

DRAINAGE STUDY

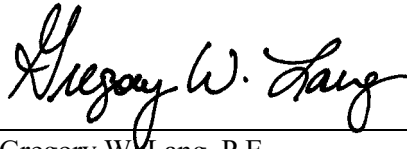
For:

Towne Centre View

PTS#: 624751

APN 343-121-35, 36, 37, 42, 43
9855, 9865, 9875, 9885 Towne Centre Drive
San Diego, CA 92121

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EXP: 06-30-23

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Prepared for:

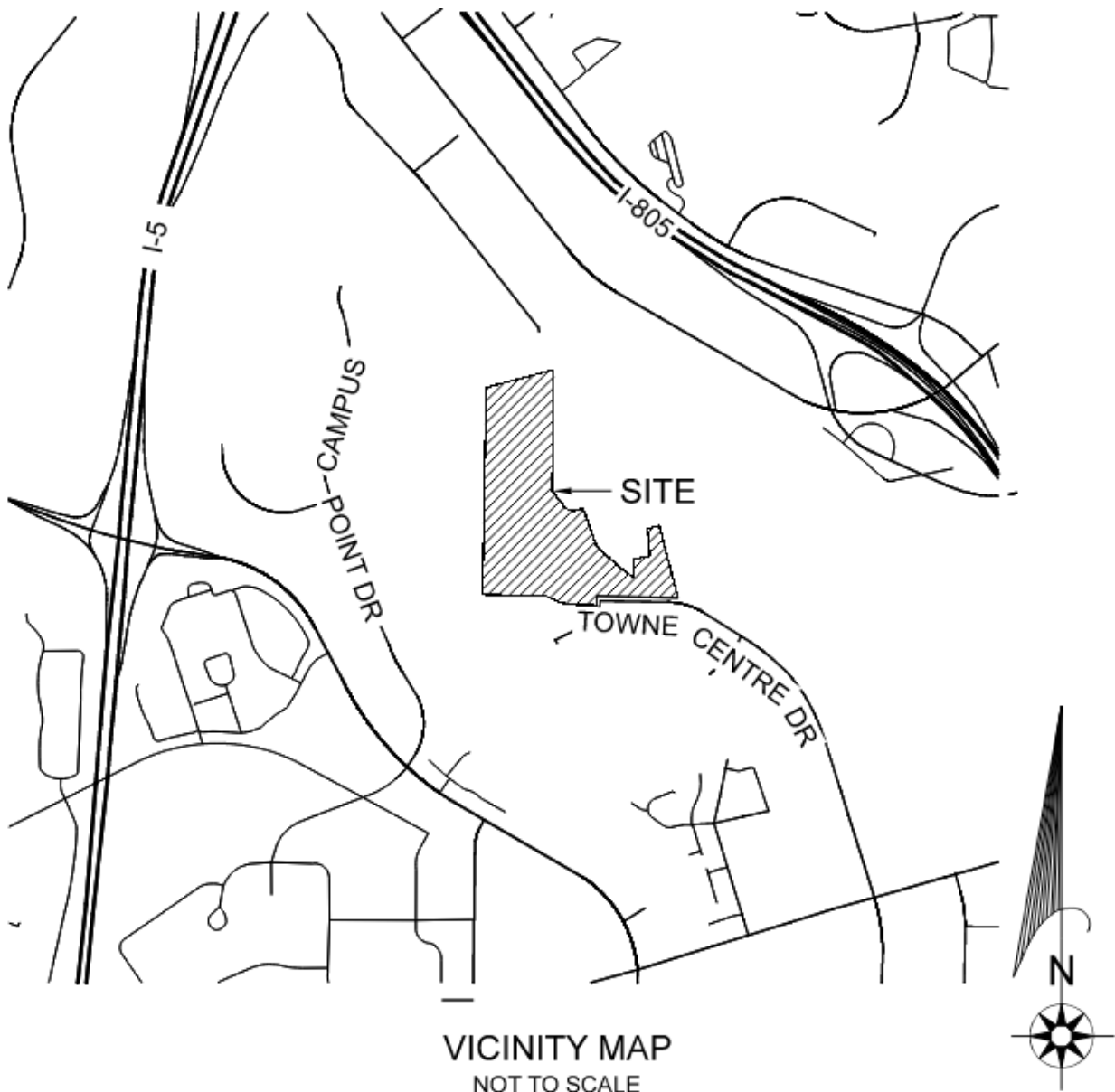
BRE-BMR Towne Centre Science Park LLC
c/o Project Management Advisors, Inc.
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September 2020

Revised December 2021

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VICINITY MAP
NOT TO SCALE

1. INTRODUCTION

1.1 Project Description

The project site is located at the north end of Towne Centre Drive in San Diego, California. The site is located east of the I-5, west of I-805, south of the merge of I-5 and I-805 and north of La Jolla Village Drive.

The Project involves redevelopment of the Project with a five-building campus (Buildings A through E), which would include scientific R&D, laboratories, technology, and office uses, with supporting parking structures and surface parking areas, recreational facilities, amenities, and landscaping. Offsite improvements consist of three driveway entrances and a non-contiguous sidewalk along the project frontage at Towne Centre Drive.

1.2 Existing Conditions

The total property area consists of 33.52 acres. The property is located on a ridge surrounded by steep canyons and Towne Centre Drive to the south. The western portion of the project site is currently rough graded for a previous project, Summit Point Plaza, PTS#6109. Full build out of Summit Point Plaza was not completed and the project ended to include only rough grading of the site and drainage infrastructure. The eastern portion of the site consists of an existing office complex.

In the existing condition the western portion of the site, per approved Summit Point Plaza plans PTS#6109, is rough graded with building pad sites, retaining walls, large sedimentation basins and drainage infrastructure. Refer to Appendix 4 for the approved Summit Point Plaza grading plans. Drainage infrastructure was installed for each of the five drainage areas of the previously approved project. For the locations of the existing drainage basins and discharge points refer to the Existing Conditions Hydrology Exhibit located in Appendix 1. Drainage areas were listed as areas A1, B1, B3, C1 and C3. The existing drainage infrastructure includes sedimentation basins, outlet structures from the sedimentation basins including perforated riser pipes or stand pipes, brow ditch conveyance channels and level spreaders to dissipate concentrated flow and minimize the erosion potential at discharge locations.

The hydrology report associated with the approved grading plans was requested from the City of San Diego and previous engineer, however, the report is not available. The approved plans have a table of previously approved hydrology characteristics for the five drainage basins, including 100-year flow rates. Table 1 below summarizes the hydrologic information of the previously approved plans.

Control Point	Basin	Area (ac)	Q100 (cfs)
1	(A1)	2.80	12.10
2	(B1)	1.95	10.10
3	(B3)	1.04	5.40
4	(C1)	1.21	6.30
5	(C3)	2.51	12.60

The eastern portion of the site is developed and consists of office buildings, parking areas and landscape. Hydrologic calculations were performed for the eastern portion of the site. Refer to Appendix 2 for the calculations. Table 2 below summarizes the hydrologic calculations for the eastern portion of the site.

Table 2 - EXISTING CONDITION HYDROLOGY SUMMARY (EAST)			
Control Point	Basin	Area (ac)	Q100 (cfs)
1	(A2)	1.16	3.54
6	(D2)	6.75	19.72
7	(D1)	1.29	4.60

1.3 Proposed Conditions

The proposed project consists of the construction of new science, research and development, laboratory, technology and office buildings, including an underground parking garage, an above ground parking garage, a surface parking area, drive aisles, sports fields, and landscaped areas. Offsite improvements consist of three driveway entrances and a non-contiguous sidewalk along the project frontage at Towne Centre Drive.

In the proposed condition, the site consists of 7 drainage basins:

Drainage Basin 1 is located in the southwest portion of the site and includes DMA A1, A2 and A3. Storm water runoff in DMA A1 and A2 will be collected in proposed storm drain and conveyed to underground storage vaults and subsequent Modular Wetland Systems. Runoff from impervious areas in DMA A3 will be directed to landscape areas for dispersion.

Drainage Basin 2 is located along the western boundary of the site and includes DMA B1. Storm water runoff from impervious areas in DMA B1 will be directed to landscape areas for dispersion.

Drainage Basin 3 is located along the western boundary of the site and includes DMA B2. Storm water runoff from impervious areas in DMA B2 will be directed to landscape areas for dispersion.

Drainage Basin 4 is located in the northwest corner of the site and includes DMA C1. Storm water runoff from impervious areas in DMA C1 will be directed to landscape areas for dispersion.

Drainage Basin 5 is located in the northwest portion of the site and includes DMA C2. Storm water runoff in DMA C2 will be collected in proposed storm drain and conveyed to an underground storage vault and subsequent biofiltration basin.

Drainage Basin 6 is located in the central portion of the site and includes DMA D1 and D2. Storm water runoff in DMA D1 will be collected in proposed storm drain and conveyed to an underground storage vault and subsequent Modular Wetland System. Runoff in DMA D2 will be collected in proposed storm drain and conveyed to an underground storage vault and subsequent biofiltration basin.

Drainage Basin 7 is located in the eastern portion of the site and includes DMA D3 and D4. Storm water runoff from impervious areas in DMA D3 will be directed to landscape areas for dispersion. Storm water runoff in DMA D4 will be collected in proposed storm drain and conveyed to underground storage vaults and subsequent Modular Wetland Systems.

The proposed underground storage vaults provide mitigation of the 100-year storm event peak discharge. For the locations of the proposed drainage basins and discharge points refer to the Proposed Condition Hydrology Exhibit located in Appendix 1.

The table below provides a summary of the hydrologic information for the proposed conditions.

Table 3 – PROPOSED CONDITION HYDROLOGY SUMMARY			
Control Point	Basin	Area (ac)	Q100 (cfs)
1	A1	2.42	7.99
	A2	1.35	3.16
	A3	1.88	4.30
2	B1	0.85	1.87
3	B2	0.59	1.30
4	C1	1.31	2.88
5	C2	4.13	9.99
6	D1	3.38	7.58
	D2	3.40	9.42
7	D3	0.51	1.12
	D4a	1.14	2.86
	D4b	0.45	1.35

2. METHODOLOGY

Pursuant to the 2017 City of San Diego Drainage Design Manual, the Rational Method is recommended for analyzing the runoff response from drainage areas less than 0.5 square mile, therefore the Rational Method was used to analyze this project’s hydrologic characteristics.

2.1 Rational Method

Runoff was calculated for the 100-year, 6-hour storm event using the Rational Method which is calculated using the following equation:

$$Q = C \times I \times A \qquad \text{Equation A-1 of 2017 City of SD Drainage Design Manual}$$

Where:

- Q = Flow rate in cubic feet per second (cfs)
- C = Runoff coefficient (Table A-1 of City of SD Drainage Design Manual)
- I = Rainfall Intensity in inches per hour (in/hr)
- A = Drainage basin area in acres (ac)

2.2 Runoff Coefficient

The runoff coefficients for the project are based on Table A-1 and Footnote 2 from the 2017 City of San Diego Drainage Design Manual.

2.3 Rainfall Intensity

Rainfall intensity was determined using the Rainfall Intensity-Duration-Frequency Curves shown in Section A.1.3 of the 2017 City of San Diego Drainage Design Manual. Based on Figure A-1 and a 5-minute time of concentration, the 100-year intensity is 4.4 inches per hour.

2.4 Detention

The underground storage vaults provide mitigation of the 100-year storm event peak flow rate. The 100-year storm event detention analysis was performed using HydroCAD Stormwater Modeling software. The inflow runoff hydrographs to the vaults were modeled using RatHydro which is a Rational Method Design Storm Hydrograph software that creates a hydrograph using the results of the Rational Method calculations. HydroCAD has the ability to route the 100-year 6-hour storm event inflow hydrograph through the facilities considering dynamic tailwater effects. Based on the facility cross sectional geometry, stage storage and outlet structure data, HydroCAD calculates the detained peak flow rate and detained time to peak. Refer to the plans for details of each facility.

Based on the results of the HydroCAD analysis, mitigation for the 100-year storm event peak flow rate is provided, detaining the peak flow rate in the proposed condition to below the existing condition. Refer to Appendix 3 for the HydroCAD detention detailed output.

2.5 Section 401/404 Water Quality Certification

This project does not have any waters of the United States (e.g., creek, drainage, wetland) on the property and does not require Federal permitting or approval.

3. CALCULATIONS/RESULTS

3.1 Existing and Proposed Peak Flow Comparison

The table below summarizes the 100-year 6-hour peak flow rate calculations for the project.

SUMMARY OF 100-YR STORM EVENT HYDROLOGIC ANALYSIS							
Control Point	Existing Condition			Proposed Condition			Proposed Detained Condition
	Basin	Area (ac)	Q100 (cfs)	Basin	Area (ac)	Q100 (cfs)	Q100 (cfs)
1	A1	2.80	12.10	A1	2.42	7.99	6.19
				A2	1.35	3.16	3.06
	A2	1.16	3.54	A3	1.88	4.30	4.30
2	B1	1.95	10.10	B1	0.85	1.87	1.87
3	B3	1.04	5.40	B2	0.59	1.30	1.30
4	C1	1.21	6.30	C1	1.31	2.88	2.88
5	C3	2.51	12.60	C2	4.13	9.99	0.77
6	D2	6.75	19.72	D1	3.38	7.58	3.64
				D2	3.40	9.42	8.81
7	D1	1.29	4.60	D3	0.51	1.12	1.12
				D4a	1.14	2.86	0.26
				D4b	0.45	1.35	0.10

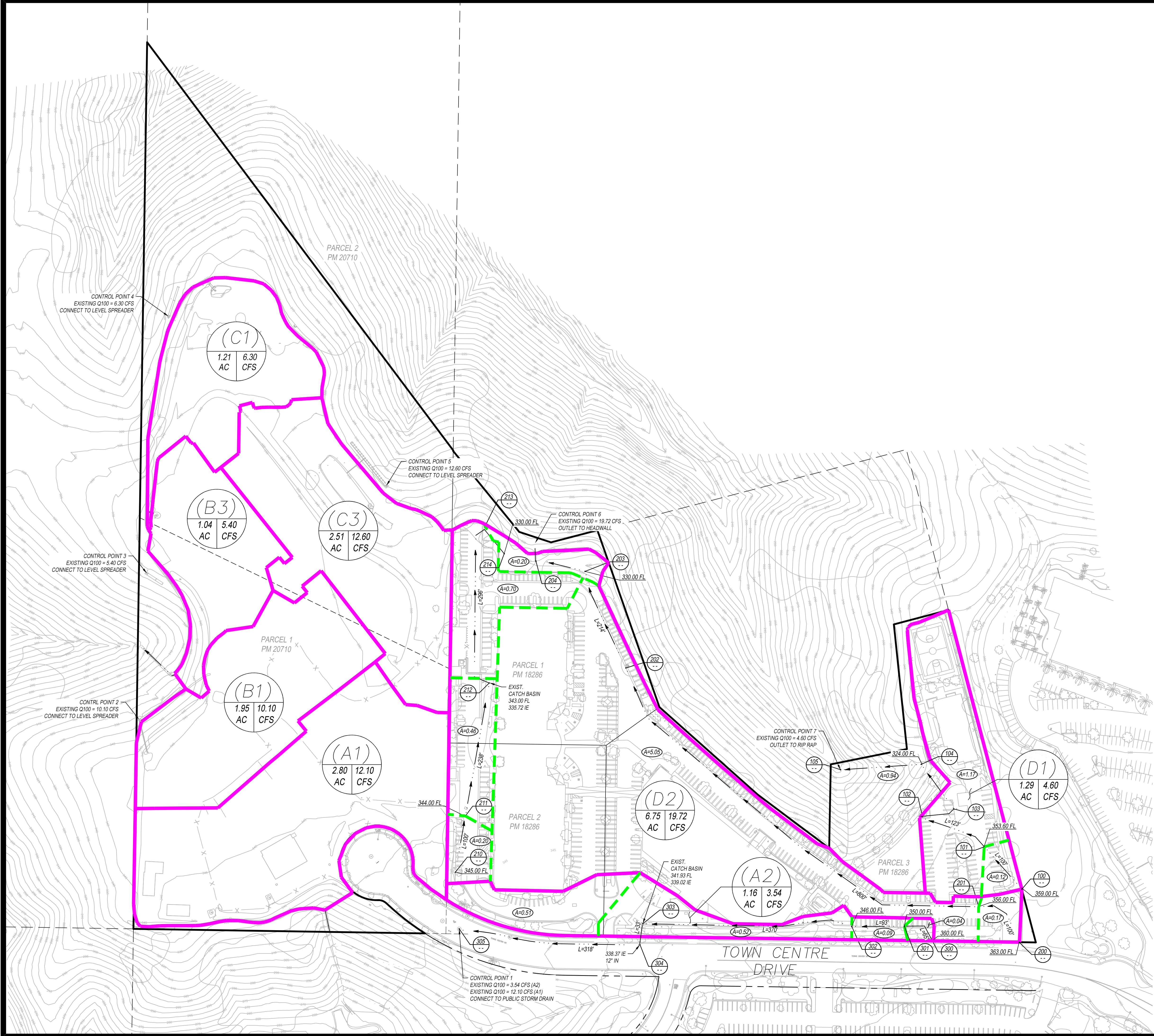
In the proposed detained condition, the 100-year storm event peak discharge rates are lower than the existing flow rates. The project will not have adverse impacts to downstream drainage facilities.

4. CONCLUSION

The proposed project was designed to honor previously approved drainage infrastructure and flow rates and minimize the effects of the development to downstream drainage facilities. Storm water runoff rates will be decreased from existing conditions.

Appendix 1

Existing and Proposed Hydrology Exhibits



LEGEND

DESCRIPTION	SYMBOL
RIGHT-OF-WAY	--- ---
PROPERTY LINE	— — — —
BASIN BOUNDARY	— — — —
BASIN SUBAREA	— — — —

BASIN SUMMARY Q100 EXISTING (PRE MITIGATION)

(XX)	(XX)
X.XX AC	X.XX CFS

HYDROLOGIC SOIL GROUP

HYDROLOGIC SOIL TYPE: C & D*
 *FOR THE PURPOSE OF DRAINAGE CALCS, THE ENTIRE SITE WILL BE MODELED WITH TYPE D SOILS

DEPTH TO GROUNDWATER

DEPTH TO GROUNDWATER > 20 FT

PROJECT CHARACTERISTICS

PARCEL AREA: 25.45 AC
 EXISTING IMPERVIOUS AREA: 8.12 AC
 EXISTING LANDSCAPE AREA: 12.83 AC

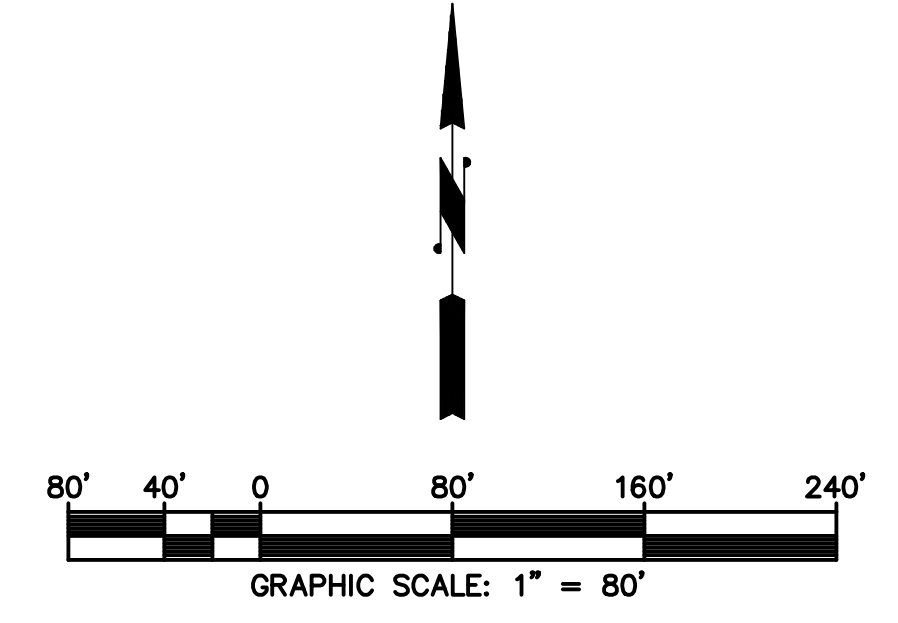
SUMMARY OF EXISTING CONDITIONS (WEST)

EXIST. DRAINAGE BASIN	EXIST. DRAINAGE AREA (AC)*	RUNOFF COEFFICIENT, C*	Q100 (CFS)*
(A1)	2.80	0.85	12.10
(B1)	1.95	0.85	10.10
(B3)	1.04	0.85	5.40
(C1)	1.21	0.85	6.30
(C3)	2.51	0.85	12.60

*TABULATED VALUES FROM SUMMIT POINT PLAZA GRADING PLANS, PTS#6109, 32375-6-D, DETENTION FACILITIES AND DETAILS

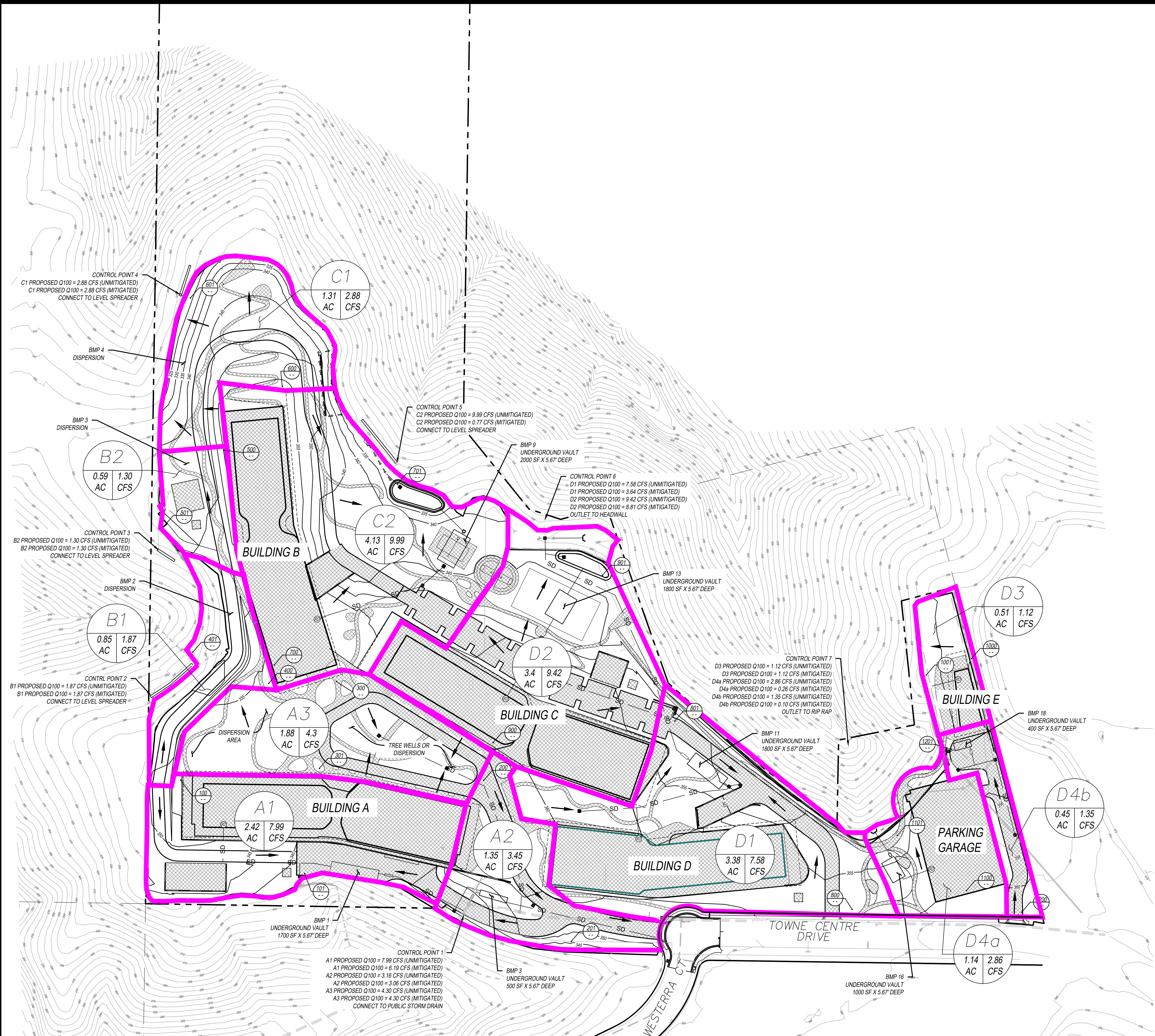
SUMMARY OF EXISTING CONDITIONS (EAST)

EXIST. DRAINAGE BASIN	EXIST. DRAINAGE AREA (AC)	RUNOFF COEFFICIENT, C	Q100 (CFS)
(A2)	1.16	0.85	3.54
(D1)	1.29	0.85	4.60
(D2)	6.75	0.85	19.72



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 Phone 858.259.8212 | www.pisaengineering.com

EXISTING CONDITION DRAINAGE EXHIBIT
 TOWNE CENTRE VIEW
 TOWN CENTRE DRIVE
 SAN DIEGO, CA 92121
 PLSA JOB # 3342
 SCALE 1"=80'
 OCTOBER 2020
 SHEET 1 OF 1



