



Thienes Engineering, Inc.

CIVIL ENGINEERING • LAND SURVEYING

**PRELIMINARY HYDROLOGY
CALCULATIONS**

FOR

VALLEY BOULEVARD INDUSTRIAL BUILDING
VALLEY BLVD. BETWEEN WILLOW AVE. AND LILAC AVE.
RIALTO, CALIFORNIA

PREPARED FOR

QR BIRTCHEW WILLOW AVE OWNER LLC
450 NEWPORT CENTER DRIVE, SUITE 220
NEWPORT BEACH, CA 92660
PHONE: (949) 440-1052

DECEMBER 23, 2019
REVISED FEBRUARY 05, 2020
REVISED FEBRUARY 20, 2020
REVISED AUGUST 22, 2020
REVISED DECEMBER 22, 2020
REVISED JULY 6, 2021

JOB NO. 3836

PREPARED BY

THIENES ENGINEERING
14349 FIRESTONE BOULEVARD
LA MIRADA, CALIFORNIA 90638
P. (714) 521-4811
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PRELIMINARY HYDROLOGY CALCULATIONS

FOR

VALLEY AND WILLOW

PREPARED BY TONY NUÑEZ
UNDER THE SUPERVISION OF



 7/6/21
REINHARD STENZEL DATE:
R.C.E. 56155
EXP. 12/31/22

INTRODUCTION

A: PROJECT LOCATION

The project site is located on the north side of Valley Boulevard and west of Willow Avenue in the City of Rialto, California. Please see following page for vicinity map.

B: STUDY PURPOSE

The purpose of this study is to determine the 100-year existing condition and proposed condition discharges from the project site that ultimately drains to an existing Caltrans maintained concrete channel adjacent to the Interstate 10 Freeway.

C: PROJECT STAFF:

Thienes Engineering staff involved in this study include:

Reinhard Stenzel

Tony Nuñez



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"VICINITY MAP"

FOR
VALLEY BOULEVARD INDUSTRIAL BUILDING
W. VALLEY BLVD AND S. WILLOW AVE. RIALTO, CA



DISCUSSION

Project Description

The project site encompasses approximately 21.00 acres. Improvements to the site include a warehouse type building that is 494,194 square feet. There will be a truck yard on the east side of the proposed building. Vehicle parking will be on the north, west, and south sides of the project. Proposed landscaping will be street adjacent and throughout the site.

Master Plan of Drainage

The City of Rialto Storm Drain Master Plan dated May 19, 2010, delineates proposed storm drain in Valley Boulevard and Willow Avenue. The proposed storm drain will connect to the existing Caltrans maintained concrete channel adjacent to the interstate 10 Freeway. Please see Appendix "A" for Master Drainage Plan and other pertinent reference materials.

Existing Conditions

The project site consists of undeveloped dirt lots that are used for vehicle, equipment, and miscellaneous storage. The barren land is sufficiently compact. The site generally surface drains to the southeast and discharges into Willow Avenue through a parkway culvert. Stormwater is collected in a catch basin that is located south of the parkway culvert. A box culvert carries drainage to the south, under the intersection of Willow Avenue and Valley Boulevard. The stormwater discharges from a culvert in Willow Avenue, continues south via concrete curb and gutter, and spills into the Caltrans maintained concrete channel adjacent to the Interstate 10 Freeway.

The existing condition 100-year peak flow rate from the project site is approximately 39.4 cfs (Node 103).

See Appendix "B" for existing condition hydrology calculations and Appendix "C" for existing condition hydrology map.

Off Site Run-on

Under existing conditions, the project site is currently accepting offsite flows from an adjacent property in the northwest section of the site. The flows enter the site via spillover from a retention basin. The existing condition 100-year peak flow rate from the neighboring property is approximately 19.4 cfs. These flows will be conveyed by a proposed u-channel and storm drain pipe that runs south along the project's westerly property line and will "burp out" a catch basin and parkway drains into Valley Boulevard. A sump pump will drain residual flow that is stored in the catch basin and pipe.

Proposed Conditions

Drainage is collected in catch basins throughout the site. A proposed storm drain system, Line "A", conveys storm water from the northeastern portion of the building to the north, then westerly around the building collecting runoff from the north drive aisle (nodes 100-110), and then south to the west truck yard. The runoff from the western portion of the building and the truck yard is collected in a series of grates (nodes 200-202). The approximate 100 year peak flow rate at node 202 is approximately 36.4 cfs, undetained. The private storm drain continues easterly in the southerly vehicle parking collecting runoff from southern drive aisle and the southeast portion of the site (nodes 210-213). The private storm drain will discharge into the existing public catch basin at the northwest corner of the intersection of Willow Avenue and Valley Boulevard. The total 100 year peak flow rate from the project site is approximately 52.6 cfs.

See Appendix "B" for proposed condition hydrology calculations, Appendix "C" for proposed condition hydrology map and storm drain plans.

Proposed Public Storm Drain Conditions

The runoff will be directed into a proposed 30" RCP which replaces an existing 18"x24" RCB storm drain that discharges at the southwest corner of Valley and Willow. The proposed 30" RCP will transition to a 42" RCP at the northwest corner of Valley and Willow. It will continue southerly in Willow and connect to the existing Caltrans maintained concrete channel where runoff will discharge.

Methodology

The San Bernardino County Rational Method program (AES Software) was used for hydrology calculations. The site is composed of soil type "A" per the San Bernardino County Hydrology Manual. See Appendix "A" for pertinent reference materials. The Flood Routing Analysis program (also AES Software) for San Bernardino County was used for hydrograph and detention calculations.

