

## Memorandum

DATE: January 2, 2023  
TO: City of Chino, Development Services  
FROM: David White  
SUBJECT: PL20-0004 – Preliminary Offsite Drainage Study  
PROJECT NO.: R310158.01

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### Introduction

Pursuant to the DRC Level 2C Comments dated June 8, 2021 from the City of Chino Engineering Department and follow up letter dated June 9, 2021 from the City Engineer, Huitt-Zollars has prepared this Offsite Drainage Study on behalf of Golden West Management (PAMA Management). The study focused on the following objectives:

1. Determine the capacity of East End Avenue and Philadelphia Street to carry storm water per City of Chino Standards and Specifications.
2. Analyze the runoff from upstream properties and determine its potential impacts to the subject property.
3. Identify Master Plan of Drainage updates, if applicable, based on the findings of 1 and 2.

As part of the development of the Industrial Warehouse Development Project on the subject site, street improvements are proposed on the west half of East End Avenue and north half of Philadelphia Street along the project frontage. This includes pavement widening, 8” curb & gutter, and sidewalk. The majority of East End Avenue north of the project site has existing curb & gutter on both sides of the street. The curb to curb width is 76’ with 36’ on the west half and 40’ on the east half.

Philadelphia Street has existing improvements on both sides of the street east of East End Avenue. The curb to curb width is 72’. There are no improvements along the project frontage or west of the subject site on either side of Philadelphia Street. The ultimate curb to curb width is 72’ with a 16’ parkway.

Analysis of the City of Chino’s Master Plan of Drainage and storm drain plans indicate an existing 33” storm drain conveys runoff from the intersection of East End Avenue and Philadelphia Street to the San Antonio Creek Channel.

The hydrologic criteria used in this study was: runoff from 10-year storm event does not flood inside traffic lanes, 25-year runoff does not exceed top of curb, and the 100-year runoff will not exceed the ultimate right-of-way.

The drainage map is included as Attachment 1, the plan for the existing 33” storm drain is included as Attachment 2, the hydraulic calculations are included as Attachment 3, and the hydrology calculations are included as Attachment 4.

## Hydrologic Analysis

The drainage area tributary to the intersection of East End Avenue and Philadelphia Street was delineated using a combination of Google imagery, record maps, and field visits. The drainage area is approximately 56 acres and consists mostly of East End Avenue extending north to Phillips Blvd and a portion of residential area adjacent to East End Avenue comprised largely of the gated Sullivan Ranch. The limited extent of the drainage area can be attributed to a few factors. One is that flows on the western half of East End Avenue coming southward are redirected at Francis Street to a channel that takes flows directly to the San Antonio Creek Channel. Also, the majority of the area west of East End Avenue between Philadelphia Street and Francis Street drains directly to the channel. Lastly, a system of north-south cross gutters at most major intersections east of the project area diverts flows southward to the large System 11 storm drain system parallel to the Pomona Freeway rather than westward to San Antonio Creek Channel. These factors kept the resulting tributary flows within a manageable range.

After the delineation of the drainage area into smaller sub drainage areas, peak discharges were determined at each of the corresponding hydrologic nodes using the AES rational method consistent with the San Bernardino County Hydrology Manual. Soils in the area fell under Hydrologic Soil Group A according to the City of Chino Master Plan of Drainage and USGS soil survey indicating high to moderate infiltration potential. Land Uses in the area included residential (2 DU/acre) and commercial for the streets and industrial complexes.

Storm intensities for the 10, 25, and 100-year storm events were derived from the NOAA Atlas 14 website and can be seen in the following table:

Storm Event	Intensity (in/hr)
10 year	0.95 in/hr
25 year	1.17 in/hr
100 year	1.53 in/hr

## Hydraulic Analysis

Once street and surface flows were calculated, they were analyzed for hydraulic feasibility. The half street cross sections for East End and Philadelphia were plotted in Flowmaster to determine the maximum half street flow capacity. These were determined to be 62.8 cfs for East End and 49.3 cfs for Philadelphia at the right of way (ROW) and 24.1 cfs for East End and 19.9 cfs for Philadelphia at the top of curb (TC). For East End these are well above the projected maximum 100-year half street flows of 14.3 cfs and 17.9 cfs found approaching the intersection of East End Avenue and Philadelphia Street, indicating that there is no immediate need for upstream catch basins or storm drain pipe to dewater East End Avenue. For Philadelphia Street, the runoff between nodes 303 and 106 is contained within the public right of way utilizing a combination of pipe flow and surface flow.

Next, WSPG was run to determine the maximum capacity of the existing 33" storm drain, which was designed for Q25 as indicated on the plan. The storm drain appears to continue east to Humboldt although the County does not have the improvement plans for this reach, which was installed after the original segment per City of Chino plan A-757. Through trial and error, the capacity of the storm drain was calculated to be approximately 57 cfs before water levels begin to rise above the existing grates at the intersection. This is less than the 25-year flow of 72.9 cfs from the rational method, suggesting that the existing pipe infrastructure is inadequate for larger storm events. During larger storm events as the water level rises, ponding will be localized around the east grate and will spill over the crown of Philadelphia and continue south on East End. The ponding will not affect East End Avenue or the subject property since the crown of Philadelphia is less than a foot above the grate elevation.

**Conclusion**

This preliminary offsite drainage study was prepared to determine the impacts of upstream runoff, from both private properties and public streets, on the subject property and assess whether storm drain infrastructure improvements would be required to protect the subject property after development.

We have concluded there is no private off-site runoff impacting the subject property from the other properties north or west of the subject property. The runoff from those lots either sheets flows directly towards the channel or is directed to East End Avenue.

Furthermore, based on the hydrology and hydraulic results, East End Avenue has more than enough capacity to carry the tributary runoff from Philips Blvd. to Philadelphia Street. New curb & gutter is being installed along the project frontage to protect the property and the depth of flow in East End Avenue will be below the top of curb during a Q<sub>100</sub> storm. There is no runoff tributary to Philadelphia Street along the project frontage. Philadelphia has a high point midway between East End and the Channel so there will be negligible runoff in the gutter. Philadelphia Street east of East End is conveying runoff to the intersection via surface and storm drain. It is estimated that the pipe will carry 32 cfs and the rest will be carried in the street. The follow table summarizes the calculated flows and capacities for both streets.

