 Construction Noise Outside of Permitted Hours Reduction Measures – Kern County

The applicant shall apply one of the following measures during active construction work for the Project occurring outside of permitted hours per Section 8.36.020 of the Kern County Code:

1) Development Services Agency Director Approval. The applicant shall obtain approval from the development services agency director or designated representative for Project construction activities occurring between the hours of 9:00 PM and 6:00 AM on weekdays and 9:00 PM and 8:00 AM on weekends, within 1,000 feet of an occupied residential building, if audible to a person with average hearing ability at a distance of 150 feet from a construction site. As a condition of approval for exempting construction activity outside of permitted hours, the applicant shall implement a noise control plan including appropriate noise-reduction measures to the satisfaction of the development services agency director or designated representative, which may include the measures listed in Recommended Measure N-1. In addition, the noise control plan may include a requirement to restrict the duration of construction activities outside of permitted hours within 1,000 feet of an occupied residential building.

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#### Kudu Solar Farm Project

2) Restrict Construction Activity within 1,000 feet of Noise-Sensitive Receptors in Kern County. Construction activities that are located within 1,000 feet of the nearest noise-sensitive receptors, and that would generate audible noise at a distance of 150 feet from the source between the hours of 9:00 PM and 6:00 AM on weekdays and the hours of 9:00 PM and 8:00 AM on weekends, shall be prohibited.

# 5 Conclusions

As discussed in Section 3, *Impact Analysis*, the Project would not generate construction traffic noise, construction vibration, on-site operational noise, or operational traffic noise exceeding applicable standards. However, construction activity would temporarily expose nearby residences to high daytime noise levels and could expose them to nighttime noise. Compliance with California City Municipal Code Section 5-1.412 to obtain a variance to conduct nighttime construction activities in California City limits would ensure that impacts would be less than significant. For construction in Kern County, implementation of the recommended Measure N-1 would be necessary to reduce the exposure of residences located within 1,000 feet of construction activity to potentially disruptive noise levels during permitted construction hours, to the extent feasible. In addition, implementation of the recommended Measure N-2 would provide for Kern County approval of nighttime noise outside of permitted construction hours or restrict nighttime construction activity near residences. Therefore, impacts to nearby sensitive receivers would be less than significant with mitigation.

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Noise Study 39

## Appendix A

On-Site Noise Measurement Data

LT1

```
Data Logger 2
SET 240
Α
SLOW
Range 30-90
L05 65.4
L10 62.8
L50 48.7
L90 31.6
L95 29.6
Max dB 85.2
2019/09/19 12:27:05
SEL 119.3
Leg 70.0
No.s Date Time
                 dВ
      2019/09/18 12:28:03
                              36.9
2
      2019/09/18 12:32:03
                              35.1
3
      2019/09/18 12:36:03
                              45.7
4
      2019/09/18 12:40:03
                              50.6
5
      2019/09/18 12:44:03
                              51.4
6
      2019/09/18 12:48:03
                              38.9
7
      2019/09/18 12:52:03
                              48.2
8
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                              63.0
9
      2019/09/18 13:00:03
                              52.8
10
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                              65.7
11
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LT2

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ST1

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| 90<br>91<br>92<br>93     | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 35: 30<br>12: 35: 33<br>12: 35: 36 | 39. 3<br>30. 1<br>32. 8<br>46. 4 |
| 94<br>95<br>96           | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 35: 39<br>12: 35: 42<br>12: 35: 45 | 41. 0<br>43. 5<br>32. 8          |
| 97<br>98<br>99<br>100    | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 35: 51<br>12: 35: 54               | 27. 0<br>26. 4<br>26. 5<br>28. 8 |
| 101<br>102<br>103        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 36: 00<br>12: 36: 03<br>12: 36: 06 | 31. 6<br>40. 6<br>35. 4          |
| 104<br>105<br>106        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 36: 12<br>12: 36: 15               | 32. 9<br>37. 7<br>47. 5          |
| 107<br>108<br>109<br>110 | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 36: 21<br>12: 36: 24               | 46. 6<br>45. 6<br>69. 3<br>69. 7 |
| 111<br>112<br>113        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 36: 30<br>12: 36: 33<br>12: 36: 36 | 60. 6<br>51. 3<br>44. 2          |
| 114<br>115<br>116<br>117 | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 36: 42<br>12: 36: 45               | 43. 9<br>45. 9<br>42. 2<br>42. 3 |
| 118<br>119<br>120        | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 36: 51<br>12: 36: 54<br>12: 36: 57 | 41. 4<br>37. 7<br>33. 8          |
| 121<br>122<br>123        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 37: 00<br>12: 37: 03<br>12: 37: 06 | 29. 4<br>34. 0<br>36. 1          |
| 124<br>125<br>126<br>127 | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 37: 12<br>12: 37: 15               | 34. 2<br>32. 6<br>34. 5<br>30. 4 |
| 128<br>129<br>130        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 37: 21<br>12: 37: 24               | 30. 1<br>31. 9<br>29. 5          |
| 131<br>132<br>133        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 37: 33<br>12: 37: 36               | 31. 4<br>32. 1<br>36. 0          |
| 134<br>135<br>136<br>137 | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 37: 42<br>12: 37: 45               | 33. 6<br>33. 4<br>33. 0<br>29. 7 |
| 138<br>139<br>140        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 37: 51<br>12: 37: 54<br>12: 37: 57 | 28. 6<br>28. 7<br>33. 0          |
| 141<br>142<br>143<br>144 | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 38: 03<br>12: 38: 06               | 29. 2<br>26. 9<br>26. 7<br>26. 4 |
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| 148<br>149<br>150        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 38: 21<br>12: 38: 24<br>12: 38: 27 | 28. 4<br>27. 3<br>29. 2          |
| 151<br>152<br>153<br>154 | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 38: 33<br>12: 38: 36               | 29. 6<br>27. 2<br>24. 9<br>27. 4 |
| 155<br>156<br>157        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 38: 42<br>12: 38: 45<br>12: 38: 48 | 28. 4<br>31. 7<br>29. 7          |
| 158<br>159<br>160        | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 38: 54<br>12: 38: 57               | 34. 0<br>29. 5<br>26. 1<br>26. 0 |
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| 165<br>166<br>167        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 39: 12<br>12: 39: 15<br>12: 39: 18 | 28. 4<br>27. 0<br>25. 6          |
| 168<br>169<br>170<br>171 | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 39: 24<br>12: 39: 27               | 27. 1<br>26. 5<br>25. 1<br>24. 9 |
| 172<br>173<br>174        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 39: 33<br>12: 39: 36<br>12: 39: 39 | 30. 8<br>30. 9<br>26. 1          |
| 175<br>176<br>177<br>178 | 2019/09/18<br>2019/09/18<br>2019/09/18<br>2019/09/18 | 12: 39: 42<br>12: 39: 45<br>12: 39: 48 | 24. 8<br>24. 8<br>26. 7<br>27. 0 |
| 178<br>179<br>180<br>181 | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 39: 54<br>12: 39: 57<br>12: 40: 00 | 34. 8<br>34. 6<br>39. 4          |
| 182<br>183<br>184        | 2019/09/18<br>2019/09/18<br>2019/09/18               | 12: 40: 03<br>12: 40: 06               | 41. 5<br>45. 5<br>48. 2          |

| 272 2019/09/18 12: 44: 33 30 | 185<br>186<br>187<br>188<br>189<br>190<br>191<br>192<br>193<br>194<br>195<br>197<br>198<br>199<br>201<br>202<br>203<br>204<br>205<br>207<br>208<br>209<br>210<br>211<br>213<br>214<br>215<br>217<br>218<br>222<br>223<br>224<br>225<br>227<br>228<br>229<br>230<br>241<br>242<br>253<br>264<br>265<br>267<br>267<br>268<br>267<br>268<br>267<br>268<br>268<br>268<br>268<br>268<br>268<br>268<br>268<br>268<br>268 | 2019/09/18 | 12: 40: 12 12: 40: 15 12: 40: 15 12: 40: 21 12: 40: 23 12: 40: 33 12: 40: 33 12: 40: 33 12: 40: 45 12: 40: 45 12: 40: 54 12: 40: 54 12: 40: 54 12: 41: 03 12: 41: 03 12: 41: 03 12: 41: 03 12: 41: 15 12: 41: 21 12: 41: 21 12: 41: 21 12: 41: 24 12: 41: 24 12: 41: 24 12: 41: 24 12: 41: 24 12: 41: 36 12: 41: 45 12: 41: 45 12: 41: 45 12: 41: 45 12: 41: 45 12: 41: 45 12: 42: 41 12: 42: 42 12: 42: 42 12: 42: 43 12: 42: 43 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 36 12: 43: 43 12: 43: 44 12: 44: 45 12: 44: 45 12: 44: 45 12: 44: 45 12: 44: 45 12: 44: 45 12: 44: 45 12: 44: 45 12: 44: 45 12: 44: 44 | 33<br>35<br>31<br>33<br>29<br>29                               |
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| 284 | 2019/09/18 | 12: 45: 09 | 49.8  |
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| 286 | 2019/09/18 | 12: 45: 15 | 47. 9 |
| 287 | 2019/09/18 | 12: 45: 18 | 43. 2 |
| 288 | 2019/09/18 | 12: 45: 21 | 36. 3 |
| 289 | 2019/09/18 | 12: 45: 24 | 34. 9 |
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| 291 | 2019/09/18 | 12: 45: 30 | 42. 9 |
| 292 | 2019/09/18 | 12: 45: 33 | 44. 1 |
| 293 | 2019/09/18 | 12: 45: 36 | 45. 0 |
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| 295 | 2019/09/18 | 12: 45: 42 | 44.4  |
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| 297 | 2019/09/18 | 12: 45: 48 | 43.0  |
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| 300 | 2019/09/18 | 12: 45: 57 | 34.0  |
|     |            |            |       |

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Time Weight: SLOW
Level Range: 30-90
Max dB: 71.4 - 2019/09/18 11:37:49
Level Range: 30-90
SEL: 81.9
Leq: 52.4 ST2

| Leq: 52.4   |   |   |
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| 86         | 2019/09/18                             |                | 36: 28                     | 30. 0          |
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| 87         | 2019/09/18                             |                | 36: 31                     | 27. 2          |
| 88<br>89   | 2019/09/18<br>2019/09/18<br>2019/09/18 | 11:3           | 36: 34<br>36: 37           | 40. 7<br>30. 8 |
| 90<br>91   | 2019/09/18<br>2019/09/18<br>2019/09/18 | 11: 3          | 36: 40<br>36: 43           | 36. 7<br>29. 3 |
| 92         | 2019/09/18                             | 11: 3          | 36: 46                     | 27.4           |
| 93<br>94   | 2019/09/18<br>2019/09/18               | 11:3           | 36: 49<br>36: 52           | 35.7           |
| 95         | 2019/09/18                             | 11:3           | 36: 55                     | 40. 4          |
| 96         | 2019/09/18                             |                | 36: 58                     | 33. 2          |
| 97<br>98   | 2019/09/18<br>2019/09/18               | 11: 3<br>11: 3 | 37: 01<br>37: 04<br>37: 07 | 29. 7<br>31. 8 |
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| 105<br>106 | 2019/09/18<br>2019/09/18               | 11: 3<br>11: 3 | 37: 22<br>37: 25<br>37: 28 | 34. 2<br>31. 2 |
| 107        | 2019/09/18                             | 11: 3          | 37: 31                     | 30. 1          |
| 108        | 2019/09/18                             |                | 37: 34                     | 32. 5          |
| 109        | 2019/09/18                             | 11: 3          | 37: 37                     | 37. 2          |
| 110        | 2019/09/18                             |                | 37: 40                     | 40. 5          |
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| 112        | 2019/09/18                             |                | 37: 46                     | 64. 2          |
| 113        | 2019/09/18<br>2019/09/18               | 11: 3          | 37: 49<br>37: 52           | 65. 0<br>54. 7 |
| 115<br>116 | 2019/09/18<br>2019/09/18<br>2019/09/18 | 11:3           | 37: 52<br>37: 55<br>37: 58 | 48. 3<br>46. 0 |
| 117        | 2019/09/18                             | 11: 3          | 38: 01                     | 60. 8<br>63. 6 |
| 118<br>119 | 2019/09/18<br>2019/09/18               | 11:3           | 38: 04<br>38: 07           | 59. 9          |
| 120        | 2019/09/18                             | 11: 3          | 38: 10                     | 55. 6          |
| 121        | 2019/09/18                             |                | 38: 13                     | 49. 0          |
| 122        | 2019/09/18                             | 11: 3          | 38: 16                     | 50. 1          |
| 123        | 2019/09/18                             |                | 38: 19                     | 46. 5          |
| 124        | 2019/09/18                             | 11:3           | 38: 22                     | 40. 9          |
| 125        | 2019/09/18                             |                | 38: 25                     | 40. 4          |
| 126        | 2019/09/18                             |                | 38: 28                     | 34. 3          |
| 127        | 2019/09/18                             |                | 38: 31                     | 31. 1          |
| 128        | 2019/09/18                             | 11: 3          | 38: 34                     | 33. 3          |
| 129        | 2019/09/18                             |                | 38: 37                     | 34. 0          |
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| 131        | 2019/09/18                             |                | 38: 43                     | 33. 7          |
| 132        | 2019/09/18                             | 11:3           | 38: 46                     | 30. 0          |
| 133        | 2019/09/18                             |                | 38: 49                     | 29. 7          |
| 134<br>135 | 2019/09/18<br>2019/09/18               | 11:3           | 38: 52<br>38: 55           | 31. 1          |
| 136        | 2019/09/18                             | 11: 3          | 38: 58                     | 30. 0          |
| 137        | 2019/09/18                             |                | 39: 01                     | 28. 6          |
| 138        | 2019/09/18                             | 11:3           | 39: 04                     | 28. 2          |
| 139        | 2019/09/18                             |                | 39: 07                     | 27. 7          |
| 140<br>141 | 2019/09/18<br>2019/09/18<br>2019/09/18 | 11: 3          | 39: 10<br>39: 13           | 27. 5<br>27. 5 |
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| 144        | 2019/09/18                             | 11: 3          | 39: 22                     | 27.7           |
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| 158        | 2019/09/18                             | 11: 4          | 10: 04                     | 36. 7          |
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| 162        | 2019/09/18                             |                | 10: 16                     | 56. 1          |
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| 164        | 2019/09/18                             |                | 10: 22                     | 45. 6          |
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| 166        | 2019/09/18                             |                | 10: 28                     | 44. 0          |
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| 169        | 2019/09/18                             | 11: 4          | 10: 34<br>10: 37           | 65.7           |
| 170        | 2019/09/18                             | 11: 4          | 10: 40                     | 58. 2          |
| 171        | 2019/09/18                             |                | 10: 43                     | 52. 0          |
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| 174        | 2019/09/18                             | 11: 4          | 10: 52                     | 43. 1          |
| 175        | 2019/09/18                             |                | 10: 55                     | 44. 9          |
| 176        | 2019/09/18                             | 11: 4          | 10: 58                     | 47. 1          |
| 177        | 2019/09/18                             |                | 11: 01                     | 48. 6          |
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| 179        | 2019/09/18                             |                | 11: 07                     | 47. 3          |
| 180        | 2019/09/18                             | 11: 4          | 11: 10                     | 47. 5          |
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| 182        | 2019/09/18                             |                | 11: 16                     | 50. 9          |
| 183        | 2019/09/18                             |                | 11: 19                     | 51. 7          |
| 184        | 2019/09/18                             |                | 11: 22                     | 48. 0          |

| 185               | 2019/09/18                             | 11: 41: 25                             | 45. 9          |
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| 187               | 2019/09/18                             | 11: 41: 31                             | 41. 6          |
| 188               | 2019/09/18                             | 11: 41: 34                             | 44. 1          |
| 189               | 2019/09/18                             | 11: 41: 37                             | 39. 3          |
| 190               | 2019/09/18                             | 11: 41: 40                             | 39. 5          |
| 191               | 2019/09/18                             | 11: 41: 43                             | 35. 2          |
| 192               | 2019/09/18                             | 11: 41: 46                             | 36. 0          |
| 193               | 2019/09/18                             | 11: 41: 49                             | 38. 9          |
| 194               | 2019/09/18                             | 11: 41: 52                             | 39. 1          |
| 195               | 2019/09/18                             | 11: 41: 55                             | 43. 0          |
| 196               | 2019/09/18                             | 11: 41: 58                             | 46. 8          |
| 197<br>198        | 2019/09/18<br>2019/09/18<br>2019/09/18 | 11: 42: 01<br>11: 42: 04               | 50. 1<br>63. 3 |
| 199<br>200        | 2019/09/18                             | 11: 42: 07                             | 66. 4          |
| 201               | 2019/09/18<br>2019/09/18               | 11: 42: 13                             | 54. 1          |
| 202<br>203        | 2019/09/18<br>2019/09/18               | 11: 42: 19                             | 46.0           |
| 204               | 2019/09/18                             | 11: 42: 22                             | 42. 1          |
| 205               | 2019/09/18                             | 11: 42: 25                             | 45. 9          |
| 206               | 2019/09/18                             | 11: 42: 28                             | 42. 8          |
| 207               | 2019/09/18                             | 11: 42: 31                             | 44. 4          |
| 208               | 2019/09/18                             | 11: 42: 34                             | 45. 8          |
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| 210               | 2019/09/18                             | 11: 42: 40                             | 44. 1          |
| 211               | 2019/09/18                             | 11: 42: 43                             | 41. 3          |
| 212               | 2019/09/18                             | 11: 42: 46                             | 40. 4          |
| 213               | 2019/09/18                             | 11: 42: 49                             | 42. 4          |
| 214               | 2019/09/18                             | 11: 42: 52                             | 41. 0          |
| 215               | 2019/09/18                             | 11: 42: 55                             | 41. 7          |
| 216               | 2019/09/18                             | 11: 42: 58                             | 42. 4          |
| 217               | 2019/09/18                             | 11: 43: 01                             | 46. 4          |
| 218               | 2019/09/18                             | 11: 43: 04                             | 41. 3          |
| 219               | 2019/09/18                             | 11: 43: 07                             | 38. 9          |
| 220               | 2019/09/18                             | 11: 43: 10                             | 39. 5          |
| 221               | 2019/09/18                             | 11: 43: 13                             | 38. 9          |
| 222               | 2019/09/18                             | 11: 43: 16                             | 45. 4          |
| 223               | 2019/09/18                             | 11: 43: 19                             | 45. 1          |
| 224               | 2019/09/18                             | 11: 43: 22                             | 43. 8          |
| 225               | 2019/09/18                             | 11: 43: 25                             | 41. 9          |
| 226               | 2019/09/18                             | 11: 43: 28                             | 45. 2          |
| 227               | 2019/09/18                             | 11: 43: 31                             | 40. 9          |
| 228               | 2019/09/18                             | 11: 43: 34                             | 47. 5          |
| 229               | 2019/09/18                             | 11: 43: 37                             | 46. 7          |
| 230               | 2019/09/18                             | 11: 43: 40                             | 53. 0          |
| 231               | 2019/09/18                             | 11: 43: 43                             | 56. 1          |
| 232               | 2019/09/18                             | 11: 43: 46                             | 54. 3          |
| 233               | 2019/09/18                             | 11: 43: 49                             | 53. 2          |
| 234               | 2019/09/18                             | 11: 43: 52                             | 51. 2          |
| 235               | 2019/09/18                             | 11: 43: 55                             | 52. 8          |
| 236               | 2019/09/18                             | 11: 43: 58                             | 52. 4          |
| 237               | 2019/09/18                             | 11: 44: 01                             | 51. 4          |
| 238               | 2019/09/18                             | 11: 44: 04                             | 47. 9          |
| 239               | 2019/09/18                             | 11: 44: 07                             | 46. 5          |
| 240               | 2019/09/18                             | 11: 44: 10                             | 42. 3          |
| 241               | 2019/09/18                             | 11: 44: 13                             | 42. 9          |
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| 243               | 2019/09/18                             | 11: 44: 19                             | 37. 7          |
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| 245               | 2019/09/18                             | 11: 44: 25                             | 38. 9          |
| 246               | 2019/09/18                             | 11: 44: 28                             | 41. 4          |
| 247               | 2019/09/18                             | 11: 44: 31                             | 35. 9          |
| 248               | 2019/09/18                             | 11: 44: 34                             | 40. 2          |
| 249               | 2019/09/18                             | 11: 44: 37                             | 42. 3          |
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| 251               | 2019/09/18                             | 11: 44: 43                             | 45. 6          |
| 252               | 2019/09/18                             | 11: 44: 46                             | 53. 6          |
| 253               | 2019/09/18                             | 11: 44: 49                             | 45. 7          |
| 254               | 2019/09/18                             | 11: 44: 52                             | 43. 3          |
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| 256               | 2019/09/18                             | 11: 44: 58                             | 62. 6          |
| 257               | 2019/09/18                             | 11: 45: 01                             | 56. 6          |
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| 260<br>261        | 2019/09/18<br>2019/09/18<br>2019/09/18 | 11: 45: 10<br>11: 45: 13               | 38. 1<br>35. 4 |
| 262<br>263        | 2019/09/18<br>2019/09/18<br>2019/09/18 | 11: 45: 16<br>11: 45: 16<br>11: 45: 19 | 40. 7<br>37. 9 |
| 264<br>265        | 2019/09/18<br>2019/09/18<br>2019/09/18 | 11: 45: 22                             | 33. 4<br>33. 2 |
| 266               | 2019/09/18<br>2019/09/18<br>2019/09/18 | 11: 45: 25<br>11: 45: 28<br>11: 45: 31 | 34. 9<br>35. 3 |
| 267<br>268        | 2019/09/18                             | 11: 45: 34                             | 40. 3          |
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| 271               | 2019/09/18                             | 11: 45: 43                             | 48. 5          |
| 272               | 2019/09/18                             | 11: 45: 46                             | 48. 3          |