APPENDIX

DESCRIPTION

A

REFERENCE MATERIAL

B

HYDROLOGY CALCULATIONS

C

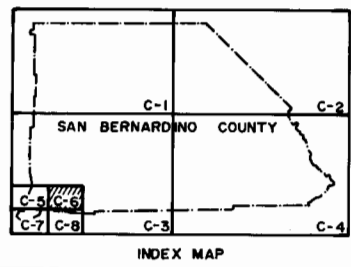
HYDROLOGY MAPS

APPENDIX A

REFERENCE MATERIAL



Project Site

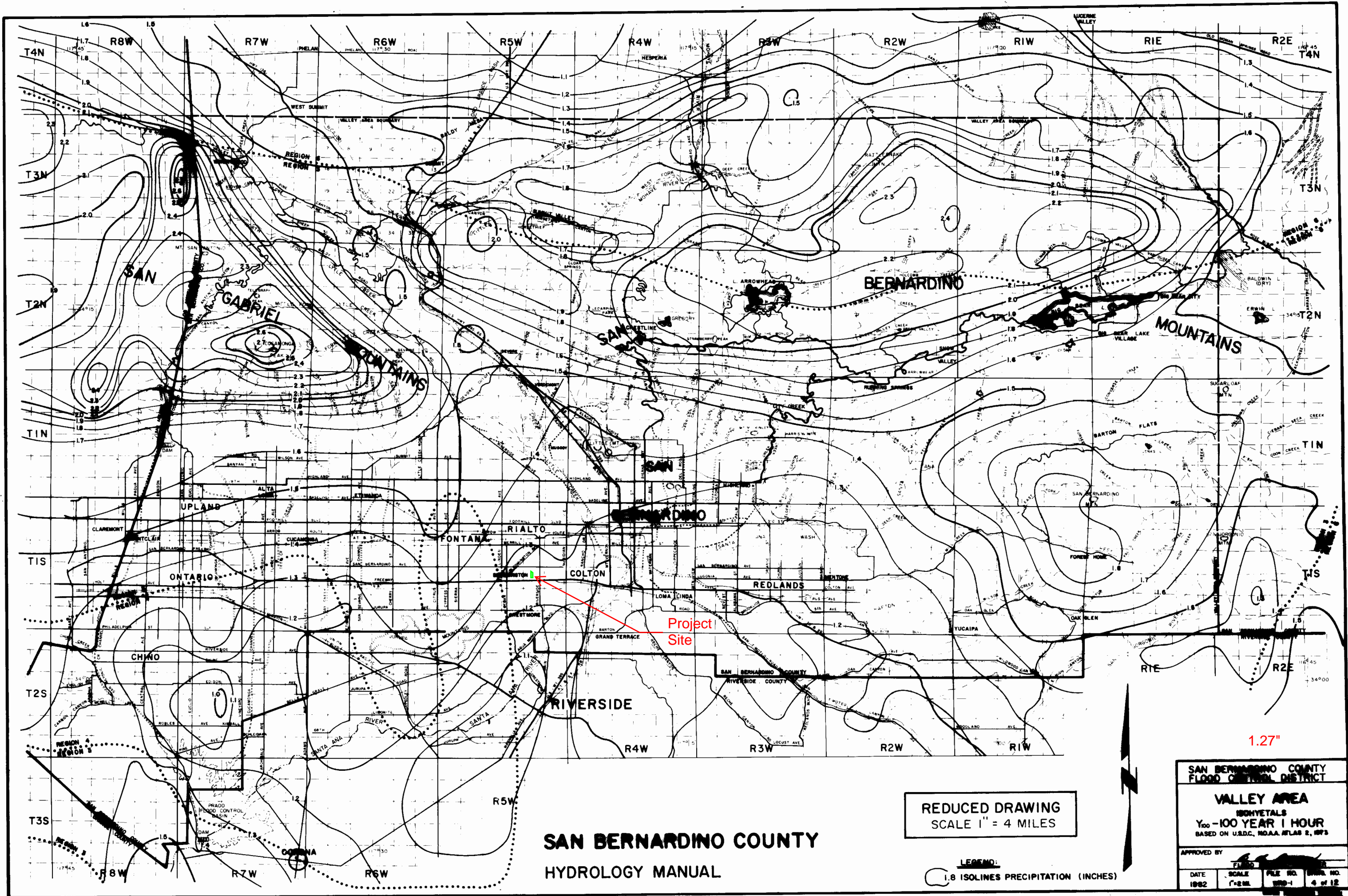


- LEGEND
- SOIL GROUP BOUNDARY
 - A SOIL GROUP DESIGNATION
 - - - BOUNDARY OF INDICATED SOURCE

SCALE 1:48,000
SCALE REDUCED BY 1/2

SAN BERNARDINO COUNTY
 HYDROLOGY MANUAL

HYDROLOGIC SOILS GROUP MAP
 FOR
SOUTHWEST-B AREA



**SAN BERNARDINO COUNTY
HYDROLOGY MANUAL**

**REDUCED DRAWING
SCALE 1" = 4 MILES**

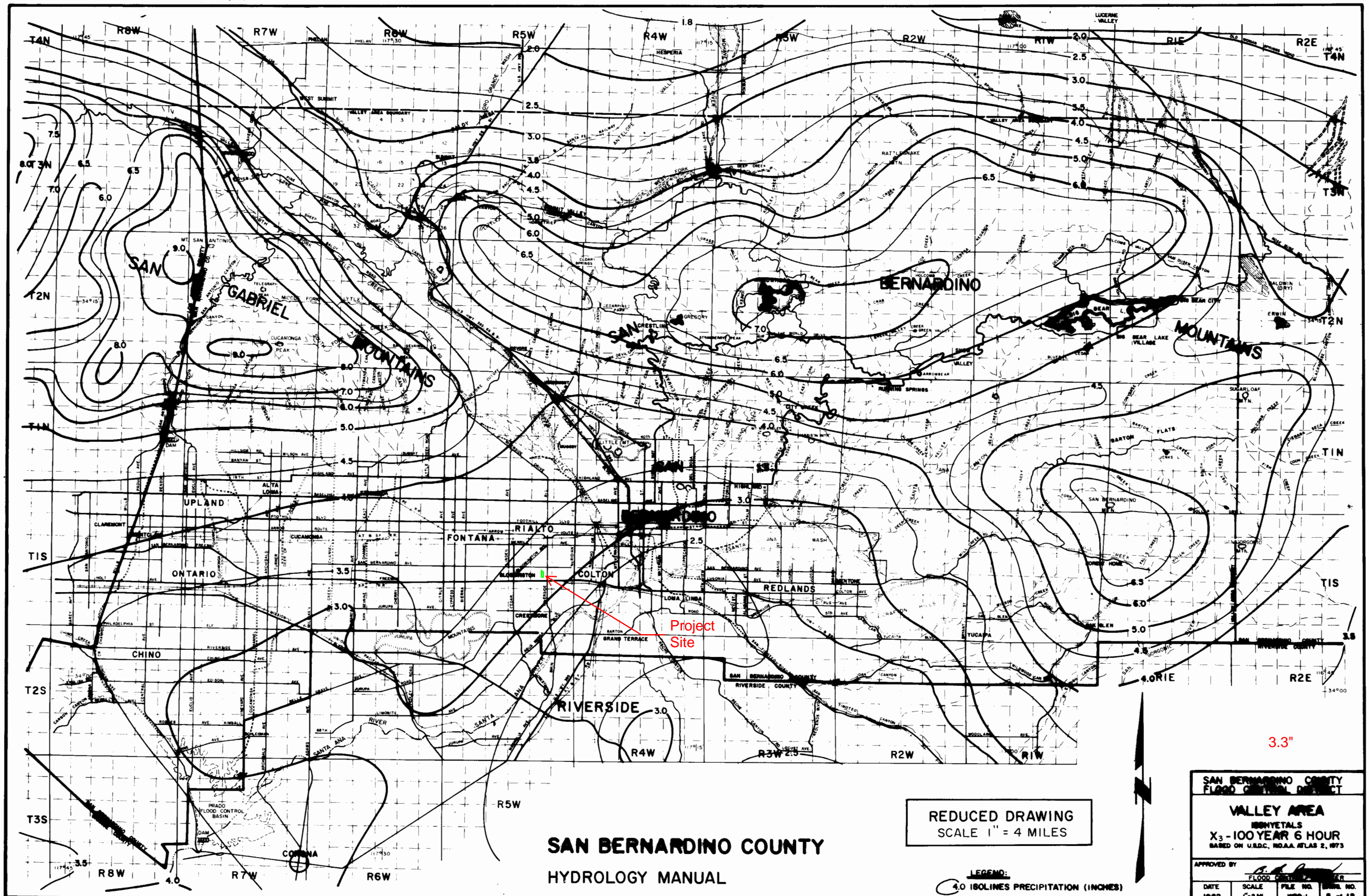
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1.8 ISOLINES PRECIPITATION (INCHES)**