	Q100 capacity	Q100 flows	Q25 capacity	Q250 flows
East End	62.8	17.9	24.1	13.2
Philadelphia	49.3	*40	19.9	*12

\*assuming 32 cfs is being conveyed in the existing storm drain

The hydrology calculations did not include the subject property as part of the area tributary to the intersection because the site will no longer contribute surface flows to the intersection. Once developed the subject site will provide water quality treatment and storm mitigation and the resulting reduced discharge will enter the existing 33” storm drain directly via private storm drain line C as depicted on the map.

Runoff in excess of the capacity of the existing 33” storm drain will pond at the northeast corner of the intersection and sheet flow across the crown of Philadelphia and continue south on East End Avenue, which the street can adequately convey. This is an existing condition and is not impacted by the development of the 3.6 acre subject property.

Based on the foregoing results and conclusions, additional storm drain infrastructure is not warranted since there are no impacts to the subject property from upstream runoff and the subject property does not impact downstream runoff.

**LEGEND**

- 31 SYSTEM AREA NUMBER
- SYSTEM AREA BOUNDARY
- EXISTING STORM DRAIN CONDUIT SIZE.
- 60"
- 42"
- PLANNED FACILITIES CONDUIT SIZE.
- 42"
- PLANNED FACILITIES IN OTHER JURISDICTIONS
- EXISTING OPEN CHANNEL.
- EARTHEN CHANNEL
- 24" REINFORCED CONCRETE PIPE SIZE
- CIPP CAST-IN-PLACE PIPE
- CMP CORRUGATED METAL PIPE
- RCB REINFORCED CONCRETE BOX
- TCC TRAPEZOIDAL CONCRETE CHANNEL
- RCC RECTANGULAR CONCRETE CHANNEL
- ☒ EXISTING LIFT STATION

System 28 Storm Drain, see following pages

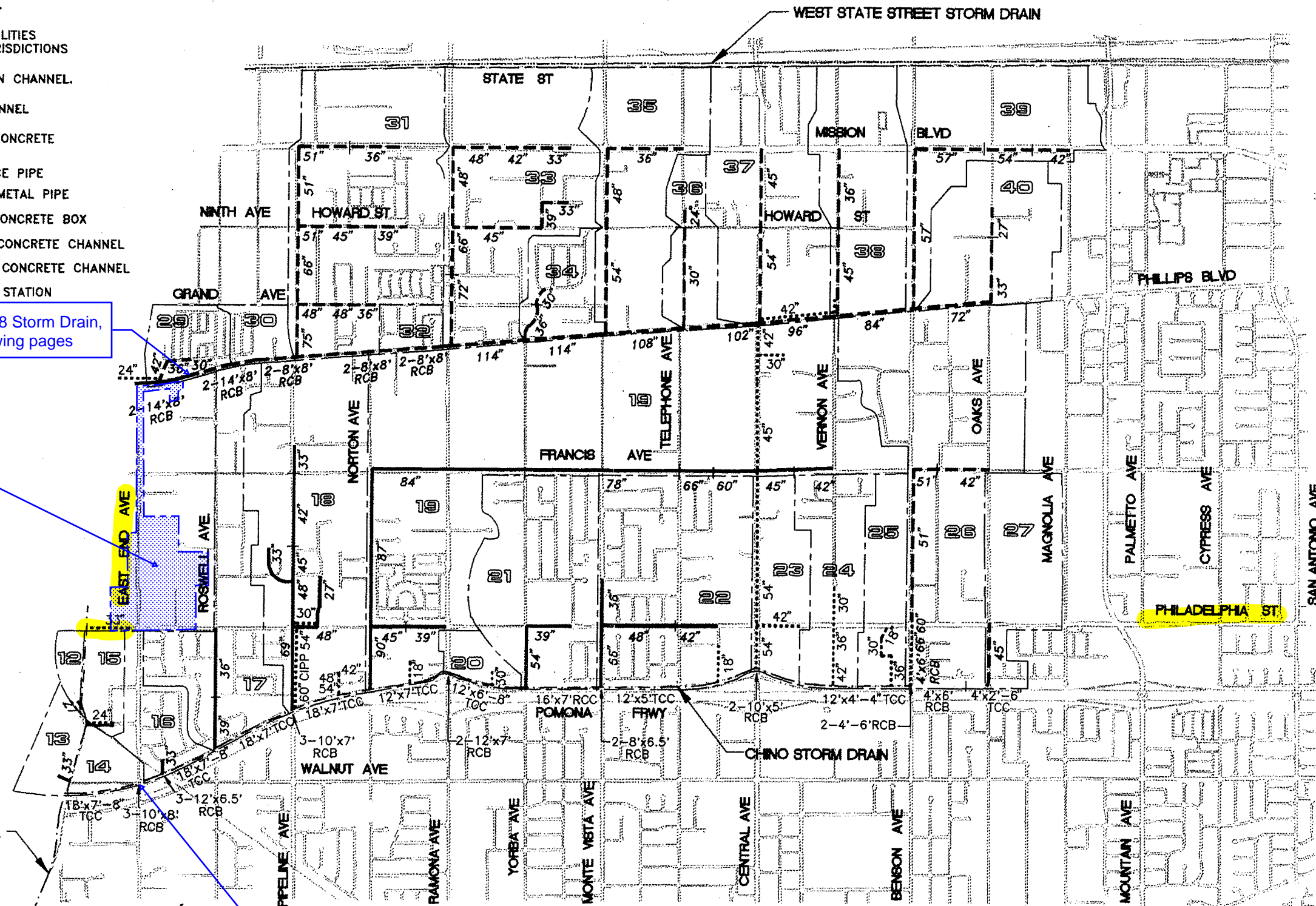
System Area Boundary tributary to the intersection of East End Avenue and Philadelphia Street

System 11 Storm Drain, see following page

SAN ANTONIO CHANNEL



SCALE : 1" = 2000'



BSI Consultants, Inc.  
2001 E. First Street  
San Jose, CA 95128  
(415) 568-7300

