

Appendix E Preliminary WQMP

Appendix

This page intentionally left blank.

Preliminary Water Quality Management Plan (PWQMP)

Project Name:

Oak Creek Community Park

Prepared for:

City of Irvine

Community Services Department

One Civic Center Plaza

Irvine, CA 92623

Prepared by:

Adams Streeter Civil Engineers

Engineer: Mo Abadi Registration No. 42615

16755 Von Karman Ave. Suite 150

Irvine CA, 92606

949.474.2330

Prepared on:

April 8, 2022

Template Prepared:

July 15, 2011



Preliminary Water Quality Management Plan (PWQMP)
Oak Creek Community Park

Project Owner's Certification			
Permit/Application No.		Grading Permit No.	
Tract/Parcel Map No.		Building Permit No.	
CUP, SUP, and/or APN (Specify Lot Numbers if Portions of Tract)			APN 466-022-26

This Water Quality Management Plan (WQMP) has been prepared for City of Irvine by Adams Streeter Civil Engineers. The WQMP is intended to comply with the requirements of the local NPDES Stormwater Program requiring the preparation of the plan.

The undersigned, while it owns the subject property, is responsible for the implementation of the provisions of this plan and will ensure that this plan is amended as appropriate to reflect up-to-date conditions on the site consistent with the current Orange County Drainage Area Management Plan (DAMP) and the intent of the non-point source NPDES Permit for Waste Discharge Requirements for the County of Orange, Orange County Flood Control District and the incorporated Cities of Orange County within the [Santa Ana Region](#). Once the undersigned transfers its interest in the property, its successors-in-interest shall bear the aforementioned responsibility to implement and amend the WQMP. An appropriate number of approved and signed copies of this document shall be available on the subject site in perpetuity.

Owner:			
Title			
Company			
Address			
Email			
Telephone #			
Signature		Date	

Contents

Page No.

Section I Discretionary Permit(s) and Water Quality Conditions.....3
Section II Project Description.....4
Section III Site Description10
Section IV Best Management Practices (BMPs).....12
Section V Inspection/Maintenance Responsibility for BMPs.....24
Section VI Site Plan and Drainage Plan26
Section VII Educational Materials.....27

Attachments

Attachment AEducational Materials
Attachment BBMP Calculations
Attachment C BMP Site Plan
Attachment D Hydromodification Calculations
Attachment E Orange County Rainfall Zones Map

Section I Discretionary Permit(s) and Water Quality Conditions

Project Information	
Permit/Application No.	Tract/Parcel Map No.
Additional Information/ Comments:	
Water Quality Conditions	
Water Quality Conditions (list verbatim)	N/A
Watershed-Based Plan Conditions	
Provide applicable conditions from watershed - based plans including WIHMPs and TMDLS.	N/A

Section II Project Description

II.1 Project Description

Description of Proposed Project				
Development Category (Verbatim from WQMP):	<p>New development projects that create 10,000 square feet or more of impervious surface. This category includes commercial, industrial, residential housing subdivisions, mixed-use, and public projects on private or public property that falls under the planning and building authority or the Permittees.</p> <p>Parking lots 5,000 square feet or more including associated drive aisle, and potentially exposed to urban stormwater runoff. A parking lot is defined as a land area or facility for the temporary parking or storage of motor vehicles used personally, for business, or for commerce.</p>			
Project Area (ft ²): ___831,996___	Number of Dwelling Units ___N/A___		SIC Code: ___N/A___	
Narrative Project Description:	<p>The Oak Creek Community Park renovation project will consist of converting an existing baseball field to a new synthetic turf soccer field, the refurbishment of an existing soccer field, the addition of two new dog parks and the construction of a new 141 stall asphalt parking lot. In addition, new concrete and decomposed granite walkways are intended to provide access to the new amenities.</p>			
Project Area	Pervious		Impervious	
	Area (acres)	Percentage	Area (acres)	Percentage
	Pre-Project Conditions	17.10 89	2.00 11	
Post-Project Conditions	15.13 79	3.97 21		
Drainage Patterns/Connections	<p>The drainage for the existing site is achieved via surface flows draining from northeast towards the southwest direction to be picked-up in an existing storm drain facility located in Valley Oak Drive. The existing site drains southwest at two locations with connections to an existing 78-inch RCP located in Valley Oak Drive, a 36" RCP pipe drains the existing community park and an 18" RCP pipe drains the existing SCE property. The existing storm drain pipe is located along the south side</p>			

of the community park. Currently, the site is bermed along the perimeter with drainage surface-flowing towards the parkway.

The proposed drainage condition includes provisions to capture and treat runoff from the new parking lot that will be constructed on the SCE site. Storm drain improvements consisting of a trench drain and 18" RCP pipe conveys drainage from the proposed parking lot to a water quality unit. Treated and overflow runoff from the water quality unit drains towards the westerly corner of the site and is captured by the existing 24" CSP riser that conveys runoff to Valley Oak Drive.

The existing turf / green areas located on-site will largely remain as turf or synthetic turf. Existing drainage patterns will be held for the proposed improvements as the site is already tabled to drain toward the Existing 78-inch RCP located on Valley Oak Drive.

II.2 Potential Stormwater Pollutants

Pollutants of Concern			
Pollutant	Circle One: E=Expected to be of concern N=Not Expected to be of concern		Additional Information and Comments
Suspended-Solid/ Sediment	(E)	N	
Nutrients	(E)	N	
Heavy Metals	(E)	N	
Pathogens (Bacteria/Virus)	(E)	N	
Pesticides	(E)	N	
Oil and Grease	(E)	N	
Toxic Organic Compounds	(E)	N	
Trash and Debris	(E)	N	

II.3 Hydrologic Conditions of Concern

No - Show map

Yes - Describe applicable hydrologic conditions of concern below. *Refer to Section 2.2.3 in the TGD.*

The project drains to Newport Bay that is potentially susceptible to hydromodification impacts. However, the proposed project is projected to mitigate any hydrologic conditions of concern and is not expected to cause an adverse impact on downstream receiving waters. The total increase in storm water runoff for the 2yr-24hr storm event is 3.15%.

2 year existing storm flow rate: 17.47 cfs

2 year proposed storm flow rate: 18.02 cfs

Please see hydrologic calculations located in Attachment D for further details

II.4 Post Development Drainage Characteristics

Generally, the runoff from the new parking area will sheet flow to the southwest into a concrete curb and gutters. Drainage from the gutters will be diverted into a proposed Modular Wetlands Biofiltration System. A small portion of runoff will be diverted to the north where a trench drain spanning the width of the parking lot entrance will intercept the runoff and redirect the runoff to the MWS unit.

The MWS will be located in a landscape buffer on the southwest corner of the parking lot. Qdesign flows will be treated by the MWS unit and the remaining bypass flows drain towards the westerly corner of the site and are captured by the existing 24" CSP riser that conveys runoff to Valley Oak Drive.

Once the Qdesign flow cycles through the MWS unit, the treated runoff will be diverted back into the existing SD system terminating into the San Diego Creek and then into the Newport Bay.

In addition to the parking lot improvements, concrete walkways are proposed along the east perimeter of the new soccer field, south and west perimeter of the proposed dog parks as well as along the south side of the existing parking lot. The walkways are 5' wide paths designed to provide access to the new amenities and have landscaping on both sides. The minimal runoff generated from the walkways will discharge onto the adjacent landscaping where it will be absorbed by the soil.

II.5 Property Ownership/Management

The property will be owned and operated by The City of Irvine.

Section III Site Description

III.1 Physical Setting

Planning Area/ Community Name	Planning Area 12 - Oakcreek
Location/ Address	15616 Valley Oak Drive, Irvine CA, 92606
Land Use	Recreation
Zoning	1.5
Acreage	19.10
Predominant Soil Type	Soil type B Per Figure XVI-2a of the North County TGD.

III.2 Site Characteristics

<i>Precipitation Zone</i>	<i>Design capture storm depth = 0.75 inches</i>
<i>Topography</i>	<i>The project has no large variations in grade and generally slopes to the southwest.</i>
<i>Drainage Patterns/Connections</i>	<i>See section II.2 for details</i>
<i>Soil Type, Geology, and Infiltration Properties</i>	<i>Soil Type B Per Figure XVI-2a of the North County TGD.</i>

<i>Site Characteristics (continued)</i>	
<i>Hydrogeologic (Groundwater) Conditions</i>	
<i>Geotechnical Conditions (relevant to infiltration)</i>	<i>The percolation rate on this site is infeasible for infiltration</i>
<i>Off-Site Drainage</i>	<i>No offsite drainage will be directed onto the site</i>
<i>Utility and Infrastructure Information</i>	<i>The project site discharges into an existing 78" RCP located in Valley Oak Drive.</i>

III.3 Watershed Description

Receiving Waters	San Diego Creek Reach 1, Upper Newport Bay, and Lower Newport Bay
303(d) Listed Impairments	San Diego Creek Reach 1 –Fecal Coliform, Nutrients, Pesticides, Sedimentation/Siltation, Selenium, Toxaphene Newport Bay (Upper) Chlordane, Copper, DDT, indicator Bacteria, metals, nutrients, PCBs, sediment toxicity, Sedimentation/Siltation Newport Bay (Lower) Chlordane, Copper, DDT, indicator Bacteria, nutrients, PCBs, pesticides, sediment toxicity
Applicable TMDLs	San Diego Creek Reach 1 –Metals, Nutrients, Pesticides, Siltation Newport Bay (Upper) Metals, Nutrients, Pathogens, Pesticides, Siltation Newport Bay (Lower) Metals, Nutrients, Pathogens, Pesticides, Priority Organics, Siltation
Pollutants of Concern for the Project	The pollutants of concern for this project are Suspended Solids/Sediments, Nutrients, Heavy Metals, Pathogens, Pesticides, Toxic Organic Compounds, and Trash.

Preliminary Water Quality Management Plan (PWQMP)
Oak Creek Community Park

Environmentally Sensitive and Special Biological Significant Areas	N/A
--	-----

Section IV Best Management Practices (BMPs)

IV. 1 Project Performance Criteria

<p>(NOC Permit Area only) Is there an approved WIHMP or equivalent for the project area that includes more stringent LID feasibility criteria or if there are opportunities identified for implementing LID on regional or sub-regional basis?</p>	YES <input type="checkbox"/>	NO <input checked="" type="checkbox"/>
<p>If yes, describe WIHMP feasibility criteria or regional/sub-regional LID opportunities.</p>		

Project Performance Criteria (continued)

<p>If HCOC exists, list applicable hydromodification control performance criteria (Section 7.II-2.4.2.2 in MWQMP)</p>	<p>N/A</p>
<p>List applicable LID performance criteria (Section 7.II-2.4.3 from MWQMP)</p>	<p>The project will be designed to treat the 85th percentile, 24-hour storm event (Design Flow) of 0.31 cfs.</p>
<p>List applicable treatment control BMP performance criteria (Section 7.II-3.2.2 from MWQMP)</p>	<p>Modular Wetlands Systems: The treatment capacity (cfs) for the single MWS unit that will treat the flow from drainage A is 0.34 CFS</p>
<p>Calculate LID design storm capture volume for Project.</p>	<p>Capture Volume: 1,163.87 cf (Worksheet B) Treatment Capacity= 0.34 cfs > Design Flow = 0.31 cfs</p>

IV.2. SITE DESIGN AND DRAINAGE PLAN

The following section describes the site design BMPs used in this project and the methods used to incorporate them. Careful consideration of site design is a critical first step in storm water pollution prevention from new developments and redevelopments.

SITE DESIGN BMPs

Minimize Impervious Area

Impervious surfaces have been minimized by incorporating landscaped areas throughout the site surrounding the proposed hardscape areas.

Maximize Natural Infiltration Capacity

Under the existing conditions, infiltration capacity is low due to soils. Under the proposed condition, infiltration capacity will remain limited.

Disconnect Impervious Areas

Landscaping will be provided throughout the site, adjacent to walkways to disconnect impervious areas.

Protect Existing Vegetation and Sensitive Areas, and Revegetate Disturbed Areas

Landscaping will be replaced as appropriate in disturbed areas.

Xeriscape Landscaping

Proposed Landscaping will comprise of native draught tolerant material with efficient irrigation

DRAINAGE MANAGEMENT AREAS

In accordance with the MS4 permit and the Model WQMP, the project site has been divided into 1 Drainage Management Area (DMA) to be utilized for defining drainage areas and sizing LID and other treatment control BMPs. The DMA has been delineated based on the proposed site grading patterns, drainage patterns, storm drain and catch basin locations.

The design capture volume (DCV) and treatment flow rate (Q_{Design}) for the DMA is summarized in the table below. It have been derived utilizing the “Simple Method” in accordance with the TGD Section III.1.1. Actual BMP sizing requirements, including 80 percent capture design volumes, flow rates, depths, and other design details for the specific BMPs proposed are provided in Section IV.3.4 below. Location of DMA and associated

Preliminary Water Quality Management Plan (PWQMP)
Oak Creek Community Park

LID and treatment BMP are identified on the exhibits in Section VI. Additional calculations and TGD Worksheets are provided in Attachment B.

DMA/ Drainage Area ID ⁽¹⁾	BMP	Drainage Area (ac)	% Imp.	Design Storm Depth ⁽²⁾ (in)	Estimated Tc (min.)	Rainfall Intensity ⁽³⁾ (in/hr)	Q _{Design} ⁽⁴⁾ (cfs)
A	Modular Wetlands System	1.71	90%	0.75	10	0.22	0.31

Notes:

1. Refer to exhibits in Section VI for location each DMA.
2. Per Figure XVI-1 of the Model WQMP Technical Guidance Document
3. Per Figure III.4 of the Model WQMP Technical Guidance Document
4. Per Section III.3.3 and Worksheet D of the Model WQMP Technical Guidance Document.

V.3 LID BMP SELECTION AND PROJECT CONFORMANCE ANALYSIS

IV.3.1 Hydrologic Source Controls

Name	Included?
Localized on-lot infiltration	<input type="checkbox"/>
Impervious area dispersion (e.g. roof top disconnection)	<input type="checkbox"/>
Street trees (canopy interception)	<input type="checkbox"/>
Residential rain barrels (not actively managed)	<input type="checkbox"/>
Green roofs/Brown roofs	<input type="checkbox"/>
Blue roofs	<input type="checkbox"/>
Impervious area reduction (e.g. permeable pavers, site design)	<input type="checkbox"/>
Other:	<input type="checkbox"/>
Other:	<input type="checkbox"/>

IV.3.2 Infiltration BMPs

Name	Included?
Bioretention without underdrains	<input type="checkbox"/>
Rain gardens	<input type="checkbox"/>
Porous landscaping	<input type="checkbox"/>
Infiltration planters	<input type="checkbox"/>
Retention swales	<input type="checkbox"/>
Infiltration trenches	<input type="checkbox"/>
Infiltration basins	<input type="checkbox"/>
Drywells	<input type="checkbox"/>
Subsurface infiltration galleries	<input type="checkbox"/>
French drains	<input type="checkbox"/>
Permeable asphalt	<input type="checkbox"/>
Permeable concrete	<input type="checkbox"/>
Permeable concrete pavers	<input type="checkbox"/>
Other:	<input type="checkbox"/>
Other:	<input type="checkbox"/>

Infiltration on the site is the most desirable BMP and must be used as much as possible however, is infeasible at this site due to existing soil conditions. In light of this, the next tier of the hierarchy was considered

IV.3.3 Evapotranspiration, Rainwater Harvesting BMPs

Name	Included?
All HSCs; <i>See Section IV.3.1</i>	<input type="checkbox"/>
Surface-based infiltration BMPs	<input type="checkbox"/>
Biotreatment BMPs	<input type="checkbox"/>
Above-ground cisterns and basins	<input type="checkbox"/>
Underground detention	<input type="checkbox"/>
Other:	<input type="checkbox"/>
Other:	<input type="checkbox"/>
Other:	<input type="checkbox"/>

Rainwater harvesting was considered for this project. This involves capturing the initial storm water runoff in a tank either above ground or below ground and later reusing it for irrigation or toilet flushing. The goal with this method is to keep the initial runoff from entering the storm drain system. The major concern with this method is the situation in which there are two successive storms in a short amount of time. The first storm would fill the tank and then before there was sufficient time to empty the tank the second storm would hit. The initial runoff from the second storm would have to bypass the tank and would end up draining untreated to the storm drain. In light of this, the next tier of biotreatment was considered.

IV.3.4 Biotreatment BMPs

Name	Included?
Bioretention with underdrains	<input type="checkbox"/>
Stormwater planter boxes with underdrains	<input type="checkbox"/>
Rain gardens with underdrains	<input type="checkbox"/>
Constructed wetlands	<input type="checkbox"/>
Vegetated swales	<input type="checkbox"/>
Vegetated filter strips	<input type="checkbox"/>
Proprietary vegetated biotreatment systems	<input checked="" type="checkbox"/>
Wet extended detention basin	<input type="checkbox"/>
Dry extended detention basins	<input type="checkbox"/>
Other:	<input type="checkbox"/>
Other:	<input type="checkbox"/>

Since both infiltration and harvest and reuse are considered infeasible, runoff from the project site will be treated through the use of a biofiltration BMP: a proprietary biotreatment system (Modular Wetlands) with downstream of the improvements. In accordance with the Model WQMP and TGD, the biofiltration BMPs will be sized to treat runoff from the Design Capture Storm (85th percentile, 24-hour). Location and tributary drainage area is shown on the WQMP Exhibit. Detailed calculations, associated TGD Worksheets and BMP details are included in Attachment B.

Modular Wetlands by Modular Wetlands Systems, Inc. are proprietary biotreatment systems that utilize multi-stage treatment processes including screening media filtration, settling, and biofiltration. The pre-treatment chamber contains the first three stages of treatment, and includes a catch basin inlet filter to capture trash, debris, gross solids and sediments, a settling chamber for separating out larger solids, and a media filter cartridge for capturing fine TSS, metals, nutrients, and bacteria. Runoff then flows through the wetland chamber where treatment is achieved through a variety of physical, chemical, and biological processes. As storm water passes down through the planting soil, pollutants are filtered, adsorbed, biodegraded and sequestered by the soil and plants, functioning similar to bioretention systems. The discharge chamber at the end of the unit collects treated flows and discharges back into the storm drain system.

IV.3.5 Hydromodification Control BMPs

BMP Name	BMP Description

IV.3.6 Regional/Sub-Regional LID BMPs

Regional/Sub-Regional LID BMPs	
Not Applicable	

IV.3.7 Treatment Control BMPs

Treatment Control BMPs	
BMP Name	BMP Description

IV.3.8 Non-structural Source Control BMPs

Non-Structural Source Control BMPs				
Identifier	Name	Check One		If not applicable, state brief reason
		Included	Not Applicable	
N1	Education for Property Owners, Tenants and Occupants	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
N2	Activity Restrictions	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
N3	Common Area Landscape Management	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
N4	BMP Maintenance	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
N5	Title 22 CCR Compliance (How development will comply)	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No hazardous material on site
N6	Local Industrial Permit Compliance	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No local industrial permits required
N7	Spill Contingency Plan	<input type="checkbox"/>	<input checked="" type="checkbox"/>	There are no loading docks or vehicle maintenance areas
N8	Underground Storage Tank Compliance	<input type="checkbox"/>	<input checked="" type="checkbox"/>	There are no underground storage tanks on site
N9	Hazardous Materials Disclosure Compliance	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No hazardous material on site
N10	Uniform Fire Code Implementation	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No hazardous material on site
N11	Common Area Litter Control	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
N12	Employee Training	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
N13	Housekeeping of Loading Docks	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No loading dock on site
N14	Common Area Catch Basin Inspection	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
N15	Street Sweeping Private Streets and Parking Lots	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
N16	Retail Gasoline Outlets	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No gas outlet onsite.

N1. Education of Property Owners, Tenants and Occupants.

Proper education of onsite occupants will help to reduce all potential and anticipated pollutants from the site. Practical information shall be provided by the property owner to the employees on general good housekeeping BMP's and other practices that contribute to protection of storm water quality. This WQMP shall be provided with emphasis placed on the materials included in, but not limited to, Sections IV, V, VI, VII and Attachment A of this report. For additional information, see BMP SC-10, Non-Stormwater Discharges, included in Section Attachment A and the BMP Maintenance Responsibility/Frequency Matrix in Section V. Copies of The Ocean Begins at Your Front Door, Sewer Spill, Tips for Landscaping and Gardening, and Proper Maintenance Practices for Your Business are contained in Attachment A. Additional Education Materials to be used include, but are not limited to, SC-10, Non-Stormwater Discharges, SC-11, Spill Prevention, Control, and Cleanup, SC-34, Waste Handling and Disposal, and SC-41, Building & Grounds Maintenance. Also reference the Orange County Public Works website at <http://www.ocwatersheds.com>.

N2. Activity Restrictions.