LEGEND

DESCRIPTION	SYMBOL				
RIGHT-OF-WAY	--- ---				
PROPERTY LINE	---				
BASIN BOUNDARY	—				
PROPOSED IMPERVIOUS AREA	▨				
DRAINAGE ARROW	→				
BASIN SUMMARY Q100 PROPOSED (PRE MITIGATION)	<table border="1"> <tr> <td>XX</td> <td>XX</td> </tr> <tr> <td>AC</td> <td>CFS</td> </tr> </table>	XX	XX	AC	CFS
XX	XX				
AC	CFS				

HYDROLOGIC SOIL GROUP
 HYDROLOGIC SOIL TYPE: C & D*
 *FOR THE PURPOSE OF DRAINAGE CALCS, THE ENTIRE SITE WILL BE MODELED WITH TYPE D SOILS

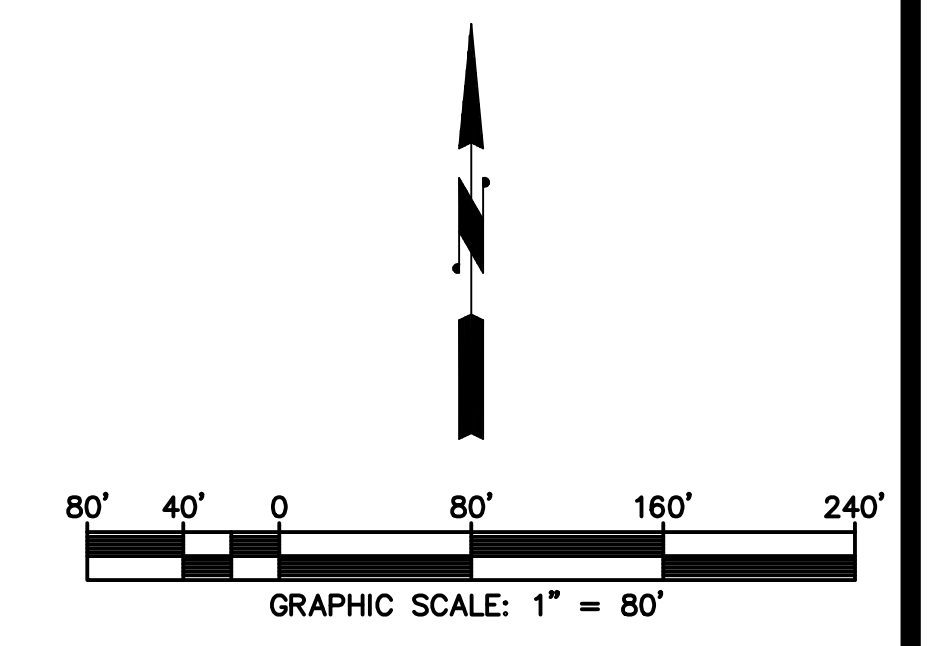
DEPTH TO GROUNDWATER
 DEPTH TO GROUNDWATER > 20 FT

PROJECT CHARACTERISTICS

TOTAL SITE AREA:	33.52 AC
PROPOSED DISTURBED AREA:	20.64 AC
PROPOSED IMPERVIOUS AREA:	10.62 AC
PROPOSED LANDSCAPE AREA:	10.02 AC

SUMMARY OF PROPOSED CONDITIONS

PROP. DRAINAGE BASIN	PROP. DRAINAGE AREA (AC)	Q100 (CFS)	Q100 DETAINED (CFS)
A1	2.42	7.99	6.19
A2	1.35	3.45	3.34
A3	1.88	4.30	4.30
B1	0.85	1.87	1.87
B2	0.59	1.30	1.30
C1	1.31	2.88	2.88
C2	4.13	9.99	0.77
D1	3.38	7.58	3.64
D2	3.40	9.42	8.81
D3	0.51	1.12	1.12
D4a	1.14	2.86	0.26
D4b	0.45	1.35	0.10



PROPOSED CONDITION DRAINAGE EXHIBIT
 TOWNE CENTRE VIEW
 TOWNE CENTRE DRIVE
 SAN DIEGO, CA 92121
 PLSA JOB # 3342
 SCALE 1"=80'
 JULY, 2022
 SHEET 1 OF 1

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Appendix 2
Hydrology Support Material and Calculations



Table A-1. Runoff Coefficients for Rational Method

Land Use	Runoff Coefficient (C)
	Soil Type ⁽¹⁾
Residential:	
Single Family	0.55
Multi-Units	0.70
Mobile Homes	0.65
Rural (lots greater than 1/2 acre)	0.45
Commercial ⁽²⁾	
80% Impervious	0.85
Industrial ⁽²⁾	
90% Impervious	0.95

Note:

⁽¹⁾ Type D soil to be used for all areas.

⁽²⁾ Where actual conditions deviate significantly from the tabulated imperviousness values of 80% or 90%, the values given for coefficient C, may be revised by multiplying 80% or 90% by the ratio of actual imperviousness to the tabulated imperviousness. However, in case shall the final coefficient be less than 0.50. For example: Consider commercial property on D soil.

$$\begin{aligned}
 \text{Actual imperviousness} &= 50\% \\
 \text{Tabulated imperviousness} &= 80\% \\
 \text{Revised C} &= (50/80) \times 0.85 = 0.53
 \end{aligned}$$

The values in Table A-1 are typical for urban areas. However, if the basin contains rural or agricultural land use, parks, golf courses, or other types of nonurban land use that are expected to be permanent, the appropriate value should be selected based upon the soil and cover and approved by the City.

A.1.3. Rainfall Intensity

The rainfall intensity (I) is the rainfall in inches per hour (in/hr.) for a duration equal to the T_c for a selected storm frequency. Once a particular storm frequency has been selected for design and a T_c calculated for the drainage area, the rainfall intensity can be determined from the Intensity-Duration-Frequency Design Chart (Figure A-1).



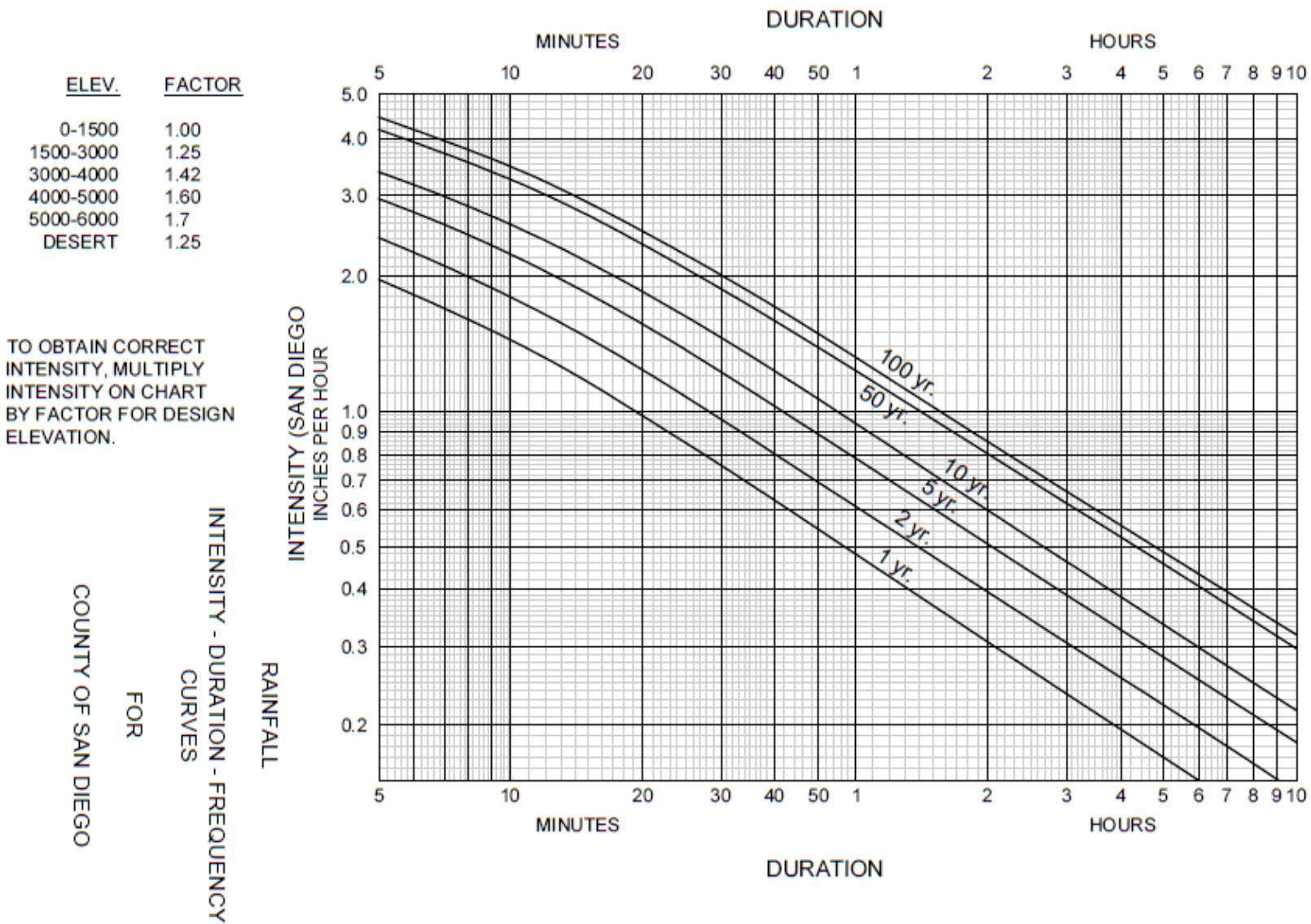


Figure A-1. Intensity-Duration-Frequency Design Chart



RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1452

Analysis prepared by:

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***** DESCRIPTION OF STUDY *****
* 3342 TOWNE CENTRE VIEW *
* EASTERN SITE EXISTING CONDITION *
* 100-YR *

FILE NAME: 3342E100.DAT
TIME/DATE OF STUDY: 17:12 09/17/2020

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

USER SPECIFIED STORM EVENT (YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 4.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
RAINFALL-INTENSITY ADJUSTMENT FACTOR = 1.000

*USER SPECIFIED:

NUMBER OF [TIME,INTENSITY] DATA PAIRS = 9

- 1) 5.000; 4.400
- 2) 10.000; 3.450
- 3) 15.000; 2.900
- 4) 20.000; 2.500
- 5) 25.000; 2.200
- 6) 30.000; 2.000
- 7) 40.000; 1.700
- 8) 50.000; 1.500
- 9) 60.000; 1.300

SPECIFIED CONSTANT RUNOFF COEFFICIENT = 0.850

NOTE: ONLY PEAK CONFLUENCE VALUES CONSIDERED

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	WIDTH (FT)	CROSSFALL (FT)	IN- / SIDE (FT)	OUT- / SIDE (FT)	PARK- / WAY (FT)	HEIGHT (FT)	WIDTH (FT)	LIP (FT)	HKE (FT)	FACTOR (n)
1	30.0	20.0	0.018	0.018	0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

- 1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 - 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

*USER SPECIFIED(GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500

S.C.S. CURVE NUMBER (AMC II) = 72
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 0.45
TOTAL AREA (ACRES) = 0.12 TOTAL RUNOFF (CFS) = 0.45

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 353.60 DOWNSTREAM (FEET) = 347.00
CHANNEL LENGTH THRU SUBAREA (FEET) = 123.00 CHANNEL SLOPE = 0.0537
CHANNEL BASE (FEET) = 50.00 "Z" FACTOR = 50.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH (FEET) = 1.00
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.197
*USER SPECIFIED (GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 2.54
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 1.92
AVERAGE FLOW DEPTH (FEET) = 0.03 TRAVEL TIME (MIN.) = 1.07
Tc (MIN.) = 6.07
SUBAREA AREA (ACRES) = 1.17 SUBAREA RUNOFF (CFS) = 4.17
AREA-AVERAGE RUNOFF COEFFICIENT = 0.850
TOTAL AREA (ACRES) = 1.3 PEAK FLOW RATE (CFS) = 4.60

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH (FEET) = 0.04 FLOW VELOCITY (FEET/SEC.) = 2.52
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 393.00 FEET.

FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 339.66 DOWNSTREAM (FEET) = 338.41
FLOW LENGTH (FEET) = 60.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 9.3 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 7.06
GIVEN PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 4.60
PIPE TRAVEL TIME (MIN.) = 0.14 Tc (MIN.) = 6.21
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 453.00 FEET.

FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 338.11 DOWNSTREAM (FEET) = 324.00
FLOW LENGTH (FEET) = 95.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 3.8 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 14.15
GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 4.60
PIPE TRAVEL TIME (MIN.) = 0.11 Tc (MIN.) = 6.32
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 548.00 FEET.

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 22

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
USER SPECIFIED Tc(MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF(CFS) = 0.64
TOTAL AREA(ACRES) = 0.17 TOTAL RUNOFF(CFS) = 0.64
*****
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 356.00 DOWNSTREAM( FEET) = 340.86
CHANNEL LENGTH THRU SUBAREA( FEET) = 800.00 CHANNEL SLOPE = 0.0189
CHANNEL BASE( FEET) = 10.00 "Z" FACTOR = 50.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH( FEET) = 1.00
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 3.564
*USER SPECIFIED(GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.37
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) = 3.03
AVERAGE FLOW DEPTH( FEET) = 0.16 TRAVEL TIME( MIN.) = 4.40
Tc( MIN.) = 9.40
SUBAREA AREA( ACRES) = 5.05 SUBAREA RUNOFF( CFS) = 15.30
AREA-AVERAGE RUNOFF COEFFICIENT = 0.850
TOTAL AREA( ACRES) = 5.2 PEAK FLOW RATE( CFS) = 15.81

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH( FEET) = 0.21 FLOW VELOCITY( FEET/SEC.) = 3.65
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 895.00 FEET.
*****
FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 331.83 DOWNSTREAM( FEET) = 330.00
FLOW LENGTH( FEET) = 214.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES
PIPE-FLOW VELOCITY( FEET/SEC.) = 7.01
GIVEN PIPE DIAMETER( INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW( CFS) = 15.81
PIPE TRAVEL TIME( MIN.) = 0.51 Tc( MIN.) = 9.91
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 203.00 = 1109.00 FEET.
*****
FLOW PROCESS FROM NODE 203.00 TO NODE 204.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 3.467
*USER SPECIFIED(GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8500
SUBAREA AREA( ACRES) = 0.20 SUBAREA RUNOFF( CFS) = 0.59
TOTAL AREA( ACRES) = 5.4 TOTAL RUNOFF( CFS) = 15.97
TC( MIN.) = 9.91

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*****
FLOW PROCESS FROM NODE 204.00 TO NODE 204.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====
*****
FLOW PROCESS FROM NODE 210.00 TO NODE 211.00 IS CODE = 22
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
USER SPECIFIED Tc(MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF(CFS) = 0.75
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.75
*****
FLOW PROCESS FROM NODE 211.00 TO NODE 212.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 344.00 DOWNSTREAM( FEET) = 343.00
CHANNEL LENGTH THRU SUBAREA( FEET) = 238.00 CHANNEL SLOPE = 0.0042
CHANNEL BASE( FEET) = 10.00 "Z" FACTOR = 50.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH( FEET) = 1.00
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 3.691
*USER SPECIFIED(GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.48
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) = 1.06
AVERAGE FLOW DEPTH( FEET) = 0.09 TRAVEL TIME( MIN.) = 3.73
Tc( MIN.) = 8.73
SUBAREA AREA( ACRES) = 0.46 SUBAREA RUNOFF( CFS) = 1.44
AREA-AVERAGE RUNOFF COEFFICIENT = 0.850
TOTAL AREA( ACRES) = 0.7 PEAK FLOW RATE( CFS) = 2.07

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH( FEET) = 0.11 FLOW VELOCITY( FEET/SEC.) = 1.22
LONGEST FLOWPATH FROM NODE 210.00 TO NODE 212.00 = 452.00 FEET.
*****
FLOW PROCESS FROM NODE 212.00 TO NODE 213.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 335.72 DOWNSTREAM( FEET) = 332.60
FLOW LENGTH( FEET) = 296.00 MANNING'S N = 0.013
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY( FEET/SEC.) = 3.07
(Pipe flow velocity corresponding to normal-depth flow
at depth = 0.94 * diameter)
GIVEN PIPE DIAMETER( INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW( CFS) = 2.07
PIPE TRAVEL TIME( MIN.) = 1.61 Tc( MIN.) = 10.34
LONGEST FLOWPATH FROM NODE 210.00 TO NODE 213.00 = 748.00 FEET.
*****
FLOW PROCESS FROM NODE 213.00 TO NODE 213.00 IS CODE = 81
-----

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```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 3.413
*USER SPECIFIED(GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8500
SUBAREA AREA (ACRES) = 0.70 SUBAREA RUNOFF (CFS) = 2.03
TOTAL AREA (ACRES) = 1.4 TOTAL RUNOFF (CFS) = 3.94
TC (MIN.) = 10.34
*****
FLOW PROCESS FROM NODE 213.00 TO NODE 214.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 332.60 DOWNSTREAM(FEET) = 330.00
FLOW LENGTH(FEET) = 55.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 6.3 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 9.52
GIVEN PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 3.94
PIPE TRAVEL TIME (MIN.) = 0.10 Tc (MIN.) = 10.44
LONGEST FLOWPATH FROM NODE 210.00 TO NODE 214.00 = 803.00 FEET.
*****
FLOW PROCESS FROM NODE 214.00 TO NODE 204.00 IS CODE = 11
-----
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<
=====
** MAIN STREAM CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 3.94 10.44 3.402 1.36
LONGEST FLOWPATH FROM NODE 210.00 TO NODE 204.00 = 803.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 15.97 9.91 3.467 5.42
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 204.00 = 1109.00 FEET.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 19.72 9.91 3.467
2 19.62 10.44 3.402

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE (CFS) = 19.72 Tc (MIN.) = 9.91
TOTAL AREA (ACRES) = 6.8
*****
FLOW PROCESS FROM NODE 204.00 TO NODE 205.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 328.50 DOWNSTREAM(FEET) = 328.00
FLOW LENGTH(FEET) = 26.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 14.3 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 10.13
GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1

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PIPE-FLOW (CFS) = 19.72
PIPE TRAVEL TIME (MIN.) = 0.04 Tc (MIN.) = 9.95
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 205.00 = 1135.00 FEET.
*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 22
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 0.15
TOTAL AREA (ACRES) = 0.04 TOTAL RUNOFF (CFS) = 0.15
*****
FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVEL TIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 350.00 DOWNSTREAM(FEET) = 346.00
CHANNEL LENGTH THRU SUBAREA (FEET) = 93.00 CHANNEL SLOPE = 0.0430
CHANNEL BASE (FEET) = 10.00 "Z" FACTOR = 50.000
MANNING'S FACTOR = 0.015 MAXIMUM DEPTH (FEET) = 1.00
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.191
*USER SPECIFIED(GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 0.31
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 1.41
AVERAGE FLOW DEPTH (FEET) = 0.02 TRAVEL TIME (MIN.) = 1.10
Tc (MIN.) = 6.10
SUBAREA AREA (ACRES) = 0.09 SUBAREA RUNOFF (CFS) = 0.32
AREA-AVERAGE RUNOFF COEFFICIENT = 0.850
TOTAL AREA (ACRES) = 0.1 PEAK FLOW RATE (CFS) = 0.46

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH (FEET) = 0.03 FLOW VELOCITY (FEET/SEC.) = 1.59
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 119.00 FEET.
*****
FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 342.00 DOWNSTREAM(FEET) = 339.02
FLOW LENGTH(FEET) = 370.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 6.0 INCH PIPE IS 4.7 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 2.78
GIVEN PIPE DIAMETER (INCH) = 6.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 0.46
PIPE TRAVEL TIME (MIN.) = 2.22 Tc (MIN.) = 8.32
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 489.00 FEET.
*****
FLOW PROCESS FROM NODE 303.00 TO NODE 303.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 3.769
*USER SPECIFIED(GLOBAL):

```

NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
 S.C.S. CURVE NUMBER (AMC II) = 72
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.8500
 SUBAREA AREA (ACRES) = 0.52 SUBAREA RUNOFF (CFS) = 1.67
 TOTAL AREA (ACRES) = 0.6 TOTAL RUNOFF (CFS) = 2.08
 TC (MIN.) = 8.32