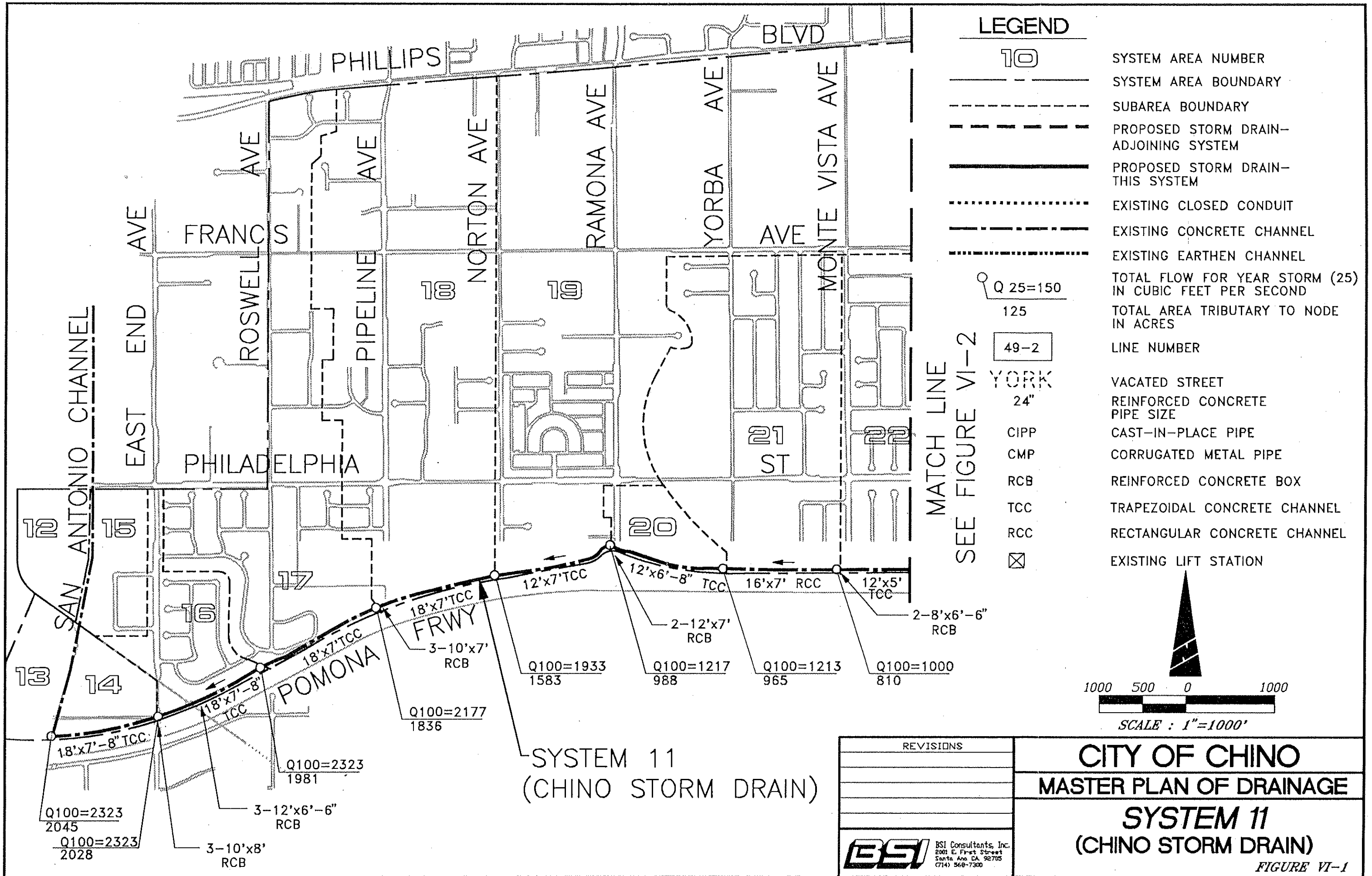


CITY OF CHINO  
CHINO, CALIFORNIA

MASTER PLAN OF DRAINAGE  
FACILITIES MAP  
NORTHERN BASIN

Description	Date	Initial
Revisions		

FIGURE II-1



SPRR WEST STATE STREET STORM DRAIN

SAN ANTONIO CHANNEL

2-14'x8' RCB

Q100=2055  
1457

**LEGEND**

10

SYSTEM AREA NUMBER

SYSTEM AREA BOUNDARY

SUBAREA BOUNDARY

PROPOSED STORM DRAIN-  
ADJOINING SYSTEM

PROPOSED STORM DRAIN-  
THIS SYSTEM

EXISTING CLOSED CONDUIT

EXISTING CONCRETE CHANNEL

EXISTING EARTHEN CHANNEL

Q 25=150

125

TOTAL FLOW FOR YEAR STORM (25)  
IN CUBIC FEET PER SECOND

TOTAL AREA TRIBUTARY TO NODE  
IN ACRES

49-2

YORK

24"

CIPP

CMP

RCB

TCC

RCC

☒

LINE NUMBER

VACATED STREET

REINFORCED CONCRETE  
PIPE SIZE

CAST-IN-PLACE PIPE

CORRUGATED METAL PIPE

REINFORCED CONCRETE BOX

TRAPEZOIDAL CONCRETE CHANNEL

RECTANGULAR CONCRETE CHANNEL

EXISTING LIFT STATION

Q100=2055 1457  
Q100=2055 1415  
Q100=2047 1395  
Q100=1585 1114  
Q100=1576 1094

Q100=1168 869

Q100=1064 817

Q100=857 652

114"

114"

108"

102"

1000 500 0 1000

SCALE : 1"=1000'