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| 276               | 2019/09/18<br>2019/09/18               | 11: 45: 58                             | 38. 6<br>40. 3 |
| 277               | 2019/09/18                             | 11: 46: 01                             | 35. 9          |
| 278               | 2019/09/18                             | 11: 46: 04                             | 41. 1          |
| 279               | 2019/09/18                             | 11: 46: 07                             | 42. 7          |
| 280               | 2019/09/18                             | 11: 46: 10                             | 42. 6          |
| 281               | 2019/09/18                             | 11: 46: 13                             | 47. 1          |
| 282               | 2019/09/18                             | 11: 46: 16                             | 43. 8          |
| 283               | 2019/09/18                             | 11: 46: 19                             | 46.8           |

| 284 | 2019/09/18 | 11: 46: 22 | 42. 9 |
|-----|------------|------------|-------|
| 285 | 2019/09/18 | 11: 46: 25 | 41. 5 |
| 286 | 2019/09/18 | 11: 46: 28 | 43.0  |
| 287 | 2019/09/18 | 11: 46: 31 | 45.0  |
| 288 | 2019/09/18 | 11: 46: 34 | 39. 7 |
| 289 | 2019/09/18 | 11: 46: 37 | 41.8  |
| 290 | 2019/09/18 | 11: 46: 40 | 43. 9 |
| 291 | 2019/09/18 | 11: 46: 43 | 46. 4 |
| 292 | 2019/09/18 | 11: 46: 46 | 50. 2 |
| 293 | 2019/09/18 | 11: 46: 49 | 57. 3 |
| 294 | 2019/09/18 | 11: 46: 52 | 65.3  |
| 295 | 2019/09/18 | 11: 46: 55 | 64. 7 |
| 296 | 2019/09/18 | 11: 46: 58 | 63. 7 |
| 297 | 2019/09/18 | 11: 47: 01 | 57. 1 |
| 298 | 2019/09/18 | 11: 47: 04 | 55. 6 |
| 299 | 2019/09/18 | 11: 47: 07 | 55. 5 |
| 300 | 2019/09/18 | 11: 47: 10 | 55.8  |

Freq Weight: A
Time Weight: SLOW
Level Range: 30-90
Max dB: 75.5 - 2019/09/18 13:46:06
Level Range: 30-90
SEL: 84.2
Leq: 54.7 ST3

| Leq:   | 54. 7   |  |  |
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|--|----------|--------------------------|--------------------------|----------------|
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| 94 2019/09/18 13: 48: 02 51. 9 96 2019/09/18 13: 48: 05 46. 9 97 2019/09/18 13: 48: 08 53. 4 97 2019/09/18 13: 48: 14 41. 3 99 2019/09/18 13: 48: 14 41. 3 100 2019/09/18 13: 48: 20 51. 3 101 2019/09/18 13: 48: 20 51. 3 101 2019/09/18 13: 48: 20 51. 3 102 2019/09/18 13: 48: 29 44. 1 103 2019/09/18 13: 48: 29 44. 1 104 2019/09/18 13: 48: 29 44. 1 105 2019/09/18 13: 48: 32 47. 1 105 2019/09/18 13: 48: 32 47. 1 106 2019/09/18 13: 48: 35 48. 1 107 2019/09/18 13: 48: 35 52. 48. 1 107 2019/09/18 13: 48: 44 41. 2 109 2019/09/18 13: 48: 44 41. 2 109 2019/09/18 13: 48: 44 41. 2 109 2019/09/18 13: 48: 50 53. 6 111 2019/09/18 13: 48: 50 53. 6 111 2019/09/18 13: 48: 55 52. 8 112 2019/09/18 13: 48: 59 54. 6 113 2019/09/18 13: 49: 02 47. 7 115 2019/09/18 13: 49: 02 47. 7 115 2019/09/18 13: 49: 05 58. 5 116 2019/09/18 13: 49: 10 58. 3 117 2019/09/18 13: 49: 10 58. 3 117 2019/09/18 13: 49: 10 58. 3 118 2019/09/18 13: 49: 10 58. 3 119 2019/09/18 13: 49: 10 58. 3 111 2019/09/18 13: 49: 10 58. 3 112 2019/09/18 13: 49: 10 58. 3 113 2019/09/18 13: 49: 10 58. 3 114 2019/09/18 13: 49: 10 58. 3 115 2019/09/18 13: 49: 10 58. 3 116 2019/09/18 13: 49: 10 58. 3 117 2019/09/18 13: 49: 10 58. 3 117 2019/09/18 13: 49: 10 58. 3 118 2019/09/18 13: 49: 10 58. 3 117 2019/09/18 13: 49: 10 58. 3 122 2019/09/18 13: 49: 10 58. 3 123 2019/09/18 13: 49: 10 58. 3 124 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 59: 20 45. 6 121 2019/09/18 13: 59: 20 45. 6 121 2019/09/18 13: 49: 49: 40 40: 40: 40: 40: 40: 40: 40: 40: 40:   | 92       | 2019/09/18               | 13: 47: 56               | 48. 3          |
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| 101 2019/09/18 13: 48: 23  | 99       | 2019/09/18               | 13: 48: 17               | 53.3           |
| 103  | 101      | 2019/09/18               | 13: 48: 23               | 48. 2          |
| 105 2019/09/18 13: 48: 35  | 103      | 2019/09/18               | 13: 48: 29               | 44. 1          |
| 107 2019/09/18 13: 48: 41 42. 3 108 2019/09/18 13: 48: 44 41. 3 110 2019/09/18 13: 48: 45 55 53. 6 111 2019/09/18 13: 48: 50 53. 6 111 2019/09/18 13: 48: 55 57. 6 113 2019/09/18 13: 48: 59 54. 9 114 2019/09/18 13: 49: 02 47. 7 115 2019/09/18 13: 49: 02 47. 7 115 2019/09/18 13: 49: 05 58. 5 116 2019/09/18 13: 49: 05 58. 5 116 2019/09/18 13: 49: 08 53. 3 117 2019/09/18 13: 49: 11 47. 5 118 2019/09/18 13: 49: 11 47. 6 118 2019/09/18 13: 49: 11 47. 6 119 2019/09/18 13: 49: 17 46. 8 120 2019/09/18 13: 49: 20 47. 5 120 2019/09/18 13: 49: 20 47. 5 121 2019/09/18 13: 49: 20 47. 5 122 2019/09/18 13: 49: 20 47. 5 123 2019/09/18 13: 49: 20 47. 5 124 2019/09/18 13: 49: 23 47. 5 125 2019/09/18 13: 49: 32 60. 3 125 2019/09/18 13: 49: 35 60. 3 125 2019/09/18 13: 49: 35 60. 3 125 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 44 57. 6 128 2019/09/18 13: 49: 41 57. 6 128 2019/09/18 13: 49: 44 62. 7 130 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 132 2019/09/18 13: 50: 05 47. 8 133 2019/09/18 13: 50: 05 47. 8 134 2019/09/18 13: 50: 05 48. 1 135 2019/09/18 13: 50: 20 47. 2 136 2019/09/18 13: 50: 20 47. 2 137 2019/09/18 13: 50: 20 47. 2 138 2019/09/18 13: 50: 24 44. 9 140 2019/09/18 13: 50: 24 44. 9 140 2019/09/18 13: 50: 24 44. 9 141 2019/09/18 13: 50: 24 44. 9 142 2019/09/18 13: 50: 34 44. 9 144 2019/09/18 13: 50: 35 49. 5 145 2019/09/18 13: 50: 34 44. 9 146 2019/09/18 13: 50: 34 44. 9 147 2019/09/18 13: 50: 34 44. 9 148 2019/09/18 13: 50: 34 44. 9 149 2019/09/18 13: 50: 34 44. 9 140 2019/09/18 13: 50: 34 44. 9 141 2019/09/18 13: 50: 35 49. 5 155 2019/09/18 13: 50: 41 40. 4 148 2019/09/18 13: 50: 50 141 2019/09/18 13: 50: 50 141 2019/09/18 13: 50: 50 141 2019/09/18 13: 50: 50 142 2019/09/18 13: 50: 50 143 2019/09/18 13: 50: 50 144 2019/09/18 13: 50: 50 145 2019/09/18 13: 50: 50 146 2019/09/18 13: 50: 50 147 2019/09/18 13: 50: 50 148 2019/09/18 13: 50: 41 149 2019/09/18 13: 50: 50 140 2019/09/18 13: 50: 50 141 2019/ | 105      | 2019/09/18               | 13: 48: 35               | 48. 1          |
| 109 2019/09/18 13: 48: 47 53. 6 111 2019/09/18 13: 48: 50 53. 6 112 2019/09/18 13: 48: 55 52. 8 112 2019/09/18 13: 48: 59 54. 9 114 2019/09/18 13: 49: 05 58. 5 116 2019/09/18 13: 49: 05 58. 5 116 2019/09/18 13: 49: 05 58. 5 116 2019/09/18 13: 49: 10 58. 5 116 2019/09/18 13: 49: 11 47. 5 118 2019/09/18 13: 49: 11 47. 5 118 2019/09/18 13: 49: 14 50. 8 119 2019/09/18 13: 49: 17 46. 8 119 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 122 2019/09/18 13: 49: 20 45. 6 123 2019/09/18 13: 49: 20 45. 6 124 2019/09/18 13: 49: 20 45. 6 125 2019/09/18 13: 49: 20 45. 6 126 2019/09/18 13: 49: 20 45. 6 127 2019/09/18 13: 49: 20 45. 6 128 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 44 62. 7 129 2019/09/18 13: 49: 44 62. 7 129 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 132 2019/09/18 13: 49: 50 57. 2 133 2019/09/18 13: 50: 05 46. 9 134 2019/09/18 13: 50: 05 48. 1 136 2019/09/18 13: 50: 05 48. 1 137 2019/09/18 13: 50: 05 48. 1 138 2019/09/18 13: 50: 14 52. 9 134 2019/09/18 13: 50: 14 52. 9 134 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 35 49. 5 142 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 34 49. 1 149 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 147 2019/09/18 13: 50: 50 40. 8 147 2019/09/18 13: 50: 50 40. 8 147 2019/09/18 13: 50: 50 40. 8 148 2019/09/18 13: 50: 44 49. 1 149 2019/09/18 13: 50: 50 40. 8 147 2019/09/18 13: 50: 50 40. 8 147 2019/09/18 13: 50: 50 40. 8 147 2019/09/18 13: 50: 50 40. 40. 4 149 2019/09/18 13: 50: 50 40. 8 147 2019/09/18 13: 50: 50 40. 8 147 2019/09/18 13: 50: 50 40. 8 147 2019/09/18 13: 50: 50 40. 8 149 2019/09/18 13: 50: 50 40. 8 140 2019/09/18 13: 50: 50 40. 8 141 2019/09/18 13: 50: 50 40. 8 141 2019/09/18 13: 50: 50 40. 8 141 2019/09/18 13: 50: 50 40. 8 141 2019/09/18 13: 50: 50  | 107      | 2019/09/18               | 13: 48: 41               | 42. 3          |
| 111 2019/09/18 13: 48: 53 52. 8 112 2019/09/18 13: 48: 59 114 2019/09/18 13: 49: 02 47. 7 115 2019/09/18 13: 49: 05 58. 5 116 2019/09/18 13: 49: 05 58. 5 116 2019/09/18 13: 49: 01 58. 3 117 2019/09/18 13: 49: 11 47. 5 118 2019/09/18 13: 49: 11 47. 5 118 2019/09/18 13: 49: 11 47. 5 120 2019/09/18 13: 49: 11 47. 5 120 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 20 45. 6 122 2019/09/18 13: 49: 20 45. 6 123 2019/09/18 13: 49: 20 45. 6 124 2019/09/18 13: 49: 20 53. 3 125 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 35 60. 3 127 2019/09/18 13: 49: 44 62. 7 129 2019/09/18 13: 49: 44 62. 7 130 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 132 2019/09/18 13: 49: 50 57. 2 133 2019/09/18 13: 49: 50 57. 2 135 2019/09/18 13: 50: 05 47. 8 137 2019/09/18 13: 50: 05 48. 1 138 2019/09/18 13: 50: 05 48. 1 139 2019/09/18 13: 50: 11 55. 7 138 2019/09/18 13: 50: 14 52. 9 134 2019/09/18 13: 50: 14 52. 9 135 2019/09/18 13: 50: 14 52. 9 140 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 20 50. 6 144 2019/09/18 13: 50: 20 50. 6 145 2019/09/18 13: 50: 20 50. 6 146 2019/09/18 13: 50: 32 47. 0 147 2019/09/18 13: 50: 32 47. 0 148 2019/09/18 13: 50: 32 47. 0 149 2019/09/18 13: 50: 34 49. 1 148 2019/09/18 13: 50: 44 49. 1 148 2019/09/18 13: 50: 44 49. 1 148 2019/09/18 13: 50: 50 151 2019/09/18 13: 50: 50 152 2019/09/18 13: 50: 50 153 2019/09/18 13: 50: 50 154 2019/09/18 13: 50: 50 155 2019/09/18 13: 50: 50 156 2019/09/18 13: 50: 50 157 2019/09/18 13: 50: 50 158 2019/09/18 13: 50: 50 159 2019/09/18 13: 50: 50 160 2019/09/18 13: 51: 14 49. 2 179 2019/09/18 13: 51: 35 140 2019/09/18 13: 51: 30 140 2019/09/18 13: 51: 30 141 2019/09/18 13: 51: 30 142 2019/09/18 13: 51: 30 143 2019/09/18 13: 52: 20 144  |          |                          | 13: 48: 47               | 54. 1          |
| 1112         2019/09/18         13: 48: 59         57. 6           113         2019/09/18         13: 49: 02         57. 6           115         2019/09/18         13: 49: 05         58. 5           116         2019/09/18         13: 49: 05         58. 5           116         2019/09/18         13: 49: 05         58. 5           116         2019/09/18         13: 49: 08         53. 3           117         2019/09/18         13: 49: 14         50. 8           118         2019/09/18         13: 49: 17         46. 8           120         2019/09/18         13: 49: 20         45. 6           121         2019/09/18         13: 49: 26         53. 3           122         2019/09/18         13: 49: 25         53. 3           123         2019/09/18         13: 49: 35         60. 3           124         2019/09/18         13: 49: 35         60. 3           127         2019/09/18         13: 49: 35         60. 3           127         2019/09/18         13: 49: 41         57. 6           128         2019/09/18         13: 49: 50         57. 2           130         2019/09/18         13: 49: 50         57. 2 <td< td=""><td></td><td></td><td></td><td></td></td<>   |          |                          |                          |                |
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| 116 2019/09/18 13: 49: 11 47. 5 118 2019/09/18 13: 49: 11 47. 5 118 2019/09/18 13: 49: 14 50. 8 119 2019/09/18 13: 49: 17 46. 8 119 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 26 53. 3 122 2019/09/18 13: 49: 26 53. 3 123 2019/09/18 13: 49: 29 53. 4 124 2019/09/18 13: 49: 35 60. 3 125 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 44 57. 6 128 2019/09/18 13: 49: 44 62. 7 129 2019/09/18 13: 49: 44 62. 7 129 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 132 2019/09/18 13: 49: 50 57. 2 133 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 50: 05 48. 1 136 2019/09/18 13: 50: 05 48. 1 137 2019/09/18 13: 50: 05 48. 1 138 2019/09/18 13: 50: 05 48. 1 139 2019/09/18 13: 50: 20 47. 2 135 2019/09/18 13: 50: 20 47. 2 135 2019/09/18 13: 50: 20 47. 2 135 2019/09/18 13: 50: 20 47. 2 135 2019/09/18 13: 50: 20 47. 2 135 2019/09/18 13: 50: 20 47. 2 136 2019/09/18 13: 50: 14 52. 9 140 2019/09/18 13: 50: 20 47. 2 141 2019/09/18 13: 50: 20 45. 7 142 2019/09/18 13: 50: 20 45. 7 144 2019/09/18 13: 50: 20 45. 7 145 2019/09/18 13: 50: 20 47. 2 145 2019/09/18 13: 50: 20 47. 2 145 2019/09/18 13: 50: 20 47. 2 146 2019/09/18 13: 50: 32 47. 0 147 2019/09/18 13: 50: 34 49. 5 146 2019/09/18 13: 50: 50 44 49. 1 149 2019/09/18 13: 50: 50 44 49. 1 149 2019/09/18 13: 50: 50 44 49. 1 140 2019/09/18 13: 50: 50 50 45. 3 152 2019/09/18 13: 50: 50 50 45. 3 154 2019/09/18 13: 50: 50 50 45. 3 155 2019/09/18 13: 50: 50 50 45. 3 156 2019/09/18 13: 50: 50 50 45. 3 157 2019/09/18 13: 50: 50 50 45. 3 158 2019/09/18 13: 50: 50 50 45. 3 159 2019/09/18 13: 50: 50 50 45. 3 150 2019/09/18 13: 50: 50 47 44. 0 160 2019/09/18 13: 50: 50 50 45. 3 151 2019/09/18 13: 50: 50 50 45. 3 152 2019/09/18 13: 50: 50 50 45. 3 157 2019/09/18 13: 50: 50 50 45. 3 158 2019/09/18 13: 51: 20 40. 8 177 2019/09/18 13: 51: 20 40. 8 177 2019/09/18 13: 51: 20 40. 8 177 2019/09/18 13: 51: 20 40. 8 178 2019/09/18 13: 51: 40 40. 40. 40. 40. 40. 40. 40. 40. 40.                  | 114      | 2019/09/18               | 13: 49: 02               | 47.7           |
| 118  | 116      | 2019/09/18               | 13: 49: 08               | 53. 3          |
| 120 2019/09/18 13: 49: 20 45. 6 121 2019/09/18 13: 49: 23 47. 5 122 2019/09/18 13: 49: 29 53. 4 123 2019/09/18 13: 49: 32 60. 3 125 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 35 67. 9 127 2019/09/18 13: 49: 35 67. 6 128 2019/09/18 13: 49: 41 57. 6 128 2019/09/18 13: 49: 44 62. 7 129 2019/09/18 13: 49: 45 55. 2 130 2019/09/18 13: 49: 50 57. 2 130 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 132 2019/09/18 13: 49: 50 57. 2 133 2019/09/18 13: 49: 50 57. 2 134 2019/09/18 13: 50: 02 47. 2 135 2019/09/18 13: 50: 02 47. 2 135 2019/09/18 13: 50: 05 48. 1 136 2019/09/18 13: 50: 05 48. 1 137 2019/09/18 13: 50: 11 55. 7 138 2019/09/18 13: 50: 14 52. 9 139 2019/09/18 13: 50: 14 52. 9 139 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 23 45. 7 142 2019/09/18 13: 50: 23 45. 7 142 2019/09/18 13: 50: 35 49. 5 144 2019/09/18 13: 50: 35 49. 5 145 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 34 49. 5 147 2019/09/18 13: 50: 35 49. 5 148 2019/09/18 13: 50: 35 49. 5 149 2019/09/18 13: 50: 35 49. 5 140 2019/09/18 13: 50: 35 49. 5 141 2019/09/18 13: 50: 35 49. 5 142 2019/09/18 13: 50: 35 49. 5 145 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 147 2019/09/18 13: 50: 35 49. 5 148 2019/09/18 13: 50: 50 50 6 153 2019/09/18 13: 50: 50 50 50. 6 153 2019/09/18 13: 50: 50 50 43. 7 157 2019/09/18 13: 50: 50 50 50. 6 153 2019/09/18 13: 50: 50 50 50. 6 154 2019/09/18 13: 50: 50 50 50. 6 155 2019/09/18 13: 51: 10 5 46. 2 156 2019/09/18 13: 51: 20 52. 0 161 2019/09/18 13: 51: 20 52. 0 161 2019/09/18 13: 51: 35 46. 2 170 2019/09/18 13: 51: 35 46. 2 171 2019/09/18 13: 51: 35 46. 2 172 2019/09/18 13: 51: 35 49. 3 174 2019/09/18 13: 51: 30 40. 3 175 2019/09/18 13: 51: 30 40. 3 176 2019/09/18 13: 51: 49 40. 4 177 2019/09/18 13: 51: 20 52. 0 161 2019/09/18 13: 51: 20 52. 0 161 2019/09/18 13: 51: 35 40. 3 171 2019/09/18 13: 51: 35 40. 3 172 2019/09/18 13: 51: 30 40. 3 173 2019/09/18 13: 51: 30 40. 3 174 2019/09/18 13: 51: 30 40. 3 175 2019/09/18 13: 51: 30 40. 3 177 2019/09/18 | 118      | 2019/09/18               | 13: 49: 14               | 50.8           |
| 122 2019/09/18 13: 49: 26 53. 3 125 2019/09/18 13: 49: 35 60. 3 125 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 35 60. 3 126 2019/09/18 13: 49: 41 57. 6 128 2019/09/18 13: 49: 41 57. 6 128 2019/09/18 13: 49: 41 57. 6 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 50 47. 8 133 2019/09/18 13: 49: 50 47. 8 133 2019/09/18 13: 50: 02 47. 2 135 2019/09/18 13: 50: 02 47. 2 135 2019/09/18 13: 50: 01 47. 2 135 2019/09/18 13: 50: 01 47. 2 137 2019/09/18 13: 50: 11 55. 7 138 2019/09/18 13: 50: 14 52. 9 40. 8 14 2019/09/18 13: 50: 23 45. 7 142 2019/09/18 13: 50: 23 45. 7 142 2019/09/18 13: 50: 24 47. 0 144 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 15 2019/09/18 13: 50: 56 50. 2 14 5 2019/09/18 13: 50: 56 50. 2 15 2019/09/18 13: 50: 56 50. 2 15 2019/09/18 13: 50: 56 50. 2 15 2019/09/18 13: 50: 56 50. 2 15 2019/09/18 13: 50: 56 50. 2 15 2019/09/18 13: 50: 56 50. 2 15 2019/09/18 13: 50: 56 50. 2 15 2019/09/18 13: 51: 05 40. 40. 4 149 2019/09/18 13: 50: 56 50. 2 15 2019/09/18 13: 51: 50: 50 43. 7 15 2019/09/18 13: 51: 50: 50 43. 7 15 2019/09/18 13: 51: 51 44 49. 1 15 2019/09/18 13: 51: 51 50 50 43. 7 15 2019/09/18 13: 51: 51 50 50 43. 7 15 2019/09/18 13: 51: 51 50 50 40. 8 47. 7 15 2019/09/18 13: 51: 51 50 50 40. 8 47. 7 15 2019/09/18 13: 51: 50 50 40. 8 47. 7 15 2019/09/18 13: 51: 50 50 40. 8 47. 7 17 2019/09/18 13: 51: 51 44 49. 2 14 49. | 120      | 2019/09/18               | 13: 49: 20               | 45. 6          |
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| 127 2019/09/18 13: 49: 41 57. 6 128 2019/09/18 13: 49: 44 55. 2 130 2019/09/18 13: 49: 50 57. 2 131 2019/09/18 13: 49: 56 132 2019/09/18 13: 49: 56 133 2019/09/18 13: 50: 02 47. 2 135 2019/09/18 13: 50: 05 48. 1 136 2019/09/18 13: 50: 05 48. 1 136 2019/09/18 13: 50: 01 55. 7 138 2019/09/18 13: 50: 01 55. 7 138 2019/09/18 13: 50: 11 55. 7 138 2019/09/18 13: 50: 11 55. 7 138 2019/09/18 13: 50: 11 55. 7 138 2019/09/18 13: 50: 11 55. 7 144 2019/09/18 13: 50: 20 50. 6 141 2019/09/18 13: 50: 23 45. 7 142 2019/09/18 13: 50: 23 45. 7 142 2019/09/18 13: 50: 23 45. 7 142 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 35 49. 5 146 2019/09/18 13: 50: 44 49. 1 149 2019/09/18 13: 50: 47 44. 0 149 2019/09/18 13: 50: 50 47 144 2019/09/18 13: 50: 50 47 145 2019/09/18 13: 50: 50 47 146 2019/09/18 13: 50: 50 47 147 2019/09/18 13: 50: 50 47 148 2019/09/18 13: 50: 50 47 149 2019/09/18 13: 50: 50 47 140 2019/09/18 13: 50: 50 47 141 2019/09/18 13: 50: 50 47 142 2019/09/18 13: 50: 50 153 2019/09/18 13: 50: 50 154 2019/09/18 13: 50: 50 155 2019/09/18 13: 51: 05 46. 2 156 2019/09/18 13: 51: 05 46. 2 157 2019/09/18 13: 51: 05 46. 2 158 2019/09/18 13: 51: 05 46. 2 159 2019/09/18 13: 51: 50 160 2019/09/18 13: 51: 51 160 2019/09/18 13: 51: 51 17 49. 0 180 2019/09/18 13: 51: 51 180 2019/09/18 13: 51: 50 180 2019/09/18 13: 52: 20 181 2019/09/18 13: 52: 20 182 2019/09/18 13: 52: 20 183 2019/09/18 13: 52: 20 184 2019/09/18 13: 52: 20 185 2019/09/18 13: 52: 20 187 2019/09/18 13: 52: 20 188 2019/09/18 |          |                          |                          |                |
| 129 2019/09/18 13: 49: 47 130 2019/09/18 13: 49: 50 131 2019/09/18 13: 49: 56 132 2019/09/18 13: 49: 56 133 2019/09/18 13: 49: 59 134 2019/09/18 13: 50: 02 135 2019/09/18 13: 50: 05 136 2019/09/18 13: 50: 05 137 2019/09/18 13: 50: 11 136 2019/09/18 13: 50: 11 137 2019/09/18 13: 50: 11 138 2019/09/18 13: 50: 17 140 2019/09/18 13: 50: 17 140 2019/09/18 13: 50: 20 141 2019/09/18 13: 50: 20 142 2019/09/18 13: 50: 20 143 2019/09/18 13: 50: 20 144 2019/09/18 13: 50: 24 145 2019/09/18 13: 50: 29 146 2019/09/18 13: 50: 35 146 2019/09/18 13: 50: 35 146 2019/09/18 13: 50: 35 146 2019/09/18 13: 50: 35 147 2019/09/18 13: 50: 41 148 2019/09/18 13: 50: 44 149 2019/09/18 13: 50: 50 145 2019/09/18 13: 50: 50 147 2019/09/18 13: 50: 50 148 2019/09/18 13: 50: 50 149 2019/09/18 13: 50: 50 151 2019/09/18 13: 50: 50 152 2019/09/18 13: 50: 50 153 2019/09/18 13: 50: 50 154 2019/09/18 13: 50: 50 155 2019/09/18 13: 51: 02 155 2019/09/18 13: 51: 02 156 2019/09/18 13: 51: 03 157 2019/09/18 13: 51: 04 149 2019/09/18 13: 51: 05 156 2019/09/18 13: 51: 05 157 2019/09/18 13: 51: 05 158 2019/09/18 13: 51: 08 157 2019/09/18 13: 51: 50 160 2019/09/18 13: 51: 51 177 2019/09/18 13: 51: 51 18 2019/09/18 13: 51: 51 19 2019/09/18 13: 51: 51 10 2019/09/18 13: 51: 51 10 2019/09/18 13: 51: 51 10 2019/09/18 13: 51: 51 11 50 12 2019/09/18 13: 51: 51 14 49. 2 159 2019/09/18 13: 51: 51 14 49. 2 159 2019/09/18 13: 51: 51 14 49. 2 150 2019/09/18 13: 51: 51 14 49. 2 150 2019/09/18 13: 51: 51 14 49. 2 150 2019/09/18 13: 51: 51 150 2019/09/18 13: 51: 51 151 2019/09/18 13: 51: 32 152 2019/09/18 13: 51: 34 172 2019/09/18 13: 51: 34 173 2019/09/18 13: 51: 51 174 2019/09/18 13: 51: 51 175 2019/09/18 13: 51: 51 176 2019/09/18 13: 51: 51 177 2019/09/18 13: 52: 20 178 2019/09/18 13: 52: 20 179 2019/09/18 13: 52: 20 170 2019/09/18 13: 52: 20 171 2019/09/18 13: 52: 20 172 2019/09/18 13: 52: 20 173 2019/09/18 13: 52: 20 174 2019/09/18 13: 52: 20 175 2019/09/18 13: 52: 20 176 2019/09/18 13: 52: 20 177 2019/09/18 13: 52: 20 178 2019/09/18 13: 52: 20 179 2019/09/18 13: 52: 20 | 127      | 2019/09/18               | 13: 49: 41               | 57. 6          |
| 131       2019/09/18       13: 49: 56       47. 8         132       2019/09/18       13: 49: 59       46. 9         134       2019/09/18       13: 50: 02       47. 2         135       2019/09/18       13: 50: 05       48. 1         136       2019/09/18       13: 50: 01       55. 7         138       2019/09/18       13: 50: 14       52. 9         139       2019/09/18       13: 50: 20       50. 6         141       2019/09/18       13: 50: 20       50. 6         141       2019/09/18       13: 50: 20       50. 6         141       2019/09/18       13: 50: 20       50. 6         141       2019/09/18       13: 50: 20       50. 6         141       2019/09/18       13: 50: 20       40. 8         142       2019/09/18       13: 50: 20       40. 8         144       2019/09/18       13: 50: 32       47. 0         145       2019/09/18       13: 50: 35       49. 5         144       2019/09/18       13: 50: 34       40. 4         148       2019/09/18       13: 50: 50       43. 7         150       2019/09/18       13: 50: 50       43. 7         151 <t< td=""><td>129</td><td>2019/09/18</td><td>13: 49: 47</td><td>55. 2</td></t<>  | 129      | 2019/09/18               | 13: 49: 47               | 55. 2          |
| 133       2019/09/18       13: 49: 59       46. 9         134       2019/09/18       13: 50: 05       48. 1         136       2019/09/18       13: 50: 08       41. 5         137       2019/09/18       13: 50: 11       55. 7         138       2019/09/18       13: 50: 14       52. 9         139       2019/09/18       13: 50: 20       50. 6         141       2019/09/18       13: 50: 23       45. 7         142       2019/09/18       13: 50: 29       40. 8         143       2019/09/18       13: 50: 32       47. 0         144       2019/09/18       13: 50: 32       47. 0         145       2019/09/18       13: 50: 32       47. 0         145       2019/09/18       13: 50: 32       47. 0         145       2019/09/18       13: 50: 32       47. 0         146       2019/09/18       13: 50: 34       49. 5         146       2019/09/18       13: 50: 34       49. 5         146       2019/09/18       13: 50: 54       49. 4         148       2019/09/18       13: 50: 50       43. 7         150       2019/09/18       13: 50: 50       43. 7         151 <t< td=""><td>131</td><td>2019/09/18</td><td>13: 49: 53</td><td>52. 9</td></t<>  | 131      | 2019/09/18               | 13: 49: 53               | 52. 9          |
| 135       2019/09/18       13: 50: 05       48. 1         136       2019/09/18       13: 50: 11       55.         137       2019/09/18       13: 50: 14       52. 9         138       2019/09/18       13: 50: 17       44. 9         140       2019/09/18       13: 50: 20       50. 6         141       2019/09/18       13: 50: 20       45. 7         142       2019/09/18       13: 50: 26       41. 2         143       2019/09/18       13: 50: 29       40. 8         144       2019/09/18       13: 50: 32       47. 0         145       2019/09/18       13: 50: 35       49. 5         144       2019/09/18       13: 50: 35       49. 5         145       2019/09/18       13: 50: 38       43. 0         147       2019/09/18       13: 50: 44       49. 1         149       2019/09/18       13: 50: 50       43. 7         150       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 51: 05       46. 2         153       2019/09/18       13: 51: 02       42. 8         155  | 133      | 2019/09/18               | 13: 49: 59               | 46. 9          |
| 137       2019/09/18       13: 50: 11       55. 7         138       2019/09/18       13: 50: 17       44. 9         139       2019/09/18       13: 50: 20       50. 6         141       2019/09/18       13: 50: 23       45. 7         142       2019/09/18       13: 50: 29       40. 8         143       2019/09/18       13: 50: 32       47. 0         144       2019/09/18       13: 50: 32       47. 0         145       2019/09/18       13: 50: 35       49. 5         146       2019/09/18       13: 50: 34       40. 4         147       2019/09/18       13: 50: 44       49. 1         148       2019/09/18       13: 50: 50       43. 7         150       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 50       43. 7         152       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 50       43. 7         152       2019/09/18       13: 50: 50       43. 7         153       2019/09/18       13: 51: 02       42. 8         152       2019/09/18       13: 51: 02       42. 8         153 <t< td=""><td>135</td><td>2019/09/18</td><td>13: 50: 05</td><td>48. 1</td></t<>  | 135      | 2019/09/18               | 13: 50: 05               | 48. 1          |
| 139       2019/09/18       13: 50: 17       44. 9         140       2019/09/18       13: 50: 20       50. 6         141       2019/09/18       13: 50: 23       45. 7         142       2019/09/18       13: 50: 29       40. 8         144       2019/09/18       13: 50: 32       47. 0         145       2019/09/18       13: 50: 35       49. 5         146       2019/09/18       13: 50: 38       43. 0         147       2019/09/18       13: 50: 44       49. 1         149       2019/09/18       13: 50: 44       49. 1         149       2019/09/18       13: 50: 50       43. 7         150       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 50       45. 3         152       2019/09/18       13: 50: 50       45. 3         152       2019/09/18       13: 51: 05       46. 2         153       2019/09/18       13: 51: 05       46. 2         155       2019/09/18       13: 51: 05       46. 2         156       2019/09/18       13: 51: 14       49. 2         159 <t< td=""><td>137</td><td>2019/09/18</td><td>13: 50: 11</td><td>55. 7</td></t<>  | 137      | 2019/09/18               | 13: 50: 11               | 55. 7          |