**SAN BERNARDINO COUNTY
FLOOD CONTROL DISTRICT**

**VALLEY AREA
ISOHYETALS
Y₁₀₀-100 YEAR 1 HOUR
BASED ON U.S.D.C. NOAA ATLAS 2, 1973**

APPROVED BY: _____

DATE	SCALE	FILE NO.	DRAW. NO.
1982	1"=4 MI.	WB-1	4 of 12



SAN BERNARDINO COUNTY
HYDROLOGY MANUAL

REDUCED DRAWING
 SCALE 1" = 4 MILES

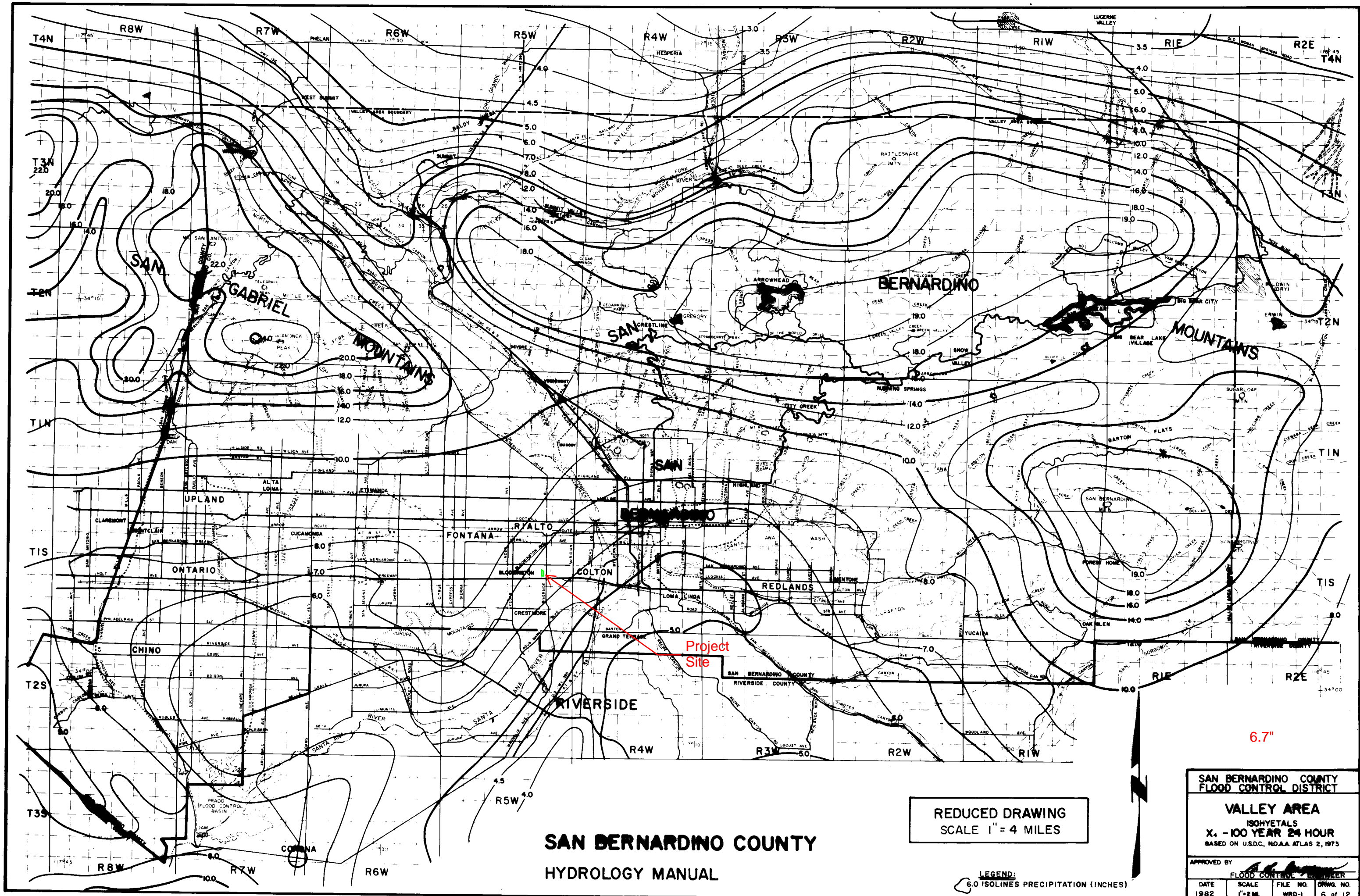
LEGEND:
 4.0 ISOLINES PRECIPITATION (INCHES)

SAN BERNARDINO COUNTY
 FLOOD CONTROL DISTRICT

VALLEY AREA
 ISOHYETALS
 X₃ - 100 YEAR 6 HOUR
 BASED ON U.S.D.C. NOAA ATLAS 2, 1973

APPROVED BY: *[Signature]*

DATE	SCALE	FILE NO.	DRAW. NO.
1982	1"=2 M.	WB-1	5 of 12



**SAN BERNARDINO COUNTY
HYDROLOGY MANUAL**

**REDUCED DRAWING
SCALE 1" = 4 MILES**

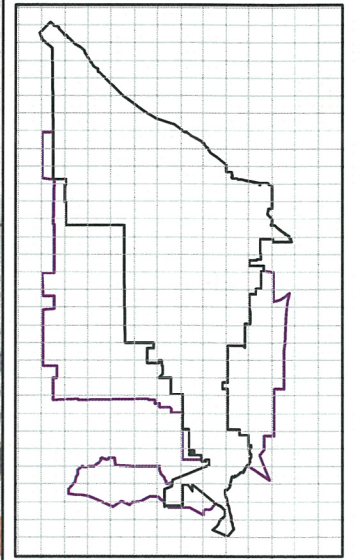
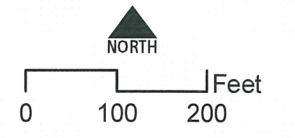
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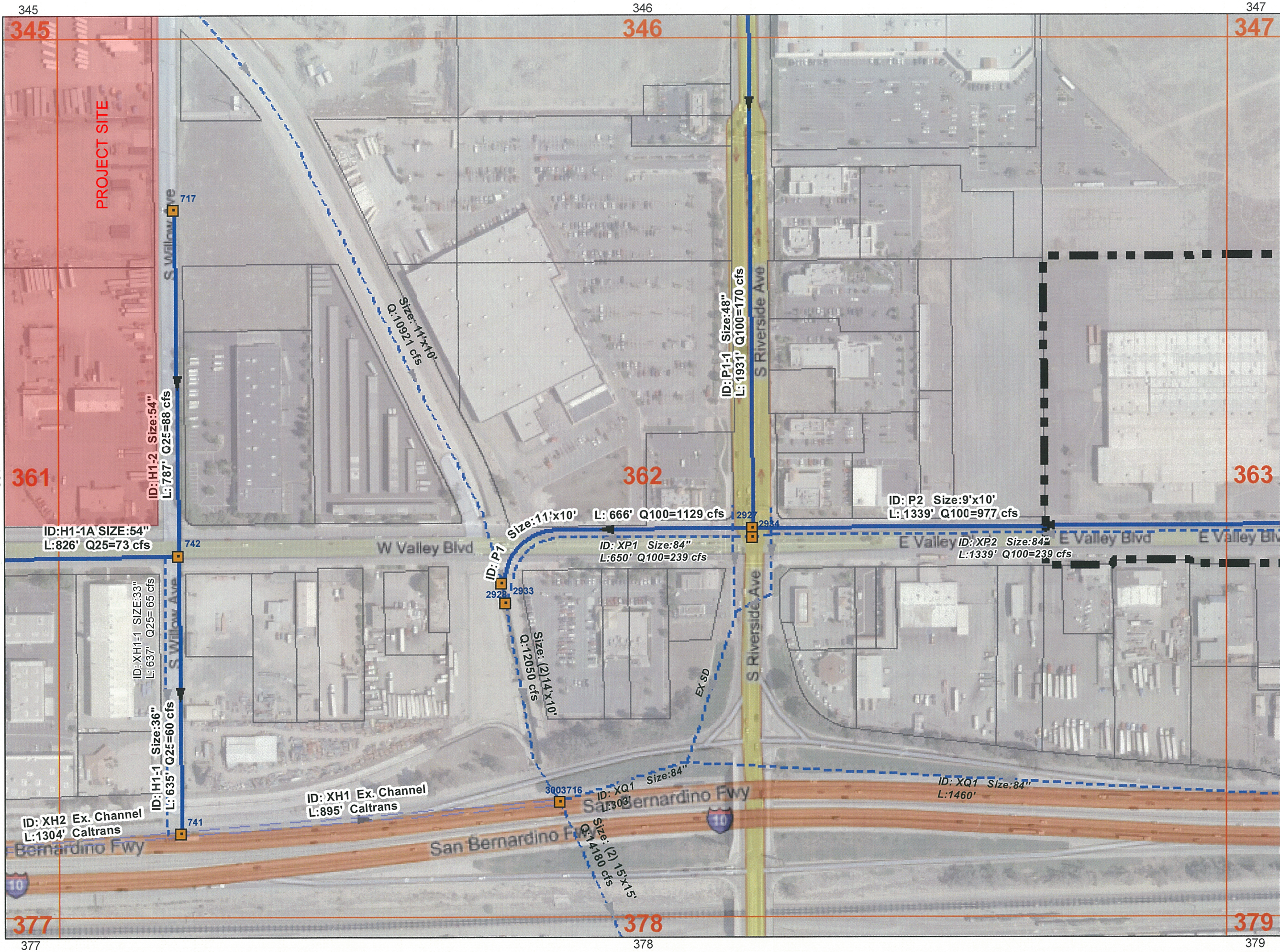
SAN BERNARDINO COUNTY FLOOD CONTROL DISTRICT			
VALLEY AREA			
ISOHYETALS X ₄ - 100 YEAR 24 HOUR BASED ON U.S.D.C. NOAA ATLAS 2, 1973			
APPROVED BY: _____			
FLOOD CONTROL ENGINEER			
DATE	SCALE	FILE NO.	DRWG. NO.
1982	1" = 2 MI.	WRD-1	6 of 12