```
*****
FLOW PROCESS FROM NODE 303.00 TO NODE 304.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM (FEET) = 339.02 DOWNSTREAM (FEET) = 338.37
FLOW LENGTH (FEET) = 33.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 5.6 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 5.83
GIVEN PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 2.08
PIPE TRAVEL TIME (MIN.) = 0.09 Tc (MIN.) = 8.42
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 304.00 = 522.00 FEET.
*****
FLOW PROCESS FROM NODE 304.00 TO NODE 305.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM (FEET) = 338.37 DOWNSTREAM (FEET) = 326.10
FLOW LENGTH (FEET) = 318.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 42.0 INCH PIPE IS 3.1 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 6.45
GIVEN PIPE DIAMETER (INCH) = 42.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 2.08
PIPE TRAVEL TIME (MIN.) = 0.82 Tc (MIN.) = 9.24
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 305.00 = 840.00 FEET.
*****
FLOW PROCESS FROM NODE 305.00 TO NODE 305.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 3.595
*USER SPECIFIED (GLOBAL):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .8500
S.C.S. CURVE NUMBER (AMC II) = 72
AREA-AVERAGE RUNOFF COEFFICIENT = 0.8500
SUBAREA AREA (ACRES) = 0.51 SUBAREA RUNOFF (CFS) = 1.56
TOTAL AREA (ACRES) = 1.2 TOTAL RUNOFF (CFS) = 3.54
TC (MIN.) = 9.24
=====
END OF STUDY SUMMARY:
TOTAL AREA (ACRES) = 1.2 TC (MIN.) = 9.24
PEAK FLOW RATE (CFS) = 3.54
=====
END OF RATIONAL METHOD ANALYSIS
```

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT
2003,1985,1981 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1452

Analysis prepared by:

PASCO LARET SUITER & ASSOCIATES
535 NORTH HIGHWAY 101, STE A
SOLANA BEACH, CA 92075
858-259-8212

***** DESCRIPTION OF STUDY *****
* 3342 TOWNE CENTRE VIEW *
* PROPOSED CONDITION *
* 100-YR *

FILE NAME: 3342P00.DAT
TIME/DATE OF STUDY: 11:19 07/09/2021

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

USER SPECIFIED STORM EVENT (YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 4.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
RAINFALL-INTENSITY ADJUSTMENT FACTOR = 1.000

*USER SPECIFIED:
NUMBER OF [TIME,INTENSITY] DATA PAIRS = 9

- 1) 5.000; 4.400
- 2) 10.000; 3.450
- 3) 15.000; 2.900
- 4) 20.000; 2.500
- 5) 25.000; 2.200
- 6) 30.000; 2.000
- 7) 40.000; 1.700
- 8) 50.000; 1.500
- 9) 60.000; 1.300

SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD
NOTE: ONLY PEAK CONFLUENCE VALUES CONSIDERED

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	WIDTH (FT)	CROSSFALL (FT)	IN- / SIDE	OUT-/PARK- SIDE / WAY	HEIGHT (FT)	WIDTH (FT)	LIP (FT)	HIKE (FT)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020		0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .7500

S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 7.99
TOTAL AREA (ACRES) = 2.42 TOTAL RUNOFF (CFS) = 7.99

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .5800
S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 3.45
TOTAL AREA (ACRES) = 1.35 TOTAL RUNOFF (CFS) = 3.45

FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .5200
S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 4.30
TOTAL AREA (ACRES) = 1.88 TOTAL RUNOFF (CFS) = 4.30

FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .5000
S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 1.87
TOTAL AREA (ACRES) = 0.85 TOTAL RUNOFF (CFS) = 1.87

FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .5000
S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 1.30
TOTAL AREA (ACRES) = 0.59 TOTAL RUNOFF (CFS) = 1.30

FLOW PROCESS FROM NODE 600.00 TO NODE 601.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .5000

S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 2.88
TOTAL AREA (ACRES) = 1.31 TOTAL RUNOFF (CFS) = 2.88

S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 2.86
TOTAL AREA (ACRES) = 1.14 TOTAL RUNOFF (CFS) = 2.86

FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 22

FLOW PROCESS FROM NODE 1200.00 TO NODE 1201.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .5500
S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 9.99
TOTAL AREA (ACRES) = 4.13 TOTAL RUNOFF (CFS) = 9.99

=====

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .6800
S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 1.35
TOTAL AREA (ACRES) = 0.45 TOTAL RUNOFF (CFS) = 1.35

FLOW PROCESS FROM NODE 800.00 TO NODE 801.00 IS CODE = 22

=====

END OF STUDY SUMMARY:
TOTAL AREA (ACRES) = 0.4 TC (MIN.) = 5.00
PEAK FLOW RATE (CFS) = 1.35

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

END OF RATIONAL METHOD ANALYSIS

=====

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .5100
S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 7.58
TOTAL AREA (ACRES) = 3.38 TOTAL RUNOFF (CFS) = 7.58

FLOW PROCESS FROM NODE 900.00 TO NODE 901.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 9.42
TOTAL AREA (ACRES) = 3.40 TOTAL RUNOFF (CFS) = 9.42

FLOW PROCESS FROM NODE 1000.00 TO NODE 1001.00 IS CODE = 22

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .5000
S.C.S. CURVE NUMBER (AMC II) = 0
USER SPECIFIED Tc (MIN.) = 5.000
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.400
SUBAREA RUNOFF (CFS) = 1.12
TOTAL AREA (ACRES) = 0.51 TOTAL RUNOFF (CFS) = 1.12

FLOW PROCESS FROM NODE 1100.00 TO NODE 1101.00 IS CODE = 22

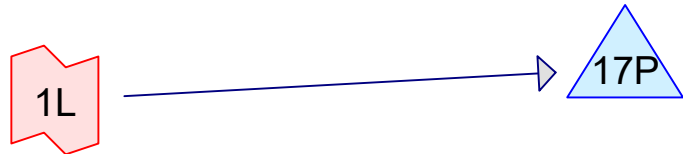
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

*USER SPECIFIED (SUBAREA):
NEIGHBORHOOD COMMERCIAL RUNOFF COEFFICIENT = .5700

Appendix 3

Detention Output



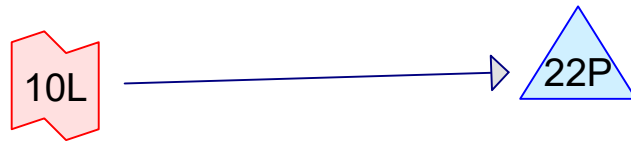
Inflow to VAULT-A1

VAULT-A1



Inflow to VAULT-A2

VAULT-A2



Inflow to VAULT-C2

VAULT-C2



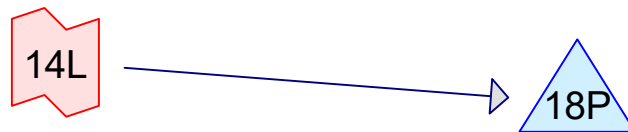
Inflow to VAULT-D1

VAULT-D1



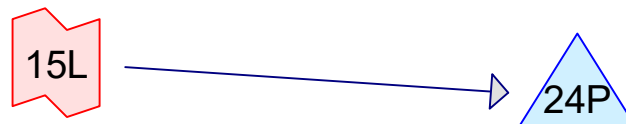
Inflow to VAULT-D2

VAULT-D2



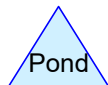
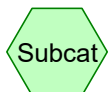
Inflow to VAULT-D4a

VAULT-D4a



Inflow to VAULT-D4b

VAULT-D4b



Routing Diagram for 3342

Prepared by Pasco Laret Suiter & Associates, Printed 9/29/2020
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Summary for Link 1L: Inflow to VAULT-A1

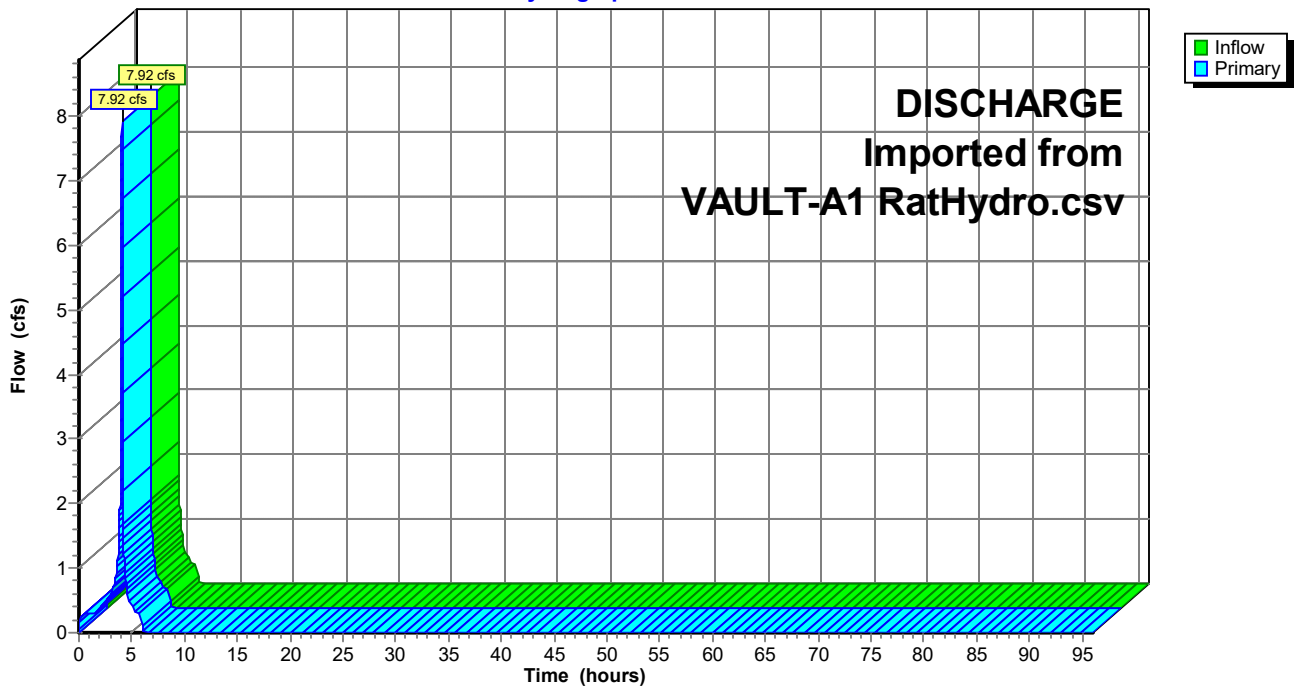
Inflow = 7.92 cfs @ 4.08 hrs, Volume= 0.349 af
Primary = 7.92 cfs @ 4.08 hrs, Volume= 0.349 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

DISCHARGE Imported from VAULT-A1 RatHydro.csv

Link 1L: Inflow to VAULT-A1

Hydrograph



Summary for Pond 17P: VAULT-A1

Inflow = 7.92 cfs @ 4.08 hrs, Volume= 0.349 af
 Outflow = 6.19 cfs @ 4.11 hrs, Volume= 0.349 af, Atten= 22%, Lag= 1.8 min
 Primary = 6.19 cfs @ 4.11 hrs, Volume= 0.349 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs
 Peak Elev= 105.55' @ 4.11 hrs Surf.Area= 1,700 sf Storage= 9,428 cf

Plug-Flow detention time= 539.6 min calculated for 0.349 af (100% of inflow)
 Center-of-Mass det. time= 539.6 min (751.1 - 211.5)

Volume	Invert	Avail.Storage	Storage Description
#1	100.00'	9,639 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
100.00	1,700	0	0	1,700