**CITY OF CHINO  
MASTER PLAN OF DRAINAGE**

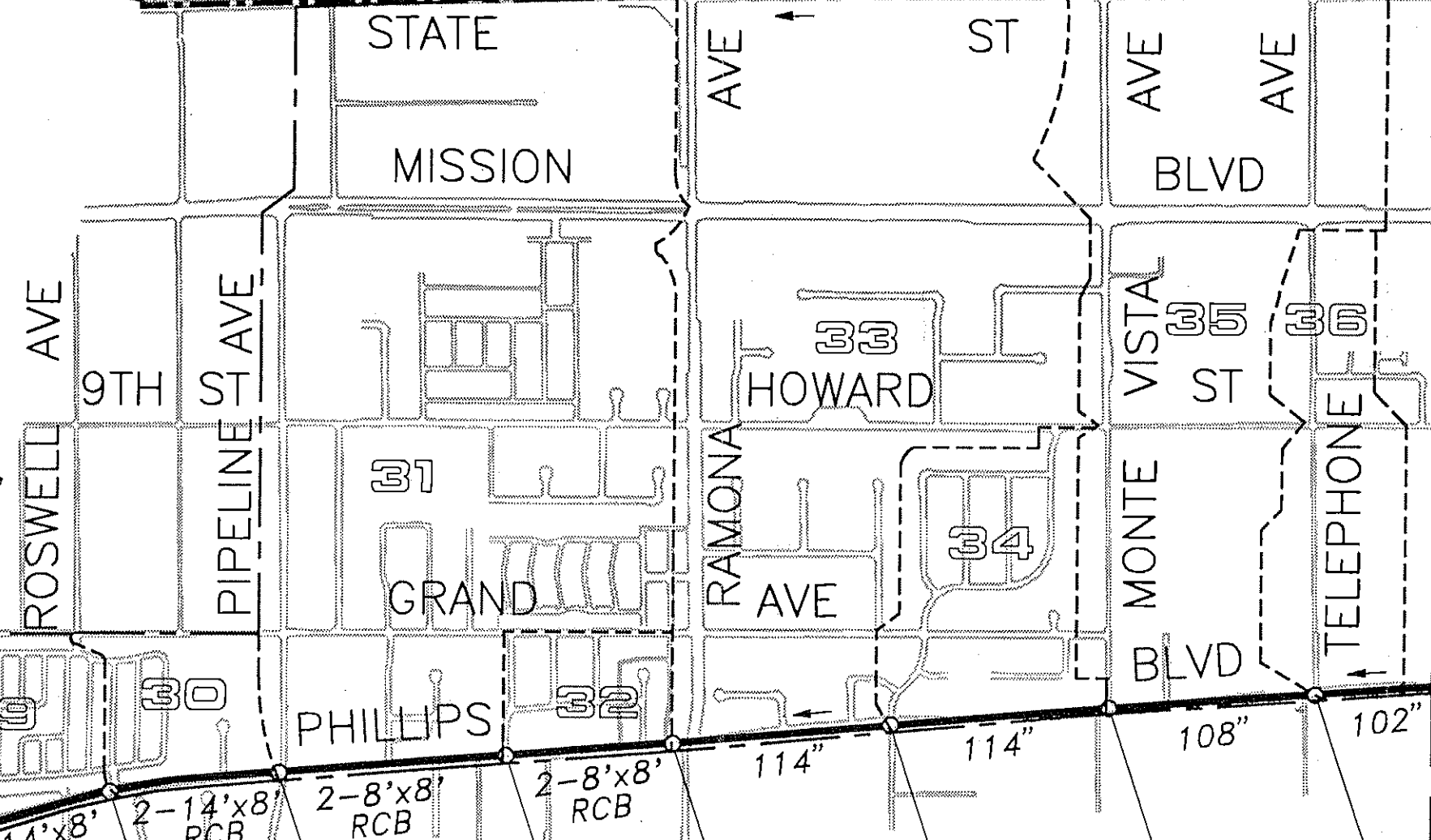
**SYSTEM 28**

FIGURE VI-20

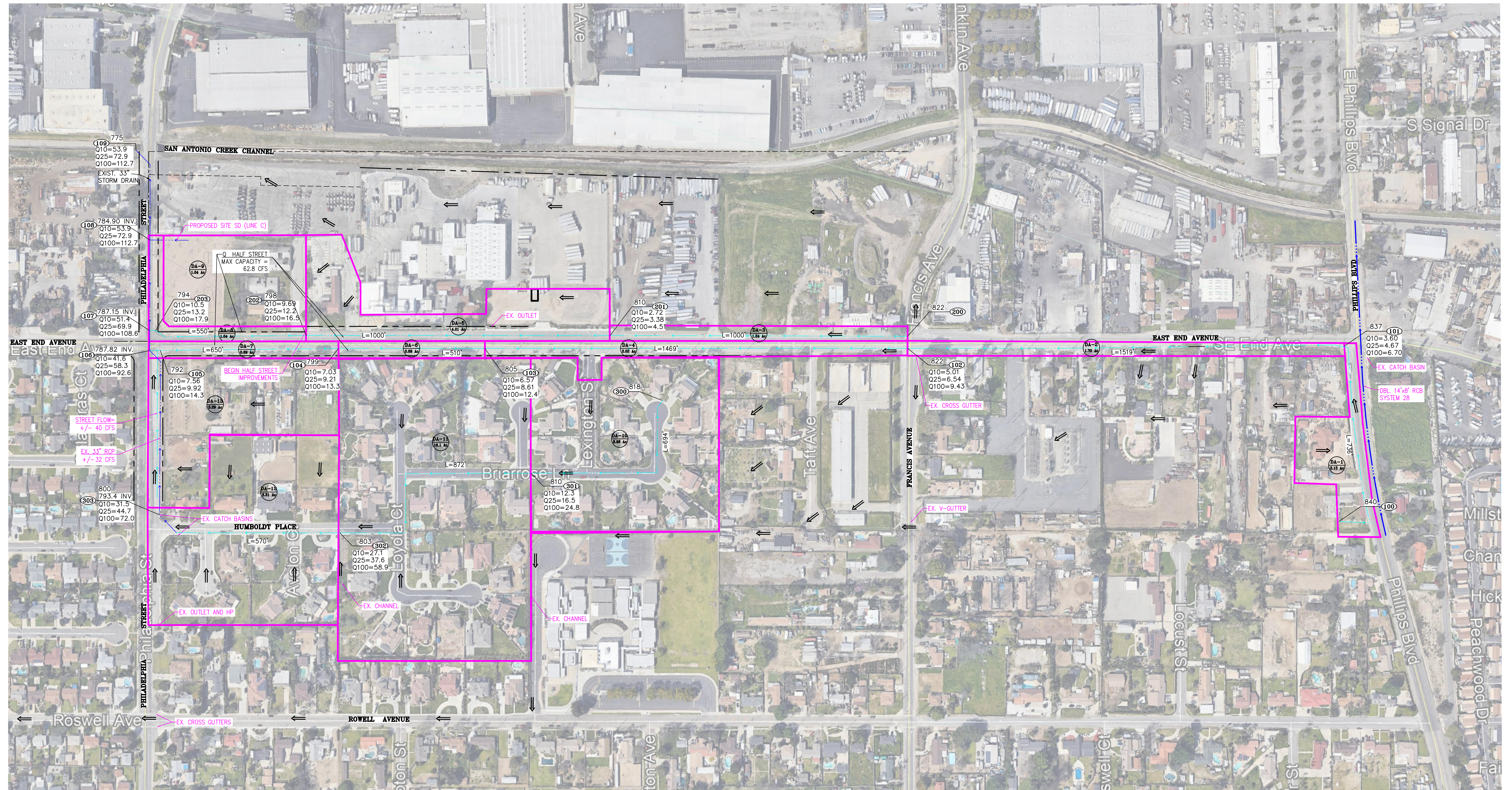