Storm Drain Network

- Legend**
- Storm Drain Master Plan**
- Proposed Storm Drain
 - Existing Storm Drain
 - Proposed Channel
 - Existing Channel
 - Junction Node
 - Transition Node
 - Detention Basin
 - Master Plan Drainage Area Boundary
 - Municipal_Boundary



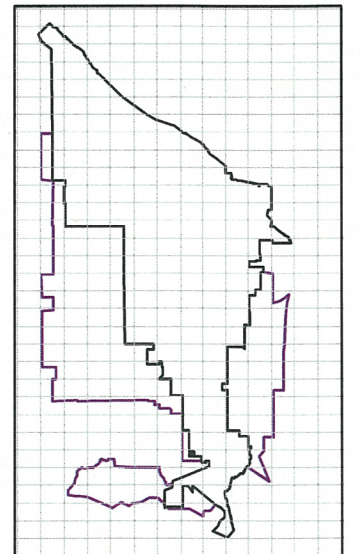
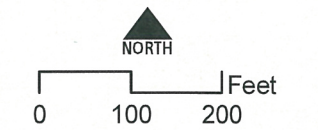


Storm Drain Network

Legend

Storm Drain Master Plan

- Proposed Storm Drain
- Existing Storm Drain
- Proposed Channel
- Existing Channel
- Junction Node
- Transition Node
- Detention Basin
- Master Plan Drainage Area Boundary
- Municipal Boundary



APPENDIX B

HYDROLOGY CALCULATIONS

EXISTING CONDITION

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA (ACRES) = 6.85 SUBAREA RUNOFF (CFS) = 13.46
 EFFECTIVE AREA (ACRES) = 13.05 AREA-AVERAGED Fm (INCH/HR) = 0.18
 AREA-AVERAGED Fp (INCH/HR) = 0.18 AREA-AVERAGED Ap = 1.00
 TOTAL AREA (ACRES) = 13.0 PEAK FLOW RATE (CFS) = 25.64

 FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 52

 >>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
 >>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 1068.39 DOWNSTREAM (FEET) = 1064.22
 CHANNEL LENGTH THRU SUBAREA (FEET) = 364.00 CHANNEL SLOPE = 0.0115
 CHANNEL FLOW THRU SUBAREA (CFS) = 25.64
 FLOW VELOCITY (FEET/SEC) = 3.43 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
 TRAVEL TIME (MIN.) = 1.77 Tc (MIN.) = 23.08
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 1689.00 FEET.

 FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 81

 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 23.08
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 2.253
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER "BARREN"	A	8.05	0.18	1.000	93

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.18
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA (ACRES) = 8.05 SUBAREA RUNOFF (CFS) = 15.02
 EFFECTIVE AREA (ACRES) = 21.10 AREA-AVERAGED Fm (INCH/HR) = 0.18
 AREA-AVERAGED Fp (INCH/HR) = 0.18 AREA-AVERAGED Ap = 1.00
 TOTAL AREA (ACRES) = 21.1 PEAK FLOW RATE (CFS) = 39.36

END OF STUDY SUMMARY:
 TOTAL AREA (ACRES) = 21.1 TC (MIN.) = 23.08
 EFFECTIVE AREA (ACRES) = 21.10 AREA-AVERAGED Fm (INCH/HR) = 0.18
 AREA-AVERAGED Fp (INCH/HR) = 0.18 AREA-AVERAGED Ap = 1.000
 PEAK FLOW RATE (CFS) = 39.36

 END OF RATIONAL METHOD ANALYSIS

^

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION)
(c) Copyright 1983-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1435

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* VALLEY BOULEVARD INDUSTRIAL BUILDING *
* EXISTING CONDITION 100-YEAR *
* NODES 100-101 (NEIGHBORING PROPERTY) *

FILE NAME: W:\3836\EXOFF.DAT
TIME/DATE OF STUDY: 09:41 12/11/2019

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 12.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL

SLOPE OF INTENSITY DURATION CURVE (LOG(I;IN/HR) vs. LOG(Tc;MIN)) = 0.6000
USER SPECIFIED 1-HOUR INTENSITY (INCH/HOUR) = 1.2700

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- CROWN TO		STREET-CROSSFALL:		CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)	IN- / SIDE/ WAY	OUT-/PARK- / SIDE/ WAY		WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020		0.67	2.00	0.0312	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 1023.00
ELEVATION DATA: UPSTREAM (FEET) = 1105.22 DOWNSTREAM (FEET) = 1077.06

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 9.974
* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.727
SUBAREA Tc AND LOSS RATE DATA (AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL A 5.90 0.74 0.100 52 9.97
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF (CFS) = 19.40
TOTAL AREA (ACRES) = 5.90 PEAK FLOW RATE (CFS) = 19.40

=====

END OF STUDY SUMMARY:
TOTAL AREA (ACRES) = 5.9 TC (MIN.) = 9.97
EFFECTIVE AREA (ACRES) = 5.90 AREA-AVERAGED Fm (INCH/HR) = 0.07
AREA-AVERAGED Fp (INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.100
PEAK FLOW RATE (CFS) = 19.40

END OF RATIONAL METHOD ANALYSIS

▲

PROPOSED CONDITION

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Analysis prepared by:

THIENES ENGINEERING, INC.
 14349 FIRESTONE BLVD
 LA MIRADA, CA 90638
 714-521-4811

***** DESCRIPTION OF STUDY *****
 * TEI JOB NO 3836 *
 * PROPOSED CONDITION *
 * 100 YEAR STORM EVENT *

FILE NAME: W:\3836\P100.DAT
 TIME/DATE OF STUDY: 12:58 07/06/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
 SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
 SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
 USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL

SLOPE OF INTENSITY DURATION CURVE(LOG(I;IN/HR) vs. LOG(Tc;MIN)) = 0.6000
 USER SPECIFIED 1-HOUR INTENSITY(INCH/HOUR) = 1.2700

ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL IN- / OUT- / SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GUTTER-LIP (FT)	GUTTER-HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
 as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.

*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

 FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 520.00
 ELEVATION DATA: UPSTREAM(FEET) = 10829.00 DOWNSTREAM(FEET) = 1076.20

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.000
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.640

SUBAREA T_c AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	1.00	0.74	0.100	52	5.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA RUNOFF(CFS) = 5.01
 TOTAL AREA(ACRES) = 1.00 PEAK FLOW RATE(CFS) = 5.01

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1074.20 DOWNSTREAM(FEET) = 1073.40
FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.012
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.82
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.01
PIPE TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 5.52
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 670.00 FEET.

FLOW PROCESS FROM NODE 102.00 TO NODE 102.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 5.52
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.316
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.80 0.74 0.100 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 3.77
EFFECTIVE AREA(ACRES) = 1.80 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 1.8 PEAK FLOW RATE(CFS) = 8.49

FLOW PROCESS FROM NODE 102.00 TO NODE 103.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1073.40 DOWNSTREAM(FEET) = 1072.90
FLOW LENGTH(FEET) = 112.00 MANNING'S N = 0.012
DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.11
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.49
PIPE TRAVEL TIME(MIN.) = 0.37 Tc(MIN.) = 5.88
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 782.00 FEET.

FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 5.88
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.116
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.40 0.74 0.100 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.81
EFFECTIVE AREA(ACRES) = 2.20 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 2.2 PEAK FLOW RATE(CFS) = 9.98

FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1072.90 DOWNSTREAM(FEET) = 1072.30
FLOW LENGTH(FEET) = 112.00 MANNING'S N = 0.012
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.67
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.98
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 6.21
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 894.00 FEET.

FLOW PROCESS FROM NODE 104.00 TO NODE 104.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 6.21
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.951
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.40 0.74 0.100 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.76
EFFECTIVE AREA(ACRES) = 2.60 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 2.6 PEAK FLOW RATE(CFS) = 11.41

FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1072.30 DOWNSTREAM(FEET) = 1071.70
FLOW LENGTH(FEET) = 112.00 MANNING'S N = 0.012
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.78
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.41
PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 6.54
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 1006.00 FEET.

FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 6.54
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.803
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 0.40 0.74 0.100 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.70
EFFECTIVE AREA(ACRES) = 3.00 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 3.0 PEAK FLOW RATE(CFS) = 12.77

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1071.70 DOWNSTREAM(FEET) = 1071.20
FLOW LENGTH(FEET) = 112.00 MANNING'S N = 0.012
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.64
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 12.77
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 6.87
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 106.00 = 1118.00 FEET.

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
MAINLINE Tc(MIN.) = 6.87
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.663
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/   SCS SOIL  AREA    Fp      Ap    SCS
  LAND USE          GROUP  (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL          A      0.40    0.74    0.100  52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.40      SUBAREA RUNOFF(CFS) = 1.65
EFFECTIVE AREA(ACRES) = 3.40    AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 3.4      PEAK FLOW RATE(CFS) = 14.04
    
```

 FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1071.20 DOWNSTREAM(FEET) = 1070.60
FLOW LENGTH(FEET) = 112.00 MANNING'S N = 0.012
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.18
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 14.04
PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 7.17
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 1230.00 FEET.
    
```

 FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
MAINLINE Tc(MIN.) = 7.17
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.544
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/   SCS SOIL  AREA    Fp      Ap    SCS
  LAND USE          GROUP  (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL          A      0.40    0.74    0.100  52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 0.40      SUBAREA RUNOFF(CFS) = 1.61
EFFECTIVE AREA(ACRES) = 3.80    AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 3.8      PEAK FLOW RATE(CFS) = 15.29
    
```

 FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1070.60 DOWNSTREAM(FEET) = 1070.10
FLOW LENGTH(FEET) = 112.00 MANNING'S N = 0.012
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.78
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 15.29
PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 7.49
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 1342.00 FEET.
    
```

 FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
MAINLINE Tc(MIN.) = 7.49
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.425
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/   SCS SOIL  AREA    Fp      Ap    SCS
  LAND USE          GROUP  (ACRES) (INCH/HR) (DECIMAL) CN
    
```

COMMERCIAL A 0.40 0.74 0.100 52
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.57
 EFFECTIVE AREA(ACRES) = 4.20 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 4.2 PEAK FLOW RATE(CFS) = 16.45

 FLOW PROCESS FROM NODE 108.00 TO NODE 109.00 IS CODE = 31

 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 1070.10 DOWNSTREAM(FEET) = 1069.50
 FLOW LENGTH(FEET) = 112.00 MANNING'S N = 0.012
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.5 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.33
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 16.45
 PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 7.79
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 109.00 = 1454.00 FEET.

 FLOW PROCESS FROM NODE 109.00 TO NODE 109.00 IS CODE = 81

 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
 =====
 MAINLINE Tc(MIN.) = 7.79
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.324
 SUBAREA LOSS RATE DATA(AMC III):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 COMMERCIAL A 0.40 0.74 0.100 52
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.53
 EFFECTIVE AREA(ACRES) = 4.60 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 4.6 PEAK FLOW RATE(CFS) = 17.59

 FLOW PROCESS FROM NODE 109.00 TO NODE 110.00 IS CODE = 31

 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 1069.50 DOWNSTREAM(FEET) = 1068.90
 FLOW LENGTH(FEET) = 112.00 MANNING'S N = 0.012
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.57
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 17.59
 PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 8.07
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 110.00 = 1566.00 FEET.

 FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 81

 >>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
 =====
 MAINLINE Tc(MIN.) = 8.07
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.232
 SUBAREA LOSS RATE DATA(AMC III):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 COMMERCIAL A 0.35 0.74 0.100 52
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 0.35 SUBAREA RUNOFF(CFS) = 1.31
 EFFECTIVE AREA(ACRES) = 4.95 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 5.0 PEAK FLOW RATE(CFS) = 18.52

FLOW PROCESS FROM NODE 110.00 TO NODE 213.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 1068.90 DOWNSTREAM(FEET) = 1063.15
 FLOW LENGTH(FEET) = 136.00 MANNING'S N = 0.012
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 14.37
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 18.52
 PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 8.23
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 213.00 = 1702.00 FEET.

FLOW PROCESS FROM NODE 213.00 TO NODE 213.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 940.00
 ELEVATION DATA: UPSTREAM(FEET) = 1082.90 DOWNSTREAM(FEET) = 1072.90

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.661
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.393
 SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	6.65	0.74	0.100	52	11.66

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA RUNOFF(CFS) = 19.87
 TOTAL AREA(ACRES) = 6.65 PEAK FLOW RATE(CFS) = 19.87

FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 1072.90
 DOWNSTREAM NODE ELEVATION(FEET) = 1070.80
 CHANNEL LENGTH THRU SUBAREA(FEET) = 407.00
 "V" GUTTER WIDTH(FEET) = 3.00 GUTTER HIKE(FEET) = 0.050
 PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0150
 PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.02000
 MAXIMUM DEPTH(FEET) = 100.00
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.027
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	7.05	0.74	0.100	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 29.23
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.77
 AVERAGE FLOW DEPTH(FEET) = 0.49 FLOOD WIDTH(FEET) = 45.78
 "V" GUTTER FLOW TRAVEL TIME(MIN.) = 2.44 Tc(MIN.) = 14.11
 SUBAREA AREA(ACRES) = 7.05 SUBAREA RUNOFF(CFS) = 18.74
 EFFECTIVE AREA(ACRES) = 13.70 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 13.7 PEAK FLOW RATE(CFS) = 36.41

END OF SUBAREA "V" GUTTER HYDRAULICS:
 DEPTH(FEET) = 0.53 FLOOD WIDTH(FEET) = 49.89
 FLOW VELOCITY(FEET/SEC.) = 2.91 DEPTH*VELOCITY(FT*FT/SEC) = 1.54
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 1347.00 FEET.

```

*****
FLOW PROCESS FROM NODE    202.00 TO NODE    212.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1066.80  DOWNSTREAM(FEET) = 1065.60
FLOW LENGTH(FEET) = 239.00  MANNING'S N = 0.012
DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.55
ESTIMATED PIPE DIAMETER(INCH) = 33.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 36.41
PIPE TRAVEL TIME(MIN.) = 0.53  Tc(MIN.) = 14.63
LONGEST FLOWPATH FROM NODE    200.00 TO NODE    212.00 = 1586.00 FEET.
*****
FLOW PROCESS FROM NODE    212.00 TO NODE    212.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.63
RAINFALL INTENSITY(INCH/HR) = 2.96
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 13.70
TOTAL STREAM AREA(ACRES) = 13.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 36.41
*****
FLOW PROCESS FROM NODE    210.00 TO NODE    211.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 408.00
ELEVATION DATA: UPSTREAM(FEET) = 1074.20  DOWNSTREAM(FEET) = 1070.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.622
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.067
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/   SCS SOIL  AREA    Fp      Ap    SCS  Tc
LAND USE           GROUP  (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL         A      1.35   0.74   0.100  52   8.62
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 4.85
TOTAL AREA(ACRES) = 1.35  PEAK FLOW RATE(CFS) = 4.85
*****
FLOW PROCESS FROM NODE    211.00 TO NODE    212.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1066.50  DOWNSTREAM(FEET) = 1063.50
FLOW LENGTH(FEET) = 13.00  MANNING'S N = 0.012
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.76
ESTIMATED PIPE DIAMETER(INCH) = 18.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.85
PIPE TRAVEL TIME(MIN.) = 0.01  Tc(MIN.) = 8.63
LONGEST FLOWPATH FROM NODE    210.00 TO NODE    212.00 = 421.00 FEET.
*****
FLOW PROCESS FROM NODE    212.00 TO NODE    212.00 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.63
RAINFALL INTENSITY(INCH/HR) = 4.06
AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 1.35
TOTAL STREAM AREA(ACRES) = 1.35
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.85
    
```

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	36.41	14.63	2.961	0.74(0.07)	0.10	13.7	200.00
2	4.85	8.63	4.064	0.74(0.07)	0.10	1.4	210.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	34.54	8.63	4.064	0.74(0.07)	0.10	9.4	210.00
2	39.92	14.63	2.961	0.74(0.07)	0.10	15.1	200.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 39.92 Tc(MIN.) = 14.63
 EFFECTIVE AREA(ACRES) = 15.05 AREA-AVERAGED Fm(INCH/HR) = 0.07
 AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 15.1
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 212.00 = 1586.00 FEET.

 FLOW PROCESS FROM NODE 212.00 TO NODE 213.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 1063.50 DOWNSTREAM(FEET) = 1063.15
FLOW LENGTH(FEET) = 211.00 MANNING'S N = 0.012
DEPTH OF FLOW IN 42.0 INCH PIPE IS 31.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.10
ESTIMATED PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 39.92
PIPE TRAVEL TIME(MIN.) = 0.69 Tc(MIN.) = 15.32
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 213.00 = 1797.00 FEET.
    
```