| 141       2019/09/18       13: 50: 23       45. 7         142       2019/09/18       13: 50: 26       41. 2         143       2019/09/18       13: 50: 32       47. 0         144       2019/09/18       13: 50: 35       49. 5         145       2019/09/18       13: 50: 38       43. 0         147       2019/09/18       13: 50: 41       40. 4         148       2019/09/18       13: 50: 44       49. 1         149       2019/09/18       13: 50: 50       43. 7         150       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 50       43. 7         152       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 50       43. 7         152       2019/09/18       13: 50: 50       43. 7         153       2019/09/18       13: 50: 50       45. 3         154       2019/09/18       13: 51: 02       42. 8         155       2019/09/18       13: 51: 02       42. 8         156       2019/09/18       13: 51: 14       49. 2         157       2019/09/18       13: 51: 14       49. 2         159 <t< td=""><td></td><td>2019/09/18</td><td></td><td></td></t<>  |          | 2019/09/18               |                          |                |
| 142       2019/09/18       13: 50: 26       41. 2         143       2019/09/18       13: 50: 32       47. 0         144       2019/09/18       13: 50: 35       49. 5         146       2019/09/18       13: 50: 41       40. 4         147       2019/09/18       13: 50: 44       49. 1         148       2019/09/18       13: 50: 44       49. 1         149       2019/09/18       13: 50: 50       43. 7         150       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 50       43. 7         152       2019/09/18       13: 50: 50       43. 7         153       2019/09/18       13: 50: 50       43. 7         154       2019/09/18       13: 50: 50       45. 3         154       2019/09/18       13: 51: 02       42. 8         155       2019/09/18       13: 51: 05       46. 2         155       2019/09/18       13: 51: 08       47. 7         157       2019/09/18       13: 51: 11       51. 0         158       2019/09/18       13: 51: 17       49. 0         160       2019/09/18       13: 51: 23       44. 9         161 <t< td=""><td></td><td></td><td></td><td></td></t<>  |          |                          |                          |                |
| 144       2019/09/18       13: 50: 32       47. 0         145       2019/09/18       13: 50: 38       43. 0         146       2019/09/18       13: 50: 41       40. 4         147       2019/09/18       13: 50: 41       40. 4         148       2019/09/18       13: 50: 50       43. 7         150       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 53       48. 8         152       2019/09/18       13: 50: 56       50. 2         153       2019/09/18       13: 50: 59       45. 3         154       2019/09/18       13: 51: 05       46. 2         155       2019/09/18       13: 51: 05       46. 2         155       2019/09/18       13: 51: 10       46. 2         156       2019/09/18       13: 51: 11       51. 0         157       2019/09/18       13: 51: 14       49. 2         159       2019/09/18       13: 51: 17       49. 0         161       2019/09/18       13: 51: 17       49. 0         161       2019/09/18       13: 51: 20       51. 3         162       2019/09/18       13: 51: 32       44. 9         163 <t< td=""><td></td><td></td><td>13: 50: 26</td><td></td></t<>  |          |                          | 13: 50: 26               |                |
| 146       2019/09/18       13: 50: 38       43. 0         147       2019/09/18       13: 50: 44       40. 4         148       2019/09/18       13: 50: 47       44. 0         150       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 53       48. 8         152       2019/09/18       13: 50: 56       50. 2         153       2019/09/18       13: 51: 02       42. 8         155       2019/09/18       13: 51: 05       46. 2         155       2019/09/18       13: 51: 08       47. 7         157       2019/09/18       13: 51: 08       47. 7         157       2019/09/18       13: 51: 08       47. 7         157       2019/09/18       13: 51: 11       51. 0         158       2019/09/18       13: 51: 14       49. 2         159       2019/09/18       13: 51: 20       52. 0         160       2019/09/18       13: 51: 23       44. 9         162       2019/09/18       13: 51: 23       44. 9         163       2019/09/18       13: 51: 29       51. 3         164       2019/09/18       13: 51: 35       46. 1         166 <t< td=""><td>144</td><td>2019/09/18</td><td>13: 50: 32</td><td>47.0</td></t<>   | 144      | 2019/09/18               | 13: 50: 32               | 47.0           |
| 148       2019/09/18       13: 50: 44       49. 1         149       2019/09/18       13: 50: 50       43. 7         150       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 56       50. 2         153       2019/09/18       13: 50: 59       45. 3         154       2019/09/18       13: 51: 05       46. 2         155       2019/09/18       13: 51: 05       46. 2         156       2019/09/18       13: 51: 10       47. 7         157       2019/09/18       13: 51: 11       51. 0         158       2019/09/18       13: 51: 17       49. 0         160       2019/09/18       13: 51: 17       49. 0         161       2019/09/18       13: 51: 20       52. 0         161       2019/09/18       13: 51: 23       44. 9         162       2019/09/18       13: 51: 23       44. 9         163       2019/09/18       13: 51: 20       51. 3         164       2019/09/18       13: 51: 32       48. 5         165       2019/09/18       13: 51: 32       46. 1         166       2019/09/18       13: 51: 34       47. 6         167 <t< td=""><td>146</td><td>2019/09/18</td><td>13: 50: 38</td><td>43.0</td></t<>   | 146      | 2019/09/18               | 13: 50: 38               | 43.0           |
| 150       2019/09/18       13: 50: 50       43. 7         151       2019/09/18       13: 50: 53       48. 8         152       2019/09/18       13: 50: 59       45. 3         154       2019/09/18       13: 51: 02       42. 8         155       2019/09/18       13: 51: 05       46. 2         156       2019/09/18       13: 51: 08       47. 7         157       2019/09/18       13: 51: 11       51. 0         158       2019/09/18       13: 51: 14       49. 2         159       2019/09/18       13: 51: 17       49. 0         160       2019/09/18       13: 51: 20       52. 0         161       2019/09/18       13: 51: 23       44. 9         162       2019/09/18       13: 51: 23       44. 9         163       2019/09/18       13: 51: 29       51. 3         164       2019/09/18       13: 51: 32       48. 5         165       2019/09/18       13: 51: 35       46. 1         166       2019/09/18       13: 51: 35       46. 1         166       2019/09/18       13: 51: 35       46. 1         166       2019/09/18       13: 51: 35       46. 1         166 <t< td=""><td>148</td><td>2019/09/18</td><td>13: 50: 44</td><td>49. 1</td></t<>  | 148      | 2019/09/18               | 13: 50: 44               | 49. 1          |
| 152       2019/09/18       13: 50: 56       50. 2         153       2019/09/18       13: 50: 59       45. 3         154       2019/09/18       13: 51: 02       42. 8         155       2019/09/18       13: 51: 05       46. 2         156       2019/09/18       13: 51: 108       47. 7         157       2019/09/18       13: 51: 11       51. 0         158       2019/09/18       13: 51: 17       49. 0         160       2019/09/18       13: 51: 20       52. 0         161       2019/09/18       13: 51: 23       44. 9         162       2019/09/18       13: 51: 23       44. 9         162       2019/09/18       13: 51: 29       51. 3         163       2019/09/18       13: 51: 32       48. 5         164       2019/09/18       13: 51: 32       48. 5         165       2019/09/18       13: 51: 34       47. 6         166       2019/09/18       13: 51: 34       47. 6         168       2019/09/18       13: 51: 44       47. 0         168       2019/09/18       13: 51: 50       38. 8         171       2019/09/18       13: 51: 50       38. 8         171       <   | 150      | 2019/09/18               | 13: 50: 50               | 43.7           |
| 154         2019/09/18         13:51:02         42.8           155         2019/09/18         13:51:05         46.2           156         2019/09/18         13:51:08         47.7           157         2019/09/18         13:51:11         51.0           158         2019/09/18         13:51:17         49.0           159         2019/09/18         13:51:17         49.0           160         2019/09/18         13:51:20         52.0           161         2019/09/18         13:51:23         44.9           162         2019/09/18         13:51:29         51.3           163         2019/09/18         13:51:32         48.5           163         2019/09/18         13:51:32         48.5           165         2019/09/18         13:51:35         46.1           166         2019/09/18         13:51:35         46.1           167         2019/09/18         13:51:44         47.0           168         2019/09/18         13:51:47         39.2           170         2019/09/18         13:51:50         38.8           171         2019/09/18         13:51:50         38.8           171         2019/09/18         13   | 152      | 2019/09/18               | 13: 50: 56               | 50. 2          |
| 156         2019/09/18         13: 51: 08         47. 7           157         2019/09/18         13: 51: 11         51. 0           158         2019/09/18         13: 51: 17         49. 0           159         2019/09/18         13: 51: 17         49. 0           160         2019/09/18         13: 51: 20         52. 0           161         2019/09/18         13: 51: 23         44. 9           162         2019/09/18         13: 51: 23         44. 9           163         2019/09/18         13: 51: 29         51. 2           163         2019/09/18         13: 51: 29         51. 2           164         2019/09/18         13: 51: 29         51. 2           165         2019/09/18         13: 51: 32         48. 5           165         2019/09/18         13: 51: 35         46. 1           166         2019/09/18         13: 51: 34         47. 6           167         2019/09/18         13: 51: 44         47. 0           168         2019/09/18         13: 51: 50         38. 8           171         2019/09/18         13: 51: 50         38. 8           171         2019/09/18         13: 51: 50         48. 7  | 154      | 2019/09/18               | 13: 51: 02               | 42.8           |
| 157       2019/09/18       13: 51: 11       49. 2         158       2019/09/18       13: 51: 17       49. 0         159       2019/09/18       13: 51: 17       49. 0         160       2019/09/18       13: 51: 20       52. 0         161       2019/09/18       13: 51: 23       44. 9         162       2019/09/18       13: 51: 29       51. 2         163       2019/09/18       13: 51: 32       48. 5         164       2019/09/18       13: 51: 32       48. 5         165       2019/09/18       13: 51: 35       46. 1         166       2019/09/18       13: 51: 34       47. 6         167       2019/09/18       13: 51: 44       47. 0         168       2019/09/18       13: 51: 44       47. 0         169       2019/09/18       13: 51: 50       38. 8         171       2019/09/18       13: 51: 50       38. 8         171       2019/09/18       13: 51: 50       38. 8         172       2019/09/18       13: 51: 50       48. 7         173       2019/09/18       13: 52: 53       42. 4         174       2019/09/18       13: 52: 05       38. 5         175 <t< td=""><td></td><td></td><td></td><td></td></t<>  |          |                          |                          |                |
| 159       2019/09/18       13: 51: 17       49. 0         160       2019/09/18       13: 51: 20       52. 0         161       2019/09/18       13: 51: 23       44. 9         162       2019/09/18       13: 51: 26       51. 2         163       2019/09/18       13: 51: 32       48. 5         164       2019/09/18       13: 51: 35       46. 1         165       2019/09/18       13: 51: 38       47. 6         166       2019/09/18       13: 51: 44       47. 0         168       2019/09/18       13: 51: 44       47. 0         169       2019/09/18       13: 51: 50       38. 8         170       2019/09/18       13: 51: 50       38. 8         171       2019/09/18       13: 51: 50       38. 8         172       2019/09/18       13: 51: 50       42. 4         173       2019/09/18       13: 51: 50       48. 7         174       2019/09/18       13: 52: 02       38. 9         175       2019/09/18       13: 52: 05       38. 5         176       2019/09/18       13: 52: 08       35. 7         177       2019/09/18       13: 52: 11       49. 7         179 <t< td=""><td></td><td></td><td>13: 51: 11</td><td>49. 2</td></t<>   |          |                          | 13: 51: 11               | 49. 2          |
| 161       2019/09/18       13: 51: 23       44. 9         162       2019/09/18       13: 51: 26       51. 2         163       2019/09/18       13: 51: 32       48. 5         164       2019/09/18       13: 51: 35       46. 1         165       2019/09/18       13: 51: 38       47. 6         166       2019/09/18       13: 51: 41       46. 0         168       2019/09/18       13: 51: 44       47. 0         169       2019/09/18       13: 51: 50       38. 8         171       2019/09/18       13: 51: 50       38. 8         171       2019/09/18       13: 51: 53       42. 4         172       2019/09/18       13: 51: 50       38. 8         171       2019/09/18       13: 51: 50       38. 8         172       2019/09/18       13: 51: 50       48. 7         173       2019/09/18       13: 52: 02       38. 9         175       2019/09/18       13: 52: 05       38. 5         176       2019/09/18       13: 52: 05       38. 5         177       2019/09/18       13: 52: 11       49. 7         179       2019/09/18       13: 52: 21       49. 7         180 <t< td=""><td>159</td><td>2019/09/18</td><td>13: 51: 17</td><td>49.0</td></t<>   | 159      | 2019/09/18               | 13: 51: 17               | 49.0           |
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| 176       2019/09/18       13: 52: 08       35. 7         177       2019/09/18       13: 52: 11       34. 9         178       2019/09/18       13: 52: 14       49. 7         179       2019/09/18       13: 52: 17       41. 9         180       2019/09/18       13: 52: 20       42. 4         181       2019/09/18       13: 52: 23       57. 0         182       2019/09/18       13: 52: 26       48. 0         183       2019/09/18       13: 52: 29       49. 0  | 174      | 2019/09/18               | 13: 52: 02               | 38. 9          |
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| 180     2019/09/18     13: 52: 20     42. 4       181     2019/09/18     13: 52: 23     57. 0       182     2019/09/18     13: 52: 26     48. 0       183     2019/09/18     13: 52: 29     49. 0  | 178      | 2019/09/18               | 13: 52: 14               | 49. 7          |
| 182 2019/09/18 13: 52: 26 48. 0<br>183 2019/09/18 13: 52: 29 49. 0   | 180      | 2019/09/18               | 13: 52: 20               | 42.4           |
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| 292 | 2019/09/18 | 13: 57: 56 | 39. 6 |
| 293 | 2019/09/18 | 13: 57: 59 | 40. 7 |
| 294 | 2019/09/18 | 13: 58: 02 | 49. 9 |
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Freq Weight: A
Time Weight: SLOW
Level Range: 30-90
Max dB: 86.8 - 2019/09/18 13:06:01
Level Range: 30-90
SEL: 92.3
Leg: 62.8 ST4

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| 295 | 2019/09/18 | 13: 16: 41 | 69. 7 |
| 296 | 2019/09/18 | 13: 16: 44 | 57. 6 |
| 297 | 2019/09/18 | 13: 16: 47 | 48. 6 |
| 298 | 2019/09/18 | 13: 16: 50 | 45. 6 |
| 299 | 2019/09/18 | 13: 16: 53 | 48. 3 |
| 300 | 2019/09/18 | 13: 16: 56 | 47. 4 |
|     |            |            |       |

## Appendix B

Roadway Construction Noise Model (RCNM) Results

Report date: 9/11/2019

Case Descripti Bellefield Solar - Construction on Parcels

---- Receptor #1 ----

Baselines (dBA)

Description Land Use Daytime Evening Night
Residential Residential 75 75 75

Equipment Spec Actual Receptor Estimated **Impact** Lmax Lmax Distance Shielding (feet) Description Device Usage(%) (dBA) (dBA) (dBA) Auger Drill Rig 20 84.4 1300 0 No Backhoe No 40 77.6 1300 0 Compactor (ground) 20 83.2 1300 0 No Concrete Mixer Truck 78.8 0 No 40 1300 80.6 1300 0 Crane No 16 Dozer No 40 81.7 1300 0 **Dump Truck** 40 76.5 1300 0 No 80.7 0 Excavator No 40 1300 Flat Bed Truck 40 74.3 1300 0 No Front End Loader 79.1 0 40 1300 No Generator 50 80.6 1300 0 No Grader 85 0 No 40 1300 Pickup Truck No 40 75 1300 0 0 **Pneumatic Tools** No 50 85.2 1300 Roller 20 80 1300 0 No 0 Scraper No 40 83.6 1300 Warning Horn 5 83.2 1300 0 No Welder / Torch 40 74 1300 0 No

## Calculated (dBA)

| Equipment            | *Lmax | Leq |      |
|----------------------|-------|-----|------|
| Auger Drill Rig      | 56.1  |     | 49.1 |
| Backhoe              | 49.3  |     | 45.3 |
| Compactor (ground)   | 54.9  |     | 47.9 |
| Concrete Mixer Truck | 50.5  |     | 46.5 |
| Crane                | 52.3  |     | 44.3 |
| Dozer                | 53.4  |     | 49.4 |
| Dump Truck           | 48.2  |     | 44.2 |
| Excavator            | 52.4  |     | 48.4 |
| Flat Bed Truck       | 46    |     | 42   |
| Front End Loader     | 50.8  |     | 46.8 |

| Generator       | 52.3 | 49.3 |
|-----------------|------|------|
| Grader          | 56.7 | 52.7 |
| Pickup Truck    | 46.7 | 42.7 |
| Pneumatic Tools | 56.9 | 53.9 |
| Roller          | 51.7 | 44.7 |
| Scraper         | 55.3 | 51.3 |
| Warning Horn    | 54.9 | 41.9 |
| Welder / Torch  | 45.7 | 41.7 |
| Total           | 56.9 | 60.9 |

<sup>\*</sup>Calculated Lmax is the Loudest value.

Report date: 9/11/2019

Case Descriptio Kudu Solar - Construction on Parcels

---- Receptor #1 ----

Baselines (dBA)

Description Land Use Daytime Evening Night
Residential Residential 75 75 75

Equipment

|                      |        |          | -1 - 1- |    |        |          |           |
|----------------------|--------|----------|---------|----|--------|----------|-----------|
|                      |        |          | Spec    |    | Actual | Receptor | Estimated |
|                      | Impact |          | Lmax    |    | Lmax   | Distance | Shielding |
| Description          | Device | Usage(%) | (dBA)   |    | (dBA)  | (feet)   | (dBA)     |
| Auger Drill Rig      | No     | 20       | 1       |    | 84.4   | 3250     | 0         |
| Backhoe              | No     | 40       | 1       |    | 77.6   | 3250     | 0         |
| Compactor (ground)   | No     | 20       | 1       |    | 83.2   | 3250     | 0         |
| Concrete Mixer Truck | No     | 40       | 1       |    | 78.8   | 3250     | 0         |
| Crane                | No     | 16       | i       |    | 80.6   | 3250     | 0         |
| Dozer                | No     | 40       | 1       |    | 81.7   | 3250     | 0         |
| Dump Truck           | No     | 40       | 1       |    | 76.5   | 3250     | 0         |
| Excavator            | No     | 40       | 1       |    | 80.7   | 3250     | 0         |
| Flat Bed Truck       | No     | 40       | 1       |    | 74.3   | 3250     | 0         |
| Front End Loader     | No     | 40       | 1       |    | 79.1   | 3250     | 0         |
| Generator            | No     | 50       | 1       |    | 80.6   | 3250     | 0         |
| Grader               | No     | 40       | 1       | 85 |        | 3250     | 0         |
| Pickup Truck         | No     | 40       | 1       |    | 75     | 3250     | 0         |
| Pneumatic Tools      | No     | 50       | 1       |    | 85.2   | 3250     | 0         |
| Roller               | No     | 20       | 1       |    | 80     | 3250     | 0         |
| Scraper              | No     | 40       | 1       |    | 83.6   | 3250     | 0         |
| Warning Horn         | No     | 5        |         |    | 83.2   | 3250     | 0         |
| Welder / Torch       | No     | 40       |         |    | 74     | 3250     | 0         |
|                      |        |          |         |    |        |          |           |

## Calculated (dBA)

| Equipment            | *Lmax | Leq      |      |
|----------------------|-------|----------|------|
| Auger Drill Rig      | 48.1  |          | 41.1 |
| Backhoe              | 41.3  | ,        | 37.3 |
| Compactor (ground)   | 47    | ,        | 40   |
| Concrete Mixer Truck | 42.5  | ,        | 38.6 |
| Crane                | 44.3  | ,        | 36.3 |
| Dozer                | 45.4  | <u>.</u> | 41.4 |
| Dump Truck           | 40.2  |          | 36.2 |
| Excavator            | 44.5  | ,        | 40.5 |
| Flat Bed Truck       | 38    | }        | 34   |
| Front End Loader     | 42.9  | )        | 38.9 |

| Generator       | 44.4 | 41.4 |
|-----------------|------|------|
| Grader          | 48.7 | 44.8 |
| Pickup Truck    | 38.7 | 34.8 |
| Pneumatic Tools | 48.9 | 45.9 |
| Roller          | 43.7 | 36.8 |
| Scraper         | 47.3 | 43.3 |
| Warning Horn    | 46.9 | 33.9 |
| Welder / Torch  | 37.7 | 33.8 |
| Total           | 48.9 | 52.9 |

<sup>\*</sup>Calculated Lmax is the Loudest value.

## Roadway Construction Noise Model (RCNM), Version 1.1

Report date: 9/11/2019

Case Description: Bellefield Solar - Gen Tie Construction

---- Receptor #1 ----

Baselines (dBA)

Description Land Use Daytime Evening Night
Residential Residential 75 75 75

Equipment

|                      |        | Spec           | Actual | Receptor | Estimated |
|----------------------|--------|----------------|--------|----------|-----------|
|                      | Impact | Lmax           | Lmax   | Distance | Shielding |
| Description          | Device | Usage(%) (dBA) | (dBA)  | (feet)   | (dBA)     |
| Auger Drill Rig      | No     | 20             | 84.    | 4 50     | 0         |
| Front End Loader     | No     | 40             | 79.    | 1 50     | 0         |
| Grader               | No     | 40             | 85     | 50       | 0         |
| Pickup Truck         | No     | 40             | 7      | 5 50     | 0         |
| Crane                | No     | 16             | 80.    | 6 50     | 0         |
| Concrete Mixer Truck | No     | 40             | 78.    | 8 50     | 0         |

## Calculated (dBA)

| Equipment            | *Lmax | Leq  |
|----------------------|-------|------|
| Auger Drill Rig      | 84.4  | 77.4 |
| Front End Loader     | 79.1  | 75.1 |
| Grader               | 85    | 81   |
| Pickup Truck         | 75    | 71   |
| Crane                | 80.6  | 72.6 |
| Concrete Mixer Truck | 78.8  | 74.8 |
| Total                | 85    | 84.4 |

<sup>\*</sup>Calculated Lmax is the Loudest value.

# Appendix K-1

Traffic Impact Analysis

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## Kudu Solar Farm Traffic Impact Analysis

California City & Kern County

September 4, 2020

Prepared for:

69SV 8ME LLC c/o 8minute Solar Energy 250 Sutter Street, Suite 600 San Francisco, CA 94108

Prepared by:

Stantec Consulting Services Inc.

This document entitled Kudu Solar Farm Traffic Impact Analysis was prepared by Stantec Consulting Services Inc. ("Stantec") for the account of 69SV 8me LLC (the "Client").

No. 1824 exp. 6/30/2

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## **Table of Contents**

| ACR                              | ONYMS AN  | ND ABBREVIATIONS  | II       |
|----------------------------------|---|---|----------|
| <b>1.0</b><br>1.1                |   | UCTION SED PROJECT Project Components Construction Activities Workforce   | 5        |
| <b>2.0</b><br>2.1<br>2.2         | EXISTIN   | G TRAFFIC VOLUMES   | 7        |
| <b>3.0</b><br>3.1                |   | G TRAFFIC CONDITIONS  |          |
| <b>4.0</b><br>4.1<br>4.2<br>4.3  | CONSTF<br>OPERAT  | RUCTION AND TRUCK ROUTINGRUCTION TRIP GENERATIONRUCTION TRUCK ROUTINGRUCTION TRUCK ROUTING  | 11<br>12 |
| <b>5.0</b><br>5.1                |   | G PLUS CONSTRUCTION CONDITIONS  |          |
| 6.0                              | VMT AN  | ALYSIS  | 15       |
| <b>7.0</b> 7.1 7.2 7.3           | EXISTIN<br>EXISTIN  | JSIONSG TRAFFIC CONDITIONSG PLUS CONSTRUCTION TRAFFIC CONDITIONS  | 16       |
| 8.0                              | REFERE  | NCES  | 17       |
| LIST                             | OF TABLE  | ES CONTRACTOR OF THE PROPERTY |          |
| Table<br>Table<br>Table<br>Table | e 2. Annual<br>e 3. Peak H<br>e 4. Existing<br>e 5. Highest | arcels  |          |
| LIST                             | OF FIGUR  | ES  |          |
| Figur                            | e 1: Project  | t Location Map  | 2        |

## **LIST OF APPENDICES**



| APPENDIX A | HCS WORKSHEETS                    | A.1 |
|------------|-----------------------------------|-----|
| APPENDIX B | DAILY SERVICE VOLUME CALCULATIONS | B.1 |
| APPENDIX C | TRIP GENERATION                   | C.1 |

## **Acronyms and Abbreviations**

AADT annual average daily traffic

AC alternating current

ADT average daily traffic

Applicant 69SV 8me LLC

Caltrans California Department of Transportation

Client 69SV 8me LLC

CUP conditional use permit

EB eastbound

ESS energy storage system

gen-tie generation tie

HCM Highway Capacity Manual

I-5 Interstate 5

kV kilovolt

LADWP Los Angeles Department of Water and Power

LOS level of service

MP Mile Post
MW megawatt
NB Northbound

O&M operations and maintenance

PCE Passenger car equivalent

PHV peak hour volume

Project Kudu Solar Farm Project

PV photovoltaic
SB southbound
SR State Route

Stantec Stantec Consulting Services Inc.

WB westbound



Introduction September 2020

## 1.0 INTRODUCTION

Stantec Consulting Services Inc. (Stantec) has performed a traffic impact analysis for the Kudu Solar Farm Project (project), the proposed construction and operation of a 500-megawatt (MW) alternating current (AC) utility-scale solar farm with an energy storage system (ESS) located in unincorporated Kern County and California City, California. 69SV 8me LLC (Applicant) is seeking approval of a conditional use permit (CUP) for the project. The purpose of the analysis is to determine the amount of traffic generated by the project during construction and operation and to identify potential traffic-related significant impacts on the affected portions of the circulation system.

#### 1.1 PROPOSED PROJECT

The project area is located in portions of unincorporated Kern County and California City, north of the California City Municipal Airport. The majority of the project area is bisected by Washburn Boulevard (which is also the California City Boundary) and Neuralia Road. See Figure 1 for Project Location Map.