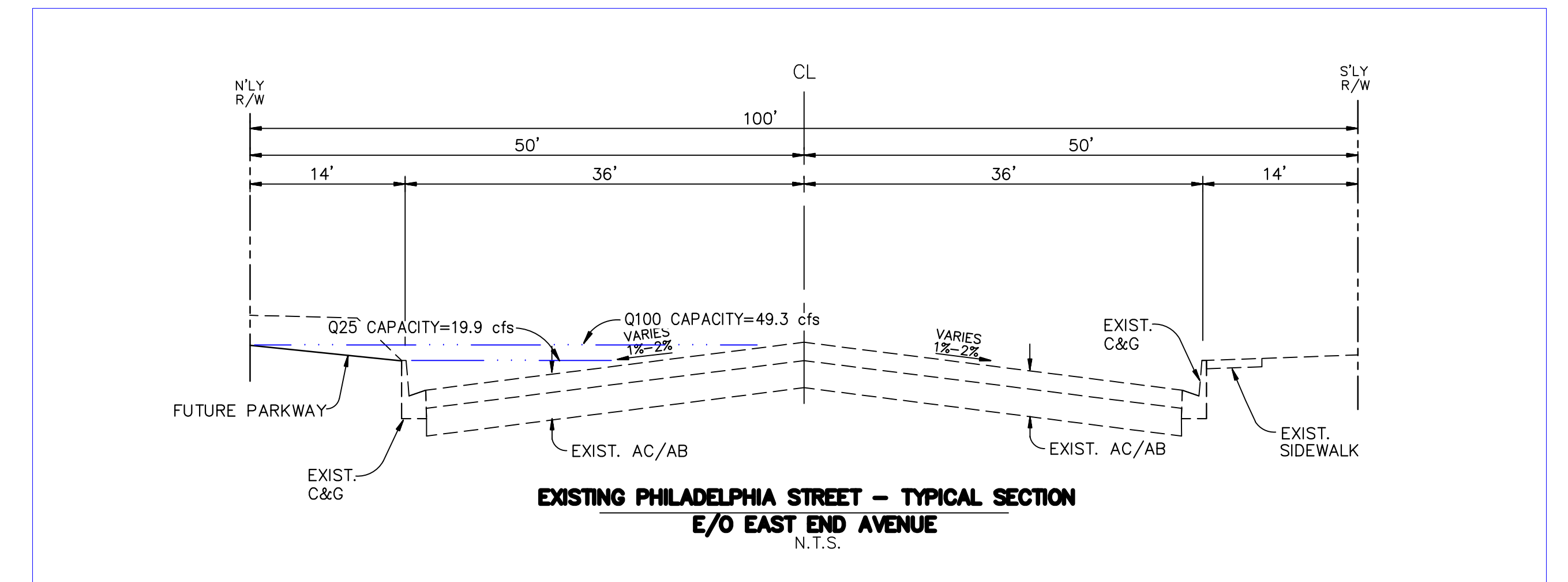
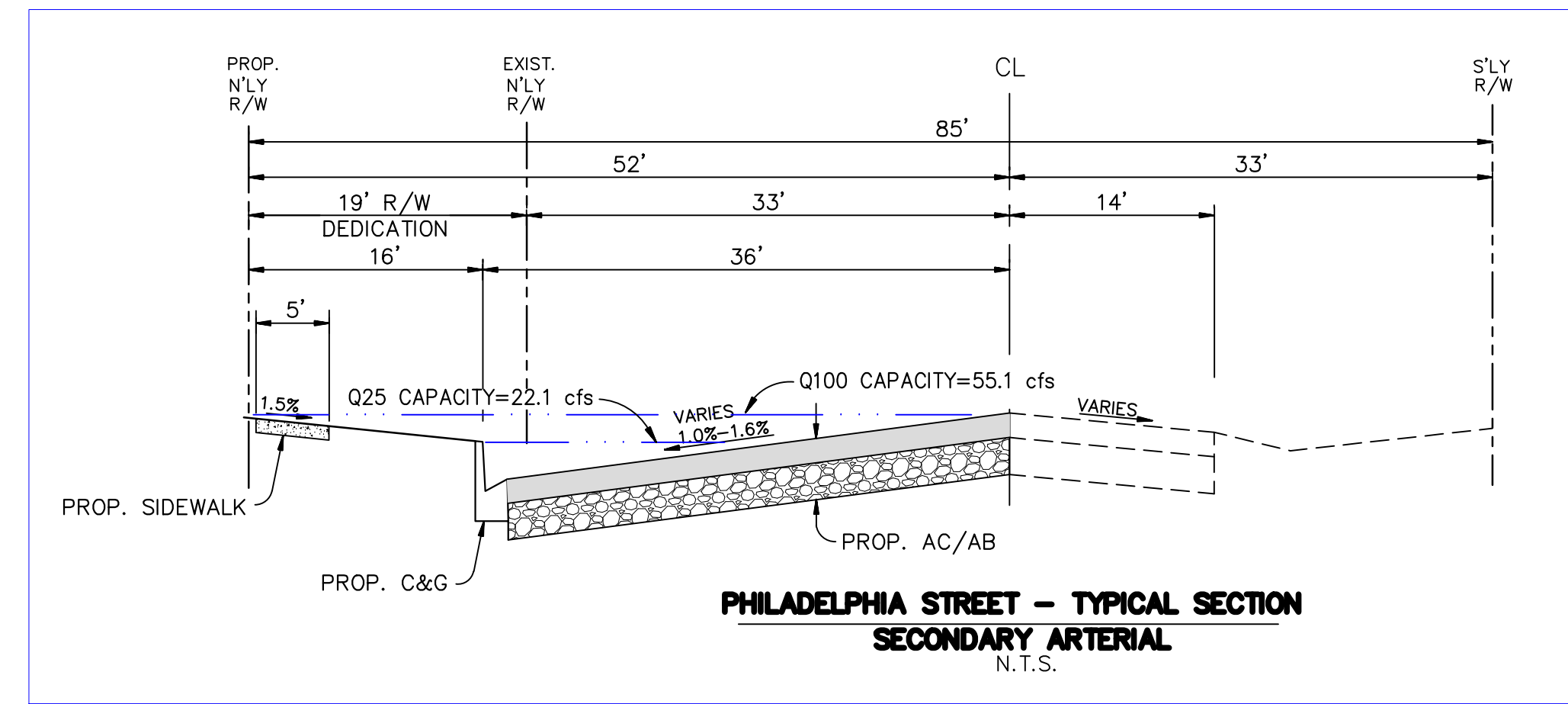
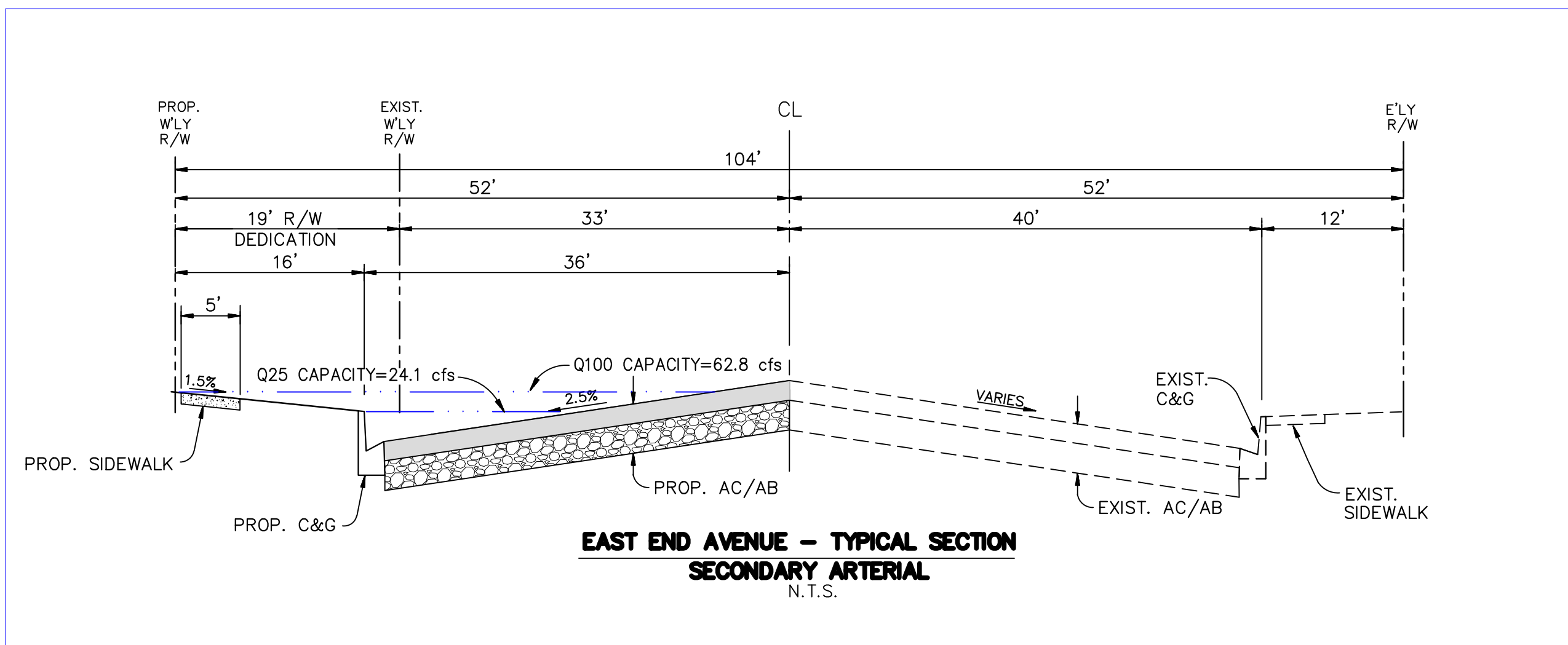
REVISIONS	