101.00	1,700	1,700	1,700	1,846
102.00	1,700	1,700	3,400	1,992
103.00	1,700	1,700	5,100	2,138
104.00	1,700	1,700	6,800	2,285
105.17	1,700	1,989	8,789	2,456
105.67	1,700	850	9,639	2,529

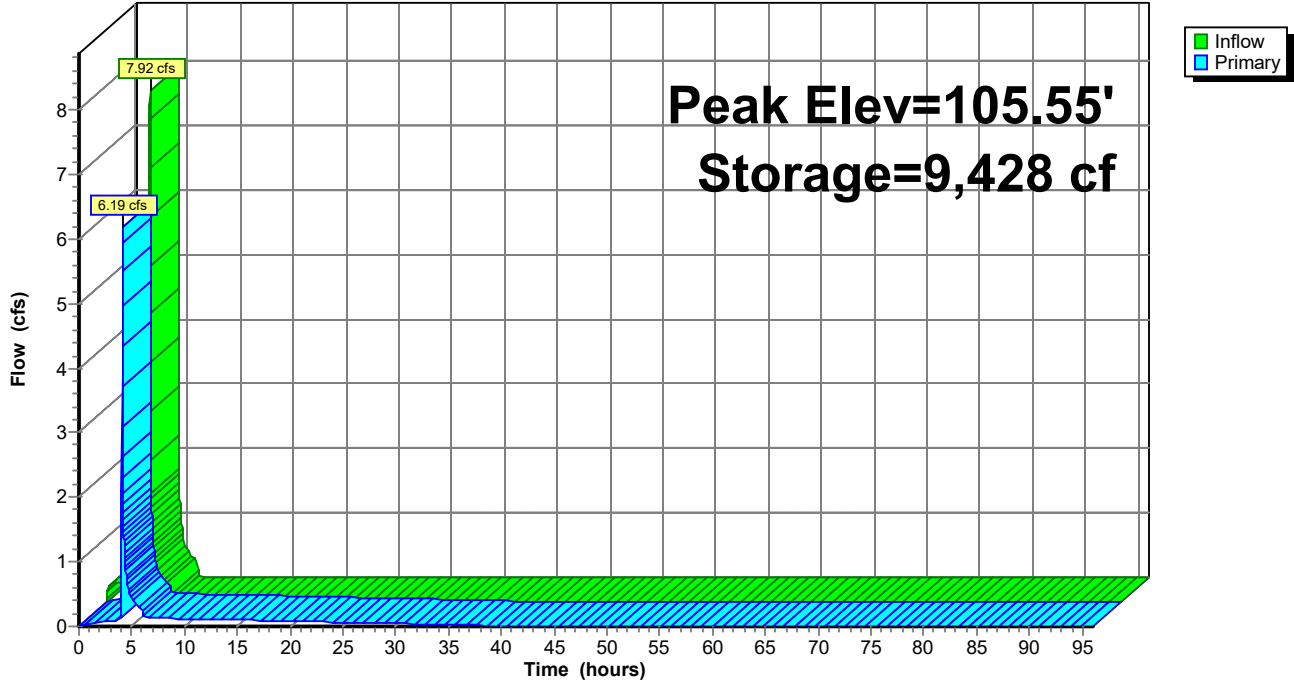
Device	Routing	Invert	Outlet Devices
#1	Primary	100.00'	12.0" Round Culvert L= 10.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 100.00' / 99.90' S= 0.0100 '/ Cc= 0.900 n= 0.013, Flow Area= 0.79 sf
#2	Device 1	100.00'	1.5" Vert. Orifice C= 0.600 Limited to weir flow at low heads
#3	Device 1	105.17'	Custom Weir, Cv= 2.62 (C= 3.28) Head (feet) 0.00 0.50 0.50 Width (feet) 8.00 8.00 0.00

Primary OutFlow Max=6.15 cfs @ 4.11 hrs HW=105.54' (Free Discharge)

- ↑ 1=Culvert (Passes 6.15 cfs of 10.62 cfs potential flow)
- ↑ 2=Orifice (Orifice Controls 0.14 cfs @ 11.27 fps)
- ↑ 3=Custom Weir (Weir Controls 6.02 cfs @ 2.01 fps)

Pond 17P: VAULT-A1

Hydrograph



Summary for Link 4L: Inflow to VAULT-A2

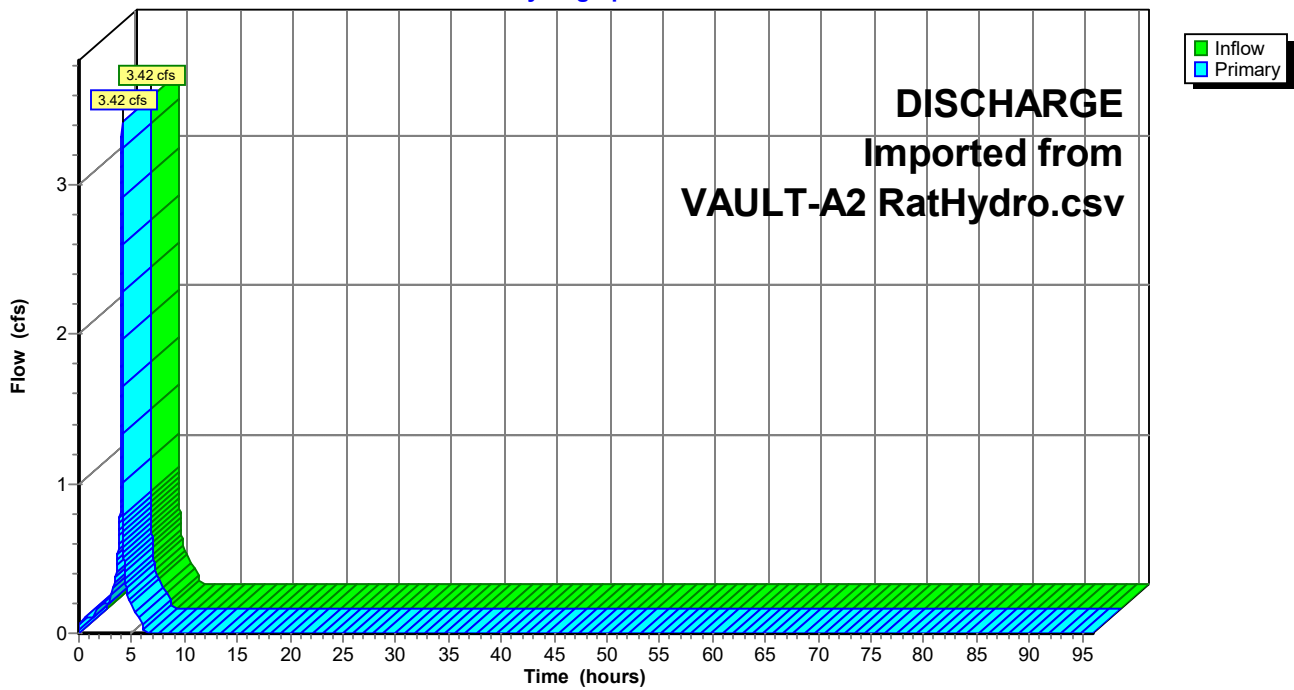
Inflow = 3.42 cfs @ 4.08 hrs, Volume= 0.146 af
Primary = 3.42 cfs @ 4.08 hrs, Volume= 0.146 af, Atten= 0%, Lag= 0.0 min
Routed to Pond 5P : VAULT-A2

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

DISCHARGE Imported from VAULT-A2 RatHydro.csv

Link 4L: Inflow to VAULT-A2

Hydrograph



Summary for Pond 5P: VAULT-A2

Inflow = 3.42 cfs @ 4.08 hrs, Volume= 0.146 af
 Outflow = 3.34 cfs @ 4.08 hrs, Volume= 0.146 af, Atten= 2%, Lag= 0.4 min
 Primary = 3.34 cfs @ 4.08 hrs, Volume= 0.146 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs
 Peak Elev= 105.47' @ 4.08 hrs Surf.Area= 500 sf Storage= 2,737 cf

Plug-Flow detention time= 327.9 min calculated for 0.146 af (100% of inflow)
 Center-of-Mass det. time= 327.7 min (541.6 - 213.8)

Volume	Invert	Avail.Storage	Storage Description
#1	100.00'	2,835 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
100.00	500	0	0	500
101.00	500	500	500	579
102.00	500	500	1,000	659
103.00	500	500	1,500	738
104.00	500	500	2,000	817
105.17	500	585	2,585	910
105.67	500	250	2,835	949

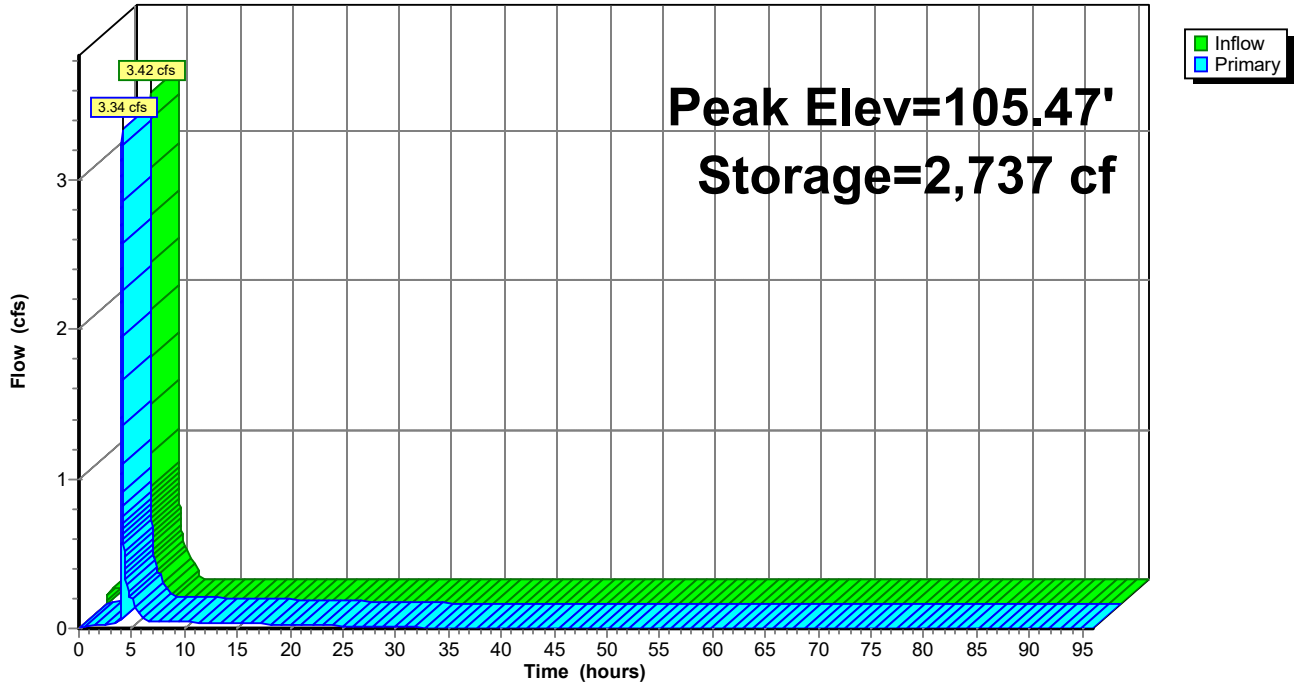
Device	Routing	Invert	Outlet Devices
#1	Primary	100.00'	12.0" Round Culvert L= 10.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 100.00' / 99.90' S= 0.0100 '/ Cc= 0.900 n= 0.013, Flow Area= 0.79 sf
#2	Device 1	100.00'	0.9" Vert. Orifice C= 0.600 Limited to weir flow at low heads
#3	Device 1	105.17'	Custom Weir, Cv= 2.62 (C= 3.28) Head (feet) 0.00 0.50 0.50 Width (feet) 6.00 6.00 0.00

Primary OutFlow Max=3.32 cfs @ 4.08 hrs HW=105.47' (Free Discharge)

- ↑ 1=Culvert (Passes 3.32 cfs of 10.54 cfs potential flow)
- ↑ 2=Orifice (Orifice Controls 0.05 cfs @ 11.23 fps)
- ↑ 3=Custom Weir (Weir Controls 3.27 cfs @ 1.80 fps)

Pond 5P: VAULT-A2

Hydrograph



Summary for Link 10L: Inflow to VAULT-C2

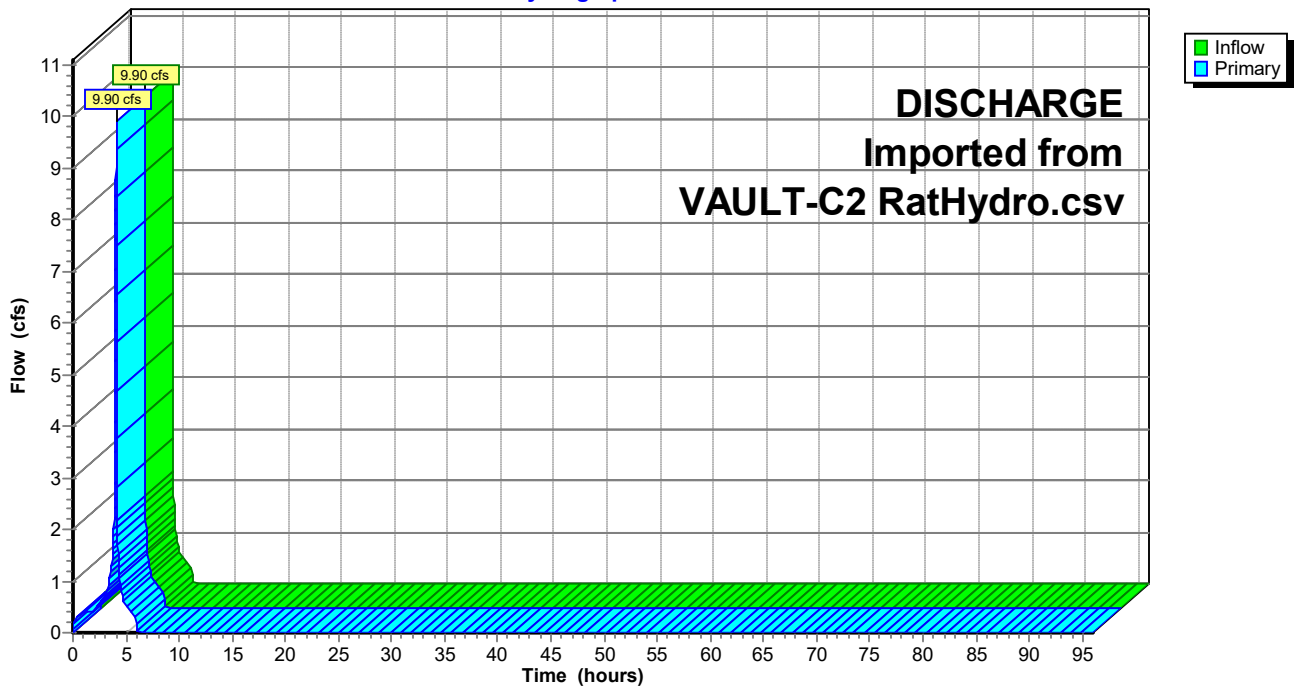
Inflow = 9.90 cfs @ 4.08 hrs, Volume= 0.432 af
Primary = 9.90 cfs @ 4.08 hrs, Volume= 0.432 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

DISCHARGE Imported from VAULT-C2 RatHydro.csv

Link 10L: Inflow to VAULT-C2

Hydrograph



Summary for Pond 22P: VAULT-C2

Inflow = 9.90 cfs @ 4.08 hrs, Volume= 0.432 af
 Outflow = 0.77 cfs @ 4.52 hrs, Volume= 0.432 af, Atten= 92%, Lag= 26.7 min
 Primary = 0.77 cfs @ 4.52 hrs, Volume= 0.432 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs
 Peak Elev= 107.10' @ 4.52 hrs Surf.Area= 2,000 sf Storage= 14,192 cf

Plug-Flow detention time= 661.1 min calculated for 0.432 af (100% of inflow)
 Center-of-Mass det. time= 661.5 min (873.5 - 212.0)

Volume	Invert	Avail.Storage	Storage Description
#1	100.00'	20,000 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
100.00	2,000	0	0	2,000
101.00	2,000	2,000	2,000	2,159
102.00	2,000	2,000	4,000	2,317
103.00	2,000	2,000	6,000	2,476
104.00	2,000	2,000	8,000	2,634
104.50	2,000	1,000	9,000	2,713
105.00	2,000	1,000	10,000	2,793
106.00	2,000	2,000	12,000	2,951
107.00	2,000	2,000	14,000	3,110
108.00	2,000	2,000	16,000	3,268
109.00	2,000	2,000	18,000	3,427
109.50	2,000	1,000	19,000	3,506
110.00	2,000	1,000	20,000	3,585

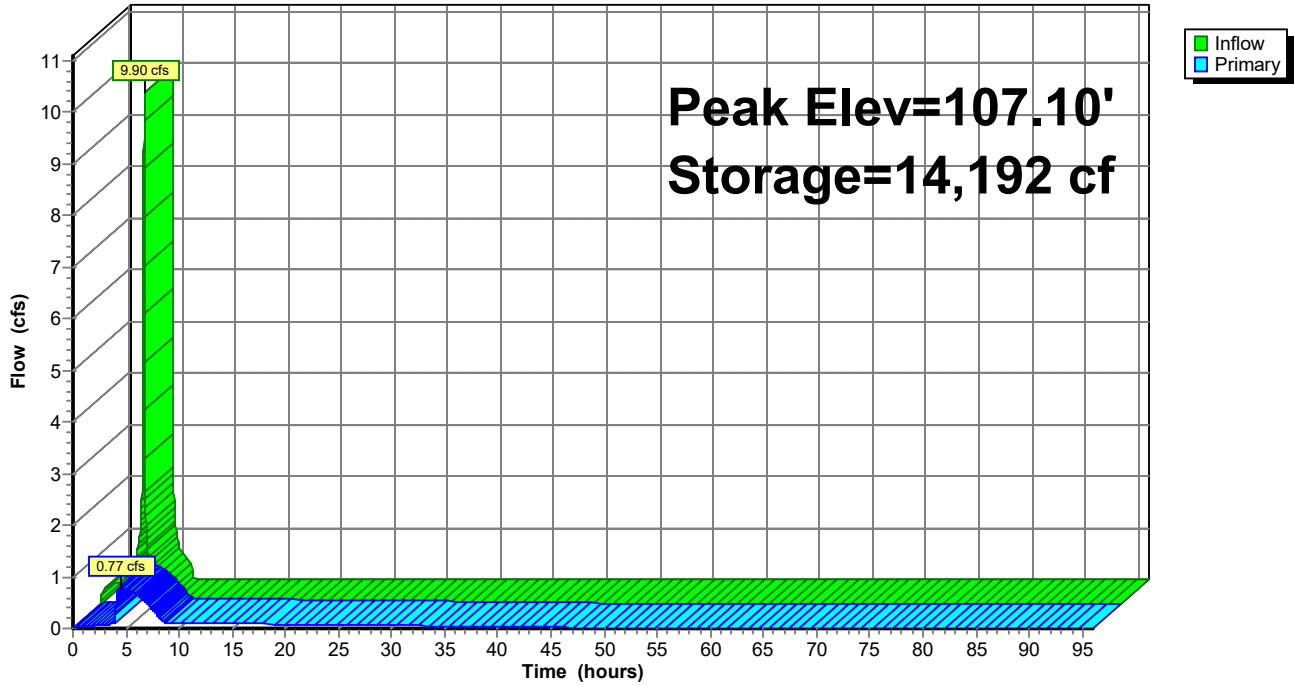
Device	Routing	Invert	Outlet Devices
#1	Primary	100.00'	18.0" Round Culvert L= 10.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 100.00' / 99.90' S= 0.0100 '/ Cc= 0.900 n= 0.013, Flow Area= 1.77 sf
#2	Device 1	100.00'	1.4" Vert. Orifice C= 0.600 Limited to weir flow at low heads
#3	Device 1	104.50'	6.0" W x 2.0" H Vert. Orifice C= 0.600 Limited to weir flow at low heads
#4	Device 1	109.50'	Custom Weir, Cv= 2.62 (C= 3.28) Head (feet) 0.00 0.50 0.50 Width (feet) 12.00 12.00 0.00

Primary OutFlow Max=0.77 cfs @ 4.52 hrs HW=107.10' (Free Discharge)

- 1=Culvert (Passes 0.77 cfs of 26.79 cfs potential flow)
- 2=Orifice (Orifice Controls 0.14 cfs @ 12.77 fps)
- 3=Orifice (Orifice Controls 0.64 cfs @ 7.63 fps)
- 4=Custom Weir (Controls 0.00 cfs)

Pond 22P: VAULT-C2

Hydrograph



Summary for Link 11L: Inflow to VAULT-D1

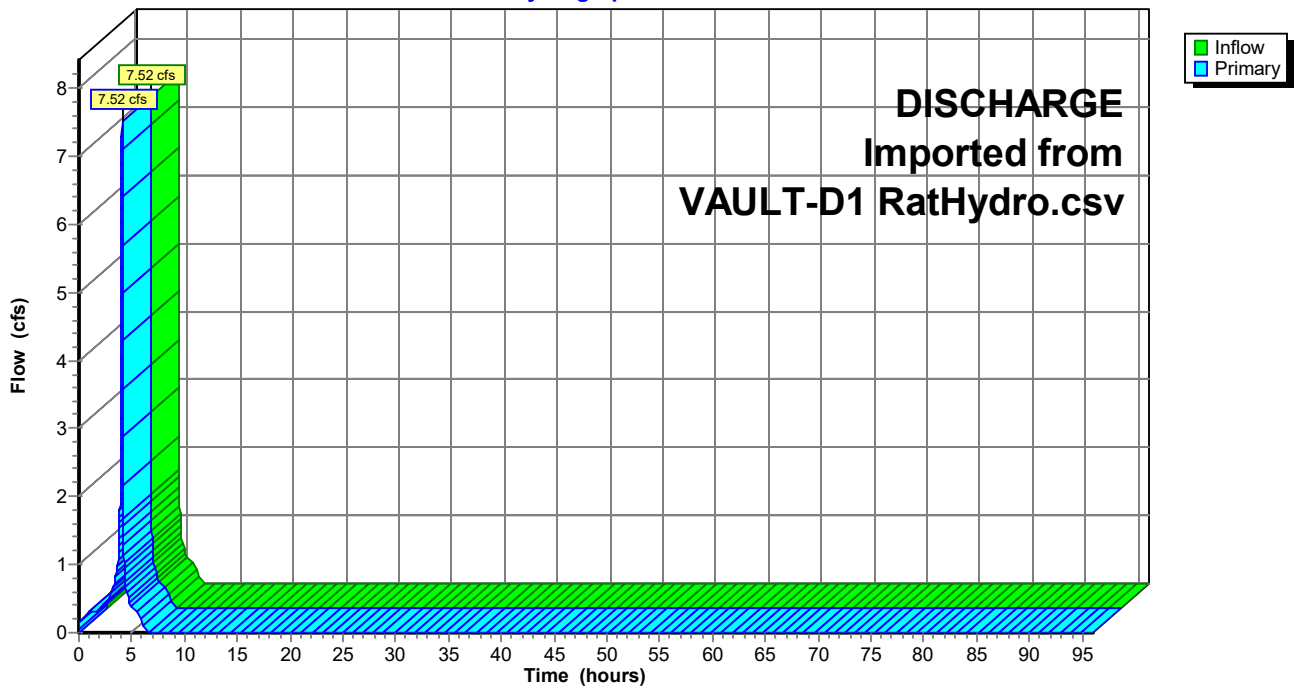
Inflow = 7.52 cfs @ 4.08 hrs, Volume= 0.328 af
Primary = 7.52 cfs @ 4.08 hrs, Volume= 0.328 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

DISCHARGE Imported from VAULT-D1 RatHydro.csv

Link 11L: Inflow to VAULT-D1

Hydrograph



Summary for Pond 23P: VAULT-D1

Inflow = 7.52 cfs @ 4.08 hrs, Volume= 0.328 af
 Outflow = 3.64 cfs @ 4.14 hrs, Volume= 0.328 af, Atten= 52%, Lag= 3.7 min
 Primary = 3.64 cfs @ 4.14 hrs, Volume= 0.328 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs
 Peak Elev= 105.39' @ 4.14 hrs Surf.Area= 1,800 sf Storage= 9,711 cf

Plug-Flow detention time= 628.4 min calculated for 0.328 af (100% of inflow)
 Center-of-Mass det. time= 628.8 min (840.8 - 212.0)

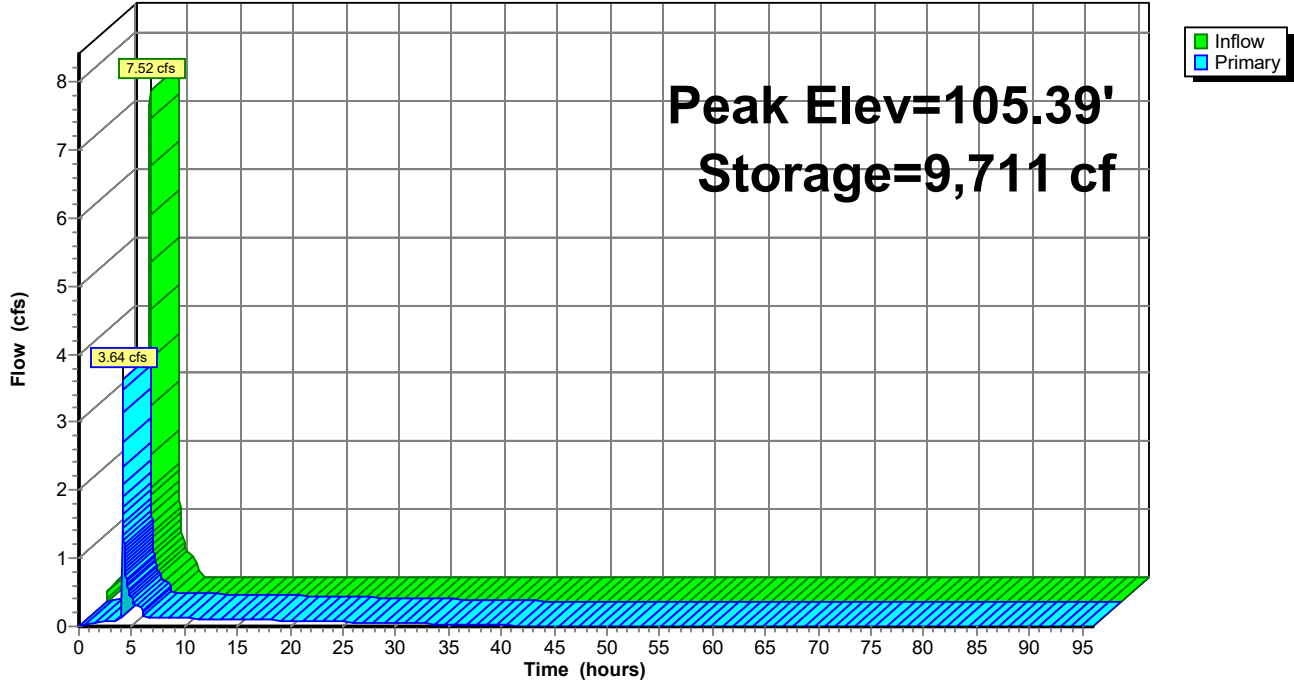
Volume	Invert	Avail.Storage	Storage Description		
#1	100.00'	10,206 cf	Custom Stage Data (Conic) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
100.00	1,800	0	0	1,800	
101.00	1,800	1,800	1,800	1,950	
102.00	1,800	1,800	3,600	2,101	
103.00	1,800	1,800	5,400	2,251	
104.00	1,800	1,800	7,200	2,402	
105.00	1,800	1,800	9,000	2,552	
105.17	1,800	306	9,306	2,578	
105.67	1,800	900	10,206	2,653	

Device	Routing	Invert	Outlet Devices
#1	Primary	100.00'	12.0" Round Culvert L= 10.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 100.00' / 99.90' S= 0.0100 '/ Cc= 0.900 n= 0.013, Flow Area= 0.79 sf
#2	Device 1	100.00'	1.5" Vert. Orifice C= 0.600 Limited to weir flow at low heads
#3	Device 1	105.17'	Custom Weir, Cv= 2.62 (C= 3.28) Head (feet) 0.00 0.50 0.50 Width (feet) 10.00 10.00 0.00

Primary OutFlow Max=3.62 cfs @ 4.14 hrs HW=105.39' (Free Discharge)
 1=Culvert (Passes 3.62 cfs of 10.46 cfs potential flow)
 2=Orifice (Orifice Controls 0.14 cfs @ 11.12 fps)
 3=Custom Weir (Weir Controls 3.48 cfs @ 1.55 fps)

Pond 23P: VAULT-D1

Hydrograph



Summary for Link 12L: Inflow to VAULT-D2

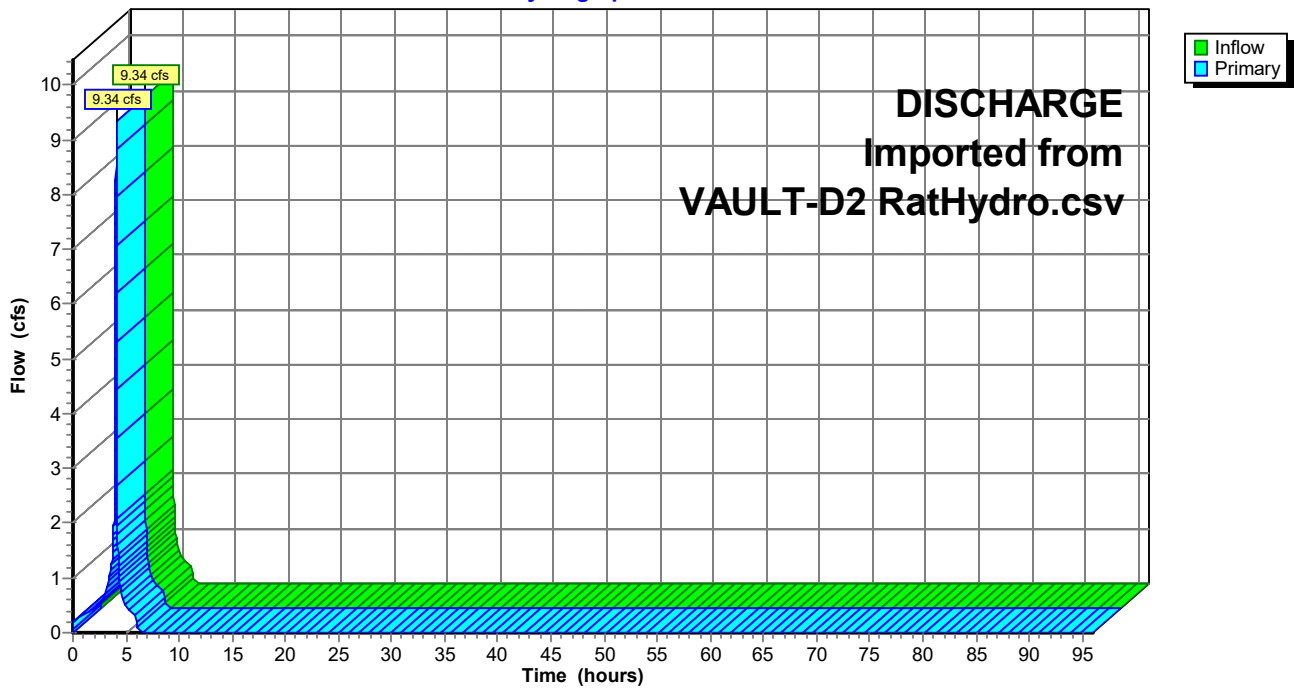
Inflow = 9.34 cfs @ 4.08 hrs, Volume= 0.409 af
Primary = 9.34 cfs @ 4.08 hrs, Volume= 0.409 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

DISCHARGE Imported from VAULT-D2 RatHydro.csv

Link 12L: Inflow to VAULT-D2