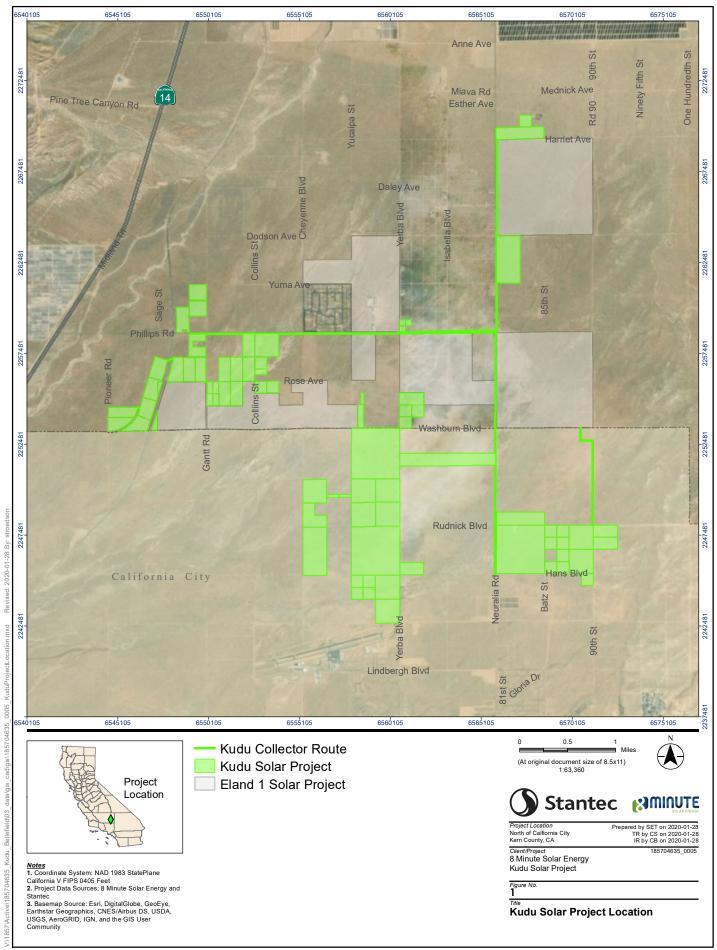
The project comprises 75 assessor's parcels (project area) totaling approximately 1,955 gross acres. See Table 1 for the list of Kudu parcels. The permanent disturbance acreage associated with the development of the solar facility and associated infrastructure (project site) would be less than the gross acreage of the project area. The project area is adjacent to the approved Eland 1 Solar Farm, south of the existing Springbok 1 & 2 solar farms and southeast of the Los Angeles Department of Water and Power (LADWP) Beacon Solar Facility. The topography of the project area is relatively flat.

Power generated by the project would be collected using up to 230-kilovolt (kV) collector lines that run underground and/or overhead to a dedicated project substation, or to the Eland 1 Substation. The project may also share the Eland 1 generation tie (gen-tie) line facilities, or gen-tie rights-of-way. The Eland 1 substation and gen-tie line have gone through environmental analysis and subsequent approval by Kern County and are not part of the project. Additionally, the project may share an operations and maintenance (O&M) building, substations, ESS, and/or transmission facilities, as necessary, with one or more nearby solar projects and may be remotely operated. Any unused O&M, substations, and/or transmission facility areas onsite could be occupied by solar panels under such scenarios.

The project would require an operational staff of up to 20 full-time employees (includes both day and night shifts). Typically, the majority of the staff would work during the day shift (sunrise to sunset), and the remainder would work during the night shifts and weekend. It is possible that the project would share O&M, substation, ESS, and/or transmission facilities, as necessary, with one or more nearby solar projects, and may be remotely operated. In such a scenario, the projects would share personnel and thereby could reduce onsite staff.

After the useful life of the project, the panels would be disassembled from the mounting frames and the project area would be restored to its pre-development condition.





Introduction September 2020

**Table 1: Kudu Parcels** 

| APN        | Gross Acreage |
|------------|---------------|
| Kern Co    | ounty Parcels |
| 469-170-10 | 10.02         |
| 469-170-18 | 39.49         |
| 470-020-08 | 2.31          |
| 470-020-19 | 4.38          |
| 470-030-01 | 79.22         |
| 470-080-15 | 20.27         |
| 470-080-16 | 10.07         |
| 470-080-17 | 10.10         |
| 470-080-32 | 10.07         |
| 470-151-09 | 19.62         |
| 470-151-15 | 20.23         |
| 470-151-16 | 20.40         |
| 470-151-17 | 19.98         |
| 470-152-01 | 39.32         |
| 470-152-18 | 10.32         |
| 470-152-19 | 4.93          |
| 470-302-24 | 2.59          |
| 470-302-25 | 2.62          |
| 470-302-26 | 2.52          |
| 470-322-13 | 2.39          |
| 470-322-15 | 9.96          |
| 470-330-01 | 5.06          |
| 470-330-02 | 4.77          |
| 470-330-03 | 19.86         |
| 470-330-04 | 20.15         |
| 470-330-06 | 9.95          |
| 470-330-07 | 10.02         |
| 470-330-14 | 4.89          |
| 470-330-15 | 5.23          |
| 470-350-04 | 18.65         |
| 470-350-05 | 18.91         |
| 470-350-06 | 18.89         |
| 470-350-07 | 18.57         |
| 470-350-08 | 19.93         |



Introduction September 2020

| APN               | Gross Acreage |
|-------------------|---------------|
| 470-360-01        | 18.43         |
| 470-360-02        | 17.85         |
| 470-360-05        | 21.15         |
| 470-380-01        | 19.92         |
| 470-380-04        | 21.35         |
| 470-380-05        | 17.34         |
| 470-380-06        | 19.88         |
| 470-380-07        | 21.95         |
| Kern County Acres | 673.55        |
| California        | City Parcels  |
| 302-020-08        | 40.17         |
| 302-020-09        | 80.09         |
| 302-020-11        | 163.68        |
| 302-020-14        | 40.99         |
| 302-020-15        | 10.52         |
| 302-020-16        | 10.15         |
| 302-020-17        | 9.59          |
| 302-020-18        | 9.98          |
| 302-290-03        | 83.58         |
| 302-305-15        | 43.54         |
| 302-321-01        | 160.93        |
| 302-322-01        | 10.10         |
| 302-322-02        | 10.09         |
| 302-322-04        | 10.24         |
| 302-322-05        | 10.28         |
| 302-322-06        | 40.04         |
| 302-322-08        | 10.33         |
| 302-322-09        | 40.50         |
| 302-322-10        | 10.27         |
| 302-322-11        | 10.29         |
| 302-325-49        | 9.74          |
| 302-330-33        | 20.21         |
| 302-330-37        | 20.38         |
| 302-341-29        | 168.79        |
| 302-342-01        | 40.23         |
| 302-342-11        | 2.67          |
| 302-342-12        | 2.66          |



Introduction September 2020

| APN                   | Gross Acreage |
|-----------------------|---------------|
| 302-342-19            | 29.69         |
| 302-342-25            | 40.77         |
| 302-342-26            | 39.89         |
| 302-342-27            | 40.29         |
| 302-342-28            | 40.68         |
| 302-470-14            | 20.20         |
| California City Acres | 1,281.51      |
| Total Acres           | 1,955.06      |

Note:

APN = Assessor Parcel Number

#### 1.1.1 Project Components

The project includes the following components:

- Photovoltaic (PV) module configuration,
- Inverter stations,
- ESS,
- Substation.
- Transmission line,
- Water usage/storage,
- O&M building, and
- Project site lighting

The project may include an O&M building of approximately 40 feet by 80 feet in size with associated onsite parking. The O&M building would be steel framed with metal siding and roof panels. The O&M building may include the following:

- Office,
- Repair building/parts storage
- Control room,
- · Restroom, and
- Septic tank and leach field

Roads, driveways, and parking lot entrances would be constructed in accordance with Kern County and California City improvement standards. Parking spaces and walkways would be constructed in conformance with all California accessibility regulations.



Introduction September 2020

#### 1.1.2 Construction Activities

The construction period for the project, from site preparation through construction, testing, and commercial operation, is expected to commence as early as the fourth quarter of 2021 and would extend for approximately 12 to 18 months. Construction of the facility would include the following activities:

- Site preparation
- Grading and earthwork
- Concrete foundations
- Structural steel work
- Electrical/instrumentation work
- · Collector line installation
- Architecture and landscaping

No roadways would be permanently affected by the project. During construction, traffic would access the site from Philips Road, Gantt Road, and Neuralia Road, or through the Eland 1 project site. Up to 1,000 workers per day (during peak construction periods) would be required during construction of the project.

Heavy construction is expected to occur between 6:00 AM and 5:00 PM, Monday through Friday. Additional hours may be necessary to offset schedule deficiencies or to complete critical construction activities. Some activities may continue 24 hours per day, 7 days per week. Low-level noise activities may potentially occur between the hours of 10:00 PM and 7:00 AM. Nighttime activities could potentially include but are not limited to refueling equipment, staging material for the following day's construction activities, quality assurance and control, and commissioning.

Materials and supplies would be delivered to the project area by truck. Truck deliveries would normally occur during daylight hours. There could be offloading and transporting to the project area on weekends and during evening hours.

Earthmoving activities are expected to be limited to the construction of the access roads, O&M building, substation, ESS(s), and any stormwater protection or storage (detention) facilities. Final grading may include revegetation with low lying grass or applying earth-binding materials to disturbed areas.

#### 1.1.3 Workforce

Once the project is constructed, maintenance would generally be limited to the following:

- Cleaning the PV panels,
- Monitoring electricity generation,
- Providing site security, and
- Facility maintenance, including replacing or repairing inverters, wiring, and PV modules.

The project would require an operational staff of up to 20 full-time employees. As mentioned earlier, it is possible that the Project would share O&M, substation, ESS, and/or transmission facilities with any future energy projects nearby. In such a scenario, the projects would share personnel and thereby potentially reduce onsite staff. The facility would operate 7 days a week, 24 hours a day and would generate electricity during normal daylight hours when the solar energy is available. Maintenance activities may occur 7 days a week, 24 hours a day to ensure PV panel output when solar energy is available.



Transportation Setting September 2020

## 2.0 TRANSPORTATION SETTING

This section describes the traffic and transportation conditions in the vicinity of the proposed project site, including the operating condition of the roadways (streets and highways) that could be affected by the project.

#### 2.1 EXISTING ROADWAY SYSTEM

State Route (SR) 14 is a four-lane divided highway adjacent to and west of the project site. For regional travel, residents of California City and other nearby communities rely primarily on SR 14, which carries traffic south to Lancaster and other major routes. SR 14 connects to SR 58 and SR 138 before reaching Interstate 5 (I-5) near Santa Clarita; I-5 provides access to Los Angeles.

SR 58 is a four-lane divided highway located approximately 8 miles south of the project site. SR 58 provides regional access to Bakersfield to the west and communities such as Barstow to the east.

Access to the project site from SR 14 would be via two-way, stop-controlled intersections. Some locations, such as Philips Road, have auxiliary right and left turn lanes.

#### 2.2 EXISTING TRAFFIC VOLUMES

This section summarizes existing traffic volumes on roadways that could be affected by the project. All data were obtained from the California Department of Transportation (Caltrans) Traffic Census Program for the most recent available year (Caltrans 2017).

#### **Segment Volumes**

The 24-hour annual average daily traffic (AADT) volumes at five study locations along SR 14 and SR 58 are shown in Table 2. Also shown in Table 2 are peak month average daily traffic (ADT) volumes, which show variations in traffic volume on the roadway segments over the course of the year.

- SR 14 at SR 58 south of project site,
- SR 14 near project site.
- SR 14 at SR 178 north of project site,
- · SR 58 at Randsburg Cut-Off Road, and
- SR 58 at Boron Avenue.



Transportation Setting September 2020

Table 2. Annual ADT Volumes on Potentially Affected Roadway Segments

| Roadway Segment  | AADT (Peak Month ADT) |
|--|-----------------------|
| SR 14 MP 16.07 - South junction with SR 58   | 10,700 (11,300)       |
| SR 14 MP 21.29 - North of Randsburg Cutoff Road to California City (near Project Site) | 5,900 (6,900)         |
| SR 14 MP 57.77 - South of Freeman junction with SR 178 (2-lane)                        | 6,500 (7,200)         |
| SR 58 MP 107.47 - Randsburg Cut-off Road   | 19,600 (20,700)       |
| SR 58 MP 142.88 - Boron Avenue   | 15,350 (16,100)       |

Source: 2017 Traffic Volumes, Caltrans Traffic Census Program.

Notes:

ADT = average daily traffic

AADT = annual average daily traffic

MP = Mile Post

SR = State Route

#### **Peak Hour Segment Volumes**

The peak hour volumes (PHVs) in the peak direction for the five study locations on SR 14 and SR 58 are shown in Table 3. Also shown are the "K" and "D" factors. The "K" factor represents the percentage of the annual ADT for both directions of travel during the peak hour. The "D" factor represents the percentage of the peak hour traffic in the peak direction.

Table 3. Peak Hour Traffic Volumes on Potentially Affected Roadway Segments

| Roadway Segment  | PHV           | %K    | %D    |
|--|---------------|-------|-------|
| SR 14 MP 16.07 – South junction with SR 58   | 630 (NB PM)   | 8.56  | 68.46 |
| SR 14 MP 21.29 – North of Randsburg Cutoff Road to California City (near Project Site) | 600 (NB PM)   | 18.38 | 55.00 |
| SR 14 MP 57.77 – South of Freeman junction with SR 178 (2-lane)                        | 630 (SB PM)   | 13.08 | 74.59 |
| SR 58 MP 107.47 – Randsburg Cut-off Road   | 1,060 (WB PM) | 8.90  | 60.53 |
| SR 58 MP 142.88 – Boron Avenue   | 850 (EB PM)   | 8.43  | 65.39 |

Source: 2017 Peak Hour Volume Data, Caltrans Traffic Census Program.

Notes:

EB = eastbound

MP = Mile Post

NB = northbound

PHV = peak hour volume

SB = southbound

SR = State Route

WB = westbound



Transportation Setting September 2020

#### **Level of Service Methodology**

Level of service (LOS) is a qualitative index of the performance of an element of a transportation system. LOS is a rating scale from A to F, with A indicating no congestion and F indicating severe congestion and delays.

The Highway Capacity Manual, a standard reference published by the Transportation Research Board, contains specific criteria and methods for assessing LOS. The Generalized Daily Service Volume Methodology was used to calculate the Allowable Daily Service Volume used in determining LOS. The LOS for multilane highways is calculated based on traffic density and the speed travelled. The LOS for two-lane highways is calculated based on vehicle mobility, which is estimated based upon travel speed and the ability of vehicles to pass slow-moving vehicles in the traffic stream.

#### Significance Criteria

Kern County uses a threshold of LOS D for the minimum acceptable operation of its transportation facilities. Facilities under the jurisdiction of Caltrans include freeway segments, ramps, ramp terminals, and arterials. Although Caltrans has not designated a LOS standard, Caltrans' Guide for the Preparation of Traffic Impact Studies (December 2002) indicates attempts to maintain the LOS of a state highway facility between the LOS "C/D" threshold (Caltrans 2002).

For the purpose of this analysis, a LOS threshold of C was used to determine the significance of project impacts on traffic and transportation. The project would be considered to have a significant impact on traffic and transportation if it would cause the operation of a transportation facility to worsen from LOS C or better to LOS D or worse.



Existing Traffic Conditions September 2020

## 3.0 EXISTING TRAFFIC CONDITIONS

This section assesses traffic conditions in the study area without the project.

## 3.1 LEVEL OF SERVICE

Existing traffic conditions for the five roadway segments shown in Table 2 were evaluated based on LOS criteria and the Generalized Daily Service Volume methodology of the HCM for estimating LOS. The roadway capacities were estimated and compared to observed traffic volumes.

The maximum daily traffic volumes that would allow the highway segments to maintain an acceptable LOS are shown in Table 4. As shown, all the multilane highway segments currently operate at an acceptable LOS of C or better. The LOS was determined by calculating allowable daily service volume using the Generalized Daily Service Volume Methodology of the HCM as well as using HCS software. See Appendix A for HCS worksheets. The LOS for the two-lane highway segment (SR 14 near MP 57.77) is calculated using the Generalized Daily Service Volume Methodology of the HCM. This segment is expected to operate at LOS D. All five roadway segments meet the Caltrans target threshold of LOS C except the roadway segment south of Freeman junction route SR 178. See Appendix B for detailed calculations of Allowable Daily Service Volumes.

Table 4. Existing LOS of Study Segments

| Roadway Segment   | Facility Type        | Allowable Daily<br>Service Volume<br>(LOS C) | ADT    | LOS |
|---|----------------------|--|--------|-----|
| SR 14 MP 16.07 – South junction with SR 58  | Multilane<br>Highway | 39,200                                       | 10,700 | А   |
| SR 14 MP 21.29 – North of Randsburg Cut-off Road to California City (near project site) | Multilane<br>Highway | 22,700                                       | 5,900  | А   |
| SR 14 MP 57.77 – South of Freeman junction with SR 178 (two-lane)                       | Two-lane<br>Highway  | <5100  | 6,500  | D   |
| SR 58 MP 107.47 – Randsburg Cut-off Road  | Multilane<br>Highway | 42,700                                       | 19,600 | В   |
| SR 58 MP 142.88 – Boron Avenue  | Multilane<br>Highway | 41,700                                       | 15,350 | А   |

Notes:

ADT = average daily traffic

LOS = level of service

MP = Mile Post

SR = State Route

Source: HCM. See Appendix A for multi-lane highway LOS calculations and Appendix B for two-lane highway calculations
The Allowable Daily Service Volume was calculated for each location based on the unique peaking factors obtained from Caltrans.
The Generalized Daily Service Volume Methodology does not provide for estimating a LOS A.



Trip Generation and Truck Routing September 2020

## 4.0 TRIP GENERATION AND TRUCK ROUTING

This section discusses trip generation and truck routing for the project.

#### 4.1 CONSTRUCTION TRIP GENERATION

Trip generation is defined as the number of vehicle trips produced by a particular type of land use or project. A trip is defined as vehicle movement in one direction. The total number of trips generated by each land use or project includes both inbound and outbound trips.

The proposed Kudu Solar Farm would cover approximately 1,955 acres. Construction of the project is expected to be completed in the following five phases:

- Phase 1: Site preparation & Grading
- Phase 2: Tracker Foundations (Piles)
- Phase 3: Underground Cabling
- Phase 4: Mechanical Installation
- Phase 5: Electrical/Instrumentation Work

The analysis of construction trip generation was prepared based on the average daily volume of construction traffic. The time period with the highest construction trip generation was found to be during the overlap of phases 1 and 2<sup>1</sup>. The highest construction trip generation for the project is shown in Table 5. Appendix C shows the trip generation estimate in relation to the project's construction schedule.

As shown, the project is expected to generate a total passenger car equivalent (PCE) volume of approximately 1,959 ADT, which includes 1,710 passenger car trips and 249 heavy vehicle PCE trips (115 heavy vehicle trips are converted to PCE). Heavy vehicles consist of light-, medium-, and heavy-duty trucks, including heavy-duty diesel construction trucks. Heavy vehicles are approximated as more than one passenger car due to their physical and mechanical characteristics, such as slower acceleration and stopping. A factor of 2.16 was used to convert heavy vehicles to PCE.

**Table 5. Highest Construction Trip Generation** 

|            | A       | ADT            |                |             |
|------------|---------|----------------|----------------|-------------|
|            | Acreage | Passenger Cars | Heavy Vehicles | Total Trips |
| Kudu Total | 1,955   | 1,710          | 249*           | 1,959       |

Notes:

\*115 heavy truck trips x 2.16 PCE factor = 249 PCE

PCE Source: average of light duty trucks PCE of 1.5, medium duty trucks PCE of 2.0, and heavy-duty trucks PCE of 3.0 ADT = average daily traffic

<sup>&</sup>lt;sup>1</sup> Based upon a synthesis of the construction schedule for the Kudu Solar Farm and trip generation rates based on other 69SV 8me LLC solar farm projects.



Trip Generation and Truck Routing September 2020

#### 4.2 OPERATIONS TRIP GENERATION

Once constructed, the solar facility would have up to 20 full-time employees, and the majority of the staff would work during the day shift. To be conservative, assuming all employees work during the day shift, there would be approximately 50 trips per day for the full facility based on an average trip rate of 2.5 trips per employee.

## 4.3 CONSTRUCTION TRUCK ROUTING

The routing of trucks during construction of the project would be on SR 14 and SR 58 depending on the type of construction activity. No direct access from either SR 14 or SR 58 is proposed. Upon exiting SR 14, construction traffic would access the project site from Philips Road, Gantt Road and Neuralia Road, or through the Eland 1 project site. The specific locations where construction traffic would access the highway has not yet been determined. It is recommended that the contractor prepare traffic control plans for access to the public roadway for review and approval by the applicable agency.



Existing Plus Construction Conditions September 2020

## 5.0 EXISTING PLUS CONSTRUCTION CONDITIONS

This section describes the potential impacts of the Project on traffic and transportation.

#### 5.1 LEVEL OF SERVICE

Similar to the analysis of existing traffic conditions, the existing plus construction conditions for the roadway segments were evaluated based on LOS criteria and the Generalized Daily Service Volume methodology of the HCM for estimating LOS. The roadway capacities were estimated and compared to the existing plus construction traffic volumes.

For this analysis, to evaluate the most conservative scenario for each roadway segment, 100 percent of the construction trips were assigned to each roadway segment individually as a worst-case scenario, except for the less traveled segment of SR 14 north of the project site where a conservative assumption of 50 percent construction trips is evaluated.

For the multilane highway segments, given the "K" and "D" factors previously discussed, the maximum daily traffic volume accommodated by the roadway to maintain the target LOS is shown in Table 6. All the multilane highway segments, with the most conservative scenario construction traffic added, operate at an acceptable LOS C or better.

The LOS for the two-lane highway segment (SR 14 near MP 57.77) is expected to continue to operate at LOS D under the worst-case construction traffic scenario as the project would not be expected to add more than 3,000 vehicles, which is the additional volume that would be required to cause LOS E. As the construction traffic would not be expected to worsen the operations to LOS E, the impacts would be considered less than significant.

Since the capacity analysis indicates that there would be no significant impacts on roadway segments based on the conservative assumption regarding construction trips, the impact of construction trips would be less than significant.



Existing Plus Construction Conditions September 2020

Table 6. Existing plus Construction Traffic LOS of Study Segments

| Roadway Segment   | Facility Type        | Allowable Daily<br>Service Volume<br>(LOS C) | Allowable Daily<br>Service Volume<br>(LOS D) | Existing ADT | Project<br>ADT | Existing<br>+<br>Project<br>ADT | LOS |
|---|----------------------|--|--|--------------|----------------|---------------------------------|-----|
| SR 14 MP 16.07 – South junction with SR 58  | Multilane<br>Highway | 39,200                                       | -  | 10,700       | 1,959          | 12,659                          | А   |
| SR 14 MP 21.29 – North of Randsburg Cut-<br>off Road to California City (near Project Site) | Multilane<br>Highway | 22,700                                       | -  | 5,900        | 1,959          | 7,859                           | А   |
| SR 14 MP 57.77 – South of Freeman junction with SR 178 (2-lane)                             | Two-lane<br>Highway  | <5,100                                       | <8,200                                       | 6,500        | 980            | 7,480                           | D   |
| SR 58 MP 107.47 – Randsburg Cut-off Road  | Multilane<br>Highway | 42,700                                       | -  | 19,600       | 1,959          | 21,559                          | В   |
| SR 58 MP 142.88 – Boron Avenue  | Multilane<br>Highway | 41,700                                       | -  | 15,350       | 1,959          | 17,309                          | Α   |

Notes:

ADT = average daily traffic

MP = Mile Post

SR = State Route

See Appendix A for multi-lane highway LOS calculations and Appendix B for two-lane highway calculations

The Allowable Daily Service Volume was calculated for each location based on the unique peak factors obtained from Caltrans. The Generalized Daily Service Volume Methodology does not provide for estimating a LOS A. Allowable Daily Service Volume for LOS D is shown only where applicable to the roadway volumes.



VMT Analysis September 2020

## 6.0 VMT ANALYSIS

The following analysis evaluates Project-related vehicle miles traveled (VMT) and complies with the updated California Environmental Quality Act (CEQA) guidelines that incorporate the requirements of Senate Bill 743 (SB 743). SB 743 requires the Governor's Office of Planning and Research (OPR) to establish recommendations for identifying and mitigating transportation impacts under CEQA. Generally, SB 743 moves away from using delay-based level-of-service (LOS) as the metric for identifying a project's significant impact and instead uses VMT. The final Technical Advisory released by OPR in December 2018 provides guidance on evaluating transportation impacts and VMT and is the guidance on which this analysis is based.

Prior to undertaking a detailed VMT analysis, the Technical Advisory recommends that lead agencies conduct a screening process "to quickly identify when a project should be expected to cause a less-than-significant impact without conducting a detailed study". The Technical Advisory suggests that lead agencies may screen out VMT impacts using project size criteria, maps of low VMT areas, transit availability, and provision of affordable housing. For this Project, the screening criteria related to project size is applicable in regard to the amount of traffic that is generated.

The OPR Technical Advisory recommends that absent substantial evidence indicating that a project would generate a potentially significant level of VMT, or inconsistency with a Sustainable Communities Strategy (SCS) or general plan, projects that generate or attract fewer than 110 trips per day generally may be assumed to cause a less-than-significant transportation impact.

The Project is consistent with the County's General Plan and SCS. And as discussed in Section 4.2, a conservative estimate of the Project's daily trip generation is approximately 50 trips per day for the full facility based on an average trip rate of 2.5 trips per employee. Therefore, the Project would generate substantially fewer than the 110-trip-per-day threshold and can be assumed to cause a less-than-significant transportation impact.

Construction-related VMT is addressed in the context of air quality and greenhouse gas (GHG) as part of a separate study. Construction VMT is temporary, and therefore is not applicable to the transportation thresholds of significance recommended in the OPR Technical Advisory, which are based on a measurement of the operational average VMT per capita.



Conclusions September 2020

## 7.0 CONCLUSIONS

Based on the results of the analysis, the following is a summary of our findings:

## 7.1 EXISTING TRAFFIC CONDITIONS

- All the multilane highway study segments operate at better than the target LOS C threshold.
- The two-lane highway segment of SR 14 at MP 57.77 (south of Freeman Junction with SR 178) operates at LOS D under existing conditions, which is below Caltrans' target LOS threshold.

#### 7.2 EXISTING PLUS CONSTRUCTION TRAFFIC CONDITIONS

- Truck traffic is expected to reach the project site via SR 14, SR 58, Philips Road, Gantt Road and Neuralia Road.
- The most conservative overall daily trip generation (ADT with PCE) during construction is estimated to be 1,959 trips using a PCE factor 2.16.
- Similar to the existing conditions, multilane highway study segments operate at better than the acceptable LOS C threshold.
- The two-lane highway study segment operates at LOS D under both existing and existing plus project conditions, which is below the Caltrans' target LOS threshold. However, because the LOS does not fall below LOS D due to the project, the impact is less than significant.
- Construction of the project is not expected to cause a significant impact to the surrounding transportation network.

## 7.3 VMT ANALYSIS

- The Project is consistent with the County's General Plan and SCS and generates substantially fewer daily
  operational trips than the 110 trip per day threshold of significance for VMT impact. Therefore, based on the OPR
  recommended screening criteria, the Project can be assumed to cause a less-than-significant transportation
  impact.
- VMT associated with construction of the project is addressed in the context of air quality and GHG as part of a separate study. Construction VMT is temporary and is not applicable to the transportation impact thresholds of significance.