**BSI** BSI Consultants, Inc.  
2001 E. First Street  
Santa Ana, CA 92705  
(714) 568-7300

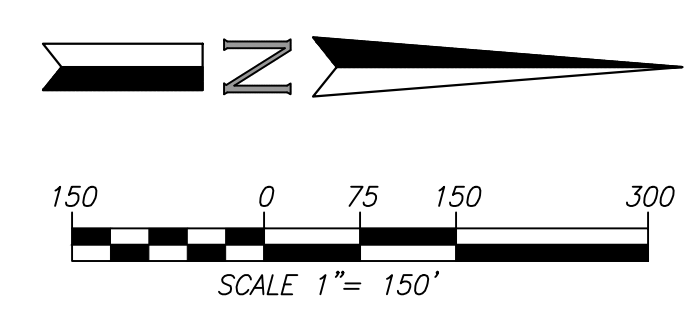
MATCH-LINE  
SEE FIGURE VI-21



## Attachment 1 – PAMA Offsite Drainage Exhibit



- LEGEND**
- HYDROLOGY MODEL NODE NUMBER
  - TRIBUTARY AREA IN ACRES
  - LENGTH OF FLOW
  - DRAINAGE BOUNDARY
  - STREET FLOW LINE
  - PIPE FLOW LINE
  - FLOW DIRECTION