Hydrograph



Summary for Pond 9P: VAULT-D2

Inflow = 9.34 cfs @ 4.08 hrs, Volume= 0.409 af
 Outflow = 8.81 cfs @ 4.09 hrs, Volume= 0.409 af, Atten= 6%, Lag= 0.7 min
 Primary = 8.81 cfs @ 4.09 hrs, Volume= 0.409 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs
 Peak Elev= 105.58' @ 4.09 hrs Surf.Area= 1,800 sf Storage= 10,047 cf

Plug-Flow detention time= 513.3 min calculated for 0.409 af (100% of inflow)
 Center-of-Mass det. time= 513.2 min (725.3 - 212.1)

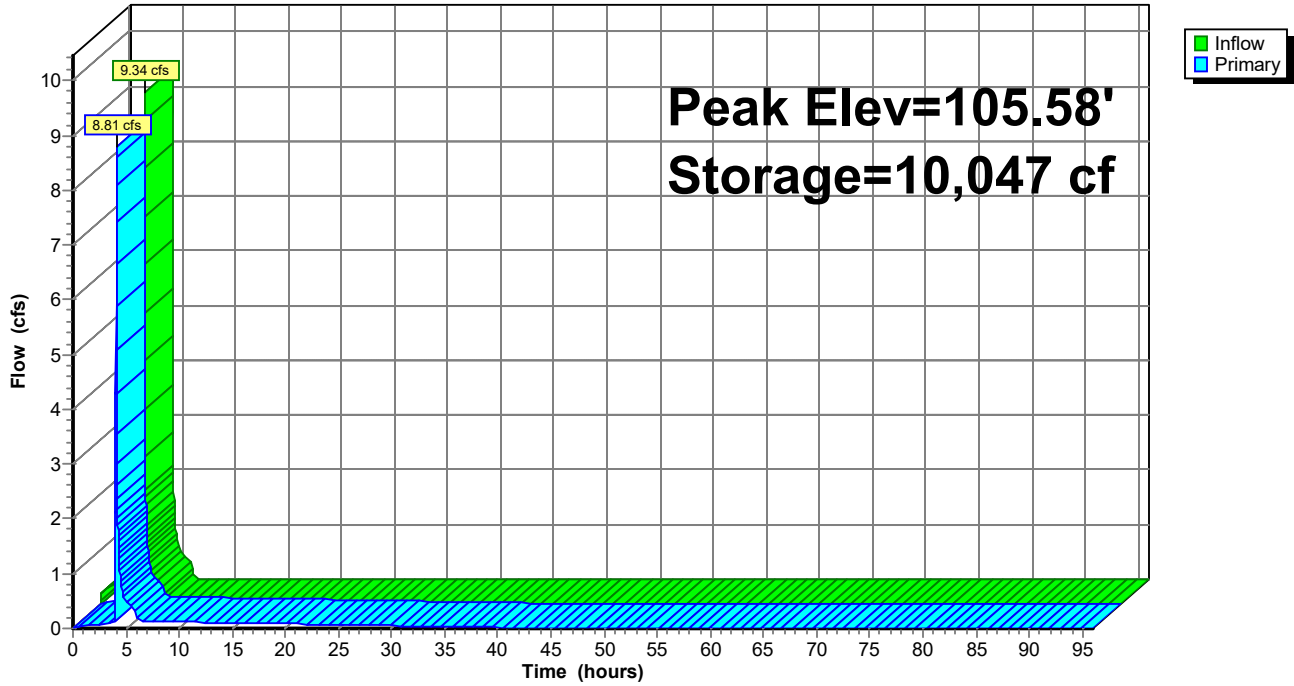
Volume	Invert	Avail.Storage	Storage Description		
#1	100.00'	10,206 cf	Custom Stage Data (Conic) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
100.00	1,800	0	0	1,800	
101.00	1,800	1,800	1,800	1,950	
102.00	1,800	1,800	3,600	2,101	
103.00	1,800	1,800	5,400	2,251	
104.00	1,800	1,800	7,200	2,402	
105.00	1,800	1,800	9,000	2,552	
105.17	1,800	306	9,306	2,578	
105.67	1,800	900	10,206	2,653	

Device	Routing	Invert	Outlet Devices
#1	Primary	100.00'	12.0" Round Culvert L= 10.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 100.00' / 99.90' S= 0.0100 '/ Cc= 0.900 n= 0.013, Flow Area= 0.79 sf
#2	Device 1	100.00'	1.5" Vert. Orifice C= 0.600 Limited to weir flow at low heads
#3	Device 1	105.17'	Custom Weir, Cv= 2.62 (C= 3.28) Head (feet) 0.00 0.50 0.50 Width (feet) 10.00 10.00 0.00

Primary OutFlow Max=8.79 cfs @ 4.09 hrs HW=105.58' (Free Discharge)
 1=Culvert (Passes 8.79 cfs of 10.66 cfs potential flow)
 2=Orifice (Orifice Controls 0.14 cfs @ 11.31 fps)
 3=Custom Weir (Weir Controls 8.65 cfs @ 2.10 fps)

Pond 9P: VAULT-D2

Hydrograph



Summary for Link 14L: Inflow to VAULT-D4a

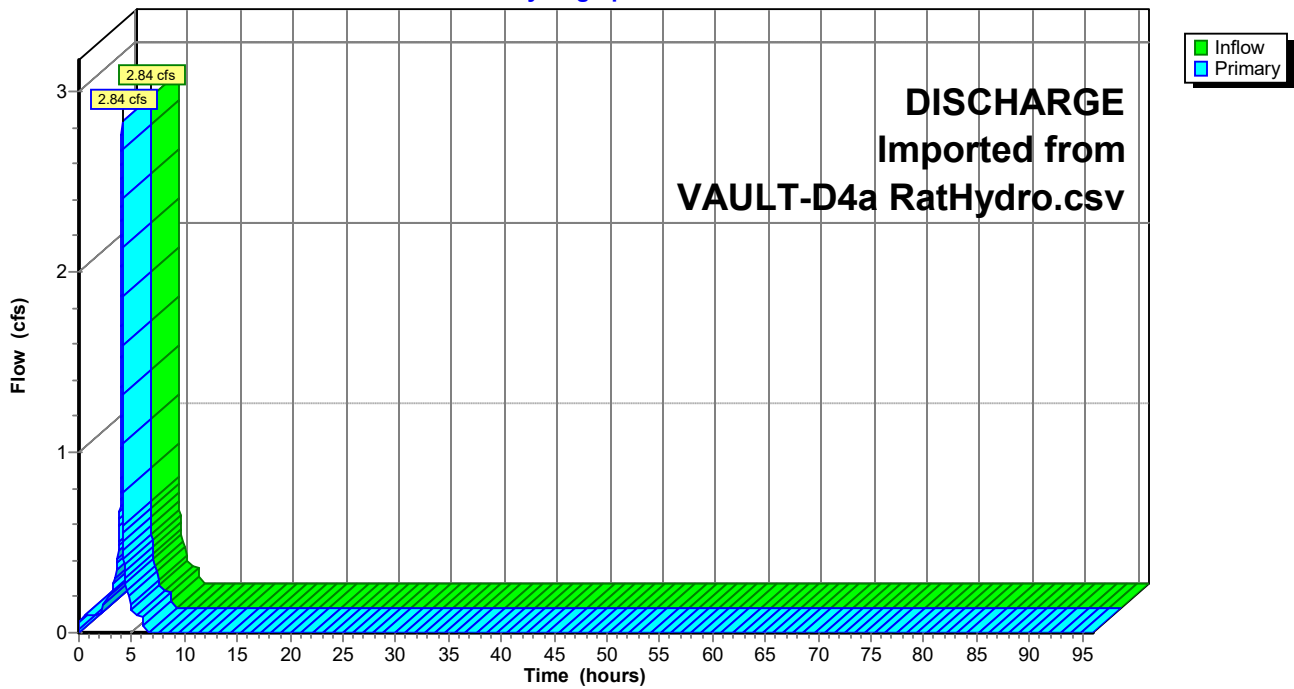
Inflow = 2.84 cfs @ 4.08 hrs, Volume= 0.122 af
Primary = 2.84 cfs @ 4.08 hrs, Volume= 0.122 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

DISCHARGE Imported from VAULT-D4a RatHydro.csv

Link 14L: Inflow to VAULT-D4a

Hydrograph



Summary for Pond 18P: VAULT-D4a

Inflow = 2.84 cfs @ 4.08 hrs, Volume= 0.122 af
 Outflow = 0.26 cfs @ 4.45 hrs, Volume= 0.122 af, Atten= 91%, Lag= 22.2 min
 Primary = 0.26 cfs @ 4.45 hrs, Volume= 0.122 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs
 Peak Elev= 104.17' @ 4.45 hrs Surf.Area= 1,000 sf Storage= 4,171 cf

Plug-Flow detention time= 1,152.6 min calculated for 0.122 af (100% of inflow)
 Center-of-Mass det. time= 1,152.6 min (1,364.9 - 212.3)

Volume	Invert	Avail.Storage	Storage Description		
#1	100.00'	5,670 cf	Custom Stage Data (Conic) Listed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
100.00	1,000	0	0	1,000	
101.00	1,000	1,000	1,000	1,112	
102.00	1,000	1,000	2,000	1,224	
103.00	1,000	1,000	3,000	1,336	
104.00	1,000	1,000	4,000	1,448	
105.00	1,000	1,000	5,000	1,560	
105.17	1,000	170	5,170	1,580	
105.67	1,000	500	5,670	1,636	

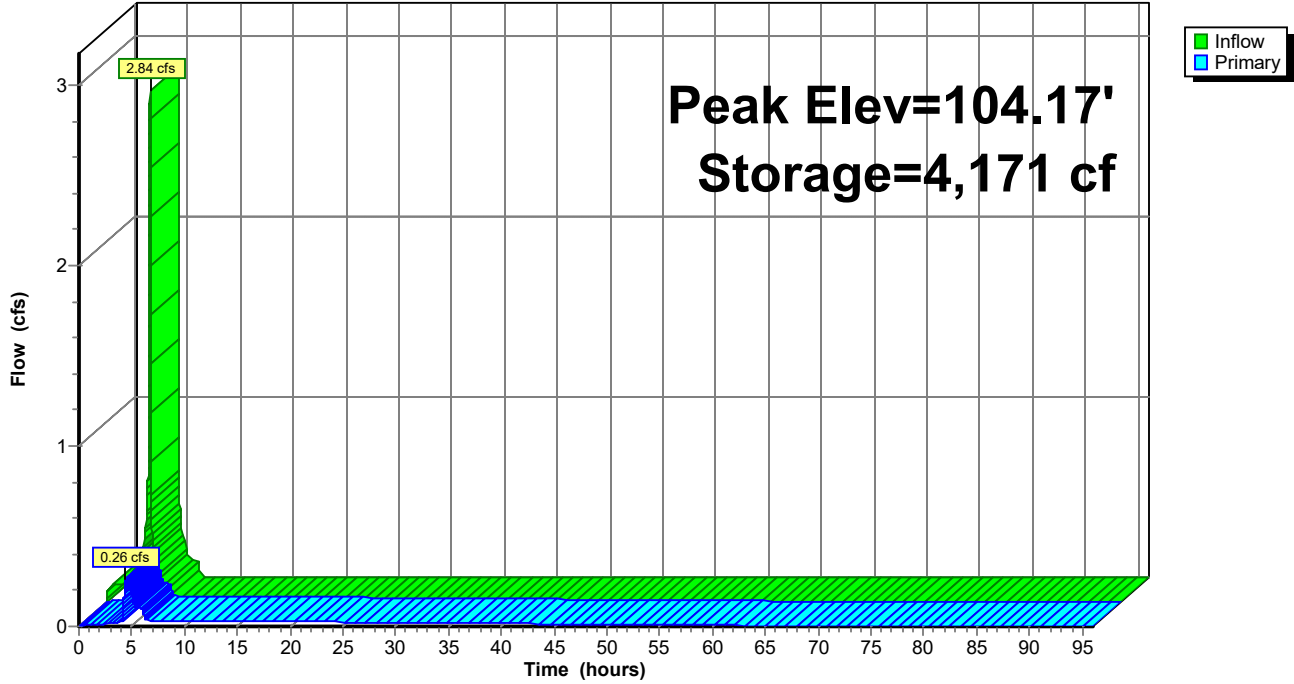
Device	Routing	Invert	Outlet Devices
#1	Primary	100.00'	12.0" Round Culvert L= 10.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 100.00' / 99.90' S= 0.0100 '/ Cc= 0.900 n= 0.013, Flow Area= 0.79 sf
#2	Device 1	100.00'	0.8" Vert. Orifice C= 0.600 Limited to weir flow at low heads
#3	Device 1	104.00'	12.0" W x 3.0" H Vert. Orifice C= 0.600 Limited to weir flow at low heads
#4	Device 1	105.17'	Custom Weir, Cv= 2.62 (C= 3.28) Head (feet) 0.00 0.50 0.50 Width (feet) 5.00 5.00 0.00

Primary OutFlow Max=0.26 cfs @ 4.45 hrs HW=104.17' (Free Discharge)

- 1=Culvert (Passes 0.26 cfs of 9.06 cfs potential flow)
- 2=Orifice (Orifice Controls 0.03 cfs @ 9.79 fps)
- 3=Orifice (Orifice Controls 0.23 cfs @ 1.33 fps)
- 4=Custom Weir (Controls 0.00 cfs)

Pond 18P: VAULT-D4a

Hydrograph



Summary for Link 15L: Inflow to VAULT-D4b

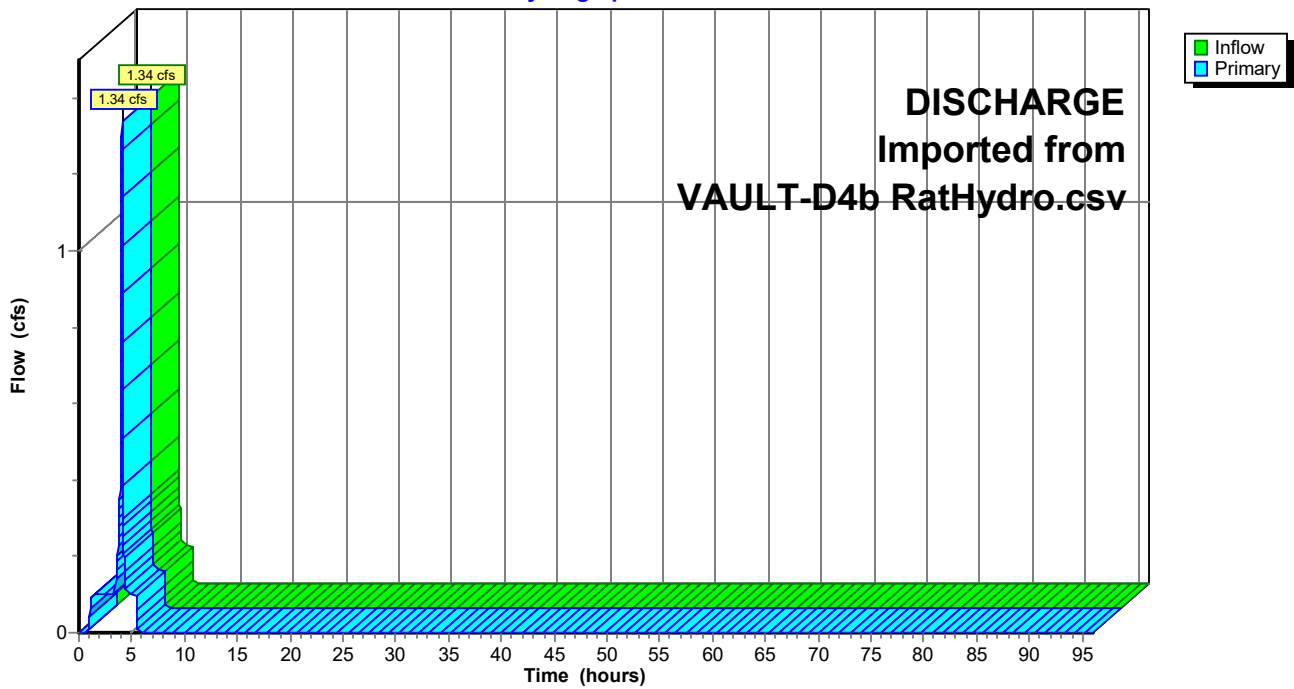
Inflow = 1.34 cfs @ 4.08 hrs, Volume= 0.060 af
Primary = 1.34 cfs @ 4.08 hrs, Volume= 0.060 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

DISCHARGE Imported from VAULT-D4b RatHydro.csv

Link 15L: Inflow to VAULT-D4b

Hydrograph



Summary for Pond 24P: VAULT-D4b

Inflow = 1.34 cfs @ 4.08 hrs, Volume= 0.060 af
 Outflow = 0.10 cfs @ 5.50 hrs, Volume= 0.060 af, Atten= 93%, Lag= 85.3 min
 Primary = 0.10 cfs @ 5.50 hrs, Volume= 0.060 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs
 Peak Elev= 105.20' @ 5.50 hrs Surf.Area= 400 sf Storage= 2,081 cf

Plug-Flow detention time= 731.9 min calculated for 0.060 af (100% of inflow)
 Center-of-Mass det. time= 732.1 min (946.1 - 214.0)

Volume	Invert	Avail.Storage	Storage Description
#1	100.00'	2,268 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
100.00	400	0	0	400
101.00	400	400	400	471
102.00	400	400	800	542
103.00	400	400	1,200	613
104.00	400	400	1,600	684
105.17	400	468	2,068	767
105.67	400	200	2,268	802

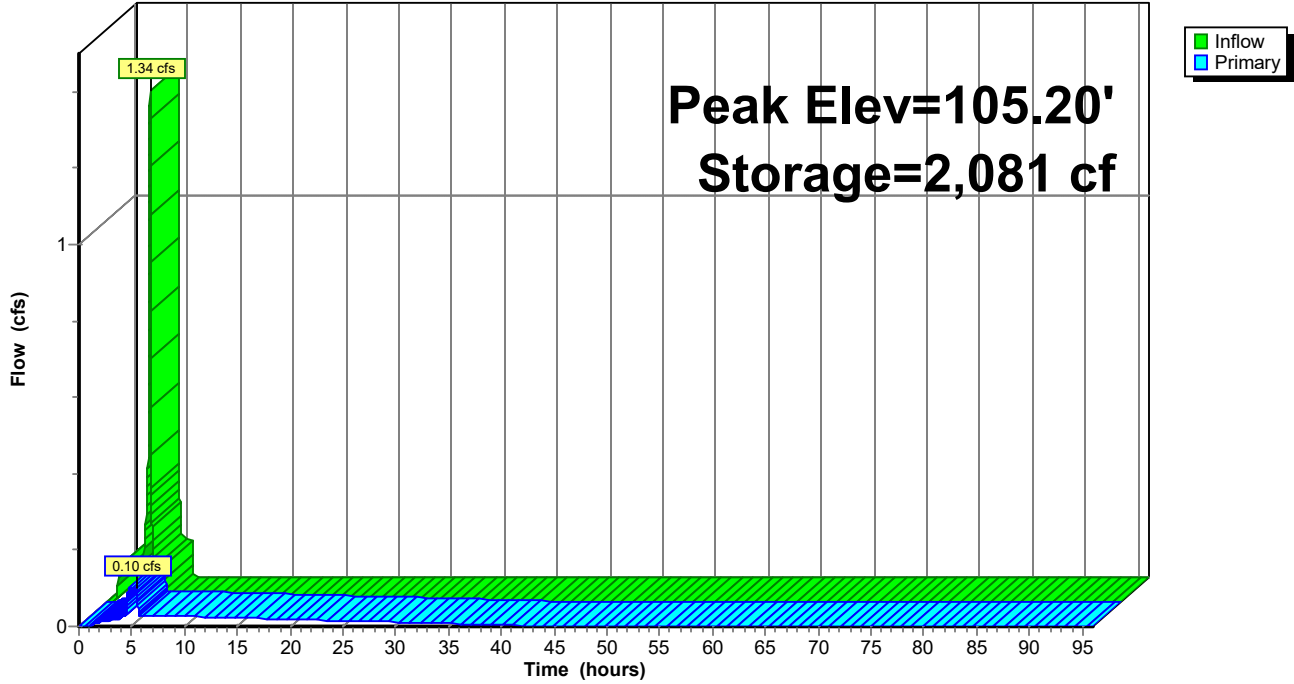
Device	Routing	Invert	Outlet Devices
#1	Primary	100.00'	12.0" Round Culvert L= 10.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 100.00' / 99.90' S= 0.0100 '/ Cc= 0.900 n= 0.013, Flow Area= 0.79 sf
#2	Device 1	100.00'	0.7" Vert. Orifice C= 0.600 Limited to weir flow at low heads
#3	Device 1	105.17'	Custom Weir, Cv= 2.62 (C= 3.28) Head (feet) 0.00 0.50 0.50 Width (feet) 3.00 3.00 0.00

Primary OutFlow Max=0.09 cfs @ 5.50 hrs HW=105.20' (Free Discharge)

- ↑ 1=Culvert (Passes 0.09 cfs of 10.25 cfs potential flow)
- ↑ 2=Orifice (Orifice Controls 0.03 cfs @ 10.95 fps)
- ↑ 3=Custom Weir (Weir Controls 0.06 cfs @ 0.60 fps)

Pond 24P: VAULT-D4b

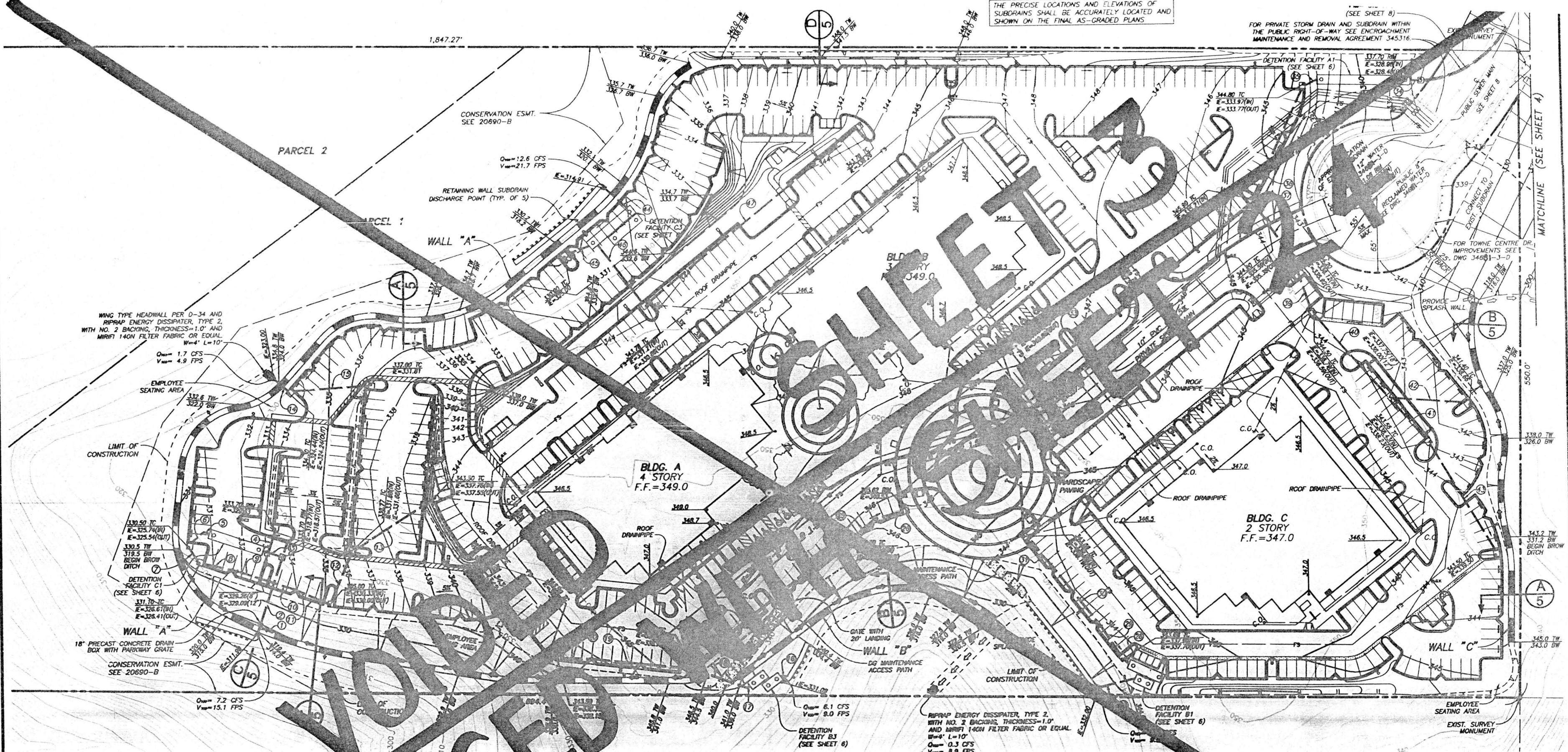
Hydrograph





Appendix 4
Summit Pointe Plaza Grading Plans, PTS 6109





STORM DRAIN DATA (P.V.T.)				STORM DRAIN DATA (P.V.T.) CONT.			
NO.	LENGTH	SLOPE	REMARKS	NO.	LENGTH	SLOPE	REMARKS
1	8.30'	10.00%	12" PVC	16	4.00'	3.00%	12" PVC
2	58.35'	10.00%	12" PVC	17	3.00'	1.00%	12" PVC
3	15.00'	5.00%	12" PVC	18	47.25'	1.00%	12" PVC
4	43.00'	1.00%	8" PVC	19	85.50'	1.00%	12" PVC
5	5.00'	5.00%	12" PVC	20	26.35'	1.00%	12" PVC
6	15.50'	5.00%	12" PVC	21	2.00'	2.00%	8" PVC
7	13.50'	5.00%	12" PVC	22	1.00'	1.00%	12" PVC
8	30.40'	3.00%	12" PVC	23	93.25'	1.00%	12" PVC
9	20.00'	3.00%	12" PVC	24	30.15'	1.50%	12" PVC
10	32.00'	3.00%	12" PVC	25	41.00'	1.00%	12" PVC
11	30.50'	3.00%	12" PVC	26	1.00'	1.00%	12" PVC
12	45.00'	3.00%	12" PVC	27	1.00'	1.00%	12" PVC
13	81.00'	7.00%	12" PVC	28	1.00'	1.00%	12" PVC
14	15.50'	8.00%	8" PVC	29	1.00'	1.00%	12" PVC
15	67.00'	1.00%	8" PVC	30	1.00'	1.00%	12" PVC
				31	30.15'	1.00%	12" PVC
				32	117.25'	1.00%	12" PVC
				33	120.00'	1.00%	12" PVC
				34	7.00'	1.20%	18" PVC
				35	12.50'	1.20%	18" PVC
				36	104.00'	1.20%	18" PVC
				37	1.00'	1.00%	18" PVC
				38	1.00'	1.00%	18" PVC
				39	1.00'	1.00%	18" PVC
				40	95.50'	1.00%	18" PVC
				41	48.38'	1.00%	18" PVC
				42	66.00'	3.00%	12" PVC
				43	107.00'	1.00%	18" PVC
				44	25.50'	18.00%	18" PVC
				45	20.50'	2.40%	8" PVC

NOTES

- ALL ON-SITE PRIVATE IMPROVEMENTS SHOWN ON THIS DRAWING ARE FOR INFORMATION ONLY. THE CITY ENGINEER APPROVAL OF THIS DRAWING IN NO WAY CONSTITUTES AN APPROVAL OF SAID PRIVATE IMPROVEMENTS. A SEPARATE PERMIT FOR SUCH IMPROVEMENTS MAY BE REQUIRED.