 FLOW PROCESS FROM NODE 213.00 TO NODE 213.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	34.54	9.36	3.873	0.74(0.07)	0.10	9.4	210.00
2	39.92	15.32	2.881	0.74(0.07)	0.10	15.1	200.00

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 213.00 = 1797.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	18.52	8.23	4.183	0.74(0.07)	0.10	5.0	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 213.00 = 1702.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	51.38	8.23	4.183	0.74(0.07)	0.10	13.2	100.00
2	51.67	9.36	3.873	0.74(0.07)	0.10	14.4	210.00
3	52.57	15.32	2.881	0.74(0.07)	0.10	20.0	200.00

TOTAL AREA(ACRES) = 20.0

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 52.57 Tc(MIN.) = 15.323
EFFECTIVE AREA(ACRES) = 20.00 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10
TOTAL AREA(ACRES) = 20.0
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 213.00 = 1797.00 FEET.

FLOW PROCESS FROM NODE 213.00 TO NODE 214.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1063.15 DOWNSTREAM(FEET) = 1061.25
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.012
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.27
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 52.57
PIPE TRAVEL TIME(MIN.) = 0.02 Tc(MIN.) = 15.34
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 214.00 = 1822.00 FEET.

END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 20.0 TC(MIN.) = 15.34
EFFECTIVE AREA(ACRES) = 20.00 AREA-AVERAGED Fm(INCH/HR)= 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.100
PEAK FLOW RATE(CFS) = 52.57

** PEAK FLOW RATE TABLE **

Table with 8 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 3 rows of data.

=====

END OF RATIONAL METHOD ANALYSIS

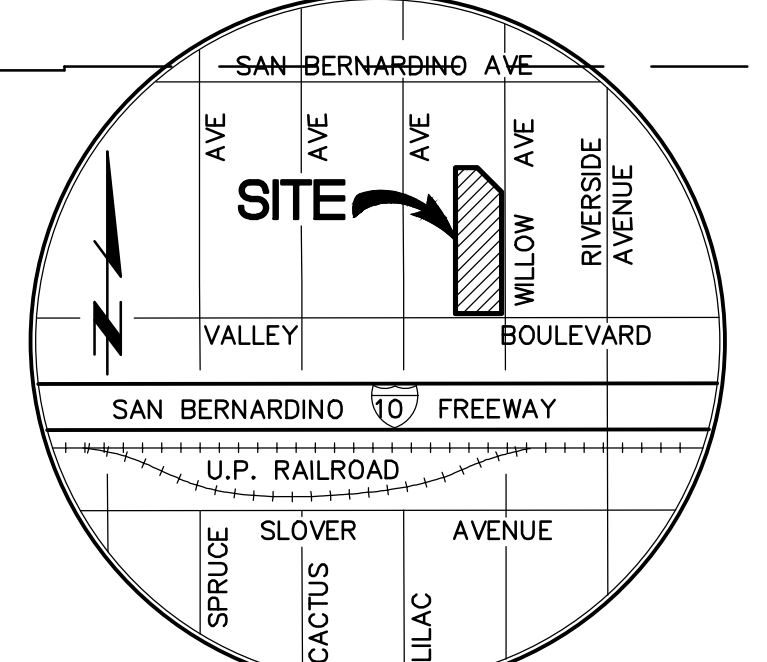
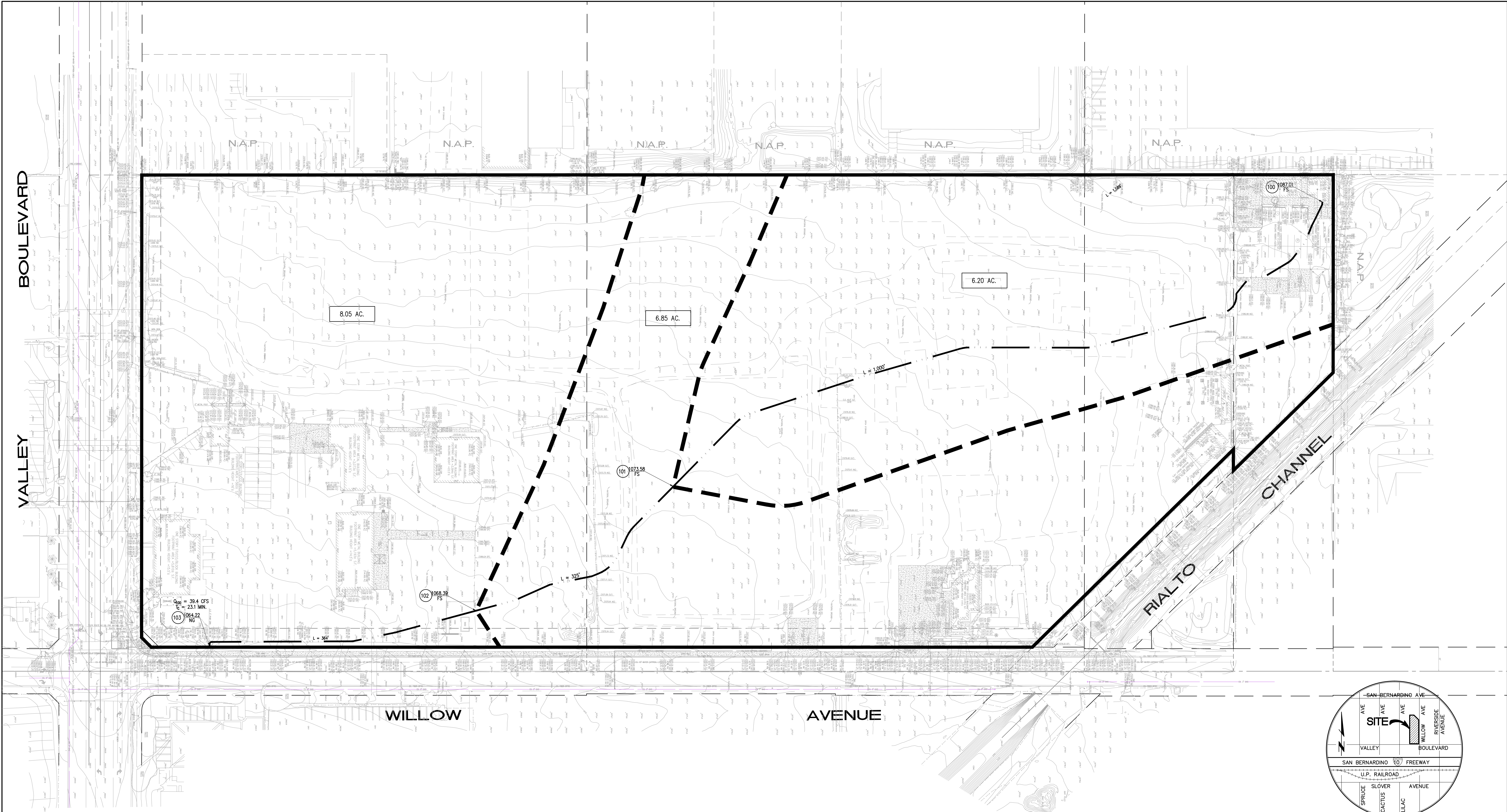


APPENDIX C

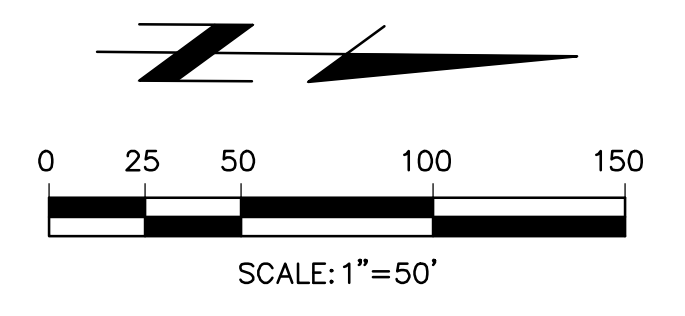
DETENTION CALCULATIONS

APPENDIX C

HYDROLOGY MAPS



VICINITY MAP
N.T.S.