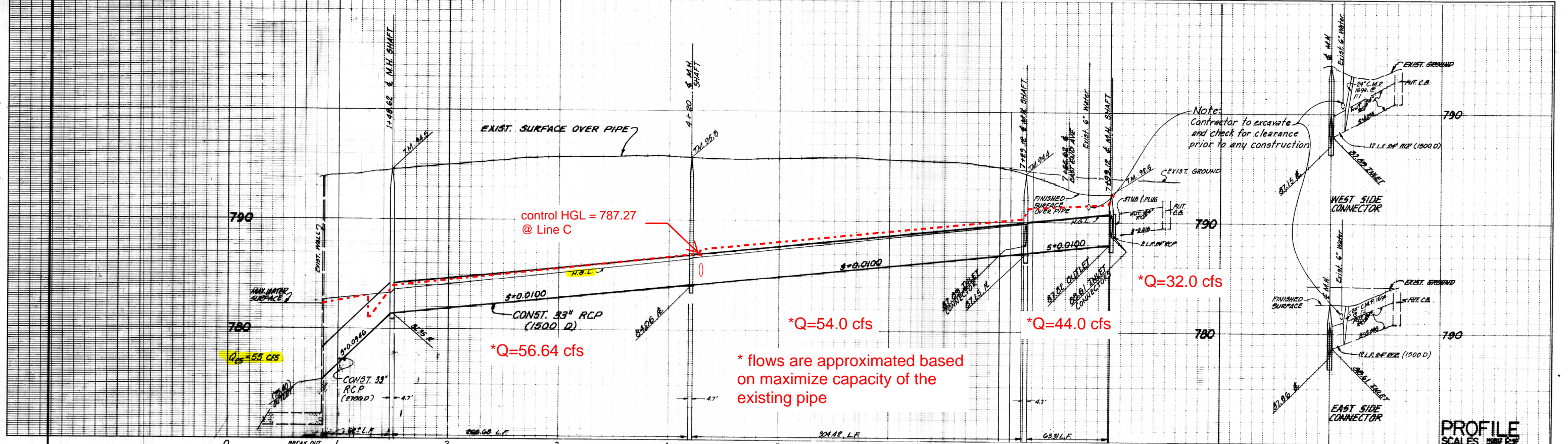


**HUITT-ZOLLARS**  
Huitt-Zollars, Inc. Ontario  
3960 SONDORS, SUITE 330 • ONTARIO, CALIFORNIA 91764 • (909) 941-7799

**COUNTY OF SAN BERNARDINO**  
EXISTING OFF-SITE DRAINAGE MAP FOR  
PHILADELPHIA AND EAST END  
COUNTY OF SAN BERNARDINO  
SHEET **1** NO. **1**



Attachment 2 – City of Chino Existing 33” RCP Plan and Profile

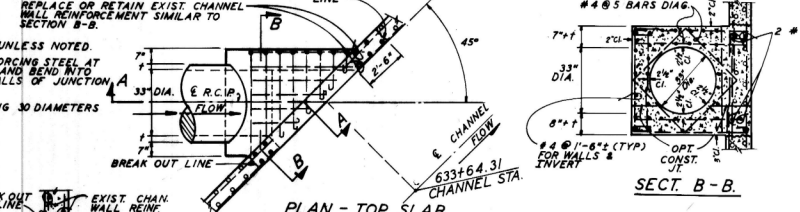


PROFILE  
SCALE 1"=40'

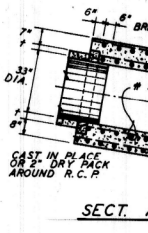
PLAN  
SCALE 1"=40'

**NOTES**

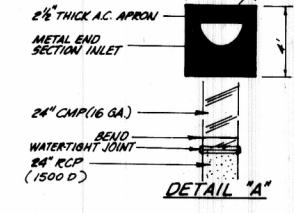
- ALL BARS #4 12" UNLESS NOTED.
- CUT EXPOSED REINFORCING STEEL AT CENTER OF OPENING AND BEND INTO TOP BOTTOM AND WALLS OF JUNCTION STRUCTURE.
- LAP ALL REINFORCING 30 DIAMETERS MIN.



PLAN - TOP SLAB  
JUNCTION STRUCTURE "C" - CASE I



SECT. A-A

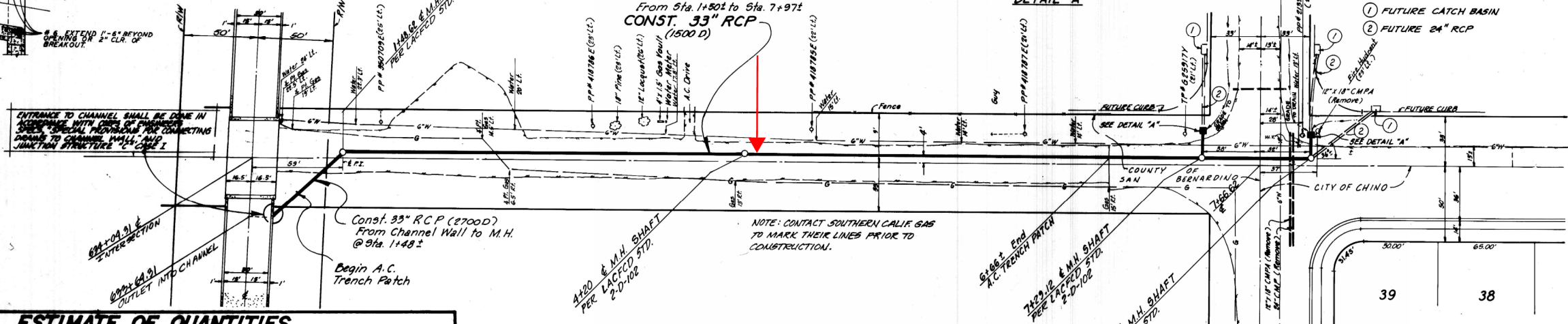


DETAIL "A"