- RETAINING WALLS SHOWN ON THESE PLANS ARE FOR INFORMATION ONLY. A SEPARATE BUILDING PERMIT AND INSPECTION WILL BE REQUIRED FROM THE DEVELOPMENT SERVICES DEPARTMENT FOR THEIR CONSTRUCTION.
- ALL ROOF DRAIN PIPES SHOWN HEREON ARE FOR INFORMATION ONLY. THEY WILL BE CONSTRUCTED PER THE BUILDING PLANS.
- NO GRADING WILL BE ALLOWED IMMEDIATELY ADJACENT TO THE PROPOSED RETAINING WALLS UNTIL A RETAINING WALL PERMIT HAS BEEN OBTAINED BY THE OWNER'S REPRESENTATIVE.

W.S. WILLIAM A. STEEN & ASSOCIATES
 CONSULTING CIVIL ENGINEERS, LAND SURVEYING & PLANNING
 8580 LA MESA BLVD., SUITE 102, LA MESA, CALIFORNIA 91941
 (619) 480-8000 • FAX (619) 480-8005

ENGINEER: *William A. Steen* 10-5-07 JOB NO. 6247-101
 WILLIAM A. STEEN R.C.E. 18138 DATE



PRIVATE CONTRACT
 GRADING PLANS FOR:
SUMMIT POINTE PLAZA

LOT "A", PL. 1320, SEC. 17822
 CITY OF SAN DIEGO, CALIFORNIA
 DEVELOPMENT SERVICES DEPARTMENT
 SHEET 3 OF 30 SHEETS

FOR CITY ENGINEER	DATE	FILED	W.O. NO.
DESCRIPTION	BY	APPROVED	DATE
ORIGINAL	WAS	DZL	11/24/08
CHANGE	WAS	DZL	11/24/10

AS-BUILT WAS SE 6/16/11 10-01-11
 COMMISSIONER LEBACY BUILDING DATE STARTED 1/03/08
 INSPECTOR SERRAO INQUIRY DATE COMPLETED 8/30/11

32375-3-D
 LAMBERT COORDINATES
 284-1703

Construction contracts... that in accordance with generally accepted engineering practices, construction... shall be required to assume sole and complete responsibility for job site conditions...
CELSOC

UNAUTHORIZED CHANGES & USES: The engineer preparing these plans will not be responsible for, or liable for, unauthorized changes to or uses of these plans. All changes to the plans must be in writing and must be approved by the preparer of these plans.
CELSOC

AS-BUILT



MATCHLINE (SEE SHEET 24)

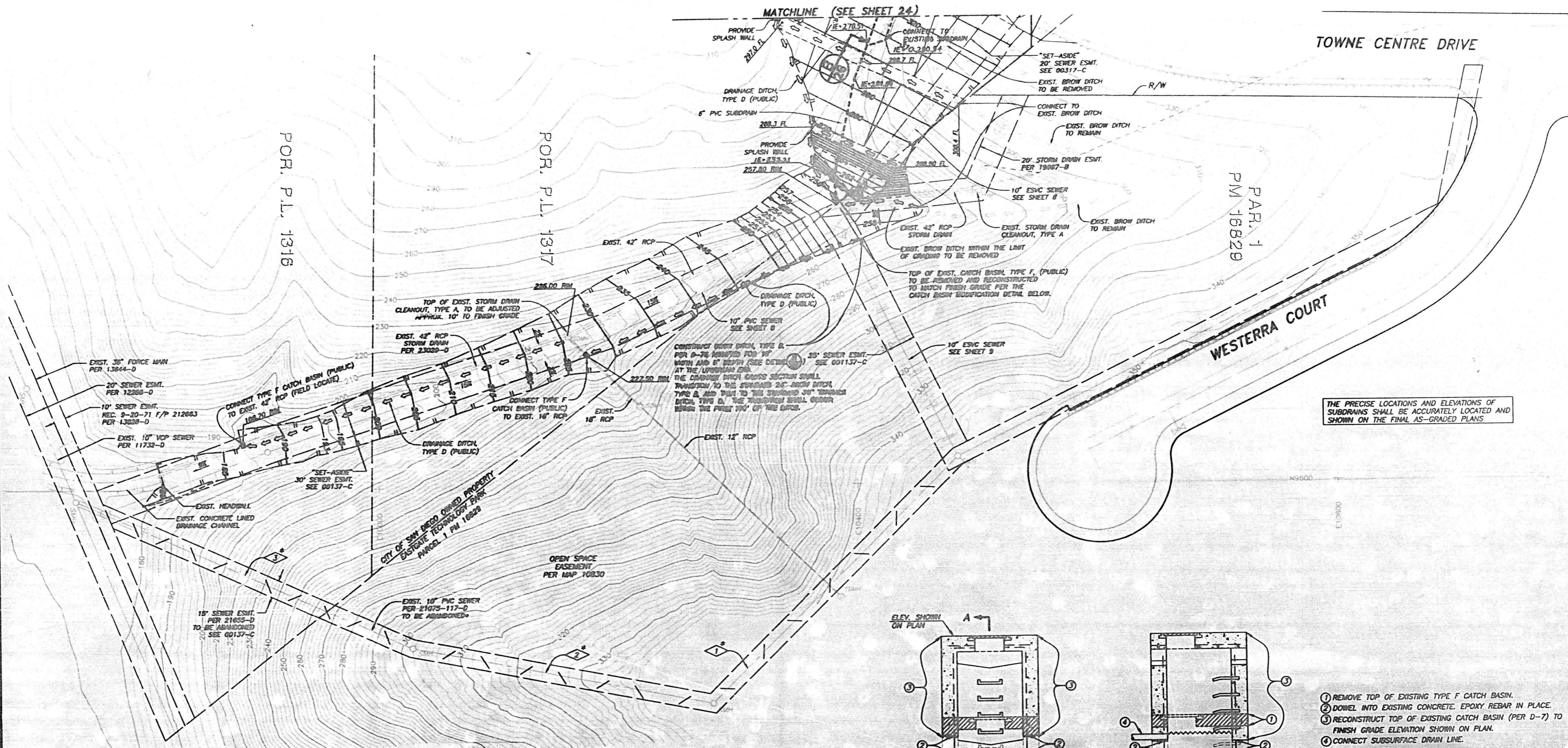
TOWNE CENTRE DRIVE

P.A.R. 1
P.M. 16829

WESTERRA COURT

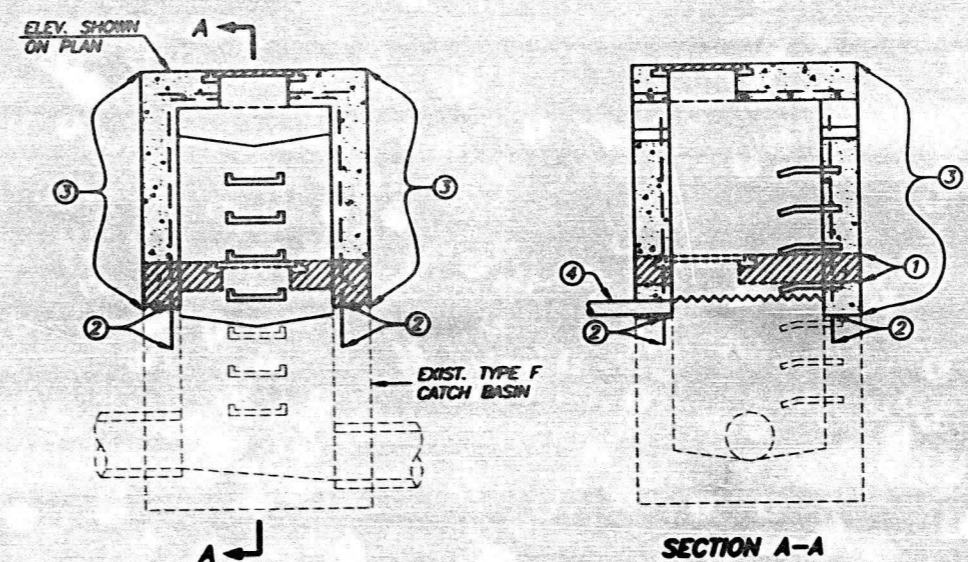
P.O.R. P.L. 1316

P.O.R. P.L. 1317

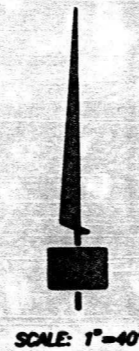


THE PRECISE LOCATIONS AND ELEVATIONS OF SUBDRAINS SHALL BE ACCURATELY LOCATED AND SHOWN ON THE FINAL AS-GRADED PLANS

* SEE SEWER ABANDONMENT TABLE ON SHEET 2



- 1 REMOVE TOP OF EXISTING TYPE F CATCH BASIN.
- 2 DOBREL INTO EXISTING CONCRETE. EPOXY REBAR IN PLACE.
- 3 RECONSTRUCT TOP OF EXISTING CATCH BASIN (PER D-7) TO FINISH GRADE ELEVATION SHOWN ON PLAN.
- 4 CONNECT SUBSURFACE DRAIN LINE.



Construction contractor agrees that in accordance with generally accepted construction practices, construction contractor will be required to assume sole and complete responsibility for job site conditions during the course of construction of the project, including safety of all persons and property; that this requirement shall be made to apply continuously and not be limited to normal working hours, and construction contractor further agrees to defend, indemnify and hold design professional harmless from any and all liability, real or alleged, in connection with the performance of work on this project, accepting liability arising from the sole negligence of design professional.

CELSOC

UNAUTHORIZED CHANGES & USES: The engineer preparing these plans will not be responsible for, or liable for, unauthorized changes to or uses of these plans. All changes to the plans must be in writing and must be approved by the preparer of these plans.

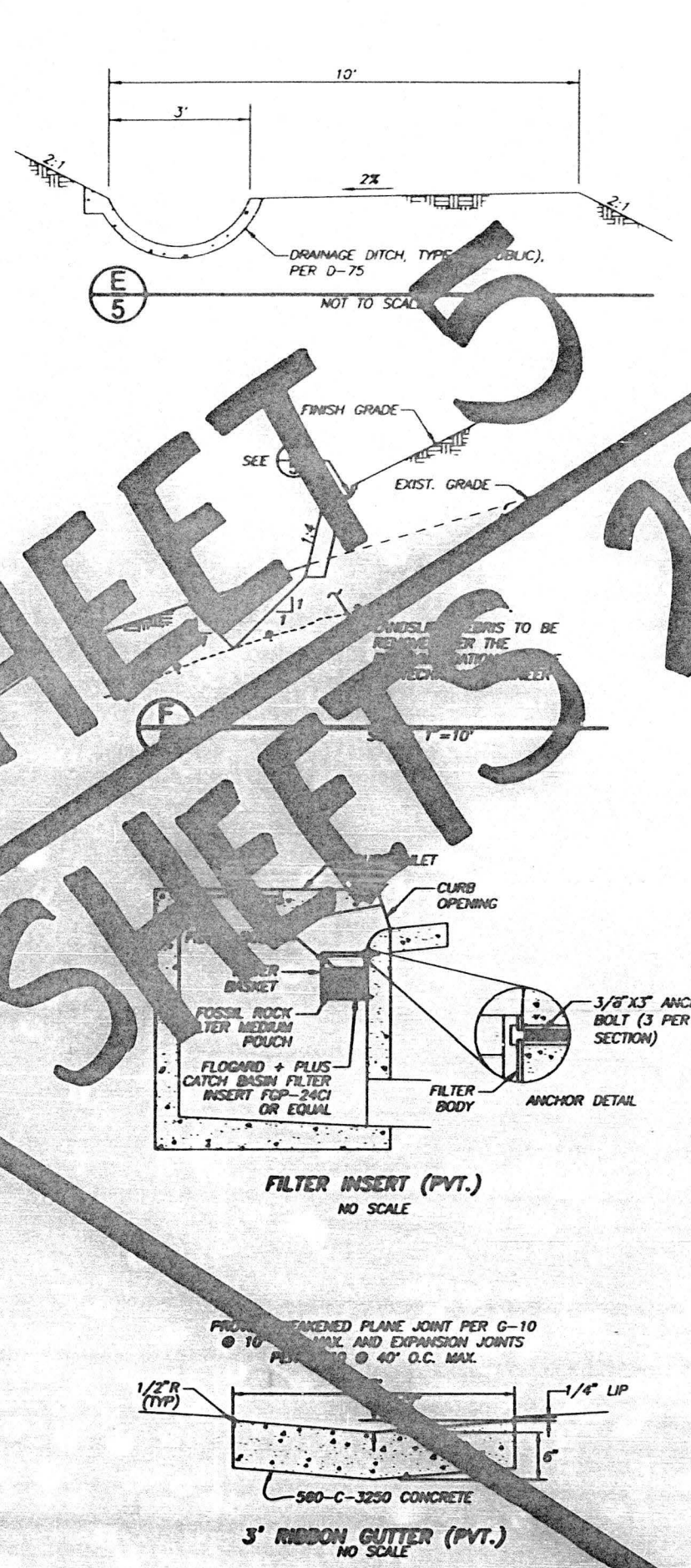
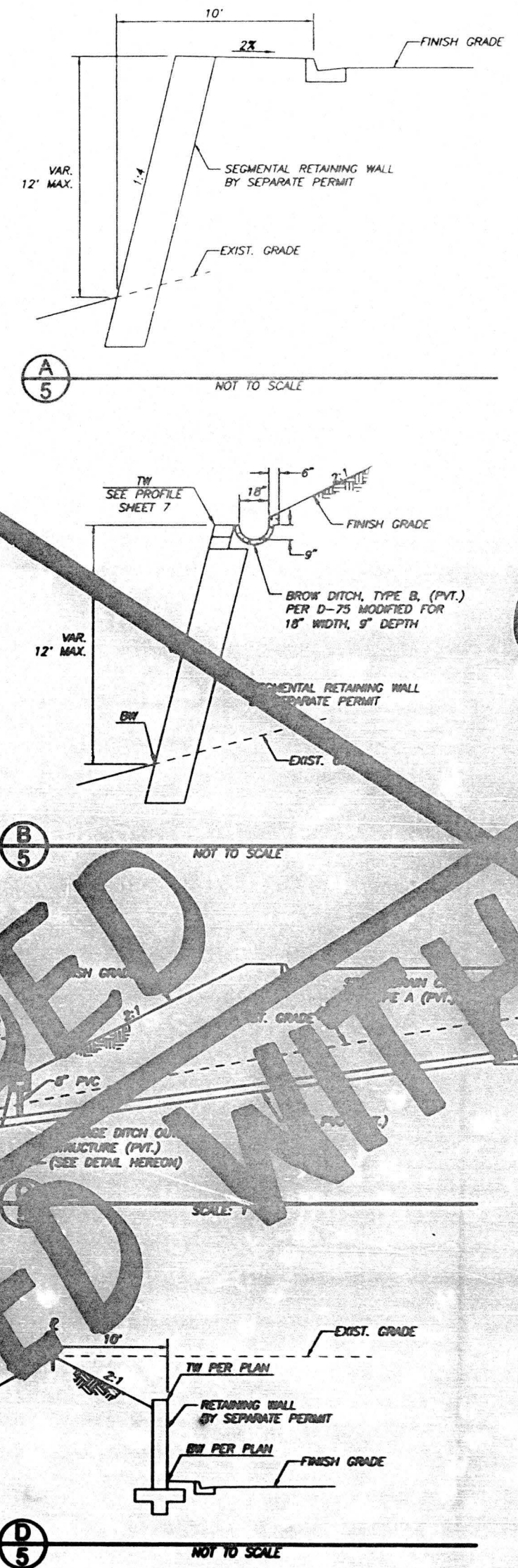
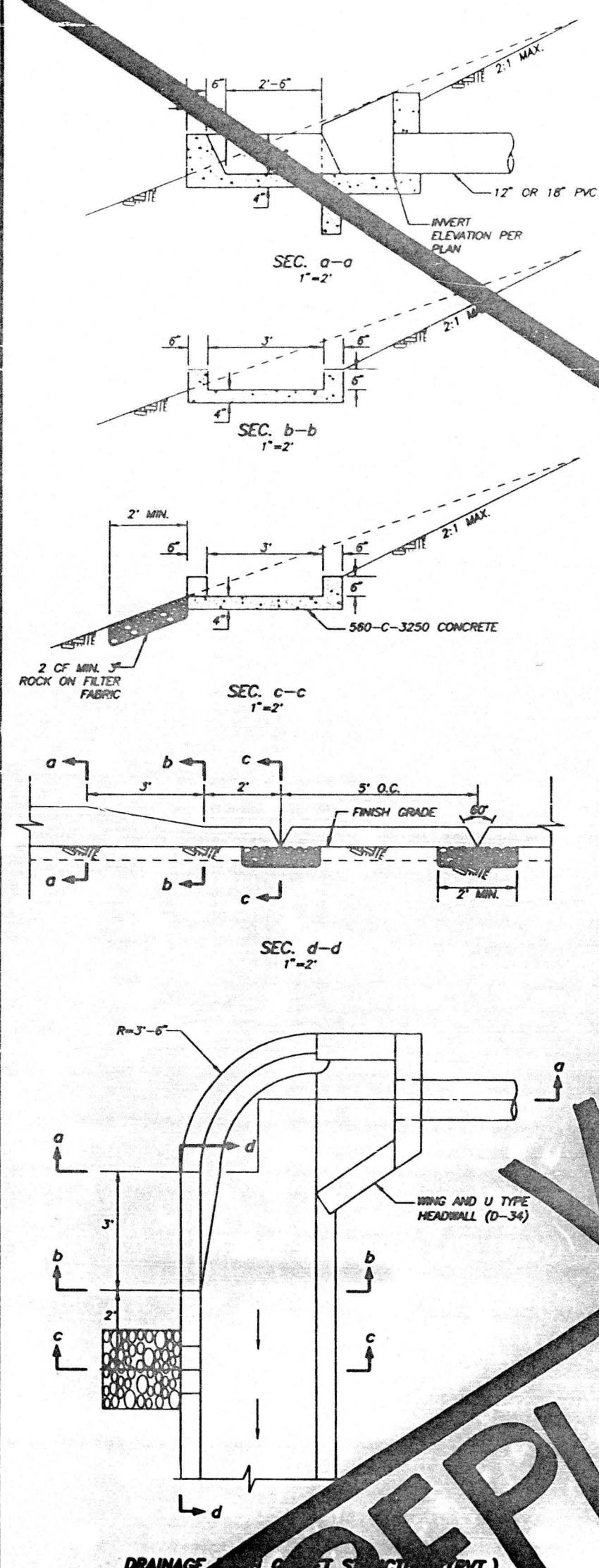
CELSOC

WILLIAM A. SEEN & ASSOCIATES
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8880 LA MESA BLVD., SUITE 102, LA MESA, CALIFORNIA 91941
(915) 480-9000 • FAX (915) 480-9005 •
ENGINEER OF RECORD
William A. Seen 10-5-07 JOB NO. 6247-101
WILLIAM A. SEEN R.C.E. 18136 DATE



PRIVATE CONTRACT			
GRADING PLANS FOR:			
SUMMIT POINTE PLAZA			
LOT "A", P.L. 1300, SEC 17822		W.O. NO. 421168	
CITY OF SAN DIEGO, CALIFORNIA		P.T.S. NO. 6109	
DEVELOPMENT SERVICES DEPARTMENT			
SHEET 4 OF 8 SHEETS			
DATE	10/17/07	T.M.	2781
FOR CITY ENGINEER	DATE	APPROVED	DATE FILMED
DESCRIPTION	BY		
ORIGINAL	N/S		JUN 14 11 28
AS-BUILTS	WAG	CE	6/25/10/08
CONTRACTOR LARRY BOLANDER DATE SUBMITTED 1/05/08			1804-6263
INSPECTOR SERGIO HERRERA DATE COMPLETED 6/20/08			284-1783
			LAMBERT COORDINATES
			32375-4-D

AS-BUILT



Construction contract documents shall govern over these plans. The contractor shall be required to ensure that all construction is in accordance with the approved plans. The contractor shall be responsible for obtaining all necessary permits and for the safety of the construction site. The contractor shall be responsible for the quality of the construction and for the safety of the construction site. The contractor shall be responsible for the safety of the construction site. The contractor shall be responsible for the safety of the construction site.

UNAUTHORIZED CHANGES & USES: The engineer preparing these plans will not be responsible for, or liable for, unauthorized changes to or uses of these plans. All changes to the plans must be in writing and must be approved by the preparer of these plans.

CESLOC
 CONSULTING CIVIL ENGINEERS, LAND SURVEYING & PLANNING
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 (619) 480-9000 • FAX (619) 480-9005

WILLIAM A. STEEN & ASSOCIATES
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 (619) 480-9000 • FAX (619) 480-9005



PRIVATE CONTRACT			
GRADING AND IMPROVEMENT PLANS FOR:			
SUMMIT POINTE PLAZA			
DETAILS			
CITY OF SAN DIEGO, CALIFORNIA	W.O. NO. 421188		
DEVELOPMENT SERVICES DEPARTMENT	P.T.S. NO. 6109		
SHEET 5 OF 25 SHEETS			
FOR CITY ENGINEER	DATE	T.M.	2781
APPROVED	11/2/07		
DESCRIPTION	BY	APPROVED	DATE
ORIGINAL	WAS		
CHANGE	WAS	1/2/07	11-14-10
AS-BUILT	WAS	1/2/07	11-14-10
CONTRACTOR	LEASLEY BUILDING	DATE STARTED	1/05/08
INSPECTOR	BRAND	DATE COMPLETED	9/26/11
			32375-5-D

VOIDED SHEET 5, REPLACED WITH SHEETS 25 & 26
AS-BUILT

LOT
PL 1820
SCC 17822

PM 14482

DETECTION FACILITY DATA

DETECTION FACILITY	A1	B1	B3	C1	C3
A (acres)	0.85	0.85	0.85	0.85	0.85
10-Year Event:					
T _c (minutes)	6.0	5.0	5.0	5.0	5.0
P ₂ (inches)	1.6	1.6	1.6	1.6	1.6
I ₁₀₀ (in/hr)	3.75	4.22	4.22	4.22	4.22
Q ₁₀₀ (cfs)	8.9	7.0	3.7	4.3	9.0
A _o Area of Orifice (ft ²) (1)	0.129	0.114	0.068	0.046	0.083
D _o Orifice Diameter (ft) (2)	0.405	0.381	0.295	0.241	0.326
Q _o (cfs)	1.7	1.5	0.9	0.6	1.1
H _o Peak Head Above Orifice (ft)	7.5	7.5	7.5	7.5	7.5
Inlet Invert Elev. (ft)	333.62	337.64	336.20	324.52	324.50
Outlet Invert Elev. (ft)	329.05	332.64	331.20	319.52	319.50
Min. Storage Volume Req'd. (cf) (3)	4000	2400	1150	1900	4200
Inside Width (ft)	7.0	7.0	7.0	7.0	7.0
Minimum Inside Length (ft) (4)	76.2	45.7	21.9	36.2	80.0

(1) $A_o = Q_o / (C_o \sqrt{2gH_o})^{3/2}$
 (2) $D_o = 2(A_o / \pi)^{1/2}$
 (3) Per Storage Routing Curves
 (4) Length = (Storage Volume) / (Inside Width)

100-Year Event:	A1	B1	B3	C1	C3
T _c (minutes)	6.6	5.0	5.0	5.0	5.0
P ₂ (inches)	2.3	2.3	2.3	2.3	2.3
I ₁₀₀ (in/hr)	5.1	6.1	6.1	6.1	6.1
Q ₁₀₀ (cfs)	12.1	10.1	5.4	6.3	12.6
Q _{spillway} (cfs) (1)	10.4	8.6	4.5	5.7	11.5
Number of 12" Spillways	1	1	2	2	1
Q _{12"} Spillway (cfs) (2)	3.20	2.65	2.25	2.85	3.20
Number of 18" Spillways	1	1	0	0	0
Q _{18"} Spillway (cfs) (2)	7.20	5.95	0.00	0.00	7.96