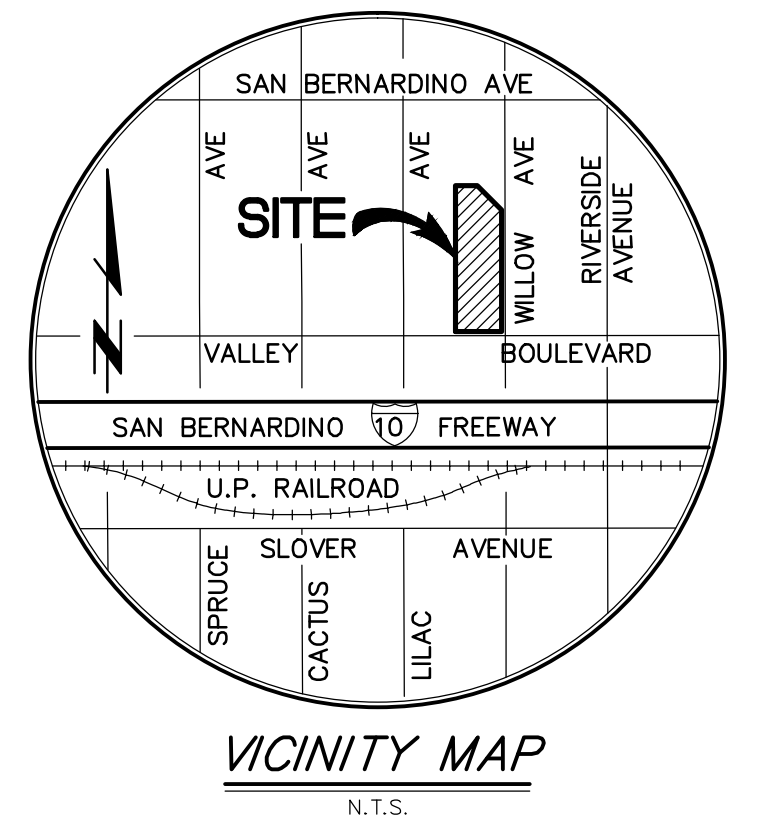
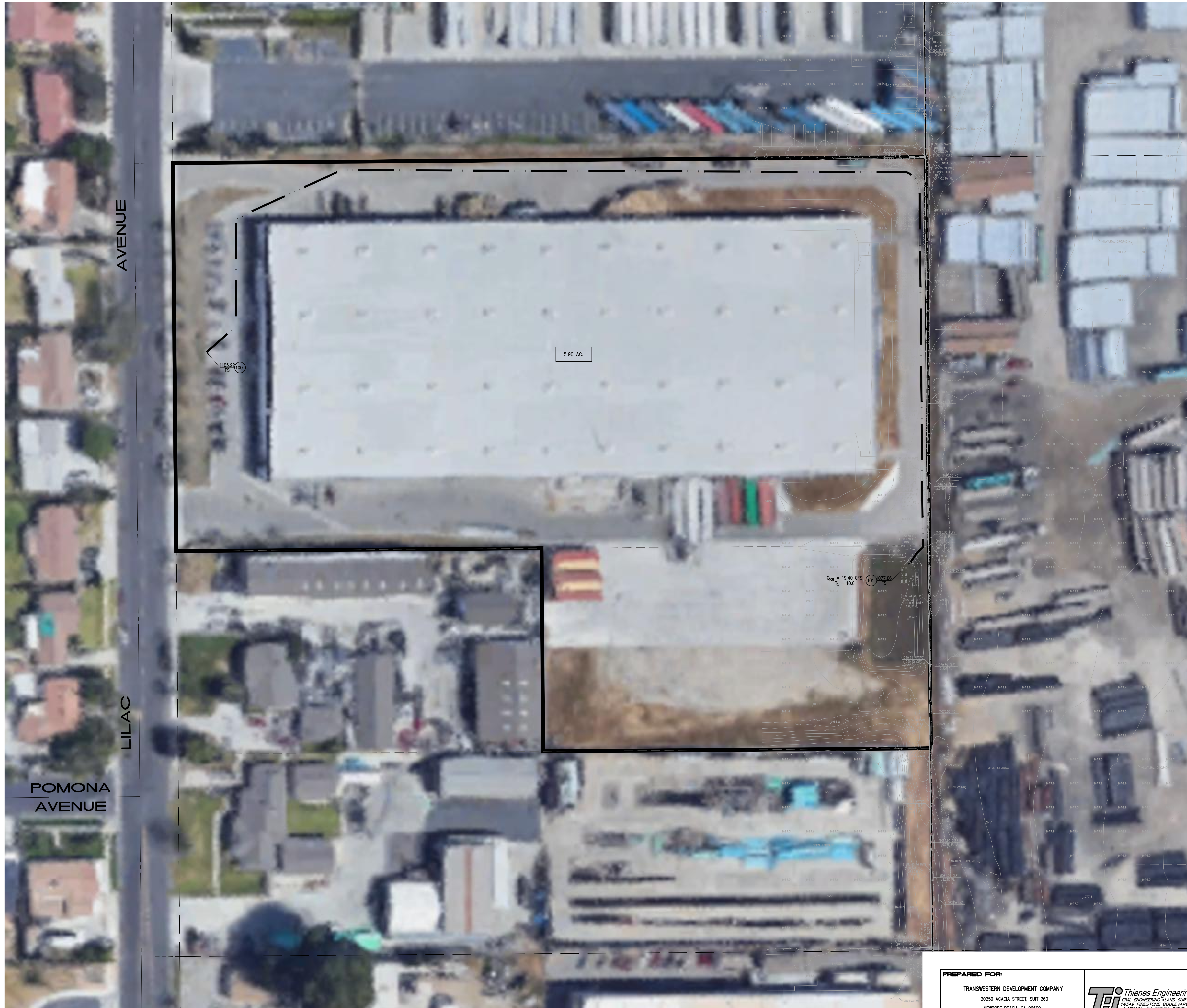
LEGEND	
	PROJECT BOUNDARY
	SUBAREA BOUNDARY
	FLOW LINE
	SUBAREA AREA
	NODE NUMBER
T_c	TIME OF CONCENTRATION
Q_{100}	DISCHARGE (CUBIC FEET PER SECOND) NUMBER DESIGNATE YEAR OF FREQUENCY

CITY OF RIALTO
PUBLIC WORKS DEPARTMENT
EXISTING CONDITION
HYDROLOGY MAP
VALLEY BOULEVARD INDUSTRIAL
BUILDING
WEST VALLEY BLVD. AND S.
WILLOW AVENUE

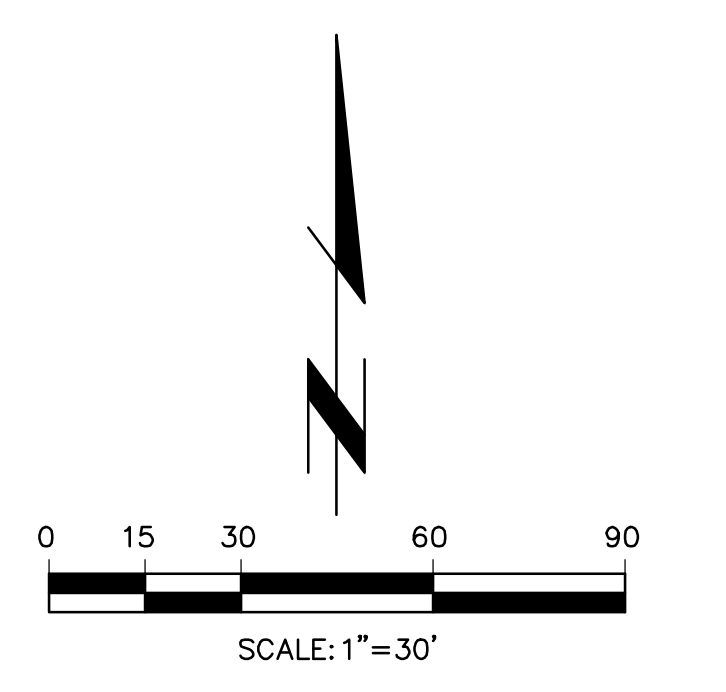
Designed by _____	Approved by _____	Date _____
Checked by _____	Public Works Director _____	R.C.E. XXXXX
Designed by _____		
Date _____		
Checked by _____		
Date _____		
Sheet 1 of 1 Sheets		