Onsite activities shall be restricted to those currently granted by the City of Irvine and as outlined throughout this WQMP. Some general activity restrictions that shall be adhered to are:

- No discharges of fertilizer, pesticides, and wastes to streets or storm drains
- No blowing or sweeping of debris into streets or storm drains
- No hosing down of paved surfaces
- No vehicle fueling, washing, or maintenance

In addition, onsite activities shall be limited to the requirements of this WQMP as described herein. Adhering to appropriate activity restrictions will help to reduce all anticipated and potential pollutants from the site.

N3. Common Area Landscape Management.

All maintenance shall be consistent with City of Irvine guidelines. Proper landscape maintenance practices will help to reduce or eliminate pollution from pesticides, nutrients, trash/debris, and sediments. General guidelines include the following: Plant vegetation that reduces water, fertilizer, herbicide, and pesticide use. Waste shall be disposed of by composting or at a permitted landfill and shall not be raked or blown into the street, gutter, or storm drains. Irrigation systems shall be inspected monthly for poorly aligned sprinkler heads, broken sprinkler heads, and leaks. Detected problems shall be repaired as soon as they are observed. Avoid over-watering of vegetation. If excessive runoff is observed, automatic timers shall be adjusted. Note that the actual irrigation schedule and levels may vary based on soil type, maturity of vegetation, exposure, and seasonal conditions. If fertilizer is spilled on a paved surface it should be swept up immediately and placed in its container. Water shall not be used to clean fertilizer spills unless necessary and only after the area has been thoroughly cleaned using

dry cleaning methods. Pesticides, herbicides, and fertilizers shall not be applied within 48 hours prior to rain or if wind speeds exceed 5 mph. Pesticides shall be applied only as a last resort and after other pest mitigation efforts have been attempted. Non-pesticide mitigation measures include cultural tactics (modifying routine landscape activities, adjusting the amount of irrigation applied to the area, etc.), mechanical tactics (mulching and manual removal of weeds and larger pests such as snails), environmental/ physical tactics (netting, etc.), and biological tactics (using living organisms such as lady bugs and herbivores to control pests). Storage of pesticides shall be away from living areas and in a covered area that is not subject to temperature extremes. For additional information, see BMP SC-41, Building & Grounds Maintenance, SC-73, Landscape Maintenance, and BMP SD-10, Site Design and Landscape Planning, included in Attachment A and the BMP Maintenance Responsibility/Frequency Matrix in Section V.

N4. BMP Maintenance.

Selected BMP's will be maintained to ensure proper operation and that they are properly maintained. See the BMP Maintenance Responsibility/Frequency Matrix in Section V for details. Appropriate BMP Maintenance practices will help to reduce all pollutants from the site.

N11. Common Area Litter Control. (SC-60)

The owner shall implement trash management and litter control procedures aimed at reducing pollution of storm water runoff due to trash and debris. The owner will contract with a maintenance firm to provide regularly scheduled landscape maintenance and parking lot maintenance that will include litter removal, emptying of trash receptacles, and picking up of grass and plant clippings. For additional information, see BMP SC-41, Building & Grounds Maintenance, and SC-43, Parking/Storage Area Maintenance, included in Attachment A. Also see the BMP Maintenance Responsibility/Frequency Matrix in Section V.

N12. Employee Training.

Ensuring that employees are properly trained will help to reduce all anticipated and potential pollutants from the site. All new employees will be trained on how to minimize impacts to water quality. The educational materials provided in Attachment A will be reviewed including The Ocean Begins at Your Front Door, Sewer Spill, Tips for Landscaping and Gardening, and Proper Maintenance Practices for Your Business are contained in Attachment A. Additional Education Materials to be used are, but are not limited to, SC-10, Non-Stormwater Discharges, SC-11, Spill Prevention, Control, and Cleanup, SC-34, Waste Handling and Disposal, and SC-41, Building & Grounds Maintenance. Also reference the Orange County Public Works website at <http://www.ocwatersheds.com>. For additional information, see the BMP Maintenance Responsibility/Frequency Matrix in Section V.

N14. Common Area Catch Basin Inspection (SC-74).

Proper maintenance of the onsite catch basins will help to reduce the amount of trash/debris and silt/sediment in runoff. The onsite catch basins shall be inspected and cleaned of any trash or debris in or around the opening prior to the rainy season (by October 1st). Thereafter, inspections will be conducted every four months. See the Maintenance Responsibility/ Frequency Matrix in Section V.

N15 Street Sweeping Private Streets and Parking Lots (SC-43 & SC-70).

Access roads and drive aisles shall be swept twice a month to remove debris or more frequently as needed. Less traffic areas to be swept once a month minimum. For additional information, see BMP SC-43, Parking/Storage Area Maintenance and BMP SC-70, Road and Street Maintenance included in Attachment A. Also see the Maintenance Responsibility/ Frequency Matrix in Section V.

IV.3.9 Structural Source Control BMPs

Fill out structural source control check box forms or provide a brief narrative explaining if Structural source controls were not used.

Structural Source Control BMPs				
Identifier	Name	Check One		If not applicable, state brief reason
		Included	Not Applicable	
S1	Provide storm drain system stenciling and signage	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
S2	Design and construct outdoor material storage areas to reduce pollution introduction	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No outdoor material storage areas proposed.
S3	Design and construct trash and waste storage areas to reduce pollution introduction	<input type="checkbox"/>	<input checked="" type="checkbox"/>	A trash enclosure already exists on the site
S4	Use efficient irrigation systems & landscape design, water conservation, smart controllers, and source control	<input checked="" type="checkbox"/>	<input type="checkbox"/>	
S5	Protect slopes and channels and provide energy dissipation	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No large slopes on site
	Incorporate requirements applicable to individual priority project categories (from SDRWQCB NPDES Permit)	<input type="checkbox"/>	<input checked="" type="checkbox"/>	Requirements applicable to individual priority project categories listed below
S6	Dock areas	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No docks are proposed
S7	Maintenance bays	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No maintenance bays are proposed
S8	Vehicle wash areas	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No vehicle wash areas are proposed
S9	Outdoor processing areas	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No outdoor processing areas are proposed
S10	Equipment wash areas	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No equipment wash areas are proposed
S11	Fueling areas	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No fueling areas are proposed
S12	Hillside landscaping	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No hillside landscaping areas are proposed
S13	Wash water control for food preparation areas	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No food prep areas are proposed
S14	Community car wash racks	<input type="checkbox"/>	<input checked="" type="checkbox"/>	No community wash areas are proposed

S1. Provide Storm Drain Stenciling and Signage.

The proposed drainage inlets will be stenciled with the phrase “No Dumping – Drains to Ocean”. Storm drain signage will help to reduce all pollution. The storm drain signage shall be inspected once per year for legibility and re-stenciled as necessary. Stenciling should be done at minimum once every five years. See BMP SD-13, Storm Drain Signage, in Attachment A and the BMP Maintenance Responsibility/Frequency Matrix in Section V.

S4. Use Efficient Irrigation Systems & Landscape Design, Water Conservation, Smart Controllers, and Source Control.

All landscape maintenance shall be consistent with City of Irvine guidelines. Efficient irrigation practices will help to reduce pollution due to pesticides, nutrients, and sediments. General guidelines include the following: Plant vegetation that reduces water, fertilizer, herbicide, and pesticide use. Group plants with similar water requirements in order to reduce excess irrigation runoff and promote surface filtration.

IV.4 ALTERNATIVE COMPLIANCE PLAN (IF APPLICABLE)

IV.4.1 Water Quality Credits

Description of Proposed Project			
Project Types that Qualify for Water Quality Credits (Select all that apply):			
<input type="checkbox"/> Redevelopment projects that reduce the overall impervious footprint of the project site.	<input type="checkbox"/> Brownfield redevelopment, meaning redevelopment, expansion, or reuse of real property which may be complicated by the presence or potential presence of hazardous substances, pollutants or contaminants, and which have the potential to contribute to adverse ground or surface WQ if not redeveloped.	<input type="checkbox"/> Higher density development projects which include two distinct categories (credits can only be taken for one category): those with more than seven units per acre of development (lower credit allowance); vertical density developments, for example, those with a Floor to Area Ratio (FAR) of 2 or those having more than 18 units per acre (greater credit allowance).	
<input type="checkbox"/> Mixed use development, such as a combination of residential, commercial, industrial, office, institutional, or other land uses which incorporate design principles that can demonstrate environmental benefits that would not be realized through single use projects (e.g. reduced vehicle trip traffic with the potential to reduce sources of water or air pollution).	<input type="checkbox"/> Transit-oriented developments, such as a mixed use residential or commercial area designed to maximize access to public transportation; similar to above criterion, but where the development center is within one half mile of a mass transit center (e.g. bus, rail, light rail or commuter train station). Such projects would not be able to take credit for both categories, but may have greater credit assigned		<input type="checkbox"/> Redevelopment projects in an established historic district, historic preservation area, or similar significant city area including core City Center areas (to be defined through mapping).

<input type="checkbox"/> Developments with dedication of undeveloped portions to parks, preservation areas and other pervious uses.	<input type="checkbox"/> Developments in a city center area.	<input type="checkbox"/> Developments in historic districts or historic preservation areas.	<input type="checkbox"/> Live-work developments, a variety of developments designed to support residential and vocational needs together - similar to criteria to mixed use development; would not be able to take credit for both categories.	<input type="checkbox"/> In-fill projects, the conversion of empty lots and other underused spaces into more beneficially used spaces, such as residential or commercial areas.
Calculation of Water Quality Credits (if applicable)				

IV.4.2 Alternative Compliance Plan Information

Not applicable. Water quality credits will not be applied for the project. LID BMPs will be utilized for water quality treatment on-site in accordance with the MS4 Permit hierarchy identified at the beginning of this Section.

Section V Inspection/Maintenance Responsibility for BMPs

BMP Inspection/Maintenance			
BMP	Reponsible Party(s)	Inspection/Maintenance Activities Required	Minimum Frequency of Activities
N1 – Education of property owners, tenants, occupants	City of Irvine	Education of employees /owners shall be done within 4 weeks of start-up and continue on an annual refreshing basis with each new on-site employee/owner being given a Water Quality orientation using this WQMP as reference within two weeks of hire date.	Ongoing. Ensure all employees are adhering to the activity restrictions and are not engaged in activities that can have a negative impact on storm water.
N2 – Activity Restrictions	City of Irvine	There shall be no discharges of fertilizer, pesticides, or wastes to streets or storm drains. There shall be no blowing or sweeping of debris into storm drain. All debris shall be collected and relocated to an approved landfill.	Ongoing. Ensure all employees are adhering to the activity restrictions and are not engaged in activities that can have a negative impact on storm water.
N3 – Common area landscape management	City of Irvine	Landscape maintenance will consist of trimming and replanting of vegetation, repair and maintenance of irrigation systems, and appropriate use of fertilizers and pesticides.	Landscape maintenance shall be performed on a weekly basis. Irrigation systems shall be inspected monthly for leaks. Leaks shall be

			repaired as soon as they are observed.
N4 – BMP Maintenance	City of Irvine	The proposed treatment BMPs will be maintained as outlined in Attachment F of this report.	As outlined in Attachment F of this report.
N11 – Common area litter control	City of Irvine	The Owner will contract with a maintenance firm to provide weekly landscape maintenance and parking lot maintenance that will include litter removal and picking up grass and plant clippings. During routine maintenance, all trash and debris will be picked up and placed in waste receptacles.	Weekly

BMP Inspection/Maintenance			
BMP	Reponsible Party(s)	Inspection/ Maintenance Activities Required	Minimum Frequency of Activities
N12 – Employee training	City of Irvine	Education of employees /owner(s) shall be done within 4 weeks of startup and continue on an annual refreshing basis with each new onsite	Ongoing. Ensure all employees are adhering to the activity restrictions and are not engaged

Preliminary Water Quality Management Plan (PWQMP)
Oak Creek Community Park

		employee/owner(s) being given a water quality orientation using this WQMP as reference within two weeks of hire date.	in activities that can have a negative impact on storm water.
N14 – Common area catch basin inspection	City of Irvine	Inspect area in around catch basins for trash/debris and clean as necessary but at a minimum once prior to the rainy season (by Oct. 1st)	Once prior to the rainy season (by Oct. 1st) and every four months thereafter
N15 – Street sweeping private streets and parking lots	City of Irvine	The access roads and drive aisles shall be swept on a regular basis to remove debris. (See BMP SC-43 and BMP SC-70)	Twice a month to remove debris in drive aisles/access roads or more frequently as needed. Areas with less traffic to be done a minimum of once a month
Efficient Irrigation	City of Irvine	Inspect irrigation equipment. Check water sensors and adjust irrigation heads and timing.	Monthly
Modular Wetlands Biofilters	City of Irvine	<ul style="list-style-type: none"> · Remove trash from screening device. · Remove sediment from separation chamber. · Replace cartridge filter media. · Replace drain down filter media. · Trim vegetation. 	Annually
Storm drain stencilling	Owner	The storm drain signage shall be inspected once per year for legibility and re-stencilled as necessary	Once every year, repaint every five years at minimum

Section VI Site Plan and Drainage Plan

VI.1 SITE PLAN AND DRAINAGE PLAN

Section VII Educational Materials

Refer to the Orange County Stormwater Program (ocwatersheds.com) for a library of materials available. For the copy submitted to the Permittee, only attach the educational materials specifically applicable to the project. Other materials specific to the project may be included as well and must be attached.

Education Materials			
Residential Material (http://www.ocwatersheds.com)	Check If Applicable	Business Material (http://www.ocwatersheds.com)	Check If Applicable
The Ocean Begins at Your Front Door	<input checked="" type="checkbox"/>	Tips for the Automotive Industry	<input type="checkbox"/>
Tips for Car Wash Fund-raisers	<input type="checkbox"/>	Tips for Using Concrete and Mortar	<input type="checkbox"/>
Tips for the Home Mechanic	<input type="checkbox"/>	Tips for the Food Service Industry	<input type="checkbox"/>
Homeowners Guide for Sustainable Water Use	<input type="checkbox"/>	Proper Maintenance Practices for Your Business	<input checked="" type="checkbox"/>
Household Tips	<input type="checkbox"/>	Other Material	Check If Attached
Proper Disposal of Household Hazardous Waste	<input type="checkbox"/>		
Recycle at Your Local Used Oil Collection Center (North County)	<input type="checkbox"/>	SC-10 Non-Stormwater Discharges	<input checked="" type="checkbox"/>
Recycle at Your Local Used Oil Collection Center (Central County)	<input type="checkbox"/>	SC-11 Spill Prevention, Control and Clean-up	<input checked="" type="checkbox"/>
Recycle at Your Local Used Oil Collection Center (South County)	<input type="checkbox"/>	SC-34 Waste Handling and Disposal	<input checked="" type="checkbox"/>
Tips for Maintaining a Septic Tank System	<input type="checkbox"/>	SC-41 Building and Grounds Maintenance	<input checked="" type="checkbox"/>
Responsible Pest Control	<input type="checkbox"/>		<input type="checkbox"/>
Sewer Spill	<input type="checkbox"/>		<input type="checkbox"/>
Tips for the Home Improvement Projects	<input type="checkbox"/>		<input type="checkbox"/>
Tips for Horse Care	<input type="checkbox"/>		<input type="checkbox"/>
Tips for Landscaping and Gardening	<input type="checkbox"/>		<input type="checkbox"/>
Tips for Pet Care	<input type="checkbox"/>		<input type="checkbox"/>
Tips for Pool Maintenance	<input type="checkbox"/>		<input type="checkbox"/>
Tips for Residential Pool, Landscape and Hardscape Drains	<input type="checkbox"/>		<input type="checkbox"/>
Tips for Projects Using Paint	<input type="checkbox"/>		<input type="checkbox"/>

ATTACHMENT A

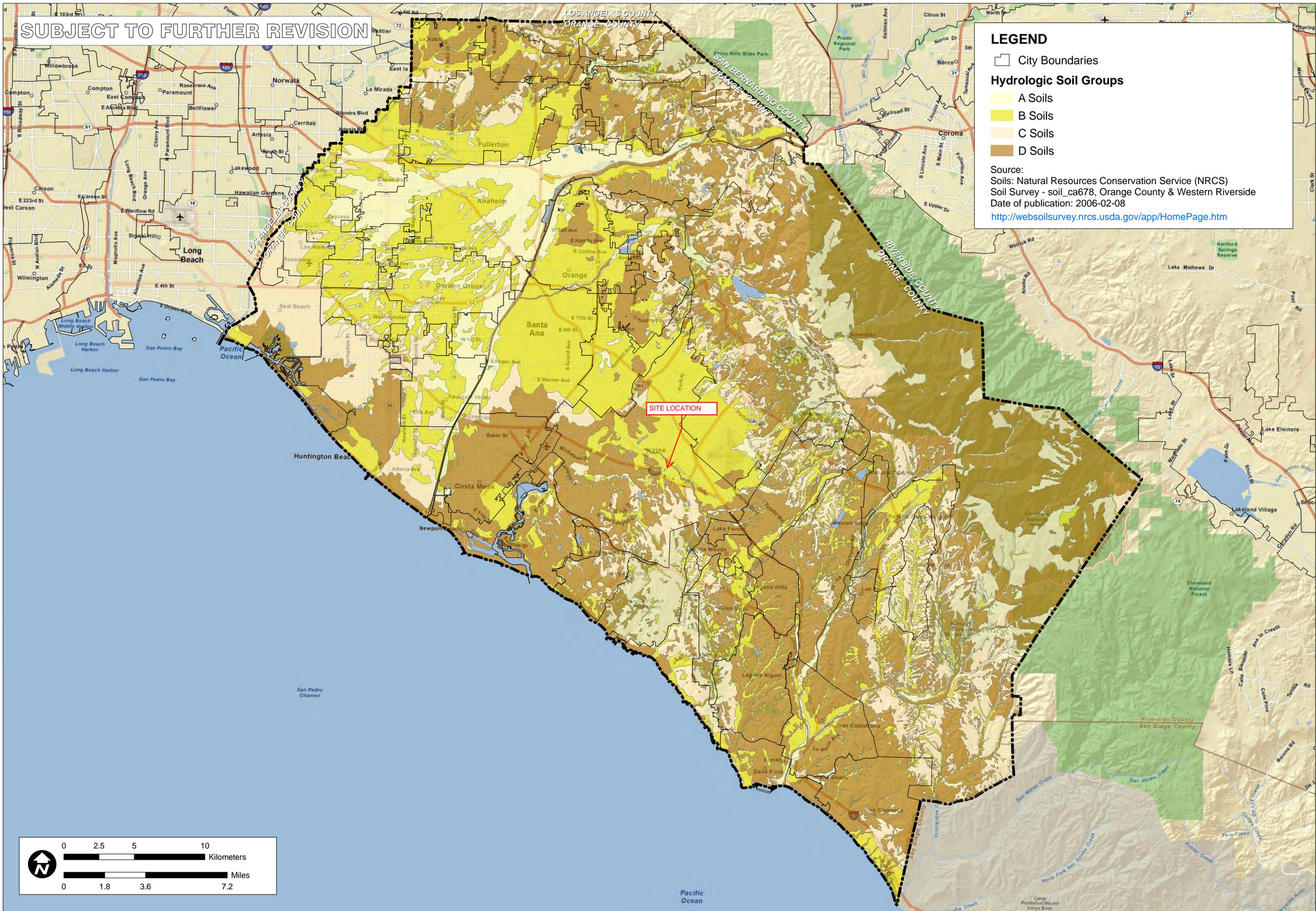
EDUCATIONAL MATERIALS

<http://www.ocwatersheds.com>

ATTACHMENT B

BMP CALCULATIONS

SUBJECT TO FURTHER REVISION



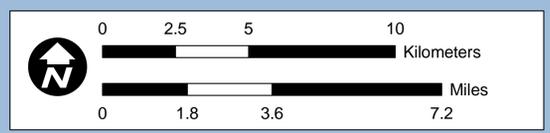
LEGEND

- City Boundaries

Hydrologic Soil Groups

- A Soils
- B Soils
- C Soils
- D Soils

Source:
 Soils: Natural Resources Conservation Service (NRCS)
 Soil Survey - soil_ca678, Orange County & Western Riverside
 Date of publication: 2006-02-08
<http://websoilsurvey.nrcs.usda.gov/app/HomePage.htm>



TITLE: NRCS HYDROLOGIC SOILS GROUPS
 JOB: ORANGE COUNTY INFILTRATION STUDY
 SCALE: 1" = 1.8 miles
 DESIGNED: TH
 DRAWING: TH
 CHECKED: BMP
 DATE: 02/09/11
 JOB NO.: 9526-E
 ORANGE CO. CA

FIGURE XVI-2a

P:\9526E\6-GIS\Mxd\Reports\InfiltrationFeasibility_20110215\9526E_FigureXVI-2a_HydroSoils_20110215.mxd