References September 2020

## 8.0 REFERENCES

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Appendix A HCS Worksheets

Appendix A HCS WORKSHEETS



|  | BASIC FR     | EEWAY SE      | GMENTS WORKSHEE                              | T                 |                                |
|--|--------------|---------------|--|-------------------|--------------------------------|
| General Information                              |              |               | Site Information                             |                   |                                |
| Analyst  |              |               | Highway/Direction of Trave                   | el <i>SR 14</i>   |                                |
| Agency or Company                                | Stantec      |               | From/To                                      |                   | 7 - junction with SR           |
| Date Performed                                   | 10/1/2019    |               | Jurisdiction                                 | 58<br>Kern Co     | ountv                          |
| Analysis Time Period                             |              |               | Analysis Year                                | 2019              |                                |
| Project Description Kudu                         | Solar Farm T | IA .          |  |                   |                                |
| ✓ Oper.(LOS)                                     |              |               | Des.(N)                                      | ✓ Plar            | nning Data                     |
| Flow Inputs                                      |              |               |  |                   |                                |
| Volume, V  | 655          | veh/h         | Peak-Hour Factor, PHF                        | 0.88              |                                |
| AADT   | 10700        | veh/day       | %Trucks and Buses, P <sub>T</sub>            | 12                |                                |
| Peak-Hr Prop. of AADT, K                         |              |               | %RVs, P <sub>R</sub>                         | 0                 |                                |
| Peak-Hr Direction Prop, D<br>DDHV = AADT x K x D | 68<br>655    | veh/h         | General Terrain: Grade % Length              | Level<br>mi       |                                |
| DDIIV - AADIXKXD                                 | 000          | ven/m         | Up/Down %                                    | 1111              |                                |
| Calculate Flow Adjus                             | tmonte       |               | ορ/Βο <b>ι</b> ιιι /σ                        |                   |                                |
|  |              |               |  | 1.2               |                                |
| f <sub>p</sub>                                   | 0.85         |               | E <sub>R</sub>                               |                   |                                |
| E <sub>T</sub>                                   | 1.5          |               | $f_{HV} = 1/[1+P_T(E_T - 1) + P_R(E_R - 1)]$ |                   |                                |
| Speed Inputs                                     |              |               | Calc Speed Adj and                           | FFS               |                                |
| Lane Width                                       |              | ft            |  |                   |                                |
| Rt-Side Lat. Clearance                           |              | ft            | $f_{LW}$                                     |                   | mph                            |
| Number of Lanes, N                               | 2            |               | f <sub>LC</sub>                              |                   | mph                            |
| Total Ramp Density, TRD                          |              | ramps/mi      | TRD Adjustment                               |                   | mph                            |
| FFS (measured)                                   | 65.0         | mph           | FFS  | 65.0              | mph                            |
| Base free-flow Speed,                            |              | mph           |  | 00.0              | тірп                           |
| BFFS   |              |               | <b>-</b>                                     |                   |                                |
| LOS and Performanc                               | e Measures   | S             | Design (N)                                   |                   |                                |
| Operational (LOS)                                |              |               | Design (N)                                   |                   |                                |
| $v_p = (V \text{ or DDHV}) / (PHF x)$            | N v f        |               | Design LOS                                   |                   |                                |
| v f )  | 11 A 1HV 464 | pc/h/ln       | $v_p = (V \text{ or DDHV}) / (PHF x)$        | $N \times f_{HV}$ | pc/h/ln                        |
| x f <sub>p</sub> )<br>S                          | 65.0         | mnh           | x f <sub>p</sub> )                           |                   | pc/11/111                      |
|  |              | mph           | s  |                   | mph                            |
| $D = v_p / S$                                    | 7.1          | pc/mi/ln      | $D = v_p / S$                                |                   | pc/mi/ln                       |
| LOS  | Α            |               | Required Number of Lanes                     | s, N              |                                |
| Glossary   |              |               | Factor Location                              |                   |                                |
| N - Number of lanes                              | S - Spe      | ed            |  |                   | 1 1 1 1 1 1 1 1                |
| V - Hourly volume                                | D - Dens     |               | E <sub>R</sub> - Exhibits 11-10, 11-12       |                   | f <sub>LW</sub> - Exhibit 11-8 |
| v <sub>p</sub> - Flow rate                       |              | e-flow speed  | E <sub>T</sub> - Exhibits 11-10, 11-11,      | 11-13             | f <sub>LC</sub> - Exhibit 11-9 |
| LOS - Level of service                           |              | ase free-flow | f <sub>p</sub> - Page 11-18                  |                   | TRD - Page 11-11               |
| speed  | <b>5</b> D.  |               | LOS, S, FFS, v <sub>p</sub> - Exhibits       | 11-2,             |                                |
| DDHV - Directional design                        | hour volume  |               | 11-3   |                   |                                |
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|  | BASIC FR        | EEWAY SE      | GMENTS WORKSHEE                              | T                 |                               |
|--|-----------------|---------------|--|-------------------|-------------------------------|
| General Information                              |                 |               | Site Information                             |                   |                               |
| Analyst  |                 |               | Highway/Direction of Trave                   | el SR 514         |                               |
| Agency or Company                                | Stantec         |               | From/To                                      |                   | Randsburg Cutoff              |
| Date Performed                                   | 10/1/2019       |               | Jurisdiction                                 | Road<br>Kern Cour | ntv                           |
| Analysis Time Period                             |                 |               | Analysis Year                                | 2019              | -9                            |
| Project Description Kudu                         | Solar Farm T    | IA            |  |                   |                               |
| ✓ Oper.(LOS)                                     |                 |               | Des.(N)                                      | ✓ Planni          | ng Data                       |
| Flow Inputs                                      |                 |               |  |                   |                               |
| Volume, V  | 584             | veh/h         | Peak-Hour Factor, PHF                        | 0.88              |                               |
| AADT   | 5900            | veh/day       | %Trucks and Buses, P <sub>T</sub>            | 12                |                               |
| Peak-Hr Prop. of AADT, K                         |                 |               | %RVs, P <sub>R</sub>                         | 0                 |                               |
| Peak-Hr Direction Prop, D<br>DDHV = AADT x K x D | 55<br>584       | veh/h         | General Terrain: Grade % Length              | Level<br>mi       |                               |
| DDIIV - AADI X K X D                             | J0 <del>4</del> | Veri/II       | Up/Down %                                    | 1111              |                               |
| Calculate Flow Adjus                             | tments          |               |  |                   |                               |
|  | 0.85            |               | E <sub>R</sub>                               | 1.2               |                               |
| f <sub>p</sub>                                   |                 |               |  |                   |                               |
| E <sub>T</sub>                                   | 1.5             |               | $f_{HV} = 1/[1+P_T(E_T - 1) + P_R(E_R - 1)]$ |                   |                               |
| Speed Inputs                                     |                 |               | Calc Speed Adj and                           | FFS               |                               |
| Lane Width                                       |                 | ft            |  |                   |                               |
| Rt-Side Lat. Clearance                           |                 | ft            | $f_{LW}$                                     |                   | mph                           |
| Number of Lanes, N                               | 2               |               | $f_{LC}$                                     |                   | mph                           |
| Total Ramp Density, TRD                          |                 | ramps/mi      | TRD Adjustment                               |                   | mph                           |
| FFS (measured)                                   | 65.0            | mph           | FFS  | 65.0              | mph                           |
| Base free-flow Speed,                            |                 | mph           |  | 00.0              |                               |
| BFFS   |                 |               | <b>5</b> . (A1)                              |                   |                               |
| LOS and Performanc                               | e Measures      | <u> </u>      | Design (N)                                   |                   |                               |
| Operational (LOS)                                |                 |               | Design (N)                                   |                   |                               |
| v <sub>p</sub> = (V or DDHV) / (PHF x l          | N x f           |               | Design LOS                                   |                   |                               |
| $x f_p$ )  | 414             | pc/h/ln       | $v_p = (V \text{ or DDHV}) / (PHF x)$        | $N \times f_{HV}$ | pc/h/ln                       |
| S  | 65.0            | mph           | x f <sub>p</sub> )                           |                   | ρο/π/π                        |
| D = v <sub>p</sub> / S                           | 6. <i>4</i>     | pc/mi/ln      | S  |                   | mph                           |
| LOS  | 0.4<br>A        | рс/пп/п       | $D = v_p / S$                                |                   | pc/mi/ln                      |
| 103  | A               |               | Required Number of Lanes                     | s, N              |                               |
| Glossary   |                 |               | Factor Location                              |                   |                               |
| N - Number of lanes                              | S - Spee        | ed            | E Evhibite 44 40 44 40                       |                   | Evhibit 44.0                  |
| V - Hourly volume                                | D - Dens        |               | E <sub>R</sub> - Exhibits 11-10, 11-12       |                   | W - Exhibit 11-8              |
| v <sub>p</sub> - Flow rate                       |                 | e-flow speed  | E <sub>T</sub> - Exhibits 11-10, 11-11,      |                   | _ <sub>C</sub> - Exhibit 11-9 |
| LOS - Level of service                           |                 | ase free-flow | f <sub>p</sub> - Page 11-18                  |                   | RD - Page 11-11               |
| speed  |                 |               | LOS, S, FFS, v <sub>p</sub> - Exhibits       | 11-2,             |                               |
| DDHV - Directional design                        | hour volume     |               | 11-3   |                   |                               |
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|   | BASIC FR                | EEWAY SE      | GMENTS WORKSHEE                              | T                   |                                 |
|---|-------------------------|---------------|--|---------------------|---------------------------------|
| General Information                     |                         |               | Site Information                             |                     |                                 |
| Analyst                                 |                         |               | Highway/Direction of Trave                   | el <i>SR 58</i>     |                                 |
| Agency or Company                       | Stantec                 |               | From/To                                      |                     | .47 Randsburg Cut-              |
| Date Performed                          | 10/1/2019               |               | Jurisdiction                                 | off Rd<br>Kern Co   | ountv                           |
| Analysis Time Period                    |                         |               | Analysis Year                                | 2019                |                                 |
| Project Description Kudu                | Solar Farm T            | IA .          |  |                     |                                 |
| ✓ Oper.(LOS)                            |                         |               | Des.(N)                                      | ✓ Plar              | nning Data                      |
| Flow Inputs                             |                         |               |  |                     |                                 |
| Volume, V                               | 1076                    | veh/h         | Peak-Hour Factor, PHF                        | 0.88                |                                 |
| AADT                                    | 19600                   | veh/day       | %Trucks and Buses, P <sub>T</sub>            | 12                  |                                 |
| Peak-Hr Prop. of AADT, K                |                         |               | %RVs, P <sub>R</sub>                         | 0                   |                                 |
| Peak-Hr Direction Prop, D               | 61                      |               | General Terrain:                             | Level               |                                 |
| DDHV = AADT x K x D                     | 1076                    | veh/h         | Grade % Length Up/Down %                     | mi                  |                                 |
| Coloulata Flaur Adius                   | 1                       |               | Op/Down 76                                   |                     |                                 |
| Calculate Flow Adjus                    |                         |               |  |                     |                                 |
| f <sub>p</sub>                          | 0.85                    |               | $E_R$  | 1.2                 |                                 |
| E <sub>T</sub>                          | 1.5                     |               | $f_{HV} = 1/[1+P_T(E_T - 1) + P_R(E_R - 1)]$ | )] <i>0.943</i>     |                                 |
| Speed Inputs                            |                         |               | Calc Speed Adj and                           | FFS                 |                                 |
| Lane Width                              |                         | ft            |  |                     |                                 |
| Rt-Side Lat. Clearance                  |                         | ft            | $f_{LW}$                                     |                     | mph                             |
| Number of Lanes, N                      | 2                       |               | f <sub>LC</sub>                              |                     | mph                             |
| Total Ramp Density, TRD                 |                         | ramps/mi      | TRD Adjustment                               |                     | mph                             |
| FFS (measured)                          | 65.0                    | mph           |  | 05.0                | ·                               |
| Base free-flow Speed,                   | 00.0                    | •             | FFS  | 65.0                | mph                             |
| BFFS                                    |                         | mph           |  |                     |                                 |
| LOS and Performanc                      | e Measures              | S             | Design (N)                                   |                     |                                 |
|   |                         |               | Design (N)                                   |                     |                                 |
| Operational (LOS)                       |                         |               | Design LOS                                   |                     |                                 |
| $v_p = (V \text{ or DDHV}) / (PHF x I)$ | N x f <sub>HV</sub> 762 | pc/h/ln       | $v_p = (V \text{ or DDHV}) / (PHF x)$        | N x f <sub>uv</sub> |                                 |
| x f <sub>p</sub> )                      |                         | •             | x f <sub>p</sub> )                           | 110                 | pc/h/ln                         |
| S                                       | 65.0                    | mph           | S P  |                     | mph                             |
| D = v <sub>p</sub> / S                  | 11.7                    | pc/mi/ln      | $D = v_p / S$                                |                     | pc/mi/ln                        |
| LOS                                     | В                       |               | Required Number of Lanes                     | s N                 | ρο/111/111                      |
| Olasaani                                |                         |               | <u> </u>                                     |                     |                                 |
| Glossary                                |                         |               | Factor Location                              |                     |                                 |
| N - Number of lanes                     | S - Spe                 |               | E <sub>R</sub> - Exhibits 11-10, 11-12       |                     | f <sub>LW</sub> - Exhibit 11-8  |
| V - Hourly volume                       | D - Dens                | •             | E <sub>T</sub> - Exhibits 11-10, 11-11,      |                     | f <sub>I C</sub> - Exhibit 11-9 |
| v <sub>p</sub> - Flow rate              |                         | e-flow speed  | f <sub>n</sub> - Page 11-18                  |                     | TRD - Page 11-1                 |
| LOS - Level of service                  | BFFS - Ba               | ase free-flow | LOS, S, FFS, v <sub>p</sub> - Exhibits       | 11-2,               | 3                               |
| speed<br>DDHV - Directional design      | hour volume             |               | 11-3   | -,                  |                                 |
|   | No. All Dights Poss     |               | 1/00 0040TM . Varreian 0.50                  |                     | ratod: 10/0/2010 3:40 B         |

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|   | BASIC FR                                    | EEWAY SE                           | GMENTS WORKSHEE  | T                              |  |
|---|---|------------------------------------|--|--------------------------------|--|
| General Information   |   |                                    | Site Information   |                                |  |
| Analyst Agency or Company Date Performed Analysis Time Period   | Stantec<br>10/1/2019                        | (4)                                | Highway/Direction of Trave<br>From/To<br>Jurisdiction<br>Analysis Year   |                                | 2.88 - Boron Avenue<br>ounty   |
| Project Description Kudu  ✓ Oper.(LOS)  | Solar Farm Ti                               |                                    | Des.(N)  | √ Dla                          | nning Data   |
| Flow Inputs   |   |                                    | Jes.(IV)   | <u>▼</u> Fla                   | nning Data   |
| Volume, V AADT Peak-Hr Prop. of AADT, K Peak-Hr Direction Prop, D DDHV = AADT x K x D                                   |   | veh/h<br>veh/day<br>veh/h          | Peak-Hour Factor, PHF<br>%Trucks and Buses, P <sub>T</sub><br>%RVs, P <sub>R</sub><br>General Terrain:<br>Grade % Length<br>Up/Down %                              | 0.88<br>12<br>0<br>Level<br>mi |  |
| Calculate Flow Adjus  | tments                                      |                                    | Op/Down 76   |                                |  |
| f <sub>p</sub><br>E <sub>T</sub>  | 0.85<br>1.5                                 |                                    | $E_R$<br>$f_{HV} = 1/[1+P_T(E_T - 1) + P_R(E_R - 1)]$  | 1.2<br>1)] 0.943               |  |
| Speed Inputs  |   |                                    | Calc Speed Adj and   | FFS                            |  |
| Lane Width Rt-Side Lat. Clearance Number of Lanes, N Total Ramp Density, TRD FFS (measured) Base free-flow Speed, BFFS  | 2<br>65.0                                   | ft<br>ft<br>ramps/mi<br>mph<br>mph | f <sub>LW</sub><br>f <sub>LC</sub><br>TRD Adjustment<br>FFS  | 65.0                           | mph<br>mph<br>mph<br>mph   |
| LOS and Performanc  | e Measures                                  | <del></del>                        | Design (N)   |                                |  |
| Operational (LOS)  v <sub>p</sub> = (V or DDHV) / (PHF x x f <sub>p</sub> )  S D = v <sub>p</sub> / S LOS               | N x f <sub>HV</sub> 565<br>65.0<br>8.7<br>A | pc/h/ln<br>mph<br>pc/mi/ln         | Design (N) Design LOS $v_p = (V \text{ or DDHV}) / (PHF \text{ x} \text{ x } f_p)$ S $D = v_p / S$ Required Number of Lanes  |                                | pc/h/ln<br>mph<br>pc/mi/ln   |
| Glossary  |   |                                    | Factor Location  |                                |  |
| N - Number of lanes V - Hourly volume v <sub>p</sub> - Flow rate LOS - Level of service speed DDHV - Directional design | BFFS - Ba                                   |                                    | E <sub>R</sub> - Exhibits 11-10, 11-12<br>E <sub>T</sub> - Exhibits 11-10, 11-11,<br>f <sub>p</sub> - Page 11-18<br>LOS, S, FFS, v <sub>p</sub> - Exhibits<br>11-3 | 11-13                          | f <sub>LW</sub> - Exhibit 11-8<br>f <sub>LC</sub> - Exhibit 11-9<br>TRD - Page 11-11 |

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|   | BASIC FR                | EEWAY SE      | GMENTS WORKSHEE                              | Т                   |                                 |
|---|-------------------------|---------------|--|---------------------|---------------------------------|
| General Information                     |                         |               | Site Information                             |                     |                                 |
| Analyst                                 |                         |               | Highway/Direction of Trave                   | SR 14               |                                 |
| Agency or Company                       | Stantec                 |               | From/To                                      |                     | 7 - junction with SR            |
| Date Performed                          | 10/1/2019               |               | Jurisdiction                                 | 58<br>Kern Co       | ountv                           |
| Analysis Time Period                    |                         |               | Analysis Year                                |                     | with Project                    |
| Project Description Kudu                | Solar Farm T            | IA            |  |                     |                                 |
| ☑ Oper.(LOS)                            |                         |               | es.(N)                                       | ✓ Pla               | nning Data                      |
| Flow Inputs                             |                         |               |  |                     |                                 |
| Volume, V                               | 775                     | veh/h         | Peak-Hour Factor, PHF                        | 0.88                |                                 |
| AADT                                    | 12659                   | veh/day       | %Trucks and Buses, P <sub>T</sub>            | 12                  |                                 |
| Peak-Hr Prop. of AADT, K                |                         |               | %RVs, P <sub>R</sub>                         | 0                   |                                 |
| Peak-Hr Direction Prop, D               | 68<br>775               | la /la        | General Terrain:                             | Level               |                                 |
| DDHV = AADT x K x D                     | 775                     | veh/h         | Grade % Length Up/Down %                     | mi                  |                                 |
| Calculate Flow Adius                    | tmonto                  |               | Op/Down 70                                   |                     | _                               |
| Calculate Flow Adjus                    |                         |               |  |                     |                                 |
| f <sub>p</sub>                          | 0.85                    |               | $E_R$  | 1.2                 |                                 |
| E <sub>T</sub>                          | 1.5                     |               | $f_{HV} = 1/[1+P_T(E_T - 1) + P_R(E_R - 1)]$ | )] 0.943            |                                 |
| Speed Inputs                            |                         |               | Calc Speed Adj and                           | FFS                 |                                 |
| Lane Width                              |                         | ft            |  |                     |                                 |
| Rt-Side Lat. Clearance                  |                         | ft            | $f_{LW}$                                     |                     | mph                             |
| Number of Lanes, N                      | 2                       |               | f <sub>LC</sub>                              |                     | mph                             |
| Total Ramp Density, TRD                 |                         | ramps/mi      | TRD Adjustment                               |                     | mph                             |
| FFS (measured)                          | 65.0                    | mph           | •  | CE 0                | •                               |
| Base free-flow Speed,                   | 00.0                    | •             | FFS  | 65.0                | mph                             |
| BFFS                                    |                         | mph           |  |                     |                                 |
| LOS and Performanc                      | e Measures              | S             | Design (N)                                   |                     |                                 |
|   |                         |               | Design (N)                                   |                     |                                 |
| Operational (LOS)                       |                         |               | Design LOS                                   |                     |                                 |
| $v_p = (V \text{ or DDHV}) / (PHF x I)$ | N x f <sub>HV</sub> 549 | pc/h/ln       | $v_p = (V \text{ or DDHV}) / (PHF x)$        | N x f <sub>uv</sub> |                                 |
| x f <sub>p</sub> )                      |                         |               | $x f_p$                                      | п                   | pc/h/ln                         |
| S                                       | 65.0                    | mph           | S P  |                     | mph                             |
| $D = v_p / S$                           | 8.4                     | pc/mi/ln      | $D = v_p / S$                                |                     | pc/mi/ln                        |
| LOS                                     | Α                       |               | Required Number of Lanes                     | s N                 | ролипли                         |
| Ola a a a mu                            |                         |               | <u> </u>                                     | , I <b>V</b>        |                                 |
| Glossary                                |                         |               | Factor Location                              |                     |                                 |
| N - Number of lanes                     | S - Spec                |               | E <sub>R</sub> - Exhibits 11-10, 11-12       |                     | f <sub>LW</sub> - Exhibit 11-8  |
| V - Hourly volume                       | D - Dens                | •             | E <sub>T</sub> - Exhibits 11-10, 11-11,      | 11-13               | f <sub>I C</sub> - Exhibit 11-9 |
| v <sub>p</sub> - Flow rate              |                         | e-flow speed  | f <sub>n</sub> - Page 11-18                  |                     | TRD - Page 11-11                |
| LOS - Level of service<br>speed         | BFFS - Ba               | ase free-flow | LOS, S, FFS, v <sub>p</sub> - Exhibits       | 11-2,               | <b>.</b>                        |
| DDHV - Directional design               | hour volume             |               | 11-3   | ,                   |                                 |
|   | No. All Dights Door     |               | , , , , , , , , , , , , , , , , , , ,        |                     | rotod: 10/0/2010 2:46 D         |

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|  | BASIC FR            | EEWAY SE      | GMENTS WORKSHEE                              | T                 |                                |
|--|---------------------|---------------|--|-------------------|--------------------------------|
| General Information                              |                     |               | Site Information                             |                   |                                |
| Analyst  |                     |               | Highway/Direction of Trave                   | el <i>SR 514</i>  |                                |
| Agency or Company                                | Stantec             |               | From/To                                      |                   | 29 Randsburg Cutof             |
| Date Performed                                   | 10/1/2019           |               | Jurisdiction                                 | Road<br>Kern Co   | ountv                          |
| Analysis Time Period                             |                     |               | Analysis Year                                |                   | with Project                   |
| Project Description Kudu                         | Solar Farm T        | IA .          |  |                   |                                |
| ✓ Oper.(LOS)                                     |                     |               | Des.(N)                                      | ✓ Plan            | nning Data                     |
| Flow Inputs                                      |                     |               |  |                   |                                |
| Volume, V  | 778                 | veh/h         | Peak-Hour Factor, PHF                        | 0.88              |                                |
| AADT   | 7859                | veh/day       | %Trucks and Buses, P <sub>T</sub>            | 12                |                                |
| Peak-Hr Prop. of AADT, K                         |                     |               | %RVs, P <sub>R</sub>                         | 0                 |                                |
| Peak-Hr Direction Prop, D<br>DDHV = AADT x K x D | 55<br>778           | veh/h         | General Terrain: Grade % Length              | Level             |                                |
| DDU – AADIXKXD                                   | 770                 | ven/n         | Grade % Length Up/Down %                     | mi                |                                |
| Calculate Flow Adjus                             | tmonte              |               | ор/ <b>Бо</b> мп 70                          |                   |                                |
|  |                     |               |  | 4.0               |                                |
| f <sub>p</sub>                                   | 0.85                |               | E <sub>R</sub>                               | 1.2               |                                |