Head Above Spillway Orifice (3)	0.72	0.49	0.35	0.49	0.88
Spillway Elev. (ft) (4)	337.55	341.14	339.85	327.02	328.00
Water Surface Elev. (ft) (5)	338.27	341.63	338.20	328.59	328.88
Spillway Diameter (inches)	18	18	12	12	18
Spillway Slope (x)	1.2	1.2	3.0	3.0	18.0
Spillway Velocity (fps)	7.4	8.0	8.9	9.0	21.7

(1) $Q_{spillway} = Q_{100} - Q_o$
 (2) Proportional to total spillway orifice area
 (3) $H_o = (Q_o / (C_o A_o))^{2/3} / (2g)$ C_o = 0.60
 (4) Spillway Elev. = Outlet Invert Elev. + 8.5ft
 (5) WSEL = Spillway Elev. + Head Above Spillway Orifice

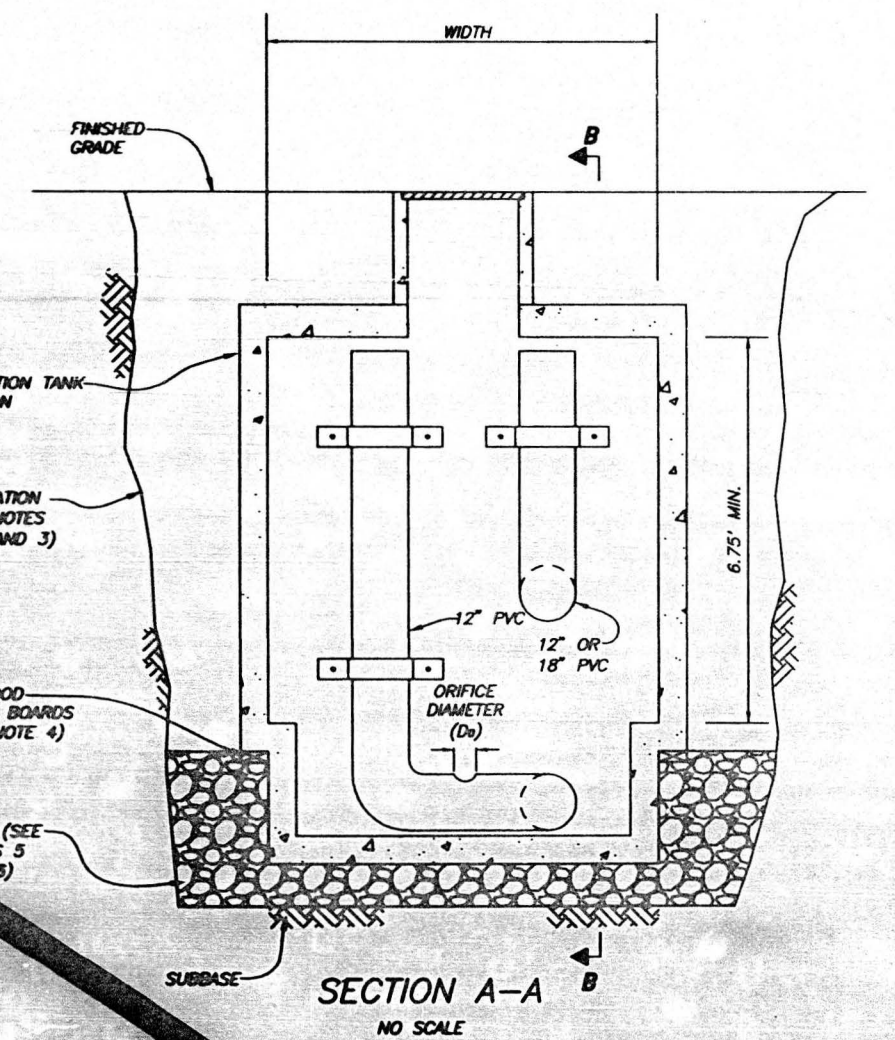
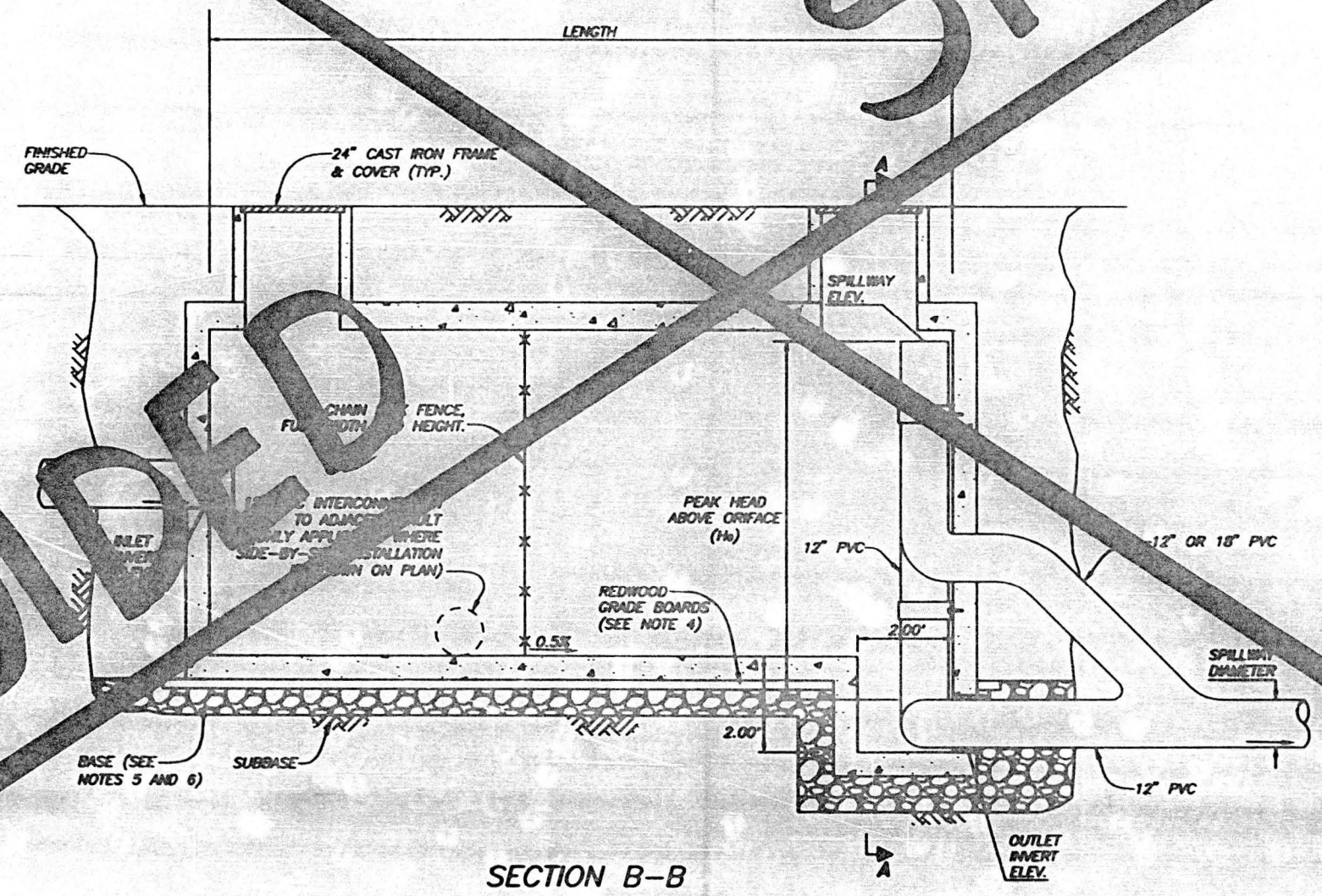
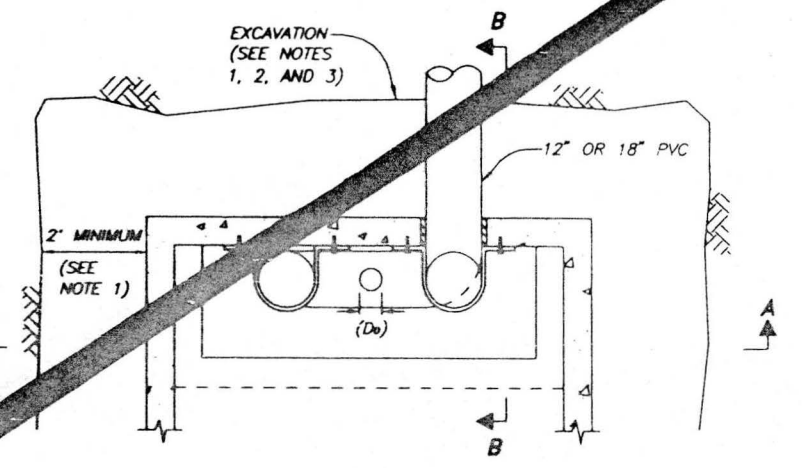
Construction contractor shall be held in accordance with generally accepted construction practices, construction methods and materials, and shall be required to assume sole and complete responsibility for all construction work on this project, including safety of all persons and property. The contractor shall be required to make to the engineer continuously and not be limited to the construction contract further agrees to defend, indemnify and hold the engineer harmless from any and all liability, real or alleged, in connection with the performance of work on this project, accepting liability arising from the sole negligence of design.



UNAUTHORIZED CHANGES & USES: The engineer preparing these plans will not be responsible for, or liable for, unauthorized changes to or uses of these plans. All changes to the plans must be in writing and must be approved by the preparer of these plans.



- NOTES:**
- AREA MUST BE PREPARED AND CLEARED TO 2" MINIMUM SURROUNDING ENTIRE TANK.
 - AREA MUST BE PREPARED AND CLEARED TO 3"x3" IN ANY SEAM OR JOINT AREA PRIOR TO DELIVERY.
 - EXCAVATION SHALL BE PREPARED IN COMPLIANCE WITH ALL STATE AND FEDERAL SAFETY LAWS AND REGULATIONS.
 - PLACE 2"x6" REDWOOD GRADE BOARDS UNDER TANK LENGTHWISE ALONG SIDES. EXTEND BOARDS TO TANK ENDS.
 - BASE MUST BE LEVEL AND EVEN IN ALL DIRECTIONS.
 - BASE MATERIAL TO BE GRANULAR MATERIAL COMPACTED TO 95% RELATIVE DENSITY OR AS SPECIFIED BY A GEOTECHNICAL ENGINEER.
 - STRING LINE OR OTHER SUITABLE MEANS FOR ALIGNING TANK ENDS TO BE PROVIDED AND IN PLACE PRIOR TO INSTALLATION.



WILLIAM A. STEEN & ASSOCIATES
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 8880 LA MESA BLVD., SUITE 102, LA MESA, CALIFORNIA 91841
 (918) 480-2020 • FAX (918) 480-2025
 LICENSED PROFESSIONAL ENGINEER
 CIVIL
 STATE OF CALIFORNIA
 JOB NO. 10-5-07
 DATE 10-5-07
 8247-101



PRIVATE CONTRACT

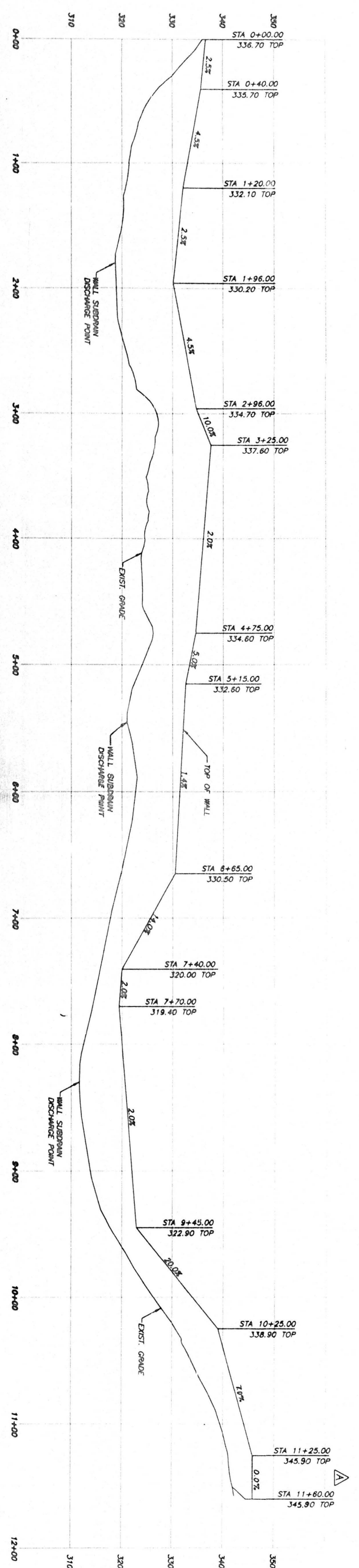
GRADING AND IMPROVEMENT PLANS FOR:

SUMMIT POINTE PLAZA

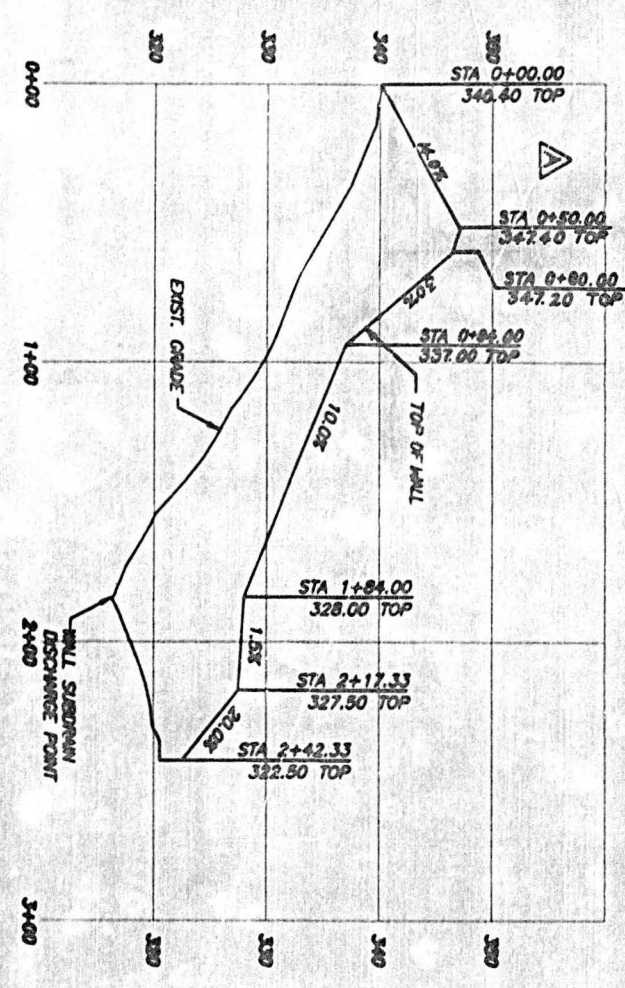
DETECTION FACILITY SPECS. AND DETAILS

CITY OF SAN DIEGO, CALIFORNIA DEVELOPMENT SERVICES DEPARTMENT SHEET 8 OF 32-SHEETS	W.O. NO. 421166 P.T.S. NO. 6100
DATE 08/10/07	T.M. 2781
FOR CITY DEPARTMENT	
DESIGNER WNS	APPROVED [Signature]
DATE 08/14/07	
CHANGE WNS	DATE 08/14/07
AS-BUILTS WNS	DATE 08/14/07
CONTRACTOR LEROY BILMERE DATE SIGNED 1/18/08	32375-6-D
INSPECTOR SCOTT BILMERE DATE COMPLETED 02/20/11	

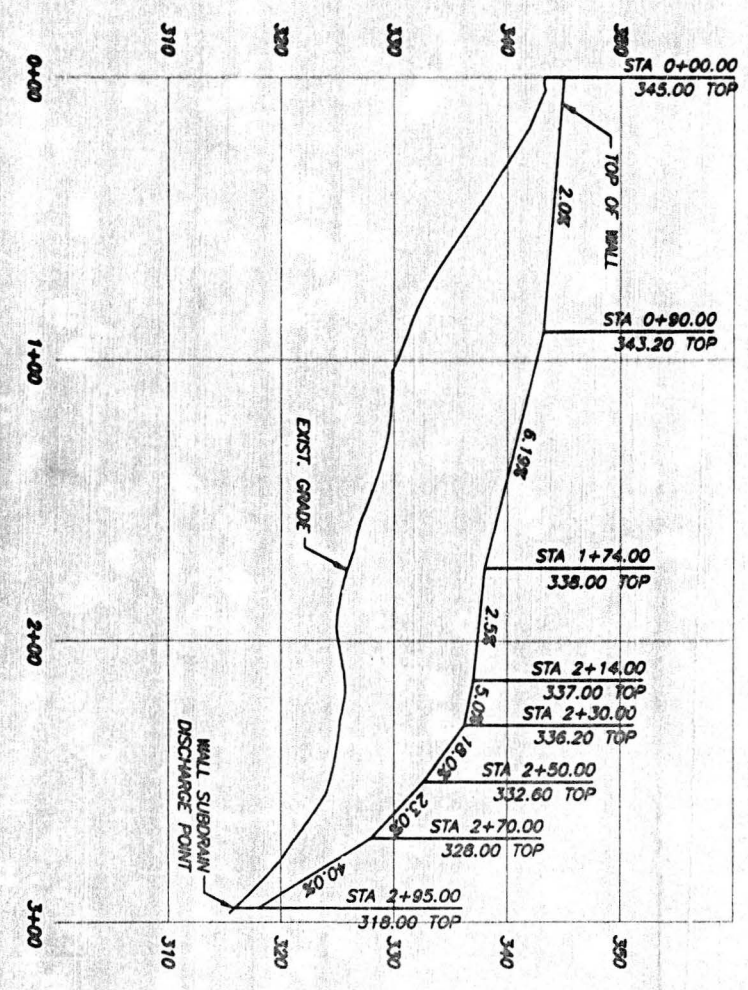
AS-BUILT



PROFILE OF WALL "A"
SCALE: HORZ. 1"=10'
VERT. 1"=10'



PROFILE OF WALL "B"
SCALE: HORZ. 1"=10'
VERT. 1"=10'



PROFILE OF WALL "C"
SCALE: HORZ. 1"=10'
VERT. 1"=10'

NOTE
RETAINING WALLS SHOWN ON THESE PLANS ARE FOR INFORMATION ONLY. A SEPARATE RETAINING WALL AND FOUNDATION DESIGN REPORT WILL BE PROVIDED TO THE SERVICES DEPARTMENT FOR THEIR CONSTRUCTION.

Construction contractor agrees that in accordance with generally accepted construction practices, the contractor shall be responsible for the construction of the wall and shall be liable for any damage to existing structures, utilities, or other property. The contractor shall be responsible for obtaining all necessary permits and approvals from the appropriate authorities. The contractor shall be responsible for the safety of the construction site and shall be liable for any accidents or injuries that may occur. The contractor shall be responsible for the quality of the construction and shall be liable for any defects in the work.



UNAUTHORIZED CHANGES & USES: The engineer's professional seal is required for any changes to these plans. Any changes to these plans must be approved by the engineer of record.



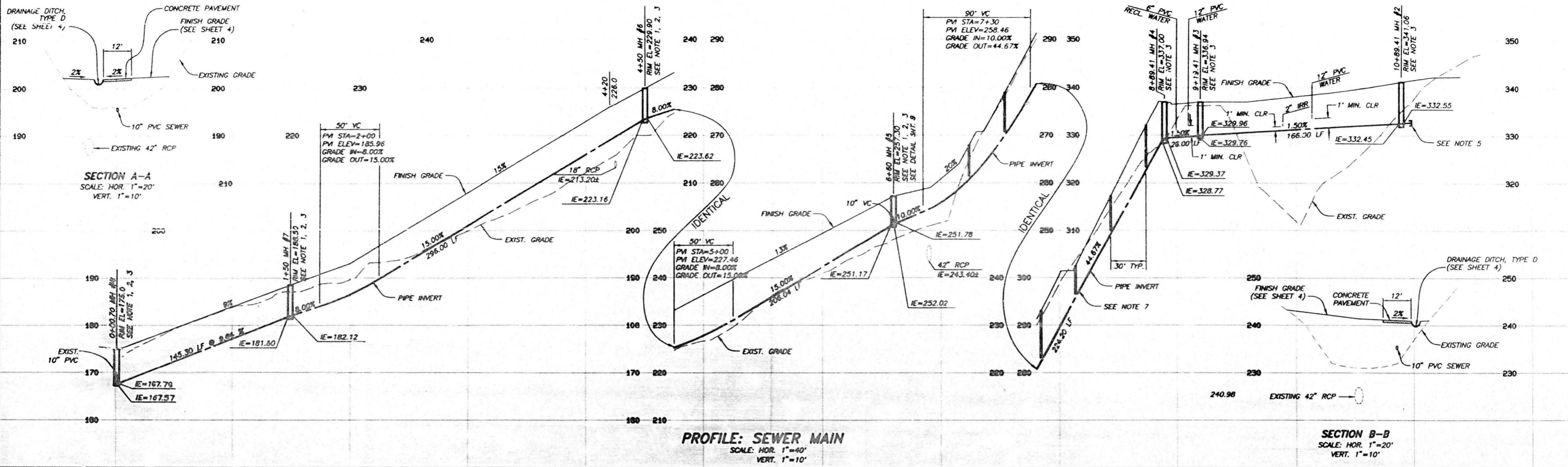
WILLIAM A. STEEN & ASSOCIATES
CONSULTING CIVIL ENGINEER, LAND SURVEYING & PLANNING
2080 LA BREA BLVD., SUITE 102, LA BREA, CALIFORNIA 91141
TEL: 323-733-8888 FAX: 323-733-8889
WWW.WAS-CA.COM
DATE: 02/11/10 DRAWING NO.: 208-101



NO.	DATE	BY	APP'D	CHK'D	REV.
1	10/11/07	WAS			
2	04/07/08	WAS			
3	01/01/09	WAS			
4	01/01/10	WAS			

PROJECT: SUMMIT POINTE PLAZA
CITY OF SAN DIEGO, CALIFORNIA
REVISIONS: AS-BUILT

AS-BUILT



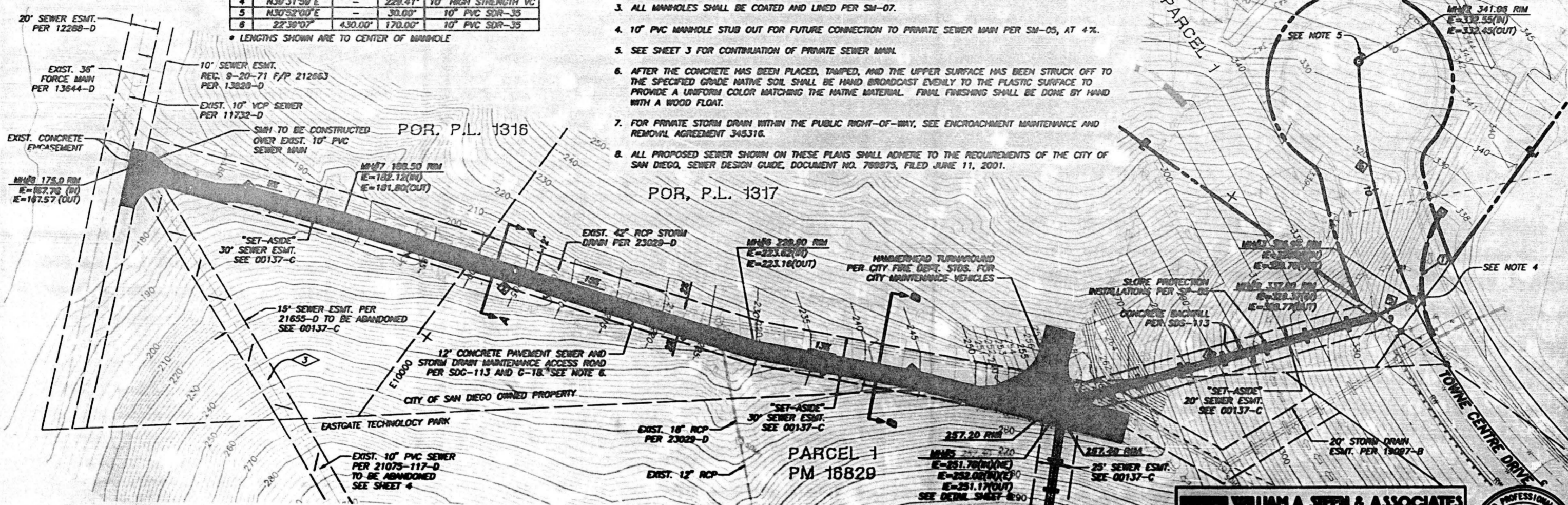
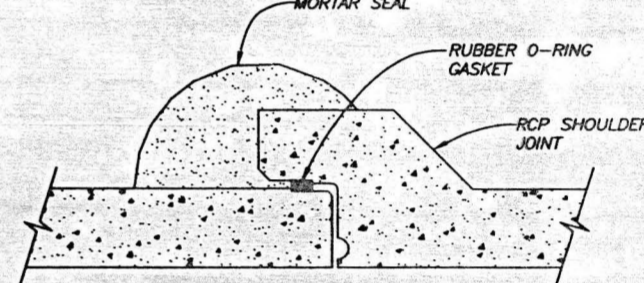
SEWER MAIN DATA			
NO.	DELTA/BEARING	RADIUS	REMARKS
1	N70°08'45"E	100.00'	10" PVC SDR-35
2	N72°10'38"E	300.00'	10" PVC SDR-35
3	N65°26'47"E	210.00'	10" PVC SDR-35
4	N30°31'19"E	223.41'	10" HIGH STRENGTH VC
5	N40°53'00"E	301.00'	10" PVC SDR-35
6	22°30'07"	430.00'	10" PVC SDR-35

* LENGTHS SHOWN ARE TO CENTER OF MANHOLE

- NOTES:**
1. WATERPROOF EXTERIOR WALLS WITH COAL TAR EMULSION APPLIED IN NO LESS THAN TWO COATS FOR A TOTAL DRY FILM THICKNESS OF 25 TO 35 MILS.
 2. ALL MANHOLES LOCATED OUTSIDE OF THE PUBLIC RIGHT-OF-WAY SHALL BE EQUIPPED WITH APPROVED LOCKING COVER WITH COLLARS PER SDR-113.
 3. ALL MANHOLES SHALL BE COATED AND LINED PER SM-07.
 4. 10" PVC MANHOLE STUB OUT FOR FUTURE CONNECTION TO PRIVATE SEWER MAIN PER SM-05, AT 4%.
 5. SEE SHEET 3 FOR CONTINUATION OF PRIVATE SEWER MAIN.
 6. AFTER THE CONCRETE HAS BEEN PLACED, TAMPED, AND THE UPPER SURFACE HAS BEEN STRUCK OFF TO THE SPECIFIED GRADE NATIVE SOIL SHALL BE HAND BROADCAST EVENLY TO THE PLASTIC SURFACE TO PROVIDE A UNIFORM COLOR MATCHING THE NATIVE MATERIAL. FINAL FINISHING SHALL BE DONE BY HAND WITH A WOOD FLOAT.
 7. FOR PRIVATE STORM DRAIN WITHIN THE PUBLIC RIGHT-OF-WAY, SEE ENCROACHMENT MAINTENANCE AND REMOVAL AGREEMENT 345316.
 8. ALL PROPOSED SEWER SHOWN ON THESE PLANS SHALL ADHERE TO THE REQUIREMENTS OF THE CITY OF SAN DIEGO, SEWER DESIGN GUIDE, DOCUMENT NO. 788875, FILED JUNE 11, 2001.

STORM DRAIN DATA (PRIVATE, SEE NOTE 7)**			
NO.	DELTA/BEARING	RADIUS	LENGTH
1	S6°01'21"	90.00'	88.00'

* 8" LENGTHS 5' BEVEL ONE END
** SEE STORM DRAIN PROFILE ON SHEET 9



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6880 LA MESA BLVD., SUITE 102, LA MESA, CALIFORNIA 91941
(619) 460-9000 • FAX (619) 460-9005

DATE: 10-5-07
JOB NO.: 6247-101

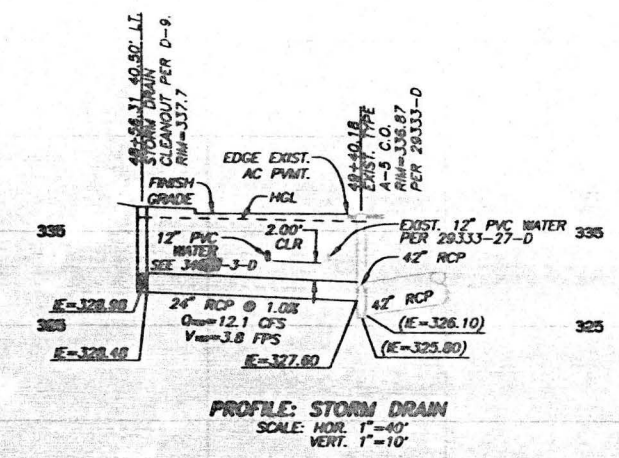
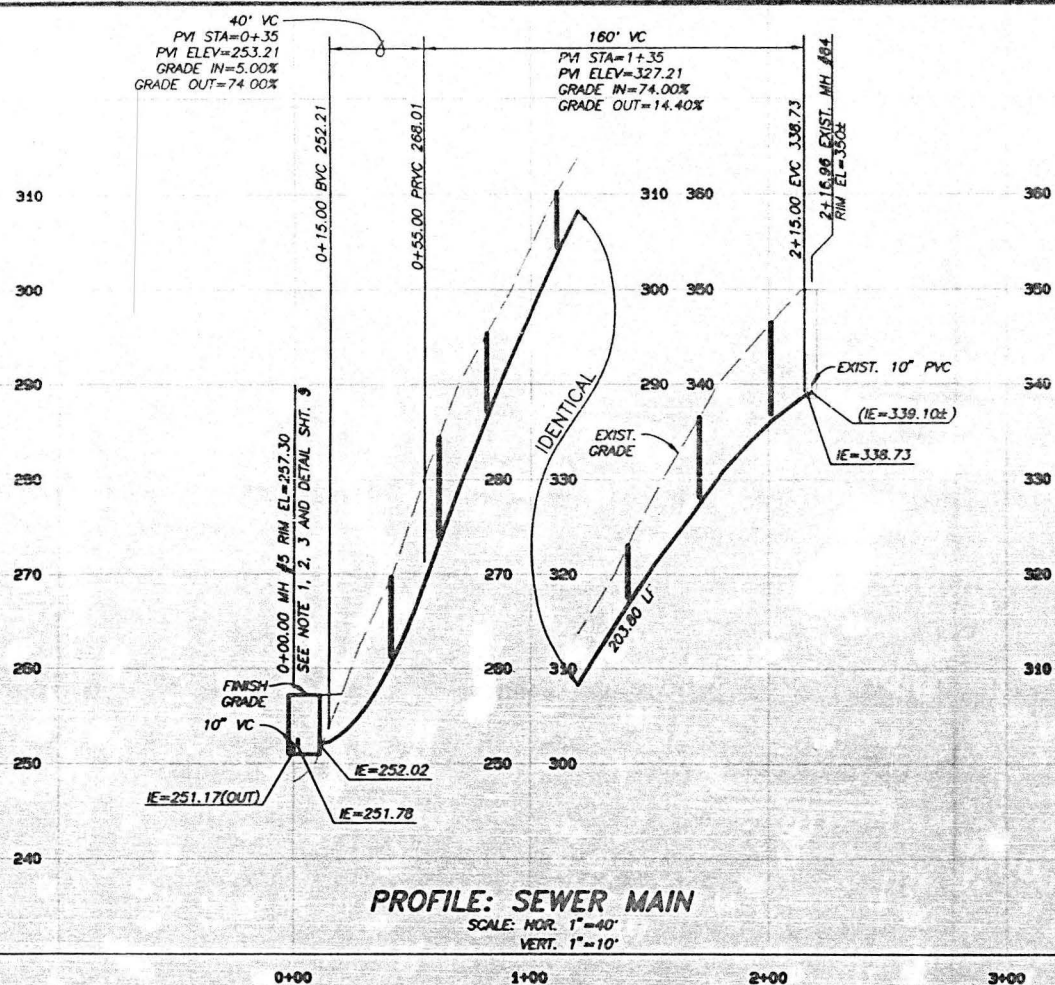


PRIVATE CONTRACT
IMPROVEMENT PLANS FOR:

**SUMMIT POINTE PLAZA
10" SEWER MAIN & PVT. STORM DRAIN**

CITY OF SAN DIEGO, CALIFORNIA DEVELOPMENT SERVICES DEPARTMENT SHEET 8 OF 32 SHEETS		W.D. NO. 421169 P.T.S. NO. 8109
DATE: 10/17/07	DATE FILMED: 10/17/07	T.M. 2781
FOR CITY ENGINEER	APPROVED	DATE
DESCRIPTION BY: WMS	DATE: 10/17/07	DATE: 10/17/07