DMA -A

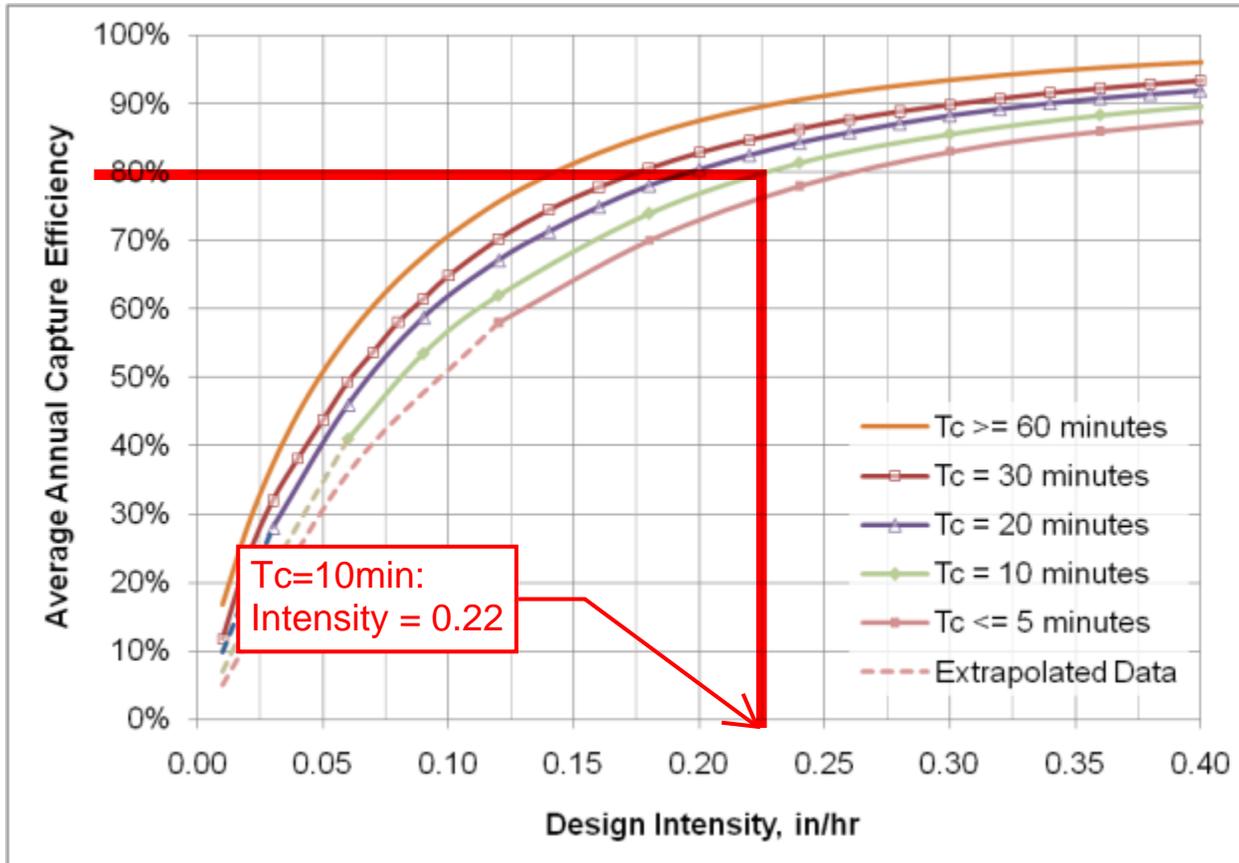
TECHNICAL GUIDANCE DOCUMENT APPENDICES

Worksheet D: Capture Efficiency Method for Flow-Based BMPs

Step 1: Determine the design capture storm depth used for calculating volume			
1	Enter the time of concentration, T_c (min) (See Appendix IV.2)	$T_c =$	10
2	Using Figure III.4 , determine the design intensity at which the estimated time of concentration (T_c) achieves 80% capture efficiency, I_1	$I_1 =$.22 in/hr
3	Enter the effect depth of provided HSCs upstream, d_{HSC} (inches) (Worksheet A)	$d_{HSC} =$	0 inches
4	Enter capture efficiency corresponding to d_{HSC} , Y_2 (Worksheet A)	$Y_2 =$	0 %
5	Using Figure III.4 , determine the design intensity at which the time of concentration (T_c) achieves the upstream capture efficiency (Y_2), I_2	$I_2 =$	0
6	Determine the design intensity that must be provided by BMP, $I_{design} = I_1 - I_2$	$I_{design} =$.22
Step 2: Calculate the design flowrate			
1	Enter Project area tributary to BMP (s), A (acres)	$A =$	1.71 acres
2	Enter Project Imperviousness, imp (unitless)	$imp =$.9
3	Calculate runoff coefficient, $C = (0.75 \times imp) + 0.15$	$C =$.825
4	Calculate design flowrate, $Q_{design} = (C \times I_{design} \times A)$	$Q_{design} =$	0.31 cfs
Supporting Calculations			
<p>Describe system:</p> <p style="color: red; margin-left: 40px;">The Q_{design} for DMA-A is 0.31.</p> <p style="color: red; margin-left: 40px;">The total treatment capacity of a 8'x12' MWS unit is 0.34 CFS</p>			
<p>Provide time of concentration assumptions:</p>			

Worksheet D: Capture Efficiency Method for Flow-Based BMPs

Graphical Operations



Provide supporting graphical operations. See Example III.7.

Worksheet B: Simple Design Capture Volume Sizing Method

Step 1: Determine the design capture storm depth used for calculating volume			
1	Enter design capture storm depth from Figure III.1, d (inches)	$d =$.75 inches
2	Enter the effect of provided HSCs, d_{HSC} (inches) (Worksheet A)	$d_{HSC} =$	inches
3	Calculate the remainder of the design capture storm depth, $d_{remainder}$ (inches) (Line 1 - Line 2)	$d_{remainder} =$.75 inches
Step 2: Calculate the DCV			
1	Enter Project area tributary to BMP (s), A (acres)	$A =$	1.71 acres
2	Enter Project Imperviousness, imp (unitless)	$imp =$.9
3	Calculate runoff coefficient, $C = (0.75 \times imp) + 0.15$	$C =$.25
4	Calculate runoff volume, $V_{design} = (C \times d_{remainder} \times A \times 43560 \times (1/12))$	$V_{design} =$	1163.87 cu-ft
Step 3: Design BMPs to ensure full retention of the DCV			
Step 3a: Determine design infiltration rate			
1	Enter measured infiltration rate, $K_{observed}^1$ (in/hr) (Appendix VII)	$K_{observed} =$	In/hr
2	Enter combined safety factor from Worksheet H, S_{total} (unitless)	$S_{total} =$	
3	Calculate design infiltration rate, $K_{design} = K_{observed} / S_{total}$	$K_{design} =$	In/hr
Step 3b: Determine minimum BMP footprint			
4	Enter drawdown time, T (max 48 hours)	$T =$	Hours
5	Calculate max retention depth that can be drawn down within the drawdown time (feet), $D_{max} = K_{design} \times T \times (1/12)$	$D_{max} =$	feet
6	Calculate minimum area required for BMP (sq-ft), $A_{min} = V_{design} / d_{max}$	$A_{min} =$	sq-ft

¹ $K_{observed}$ is the vertical infiltration measured in the field, before applying a factor of safety. If field testing measures a rate that is different than the vertical infiltration rate (for example, three-dimensional borehole percolation rate), then this rate must be adjusted by an acceptable method (for example, Porchet method) to yield the field estimate of vertical infiltration rate, $K_{observed}$. See Appendix VII.

MWS LINEAR 2.0 HGL SIZING CALCULATIONS



MWS MODEL SIZE	WETLAND PERMITTER LENGTH	LOADING RATE GPM/SF	HGL HEIGHT																																
			SHALLOW MODELS																				STANDARD HEIGHT MODEL	HIGH CAPACITY MODELS											
			1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3		3.4	3.5	3.6	3.65	3.70	3.75	3.80	3.85	3.90	3.95		
MWS-L-4-4	6.70	1.0	0.022	0.023	0.025	0.026	0.028	0.029	0.031	0.032	0.034	0.035	0.037	0.038	0.040	0.042	0.043	0.045	0.046	0.048	0.049	0.051	0.052	0.054	0.055	0.056	0.057	0.058	0.058	0.059	0.060	0.061			
MWS-L-3-6	10.06	1.0	0.032	0.035	0.037	0.039	0.042	0.044	0.046	0.048	0.051	0.053	0.055	0.058	0.060	0.062	0.065	0.067	0.069	0.072	0.074	0.076	0.078	0.081	0.083	0.084	0.085	0.087	0.088	0.089	0.090	0.091			
MWS-L-4-6	9.30	1.0	0.030	0.032	0.034	0.036	0.038	0.041	0.043	0.045	0.047	0.049	0.051	0.053	0.055	0.058	0.060	0.062	0.064	0.066	0.068	0.070	0.073	0.075	0.077	0.078	0.079	0.080	0.081	0.082	0.083	0.084			
MWS-L-4-8	14.80	1.0	0.048	0.051	0.054	0.058	0.061	0.065	0.068	0.071	0.075	0.078	0.082	0.085	0.088	0.092	0.095	0.099	0.102	0.105	0.109	0.112	0.115	0.119	0.122	0.124	0.126	0.127	0.129	0.131	0.132	0.134			
MWS-L-4-13	18.40	1.0	0.059	0.063	0.068	0.072	0.076	0.080	0.084	0.089	0.093	0.097	0.101	0.106	0.110	0.114	0.118	0.122	0.127	0.131	0.135	0.139	0.144	0.148	0.152	0.154	0.156	0.158	0.160	0.163	0.165	0.167			
MWS-L-4-15	22.40	1.0	0.072	0.077	0.082	0.087	0.093	0.098	0.103	0.108	0.113	0.118	0.123	0.129	0.134	0.139	0.144	0.149	0.154	0.159	0.165	0.170	0.175	0.180	0.185	0.188	0.190	0.193	0.195	0.198	0.200	0.203			
MWS-L-4-17	26.40	1.0	0.085	0.091	0.097	0.103	0.109	0.115	0.121	0.127	0.133	0.139	0.145	0.151	0.158	0.164	0.170	0.176	0.182	0.188	0.194	0.200	0.206	0.212	0.218	0.221	0.224	0.227	0.230	0.233	0.236	0.239			
MWS-L-4-19	30.40	1.0	0.098	0.105	0.112	0.119	0.126	0.133	0.140	0.147	0.153	0.160	0.167	0.174	0.181	0.188	0.195	0.202	0.209	0.216	0.223	0.230	0.237	0.244	0.251	0.255	0.258	0.262	0.265	0.269	0.272	0.276			
MWS-L-4-21	34.40	1.0	0.111	0.118	0.126	0.134	0.142	0.150	0.158	0.166	0.174	0.182	0.189	0.197	0.205	0.213	0.221	0.229	0.237	0.245	0.253	0.261	0.268	0.276	0.284	0.288	0.292	0.296	0.300	0.304	0.308	0.312			
MWS-L-6-8	18.80	1.0	0.060	0.065	0.069	0.073	0.078	0.082	0.086	0.091	0.095	0.099	0.104	0.108	0.112	0.116	0.121	0.125	0.129	0.134	0.138	0.142	0.147	0.151	0.155	0.157	0.160	0.162	0.164	0.166	0.168	0.170			
MWS-L-8-8	29.60	1.0	0.095	0.102	0.109	0.115	0.122	0.129	0.136	0.143	0.149	0.156	0.163	0.170	0.177	0.183	0.190	0.197	0.204	0.211	0.217	0.224	0.231	0.238	0.245	0.248	0.251	0.255	0.258	0.262	0.265	0.268			
MWS-L-8-12	44.40	1.0	0.143	0.153	0.163	0.173	0.183	0.194	0.204	0.214	0.224	0.234	0.245	0.255	0.265	0.275	0.285	0.296	0.306	0.316	0.326	0.336	0.346	0.357	0.367	0.372	0.377	0.382	0.387	0.392	0.397	0.402			
MWS-L-8-16	59.20	1.0	0.190	0.204	0.217	0.231	0.245	0.258	0.272	0.285	0.299	0.312	0.326	0.340	0.353	0.367	0.380	0.394	0.408	0.421	0.435	0.448	0.462	0.476	0.489	0.496	0.503	0.509	0.516	0.523	0.530	0.537			
MWS-L-8-20	74.00	1.0	0.238	0.255	0.272	0.289	0.306	0.323	0.340	0.357	0.374	0.391	0.408	0.425	0.442	0.459	0.476	0.493	0.509	0.526	0.543	0.560	0.577	0.594	0.611	0.620	0.628	0.637	0.645	0.654	0.662	0.671			
MWS-L-10-20 or MWS-L-8-24	88.80	1.0	0.285	0.306	0.326	0.346	0.367	0.387	0.408	0.428	0.448	0.469	0.489	0.509	0.530	0.550	0.571	0.591	0.611	0.632	0.652	0.673	0.693	0.713	0.734	0.744	0.754	0.764	0.774	0.785	0.795	0.805			
4'x'4 media cage	14.80	1.0	0.048	0.051	0.054	0.058	0.061	0.065	0.068	0.071	0.075	0.078	0.082	0.085	0.088	0.092	0.095	0.099	0.102	0.105	0.109	0.112	0.115	0.119	0.122	0.124									

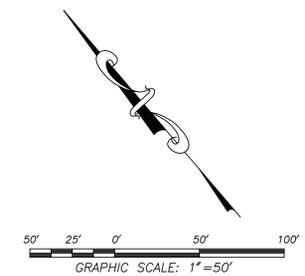
ATTACHMENT C

BMP SITE PLAN



LEGEND

-  BMP CATCHMENT AREA
-  EXISTING STORM DRAIN
-  DIRECTION OF FLOW
-  PERVIOUS AREAS
-  IMPERVIOUS AREAS
-  DRAINAGE AREA
AREA (ACRE)



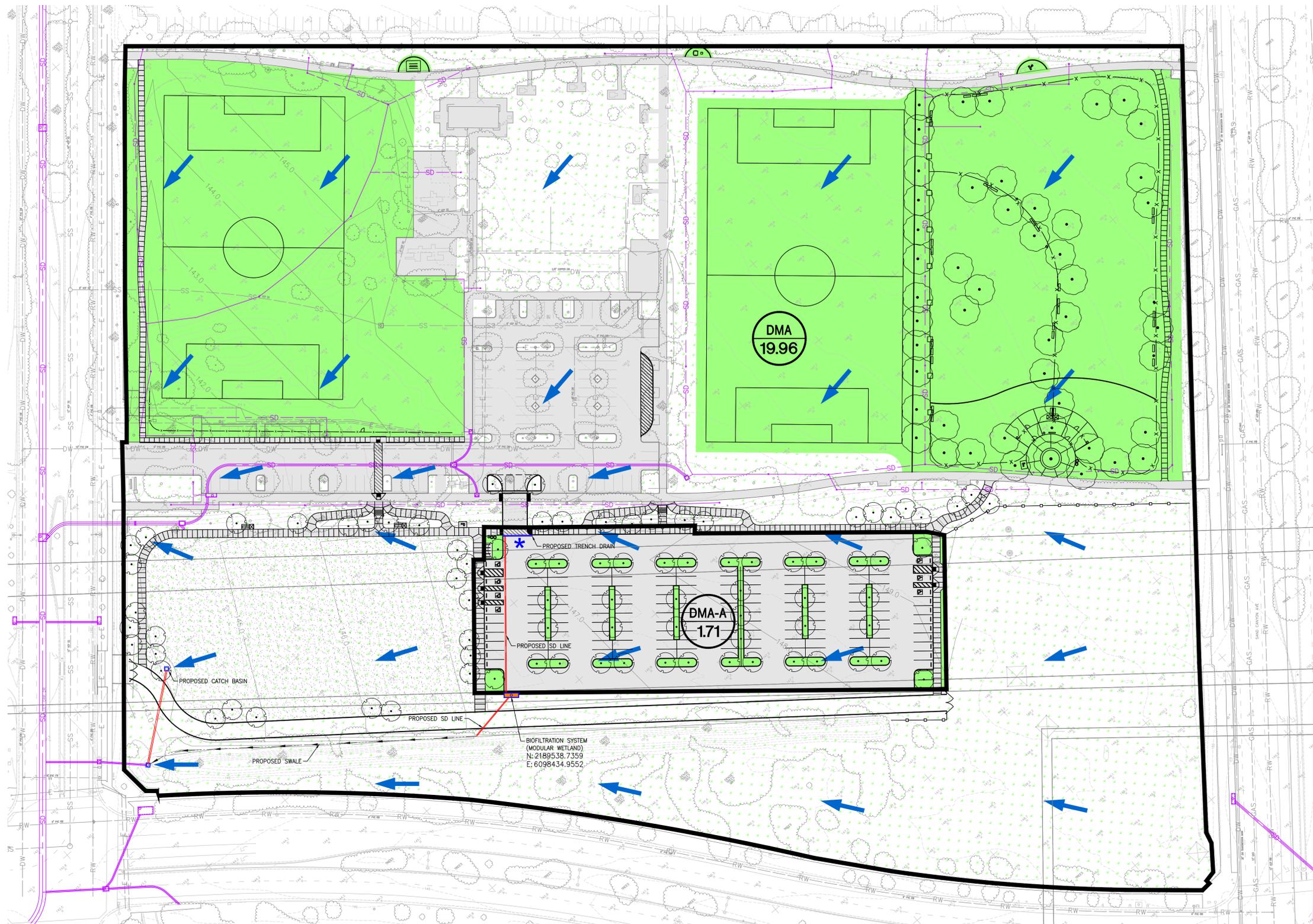
DRAINAGE AREAS					
DRAINAGE AREA	AREA (ACRE)	IMPERVIOUS AREA (ACRE)	PERVIOUS AREA (ACRE)	% IMPERVIOUS	% PERVIOUS
TOTAL	19.10	2.00	17.10	11	89

CITY OF IRVINE
OAK CREEK COMMUNITY PARK

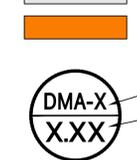
**WQMP EXHIBIT
EXISTING CONDITION**

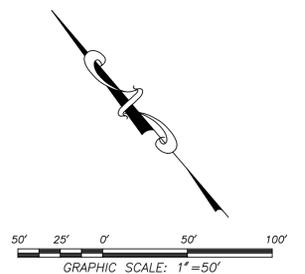
JOB NO.: 19-2260
DATE: 4/7/2022
DRAWN BY: GC
DESIGNED BY: GC
APPROVED BY: MO

SHEET
1 OF 2



LEGEND

-  BMP CATCHMENT AREA
-  SD EXISTING STORM DRAIN
-  SD PROPOSED STORM DRAIN
-  PROPOSED STORM DRAIN INLET
-  CATCH BASIN STENCILING
-  DIRECTION OF FLOW
-  PERVIOUS AREA
-  COMMON AREA EFFICIENT IRRIGATION AND RUN-OFF MINIMIZING LANDSCAPE
-  IMPERVIOUS AREA
-  BIOFILTRATION SYSTEM (BIOCLEAN MODULAR WETLAND SYSTEM)
-  DRAINAGE AREA
AREA (ACRE)



DRAINAGE AREAS					
DRAINAGE AREA	AREA (ACRE)	IMPERVIOUS AREA (ACRE)	PERVIOUS AREA (ACRE)	% IMPERVIOUS	% PERVIOUS
TOTAL	19.10	3.97	15.13	21	79