| E <sub>T</sub>                                   | 1.5                 |               | $f_{HV} = 1/[1+P_T(E_T - 1) + P_R(E_R - 1)]$ |                   |                                |
| Speed Inputs                                     |                     |               | Calc Speed Adj and                           | FFS               |                                |
| Lane Width                                       |                     | ft            |  |                   |                                |
| Rt-Side Lat. Clearance                           |                     | ft            | $f_{LW}$                                     |                   | mph                            |
| Number of Lanes, N                               | 2                   |               | f <sub>LC</sub>                              |                   | mph                            |
| Total Ramp Density, TRD                          |                     | ramps/mi      | TRD Adjustment                               |                   | mph                            |
| FFS (measured)                                   | 65.0                | mph           | FFS  | 65.0              | mph                            |
| Base free-flow Speed,                            |                     | mph           |  | 00.0              | Шрп                            |
| BFFS   |                     |               |  |                   |                                |
| LOS and Performanc                               | e Measures          | <u> </u>      | Design (N)                                   |                   |                                |
| Operational (LOS)                                |                     |               | Design (N)                                   |                   |                                |
|  | N v f               |               | Design LOS                                   |                   |                                |
| $v_p = (V \text{ or DDHV}) / (PHF x)$            | <sup>1</sup> HV 551 | pc/h/ln       | $v_p = (V \text{ or DDHV}) / (PHF x)$        | $N \times f_{HV}$ | /le /le                        |
| x f <sub>p</sub> )                               | 05.0                |               | x f <sub>p</sub> )                           |                   | pc/h/ln                        |
| S<br>D = · · / C                                 | 65.0                | mph           | s  |                   | mph                            |
| $D = v_p / S$                                    | 8.5                 | pc/mi/ln      | $D = v_p / S$                                |                   | pc/mi/ln                       |
| LOS  | Α                   |               | Required Number of Lanes                     | s, N              | •                              |
| Glossary   |                     |               | Factor Location                              |                   |                                |
| N - Number of lanes                              | S - Spe             | ed e          |  |                   |                                |
| V - Hourly volume                                | D - Dens            |               | E <sub>R</sub> - Exhibits 11-10, 11-12       |                   | f <sub>LW</sub> - Exhibit 11-8 |
| v <sub>p</sub> - Flow rate                       |                     | e-flow speed  | E <sub>T</sub> - Exhibits 11-10, 11-11,      | 11-13             | f <sub>LC</sub> - Exhibit 11-9 |
| LOS - Level of service                           |                     | ase free-flow | f <sub>p</sub> - Page 11-18                  |                   | TRD - Page 11-11               |
| speed  | 2.10 00             |               | LOS, S, FFS, v <sub>p</sub> - Exhibits       | 11-2,             |                                |
| DDHV - Directional design                        | hour volume         |               | 11-3   |                   |                                |
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|  | BASIC FR             | EEWAY SE      | GMENTS WORKSHEE                              | Т                 |                                |
|--|----------------------|---------------|--|-------------------|--------------------------------|
| General Information                              |                      |               | Site Information                             |                   |                                |
| Analyst  |                      |               | Highway/Direction of Trave                   | el <i>SR 58</i>   |                                |
| Agency or Company                                | Stantec              |               | From/To                                      |                   | 7.47 Randsburg Cut-            |
| Date Performed                                   | 10/1/2019            |               | Jurisdiction                                 | off Rd<br>Kern Co | ountv                          |
| Analysis Time Period                             |                      |               | Analysis Year                                |                   | g with Project                 |
| Project Description Kudu                         | Solar Farm T         | TIA           |  |                   |                                |
| ✓ Oper.(LOS)                                     |                      |               | Des.(N)                                      | ✓ Pla             | nning Data                     |
| Flow Inputs                                      |                      |               |  |                   |                                |
| Volume, V  | 1184                 | veh/h         | Peak-Hour Factor, PHF                        | 0.88              |                                |
| AADT   | 21559                | veh/day       | %Trucks and Buses, P <sub>T</sub>            | 12                |                                |
| Peak-Hr Prop. of AADT, K                         |                      |               | %RVs, P <sub>R</sub>                         | 0                 |                                |
| Peak-Hr Direction Prop, D<br>DDHV = AADT x K x D | 61<br>1184           | veh/h         | General Terrain: Grade % Length              | Level<br>mi       |                                |
| DDIIV - AADI XIXXD                               | 1104                 | VCII/II       | Up/Down %                                    | 1111              |                                |
| Calculate Flow Adjus                             | tments               |               | <b>5</b> F/2 5 13                            |                   |                                |
| -  | 0.85                 |               | E <sub>R</sub>                               | 1.2               |                                |
| f <sub>p</sub>                                   |                      |               |  |                   |                                |
| E <sub>T</sub>                                   | 1.5                  |               | $f_{HV} = 1/[1+P_T(E_T - 1) + P_R(E_R - 1)]$ |                   |                                |
| Speed Inputs                                     |                      |               | Calc Speed Adj and                           | FFS               |                                |
| Lane Width                                       |                      | ft            |  |                   |                                |
| Rt-Side Lat. Clearance                           |                      | ft            | $f_{LW}$                                     |                   | mph                            |
| Number of Lanes, N                               | 2                    |               | $f_{LC}$                                     |                   | mph                            |
| Total Ramp Density, TRD                          |                      | ramps/mi      | TRD Adjustment                               |                   | mph                            |
| FFS (measured)                                   | 65.0                 | mph           | FFS  | 65.0              | mph                            |
| Base free-flow Speed,                            |                      | mph           |  |                   |                                |
| BFFS   |                      |               | <b>5</b> : (A))                              |                   |                                |
| LOS and Performanc                               | e Measures           | <u> </u>      | Design (N)                                   |                   |                                |
| Operational (LOS)                                |                      |               | Design (N)                                   |                   |                                |
| $v_p = (V \text{ or DDHV}) / (PHF x I)$          | N x f                |               | Design LOS                                   |                   |                                |
| $x f_p$ )  | ** <sup>HV</sup> 839 | pc/h/ln       | $v_p = (V \text{ or DDHV}) / (PHF x)$        | $N \times f_{HV}$ | pc/h/ln                        |
| S  | 65.0                 | mph           | x f <sub>p</sub> )                           |                   | ρο/π/π                         |
| D = v <sub>p</sub> / S                           | 12.9                 | pc/mi/ln      | S  |                   | mph                            |
| LOS  | 12.9<br>B            | рс/пп/п       | $D = v_p / S$                                |                   | pc/mi/ln                       |
| LOS  | Ь                    |               | Required Number of Lanes                     | s, N              |                                |
| Glossary   |                      |               | Factor Location                              |                   |                                |
| N - Number of lanes                              | S - Spe              | ed            |  |                   | f                              |
| V - Hourly volume                                | D - Dens             |               | E <sub>R</sub> - Exhibits 11-10, 11-12       |                   | f <sub>LW</sub> - Exhibit 11-8 |
| v <sub>p</sub> - Flow rate                       |                      | e-flow speed  | E <sub>T</sub> - Exhibits 11-10, 11-11,      | 11-13             | f <sub>LC</sub> - Exhibit 11-9 |
| LOS - Level of service                           |                      | ase free-flow | f <sub>p</sub> - Page 11-18                  |                   | TRD - Page 11-11               |
| speed  |                      |               | LOS, S, FFS, v <sub>p</sub> - Exhibits       | 11-2,             |                                |
| DDHV - Directional design                        | hour volume          |               | 11-3   |                   |                                |

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|                         |   |  | T  |  |
|-------------------------|---|--|--|--|
|                         |   | Site Information   |  |  |
| Stantec<br>10/1/2019    | Δ.  |  | PM 142.<br>Kern Col  | 88 - Boron Avenue<br>unty<br>with Project  |
| Solai Fallii II.        |   | ) o o (NI)   | Z Dlan   | ning Data  |
|                         | L   | Jes.(N)  | <u>▼</u> Piani   | ning Data  |
| 000                     | a b /b  | Deals Have Factor DUF  | 0.00   |  |
| 17309<br>0.08           | ven/n<br>veh/day  | %Trucks and Buses, P <sub>T</sub> %RVs, P <sub>R</sub>   | 0.88<br>12<br>0  |  |
| 65<br>900               | veh/h   | General Terrain:<br>Grade % Length<br>Up/Down %  | Level<br>mi  |  |
| tments                  |   |  |  |  |
| 0.85<br>1.5             |   | $E_{R}$ $f_{HV} = \frac{1}{[1+P_{T}(E_{T}-1)+P_{R}(E_{R}-1)]}$                                       | 1.2<br>)] 0.943  |  |
|                         |   | •  |  |  |
|                         | ft  | - Caro opecarragement  |  |  |
|                         |   | f  |  | mph  |
| 2                       |   |  |  | ·  |
|                         | ramps/mi  |  |  | mph<br>mph   |
| 65.0                    | ·   | •  | 65.0   | •  |
|                         | mph   | FFS  | 05.0   | mph  |
| e Measures              |   | Design (N)   |  |  |
| N x f <sub>HV</sub> 638 | pc/h/ln<br>mph  | $\frac{\text{Design (N)}}{\text{Design LOS}}$ $v_p = (V \text{ or DDHV}) / (PHF \text{ x})$ $x f_p)$ | N x f <sub>HV</sub>  | pc/h/ln  |
|                         | •   |  |  | mph  |
| A                       | <b>F</b> 3333333  | · ·  | s, N   | pc/mi/ln   |
|                         |   | Factor Location  |  |  |
| D - Dens<br>FFS - Free  | ity<br>e-flow speed   | f <sub>p</sub> - Page 11-18  |  | f <sub>LW</sub> - Exhibit 11-8<br>f <sub>LC</sub> - Exhibit 11-9<br>TRD - Page 11-11   |
|                         | 900 17309 0.08 65 900  tments 0.85 1.5  2 65.0  e Measures N x f <sub>HV</sub> 638 65.0 9.8 A  S - Spee D - Dens FFS - Free BFFS - Ba hour volume | 10/1/2019   Solar Farm TIA   | Stantec 10/1/2019 From/To Jurisdiction Analysis Year Solar Farm TIA    Des.(N) | Stantec 10/1/2019    Highway/Direction of Travel   SR 58   From/To   Jurisdiction   Kern Cot   Analysis Year   Existing     Solar Farm TIA   □ Des.(N)   ✓ Plan     Peak-Hour Factor, PHF   0.88     17309   veh/day   %Trucks and Buses, P <sub>T</sub>   12     0.08   %RVs, P <sub>R</sub>   0     65   General Terrain:   Level     900   veh/h   Grade   % Length   mi     Up/Down %     tments |

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Appendix B Daily Service Volume Calculations

## Appendix BDAILY SERVICE VOLUME CALCULATIONS



| Roadway Segment (Multilane Highway)   | MSF   | N | fHV   | fp   | PHF  | K    | D    | DSV    | DSV<br>Rounded |
|---|-------|---|-------|------|------|------|------|--------|----------------|
| SR 14 MP 16.07 - South junction with SR 58 SR 14 MP 21.29 - North of Randsburg Cutoff Road to | 1,630 | 2 | 0.943 | 0.85 | 0.88 | 0.09 | 0.68 | 39,239 | 39,200         |
| California City (near project site)   | 1,630 | 2 | 0.943 | 0.85 | 0.88 | 0.18 | 0.55 | 22,747 | 22,700         |
| SR 58 MP 107.47 - Randsburg Cut-off Road  | 1,630 | 2 | 0.943 | 0.85 | 0.88 | 0.09 | 0.61 | 42,685 | 42,700         |
| SR 58 MP 142.88 - Boron Avenue  | 1,630 | 2 | 0.943 | 0.85 | 0.88 | 0.08 | 0.65 | 41,715 | 41,700         |

#### Notes:

Daily Service Volume, DSV = (MSF x N x fHV x fp x PHF) / (K x D) (Source: HCM 2010, Chapter 10, Equation 10-5)

fp = 0.85

PHF = 0.88

fHV = 0.943

Max. Service Flow rate for Target LOS C, MSF = 1,630 (Source: HCM 2010, Chapter 11, Exhibit 11-17)

K, D (Source: Caltrans Traffic Census Program)

| Roadway Segment (Two-lane Highway)                      |           | DSV    |
|---|-----------|--------|
| SR 14 MP 57.77 - South of Freeman junction with SR 178  | For LOS C | <5,100 |
| 13h 14 MF 37.77 - South of Freeman junction with 3h 176 | For LOS D | <8,200 |

#### Notes:

Source: HCM 2010, Exhibit 15-30 Generalized Daily Service Volumes for Two-lane Highways

k factor - 0.14, D-factor - 65%, Class I - Level

# KUDU SOLAR FARM TRAFFIC IMPACT ANALYSIS

Appendix C Trip Generation

Appendix C TRIP GENERATION



**Kudu - Passenger Car ADT by Phase** 

|       |                            | 2021         |     |     |      |      |      |      | 2022  |     |      |      |     |      |     |     |
|-------|----------------------------|--------------|-----|-----|------|------|------|------|-------|-----|------|------|-----|------|-----|-----|
| Phase | Description                | Work<br>Days | Oct | Nov | Dec  | Jan  | Feb  | Mar  | April | May | June | July | Aug | Sept | Oct | Nov |
| 1     | Site Preparation & Grading | 84           | 595 | 595 | 595  |      |      |      |       |     |      |      |     |      |     |     |
| 2     | Tracker Foundations        | 125          |     |     | 1115 | 1115 | 1115 | 1115 | 1115  |     |      |      |     |      |     |     |
| 3     | Undergound Cabling         | 125          |     |     |      |      |      | 40   | 40    | 40  | 40   |      |     |      |     |     |
| 4     | Mechanical Installation    | 146          |     |     |      |      |      |      |       | 40  | 40   | 40   | 40  | 40   | 40  |     |
| 5     | Electrical Installation    | 167          |     |     |      |      |      |      |       |     | 275  | 275  | 275 | 275  | 275 | 275 |
|       | Total                      | 647          | 595 | 595 | 1710 | 1115 | 1115 | 1155 | 1155  | 80  | 355  | 315  | 315 | 315  | 315 | 275 |

# **Kudu - Heavy Vehicle ADT by Phase**

|       |                            |              | 2021 |     |     |     |     |     |       | 2022 |      |      |     |      |     |     |
|-------|----------------------------|--------------|------|-----|-----|-----|-----|-----|-------|------|------|------|-----|------|-----|-----|
| Phase | Description                | Work<br>Days | Oct  | Nov | Dec | Jan | Feb | Mar | April | May  | June | July | Aug | Sept | Oct | Nov |
| 1     | Site Preparation & Grading | 84           | 55   | 55  | 55  |     |     |     |       |      |      |      |     |      |     |     |
| 2     | Tracker Foundations        | 125          |      |     | 60  | 60  | 60  | 60  | 60    |      |      |      |     |      |     |     |
| 3     | Undergound Cabling         | 125          |      |     |     |     |     | 8   | 8     | 8    | 8    |      |     |      |     |     |
| 4     | Mechanical Installation    | 146          |      |     |     |     |     |     |       | 8    | 8    | 8    | 8   | 8    | 8   |     |
| 5     | Electrical Installation    | 167          |      |     |     |     |     |     |       |      | 20   | 20   | 20  | 20   | 20  | 20  |
|       | Total                      | 647          | 55   | 55  | 115 | 60  | 60  | 68  | 68    | 16   | 36   | 28   | 28  | 28   | 28  | 20  |

#### Note:

115 heavy vehicle trips x 2.16 = 249 heavy vehicle PCE trips; Passenge Car Equivalent (PCE) factor = 2.16;

Heavy vehicles consist of light-, medium-, and heavy-duty trucks, including heavy-duty diesel construction trucks. They are approximated as more than one passenger car due to their physical and mechanical characteristics, such as slower acceleration and stopping.

**Kudu - Overall ADT with PCE trips by Phase** 

|       | 2021                       |              |     |     |      |      |      | 2022 |       |     |      |      |     |      |     |     |
|-------|----------------------------|--------------|-----|-----|------|------|------|------|-------|-----|------|------|-----|------|-----|-----|
| Phase | Description                | Work<br>Days | Oct | Nov | Dec  | Jan  | Feb  | Mar  | April | May | June | July | Aug | Sept | Oct | Nov |
| 1     | Site Preparation & Grading | 84           | 714 | 714 | 714  |      |      |      |       |     |      |      |     |      |     |     |
| 2     | 2 Tracker Foundations      |              |     |     | 1245 | 1245 | 1245 | 1245 | 1245  |     |      |      |     |      |     | ĺ   |
| 3     | Undergound Cabling         | 125          |     |     |      |      |      | 56   | 56    | 56  | 56   |      |     |      |     | ĺ   |
| 4     | Mechanical Installation    | 146          |     |     |      |      |      |      |       | 56  | 56   | 56   | 56  | 56   | 56  |     |
| 5     | Electrical Installation    | 167          |     |     |      |      |      |      |       |     | 318  | 318  | 318 | 318  | 318 | 318 |
|       | Total                      | 647          | 714 | 714 | 1959 | 1245 | 1245 | 1301 | 1301  | 112 | 430  | 374  | 374 | 374  | 374 | 318 |

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# **Appendix K-2**

Project Construction - SR 14 at Phillips Road Intersection Evaluation

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To: Erec Devost From: Daryl Zerfass / Sandhya Perumalla

8minute Solar Energy 38 Technology Drive 250 Sutter Street, Suite 600 Irvine CA 92618 San Francisco CA 94108

File: 185704635 Date: September 3, 2021

Reference: Kudu Solar Project Construction – SR-14 at Philips Road Intersection Evaluation

Traffic impacts along State Route 14 (SR 14) and SR 58 for the Kudu Solar Project (Project) were previously analyzed in a separate report¹ prepared by Stantec in September 2020. Construction of the overhead and/or underground gen-tie line for the Project is expected to occur along Philips Road and Neuralia Road. Also, construction traffic will utilize the SR 14 at Phillips Road at-grade intersection for access to the primary construction areas east of SR 14. This memo summarizes the potential construction-related effects on traffic circulation during construction of the Project in regard to the SR 14/Philips Road intersection.

# **Existing Conditions**

Philips Road is a two-lane undivided roadway with dirt shoulders on both sides of the roadway, running in an east-west direction, between SR-14 to Neuralia Road in an unincorporated portion of Kern County. The paved portion of the road is approximately 4.56 miles long with a 55-mph speed limit. The paved portion of Philips Road ends at the 3-legged stop-controlled intersection at Neuralia Road. East of Neuralia Road, Philips Road continues as an unimproved dirt roadway. There's a railroad crossing, approximately 0.4 miles west of the Gantt Road intersection, controlled by a yield sign. A stop sign is provided for eastbound and westbound Philips Road at the SR-14 and Philip Road intersection. With the exception of the traffic controls mentioned above, the remaining section of Philips Road is uncontrolled. SR-14 at Philips Road consists of two-through lanes in each direction, approximately 385 feet and 365 feet left-turn pockets on the north and south leg, respectively, and 400 feet right turn pocket on the south leg (See Figure 1).

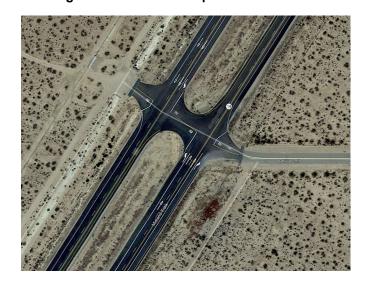


Figure 1 - SR 14 at Philips Road

Design with community in mind

<sup>&</sup>lt;sup>1</sup> Kudu Solar Farm Traffic Impact Analysis, Stantec, September 4, 2020.

September 3, 2021 Erec Devost

Page 2 of 4

Reference: Kudu Solar Project Construction – SR-14 at Philips Road Intersection Evaluation

A small single-family residential development (approximately 50 single family residential units) is located adjacent to Philips Road approximately 2.5 miles east of SR 14. Existing traffic volumes on Philips Road would be considered low and nominal. The residential development has cross streets intersecting Philips Road between Cheyenne Boulevard and Yucaipa Street.

## SR 14 at Philips Road At-Grade Intersection

Construction traffic access to the main construction areas east of SR 14 will primarily occur at the SR 14/Philips Road intersection, which is located at approximately SR 14 post-mile (PM) 27. As discussed in the Project's September 2020 traffic study referenced above, the construction period with the highest volume of construction traffic would occur during the overlap of construction phases 1 and 2. During that period, the Project is estimated to generate a maximum of 1,710 average daily passenger car trips and 115 average daily heavy vehicle trips, for a total of 1,959 average daily trips (ADT) based on a passenger car equivalent (PCE) factor of 2.16. Approximately 980 trips would be inbound to the Project site and approximately 980 trips would be outbound from the Project site each day.

Analysis of the SR 14 mainline is provided in the Project's September 2020 traffic study, which assumed a worst-case scenario of 100 percent of construction traffic on any given highway segment since the precise origin of construction related traffic is not known, except for the less traveled segment of SR 14 north of the Project site, where a conservative assumption of 50 percent of construction trips was evaluated.

The analysis determined that two of the three SR 14 highway segments would continue to operate at LOS A with the addition of construction traffic. At the segment of SR 14 north of the Project site, where a conservative assumption of 50 percent of construction trips was evaluated, the analysis determined that the two-lane highway segment would continue to operate at LOS D. At the SR 14/Philips Road intersection, existing condition (2019) traffic volume<sup>2</sup> is as follows:

• SR 14 at Philips Road - 7,700 ADT

Utilizing the same assumptions provided in the September 2020 traffic study, assuming a worst-case scenario of 100 percent of the construction traffic on the SR 14 at Philips Road, the daily traffic volume with construction traffic would be approximately 9,700 ADT. SR 14, near Philips Road intersection, is a four-lane highway with a daily capacity of approximately 22,700 at LOS C<sup>3</sup>. Therefore, with the addition of construction traffic the highway segment operates at an acceptable LOS C or better. Construction traffic would be distributed throughout the day, with the highest concentrations occurring outside the typical peak hours with construction starting in the early morning hours and ending before the typical PM peak hour.

#### **Construction Traffic Routes**

The Project site is spread out over several parcels east of SR 14 on both sides of the Philips Road, west of Santa Fe (BNSF) Railway tracks, and east of Neuralia Road. Access to each construction location is discussed in the following sections.

<sup>&</sup>lt;sup>2</sup> Caltrans Traffic Census Program, https://dot.ca.gov/programs/traffic-operations/census, 2019-Traffic-Volumes.xlxs, accessed September 1, 2021.

<sup>&</sup>lt;sup>3</sup> Table 6, Kudu Solar Farm Traffic Impact Analysis, Stantec, September 4, 2020.

Erec Devost Page 3 of 4

Reference: Kudu Solar Project Construction – SR-14 at Philips Road Intersection Evaluation

#### **Locations south of Philips Road**

The main construction area is located east of SR 14, and construction traffic would use Philips Avenue to access the site. The paved roadway section of Philips Road spans the entire 4.56-mile segment east into the site to accommodate construction traffic. Construction traffic would access this area from SR 14 via the Philips Road intersection and travel along Gantt Road, Neuralia Road and through the Eland 1 Project site that is adjacent to the Project.

#### Location north of Philips Road

A small piece of the Project site is located north of Philips Road, east of the Santa Fe (BNSF) Railway tracks and west of Gantt Road. Construction traffic would access this area from SR 14 via the Philips Road intersection and travel along Gantt Road, north of Philips Road. This road is an existing dirt road and ends at Daley Avenue, which is also a dirt road. The volumes discussed above include construction traffic to this piece of the Project site.

#### **Locations west of BNSF Railway Tracks**

This part of the Project site located east of SR 14, west of the BNSF Railway tracks, and would be accessed from Philips Road, Gantt Road and through the Eland 1 Project site. Each of these are existing dirt roads.

#### Location east of Neuralia Road

This part of the Project site located east of Neuralia Road, would be accessed from SR 14 via Philips Road, Neuralia Road and through the Eland 1 Project site. Neuralia is a two-lane undivided roadway with dirt shoulders on both sides of the roadway, running in a north-south direction.

#### **Construction Traffic Mitigation**

As mentioned, construction traffic would access the Project site from Philips Road, Gantt Road, and Neuralia Road, or through the Eland 1 Project site. To minimize potential effects from construction traffic on the roadway network, a construction traffic management plan is recommended to be prepared and implemented. The construction traffic management plan would include the following:

- Temporary traffic control devices in accordance with the California Manual on Uniform Traffic Control Devices (CA MUTCD) and notification to the Kern County Public Works Department to identify locations where construction is on-going, including:
  - signs warning of slow-moving vehicles
  - signs warning of merging trucks
  - o barriers for separating non-construction vehicles from construction activities
  - o traffic control flagmen
  - any additional measures required to manage non-construction traffic through construction areas.
- Scheduling of heavy vehicle traffic to the site during non-peak periods when feasible
- Scheduling of work shift changes to avoid the peak periods when feasible
- Encouraging carpooling among construction workers to reduce workers' passenger vehicle trips in the study area

September 3, 2021

Erec Devost Page 4 of 4

Reference: Kudu Solar Project Construction – SR-14 at Philips Road Intersection Evaluation

 Coordinating with local emergency response agencies to provide information regarding emergency response vehicle routes affected by construction activities.

#### **Conclusions**

To access the main construction areas east of SR 14, the construction traffic would primarily access the State highway system at the SR 14/Philips Road at-grade intersection. Construction traffic would access the Project site from Philips Road, Gantt Road, and Neuralia Road, or through the Eland 1 Project site. Existing traffic volumes are low and nominal on Philips Road. A worst-case scenario, assuming 100 percent of the construction traffic on SR 14, the daily traffic volume with construction traffic would be approximately 9,700 ADT. SR 14, near Philips Road intersection, is a four-lane highway with a daily capacity of approximately 22,700 at LOS C. With the addition of construction traffic the highway segment continues to operate at an acceptable LOS C or better. Construction traffic would be distributed throughout the day, with the highest concentrations occurring outside the typical peak hours with construction starting in the early morning hours and ending before the typical PM peak hour.

Prior to the start of construction, the Project would prepare a phased construction Traffic Management Plan (TMP) based on the specific construction routes and activities established at that time.

**Stantec Consulting Services Inc.** 

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# **Appendix L**

Water Supply Assessment

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# Kudu Solar Farm Water Supply Assessment

September 1, 2020

# Prepared for:

69SV 8me LLC c/o 8minute Solar Energy 5455 Wilshire Boulevard, Suite 2010 Los Angeles, CA 90036

# Prepared by:

Stantec Consulting Services Inc. 100 California Street, Suite1000 San Francisco, CA 94111



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# **Table of Contents**

| EXEC | UTIVE SUM  | MARY   | I   |
|------|------------|--|-----|
| ABBF | REVIATIONS | 3  | III |
| 1.0  | PROJECT    | DESCRIPTION  | 1   |
| 1.1  |            | INFORMATION  |     |
| 1.1  | 1.1.1      | Project Site Information   |     |
|      | 1.1.2      | Location   |     |
| 1.2  |            | TION OF PROPOSED PROJECT   |     |
| 1.2  | 1.2.1      | PV Module Configuration  |     |
|      | 1.2.2      | Inverter Stations  |     |
|      | 1.2.3      | Energy Storage System  |     |
|      | 1.2.4      | Substation   |     |
|      | 1.2.5      | Transmission Line  |     |
|      | 1.2.6      | Water Usage  |     |
|      | 1.2.7      | Water Storage Tanks  |     |
|      | 1.2.8      | Operations and Maintenance Building                              |     |
|      | 1.2.9      | Project Site Security and Fencing                                |     |
|      | 1.2.10     | Project Site Lighting  |     |
| 1.3  | ANNUAL F   | PRODUCTION   |     |
| 1.4  |            | JCTION ACTIVITIES  |     |
| 1.5  |            | PRCE   |     |
| 1.6  |            | FEATURES AND BEST MANAGEMENT PRACTICES                           |     |
| 1.0  | 1.6.1      | Waste and Hazardous Materials Management                         |     |
|      | 1.6.2      | Spill Prevention and Containment                                 |     |
|      | 1.6.3      | Wastewater/Septic System   |     |
|      | 1.6.4      | Inert Solids   |     |
|      | 1.6.5      | Health and Safety  |     |
| 1.7  | CLIMATE.   | ,  |     |
|      |            |  |     |
| 2.0  | WATER S    | UPPLY PLANNING UNDER SENATE BILL 610                             | 13  |
| 2.1  | WATER S    | UPPLY ASSESSMENT   | 13  |
|      | 2.1.1      | Is the Project Subject to CEQA?                                  | 13  |
|      | 2.1.2      | Is It a Project Under Senate Bill 610?                           | 14  |
|      | 2.1.3      | Is There a Public Water System?                                  |     |
|      | 2.1.4      | Is There a Current UWMP That Accounts for the Project Demand?    |     |
|      | 2.1.5      | Is Groundwater a Component of the Supplies of the Project?       | 15  |
|      | 2.1.6      | Are There Sufficient Supplies to Serve the Project Over the Next |     |
|      |            | Twenty Years?  |     |
|      | 2.1.7      | Conclusions  | 22  |
| 2.0  | DEEEDEN    | ICEC   | 25  |



# **LIST OF FIGURES**

| Figure 1: Kudu Solar Farm - Assessors Parcels<br>Figure 2: Fremont Valley Groundwater Basin |    |
|---|----|
| LIST OF TABLES  |    |
| Table 1: Kudu Parcels   | 1  |
| Table 2: Average Monthly and Annual Evapotranspiration, Precipitation and                   |    |
| Temperature   | 11 |
| Table 3: Future Water Supply Availability (2040) in the FVGB                                | 19 |
| Table 4: Future Water Supply Availability (2040) in California City                         | 20 |
| Table 5: Anticipated Future Project Water Demand (2040)                                     | 20 |
| Table 6: Future Water Supply Versus Project Water Demand at Build-Out in the FVGB           | 21 |
| Table 7: Future Water Supply Versus Project Demand at Build-Out in California City          | 21 |

# **Executive Summary**

Stantec Consulting Services Inc. (Stantec) completed a Water Supply Assessment (WSA) report on behalf of 69SV 8me LLC for the construction and operation of the Kudu Solar Farm (Kudu) Project (Project). This WSA was conducted in conformance with the requirements of the California Water Code, as amended in 2002 by the passage of Senate Bill (SB) 610, except as may have been modified by the scope of work and terms and conditions requested by 69SV 8me LLC.

The Project would consist of 75 parcels, totaling approximately 1,955 acres of predominantly vacant and undeveloped land in unincorporated Kern County and California City, California. The Project would lie south of Munsey Road, east and west of Neuralia Road, east of Highway 14, north and south of Philips Road, southeast of the unincorporated community of Cantil, and north of California City. The power generated by Kudu will be delivered through a 230-kilovolt overhead generation tie (gen-tie) originating from the Eland 1 substation and terminating at the Los Angeles Department of Water and Power Barren Ridge substation.