AS-BUILTS: PMS	DATE: 6/11/10	LABORATORY COORDINATES: 32375-8-D
CONTRACTOR: LEGACY BUILDING	DATE STARTED: 1/03/08	
INSPECTOR: SERGIO TORRES	DATE COMPLETED: 6/30/11	

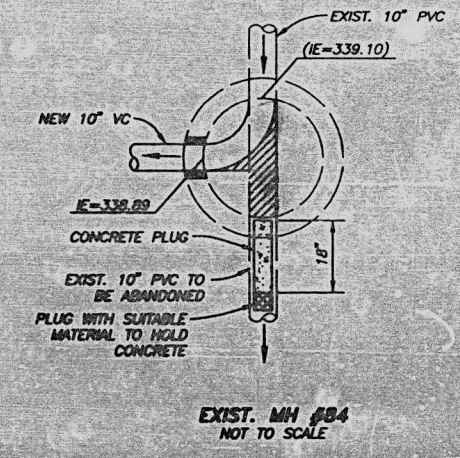
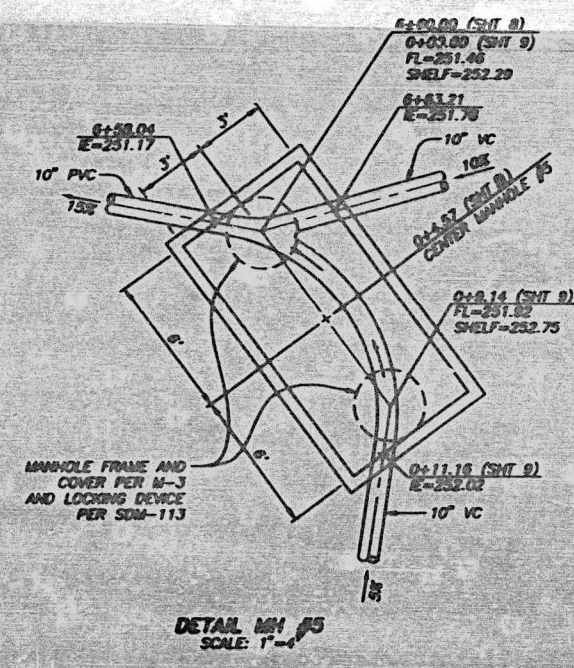
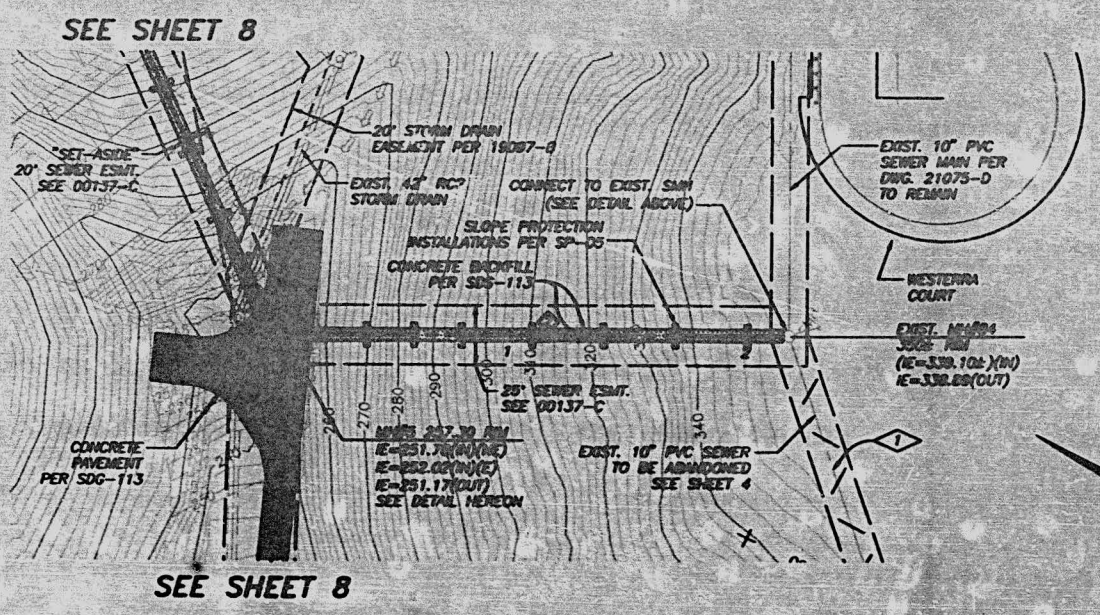
AS-BUILT



NO.	DELTA/BEARING	RADIUS	LENGTH	REMARKS
1	N71°24'04"W	—	9.14'	SEE DETAIL MH'S HEREON
2	M89°30'21"W	—	207.82'	10" HIGH STRENGTH VC

* LENGTHS SHOWN ARE TO CENTER OF MANHOLE

- NOTES**
1. WATERPROOF EXTERIOR WALLS WITH COAL TAR EMULSION APPLIED IN NO LESS THAN TWO COATS FOR A TOTAL DRY FILM THICKNESS OF 25 TO 35 MILS.
 2. ALL MANHOLES LOCATED OUTSIDE OF THE PUBLIC RIGHT-OF-WAY SHALL BE EQUIPPED WITH APPROVED LOCKING COVER WITH COLLARS PER SDM-113.
 3. ALL MANHOLES SHALL BE COATED AND LINED PER SM-07.
 4. ALL PROPOSED SEWER SHOWN ON THESE PLANS SHALL ADHERE TO THE REQUIREMENTS OF THE CITY OF SAN DIEGO, SEWER DESIGN GUIDE, DOCUMENT NO. 768075, FILED JUNE 11, 2001.



Construction contractor agrees that in accordance with generally accepted construction practices, construction contractor will be required to assume sole and complete responsibility for job site conditions during the course of construction of the project, including safety of all persons and property; that this requirement shall be made to apply continuously and not be limited to normal working hours, and construction contractor further agrees to defend, indemnify and hold design professional harmless from any and all liability, real or alleged, in connection with the performance of work on this project, accepting liability arising from the sole negligence of design professional.

CEL SOC

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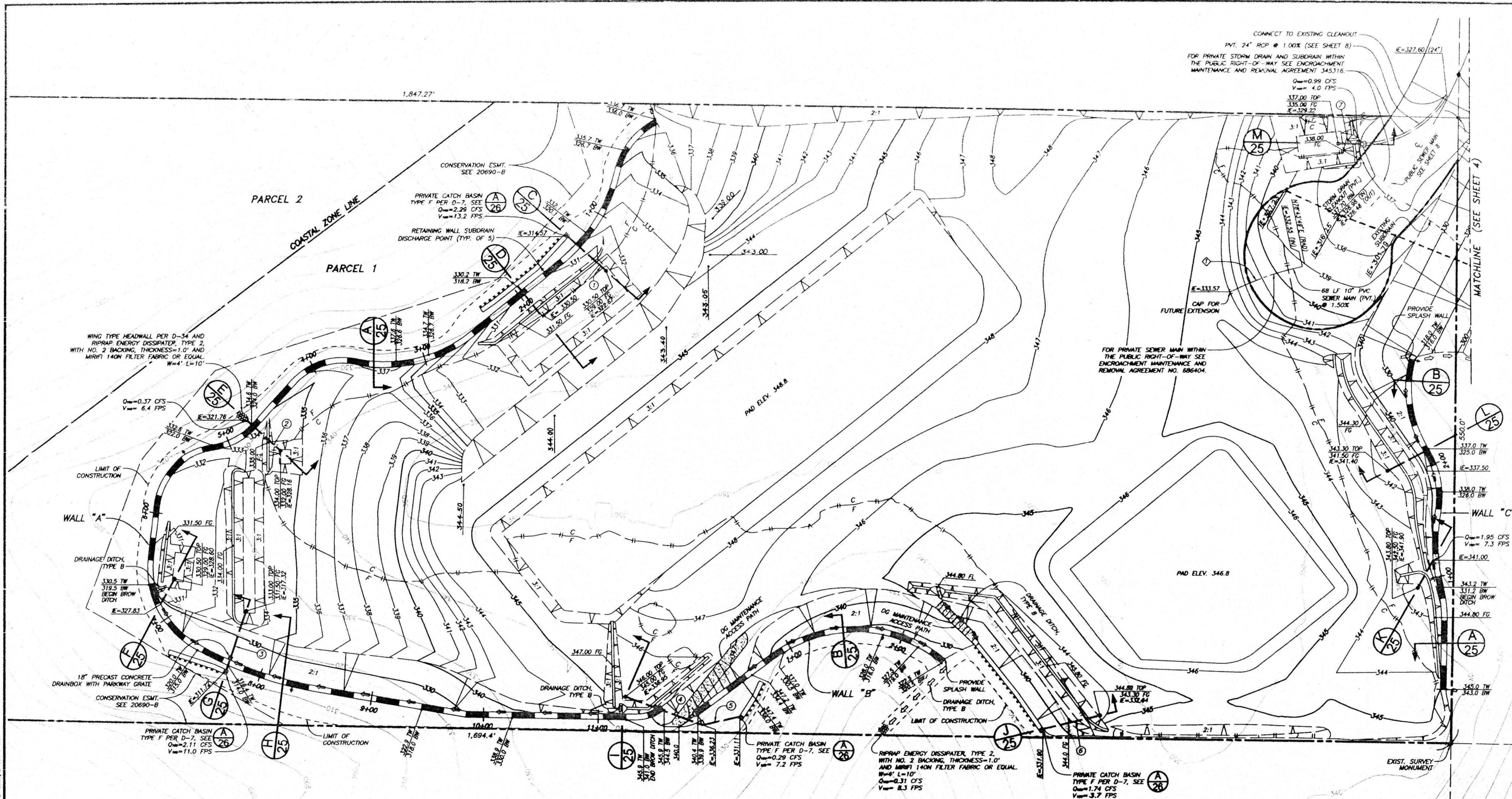
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WILLIAM A. JENSEN & ASSOCIATES
CONSULTING CIVIL ENGINEERS, LAND SURVEYING & PLANNING
2000 LA MEZA BLVD., SUITE 102, LA MEZA, CALIFORNIA 91941
TEL: 619-440-0000 • FAX: (619) 440-0000

AS-BUILT



PRIVATE CONTRACT			
IMPROVEMENT PLANS FOR:			
SUMMIT POINTE PLAZA			
10" SEWER MAIN & PVT. STORM DRAIN			
CITY OF SAN DIEGO, CALIFORNIA		W.A. NO. 521199	
DEVELOPER: SUMMIT DEVELOPMENT		P.T.S. NO. 8109	
SHEET # 65-00000002		DATE: 10/17/17	
FOR CIVIL ENGINEER:	DATE:	T.M.	2/81
DESIGNER:	APPROVED:	DATE:	28 10 17
GENERAL:	DATE:	DATE:	DATE:
AS-BUILT:	DATE:	DATE:	DATE:
CONTRACTOR: JENSEN ENGINEERS AND ARCHITECTS - JENSEN		32375-9-D	



SEWER MAIN DATA				
NO.	DELTA/BEARING	RADIUS	LENGTH	REMARKS
1	180°/34"	250.00'	70.00'	10" PVC SDR-35 (PVT.)

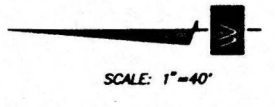
* LENGTHS SHOWN ARE TO CENTER OF MANHOLE

STORM DRAIN DATA (PVT.)			
NO.	LENGTH	SLOPE	REMARKS
1	45.00'	18.00%	18" PVC
2	40.00'	16.00%	8" PVC
3	56.00'	10.00%	12" PVC
4	72.00'	7.00%	12" PVC
5	32.00'	16.00%	12" PVC
6	57.00'	0.80%	18" PVC
7	20.00'	1.20%	18" PVC

Construction contractor agrees that in accordance with generally accepted construction practices, construction contractor shall be required to assume sole and complete responsibility for job site conditions during the course of construction of the project, including safety of all persons and property; that this requirement shall be made in every contract, and not be limited to normal working hours, and construction contractor further agrees to defend, indemnify and hold design professional harmless from any and all liability, real or alleged, in connection with the performance of work on this project, excepting liability arising from the sole negligence of design professional.



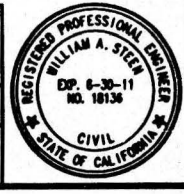
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WS WILLIAM A. STEEN & ASSOCIATES
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8080 LA MESA BLVD., SUITE 102, LA MESA, CALIFORNIA 91941
(619) 480-8000 • FAX (619) 480-8005

ENGINEER: *William A. Steen* P.E. 09
WILLIAM A. STEEN R.C.E. 18136 DATE: 6/24/09

JOB NO. 6247-101



PRIVATE CONTRACT

GRADING PLANS FOR:

SUMMIT POINTE PLAZA

LOT "A", PL. 1300, SEC 17&22
CITY OF SAN DIEGO, CALIFORNIA #.D. NO. 421186
DEVELOPMENT SERVICES DEPARTMENT P.T.S. NO. 6189
SHEET 24 OF 28 SHEETS

FOR CITY ENGINEER: DATE: 11/27/05 T.M. 2781

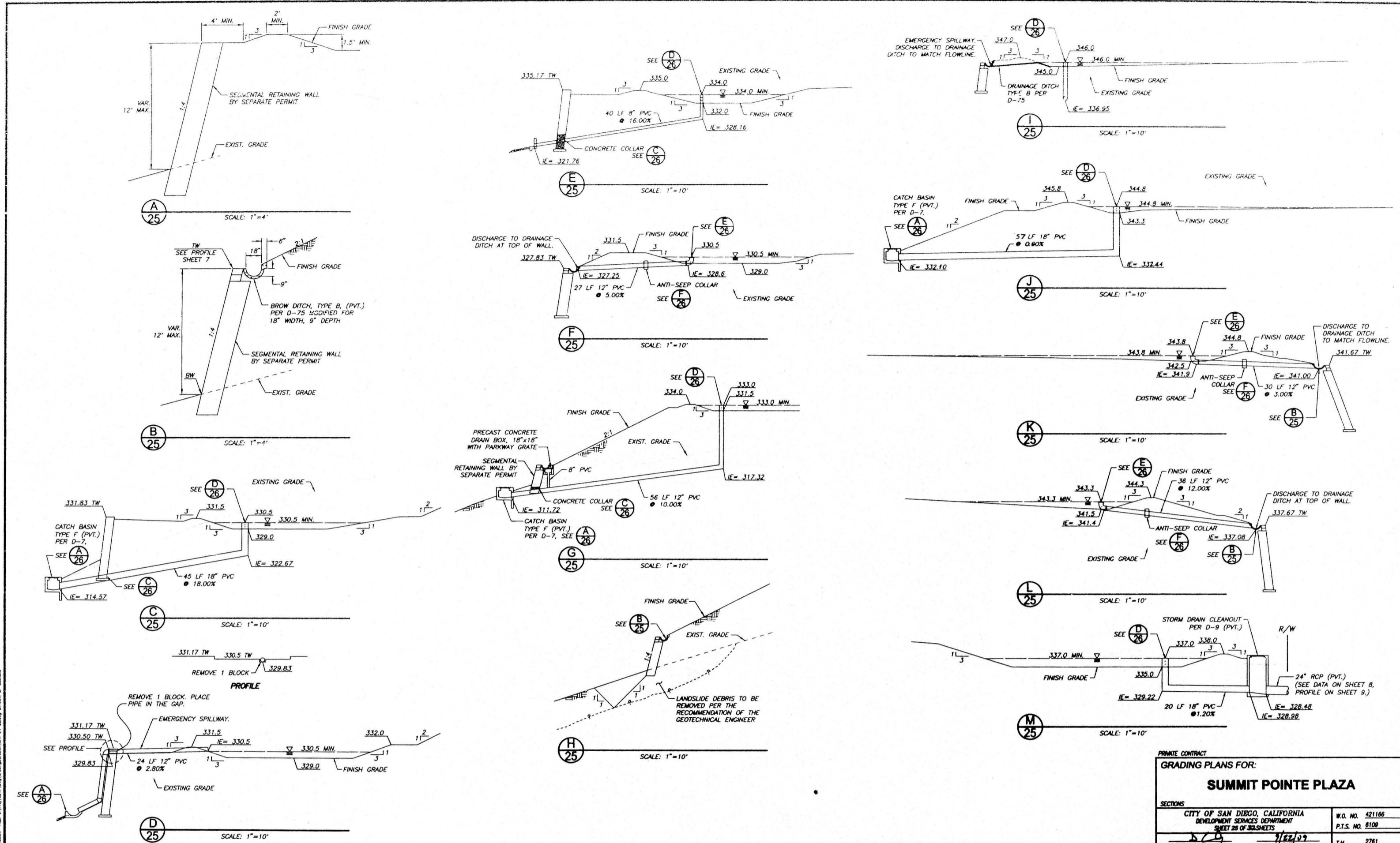
DESCRIPTION	BY	APPROVED	DATE	FILED
ORIGINAL	WAS		6-24-09	

AS-BUILT: PWS: *WAS* (11/27/05) 09-02-09
CONTRACTOR: *LEBBY BILBIE* DATE STARTED: 1/28/08
INSPECTOR: *SEYMUR BELZUE* DATE COMPLETED: 8/20/08

1904-6267
1904-1708
LAMBERT COORDINATES: 32375-24-D

NEW SHEET AS-BUILT

COMPARE WITH THE ORIGINAL. BEST QUALITY MATERIALS. EXCESSIVE GRAY MATTER. MAY CAUSE YOUR QUALITY IMPROVEMENT.



Construction contractor agrees that in accordance with generally accepted construction practices, construction contractor will be required to assume sole and complete responsibility for all conditions during the course of construction of the project, including safety of all persons on the job site, and that this requirement shall be made to apply continuously and not be limited to normal working hours, and construction contractor further agrees to defend, indemnify and hold design professional harmless from any and all liability, real or alleged, in connection with the performance of work on this project, excepting liability arising from the sole negligence of design professional.



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8080 LA MESA BLVD., SUITE 102, LA MESA, CALIFORNIA 91941
(619) 460-8000 • FAX (619) 460-8000

ENGINEER'S SEAL: WILLIAM A. STEEN, CIVIL, No. 18136, DATE 2-21-09

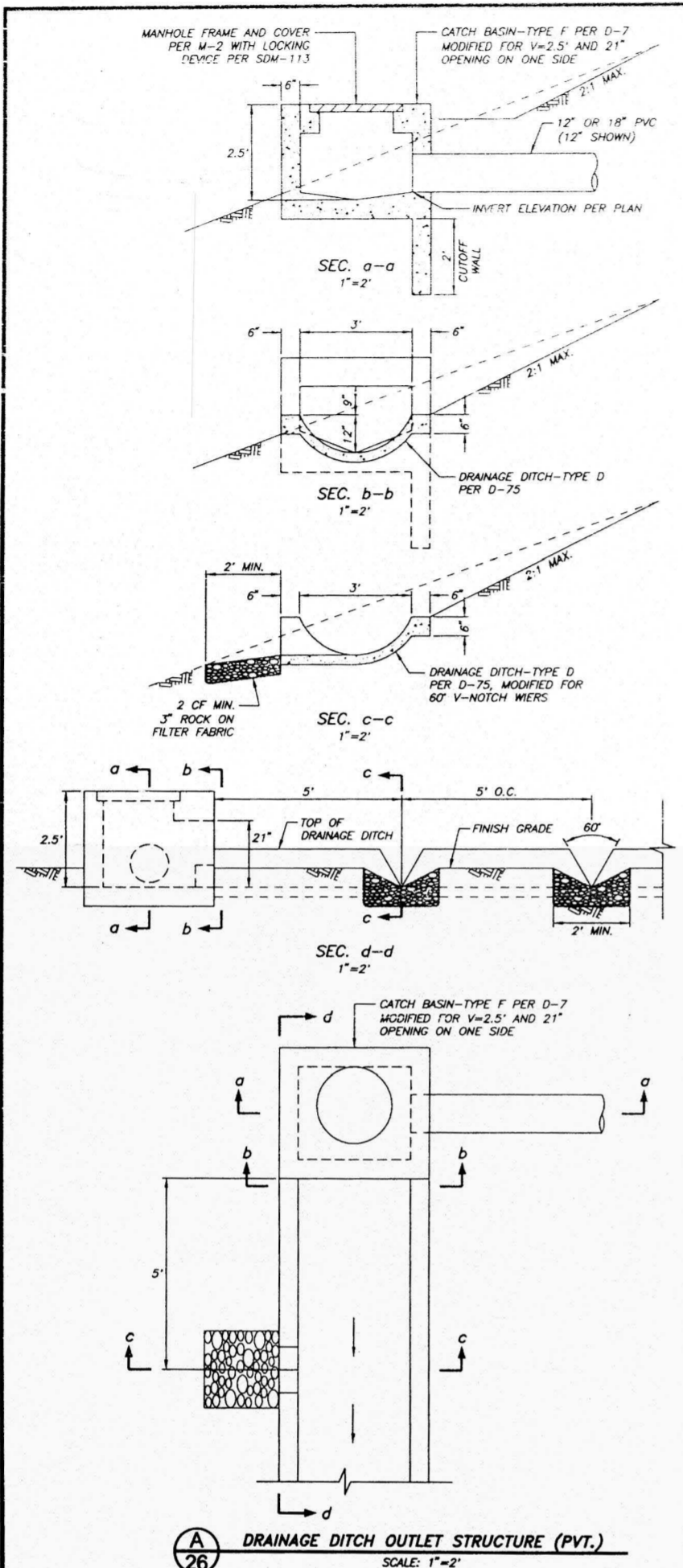


PRIVATE CONTRACT
GRADING PLANS FOR:
SUMMIT POINTE PLAZA

SECTIONS	CITY OF SAN DIEGO, CALIFORNIA DEVELOPMENT SERVICES DEPARTMENT SHEET 25 OF 33 SHEETS	W.O. NO. 421166 P.T.S. NO. 8106
FOR CITY ENGINEER	DATE 1/22/09	T.M. 2781
DESCRIPTION BY	APPROVED	DATE FILED
ORIGINAL	WAS	11-24-10
AS-BUILT	WAS	5-3-11
CONTRACTOR LEGACY BUILDING DATE STARTED	1/23/08	32375-25-D
INSPECTOR SERGIO FIGUEROA	DATE COMPLETED 8/30/11	

NEW SHEET AS-BUILT



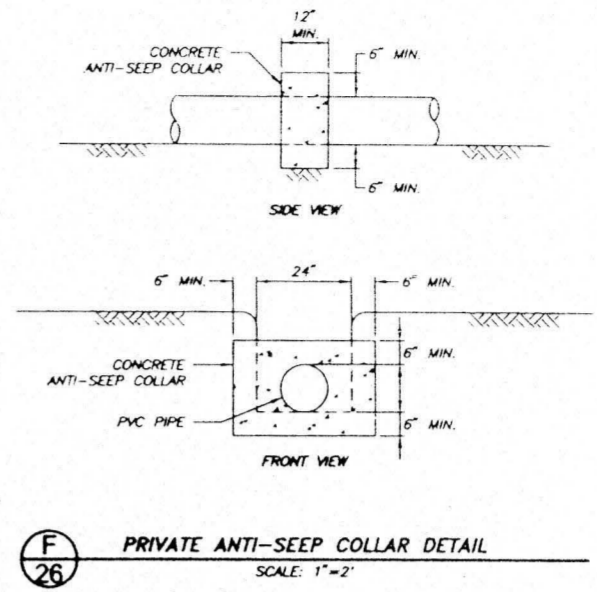
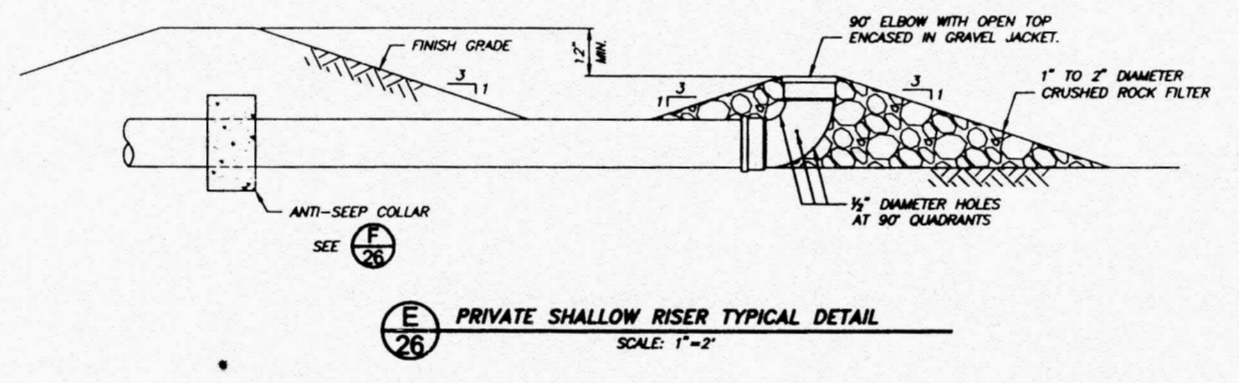
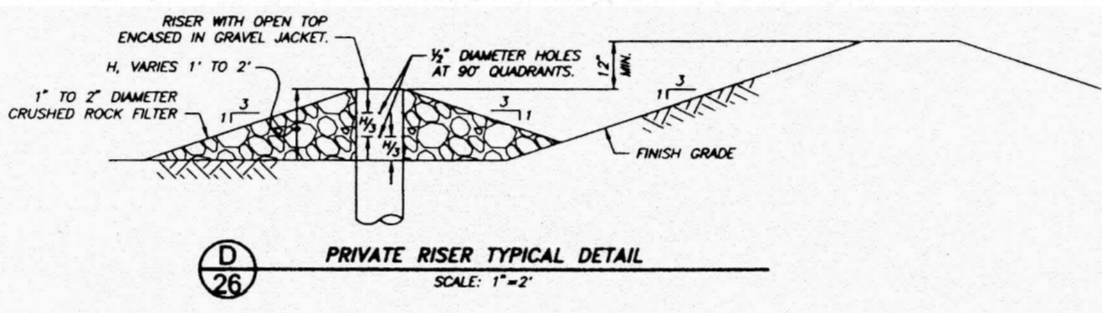
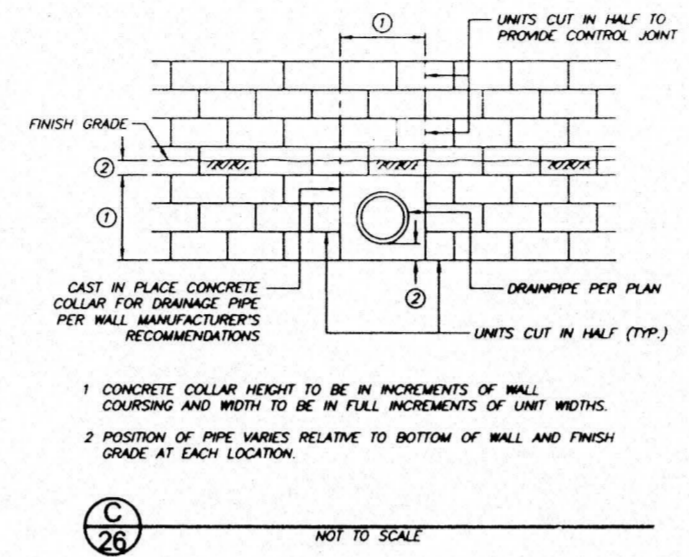
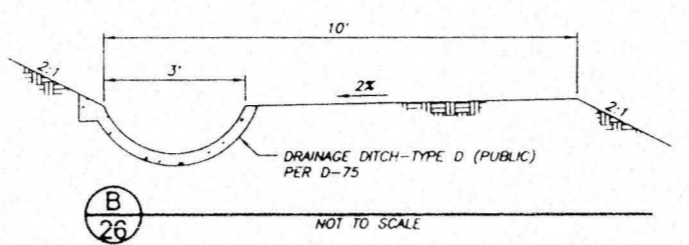


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CEL SOC



WS WILLIAM A. STEEN & ASSOCIATES

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8080 LA MESA BLVD., SUITE 102, LA MESA, CALIFORNIA 91941

☎ (619) 480-8000 ☎ FAX (619) 480-8000

ENGINEER OF WORK: *[Signature]* JOB NO. 6247-101

WILLIAM A. STEEN R.C.E. 18138 DATE



PRIVATE CONTRACT

GRADING PLANS FOR:

SUMMIT POINTE PLAZA

DETAILS			
CITY OF SAN DIEGO, CALIFORNIA		W.G. NO. 521166	
DEVELOPMENT SERVICES DEPARTMENT		P.T.S. NO. E109	
SHEET 26 OF 26 SHEETS			
FOR CITY ENGINEER	APPROVED	DATE	FILED
ORIGINAL	MS	11-14-10	
		1804-6283	
		AND 83 COORDINATES	
		284-1783	
AS-BUILTS	PHS	5-2	10/10/10 11-27-10
CONTRACTOR <i>[Signature]</i> DATE SHOWN 11/10/10		LAMBERT COORDINATES	
INSPECTOR <i>[Signature]</i> DATE COMPLETED 11/24/10		32375-26-D	

NEW SHEET AS-BUILT