CITY OF IRVINE
OAK CREEK COMMUNITY PARK

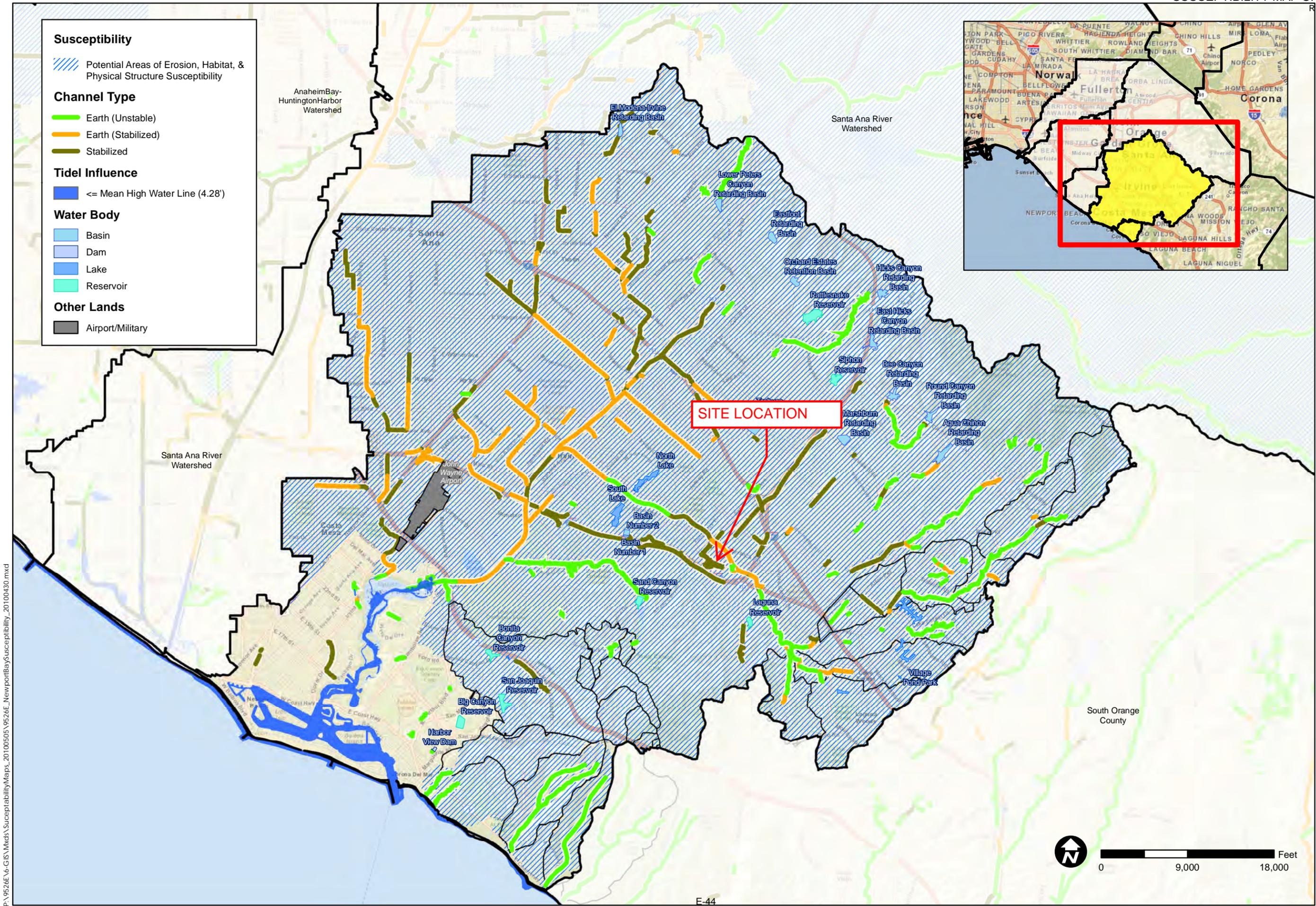
WQMP EXHIBIT
PROPOSED CONDITION

JOB NO.: 19-2260
DATE: 4/7/2022
DRAWN BY: GC
DESIGNED BY: GC
APPROVED BY: MO

SHEET
2 OF 2

ATTACHMENT D

HYDROMODIFICATION CALCULATIONS



Susceptibility

- Potential Areas of Erosion, Habitat, & Physical Structure Susceptibility

Channel Type

- Earth (Unstable)
- Earth (Stabilized)
- Stabilized

Tidel Influence

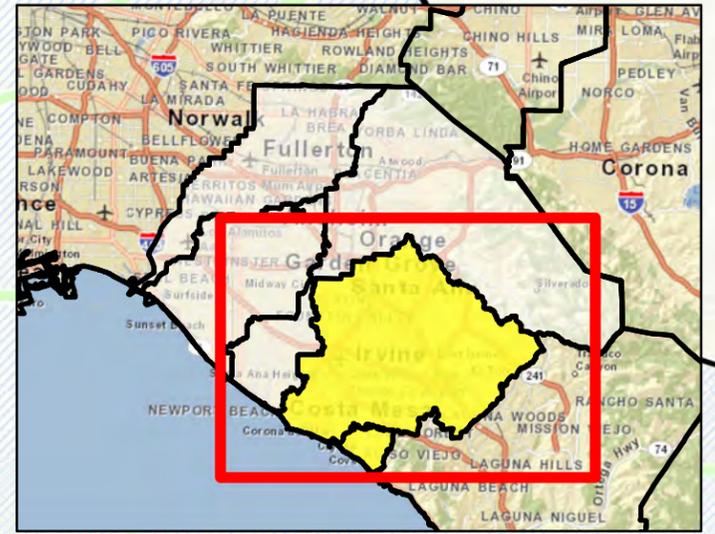
- <= Mean High Water Line (4.28')

Water Body

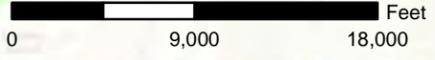
- Basin
- Dam
- Lake
- Reservoir

Other Lands

- Airport/Military



SITE LOCATION



TITLE
**SUSCEPTIBILITY ANALYSIS
 NEWPORT BAY-
 NEWPORT COASTAL STREAMS**

JOB
**ORANGE COUNTY
 WATERSHED
 MASTER PLANNING**

SCALE 1" = 12000'

DESIGNED	TH
DRAWING	TH
CHECKED	BMP
DATE	04/30/10
JOB NO.	9526 E



FIGURE
4

P:\9526E\6-GIS\Mxd\Susceptibility\Maps_20100505\9526E_NewportBaySusceptibility_20100430.mxd

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
(c) Copyright 1983-2008 Advanced Engineering Software (aes)
Ver. 15.0 Release Date: 04/01/2008 License ID 1204

Analysis prepared by:

ADAMS STREETER CIVIL ENGINEERS
16755 VON KARMAN AVENUE, SUITE 150
IRVINE, CA 92606
(949) 474-2330

***** DESCRIPTION OF STUDY *****

* 2-YEAR STORM EVENT HYDROLOGY ANALYSIS *
* OAKCREEK COMMUNITY PARK, IRVINE CALIFORNIA *
* EXISTING CONDITION *

FILE NAME: OAK02EXA.DAT
TIME/DATE OF STUDY: 15:59 04/04/2022

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 2.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 8.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN-SIDE / OUT-SIDE / PARK-WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES: LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.50	2.00	0.0313	0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 251.00
ELEVATION DATA: UPSTREAM (FEET) = 157.60 DOWNSTREAM (FEET) = 151.80

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.355

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.580

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	B	0.07	0.30	0.850	36	9.36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850

SUBAREA RUNOFF(CFS) = 0.08

TOTAL AREA(ACRES) = 0.07 PEAK FLOW RATE(CFS) = 0.08

FLOW PROCESS FROM NODE 2.00 TO NODE 3.00 IS CODE = 41

** WARNING: Computed Flowrate is less than 0.1 cfs,
Routing Algorithm is UNAVAILABLE.

FLOW PROCESS FROM NODE 3.00 TO NODE 3.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 9.36

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.580

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.24	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850

SUBAREA AREA(ACRES) = 0.24 SUBAREA RUNOFF(CFS) = 0.29

EFFECTIVE AREA(ACRES) = 0.31 AREA-AVERAGED Fm(INCH/HR) = 0.26

AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85

TOTAL AREA(ACRES) = 0.3 PEAK FLOW RATE(CFS) = 0.37

FLOW PROCESS FROM NODE 3.00 TO NODE 4.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0150

FLOW LENGTH(FEET) = 363.00 MANNING'S N = 0.010

DEPTH OF FLOW IN 8.0 INCH PIPE IS 2.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 4.12

GIVEN PIPE DIAMETER(INCH) = 8.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 0.37

PIPE TRAVEL TIME(MIN.) = 1.47 Tc(MIN.) = 10.82

LONGEST FLOWPATH FROM NODE 1.00 TO NODE 4.00 = 614.00 FEET.

FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 10.82

* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.453
SUBAREA LOSS RATE DATA (AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK B 0.46 0.30 0.850 36
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 0.46 SUBAREA RUNOFF (CFS) = 0.50
EFFECTIVE AREA (ACRES) = 0.77 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 0.8 PEAK FLOW RATE (CFS) = 0.83

FLOW PROCESS FROM NODE 4.00 TO NODE 5.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH (FEET) = 97.00 MANNING'S N = 0.010
DEPTH OF FLOW IN 8.0 INCH PIPE IS 3.8 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 5.11
GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 0.83
PIPE TRAVEL TIME (MIN.) = 0.32 Tc (MIN.) = 11.14
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 5.00 = 711.00 FEET.

FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 11.14
* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.429
SUBAREA LOSS RATE DATA (AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK B 0.11 0.30 0.850 36
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 0.11 SUBAREA RUNOFF (CFS) = 0.12
EFFECTIVE AREA (ACRES) = 0.88 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 0.9 PEAK FLOW RATE (CFS) = 0.93

FLOW PROCESS FROM NODE 5.00 TO NODE 6.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH (FEET) = 135.00 MANNING'S N = 0.010
DEPTH OF FLOW IN 8.0 INCH PIPE IS 4.0 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 5.25
GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 0.93

PIPE TRAVEL TIME (MIN.) = 0.43 Tc (MIN.) = 11.57
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 6.00 = 846.00 FEET.

FLOW PROCESS FROM NODE 6.00 TO NODE 6.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 11.57
* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.399
SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.77	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 0.77 SUBAREA RUNOFF (CFS) = 0.79
EFFECTIVE AREA (ACRES) = 1.65 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 1.6 PEAK FLOW RATE (CFS) = 1.70

FLOW PROCESS FROM NODE 6.00 TO NODE 7.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH (FEET) = 5.00 MANNING'S N = 0.010
DEPTH OF FLOW IN 12.0 INCH PIPE IS 4.6 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 6.08
GIVEN PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 1.70
PIPE TRAVEL TIME (MIN.) = 0.01 Tc (MIN.) = 11.58
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 7.00 = 851.00 FEET.

FLOW PROCESS FROM NODE 7.00 TO NODE 7.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 11.58
* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.398
SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	3.91	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 3.91 SUBAREA RUNOFF (CFS) = 4.02
EFFECTIVE AREA (ACRES) = 5.56 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 5.6 PEAK FLOW RATE (CFS) = 5.72

FLOW PROCESS FROM NODE 7.00 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0111
FLOW LENGTH (FEET) = 231.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 8.2 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 6.00
GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 5.72
PIPE TRAVEL TIME (MIN.) = 0.64 Tc (MIN.) = 12.22
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 8.00 = 1082.00 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION (MIN.) = 12.22
RAINFALL INTENSITY (INCH/HR) = 1.36
AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.85
EFFECTIVE STREAM AREA (ACRES) = 5.56
TOTAL STREAM AREA (ACRES) = 5.56
PEAK FLOW RATE (CFS) AT CONFLUENCE = 5.72

FLOW PROCESS FROM NODE 8.10 TO NODE 8.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 300.00
ELEVATION DATA: UPSTREAM (FEET) = 150.00 DOWNSTREAM (FEET) = 144.55

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 10.542

* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.475

SUBAREA Tc AND LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	B	0.76	0.30	0.850	36	10.54

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850

SUBAREA RUNOFF (CFS) = 0.83

TOTAL AREA (ACRES) = 0.76 PEAK FLOW RATE (CFS) = 0.83

FLOW PROCESS FROM NODE 8.20 TO NODE 8.30 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH (FEET) = 167.00 MANNING'S N = 0.010

DEPTH OF FLOW IN 8.0 INCH PIPE IS 3.8 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 5.10
 GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 0.83
 PIPE TRAVEL TIME (MIN.) = 0.55 Tc (MIN.) = 11.09
 LONGEST FLOWPATH FROM NODE 8.10 TO NODE 8.30 = 467.00 FEET.

FLOW PROCESS FROM NODE 8.30 TO NODE 8.30 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 11.09
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.433
 SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.60	0.30	0.100	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA (ACRES) = 0.60 SUBAREA RUNOFF (CFS) = 0.76
 EFFECTIVE AREA (ACRES) = 1.36 AREA-AVERAGED Fm (INCH/HR) = 0.16
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.52
 TOTAL AREA (ACRES) = 1.4 PEAK FLOW RATE (CFS) = 1.56

FLOW PROCESS FROM NODE 8.30 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0077
 FLOW LENGTH (FEET) = 37.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.2 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.74
 GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 1.56
 PIPE TRAVEL TIME (MIN.) = 0.17 Tc (MIN.) = 11.25
 LONGEST FLOWPATH FROM NODE 8.10 TO NODE 8.00 = 504.00 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION (MIN.) = 11.25
 RAINFALL INTENSITY (INCH/HR) = 1.42
 AREA-AVERAGED Fm (INCH/HR) = 0.16
 AREA-AVERAGED Fp (INCH/HR) = 0.30
 AREA-AVERAGED Ap = 0.52
 EFFECTIVE STREAM AREA (ACRES) = 1.36
 TOTAL STREAM AREA (ACRES) = 1.36
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 1.56

FLOW PROCESS FROM NODE 8.40 TO NODE 8.50 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 252.00
ELEVATION DATA: UPSTREAM(FEET) = 147.00 DOWNSTREAM(FEET) = 142.68

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.261

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.990

SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	B	0.44	0.30	0.100	36	6.26

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.100

SUBAREA RUNOFF(CFS) = 0.78

TOTAL AREA(ACRES) = 0.44 PEAK FLOW RATE(CFS) = 0.78

FLOW PROCESS FROM NODE 8.50 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0557

FLOW LENGTH(FEET) = 37.70 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.2 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 6.13

GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 0.78

PIPE TRAVEL TIME(MIN.) = 0.10 T_c (MIN.) = 6.36

LONGEST FLOWPATH FROM NODE 8.40 TO NODE 8.00 = 289.70 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:

TIME OF CONCENTRATION(MIN.) = 6.36

RAINFALL INTENSITY(INCH/HR) = 1.97

AREA-AVERAGED F_m (INCH/HR) = 0.03

AREA-AVERAGED F_p (INCH/HR) = 0.30

AREA-AVERAGED A_p = 0.10

EFFECTIVE STREAM AREA(ACRES) = 0.44

TOTAL STREAM AREA(ACRES) = 0.44

PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.78

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	T_c (MIN.)	Intensity (INCH/HR)	F_p (F_m) (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	5.72	12.22	1.355	0.30(0.26)	0.85	5.6	1.00
2	1.56	11.25	1.421	0.30(0.16)	0.52	1.4	8.10

3 0.78 6.36 1.971 0.30(0.03) 0.10 0.4 8.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.69	6.36	1.971	0.30(0.21)	0.71	4.1	8.40
2	7.70	11.25	1.421	0.30(0.22)	0.74	6.9	8.10
3	7.73	12.22	1.355	0.30(0.22)	0.74	7.4	1.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 7.73 Tc(MIN.) = 12.22
 EFFECTIVE AREA(ACRES) = 7.36 AREA-AVERAGED Fm(INCH/HR) = 0.22
 AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.74
 TOTAL AREA(ACRES) = 7.4
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 8.00 = 1082.00 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 9.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0050
 FLOW LENGTH(FEET) = 261.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 12.1 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.85
 GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 7.73
 PIPE TRAVEL TIME(MIN.) = 0.90 Tc(MIN.) = 13.12
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 9.00 = 1343.00 FEET.

FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 13.12
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.301
 SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.52	0.30	0.100	36
PUBLIC PARK	B	3.04	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.740
 SUBAREA AREA(ACRES) = 3.56 SUBAREA RUNOFF(CFS) = 3.46
 EFFECTIVE AREA(ACRES) = 10.92 AREA-AVERAGED Fm(INCH/HR) = 0.22
 AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.74
 TOTAL AREA(ACRES) = 10.9 PEAK FLOW RATE(CFS) = 10.60

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.08	7.29	1.823	0.30(0.22)	0.72	7.7	8.40

2 10.74 12.15 1.360 0.30(0.22) 0.74 10.5 8.10
3 10.60 13.12 1.301 0.30(0.22) 0.74 10.9 1.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE (CFS) = 11.08 Tc (MIN.) = 7.29
AREA-AVERAGED Fm (INCH/HR) = 0.22 AREA-AVERAGED Fp (INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.72 EFFECTIVE AREA (ACRES) = 7.66

FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 7.29
* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.823
SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.31	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 0.31 SUBAREA RUNOFF (CFS) = 0.44
EFFECTIVE AREA (ACRES) = 7.97 AREA-AVERAGED Fm (INCH/HR) = 0.22
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.73
TOTAL AREA (ACRES) = 11.2 PEAK FLOW RATE (CFS) = 11.51

FLOW PROCESS FROM NODE 9.00 TO NODE 10.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0050
FLOW LENGTH (FEET) = 45.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.6 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 5.31
GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 11.51
PIPE TRAVEL TIME (MIN.) = 0.14 Tc (MIN.) = 7.43
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 10.00 = 1388.00 FEET.

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0100
FLOW LENGTH (FEET) = 43.70 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 10.4 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 6.80
GIVEN PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 11.51
PIPE TRAVEL TIME (MIN.) = 0.11 Tc (MIN.) = 7.54
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 11.00 = 1431.70 FEET.

FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
=====

REPRESENTATIVE SLOPE = 0.0100
FLOW LENGTH(FEET) = 93.90 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 10.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.80
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 11.51
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 7.77
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 1525.60 FEET.
=====

=====

END OF RATIONAL METHOD ANALYSIS

FLOW PROCESS FROM NODE 21.00 TO NODE 22.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 2.35
ELEVATION DATA: UPSTREAM(FEET) = 154.00 DOWNSTREAM(FEET) = 149.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.000
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 2.264

SUBAREA Tc AND LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
NATURAL POOR COVER
"BARREN" B 0.63 0.30 1.000 72 5.00
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA RUNOFF(CFS) = 1.11
TOTAL AREA(ACRES) = 0.63 PEAK FLOW RATE(CFS) = 1.11

FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 149.00 DOWNSTREAM(FEET) = 139.90
CHANNEL LENGTH THRU SUBAREA(FEET) = 858.00 CHANNEL SLOPE = 0.0106
CHANNEL FLOW THRU SUBAREA(CFS) = 1.11
FLOW VELOCITY(FEET/SEC) = 1.58 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 9.07 Tc(MIN.) = 14.07
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 23.00 = 860.35 FEET.

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 14.07
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.250
SUBAREA LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
NATURAL POOR COVER
"BARREN" B 4.59 0.30 1.000 72
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA AREA(ACRES) = 4.59 SUBAREA RUNOFF(CFS) = 3.92
EFFECTIVE AREA(ACRES) = 5.22 AREA-AVERAGED Fm(INCH/HR) = 0.30
AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 5.2 PEAK FLOW RATE(CFS) = 4.46

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 14.07
RAINFALL INTENSITY(INCH/HR) = 1.25
AREA-AVERAGED Fm(INCH/HR) = 0.30
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 1.00
EFFECTIVE STREAM AREA(ACRES) = 5.22
TOTAL STREAM AREA(ACRES) = 5.22
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.46

FLOW PROCESS FROM NODE 23.10 TO NODE 23.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 285.00
ELEVATION DATA: UPSTREAM(FEET) = 150.80 DOWNSTREAM(FEET) = 147.80

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 12.521

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.337

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER						
"BARREN"	B	0.84	0.30	1.000	72	12.52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000

SUBAREA RUNOFF(CFS) = 0.78

TOTAL AREA(ACRES) = 0.84 PEAK FLOW RATE(CFS) = 0.78

FLOW PROCESS FROM NODE 23.20 TO NODE 23.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 147.80 DOWNSTREAM(FEET) = 139.90
CHANNEL LENGTH THRU SUBAREA(FEET) = 791.00 CHANNEL SLOPE = 0.0100
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.78
FLOW VELOCITY(FEET/SEC) = 1.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 8.79 Tc(MIN.) = 21.32
LONGEST FLOWPATH FROM NODE 23.10 TO NODE 23.00 = 1076.00 FEET.

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 21.32

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 0.985

SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER "BARREN"	B	1.81	0.30	1.000	72
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000					
SUBAREA AREA(ACRES) = 1.81		SUBAREA RUNOFF(CFS) = 1.12			
EFFECTIVE AREA(ACRES) = 2.65		AREA-AVERAGED Fm(INCH/HR) = 0.30			
AREA-AVERAGED Fp(INCH/HR) = 0.30		AREA-AVERAGED Ap = 1.00			
TOTAL AREA(ACRES) = 2.6		PEAK FLOW RATE(CFS) = 1.63			

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 21.32
RAINFALL INTENSITY(INCH/HR) = 0.98
AREA-AVERAGED Fm(INCH/HR) = 0.30
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 1.00
EFFECTIVE STREAM AREA(ACRES) = 2.65
TOTAL STREAM AREA(ACRES) = 2.65
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.63

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	4.46	14.07	1.250	0.30(0.30)	1.00	5.2	21.00
2	1.63	21.32	0.985	0.30(0.30)	1.00	2.6	23.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.96	14.07	1.250	0.30(0.30)	1.00	7.0	21.00
2	4.85	21.32	0.985	0.30(0.30)	1.00	7.9	23.10

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 5.96 Tc(MIN.) = 14.07
EFFECTIVE AREA(ACRES) = 6.97 AREA-AVERAGED Fm(INCH/HR) = 0.30
AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 7.9
LONGEST FLOWPATH FROM NODE 23.10 TO NODE 23.00 = 1076.00 FEET.

FLOW PROCESS FROM NODE 23.00 TO NODE 24.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0100

FLOW LENGTH (FEET) = 45.70 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.0 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 5.89
 GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 5.96
 PIPE TRAVEL TIME (MIN.) = 0.13 Tc (MIN.) = 14.20
 LONGEST FLOWPATH FROM NODE 23.10 TO NODE 24.00 = 1121.70 FEET.