69SV 8me LLC is seeking approval of a conditional use permit for the construction of a 500-megawatt alternating current utility-scale solar photovoltaic energy plant. Stantec analyzed water supplies available to serve the Project, including the water demand anticipated during construction and through operation of the facility. According to the requirements of California Water Code (Water Code) Section 10910(c)(3) the WSA shall include a discussion of, "whether the public water system's total projected water supplies available will meet the projected water demand associated with proposed Project, in addition to the public water system's existing and planned future uses." In summary:

- The Project will be under environmental review pursuant to the requirements of California Environmental Quality
  Act (CEQA); therefore, the information contained in this assessment will be used to support the analysis
  contained in the CEQA document.
- The Project does not meet the definition of a "Project" under Water Code Section 10912(a).
- A 1281.51-acre portion of the Kudu Project is located within California City and will be served by the California
  City Water Department. The 673.55-acre portion of the Kudu Project located in unincorporated Kern County, that
  is, outside the California City boundaries, will not be served by a public water system. California City prepared an
  Urban Water Management Plan (UWMP) 2015 Update (California City, 2017), that did not account for the Project
  water demand.
- The Project estimates a water demand of 50 acre-feet per annum (afa) for operations includes water that would be used for washing the solar panels and other operation and maintenance (O&M) activities,
- Proposed water demand for the portion of the Kudu Project located within California City will be met by California City water supplies including local groundwater from wells and imported water from Antelope Valley-East Kern Water Agency (AVEK), and is estimated at 32.75 afa. The portion of the Kudu Project located in unincorporated Kern County would be met by local groundwater pumping estimated at 17.25 afa and is not considered a de minimis extraction under Section 10721 of the Water Code.

- The groundwater supply would be extracted from the Fremont Valley Groundwater Basin (FVGB). No Groundwater Sustainability Agency (GSA) has been formed to serve this basin, and management of this basin is assumed by Kern County. A Fremont Valley Groundwater Management Plan (FVGMP) has been prepared for California City, Mojave Public Utilities District (MPUD) and AVEK (Woodard & Curran, 2018a) which is intended to serve as a pre-Groundwater Sustainability Plan (GSP) document in the event the FVGB is required to prepare a GSP. The Antelope Valley Groundwater Basin to the south is adjudicated, but the FVGB is not.
- The FVGB has been designated as a "low" priority basin by the California Department of Water Resources (DWR) and a GSP is not required under the Sustainable Groundwater Management Act (SGMA).
- According to the FVGMP, groundwater production in the FVGB in 2020 is estimated to be 7,515 acre-feet (af) and
  is projected to be 9,894 af in 2040.
- According to the Fremont Valley Basin Salt and Nutrient Management Plan (FVSNMP; Woodard & Curran, 2018b), groundwater storage in the FVGB was estimated to be 4,800,000 af in 1975, but is currently estimated at 4,070,000 af due to a reduction in storage of about 738,000 af between 1958 and 2017.
- According to the FVSNMP, average groundwater recharge to the FVGB is estimated to be 13,800 afa between 1998 and 2017.
- Average annual groundwater recharge exceeds current and projected (2040) groundwater production in the FVGB.
- Based on the large groundwater in storage remaining and average annual recharge that exceeds current and projected 2040 groundwater production in the FVGBThere is sufficient water supply available to serve the Kudu Project as proposed.

# **Abbreviations**

°F degrees Fahrenheit

AC alternating electrical current

af acre-feet

afa acre-feet annually

APN Assessor's Parcel Number

AVEK Antelope Valley-East Kern Water Agency

AVGB Antelope Valley Groundwater Basin

CASGEM California State Groundwater Elevation Modeling

CEQA California Environmental Quality Act

Applicant 69SV 8me LLC

CUP conditional use permit

DC direct electrical current

DWR California Department of Water Resources

ESS energy storage system

FVBGMP Fremont Valley Basin Groundwater Management Plan

FVGB Fremont Valley Groundwater Basin

FVSNMP Fremont Valley Salt and Nutrient Management Plan

gen-tie generation tie

gpm gallons per minute

GSA Groundwater Sustainability Agency

GSP Groundwater Sustainability Plan

In inches

IRWMP Integrated Regional Water Management Plan

Kudu Solar Farm

kV kilovolts

LADWP Los Angeles Department of Water and Power

MW megawatts

O&M operations and maintenance



Project Kudu Solar Farm Project

PV photovoltaic
ROW right-of-way
SB Senate Bill

SGMA Sustainable Groundwater Management Act of 2014

Stantec Consulting Services Inc.

UWMP Urban Water Management Plan

Water Code California Water Code

WSA Water Supply Assessment



# 1.0 PROJECT DESCRIPTION

# 1.1 PROJECT INFORMATION

69SV 8me LLC (Applicant) is seeking approval of a conditional use permit (CUP) for the construction and operation of an up to 500 megawatt (MW)-alternating electrical current (AC) utility-scale solar farm with energy storage, known as the Kudu Solar Farm (Kudu or Project) in unincorporated Kern County and California City, California (Figure 1). The Applicant proposes to construct, own, and operate the Project and would secure CUPs from both Kern County and California City along with permits from other relevant agencies as required by law.

# 1.1.1 Project Site Information

The Project is comprised of 75 assessor's parcels (Project Area) totaling approximately 1,955 gross acres (Table 1). The permanent disturbance acreage associated with development of the solar facility and associated infrastructure (Project Site) within the Project Area would be less than the gross acreage of the Project Area. The Project Area is adjacent to the approved Eland 1 Solar Farm, south of the existing Springbok 1 & 2 Solar Farms, and southeast of the Los Angeles Department of Water and Power (LADWP) Beacon Solar facility. The topography of the Project Area is relatively flat.

#### 1.1.2 Location

The Project Area is located in portions of unincorporated Kern County and California City, north of the California City Municipal Airport. The majority of the Project is bisected by Washburn Boulevard (which is also the California City boundary) and Neuralia Road (Figure 1).

**Table 1: Kudu Parcels** 

| No.             | APN        | Acres  |
|-----------------|------------|--------|
| California City |            |        |
| 1               | 302-020-08 | 40.17  |
| 2               | 302-020-09 | 80.09  |
| 3               | 302-020-11 | 163.68 |
| 4               | 302-020-14 | 40.99  |
| 5               | 302-020-15 | 10.52  |
| 6               | 302-020-16 | 10.15  |
| 7               | 302-020-17 | 9.59   |
| 8               | 302-020-18 | 9.98   |
| 9               | 302-290-03 | 83.58  |
| 10              | 302-305-15 | 43.54  |
| 11              | 302-321-01 | 160.93 |
| 12              | 302-322-01 | 10.10  |



1

| No.           | APN                   | Acres    |
|---------------|-----------------------|----------|
| 13            | 302-322-02            | 10.09    |
| 14            | 302-322-04            | 10.24    |
| 15            | 302-322-05            | 10.28    |
| 16            | 302-322-06            | 40.04    |
| 17            | 302-322-08            | 10.33    |
| 18            | 302-322-09            | 40.50    |
| 19            | 302-322-10            | 10.27    |
| 20            | 302-322-11            | 10.29    |
| 21            | 302-325-49            | 9.74     |
| 22            | 302-330-33            | 20.21    |
| 23            | 302-330-37            | 20.38    |
| 24            | 302-341-29            | 168.79   |
| 25            | 302-342-01            | 40.23    |
| 26            | 302-342-11            | 2.67     |
| 27            | 302-342-12            | 2.66     |
| 28            | 302-342-19            | 29.69    |
| 29            | 302-342-25            | 40.77    |
| 30            | 302-342-26            | 39.89    |
| 31            | 302-342-27            | 40.29    |
| 32            | 302-342-28            | 40.68    |
| 33            | 302-470-14            | 20.20    |
|               | California City Total | 1,281.51 |
| Unincorporate | ed Kern County        |          |
| 34            | 469-170-10            | 10.02    |
| 35            | 469-170-18            | 39.49    |
| 36            | 470-020-08            | 2.31     |
| 37            | 470-020-19            | 4.38     |
| 38            | 470-030-01            | 79.22    |
| 39            | 470-080-15            | 20.27    |
| 40            | 470-080-16            | 10.07    |
| 41            | 470-080-17            | 10.10    |
| 42            | 470-080-32            | 10.07    |
| 43            | 470-151-09            | 19.62    |
| 44            | 470-151-15            | 20.23    |
| 45            | 470-151-16            | 20.40    |
| 46            | 470-151-17            | 19.98    |
| 47            | 470-152-01            | 39.32    |



| No. | APN                              | Acres    |
|-----|----------------------------------|----------|
| 48  | 470-152-18                       | 10.32    |
| 49  | 470-152-19                       | 4.93     |
| 50  | 470-302-24                       | 2.59     |
| 51  | 470-302-25                       | 2.62     |
| 52  | 470-302-26                       | 2.52     |
| 53  | 470-322-13                       | 2.39     |
| 54  | 470-322-15                       | 9.96     |
| 55  | 470-330-01                       | 5.06     |
| 56  | 470-330-02                       | 4.77     |
| 57  | 470-330-03                       | 19.86    |
| 58  | 470-330-04                       | 20.15    |
| 59  | 470-330-06                       | 9.95     |
| 60  | 470-330-07                       | 10.02    |
| 61  | 470-330-14                       | 4.89     |
| 62  | 470-330-15                       | 5.23     |
| 63  | 470-350-04                       | 18.65    |
| 64  | 470-350-05                       | 18.91    |
| 65  | 470-350-06                       | 18.89    |
| 66  | 470-350-07                       | 18.57    |
| 67  | 470-350-08                       | 19.93    |
| 68  | 470-360-01                       | 18.43    |
| 69  | 470-360-02                       | 17.85    |
| 70  | 470-360-05                       | 21.15    |
| 71  | 470-380-01                       | 19.92    |
| 72  | 470-380-04                       | 21.35    |
| 73  | 470-380-05                       | 17.34    |
| 74  | 470-380-06                       | 19.88    |
| 75  | 470-380-07                       | 21.95    |
|     | Unincorporated Kern County Total | 673.55   |
|     | Total                            | 1,955.06 |

Note:

APN = Assessor Parcel Number



3

6574158 14 24 Santt Rd 25 30 29 California City 31 32 16 22 23 11 18 1: 302-020-08 20: 302-322-11 39: 470-080-15 58: 470-330-04 2: 302-020-09 21: 302-325-49 40: 470-080-16 4 3: 302-020-11 22: 302-330-33 41: 470-080-17 60: 470-330-07 4: 302-020-14 23: 302-330-37 42: 470-080-32 61: 470-330-14 43: 470-151-09 5: 302-020-15 24: 302-341-29 62: 470-330-15 25: 302-342-01 7: 302-020-17 26: 302-342-11 45: 470-151-16 64: 470-350-05 8: 302-020-18 27: 302-342-12 46: 470-151-17 65: 470-350-06 28: 302-342-19 47: 470-152-01 9: 302-290-03 66: 470-350-07 Lindbergh Blvd 10: 302-305-15 29: 302-342-25 48: 470-152-18 67: 470-350-08 11: 302-321-01 30: 302-342-26 31: 302-342-27 49: 470-152-19 68: 470-360-01 12: 302-322-01 50: 470-302-24 69: 470-360-02 13: 302-322-02 32: 302-342-28 14: 302-322-04 33: 302-470-14 51: 470-302-25 70: 470-360-05 52: 470-302-26 71: 470-380-01 15: 302-322-05 34: 469-170-10 35: 469-170-18 53: 470-322-13 72: 470-380-04 73: 470-380-05 16: 302-322-06 54: 470-322-15 17: 302-322-08 36: 470-020-08 55: 470-330-01 18: 302-322-09 37: 470-020-19 56: 470-330-02 74: 470-380-06 75: 470-380-07 Poppy Blvd Heath 19: 302-322-10 38: 470-030-01 57: 470-330-03 Kudu Solar Project Parcel (At original document size of 8.5x11) 1:63,360 Kudu Solar Project Area Project Eland 1 Solar Project Location Stantec MINUTE 8 Minute Solar Energy Kudu Solar Project Notes
1. Coordinate System: NAD 1983 StatePlane
California V FIPS 0405 Feet
2. Project Data Sources: 8 Minute Solar Energy and
Stantec Stantec
3. Basemap Source: Esri, DigitalGlobe, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Kudu Solar Project Parcels

Figure 1: Kudu Solar Farm - Assessors Parcels





# 1.2 DESCRIPTION OF PROPOSED PROJECT

The Applicant proposes to develop a photovoltaic (PV) energy facility and energy storage system (ESS) within the Project Area that is capable of producing up to 500 MW of AC power, and 600 MW hours (MWh) of storage capacity. Power generated by the Project would be collected using up to 230 kilovolt (kV) collector lines which run underground and/or overhead to a dedicated Project substation, or to the Eland 1 Substation. The Project may also share the Eland 1 generation tie- (gen-tie) line facilities, or gen-tie rights-of-way. The Eland 1 substation and gen-tie line have gone through environmental analysis and subsequent approval by Kern County and are not part of the Project.

Additionally, the Project may share operations & maintenance (O&M) buildings, ESS, and/or transmission facilities, as necessary, with one or more nearby solar Projects, and/or may be remotely operated. Any unused O&M building, substation, and/or transmission facility areas onsite may be covered by solar panels under such scenarios.

The Applicant has considered the following in its selection of the Project site for detailed evaluation:

- Land availability (approximately 1,955 gross acres)
- Land use zoning: primarily agriculture located away from high-density residential developments
- Proximity to interconnecting substation (approximately 7 miles away) and ability to share facilities with other solar
   Projects

Up to 20 full-time employees would operate the Project. Typically, the majority of the staff would work during the day shift (sunrise to sunset), and the remainder would work during the night shifts and weekend. As noted earlier, it is possible that the Project would share O&M, substation, and/or transmission facilities with one or more nearby solar projects and may be remotely operated. In such scenarios, the Project's onsite staff could be reduced.

After the useful life of the Project, the panels would be disassembled from the mounting frames, and the Project site would be restored to its pre-development function.

# 1.2.1 PV Module Configuration

The Project would use PV panels or modules¹ on mounting frameworks to convert sunlight directly into electricity. Individual panels would be installed on either fixed-tilt or tracker mount systems (single- or dual- axis, using galvanized steel or aluminum). If the panels are configured for fixed tilt, they would be oriented toward the south. For tracking configurations, the panels would rotate to follow the sun over the course of the day. Although the panels could stand up to 20 feet high, depending on the mounting system used and county building codes, panels are expected to remain between 6 and 8 feet high.

The solar panel array would be arranged in groups called blocks, with inverter stations generally located centrally within the blocks. Blocks would produce direct electrical current (DC), which is converted to AC at the inverter stations.

<sup>&</sup>lt;sup>1</sup> Including but not limited to bi-facial or concentrated photovoltaic (CPV) technology



-

Each PV module would be placed on a fixed-tilt or tracker mounting structure. The foundations for the mounting structures can extend up to 10 feet below ground, depending on the structure, soil conditions, and wind loads, and may be encased in concrete or use small concrete footings. Final solar panel layout and spacing would be optimized for Project Area characteristics and the desired energy production profile.

#### 1.2.2 Inverter Stations

DC energy is delivered from the panels via cable to inverter stations, generally located near the center of each block. Inverter stations convert the DC energy to AC energy, which can be dispatched to the transmission system. Inverter stations are typically comprised of one or more inverter modules with a rated power of up to 2 MW each, a unit transformer, and voltage switch gear. The unit transformer and voltage switch gear are housed in steel enclosures, while the inverter module(s) are housed in cabinets. Depending on the vendor selected, the inverter station may lie within an enclosed or canopied metal structure, typically on a skid or concrete mounted pad. No water demand is expected for the inverter stations.

# 1.2.3 Energy Storage System

The Project may include one or more ESS, located at or near a substation/switchyard (onsite or shared) and/or at the inverter stations, or elsewhere onsite. Such large-scale ESSs would be up to 600 MW AC in capacity and up to 25 acres in total area. ESSs consist of modular and scalable battery packs and battery control systems that conform to U.S. national safety standards. The ESS modules, which could include commercially available lithium or flow batteries, typically consist of International Organization of Standardization (ISO) standard containers (approximately 40 feet long by 8 feet wide by 8 feet high) housed in pad- or post-mounted, stackable metal structures, but may also be housed in a dedicated building(s) in compliance with applicable regulations. The maximum height of a dedicated structure is not expected to exceed 25 feet. The actual dimensions and number of energy storage modules and structures would vary depending on the application, supplier, and configuration chosen, as well as on offtaker/power purchase agreement requirements and on county building standards. The Project may share an ESS with one or more nearby solar Projects or may operate one or more standalone ESS facilities within the Project site. No water demand is expected for the ESS.

#### 1.2.4 Substation

Output from the inverter stations would be transferred via electrical conduits and electrical conductor wires to one or more Project substations or switchyards (collectively referred to as substations herein), or the Eland 1 Substation. The Project and any associated ESS would have their own dedicated substation equipment located either within the Project site, or within the Eland 1 Substation footprint. Dedicated equipment may incorporate several components, including auxiliary power transformers, distribution cabinets, revenue metering systems, a microwave transmission tower, and voltage switch gear. Each substation would occupy an area of up to approximately 5 acres, secured separately by a chain-link fence. The final location(s) of each component would be determined before the issuance of building permits.

Substations typically include a small control building (roughly 500 square feet) standing approximately 10 feet tall. The building is either prefabricated concrete or steel housing, with rooms for the voltage switch gear and the metering equipment, a room for the station supply transformer, and a separate control technology room in which the main



computer, the intrusion detection system, and the main distribution equipment are housed. Components of this building (e.g., control technology room and intrusion detection system) may instead be located at an O&M building described later in this document. No water demand is expected for the substation.

#### 1.2.5 Transmission Line

Power generated by the Project would be transmitted to the Los Angeles Department of Water and Power (LADWP) Barren Ridge Substation via a 230 kV overhead and/or underground gen-tie. The Project intends to share the Eland 1 gen-tie line and right-of-way, which may require stringing additional line on the Eland 1 transmission structures or increasing the capacity of the Eland 1 gen-tie by reconductoring the line with thicker cable. If the Project cannot share these facilities, a new gen-tie line would be developed within one of the routes previously analyzed in the Eland 1 Environmental Impact Report. No water demand is expected for the transmission lines.

#### 1.2.6 Water Usage

Water demand for panel washing and O&M domestic use is not expected to exceed 50 acre-feet per annum (afa) based on water usage at existing, similarly sized solar facilities. Water usage during construction, primarily for dust-suppression purposes, is not expected to exceed 400 acre-feet (af). It is anticipated that water would be obtained from existing onsite wells located within Fremont Valley Groundwater Basin (FVGB). Alternatively, water may be obtained from one or more offsite municipal source(s) and delivered to the Project Area via truck. If offsite water is used, it would likely be obtained from one of the nearby Springbok Projects, the Eland 1 Project, or from a commercial source. If the Applicant determines that offsite water would be used, the Applicant would submit a Will Serve Letter from the proposed offsite water purveyor(s), specifically, the City, for those parcels located within California City. A small water treatment system may be installed to provide deionized water for panel washing.

#### 1.2.7 Water Storage Tanks

One or more aboveground water storage tanks with a total capacity of up to 50,000 gallons may be placed onsite near the O&M building. The storage tank(s) near the O&M building would have the appropriate fire department connections to be used for fire suppression purposes.

## 1.2.8 Operations and Maintenance Building

The Project may include an O&M building approximately 40 feet by 80 feet in size, with associated onsite parking. The O&M building would be steel framed, with metal siding and roof panels. The O&M building may include the following:

- 1. Office
- 2. Repair building/parts storage
- 3. Control room
- 4. Restroom
- 5. Septic tank and leach field

Roads, driveways, and parking lot entrances would be constructed in accordance with Kern County and California City improvement standards. Parking spaces and walkways would be constructed in conformance with all California accessibility regulations.



As noted earlier, the Project may share O&M facilities and/or staff with one or more nearby solar Projects and may be remotely operated. Any unused O&M areas onsite may be covered by solar panels.

# 1.2.9 Project Site Security and Fencing

The Project site would be enclosed within a chain link fence with barbed wire measuring up to 8 feet in height from finished grade. An intrusion alarm system comprised of sensor cables would be integrated into the perimeter fence, intrusion detection cabinets placed approximately every 1,500 feet along the perimeter fence, and an intrusions control unit, located either in the substation control room or at the O&M building, or similar technology, may be installed. Additionally, the Project may include additional security measures including but not limited to barbed wire, low voltage fencing with warning reflective signage, controlled access points, security alarms, security camera systems, and security guard vehicle patrols to deter trespassing and/or unauthorized activities that could interfere with operation of the Project.

Controlled access gates would be maintained at the main entrances to the Project site. Project site access would be provided to offsite emergency response teams that respond in the event of an after-hours emergency. Enclosure gates would be manually operated with a key provided in an identified key box location.

# 1.2.10 Project Site Lighting

Project site lighting would be directed away from public rights-of-way. Lighting used onsite would be minimal. Site lighting may include motion sensor lights for security purposes. Lighting used onsite would be of the lowest intensity foot candle level, in compliance with any applicable regulations, measured at the property line after dark.

### 1.3 ANNUAL PRODUCTION

The Project would generate electrical power during daylight hours. Peak electricity demand in California corresponds with air conditioning use on summer afternoons when ambient temperatures are high. The Project's peak generating capacity corresponds to this time-period. There is no generating capacity between sunset and sunrise due to the lack of solar energy, though power may be released from the ESS at any time of day.

The Project would have a nominal output capacity of up to 500 MW AC and 600 MWh of storage capacity, sufficient to power roughly 240,000 homes and displacing 745,000 tons of carbon dioxide equivalent (CO<sub>2</sub>e) per year when compared to a gas-fired power plant or 1,476,000 tons when compared to a coal-fired power plant.

# 1.4 CONSTRUCTION ACTIVITIES

The construction period for the Project, from site preparation through construction, testing, and commercial operation, is expected to commence as early as Q4 2021 and would extend for approximately 12 to 18 months.

Construction of the facility would include the following activities:

- Site preparation
- Grading and earthwork
- Concrete foundations



- Structural steel work
- Electrical/instrumentation work
- Collector line installation
- Architecture and landscaping

No roadways would be affected by the Project, except during the construction period. Construction traffic would access the site from Philips Road, Gantt Road, and Neuralia Road, or through the Eland 1 Project site. It is estimated that up to 1,000 workers per day (during peak construction periods) would be required during the construction of the Project.

Heavy construction is expected to occur between 6:00 AM and 5:00 PM, Monday through Friday. Additional hours may be necessary to make up schedule deficiencies or to complete critical construction activities. Some activities may continue 24 hours per day, seven days per week. Low-level noise activities may potentially occur between the hours of 10:00 PM and 7:00 AM. Nighttime activities could potentially include but are not limited to refueling equipment, staging material for the following day's construction activities, quality assurance and control, and commissioning.

Materials and supplies would be delivered to the Project Area by truck. Truck deliveries would normally occur during daylight hours. However, there would be offloading and/or transporting to the Project Area on weekends and during evening hours.

Earth-moving activities are expected to be limited to the construction of the access roads, O&M building, substation, ESS(s), and any stormwater protection or storage (detention) facilities. Final grading may include revegetation with low-lying grass or applying earth-binding materials to disturbed areas.

#### 1.5 WORK FORCE

Once the Project is constructed, maintenance would generally be limited to the following:

- 1. Cleaning of PV panels
- 2. Monitoring electricity generation
- 3. Providing site security
- 4. Facility maintenance: replacing or repairing inverters, wiring, and PV modules

It is expected that the Project would require an operational staff of up to 20 full-time employees. As noted earlier, it is possible that the Project would share O&M, substation, ESS, and/or transmission facilities with one or more nearby Projects. In such a scenario, the Projects would share personnel, thereby potentially reducing the Project's on-site staff.

The facility would operate seven days a week, 24 hours a day, generating electricity during normal daylight hours when the solar energy is available. Maintenance activities may occur seven days a week, 24 hours a day to ensure PV panel output when solar energy is available.



# 1.6 PROJECT FEATURES AND BEST MANAGEMENT PRACTICES

The following sections describe standard Project features and best management practices that would be applied during construction and long-term operation of the Project to maintain safety and minimize or avoid environmental impact.

# 1.6.1 Waste and Hazardous Materials Management

The Project would have minimal levels of materials onsite that have been defined as hazardous under 40 Code of Federal Regulations (CFR), Part 261. The following materials are expected to be used during the construction, operation, and long-term maintenance of the Project:

- Insulating oil: used for electrical equipment
- Lubricating oil: used for maintenance vehicles
- Various solvents and detergents: equipment cleaning
- Gasoline: used for maintenance vehicles

Hazardous materials and wastes would be managed, used, handled, stored, and transported in accordance with applicable local and state regulations. All hazardous wastes would be maintained at quantities below the threshold requiring a Hazardous Material Management Program (HMMP): one 55-gallon drum. Though not expected, should any onsite storage of hazardous materials exceed one 55-gallon drum, an HMMP would be prepared and implemented.

# 1.6.2 Spill Prevention and Containment

Less than 55 gallons of hazardous materials would be stored onsite. Spill prevention and containment for construction and operation of the Project would adhere to the Environmental Protection Agency's guidance on Spill Prevention Control and Countermeasures.

# 1.6.3 Wastewater/Septic System

A standard onsite septic tank and leach field may be used at the O&M building to dispose sanitary wastewater, designed to meet O&M guidelines required by Kern County laws, ordinances, regulations, and standards.

#### 1.6.4 Inert Solids

Inert solid wastes resulting from construction activities may include recyclable items such as paper, cardboard, solid concrete and block, metals, wire, glass, type 1-4 plastics, drywall, wood, and lubricating oils. Non-recyclable items include insulation, other plastics, food waste, vinyl flooring and base, carpeting, paint containers, packing materials, and other construction wastes. A construction waste management plan would be prepared for review by the county and California City. Consistent with local regulations and the California Green Building Code, the plan would provide for diversion of a minimum of 50 percent of construction waste from landfill.

Chemical storage tanks (if any) would be designed and installed to meet applicable local and state regulations. Any wastes classified as hazardous, such as solvents, degreasing agents, concrete curing compounds, paints, adhesives,



chemicals, or chemical containers, would be stored in an approved storage facility/shed/structure and disposed of as required by local and state regulations. Material quantities of hazardous wastes are not expected.

#### 1.6.5 Health and Safety

Safety precautions and emergency systems would be implemented as part of the design and construction of the Project to ensure safe and reliable operation. Administrative controls would include classroom and hands-on training in O&M procedures, general safety items, and a planned maintenance program. These would work with the system design and monitoring features to enhance safety and reliability.

The Project would have an emergency response plan (ERP). The ERP would address potential emergencies including chemical releases, fires, and injuries. All employees would be provided with communication devices, cell phones, or walkie-talkies to provide aid in the event of an emergency.