PREPARED FOR:
TRANSWESTERN DEVELOPMENT COMPANY
20250 ACAGIA STREET, SUIT 260
NEWPORT BEACH, CA 92660
PHONE: (949) 351-5186





LEGEND	
	PROJECT BOUNDARY
	SUBAREA BOUNDARY
	FLOW LINE
	SUBAREA AREA
	NODE NUMBER
T_c	TIME OF CONCENTRATION
Q_{100}	DISCHARGE (CUBIC FEET PER SECOND) NUMBER DESIGNATE YEAR OF FREQUENCY



Last Update: 12/23/18
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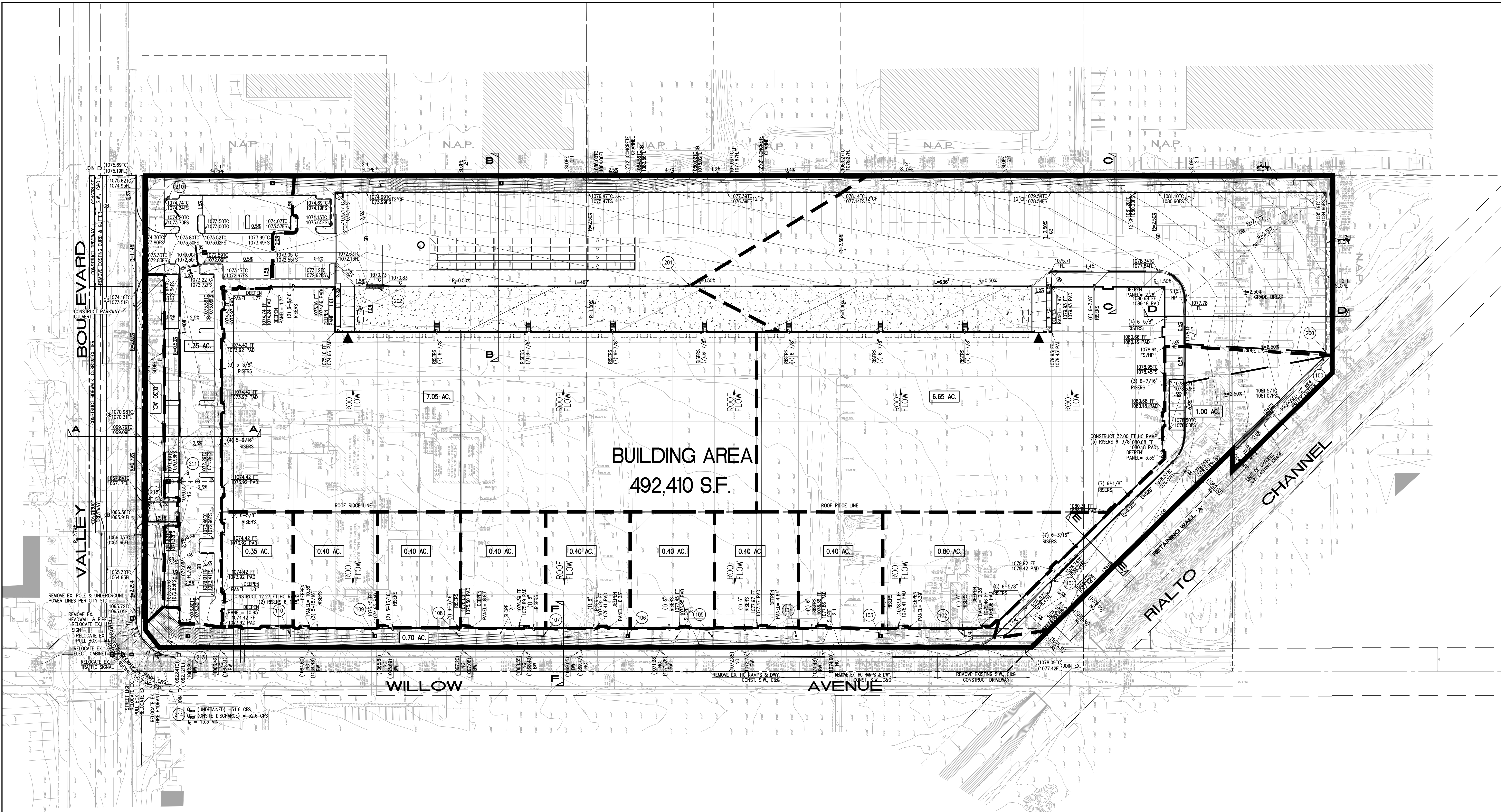
CITY OF RIALTO
PUBLIC WORKS DEPARTMENT
**EXISTING CONDITION
HYDROLOGY MAP
(ADJACENT PROPERTY)**
VALLEY BLVD INDUSTRIAL BUILDING
WEST VALLEY BLVD. AND S.
WILLOW AVENUE

PREPARED FOR:
TRANSWESTERN DEVELOPMENT COMPANY
20250 ACACIA STREET, SUIT 260
NEWPORT BEACH, CA 92660
PHONE: (949) 351-5186

TEI Thienes Engineering, Inc.
CIVIL ENGINEERING - LAND SURVEYING
14340 FIRESTONE BOULEVARD
LA MIRADA, CALIFORNIA 90638
PH: (714) 521-4811 FAX: (714) 521-4753

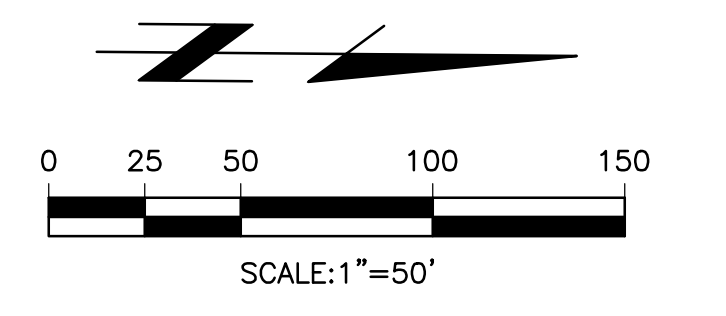
Designed by _____	Approved by _____	Date _____
Checked by _____	Public Works Director _____	R.C.E. XXXXX
Designed by _____		
Checked by _____		
Date _____	Sheet 1 of 1	Sheets

3836/1 OF 1 SHEET



LEGEND

- PROJECT BOUNDARY
- SUBAREA BOUNDARY
- FLOW PATH
- SUBAREA ACREAGE
- NODE NUMBER
- APPROXIMATE LIMITS OF 100-YEAR FLOODING
- T_c TIME OF CONCENTRATION
- Q_{100} DISCHARGE (CUBIC FEET PER SECOND) NUMBER DESIGNATE YEAR OF FREQUENCY



Last Update: 7/6/21
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CITY OF RIALTO
 PUBLIC WORKS DEPARTMENT

**PROPOSED CONDITION
 HYDROLOGY MAP
 VALLEY BOULEVARD INDUSTRIAL
 BUILDING
 WEST VALLEY BLVD. AND S.
 WILLOW AVENUE**

PREPARED FOR:
 TRANSWESTERN DEVELOPMENT COMPANY
 20250 ACACIA STREET, SUIT 260
 NEWPORT BEACH, CA 92660
 PHONE: (949) 351-5186

T*e*i Thienes Engineering, Inc.
 CIVIL ENGINEERING • LAND SURVEYING
 14146 FIRESTONE BOULEVARD
 LA MIRADA, CALIFORNIA 90638
 PH: (714) 521-4811 FAX: (714) 521-4133

Designed by _____	Approved by _____ Date _____
Checked by _____	Public Works Director _____ R.C.E. XXXXX
Designed by _____	
Checked by _____	
Date _____	
Sheet 1 of 1 Sheets	