=====
 END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 7.9 TC (MIN.) = 14.20
 EFFECTIVE AREA (ACRES) = 6.97 AREA-AVERAGED Fm (INCH/HR) = 0.30
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 1.000
 PEAK FLOW RATE (CFS) = 5.96

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.96	14.20	1.243	0.30 (0.30)	1.00	7.0	21.00
2	4.85	21.45	0.981	0.30 (0.30)	1.00	7.9	23.10

=====
 END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
(c) Copyright 1983-2008 Advanced Engineering Software (aes)
Ver. 15.0 Release Date: 04/01/2008 License ID 1204

Analysis prepared by:

ADAMS STREETER CIVIL ENGINEERS
16755 VON KARMAN AVENUE, SUITE 150
IRVINE, CA 92606
(949) 474-2330

***** DESCRIPTION OF STUDY *****
* 2-YEAR STORM EVENT HYDROLOGY ANYLISIS *
* OAKCREEK COMMUNITY PARK, IRVINE CALIFORNIA *
* PROPOSED CONDITION *

FILE NAME: OAK02PRA.DAT
TIME/DATE OF STUDY: 16:01 04/04/2022

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 2.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 8.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/ SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.50	2.00	0.0313	0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 251.00
ELEVATION DATA: UPSTREAM (FEET) = 157.00 DOWNSTREAM (FEET) = 151.80

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION CHANGE)]^{**} 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 9.562
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.560
 SUBAREA T_c AND LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.07	0.30	0.850	36	9.56

 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA RUNOFF (CFS) = 0.08
 TOTAL AREA (ACRES) = 0.07 PEAK FLOW RATE (CFS) = 0.08

 FLOW PROCESS FROM NODE 2.00 TO NODE 3.00 IS CODE = 41

** WARNING: Computed Flowrate is less than 0.1 cfs,
 Routing Algorithm is UNAVAILABLE.

 FLOW PROCESS FROM NODE 3.00 TO NODE 3.00 IS CODE = 81

>>>> ADDITION OF SUBAREA TO MAINLINE PEAK FLOW <<<<<

=====

MAINLINE T_c (MIN.) = 9.56
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.560
 SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
PUBLIC PARK	B	0.24	0.30	0.850	36

 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA AREA (ACRES) = 0.24 SUBAREA RUNOFF (CFS) = 0.28
 EFFECTIVE AREA (ACRES) = 0.31 AREA-AVERAGED F_m (INCH/HR) = 0.26
 AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 0.85
 TOTAL AREA (ACRES) = 0.3 PEAK FLOW RATE (CFS) = 0.36

 FLOW PROCESS FROM NODE 3.00 TO NODE 4.00 IS CODE = 41

>>>> COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA <<<<<
 >>>> USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT) <<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
 FLOW LENGTH (FEET) = 363.00 MANNING'S N = 0.010
 DEPTH OF FLOW IN 8.0 INCH PIPE IS 2.4 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 4.06
 GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 0.36
 PIPE TRAVEL TIME (MIN.) = 1.49 T_c (MIN.) = 11.05
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 4.00 = 614.00 FEET.

 FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 81

>>>> ADDITION OF SUBAREA TO MAINLINE PEAK FLOW <<<<<

=====

MAINLINE T_c (MIN.) = 11.05

* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.436
SUBAREA LOSS RATE DATA (AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK B 2.53 0.30 0.850 36
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 2.53 SUBAREA RUNOFF (CFS) = 2.69
EFFECTIVE AREA (ACRES) = 2.84 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 2.8 PEAK FLOW RATE (CFS) = 3.02

FLOW PROCESS FROM NODE 4.00 TO NODE 5.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH (FEET) = 97.00 MANNING'S N = 0.010
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY (FEET/SEC.) = 8.65
PIPE FLOW VELOCITY = (TOTAL FLOW) / (PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 3.02
PIPE TRAVEL TIME (MIN.) = 0.19 Tc (MIN.) = 11.24
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 5.00 = 711.00 FEET.

FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 11.24
* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.422
SUBAREA LOSS RATE DATA (AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK B 0.25 0.30 0.850 36
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 0.25 SUBAREA RUNOFF (CFS) = 0.26
EFFECTIVE AREA (ACRES) = 3.09 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 3.1 PEAK FLOW RATE (CFS) = 3.25

FLOW PROCESS FROM NODE 5.00 TO NODE 6.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH (FEET) = 135.00 MANNING'S N = 0.010
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY (FEET/SEC.) = 9.30
PIPE FLOW VELOCITY = (TOTAL FLOW) / (PIPE CROSS SECTION AREA)

GIVEN PIPE DIAMETER(INCH) = 8.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 3.25
 PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 11.48
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 6.00 = 846.00 FEET.

 FLOW PROCESS FROM NODE 6.00 TO NODE 6.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 11.48
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.405
 SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.71	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
 SUBAREA AREA(ACRES) = 0.71 SUBAREA RUNOFF(CFS) = 0.73
 EFFECTIVE AREA(ACRES) = 3.80 AREA-AVERAGED Fm(INCH/HR) = 0.26
 AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
 TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 3.93

 FLOW PROCESS FROM NODE 6.00 TO NODE 7.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
 FLOW LENGTH(FEET) = 5.00 MANNING'S N = 0.010
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.48
 GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 3.93
 PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 11.49
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 7.00 = 851.00 FEET.

 FLOW PROCESS FROM NODE 7.00 TO NODE 7.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 11.49
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.404
 SUBAREA LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	2.01	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
 SUBAREA AREA(ACRES) = 2.01 SUBAREA RUNOFF(CFS) = 2.08
 EFFECTIVE AREA(ACRES) = 5.81 AREA-AVERAGED Fm(INCH/HR) = 0.26
 AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
 TOTAL AREA(ACRES) = 5.8 PEAK FLOW RATE(CFS) = 6.01

FLOW PROCESS FROM NODE 7.00 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0111
FLOW LENGTH(FEET) = 231.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 8.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.08
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.01
PIPE TRAVEL TIME(MIN.) = 0.63 Tc(MIN.) = 12.12
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 8.00 = 1082.00 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.12
RAINFALL INTENSITY(INCH/HR) = 1.36
AREA-AVERAGED Fm(INCH/HR) = 0.26
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.85
EFFECTIVE STREAM AREA(ACRES) = 5.81
TOTAL STREAM AREA(ACRES) = 5.81
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.01

FLOW PROCESS FROM NODE 8.10 TO NODE 8.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 150.00 DOWNSTREAM(FEET) = 144.55

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 10.542

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.475

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	B	0.76	0.30	0.850	36	10.54

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850

SUBAREA RUNOFF(CFS) = 0.83

TOTAL AREA(ACRES) = 0.76 PEAK FLOW RATE(CFS) = 0.83

FLOW PROCESS FROM NODE 8.20 TO NODE 8.30 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0150
 FLOW LENGTH (FEET) = 167.00 MANNING'S N = 0.010
 DEPTH OF FLOW IN 8.0 INCH PIPE IS 3.8 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 5.10
 GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 0.83
 PIPE TRAVEL TIME (MIN.) = 0.55 Tc (MIN.) = 11.09
 LONGEST FLOWPATH FROM NODE 8.10 TO NODE 8.30 = 467.00 FEET.

 FLOW PROCESS FROM NODE 8.30 TO NODE 8.30 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 11.09
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.433
 SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.51	0.30	0.100	36

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA (ACRES) = 0.51 SUBAREA RUNOFF (CFS) = 0.64
 EFFECTIVE AREA (ACRES) = 1.27 AREA-AVERAGED Fm (INCH/HR) = 0.16
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.55
 TOTAL AREA (ACRES) = 1.3 PEAK FLOW RATE (CFS) = 1.45

 FLOW PROCESS FROM NODE 8.30 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0077
 FLOW LENGTH (FEET) = 37.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.0 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.66
 GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 1.45
 PIPE TRAVEL TIME (MIN.) = 0.17 Tc (MIN.) = 11.26
 LONGEST FLOWPATH FROM NODE 8.10 TO NODE 8.00 = 504.00 FEET.

 FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION (MIN.) = 11.26
 RAINFALL INTENSITY (INCH/HR) = 1.42
 AREA-AVERAGED Fm (INCH/HR) = 0.16
 AREA-AVERAGED Fp (INCH/HR) = 0.30
 AREA-AVERAGED Ap = 0.55
 EFFECTIVE STREAM AREA (ACRES) = 1.27
 TOTAL STREAM AREA (ACRES) = 1.27
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 1.45

FLOW PROCESS FROM NODE 8.40 TO NODE 8.50 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 255.00
ELEVATION DATA: UPSTREAM (FEET) = 147.00 DOWNSTREAM (FEET) = 142.68

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 6.305

* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.982

SUBAREA T_c AND LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
COMMERCIAL	B	0.45	0.30	0.100	36	6.31

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.100

SUBAREA RUNOFF (CFS) = 0.79

TOTAL AREA (ACRES) = 0.45 PEAK FLOW RATE (CFS) = 0.79

FLOW PROCESS FROM NODE 8.50 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0557
FLOW LENGTH (FEET) = 37.70 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.3 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 6.14
GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 0.79
PIPE TRAVEL TIME (MIN.) = 0.10 T_c (MIN.) = 6.41
LONGEST FLOWPATH FROM NODE 8.40 TO NODE 8.00 = 292.70 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION (MIN.) = 6.41
RAINFALL INTENSITY (INCH/HR) = 1.96
AREA-AVERAGED F_m (INCH/HR) = 0.03
AREA-AVERAGED F_p (INCH/HR) = 0.30
AREA-AVERAGED A_p = 0.10
EFFECTIVE STREAM AREA (ACRES) = 0.45
TOTAL STREAM AREA (ACRES) = 0.45
PEAK FLOW RATE (CFS) AT CONFLUENCE = 0.79

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	T_c (MIN.)	Intensity (INCH/HR)	F_p (F_m) (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
------------------	------------	-----------------	------------------------	------------------------------	-------	------------------	-------------------

1	6.01	12.12	1.361	0.30 (0.26)	0.85	5.8	1.00
2	1.45	11.26	1.421	0.30 (0.16)	0.55	1.3	8.10
3	0.79	6.41	1.963	0.30 (0.03)	0.10	0.4	8.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.87	6.41	1.963	0.30 (0.22)	0.72	4.2	8.40
2	7.90	11.26	1.421	0.30 (0.22)	0.75	7.1	8.10
3	7.93	12.12	1.361	0.30 (0.23)	0.75	7.5	1.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 7.93 Tc (MIN.) = 12.12
EFFECTIVE AREA (ACRES) = 7.53 AREA-AVERAGED Fm (INCH/HR) = 0.23
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.75
TOTAL AREA (ACRES) = 7.5
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 8.00 = 1082.00 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 9.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0050
FLOW LENGTH (FEET) = 261.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 12.3 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 4.88
GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 7.93
PIPE TRAVEL TIME (MIN.) = 0.89 Tc (MIN.) = 13.01
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 9.00 = 1343.00 FEET.

FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 13.01
* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.307
SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.50	0.30	0.100	36
PUBLIC PARK	B	3.13	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.747
SUBAREA AREA (ACRES) = 3.63 SUBAREA RUNOFF (CFS) = 3.54
EFFECTIVE AREA (ACRES) = 11.16 AREA-AVERAGED Fm (INCH/HR) = 0.23
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.75
TOTAL AREA (ACRES) = 11.2 PEAK FLOW RATE (CFS) = 10.86

** PEAK FLOW RATE TABLE **

STREAM	Q	Tc	Intensity	Fp (Fm)	Ap	Ae	HEADWATER
--------	---	----	-----------	---------	----	----	-----------

NUMBER	(CFS)	(MIN.)	(INCH/HR)	(INCH/HR)	(ACRES)	NODE
1	11.32	7.33	1.817	0.30 (0.22)	0.73	8.40
2	10.98	12.15	1.360	0.30 (0.22)	0.75	8.10
3	10.86	13.01	1.307	0.30 (0.23)	0.75	1.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE (CFS) = 11.32 Tc (MIN.) = 7.33
 AREA-AVERAGED Fm (INCH/HR) = 0.22 AREA-AVERAGED Fp (INCH/HR) = 0.30
 AREA-AVERAGED Ap = 0.73 EFFECTIVE AREA (ACRES) = 7.87

 FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 7.33
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.817
 SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.33	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
 SUBAREA AREA (ACRES) = 0.33 SUBAREA RUNOFF (CFS) = 0.46
 EFFECTIVE AREA (ACRES) = 8.20 AREA-AVERAGED Fm (INCH/HR) = 0.22
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.74
 TOTAL AREA (ACRES) = 11.5 PEAK FLOW RATE (CFS) = 11.79

 FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 7.33
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.817
 SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.22	0.30	0.850	36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
 SUBAREA AREA (ACRES) = 0.22 SUBAREA RUNOFF (CFS) = 0.31
 EFFECTIVE AREA (ACRES) = 8.42 AREA-AVERAGED Fm (INCH/HR) = 0.22
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.74
 TOTAL AREA (ACRES) = 11.7 PEAK FLOW RATE (CFS) = 12.10

 FLOW PROCESS FROM NODE 9.00 TO NODE 10.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0050
 FLOW LENGTH (FEET) = 45.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 5.36
 GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 12.10

PIPE TRAVEL TIME (MIN.) = 0.14 Tc (MIN.) = 7.47
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 10.00 = 1388.00 FEET.

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0100
FLOW LENGTH (FEET) = 43.70 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 10.7 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 6.90
GIVEN PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 12.10
PIPE TRAVEL TIME (MIN.) = 0.11 Tc (MIN.) = 7.58
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 11.00 = 1431.70 FEET.

FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0100
FLOW LENGTH (FEET) = 93.90 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 10.7 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 6.90
GIVEN PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 12.10
PIPE TRAVEL TIME (MIN.) = 0.23 Tc (MIN.) = 7.80
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 1525.60 FEET.

END OF RATIONAL METHOD ANALYSIS

FLOW PROCESS FROM NODE 21.00 TO NODE 22.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 314.00
ELEVATION DATA: UPSTREAM(FEET) = 154.00 DOWNSTREAM(FEET) = 148.60

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.799
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.383

SUBAREA Tc AND LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
NATURAL POOR COVER
"BARREN" B 0.88 0.30 1.000 72 11.80
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA RUNOFF(CFS) = 0.86
TOTAL AREA(ACRES) = 0.88 PEAK FLOW RATE(CFS) = 0.86

FLOW PROCESS FROM NODE 22.00 TO NODE 22.50 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 148.60 DOWNSTREAM(FEET) = 143.90
CHANNEL LENGTH THRU SUBAREA(FEET) = 472.00 CHANNEL SLOPE = 0.0100
NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION
CHANNEL FLOW THRU SUBAREA(CFS) = 0.86
FLOW VELOCITY(FEET/SEC) = 1.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 5.26 Tc(MIN.) = 17.05
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 22.50 = 786.00 FEET.

FLOW PROCESS FROM NODE 22.50 TO NODE 22.50 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 17.05
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.119
SUBAREA LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK B 0.48 0.30 0.850 36
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA(ACRES) = 0.48 SUBAREA RUNOFF(CFS) = 0.37
EFFECTIVE AREA(ACRES) = 1.36 AREA-AVERAGED Fm(INCH/HR) = 0.28
AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.95
TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 1.02

FLOW PROCESS FROM NODE 22.50 TO NODE 22.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 17.05
RAINFALL INTENSITY(INCH/HR) = 1.12
AREA-AVERAGED Fm(INCH/HR) = 0.28
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.95
EFFECTIVE STREAM AREA(ACRES) = 1.36
TOTAL STREAM AREA(ACRES) = 1.36
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.02

FLOW PROCESS FROM NODE 22.51 TO NODE 22.52 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 283.30
ELEVATION DATA: UPSTREAM(FEET) = 150.40 DOWNSTREAM(FEET) = 147.40

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.224

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.833

SUBAREA Tc AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	B	0.71	0.30	0.100	36	7.22

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA RUNOFF(CFS) = 1.15

TOTAL AREA(ACRES) = 0.71 PEAK FLOW RATE(CFS) = 1.15

FLOW PROCESS FROM NODE 22.52 TO NODE 22.53 IS CODE = 61

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

REPRESENTATIVE SLOPE = 0.0050
STREET LENGTH(FEET) = 220.70 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 20.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 10.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.73

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.32

HALFSTREET FLOOD WIDTH(FEET) = 9.90

AVERAGE FLOW VELOCITY (FEET/SEC.) = 1.58
 PRODUCT OF DEPTH&VELOCITY (FT*FT/SEC.) = 0.51
 STREET FLOW TRAVEL TIME (MIN.) = 2.33 Tc (MIN.) = 9.56
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.561
 SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.84	0.30	0.100	36

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA (ACRES) = 0.84 SUBAREA RUNOFF (CFS) = 1.16
 EFFECTIVE AREA (ACRES) = 1.55 AREA-AVERAGED Fm (INCH/HR) = 0.03
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.10
 TOTAL AREA (ACRES) = 1.5 PEAK FLOW RATE (CFS) = 2.14

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.34 HALFSTREET FLOOD WIDTH (FEET) = 10.82
 FLOW VELOCITY (FEET/SEC.) = 1.66 DEPTH*VELOCITY (FT*FT/SEC.) = 0.57
 LONGEST FLOWPATH FROM NODE 22.51 TO NODE 22.53 = 504.00 FEET.

FLOW PROCESS FROM NODE 22.53 TO NODE 22.53 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 9.56
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.561
 SUBAREA LOSS RATE DATA (AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.15	0.30	0.100	36

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA (ACRES) = 0.15 SUBAREA RUNOFF (CFS) = 0.21
 EFFECTIVE AREA (ACRES) = 1.70 AREA-AVERAGED Fm (INCH/HR) = 0.03
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.10
 TOTAL AREA (ACRES) = 1.7 PEAK FLOW RATE (CFS) = 2.34

FLOW PROCESS FROM NODE 22.53 TO NODE 22.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

REPRESENTATIVE SLOPE = 0.0100
 FLOW LENGTH (FEET) = 50.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.4 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 4.64
 ESTIMATED PIPE DIAMETER (INCH) = 12.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 2.34
 PIPE TRAVEL TIME (MIN.) = 0.18 Tc (MIN.) = 9.74
 LONGEST FLOWPATH FROM NODE 22.51 TO NODE 22.50 = 554.00 FEET.

FLOW PROCESS FROM NODE 22.50 TO NODE 22.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.74
RAINFALL INTENSITY(INCH/HR) = 1.54
AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 1.70
TOTAL STREAM AREA(ACRES) = 1.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.34

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	1.02	17.05	1.119	0.30(0.28)	0.95	1.4	21.00
2	2.34	9.74	1.544	0.30(0.03)	0.10	1.7	22.51

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	3.22	9.74	1.544	0.30(0.11)	0.37	2.5	22.51
2	2.71	17.05	1.119	0.30(0.14)	0.48	3.1	21.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 3.22 Tc(MIN.) = 9.74
EFFECTIVE AREA(ACRES) = 2.48 AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.37
TOTAL AREA(ACRES) = 3.1
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 22.50 = 786.00 FEET.

FLOW PROCESS FROM NODE 22.50 TO NODE 23.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 143.90 DOWNSTREAM(FEET) = 139.80
CHANNEL LENGTH THRU SUBAREA(FEET) = 325.40 CHANNEL SLOPE = 0.0126
CHANNEL FLOW THRU SUBAREA(CFS) = 3.22
FLOW VELOCITY(FEET/SEC) = 2.14 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.53 Tc(MIN.) = 12.27
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 23.00 = 1111.40 FEET.

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 12.27
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.352
SUBAREA LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS

LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 PUBLIC PARK B 0.25 0.30 0.850 36
 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA AREA(ACRES) = 0.25 SUBAREA RUNOFF(CFS) = 0.25
 EFFECTIVE AREA(ACRES) = 2.73 AREA-AVERAGED F_m (INCH/HR) = 0.12
 AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 0.41
 TOTAL AREA(ACRES) = 3.3 PEAK FLOW RATE(CFS) = 3.22
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 12.27
 RAINFALL INTENSITY(INCH/HR) = 1.35
 AREA-AVERAGED F_m (INCH/HR) = 0.12
 AREA-AVERAGED F_p (INCH/HR) = 0.30
 AREA-AVERAGED A_p = 0.41
 EFFECTIVE STREAM AREA(ACRES) = 2.73
 TOTAL STREAM AREA(ACRES) = 3.31
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.22

FLOW PROCESS FROM NODE 23.10 TO NODE 23.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 285.00
 ELEVATION DATA: UPSTREAM(FEET) = 150.80 DOWNSTREAM(FEET) = 147.80

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 12.521

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.337

SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
-------------------------------	-------------------	-----------------	--------------------	--------------------	-----------	-----------------

NATURAL POOR COVER

"BARREN"	B	0.84	0.30	1.000	72	12.52
----------	---	------	------	-------	----	-------

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000

SUBAREA RUNOFF(CFS) = 0.78

TOTAL AREA(ACRES) = 0.84 PEAK FLOW RATE(CFS) = 0.78

FLOW PROCESS FROM NODE 23.20 TO NODE 23.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 147.80 DOWNSTREAM(FEET) = 139.60

CHANNEL LENGTH THRU SUBAREA(FEET) = 815.80 CHANNEL SLOPE = 0.0101

NOTE: CHANNEL FLOW OF 1. CFS WAS ASSUMED IN VELOCITY ESTIMATION

CHANNEL FLOW THRU SUBAREA(CFS) = 0.78
 FLOW VELOCITY(FEET/SEC) = 1.50 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
 TRAVEL TIME(MIN.) = 9.04 Tc(MIN.) = 21.56
 LONGEST FLOWPATH FROM NODE 23.10 TO NODE 23.00 = 1100.80 FEET.