# 1.7 CLIMATE

The northern Antelope Valley region is considered a "high desert" environment, with an arid climate that is characterized by hot, dry summers and cool winters with very little precipitation. Most of the annual precipitation occurs during the period from November through April. The average annual temperature is roughly 63.8 degrees Fahrenheit (°F), although it is not unusual for the temperature to exceed 100 °F in summer (Table 2).

Table 2: Average Monthly and Annual Evapotranspiration, Precipitation and Temperature

| Month     | Average<br>Evapotranspiration (in) | Average Total Precipitation (mm/in) | Average Temperature (°F) |
|-----------|------------------------------------|-------------------------------------|--------------------------|
| January   | 1.24                               | 23/0.91                             | 45                       |
| February  | 2.24                               | 21/0.83                             | 49.3                     |
| March     | 3.72                               | 16/0.63                             | 53.1                     |
| April     | 5.7                                | 8/0.31                              | 59.5                     |
| May       | 7.44                               | 2/0.08                              | 68                       |
| June      | 8.1                                | 1/0.04                              | 76.8                     |
| July      | 8.68                               | 2/0.08                              | 83.5                     |
| August    | 7.75                               | 5/0.2                               | 81.9                     |
| September | 5.7                                | 5/0.2                               | 75.2                     |
| October   | 4.03                               | 4/0.16                              | 64.8                     |
| November  | 2.1                                | 16/0.63                             | 52.5                     |
| December  | 1.2                                | 16/0.63                             | 45                       |
| Annual    | 57.9                               | 119/4.69                            | 62.8                     |

Notes:

°F = degrees Fahrenheit

in = inches

mm/in = millimeters AND inch Source: climate-data.org



California has experienced three declared droughts in the last three decades. In 1976, the state received an average of only 7.4 inches of rain. Until recently, the drought of 1987–1992 was considered the most severe drought in California's history. However, the severity of that drought period has been eclipsed by the historic drought experienced from 2011–2016. Conversely, these drought periods are often offset by periods of intense rainfall that can lead to flooding. This extreme climatic variability is common throughout California.



# 2.0 WATER SUPPLY PLANNING UNDER SENATE BILL 610

Senate Bill (SB) 610 was passed into law on January 1, 2002. This legislation identified the need to incorporate water supply and demand analysis at the earliest possible stage in the planning process. SB 610 amended portions of the Water Code, including Section 10631, which contains the Urban Water Management Planning Act, as well as adding Sections 10910, 10911, 10912, 10913, and 10915, which describe the required elements of a WSA.

A Water Supply Assessment (WSA) is designed to build on the information that is typically contained in an Urban Water Management Plan (UWMP). The amendments to Water Code Section 10631 were designed to make WSAs and UWMPs consistent. A key difference between WSAs and UWMPs is that UWMPs are required to be revised every five years, in years ending with either zero or five, while WSAs are required as part of the environmental review process for each individually qualifying Project. Not all providers who prepare a WSA are required to prepare an UWMP.

A companion bill (SB 221) was also passed at the same time as SB 610. This law requires that approval by a city or county of certain residential subdivisions, as defined by California Government Code Section 66473.7(a)(1), must include an affirmative written verification of sufficient water supply. SB 221 is designed as a fail-safe mechanism to ensure that collaboration on identifying water supplies to serve a new large subdivision occurs early in the planning process. This verification must also include documentation of historical water deliveries for the previous 20 years, as well as a description of foreseeable impacts on the availability of water resources in the region of the proposed subdivision.

#### 2.1 WATER SUPPLY ASSESSMENT

The WSA process involves answering the following questions:

- Is the Project subject to the CEQA?
- Is it a Project under SB 610?
- Is there a public water system?
- Is there current UWMP that accounts for the Project demand?
- Is groundwater a component of the supplies for the Project?
- Are there sufficient supplies available to serve the Project over the next 20 years?

# 2.1.1 Is the Project Subject to CEQA?

The first step in the WSA process is determining whether the Project is subject to CEQA. SB 610 amended Public Resources Code Section 21151.9 to read, "Whenever a city or county determines that a Project, as defined in Section 10912 of the Water Code, is subject to this division [i.e., CEQA], it shall comply with part 2.10 (commencing with Section 10910) of Division 6 of the Water Code."

**Conclusion:** The proposed Project will undergo environmental review pursuant to the requirements of CEQA; therefore, the information contained in this assessment would be used to support the analysis contained in the CEQA document.

# 2.1.2 Is It a Project Under Senate Bill 610?

The second step in the SB 610 process is to determine if a Project meets the definition of a "Project" under Water Code Section 10912 (a). Under this section, a "Project" is defined as meeting any of the following criteria:

- A proposed residential development of more than 500 dwelling units;
- A proposed shopping center or business establishment employing more than 1,000 persons or having more than 500,000 square feet of floor space;
- A commercial building employing more than 1,000 persons or having more than 250,000 square feet of floor space;
- A hotel or motel with more than 500 rooms;
- A proposed industrial, manufacturing, or processing plant, or industrial park, planned to house more than 1,000 persons, occupying more than 40 acres of land, or having more than 650,000 square feet of floor area;

In addition, , if a public water system has less than 5,000 service connections, the definition of a "Project" also includes any proposed residential, business, commercial, hotel, or motel, or industrial development that would account for an increase of 10 percent or more in the number of service connections for the public water system. In the portion of the proposed Project that lies within California City, in 2015, there were 4,430 active service connections serving 2,469 af of water (out of 3,606 af produced) to a population of 14,233 according to the Urban Water Management Plan (UWMP) 2015 Update (California City, 2017). The proposed Kudu Project will not increase service connections by more than 10%. Based on the foregoing, the Project does not include any development listed under Section 19012(a) of the Water Code.

**Conclusion:** The proposed Kudu Project does not meet the definition of a "Project" under Water Code Section 10912(a).

#### 2.1.3 Is There a Public Water System?

The third step in the WSA process is determining if there is a "public water system" to serve the Project. Section 10912 (c) of the Water Code states, "[A] public water system means a system for the provision of piped water to the public for human consumption that has 3,000 or more service connections."

Conclusion: California City operates and maintains a public water system (No. 1510032) that provides water service to most of its residential, commercial and industrial properties within its corporate boundaries (Quad Knopf, 2002; California City, 2017). Approximately 33 parcels in the proposed Kudu project which occupy an area of 1,281.51 acres are located within California City. The portion of the Kudu project that lies within California City will be served by the California City Water Department (personal communication, Jose "Joe" Barragan, Public Works Director, May 19, 2020). The 44 unincorporated parcels in the proposed Kudu project that occupy an area of 673.55 acres are not connected to a public water system and would use groundwater or truck water from nearby sources.

# 2.1.4 Is There a Current UWMP That Accounts for the Project Demand?

Step four in the WSA process involves determining if there is a current UWMP that considers the projected water demand for the Project Area. The Water Code requires that all public water systems providing water for municipal purposes to more than 3,000 customers, or supplying more than 3,000 afa, must prepare an UWMP, and this plan must be updated at least every 5 years on or before December 31, in the years ending in five and zero. Water Code Section 10910 (c) (2) states, "If the projected water demand associated with the proposed Project was accounted for in the most recently adopted urban water management plan, the public water system may incorporate the requested information from the UWMP in preparing the elements of the assessment required to comply with subdivisions (d), (e), (f), and (g) [i.e., the WSA]."

Conclusion: The City prepared an UWMP 2015 Update (California City, 2017). According to the UWMP, California City had 4,430 active service connections in 2015 serving a population of 14,233. The portion of the Kudu project that lies within California City will be served by the California City Water Department (personal communication, Jose "Joe" Barragan, Public Works Director, May 19, 2020). However, the UWMP does not account for delivery of water to the incorporated portion of the Kudu project. The portion of the Kudu project that lies outside California City in unincorporated Kern County would not be served by a public water system and there is no current UWMP that accounts for the unincorporated Kern County portion of the Kudu project water demand.

# 2.1.5 Is Groundwater a Component of the Supplies of the Project?

This section addresses the requirements of the Water Code Section 110910 (f), paragraphs 1 through 5, which apply if groundwater is a water source for a proposed Project. Pursuant to Water Code Section 10910 (f), the groundwater analysis presented in this analysis focuses on the Fremont Valley Groundwater Basin (Figure 2).

According to DWR (2004): The FVGB (Basin No. 6-046) underlies Fremont Valley in eastern Kern County and northwestern San Bernardino County. The basin is bounded on the northwest and north by the Garlock fault zone against impermeable crystalline rocks of the Sierra Nevada and El Paso Mountains.. This FVGB is bounded by the Summit Range, Rand Mountains, Red Mountain, Lava Mountains, Castle Butte, Bissel Hills, and Rosamond Hills.

The basin is bounded on the southwest by the Antelope Valley Groundwater Basin (AVGB) along a groundwater divide from the mouth of Oak Creek through Middle Butte to exposed basement rock near Gem Hill. Average annual rainfall in the Fremont Valley ranges from 4 to 12 inches. Surface water in Fremont Valley drains toward Koehn Lake; however, surface drainage overlying the southwestern part of the basin drains southward toward the town of Rosamond. Water demand for the 673.55-acre portion of the Project within unincorporated Kern County would be entirely met through the delivery of groundwater produced by onsite wells or water purchased from other nearby sources. The unincorporated Kern County portion of the Project occupies 34.5% of the total Project Area. The total operation demand for the Project would be approximately 50 afa, and the temporary demand during construction would be 400 af. The total operation and temporary construction water demand for the portion of the Project within unincorporated Kern County would be 17.25 afa and 37.75 afa, respectively.

**Conclusion:** Groundwater production in the unincorporated portion of the Project is not considered a de minimis extraction under Section 10721 of the Water Code.

Bodish FREMONT VALLEY (6-046) Mojave 395 MOJAVE DESERT ANTELOPE VALLE Kudu Solar Farm Survey Area (At original document size of 8.5x11) 1:506,880 Fremont Valley Groundwater Basin Project Location Stantec MINUTE Fremont Valley Groundwater Basin

Figure 2: Fremont Valley Groundwater Basin

#### **Groundwater Basin Description**

According to DWR (2004), "Both Quaternary alluvium and lacustrine deposits are water-bearing; however, the alluvium is the most important water-bearing material in the basin (DWR 1969). Alluvium is about 1,190 feet thick (Bader 1969; DWR 1964) along the margin of the basin and thins toward the middle of the basin, where it is interbedded with thick layers of lacustrine silt and clay near Koehn Lake. Groundwater in the alluvium is generally unconfined, although locally confined conditions occur near Koehn Lake (DWR 1964). Average well yield is about 530 gallons per minute (gpm) with a maximum yield of 2,580 gpm (DWR 1975)."

"The Garlock and El Paso fault zones, which extend along the foothills of the Sierra Nevada and El Paso Mountains, form restrictive groundwater barriers on the west and northwest sides of the basin (Dibblee 1967). The Cantil Valley fault traverses the northeast part of the basin, but its effect on groundwater is not known. The Muroc fault traverses the central part of the basin and forms a partial barrier to groundwater flow (DWR 1964). Natural recharge of the basin includes percolation of ephemeral streams that flow from the Sierra Nevada. The general groundwater flow direction is toward Koehn Lake at the center of the valley (Bader 1969, DWR 1964). There is no appreciable quantity of groundwater flowing out of the basin (Bader 1969)." The total storage capacity of the basin is calculated to be 4,800,000 af (DWR 2004) based on DWR (1975). However, a more recent analysis of groundwater storage is presented in the FVBSNMP (Woodard & Curran, 2018b), which is based on a comparison of groundwater contour maps in 1958 and 2017. The estimated change in storage during this period is -738,100 af, results inequivalent to a groundwater in storage of 4,070,000 af. Groundwater recharge in this analysis is estimated at 13,800 afa (Woodard & Curran, 2018b).

Groundwater quality within FVGB was assessed as part of the FVGMP (Woodard & Curran, 2018a) and FVBSNMP (Woodard & Curran, 2018b). Constituents showing elevated concentrations in the basin included Total Dissolved solids near Koehn Lake, as well as localized areas of arsenic, hexavalent chromium, and nitrate. Perchlorate has not been identified as an issue in the region (Woodard & Curran, 2018a).

#### **Groundwater Management**

In November 2009, the governor signed into law SBx7-6, which established the California Statewide Groundwater Elevation Monitoring (CASGEM) Program. Groundwater level data entered into DWR's online CASGEM reporting system by monitoring entities beginning in January 2012 were used to establish groundwater basin prioritization as part of the enactment of the Sustainable Groundwater Management Act (SGMA) of 2014. Enactment of SGMA amended Water Code Section 10720 *et al.* in an effort to provide a statewide system for the sustainable management of groundwater. For medium- and high-priority groundwater basins, SGMA requires the designation of a Groundwater Sustainability Agency (GSA). GSAs have broad groundwater management powers. For example, GSAs may require groundwater well registration, measurement of groundwater extractions, and filing of annual extractions reports.

SGMA authorizes GSAs to regulate groundwater extractions by imposing well spacing requirements, limiting extractions, and establishing extraction allocations. The legislation does not apply to adjudicated groundwater basins that are managed by the courts or to basins deemed by DWR to be low priority. SGMA requires GSAs to adopt Groundwater Sustainability Plans (GSPs) for medium- and high-priority basins. These plans must set the groundwater basin on a course toward sustainable management to eliminate adverse groundwater conditions specified as undesirable results. The law allows a local agency that has, "water supply, water management, or land

use responsibilities within a groundwater basin, to elect to be a GSA." The AVGB, which borders the FVGB to the south and southwest is adjudicated but the FVGB is not.

Note: No GSA has been formed to serve the FVGB; therefore, management is assumed by Kern County.

#### **Governance and Local Control**

The SGMA requires that all high- and medium-priority groundwater basins must establish governance under one or more GSAs by June 30, 2017. GSAs for high- and medium-priority basins must adopt their GSP by January 31, 2022. Low-priority basins are not required to prepare a GSP.

The FVGB is designated under CASGEM as a "low priority" groundwater basin at this time; and as such, is not subject to SGMA GSA and GSP requirements.

In 2019, the Fremont Basin Integrated Regional Water Management Plan (IRWMP) was prepared on behalf of California City, Mojave Public Utilities District (MPUD) and AVEK; Woodard & Curran, 2019). As part of this document the FVGWMPWoodard & Curran, 2018a) and FVBSNNMP (Woodard & Curran, 2018b) were prepared as supplements to the IRWMP as Appendix B and C, respectively. According to the FVGMP, the intent of the FVGMP is..." to act as a "pre-GSP" document that will support and inform the future development of a GSP for the FVGB" (Woodard & Curran, 2018b, p. 1-3).

**Conclusion:** The FVGB has been designated as a low-priority basin and is not required to prepare a GSP. A FVBGMP was prepared as a pre-GSP document in the event the FVGB is required to prepare a GSP at a future date.

# **Groundwater Sustainability Plans**

GSPs must include minimum thresholds and measurable objectives to achieve the goal of groundwater basin sustainability within 20 years of GSP implementation. The SGMA defines GSPs that achieve sustainable groundwater management by ensuring that the applicable basin is operated within the sustainable yield. Sustainable yield is defined as the maximum quantity of water that can be withdrawn over a period of years without causing an undesirable result. An undesirable result means one or more of the following effects cause by groundwater conditions occurring throughout the basin:

- Chronic lowering of groundwater levels;
- Significant and unreasonable reduction of groundwater storage;
- Significant and unreasonable seawater intrusion;
- Significant and unreasonably degraded water quality;
- Significant and unreasonable land subsidence that substantially interferes with surface land uses; and/or
- Depletions of interconnected surface water that have significant and unreasonable adverse impacts on beneficial uses of the surface water.

The GSP must include monitoring and management for the basin over a 50-year planning horizon, and plans must articulate measurable objectives to be achieved every 5 years. The DWR will review the plans and will have the power to request changes to a submitted plan. The plan must establish measurable objectives, as well as incremental milestones every 5 years in order to achieve the sustainability goals identified in the plan within 20 years.

As noted above, the FVBGMP was prepared in 2018 (Woodard & Curran, 2018a). The FVBGMP preliminarily addressed the six GSP undesirable results and developed a strategy for monitoring five of the six undesirable results. Seawater intrusion was dismissed owing to the land locked nature of the groundwater basin and distance from a saline water body (e.g., Pacific Ocean).

**Conclusion:** The FVGB has been designated as a low priority basin. Therefore, no GSP is required. A FVBGMP was prepared as a pre-GSP document in the event the FVGB is required to prepare a GSP at a future date.

# 2.1.6 Are There Sufficient Supplies to Serve the Project Over the Next Twenty Years?

The next step in the WSA process is to prepare the actual assessment of the available water supplies, including the availability of these supplies in all water-year conditions over a 20-year planning horizon and an assessment of how these supplies relate to Project-specific and cumulative demands over that same 20-year period. To be consistent, the analysis horizon of this WSA extends to 2041. Water Code Section 10910 (c)(4) states, "If the city or county is required to comply with this part pursuant to subdivision (b), the water assessment for the Project shall include a discussion with regard to whether the total projected water supplies, determined to be available by the city or county for the Project during normal, single dry, and multiple dry water years during a 20-year projection, will meet the projected water demand associated with the proposed Project, in addition to existing and planned future uses including agricultural and manufacturing uses." Tables 3 and 4 provide future water supply availability for the Project in the FVGB and California City, respectively. The estimated annual water demand in the FVGB in 2020 is 9,487 af and is expected to increase to 12,301 af in 2040 under baseline conditions (Woodard & Curran, 2018a). Current and projected groundwater production in the FVGB is estimated to be 7,515 af in 2020 and 9,894 af in 2040 (Woodard & Curran, 2018a). In addition, imported State Water Project (SWP) water purchased from and delivered to local water agencies by AVEK is estimated to be 1,190 af in 2020 and 1,420 af in 2040. Recycled water produced locally is estimated to be 783 af in 2020 and 988 af in 2040 (Woodard & Curran, 2018a).

Table 3: Future Water Supply Availability (2040) in the FVGB

| Current Source               | Average Water | Single Dry | Multiple Dry Water Years |        |        |  |  |
|------------------------------|---------------|------------|--------------------------|--------|--------|--|--|
| Current Source               | Year          | Water Year | Year 1                   | Year 2 | Year 3 |  |  |
| Groundwater (FVGB)           | 9,894         | 9,894      | 9,894                    | 9,894  | 9,894  |  |  |
| Imported SWP Water<br>(AVEK) | 1,190         | 1,190      | 1,190                    | 600    | 0      |  |  |
| Total Supply                 | 11,084        | 11,084     | 11,084                   | 10,494 | 9,894  |  |  |

Current and projected groundwater production in California City is estimated to be 7,678 af in 2020 and 2040 (California City, 2017). In addition, imported State Water Project (SWP) water purchased from and delivered to California City by AVEK is estimated to be 962 af in 2020 and 2040. Recycled water produced locally, which is used to irrigate Tierra Del Sol Golf Course and maintain Central Park Lake, is estimated to be 761.4 af in 2020 and 962.4 af in 2040 (California City, 2017).

Table 4: Future Water Supply Availability (2040) in California City

| Current Source (a)(b)     | Average Water<br>Year | Single Dry<br>Water Year | Multiple Dry Water Years |        |        |
|---------------------------|-----------------------|--------------------------|--------------------------|--------|--------|
|                           |                       |                          | Year 1                   | Year 2 | Year 3 |
| Groundwater (c)           | 7,678                 | 7,678                    | 7,678                    | 7,678  | 7,678  |
| Imported SWP Water (AVEK) | 1,071                 | 1,071                    | 1,071                    | 1,071  | 1,071  |
| Recycled Water            | 962                   | 962                      | 962                      | 962    | 962    |
| Total Supply              | 9,711                 | 9,711                    | 9,711                    | 9,711  | 9,711  |

#### Notes:

- (a) af = acre-feet
- (b) Estimates from California City's UWMP 2015 Update (California City, 2017). Values converted from million gallons to acre-feet using 1 acre-foot = 325,850 gallons.
- (c) Estimate based on 80% of total groundwater production capacity.

**Conclusion:** According to Woodard & Curran (2018a), groundwater production in the FVGB is estimated to be 7,515 afa in 2020 and projected to be 9,894 afa in 2040 under baseline conditions. In the California City's UWMP 2015 Update (California City, 2017), groundwater production is estimated to be 7,678 afa in 2020 and 2040, with additional sources of supply including 1,071 afa of imported SWP water from AVEK in 2020 and 2040, and 761.4 afa and 962.4 afa of recycled water produced locally in 2020 and 2040, respectively.

#### **Project Site Demands**

Since the mid to late 1970s, there has been little or no consumptive demand at the proposed Kudu Project site. The Project estimates an annual demand of 50 afa for all operations, which is based on water use at other, similarly sized solar project, and includes cleaning of the solar panels. It is anticipated that the annual demand will remain constant over the 20-year projection as shown in Table 5.

Table 5: Anticipated Future Project Water Demand (2040)

| Land Use Category          | Total Acres | Avg demand (afa/acre) | Estimated Total<br>Demand (afa) |
|----------------------------|-------------|-----------------------|---------------------------------|
| California City            | 1,281.51    | 0.026                 | 32.75                           |
| Unincorporated Kern County | 673.55      | 0.026                 | 17.25                           |
| TOTAL                      | 1,955.06    | 0.026                 | 50                              |

Note:

afa = acre-feet annually

# Comparison of Available Water Supplies Versus Demand

Section 10910 (c)(3) of the Water Code states, "The water supply assessment for the Project shall include a discussion with regard to whether the public water system's total projected water supplies available for normal, dry, and multiple dry water years during a 20-year projection will meet the projected water demand associated with the proposed Project, in addition to the public water system's existing and planned future uses, including agricultural and manufacturing uses."

As described in the City's UWMP 2015 Update (California City, 2017), in 2015, the City operated and maintained six water wells with a production capacity of 5,100 gallons per minute (gpm) or 2,680.56 million gallons per annum (mga; 8,226.36 afa). In 2020, the City was projected to operate and maintain two additional wells increasing the total production capacity to 5,750 gpm or 3,127.32 mga (9,597.42 afa). In addition to groundwater, the City imports SWP water from AVEK which was 1,700 af in 2015 and is estimated to be 1,070 af in 2020. Between 2010 and 2015, groundwater pumped by the City averaged of 968.26 mga or 2,971.5 afa. During the same period, deliveries of imported SWP water from AVEK averaged 310.59 mga or 953.2 afa.

Tables 6 and 7 present future water supply demand at Project build-out in the FVGB and California City, respectively. As shown in the tables there is ample supply of water available to the portions of the Project within unincorporated Kern County in the FVGB and in California City, respectively.

Table 6: Future Water Supply Versus Project Water Demand at Build-Out in the FVGB

| Current Source               | Average Water<br>Year | Single Dry<br>Water Year | Multiple Dry Water Years |        |        |
|------------------------------|-----------------------|--------------------------|--------------------------|--------|--------|
|                              |                       |                          | Year 1                   | Year 2 | Year 3 |
| Groundwater (FVGB)           | 9,894                 | 9,894                    | 9,894                    | 9,894  | 9,894  |
| Imported SWP Water (AVEK)*   | 1,190                 | 1,190                    | 1,190                    | 600    | 0      |
| Total Demand (Kudu)          | 50                    | 50                       | 50                       | 50     | 50     |
| Estimated Surplus/ Shortfall | 11,034                | 11,034                   | 11,034                   | 10,444 | 9,844  |

Note:

af = acre-feet

\*estimates from 2040 projection.

Table 7: Future Water Supply Versus Project Demand at Build-Out in California City

| Current Source (a)(b)        | Average Water<br>Year | Single Dry<br>Water Year | Multiple Dry Water Years |         |         |
|------------------------------|-----------------------|--------------------------|--------------------------|---------|---------|
|                              |                       |                          | Year 1                   | Year 2  | Year 3  |
| Groundwater                  | 7,678                 | 7,678                    | 7,678                    | 7,678   | 7,678   |
| Imported SWP Water (AVEK)    | 1,071                 | 1,071                    | 1,071                    | 1,071   | 1,071   |
| Total Demand (Kudu) (c)      | 32.8                  | 32.8                     | 32.8                     | 32.8    | 32.8    |
| Estimated Surplus/ Shortfall | 8,716.2               | 8,716.2                  | 8,716.2                  | 8,716.2 | 8,716.2 |

Note:

<sup>(</sup>a) All units in afa

<sup>(</sup>b) Estimates from California City's UWMP 2015 Update (California City, 2017). Values converted from million gallons to acre-feet using 1 acre-foot = 325,850 gallons.

<sup>(</sup>c) Assumes only the portion of the Project within California City that will be served by the California City Water Department, or  $65.5\% \times 50$  afa = 32.8 afa.

**Conclusion:** The estimated annual demand for the Project does not represent a de minimis use compared to existing available water supplies in the FVGB and the portion of the Kudu Project located within California City; however, there are adequate supplies available to serve the proposed Kudu Project under all water year conditions..

## 2.1.7 Conclusions

According to the requirements of Water Code Section 10910(c)(3), the water supply assessment shall include a discussion of, "whether the public water system's total projected water supplies available will meet the projected water demand associated with proposed Project, in addition to the public water system's existing and planned future uses."

The following is a summary of the water supply assessment for this Project:

- The Project will be under environmental review pursuant to the requirements of CEQA; therefore, the information contained in this assessment will be used to support the analysis contained in the CEQA document.
- The Project does not meet the definition of a "Project" under Water Code Section 10912(a).
- A 1281.51-acre portion of the Kudu Project is located within California City and may be served by the California
  City Water Department. The 673.55-acre portion of the Kudu Project located in unincorporated Kern County will
  not be served by a public water system. California City prepared a UWMP 2015 Update (California City, 2017)
  that did not account for the Project water demand.
- Proposed water demand for the portion of the Kudu Project located within California City will be met by California City water supplies, but the portion of the Kudu Project located in unincorporated Kern County would be met by local groundwater pumping in an amount that is not considered a *de minimis* extraction under Section 10721 of the Water Code. The groundwater supply would be extracted from the FVGB. No Groundwater Sustainability Agency has been formed to serve this basin, and management of this basin is assumed by Kern County. A FVGMP has been prepared by California City, MPUD and AVEK (Woodard & Curran, 2018a) that is intended to serve as a pre-GSP document in the event the FVGB is required to prepare a GSP. The AVGBto the south is adjudicated, but the FVGB is not.
- The FVGB has been designated as a "low" priority basin by the DWR, and a GSP is not required under the SGMA.
- According to the FVGMP (Woodard & Curran, 2018a), groundwater production in the FVGB in 2020 is estimated to be 7,515 af and projected to be 9,894 af in 2040.
- According to the FVBSNMP (Woodard & Curran, 2018b), groundwater storage in the FVGB was estimated to be 4,800,000 af in 1975, but is currently estimated at 4,070,000 af due to a reduction in storage of about 738,000 af between 1958 and 2017.
- According to the FVSNMP, average groundwater recharge to the FVGB is estimated to be 13,800 afa between 1998 and 2017.

 Average annual groundwater recharge exceeds current and projected (2040) groundwater production in the FVGB.

Based on the large groundwater storage remaining and average annual recharge that exceeds current and projected 2040 groundwater production in the FVGB, there is sufficient water supply available to serve the Kudu Project as proposed. ProjectBased on the Based on the esults of the assessment, sufficient water supply is available to serve the Kudu Project within the unincorporated Kern County portion of the FVGB and California City as proposed, and no further analysis should be required.



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