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 21.56
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 0.978
 SUBAREA LOSS RATE DATA(AMC I):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 NATURAL POOR COVER
 "BARREN" B 1.81 0.30 1.000 72
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA(ACRES) = 1.81 SUBAREA RUNOFF(CFS) = 1.11
 EFFECTIVE AREA(ACRES) = 2.65 AREA-AVERAGED Fm(INCH/HR) = 0.30
 AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 1.00
 TOTAL AREA(ACRES) = 2.6 PEAK FLOW RATE(CFS) = 1.62

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 21.56
 RAINFALL INTENSITY(INCH/HR) = 0.98
 AREA-AVERAGED Fm(INCH/HR) = 0.30
 AREA-AVERAGED Fp(INCH/HR) = 0.30
 AREA-AVERAGED Ap = 1.00
 EFFECTIVE STREAM AREA(ACRES) = 2.65
 TOTAL STREAM AREA(ACRES) = 2.65
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.62

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	3.22	12.27	1.352	0.30(0.12)	0.41	2.7	22.51
1	2.71	19.69	1.031	0.30(0.15)	0.50	3.3	21.00
2	1.62	21.56	0.978	0.30(0.30)	1.00	2.6	23.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	4.65	12.27	1.352	0.30(0.19)	0.62	4.2	22.51
2	4.30	19.69	1.031	0.30(0.21)	0.71	5.7	21.00
3	4.16	21.56	0.978	0.30(0.22)	0.72	6.0	23.10

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 4.65 Tc (MIN.) = 12.27
EFFECTIVE AREA (ACRES) = 4.23 AREA-AVERAGED Fm (INCH/HR) = 0.19
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.62
TOTAL AREA (ACRES) = 6.0
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 23.00 = 1111.40 FEET.

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 12.27
* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.352
SUBAREA LOSS RATE DATA (AMC I):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK B 1.49 0.30 0.850 36
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 1.49 SUBAREA RUNOFF (CFS) = 1.47
EFFECTIVE AREA (ACRES) = 5.72 AREA-AVERAGED Fm (INCH/HR) = 0.20
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.68
TOTAL AREA (ACRES) = 7.4 PEAK FLOW RATE (CFS) = 5.92

FLOW PROCESS FROM NODE 23.00 TO NODE 24.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0100
FLOW LENGTH (FEET) = 45.70 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.0 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 5.88
GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 5.92
PIPE TRAVEL TIME (MIN.) = 0.13 Tc (MIN.) = 12.40
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 24.00 = 1157.10 FEET.

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 7.4 TC (MIN.) = 12.40
EFFECTIVE AREA (ACRES) = 5.72 AREA-AVERAGED Fm (INCH/HR) = 0.20
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.680
PEAK FLOW RATE (CFS) = 5.92

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	5.92	12.40	1.344	0.30 (0.20)	0.68	5.7	22.51
2	5.25	19.82	1.027	0.30 (0.22)	0.74	7.2	21.00
3	5.05	21.70	0.975	0.30 (0.22)	0.75	7.4	23.10

END OF RATIONAL METHOD ANALYSIS

Appendix I
Proposed Q₁₀ Hydrology Calculations

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
(c) Copyright 1983-2008 Advanced Engineering Software (aes)
Ver. 15.0 Release Date: 04/01/2008 License ID 1204

Analysis prepared by:

ADAMS STREETER CIVIL ENGINEERS
16755 VON KARMAN AVENUE, SUITE 150
IRVINE, CA 92606
(949) 474-2330

***** DESCRIPTION OF STUDY *****
* 10-YEAR STORM EVENT HYDROLOGY ANALYSIS *
* OAKCREEK COMMUNITY PARK, IRVINE CALIFORNIA *
* PROPOSED CONDITION *

FILE NAME: OAK10PRA.DAT
TIME/DATE OF STUDY: 16:13 04/04/2022

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 10.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 8.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.50	2.00	0.0313	0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 251.00
ELEVATION DATA: UPSTREAM (FEET) = 157.00 DOWNSTREAM (FEET) = 151.80

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 9.562
 * 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.800
 SUBAREA T_c AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.07	0.30	0.850	56	9.56

 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA RUNOFF (CFS) = 0.16
 TOTAL AREA (ACRES) = 0.07 PEAK FLOW RATE (CFS) = 0.16

FLOW PROCESS FROM NODE 2.00 TO NODE 3.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0150
 FLOW LENGTH (FEET) = 49.40 MANNING'S N = 0.010
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 1.8 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.30
 GIVEN PIPE DIAMETER (INCH) = 6.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 0.16
 PIPE TRAVEL TIME (MIN.) = 0.25 T_c (MIN.) = 9.81
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 3.00 = 300.40 FEET.

FLOW PROCESS FROM NODE 3.00 TO NODE 3.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE T_c (MIN.) = 9.81
 * 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.759
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
PUBLIC PARK	B	0.24	0.30	0.850	56

 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA AREA (ACRES) = 0.24 SUBAREA RUNOFF (CFS) = 0.54
 EFFECTIVE AREA (ACRES) = 0.31 AREA-AVERAGED F_m (INCH/HR) = 0.26
 AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 0.85
 TOTAL AREA (ACRES) = 0.3 PEAK FLOW RATE (CFS) = 0.70

FLOW PROCESS FROM NODE 3.00 TO NODE 4.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0150
 FLOW LENGTH (FEET) = 363.00 MANNING'S N = 0.010
 DEPTH OF FLOW IN 8.0 INCH PIPE IS 3.4 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 4.88
 GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 0.70

PIPE TRAVEL TIME (MIN.) = 1.24 Tc (MIN.) = 11.05
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 4.00 = 663.40 FEET.

FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 11.05
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.577
SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	2.53	0.30	0.850	56

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 2.53 SUBAREA RUNOFF (CFS) = 5.29
EFFECTIVE AREA (ACRES) = 2.84 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 2.8 PEAK FLOW RATE (CFS) = 5.94

FLOW PROCESS FROM NODE 4.00 TO NODE 5.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH (FEET) = 97.00 MANNING'S N = 0.010
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY (FEET/SEC.) = 17.00
PIPE FLOW VELOCITY = (TOTAL FLOW) / (PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 5.94
PIPE TRAVEL TIME (MIN.) = 0.10 Tc (MIN.) = 11.15
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 5.00 = 760.40 FEET.

FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 11.15
* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.564
SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.25	0.30	0.850	56

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 0.25 SUBAREA RUNOFF (CFS) = 0.52
EFFECTIVE AREA (ACRES) = 3.09 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 3.1 PEAK FLOW RATE (CFS) = 6.42

FLOW PROCESS FROM NODE 5.00 TO NODE 6.00 IS CODE = 41

```

-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
=====
REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH(FEET) = 135.00 MANNING'S N = 0.010
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY(FEET/SEC.) = 18.40
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER(INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 6.42
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 11.27
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 6.00 = 895.40 FEET.

*****
FLOW PROCESS FROM NODE 6.00 TO NODE 6.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
MAINLINE Tc(MIN.) = 11.27
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.548
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK B 0.71 0.30 0.850 56
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA(ACRES) = 0.71 SUBAREA RUNOFF(CFS) = 1.47
EFFECTIVE AREA(ACRES) = 3.80 AREA-AVERAGED Fm(INCH/HR) = 0.26
AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 7.84

*****
FLOW PROCESS FROM NODE 6.00 TO NODE 7.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
=====
REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH(FEET) = 5.00 MANNING'S N = 0.010
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.99
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.84
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 11.28
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 7.00 = 900.40 FEET.

*****
FLOW PROCESS FROM NODE 7.00 TO NODE 7.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
MAINLINE Tc(MIN.) = 11.28
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.547
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS

```

LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
PUBLIC PARK	B	2.01	0.30	0.850	56
SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850					
SUBAREA AREA (ACRES) =		2.01	SUBAREA RUNOFF (CFS) =		4.15
EFFECTIVE AREA (ACRES) =		5.81	AREA-AVERAGED F_m (INCH/HR) =		0.26
AREA-AVERAGED F_p (INCH/HR) =		0.30	AREA-AVERAGED A_p =		0.85
TOTAL AREA (ACRES) =		5.8	PEAK FLOW RATE (CFS) =		11.99

FLOW PROCESS FROM NODE 7.00 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0111
FLOW LENGTH (FEET) = 231.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 12.4 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 7.30
GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 11.99
PIPE TRAVEL TIME (MIN.) = 0.53 T_c (MIN.) = 11.80
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 8.00 = 1131.40 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION (MIN.) = 11.80
RAINFALL INTENSITY (INCH/HR) = 2.48
AREA-AVERAGED F_m (INCH/HR) = 0.26
AREA-AVERAGED F_p (INCH/HR) = 0.30
AREA-AVERAGED A_p = 0.85
EFFECTIVE STREAM AREA (ACRES) = 5.81
TOTAL STREAM AREA (ACRES) = 5.81
PEAK FLOW RATE (CFS) AT CONFLUENCE = 11.99

FLOW PROCESS FROM NODE 8.10 TO NODE 8.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 300.00
ELEVATION DATA: UPSTREAM (FEET) = 150.00 DOWNSTREAM (FEET) = 144.55

$$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 10.542

* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.648

SUBAREA T_c AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.76	0.30	0.850	56	10.54
SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30						

SUBAREA AVERAGE PERVIOUS AREA FRACTION, $A_p = 0.850$
SUBAREA RUNOFF (CFS) = 1.64
TOTAL AREA (ACRES) = 0.76 PEAK FLOW RATE (CFS) = 1.64

FLOW PROCESS FROM NODE 8.20 TO NODE 8.30 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE =	0.0150
FLOW LENGTH (FEET) =	167.00
MANNING'S N =	0.010
DEPTH OF FLOW IN	8.0 INCH PIPE IS 5.9 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) =	5.92
GIVEN PIPE DIAMETER (INCH) =	8.00
NUMBER OF PIPES =	1
PIPE-FLOW (CFS) =	1.64
PIPE TRAVEL TIME (MIN.) =	0.47
T_c (MIN.) =	11.01
LONGEST FLOWPATH FROM NODE	8.10 TO NODE 8.30 = 467.00 FEET.

FLOW PROCESS FROM NODE 8.30 TO NODE 8.30 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE T_c (MIN.) =	11.01				
* 10 YEAR RAINFALL INTENSITY (INCH/HR) =	2.582				
SUBAREA LOSS RATE DATA (AMC II):					
DEVELOPMENT TYPE/	SCS SOIL	AREA	F_p	A_p	SCS
LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
COMMERCIAL	B	0.51	0.30	0.100	56
SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) =		0.30			
SUBAREA AVERAGE PERVIOUS AREA FRACTION, $A_p =$		0.100			
SUBAREA AREA (ACRES) =	0.51	SUBAREA RUNOFF (CFS) =	1.17		
EFFECTIVE AREA (ACRES) =	1.27	AREA-AVERAGED F_m (INCH/HR) =	0.16		
AREA-AVERAGED F_p (INCH/HR) =	0.30	AREA-AVERAGED $A_p =$	0.55		
TOTAL AREA (ACRES) =	1.3	PEAK FLOW RATE (CFS) =	2.76		

FLOW PROCESS FROM NODE 8.30 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE =	0.0077
FLOW LENGTH (FEET) =	37.00
MANNING'S N =	0.013
DEPTH OF FLOW IN	18.0 INCH PIPE IS 7.0 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) =	4.39
GIVEN PIPE DIAMETER (INCH) =	18.00
NUMBER OF PIPES =	1
PIPE-FLOW (CFS) =	2.76
PIPE TRAVEL TIME (MIN.) =	0.14
T_c (MIN.) =	11.15
LONGEST FLOWPATH FROM NODE	8.10 TO NODE 8.00 = 504.00 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 11.15
 RAINFALL INTENSITY(INCH/HR) = 2.56
 AREA-AVERAGED Fm(INCH/HR) = 0.16
 AREA-AVERAGED Fp(INCH/HR) = 0.30
 AREA-AVERAGED Ap = 0.55
 EFFECTIVE STREAM AREA(ACRES) = 1.27
 TOTAL STREAM AREA(ACRES) = 1.27
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.76

 FLOW PROCESS FROM NODE 8.40 TO NODE 8.50 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 255.00
 ELEVATION DATA: UPSTREAM(FEET) = 147.00 DOWNSTREAM(FEET) = 142.68

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.305
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.554

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	B	0.45	0.30	0.100	56	6.31

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA RUNOFF(CFS) = 1.43
 TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 1.43

 FLOW PROCESS FROM NODE 8.50 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0557
 FLOW LENGTH(FEET) = 37.70 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.0 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.34
 GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 1.43
 PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 6.39
 LONGEST FLOWPATH FROM NODE 8.40 TO NODE 8.00 = 292.70 FEET.

 FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
 TIME OF CONCENTRATION(MIN.) = 6.39
 RAINFALL INTENSITY(INCH/HR) = 3.53

AREA-AVERAGED Fm (INCH/HR) = 0.03
 AREA-AVERAGED Fp (INCH/HR) = 0.30
 AREA-AVERAGED Ap = 0.10
 EFFECTIVE STREAM AREA (ACRES) = 0.45
 TOTAL STREAM AREA (ACRES) = 0.45
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 1.43

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.99	11.80	2.482	0.30 (0.26)	0.85	5.8	1.00
2	2.76	11.15	2.563	0.30 (0.16)	0.55	1.3	8.10
3	1.43	6.39	3.527	0.30 (0.03)	0.10	0.4	8.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	13.18	6.39	3.527	0.30 (0.22)	0.72	4.3	8.40
2	15.54	11.15	2.563	0.30 (0.23)	0.75	7.2	8.10
3	15.66	11.80	2.482	0.30 (0.23)	0.75	7.5	1.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 15.66 Tc (MIN.) = 11.80
 EFFECTIVE AREA (ACRES) = 7.53 AREA-AVERAGED Fm (INCH/HR) = 0.23
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.75
 TOTAL AREA (ACRES) = 7.5
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 8.00 = 1131.40 FEET.

 FLOW PROCESS FROM NODE 8.00 TO NODE 9.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0050
 FLOW LENGTH (FEET) = 261.00 MANNING'S N = 0.013
 ASSUME FULL-FLOWING PIPELINE
 PIPE-FLOW VELOCITY (FEET/SEC.) = 4.98
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
 GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 15.66
 PIPE TRAVEL TIME (MIN.) = 0.87 Tc (MIN.) = 12.68
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 9.00 = 1392.40 FEET.

 FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 12.68
 * 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.382
 SUBAREA LOSS RATE DATA (AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN

COMMERCIAL B 0.50 0.30 0.100 56
 PUBLIC PARK B 3.13 0.30 0.850 56
 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.747
 SUBAREA AREA(ACRES) = 3.63 SUBAREA RUNOFF(CFS) = 7.05
 EFFECTIVE AREA(ACRES) = 11.16 AREA-AVERAGED F_m (INCH/HR) = 0.23
 AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 0.75
 TOTAL AREA(ACRES) = 11.2 PEAK FLOW RATE(CFS) = 21.66

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	F_p (F_m) (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	22.02	7.19	3.297	0.30(0.22)	0.73	8.0	8.40
2	21.75	12.03	2.454	0.30(0.22)	0.75	10.8	8.10
3	21.66	12.68	2.382	0.30(0.23)	0.75	11.2	1.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE(CFS) = 22.02 Tc(MIN.) = 7.19
 AREA-AVERAGED F_m (INCH/HR) = 0.22 AREA-AVERAGED F_p (INCH/HR) = 0.30
 AREA-AVERAGED A_p = 0.73 EFFECTIVE AREA(ACRES) = 7.95

FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.19
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.297
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA F_p A_p SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 PUBLIC PARK B 0.33 0.30 0.850 56
 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA AREA(ACRES) = 0.33 SUBAREA RUNOFF(CFS) = 0.90
 EFFECTIVE AREA(ACRES) = 8.28 AREA-AVERAGED F_m (INCH/HR) = 0.22
 AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 0.74
 TOTAL AREA(ACRES) = 11.5 PEAK FLOW RATE(CFS) = 22.93

FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 7.19
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.297
 SUBAREA LOSS RATE DATA(AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA F_p A_p SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 PUBLIC PARK B 0.22 0.30 0.850 56
 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA AREA(ACRES) = 0.22 SUBAREA RUNOFF(CFS) = 0.60
 EFFECTIVE AREA(ACRES) = 8.50 AREA-AVERAGED F_m (INCH/HR) = 0.22
 AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 0.74
 TOTAL AREA(ACRES) = 11.7 PEAK FLOW RATE(CFS) = 23.53

FLOW PROCESS FROM NODE 9.00 TO NODE 10.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0050
FLOW LENGTH(FEET) = 45.00 MANNING'S N = 0.013
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.49
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.53
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 7.29
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 10.00 = 1437.40 FEET.

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0100
FLOW LENGTH(FEET) = 43.70 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 15.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.29
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.53
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 7.38
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 11.00 = 1481.10 FEET.

FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0100
FLOW LENGTH(FEET) = 93.90 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 15.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.29
GIVEN PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 23.53
PIPE TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 7.57
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 1575.00 FEET.

=====

END OF RATIONAL METHOD ANALYSIS

FLOW PROCESS FROM NODE 21.00 TO NODE 22.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 314.00
ELEVATION DATA: UPSTREAM(FEET) = 154.00 DOWNSTREAM(FEET) = 148.60

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.799

* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.482

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)

NATURAL POOR COVER

"BARREN" B 0.88 0.30 1.000 86 11.80

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000

SUBAREA RUNOFF(CFS) = 1.73

TOTAL AREA(ACRES) = 0.88 PEAK FLOW RATE(CFS) = 1.73

FLOW PROCESS FROM NODE 22.00 TO NODE 22.50 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 148.60 DOWNSTREAM(FEET) = 143.90

CHANNEL LENGTH THRU SUBAREA(FEET) = 472.00 CHANNEL SLOPE = 0.0100

CHANNEL FLOW THRU SUBAREA(CFS) = 1.73

FLOW VELOCITY(FEET/SEC) = 1.67 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME(MIN.) = 4.72 Tc(MIN.) = 16.52

LONGEST FLOWPATH FROM NODE 21.00 TO NODE 22.50 = 786.00 FEET.

FLOW PROCESS FROM NODE 22.50 TO NODE 22.50 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 16.52

* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.047

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN

PUBLIC PARK B 0.48 0.30 0.850 56

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850

SUBAREA AREA(ACRES) = 0.48 SUBAREA RUNOFF(CFS) = 0.77

EFFECTIVE AREA(ACRES) = 1.36 AREA-AVERAGED Fm(INCH/HR) = 0.28

AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.95

TOTAL AREA(ACRES) = 1.4 PEAK FLOW RATE(CFS) = 2.16

FLOW PROCESS FROM NODE 22.50 TO NODE 22.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.52
RAINFALL INTENSITY(INCH/HR) = 2.05
AREA-AVERAGED Fm(INCH/HR) = 0.28
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.95
EFFECTIVE STREAM AREA(ACRES) = 1.36
TOTAL STREAM AREA(ACRES) = 1.36
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.16

*****
FLOW PROCESS FROM NODE 22.51 TO NODE 22.52 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 283.30
ELEVATION DATA: UPSTREAM(FEET) = 150.40 DOWNSTREAM(FEET) = 147.40

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.224
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 3.288
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL B 0.71 0.30 0.100 56 7.22
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 2.08
TOTAL AREA(ACRES) = 0.71 PEAK FLOW RATE(CFS) = 2.08

*****
FLOW PROCESS FROM NODE 22.52 TO NODE 22.53 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
REPRESENTATIVE SLOPE = 0.0050
STREET LENGTH(FEET) = 220.70 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 20.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 10.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.15
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.38
HALFSTREET FLOOD WIDTH(FEET) = 12.70
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.82

```

PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.69
 STREET FLOW TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 9.24
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.855
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.84	0.30	0.100	56

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 0.84 SUBAREA RUNOFF(CFS) = 2.14
 EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.03
 AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 3.94

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 13.95
 FLOW VELOCITY(FEET/SEC.) = 1.91 DEPTH*VELOCITY(FT*FT/SEC.) = 0.77
 LONGEST FLOWPATH FROM NODE 22.51 TO NODE 22.53 = 504.00 FEET.

 FLOW PROCESS FROM NODE 22.53 TO NODE 22.53 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 9.24
 * 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.855
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.15	0.30	0.100	56

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 0.15 SUBAREA RUNOFF(CFS) = 0.38
 EFFECTIVE AREA(ACRES) = 1.70 AREA-AVERAGED Fm(INCH/HR) = 0.03
 AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 4.32

 FLOW PROCESS FROM NODE 22.53 TO NODE 22.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

REPRESENTATIVE SLOPE = 0.0100
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 9.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.41
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 4.32
 PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 9.40
 LONGEST FLOWPATH FROM NODE 22.51 TO NODE 22.50 = 554.00 FEET.

 FLOW PROCESS FROM NODE 22.50 TO NODE 22.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.40
RAINFALL INTENSITY(INCH/HR) = 2.83
AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 1.70
TOTAL STREAM AREA(ACRES) = 1.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.32

```

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.16	16.52	2.047	0.30(0.28)	0.95	1.4	21.00
2	4.32	9.40	2.828	0.30(0.03)	0.10	1.7	22.51

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.09	9.40	2.828	0.30(0.11)	0.36	2.5	22.51
2	5.27	16.52	2.047	0.30(0.14)	0.48	3.1	21.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 6.09 Tc(MIN.) = 9.40
EFFECTIVE AREA(ACRES) = 2.47 AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.36
TOTAL AREA(ACRES) = 3.1
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 22.50 = 786.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 22.50 TO NODE 23.00 IS CODE = 52

```

```

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 143.90 DOWNSTREAM(FEET) = 139.80
CHANNEL LENGTH THRU SUBAREA(FEET) = 325.40 CHANNEL SLOPE = 0.0126
CHANNEL FLOW THRU SUBAREA(CFS) = 6.09
FLOW VELOCITY(FEET/SEC) = 2.48 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.18 Tc(MIN.) = 11.58
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 23.00 = 1111.40 FEET.

```

```

*****
FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

```

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

```

=====
MAINLINE Tc(MIN.) = 11.58
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.508
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN

```

PUBLIC PARK B 0.25 0.30 0.850 56
 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA AREA (ACRES) = 0.25 SUBAREA RUNOFF (CFS) = 0.51
 EFFECTIVE AREA (ACRES) = 2.72 AREA-AVERAGED F_m (INCH/HR) = 0.12
 AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 0.41
 TOTAL AREA (ACRES) = 3.3 PEAK FLOW RATE (CFS) = 6.09
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

 FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION (MIN.) = 11.58
 RAINFALL INTENSITY (INCH/HR) = 2.51
 AREA-AVERAGED F_m (INCH/HR) = 0.12
 AREA-AVERAGED F_p (INCH/HR) = 0.30
 AREA-AVERAGED A_p = 0.41
 EFFECTIVE STREAM AREA (ACRES) = 2.72
 TOTAL STREAM AREA (ACRES) = 3.31
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 6.09

 FLOW PROCESS FROM NODE 23.10 TO NODE 23.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 285.00
 ELEVATION DATA: UPSTREAM (FEET) = 150.80 DOWNSTREAM (FEET) = 147.80

$$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 12.521

* 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.399

SUBAREA T_c AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
NATURAL POOR COVER						
"BARREN"	B	0.84	0.30	1.000	86	12.52

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000

SUBAREA RUNOFF (CFS) = 1.59
 TOTAL AREA (ACRES) = 0.84

PEAK FLOW RATE (CFS) = 1.59

 FLOW PROCESS FROM NODE 23.20 TO NODE 23.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 147.80 DOWNSTREAM (FEET) = 139.60
 CHANNEL LENGTH THRU SUBAREA (FEET) = 815.80 CHANNEL SLOPE = 0.0101
 CHANNEL FLOW THRU SUBAREA (CFS) = 1.59
 FLOW VELOCITY (FEET/SEC) = 1.65 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME (MIN.) = 8.26 Tc (MIN.) = 20.78
 LONGEST FLOWPATH FROM NODE 23.10 TO NODE 23.00 = 1100.80 FEET.

 FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 20.78
 * 10 YEAR RAINFALL INTENSITY (INCH/HR) = 1.794
 SUBAREA LOSS RATE DATA (AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 NATURAL POOR COVER
 "BARREN" B 1.81 0.30 1.000 86
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA (ACRES) = 1.81 SUBAREA RUNOFF (CFS) = 2.43
 EFFECTIVE AREA (ACRES) = 2.65 AREA-AVERAGED Fm (INCH/HR) = 0.30
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 1.00
 TOTAL AREA (ACRES) = 2.6 PEAK FLOW RATE (CFS) = 3.56

 FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION (MIN.) = 20.78
 RAINFALL INTENSITY (INCH/HR) = 1.79
 AREA-AVERAGED Fm (INCH/HR) = 0.30
 AREA-AVERAGED Fp (INCH/HR) = 0.30
 AREA-AVERAGED Ap = 1.00
 EFFECTIVE STREAM AREA (ACRES) = 2.65
 TOTAL STREAM AREA (ACRES) = 2.65
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 3.56

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.09	11.58	2.508	0.30 (0.12)	0.41	2.7	22.51
1	5.27	18.78	1.902	0.30 (0.15)	0.50	3.3	21.00
2	3.56	20.78	1.794	0.30 (0.30)	1.00	2.6	23.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	9.03	11.58	2.508	0.30 (0.19)	0.62	4.2	22.51
2	8.72	18.78	1.902	0.30 (0.21)	0.71	5.7	21.00
3	8.51	20.78	1.794	0.30 (0.22)	0.72	6.0	23.10

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 9.03 Tc (MIN.) = 11.58
 EFFECTIVE AREA (ACRES) = 4.20 AREA-AVERAGED Fm (INCH/HR) = 0.19
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.62
 TOTAL AREA (ACRES) = 6.0
 LONGEST FLOWPATH FROM NODE 21.00 TO NODE 23.00 = 1111.40 FEET.

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 11.58
 * 10 YEAR RAINFALL INTENSITY (INCH/HR) = 2.508
 SUBAREA LOSS RATE DATA (AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 PUBLIC PARK B 1.49 0.30 0.850 56
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
 SUBAREA AREA (ACRES) = 1.49 SUBAREA RUNOFF (CFS) = 3.02
 EFFECTIVE AREA (ACRES) = 5.69 AREA-AVERAGED Fm (INCH/HR) = 0.20
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.68
 TOTAL AREA (ACRES) = 7.4 PEAK FLOW RATE (CFS) = 11.81

FLOW PROCESS FROM NODE 23.00 TO NODE 24.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0100
 FLOW LENGTH (FEET) = 45.70 MANNING'S N = 0.013
 ASSUME FULL-FLOWING PIPELINE
 PIPE-FLOW VELOCITY (FEET/SEC.) = 6.68
 PIPE FLOW VELOCITY = (TOTAL FLOW) / (PIPE CROSS SECTION AREA)
 GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 11.81
 PIPE TRAVEL TIME (MIN.) = 0.11 Tc (MIN.) = 11.70
 LONGEST FLOWPATH FROM NODE 21.00 TO NODE 24.00 = 1157.10 FEET.

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 7.4 TC (MIN.) = 11.70
 EFFECTIVE AREA (ACRES) = 5.69 AREA-AVERAGED Fm (INCH/HR) = 0.20
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.678
 PEAK FLOW RATE (CFS) = 11.81

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	11.81	11.70	2.494	0.30 (0.20)	0.68	5.7	22.51
2	10.87	18.91	1.895	0.30 (0.22)	0.74	7.2	21.00
3	10.52	20.91	1.788	0.30 (0.22)	0.75	7.4	23.10

END OF RATIONAL METHOD ANALYSIS

Appendix J
Proposed Q₂₅ Hydrology Calculations

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
(c) Copyright 1983-2008 Advanced Engineering Software (aes)
Ver. 15.0 Release Date: 04/01/2008 License ID 1204

Analysis prepared by:

ADAMS STREETER CIVIL ENGINEERS
16755 VON KARMAN AVENUE, SUITE 150
IRVINE, CA 92606
(949) 474-2330

***** DESCRIPTION OF STUDY *****
* 25-YEAR STORM EVENT HYDROLOGY ANALYSIS *
* OAKCREEK COMMUNITY PARK, IRVINE CALIFORNIA *
* PROPOSED CONDITION *

FILE NAME: OAK25PRA.DAT
TIME/DATE OF STUDY: 16:23 04/04/2022

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 25.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 8.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.50	2.00	0.0313	0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 1.00 TO NODE 2.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 251.00
ELEVATION DATA: UPSTREAM (FEET) = 157.00 DOWNSTREAM (FEET) = 151.80

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION CHANGE)]^{**0.20}$
 SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 9.562
 * 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.342
 SUBAREA T_c AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
PUBLIC PARK	B	0.07	0.30	0.850	56	9.56

 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA RUNOFF (CFS) = 0.19
 TOTAL AREA (ACRES) = 0.07 PEAK FLOW RATE (CFS) = 0.19

FLOW PROCESS FROM NODE 2.00 TO NODE 3.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0150
 FLOW LENGTH (FEET) = 49.40 MANNING'S N = 0.010
 DEPTH OF FLOW IN 6.0 INCH PIPE IS 2.0 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 3.46
 GIVEN PIPE DIAMETER (INCH) = 6.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 0.19
 PIPE TRAVEL TIME (MIN.) = 0.24 T_c (MIN.) = 9.80
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 3.00 = 300.40 FEET.

FLOW PROCESS FROM NODE 3.00 TO NODE 3.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE T_c (MIN.) = 9.80
 * 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.296
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
PUBLIC PARK	B	0.24	0.30	0.850	56

 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA AREA (ACRES) = 0.24 SUBAREA RUNOFF (CFS) = 0.66
 EFFECTIVE AREA (ACRES) = 0.31 AREA-AVERAGED F_m (INCH/HR) = 0.26
 AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 0.85
 TOTAL AREA (ACRES) = 0.3 PEAK FLOW RATE (CFS) = 0.85

FLOW PROCESS FROM NODE 3.00 TO NODE 4.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0150
 FLOW LENGTH (FEET) = 363.00 MANNING'S N = 0.010
 DEPTH OF FLOW IN 8.0 INCH PIPE IS 3.8 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 5.13
 GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 0.85

PIPE TRAVEL TIME (MIN.) = 1.18 Tc (MIN.) = 10.98
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 4.00 = 663.40 FEET.

FLOW PROCESS FROM NODE 4.00 TO NODE 4.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 10.98
* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.090
SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	2.53	0.30	0.850	56

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 2.53 SUBAREA RUNOFF (CFS) = 6.46
EFFECTIVE AREA (ACRES) = 2.84 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 2.8 PEAK FLOW RATE (CFS) = 7.25

FLOW PROCESS FROM NODE 4.00 TO NODE 5.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH (FEET) = 97.00 MANNING'S N = 0.010
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY (FEET/SEC.) = 20.76
PIPE FLOW VELOCITY = (TOTAL FLOW) / (PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 7.25
PIPE TRAVEL TIME (MIN.) = 0.08 Tc (MIN.) = 11.06
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 5.00 = 760.40 FEET.

FLOW PROCESS FROM NODE 5.00 TO NODE 5.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 11.06
* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.078
SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.25	0.30	0.850	56

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA (ACRES) = 0.25 SUBAREA RUNOFF (CFS) = 0.64
EFFECTIVE AREA (ACRES) = 3.09 AREA-AVERAGED Fm (INCH/HR) = 0.26
AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA (ACRES) = 3.1 PEAK FLOW RATE (CFS) = 7.85

FLOW PROCESS FROM NODE 5.00 TO NODE 6.00 IS CODE = 41

```

-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
=====
REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH(FEET) = 135.00 MANNING'S N = 0.010
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY(FEET/SEC.) = 22.49
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER(INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.85
PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 11.16
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 6.00 = 895.40 FEET.

*****
FLOW PROCESS FROM NODE 6.00 TO NODE 6.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
MAINLINE Tc(MIN.) = 11.16
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.062
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
PUBLIC PARK B 0.71 0.30 0.850 56
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA(ACRES) = 0.71 SUBAREA RUNOFF(CFS) = 1.79
EFFECTIVE AREA(ACRES) = 3.80 AREA-AVERAGED Fm(INCH/HR) = 0.26
AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.85
TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 9.60

*****
FLOW PROCESS FROM NODE 6.00 TO NODE 7.00 IS CODE = 41
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<
=====
REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH(FEET) = 5.00 MANNING'S N = 0.010
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.22
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.60
PIPE TRAVEL TIME(MIN.) = 0.01 Tc(MIN.) = 11.16
LONGEST FLOWPATH FROM NODE 1.00 TO NODE 7.00 = 900.40 FEET.

*****
FLOW PROCESS FROM NODE 7.00 TO NODE 7.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
MAINLINE Tc(MIN.) = 11.16
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.061
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS

```

```

      LAND USE          GROUP   (ACRES)   (INCH/HR)   (DECIMAL)   CN
PUBLIC PARK           B       2.01      0.30      0.850      56
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
SUBAREA AREA(ACRES) = 2.01      SUBAREA RUNOFF(CFS) = 5.08
EFFECTIVE AREA(ACRES) = 5.81    AREA-AVERAGED Fm(INCH/HR) = 0.26
AREA-AVERAGED Fp(INCH/HR) = 0.30  AREA-AVERAGED Ap = 0.85
TOTAL AREA(ACRES) = 5.8      PEAK FLOW RATE(CFS) = 14.67

```

```

*****
FLOW PROCESS FROM NODE      7.00 TO NODE      8.00 IS CODE = 41
-----

```

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====

```

```

REPRESENTATIVE SLOPE = 0.0111
FLOW LENGTH(FEET) = 231.00  MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 14.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.66
GIVEN PIPE DIAMETER(INCH) = 24.00  NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 14.67
PIPE TRAVEL TIME(MIN.) = 0.50  Tc(MIN.) = 11.67
LONGEST FLOWPATH FROM NODE      1.00 TO NODE      8.00 = 1131.40 FEET.

```

```

*****
FLOW PROCESS FROM NODE      8.00 TO NODE      8.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====

```

```

TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.67
RAINFALL INTENSITY(INCH/HR) = 2.99
AREA-AVERAGED Fm(INCH/HR) = 0.26
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.85
EFFECTIVE STREAM AREA(ACRES) = 5.81
TOTAL STREAM AREA(ACRES) = 5.81
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.67

```

```

*****
FLOW PROCESS FROM NODE      8.10 TO NODE      8.20 IS CODE = 21
-----

```

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

```

```

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 150.00  DOWNSTREAM(FEET) = 144.55

```

$$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$$

```

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 10.542

```

```

* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.162

```

```

SUBAREA Tc AND LOSS RATE DATA(AMC II):

```

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
PUBLIC PARK	B	0.76	0.30	0.850	56	10.54
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30						

SUBAREA AVERAGE PERVIOUS AREA FRACTION, $A_p = 0.850$
SUBAREA RUNOFF (CFS) = 1.99
TOTAL AREA (ACRES) = 0.76 PEAK FLOW RATE (CFS) = 1.99

FLOW PROCESS FROM NODE 8.20 TO NODE 8.30 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0150
FLOW LENGTH (FEET) = 167.00 MANNING'S N = 0.010
ASSUME FULL-FLOWING PIPELINE
PIPE-FLOW VELOCITY (FEET/SEC.) = 5.70
PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
GIVEN PIPE DIAMETER (INCH) = 8.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 1.99
PIPE TRAVEL TIME (MIN.) = 0.49 T_c (MIN.) = 11.03
LONGEST FLOWPATH FROM NODE 8.10 TO NODE 8.30 = 467.00 FEET.

FLOW PROCESS FROM NODE 8.30 TO NODE 8.30 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE T_c (MIN.) = 11.03
* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.082
SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
COMMERCIAL	B	0.51	0.30	0.100	56

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, $A_p = 0.100$
SUBAREA AREA (ACRES) = 0.51 SUBAREA RUNOFF (CFS) = 1.40
EFFECTIVE AREA (ACRES) = 1.27 AREA-AVERAGED F_m (INCH/HR) = 0.16
AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED $A_p = 0.55$
TOTAL AREA (ACRES) = 1.3 PEAK FLOW RATE (CFS) = 3.33

FLOW PROCESS FROM NODE 8.30 TO NODE 8.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0077
FLOW LENGTH (FEET) = 37.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.7 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 4.62
GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 3.33
PIPE TRAVEL TIME (MIN.) = 0.13 T_c (MIN.) = 11.16
LONGEST FLOWPATH FROM NODE 8.10 TO NODE 8.00 = 504.00 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 11.16
RAINFALL INTENSITY(INCH/HR) = 3.06
AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.55
EFFECTIVE STREAM AREA(ACRES) = 1.27
TOTAL STREAM AREA(ACRES) = 1.27
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.33

*****
FLOW PROCESS FROM NODE 8.40 TO NODE 8.50 IS CODE = 21
=====
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 255.00
ELEVATION DATA: UPSTREAM(FEET) = 147.00 DOWNSTREAM(FEET) = 142.68

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.305
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 4.230
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL B 0.45 0.30 0.100 56 6.31
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 1.70
TOTAL AREA(ACRES) = 0.45 PEAK FLOW RATE(CFS) = 1.70

*****
FLOW PROCESS FROM NODE 8.50 TO NODE 8.00 IS CODE = 41
=====
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<
=====
REPRESENTATIVE SLOPE = 0.0557
FLOW LENGTH(FEET) = 37.70 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.75
GIVEN PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.70
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 6.39
LONGEST FLOWPATH FROM NODE 8.40 TO NODE 8.00 = 292.70 FEET.

*****
FLOW PROCESS FROM NODE 8.00 TO NODE 8.00 IS CODE = 1
=====
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 6.39

```

RAINFALL INTENSITY (INCH/HR) = 4.20
 AREA-AVERAGED Fm (INCH/HR) = 0.03
 AREA-AVERAGED Fp (INCH/HR) = 0.30
 AREA-AVERAGED Ap = 0.10
 EFFECTIVE STREAM AREA (ACRES) = 0.45
 TOTAL STREAM AREA (ACRES) = 0.45
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 1.70

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.67	11.67	2.986	0.30 (0.26)	0.85	5.8	1.00
2	3.33	11.16	3.061	0.30 (0.16)	0.55	1.3	8.10
3	1.70	6.39	4.200	0.30 (0.03)	0.10	0.4	8.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	15.96	6.39	4.200	0.30 (0.22)	0.72	4.4	8.40
2	19.00	11.16	3.061	0.30 (0.23)	0.75	7.3	8.10
3	19.13	11.67	2.986	0.30 (0.23)	0.75	7.5	1.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 19.13 Tc (MIN.) = 11.67
 EFFECTIVE AREA (ACRES) = 7.53 AREA-AVERAGED Fm (INCH/HR) = 0.23
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.75
 TOTAL AREA (ACRES) = 7.5
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 8.00 = 1131.40 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 9.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0050
 FLOW LENGTH (FEET) = 261.00 MANNING'S N = 0.013
 ASSUME FULL-FLOWING PIPELINE
 PIPE-FLOW VELOCITY (FEET/SEC.) = 6.09
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
 GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 19.13
 PIPE TRAVEL TIME (MIN.) = 0.71 Tc (MIN.) = 12.38
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 9.00 = 1392.40 FEET.

FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 12.38
 * 25 YEAR RAINFALL INTENSITY (INCH/HR) = 2.887
 SUBAREA LOSS RATE DATA (AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS

LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
COMMERCIAL	B	0.50	0.30	0.100	56
PUBLIC PARK	B	3.13	0.30	0.850	56
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.747					
SUBAREA AREA(ACRES) =		3.63	SUBAREA RUNOFF(CFS) =		8.70
EFFECTIVE AREA(ACRES) =		11.16	AREA-AVERAGED Fm(INCH/HR) =		0.23
AREA-AVERAGED Fp(INCH/HR) =		0.30	AREA-AVERAGED Ap =		0.75
TOTAL AREA(ACRES) =		11.2	PEAK FLOW RATE(CFS) =		26.73

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	26.53	7.24	3.911	0.30(0.22)	0.73	8.0	8.40
2	26.81	11.88	2.955	0.30(0.22)	0.75	10.9	8.10
3	26.73	12.38	2.887	0.30(0.23)	0.75	11.2	1.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE(CFS) = 26.81 Tc(MIN.) = 11.88
 AREA-AVERAGED Fm(INCH/HR) = 0.22 AREA-AVERAGED Fp(INCH/HR) = 0.30
 AREA-AVERAGED Ap = 0.75 EFFECTIVE AREA(ACRES) = 10.91

 FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 11.88
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.955
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.33	0.30	0.850	56
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850					
SUBAREA AREA(ACRES) =		0.33	SUBAREA RUNOFF(CFS) =		0.80
EFFECTIVE AREA(ACRES) =		11.24	AREA-AVERAGED Fm(INCH/HR) =		0.23
AREA-AVERAGED Fp(INCH/HR) =		0.30	AREA-AVERAGED Ap =		0.75
TOTAL AREA(ACRES) =		11.5	PEAK FLOW RATE(CFS) =		27.61

 FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 11.88
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.955
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
PUBLIC PARK	B	0.22	0.30	0.850	56
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850					
SUBAREA AREA(ACRES) =		0.22	SUBAREA RUNOFF(CFS) =		0.53
EFFECTIVE AREA(ACRES) =		11.46	AREA-AVERAGED Fm(INCH/HR) =		0.23
AREA-AVERAGED Fp(INCH/HR) =		0.30	AREA-AVERAGED Ap =		0.75
TOTAL AREA(ACRES) =		11.7	PEAK FLOW RATE(CFS) =		28.14

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	28.34	7.24	3.911	0.30 (0.22)	0.74	8.5	8.40
2	28.14	11.88	2.955	0.30 (0.23)	0.75	11.5	8.10
3	28.04	12.38	2.887	0.30 (0.23)	0.76	11.7	1.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE (CFS) = 28.34 Tc (MIN.) = 7.24
 AREA-AVERAGED Fm (INCH/HR) = 0.22 AREA-AVERAGED Fp (INCH/HR) = 0.30
 AREA-AVERAGED Ap = 0.74 EFFECTIVE AREA (ACRES) = 8.54

 FLOW PROCESS FROM NODE 9.00 TO NODE 10.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0050
 FLOW LENGTH (FEET) = 45.00 MANNING'S N = 0.013
 ASSUME FULL-FLOWING PIPELINE
 PIPE-FLOW VELOCITY (FEET/SEC.) = 9.02
 PIPE FLOW VELOCITY = (TOTAL FLOW)/(PIPE CROSS SECTION AREA)
 GIVEN PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 28.34
 PIPE TRAVEL TIME (MIN.) = 0.08 Tc (MIN.) = 7.33
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 10.00 = 1437.40 FEET.

 FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0100
 FLOW LENGTH (FEET) = 43.70 MANNING'S N = 0.013
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 16.9 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 8.71
 GIVEN PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 28.34
 PIPE TRAVEL TIME (MIN.) = 0.08 Tc (MIN.) = 7.41
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 11.00 = 1481.10 FEET.

 FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

=====

REPRESENTATIVE SLOPE = 0.0100
 FLOW LENGTH (FEET) = 93.90 MANNING'S N = 0.013
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 16.9 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 8.71
 GIVEN PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 28.34
 PIPE TRAVEL TIME (MIN.) = 0.18 Tc (MIN.) = 7.59
 LONGEST FLOWPATH FROM NODE 1.00 TO NODE 12.00 = 1575.00 FEET.

=====

=====

END OF RATIONAL METHOD ANALYSIS

```

*****
FLOW PROCESS FROM NODE      21.00 TO NODE      22.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) =  314.00
ELEVATION DATA: UPSTREAM(FEET) =  154.00  DOWNSTREAM(FEET) =  148.60

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =  11.799
* 25 YEAR RAINFALL INTENSITY(INCH/HR) =  2.967
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp          Ap      SCS   Tc
LAND USE              GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN   (MIN.)
NATURAL POOR COVER
"BARREN"                B        0.88      0.30      1.000      86   11.80
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  1.000
SUBAREA RUNOFF(CFS) =  2.11
TOTAL AREA(ACRES) =  0.88  PEAK FLOW RATE(CFS) =  2.11

*****
FLOW PROCESS FROM NODE      22.00 TO NODE      22.50 IS CODE =  52
-----
>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  148.60  DOWNSTREAM(FEET) =  143.90
CHANNEL LENGTH THRU SUBAREA(FEET) =  472.00  CHANNEL SLOPE =  0.0100
CHANNEL FLOW THRU SUBAREA(CFS) =  2.11
FLOW VELOCITY(FEET/SEC) =  1.74 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) =  4.53  Tc(MIN.) =  16.33
LONGEST FLOWPATH FROM NODE      21.00 TO NODE      22.50 =  786.00 FEET.

*****
FLOW PROCESS FROM NODE      22.50 TO NODE      22.50 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
MAINLINE Tc(MIN.) =  16.33
* 25 YEAR RAINFALL INTENSITY(INCH/HR) =  2.469
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp          Ap      SCS
LAND USE              GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN
PUBLIC PARK            B        0.48      0.30      0.850      56
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.850
SUBAREA AREA(ACRES) =  0.48  SUBAREA RUNOFF(CFS) =  0.96
EFFECTIVE AREA(ACRES) =  1.36  AREA-AVERAGED Fm(INCH/HR) =  0.28
AREA-AVERAGED Fp(INCH/HR) =  0.30  AREA-AVERAGED Ap =  0.95
TOTAL AREA(ACRES) =  1.4  PEAK FLOW RATE(CFS) =  2.67

*****
FLOW PROCESS FROM NODE      22.50 TO NODE      22.50 IS CODE =  1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

```

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 16.33
RAINFALL INTENSITY(INCH/HR) = 2.47
AREA-AVERAGED Fm(INCH/HR) = 0.28
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.95
EFFECTIVE STREAM AREA(ACRES) = 1.36
TOTAL STREAM AREA(ACRES) = 1.36
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.67

*****
FLOW PROCESS FROM NODE 22.51 TO NODE 22.52 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 283.30
ELEVATION DATA: UPSTREAM(FEET) = 150.40 DOWNSTREAM(FEET) = 147.40

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.224
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.917
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
COMMERCIAL B 0.71 0.30 0.100 56 7.22
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 2.48
TOTAL AREA(ACRES) = 0.71 PEAK FLOW RATE(CFS) = 2.48

*****
FLOW PROCESS FROM NODE 22.52 TO NODE 22.53 IS CODE = 61
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STANDARD CURB SECTION USED)<<<<
=====
REPRESENTATIVE SLOPE = 0.0050
STREET LENGTH(FEET) = 220.70 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 20.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 10.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.77
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.40
HALFSTREET FLOOD WIDTH(FEET) = 13.63
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.91

```

PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.76
 STREET FLOW TRAVEL TIME(MIN.) = 1.93 Tc(MIN.) = 9.15
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.426
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.84	0.30	0.100	56

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 0.84 SUBAREA RUNOFF(CFS) = 2.57
 EFFECTIVE AREA(ACRES) = 1.55 AREA-AVERAGED Fm(INCH/HR) = 0.03
 AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 1.5 PEAK FLOW RATE(CFS) = 4.74

END OF SUBAREA STREET FLOW HYDRAULICS:
 DEPTH(FEET) = 0.43 HALFSTREET FLOOD WIDTH(FEET) = 14.96
 FLOW VELOCITY(FEET/SEC.) = 2.01 DEPTH*VELOCITY(FT*FT/SEC.) = 0.86
 LONGEST FLOWPATH FROM NODE 22.51 TO NODE 22.53 = 504.00 FEET.

 FLOW PROCESS FROM NODE 22.53 TO NODE 22.53 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 9.15
 * 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.426
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	B	0.15	0.30	0.100	56

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 0.15 SUBAREA RUNOFF(CFS) = 0.46
 EFFECTIVE AREA(ACRES) = 1.70 AREA-AVERAGED Fm(INCH/HR) = 0.03
 AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 5.20

 FLOW PROCESS FROM NODE 22.53 TO NODE 22.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

REPRESENTATIVE SLOPE = 0.0100
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 15.0 INCH PIPE IS 10.6 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.60
 ESTIMATED PIPE DIAMETER(INCH) = 15.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 5.20
 PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 9.30
 LONGEST FLOWPATH FROM NODE 22.51 TO NODE 22.50 = 554.00 FEET.

 FLOW PROCESS FROM NODE 22.50 TO NODE 22.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 9.30
RAINFALL INTENSITY(INCH/HR) = 3.39
AREA-AVERAGED Fm(INCH/HR) = 0.03
AREA-AVERAGED Fp(INCH/HR) = 0.30
AREA-AVERAGED Ap = 0.10
EFFECTIVE STREAM AREA(ACRES) = 1.70
TOTAL STREAM AREA(ACRES) = 1.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.20

```

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	2.67	16.33	2.469	0.30(0.28)	0.95	1.4	21.00
2	5.20	9.30	3.394	0.30(0.03)	0.10	1.7	22.51

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.36	9.30	3.394	0.30(0.11)	0.37	2.5	22.51
2	6.44	16.33	2.469	0.30(0.14)	0.48	3.1	21.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 7.36 Tc(MIN.) = 9.30
EFFECTIVE AREA(ACRES) = 2.47 AREA-AVERAGED Fm(INCH/HR) = 0.11
AREA-AVERAGED Fp(INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.37
TOTAL AREA(ACRES) = 3.1
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 22.50 = 786.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 22.50 TO NODE 23.00 IS CODE = 52

```

```

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 143.90 DOWNSTREAM(FEET) = 139.80
CHANNEL LENGTH THRU SUBAREA(FEET) = 325.40 CHANNEL SLOPE = 0.0126
CHANNEL FLOW THRU SUBAREA(CFS) = 7.36
FLOW VELOCITY(FEET/SEC) = 2.60 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)
TRAVEL TIME(MIN.) = 2.09 Tc(MIN.) = 11.39
LONGEST FLOWPATH FROM NODE 21.00 TO NODE 23.00 = 1111.40 FEET.

```

```

*****
FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

```

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

```

=====
MAINLINE Tc(MIN.) = 11.39
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.027
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN

```

PUBLIC PARK B 0.25 0.30 0.850 56
 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.850
 SUBAREA AREA (ACRES) = 0.25 SUBAREA RUNOFF (CFS) = 0.62
 EFFECTIVE AREA (ACRES) = 2.72 AREA-AVERAGED F_m (INCH/HR) = 0.12
 AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 0.41
 TOTAL AREA (ACRES) = 3.3 PEAK FLOW RATE (CFS) = 7.36
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

 FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION (MIN.) = 11.39
 RAINFALL INTENSITY (INCH/HR) = 3.03
 AREA-AVERAGED F_m (INCH/HR) = 0.12
 AREA-AVERAGED F_p (INCH/HR) = 0.30
 AREA-AVERAGED A_p = 0.41
 EFFECTIVE STREAM AREA (ACRES) = 2.72
 TOTAL STREAM AREA (ACRES) = 3.31
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 7.36

 FLOW PROCESS FROM NODE 23.10 TO NODE 23.20 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 285.00
 ELEVATION DATA: UPSTREAM (FEET) = 150.80 DOWNSTREAM (FEET) = 147.80

$$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 12.521

* 25 YEAR RAINFALL INTENSITY (INCH/HR) = 2.869

SUBAREA T_c AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
NATURAL POOR COVER						
"BARREN"	B	0.84	0.30	1.000	86	12.52

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000

SUBAREA RUNOFF (CFS) = 1.94
 TOTAL AREA (ACRES) = 0.84

PEAK FLOW RATE (CFS) = 1.94

 FLOW PROCESS FROM NODE 23.20 TO NODE 23.00 IS CODE = 52

>>>>COMPUTE NATURAL VALLEY CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 147.80 DOWNSTREAM (FEET) = 139.60
 CHANNEL LENGTH THRU SUBAREA (FEET) = 815.80 CHANNEL SLOPE = 0.0101
 CHANNEL FLOW THRU SUBAREA (CFS) = 1.94
 FLOW VELOCITY (FEET/SEC) = 1.71 (PER LACFCD/RCFC&WCD HYDROLOGY MANUAL)

TRAVEL TIME (MIN.) = 7.93 Tc (MIN.) = 20.45
 LONGEST FLOWPATH FROM NODE 23.10 TO NODE 23.00 = 1100.80 FEET.

 FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 20.45
 * 25 YEAR RAINFALL INTENSITY (INCH/HR) = 2.173
 SUBAREA LOSS RATE DATA (AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 NATURAL POOR COVER
 "BARREN" B 1.81 0.30 1.000 86
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA (ACRES) = 1.81 SUBAREA RUNOFF (CFS) = 3.05
 EFFECTIVE AREA (ACRES) = 2.65 AREA-AVERAGED Fm (INCH/HR) = 0.30
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 1.00
 TOTAL AREA (ACRES) = 2.6 PEAK FLOW RATE (CFS) = 4.47

 FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION (MIN.) = 20.45
 RAINFALL INTENSITY (INCH/HR) = 2.17
 AREA-AVERAGED Fm (INCH/HR) = 0.30
 AREA-AVERAGED Fp (INCH/HR) = 0.30
 AREA-AVERAGED Ap = 1.00
 EFFECTIVE STREAM AREA (ACRES) = 2.65
 TOTAL STREAM AREA (ACRES) = 2.65
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 4.47

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.36	11.39	3.027	0.30 (0.12)	0.41	2.7	22.51
1	6.44	18.48	2.301	0.30 (0.15)	0.50	3.3	21.00
2	4.47	20.45	2.173	0.30 (0.30)	1.00	2.6	23.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	10.99	11.39	3.027	0.30 (0.19)	0.62	4.2	22.51
2	10.75	18.48	2.301	0.30 (0.21)	0.71	5.7	21.00
3	10.52	20.45	2.173	0.30 (0.22)	0.72	6.0	23.10

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 10.99 Tc (MIN.) = 11.39
 EFFECTIVE AREA (ACRES) = 4.20 AREA-AVERAGED Fm (INCH/HR) = 0.19
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.62
 TOTAL AREA (ACRES) = 6.0
 LONGEST FLOWPATH FROM NODE 21.00 TO NODE 23.00 = 1111.40 FEET.

FLOW PROCESS FROM NODE 23.00 TO NODE 23.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 11.39
 * 25 YEAR RAINFALL INTENSITY (INCH/HR) = 3.027
 SUBAREA LOSS RATE DATA (AMC II):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 PUBLIC PARK B 1.49 0.30 0.850 56
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.850
 SUBAREA AREA (ACRES) = 1.49 SUBAREA RUNOFF (CFS) = 3.72
 EFFECTIVE AREA (ACRES) = 5.69 AREA-AVERAGED Fm (INCH/HR) = 0.20
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.68
 TOTAL AREA (ACRES) = 7.4 PEAK FLOW RATE (CFS) = 14.46

FLOW PROCESS FROM NODE 23.00 TO NODE 24.00 IS CODE = 41

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING USER-SPECIFIED PIPESIZE (EXISTING ELEMENT)<<<<<

REPRESENTATIVE SLOPE = 0.0100
 FLOW LENGTH (FEET) = 45.70 MANNING'S N = 0.013
 ASSUME FULL-FLOWING PIPELINE
 PIPE-FLOW VELOCITY (FEET/SEC.) = 8.18
 PIPE FLOW VELOCITY = (TOTAL FLOW) / (PIPE CROSS SECTION AREA)
 GIVEN PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 14.46
 PIPE TRAVEL TIME (MIN.) = 0.09 Tc (MIN.) = 11.48
 LONGEST FLOWPATH FROM NODE 21.00 TO NODE 24.00 = 1157.10 FEET.

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 7.4 TC (MIN.) = 11.48
 EFFECTIVE AREA (ACRES) = 5.69 AREA-AVERAGED Fm (INCH/HR) = 0.20
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.678
 PEAK FLOW RATE (CFS) = 14.46

** PEAK FLOW RATE TABLE **

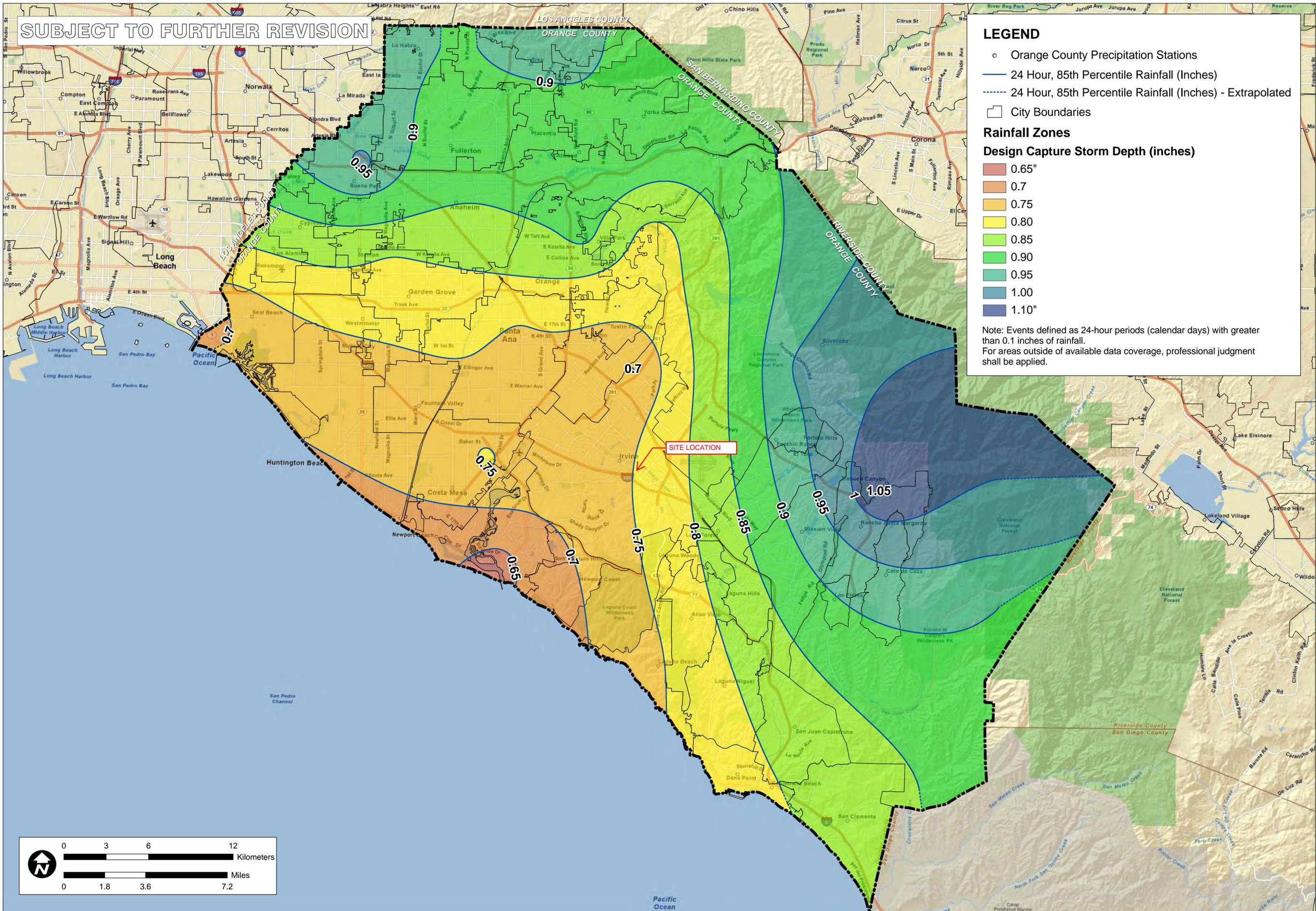
STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.46	11.48	3.013	0.30 (0.20)	0.68	5.7	22.51
2	13.46	18.58	2.294	0.30 (0.22)	0.74	7.2	21.00
3	13.06	20.55	2.167	0.30 (0.22)	0.75	7.4	23.10

END OF RATIONAL METHOD ANALYSIS

ATTACHMENT E

ORANGE COUNTY RAINFALL ZONES MAP

SUBJECT TO FURTHER REVISION



LEGEND

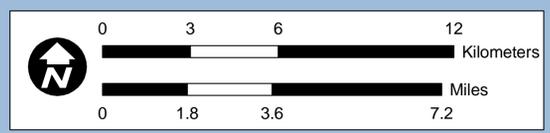
- Orange County Precipitation Stations
- 24 Hour, 85th Percentile Rainfall (Inches)
- - - 24 Hour, 85th Percentile Rainfall (Inches) - Extrapolated
- City Boundaries

Rainfall Zones

Design Capture Storm Depth (inches)

- 0.65"
- 0.7
- 0.75
- 0.80
- 0.85
- 0.90
- 0.95
- 1.00
- 1.10"

Note: Events defined as 24-hour periods (calendar days) with greater than 0.1 inches of rainfall.
For areas outside of available data coverage, professional judgment shall be applied.



RAINFALL ZONES

ORANGE COUNTY
TECHNICAL GUIDANCE
DOCUMENT

ORANGE CO. CA

SCALE	1" = 1.8 miles
DESIGNED	TH
DRAWING	TH
CHECKED	BMP
DATE	04/22/10
JOB NO.	9526-E

FIGURE
XVI-1

P:\9526E\6-GIS\Mxd\Reports\Infiltration\Feasibility_20110215\9526E_FigureXVI-1_RainfallZones_20110215.mxd