**RECORD DRAWING**  
OCT 11 1974

**GENERAL NOTES**

- ALL WORK SHALL BE DONE IN ACCORDANCE WITH THE CITY OF CHINO STANDARD DRAWINGS, STANDARD SPECIAL PROVISIONS, SPECIAL PROJECT PROVISIONS AND STANDARD SPECIFICATION FOR PUBLIC WORKS CONSTRUCTION 1973 EDITION WITH SUPPLEMENTS, AND LOS ANGELES COUNTY FLOOD CONTROL DISTRICT (LACFD) STANDARD DRAWINGS AND SPECIFICATIONS, AND UNITED STATES ARMY CORPS OF ENGINEERS SPECIFICATIONS.
- ALL EXISTING PAVEMENT TO BE REMOVED SHALL BE REMOVED TO CLEAN STRAIGHT LINES.
- EXISTING PAVEMENT SHALL BE COATED WITH ASPHALTIC EMULSION AT ALL LOCATIONS WHERE NEW PAVEMENT JOINS EXISTING PAVEMENT, FOR A MIN. OF 2 FT. BEYOND THE ADJOINING EDGE.
- ALL EXISTING P.C.C. SHALL BE SAW CUT PRIOR TO REMOVALS.
- ALL MANHOLE FRAMES AND COVERS SHALL BE LOWERED A MIN. OF 2" BELOW SUBGRADE PRIOR TO FINE GRADING AND RAISED TO 1/8" BELOW FINISH GRADE AFTER COMPLETION OF PAVING. MANHOLES NOT LOCATED IN PAVED AREAS SHALL HAVE TOP OF FRAMES AND COVERS AT ELEVATION SHOWN ON PLAN.
- THE CONTRACTOR IS RESPONSIBLE FOR THE PROTECTION AND ADJUSTING OF ALL WATER VALVE BOXES AND COVERS.
- THE CONTRACTOR SHALL MAINTAIN DUST CONTROL AT ALL TIMES BY WATERING.
- AN APPROVED SOIL STERILIZER SHALL BE USED ON ALL SUBGRADES WHEN PLACING A.C. PAVEMENT DIRECTLY ON SUBGRADE.
- WORK IN PUBLIC STREET, ONCE BEGUN, SHALL BE PROSECUTED TO COMPLETION WITHOUT DELAY SO AS TO PROVIDE MINIMUM INCONVENIENCE TO ADJACENT PROPERTY OWNERS AND TO TRAVELING PUBLIC.
- CONTRACTOR SHALL FURNISH THE CITY ENGINEER WITH "AS BUILTS".
- PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL OBTAIN AN ENCROACHMENT PERMIT FROM SAN BERNARDINO COUNTY TRANSPORTATION DEPT.
- PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL OBTAIN A CONSTRUCTION PERMIT FROM THE ARMY CORPS OF ENGINEERS FOR CONSTRUCTION FOR CHANNEL WALL TO MANHOLE AT STATION 7+48.2.
- WORK FROM CHANNEL WALL, STATION 7+97 THROUGH MANHOLE, STATION 7+48.2, SHALL BE COMPLETED PRIOR TO OCTOBER 15, 1978 OR LATER THAN APRIL 15, 1977. MANHOLE AT STATION 7+48.2 SHALL HAVE A WATER TIGHT SEAL AT THE OUTLET IF ENTIRE CONSTRUCTION OF UPSTREAM STORM DRAIN IS NOT COMPLETED PRIOR TO OCTOBER, 1976.
- ANY CONTRACTOR PERFORMING WORK ON THIS PROJECT SHALL FAMILIARIZE HIMSELF WITH THE SITE AND SHALL BE SOLELY RESPONSIBLE FOR ANY DAMAGE TO EXISTING FACILITIES RESULTING DIRECTLY OR INDIRECTLY FROM HIS OPERATIONS, WHETHER OR NOT SUCH FACILITIES ARE SHOWN ON THESE PLANS.



**ESTIMATE OF QUANTITIES**

ITEM	DESCRIPTION	QUANTITY	UNIT	REMARKS
1	33" RCP (1500 D)	639	LF	
2	MANHOLE PER LACFD STD. 2-D-102	4	EA	
3	24" CMP (16 GA)	12	LF	
4	24" RCP (1500 D)	26	LF	
5	METAL END SECTION INLETS	2	EA	
6	CONNECTION TO CONCRETE CHANNEL	LARGE SUM	L.S.	
7	2 1/2" THICK A.C. APRON	38	SF	
8	A.C. TRENCH PATCH	560	LF	
9	33" RCP (2700 D)	62	LF	
10	Adjust M.H. To Grade	4	CA	

**PHILADELPHIA STREET**

NOTE: ARMY CORPS DATUM = 3.25' ± + CITY OF CHINO DATUM

TRACT NO. 9092

EAST END AVENUE

SPECIAL NOTE FROM PRIVATE ENGINEER TO CONTRACTOR  
Contractor agrees that he shall assume sole and complete responsibility for job site conditions during the course of construction of this Project, including safety of all persons and property; that this requirement shall apply continuously and not be limited to normal working hours; and that the Contractor shall defend, indemnify and hold the Owner and the Engineer harmless from any and all liability, real or alleged, in connection with the performance of work on this Project, excepting for liability arising from the sole negligence of the Owner or the Engineer.

DESIGNED BY  
300 EAST 1<sup>ST</sup> STREET  
CHINO, CALIF., 91710  
DATE 8-1-77

NO.	REVISIONS	DATE

BENCH MARK NO. 248 ELEV. 772.55  
LOCATION: CITY OF CHINO  
SPIKE IN EAST CURB OF ROSWELL AVENUE 40' NORTH OF NORTH B.C.R. AT NORTHEAST CORNER OF ROSWELL AVENUE AND MAXON PLACE.

APPROVED BY	DATE	CITY ENGINEER'S STAMP	DATE
TRAFFIC		DRAWN BY	
WATER		CHECKED BY	
SEWER		ENGINEER	
LIGHTS		RECOMMENDED BY	

APPROVED BY  
DATE 3/2/77  
ASSISTANT CITY ENGINEER

**City of Chino Engineering Department**

STORM DRAIN PLAN  
WEST OF EAST END AVENUE  
PHILADELPHIA STREET

Sheet 1 of 1  
DATE 8-1-77  
AA-757

Attachment 3 – Hydraulics: Flowmaster (Street Capacity), WSPG (HGL)

# East End Ave - half street capacity at ROW

## Project Description

Friction Method                      Manning Formula  
Solve For                                Discharge

## Input Data

Channel Slope    0.01070    ft/ft  
Normal Depth    0.91    ft  
Section Definitions

Station (ft)		Elevation (ft)
0+00	@ R/W	0.00
0+16	@ TC	-0.24
0+16	@ FL	-0.91
0+18	@ gutter lip	-0.72
0+52	@ C/L	0.13

## Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.00)	(0+52, 0.13)	0.015

## Options

Current Roughness weighted Method              Pavlovskii's Method  
Open Channel Weighting Method                  Pavlovskii's Method  
Closed Channel Weighting Method              Pavlovskii's Method

## Results

Discharge    **62.83**    **ft<sup>3</sup>/s**  
Elevation Range    -0.91 to 0.13 ft  
Flow Area    13.89    ft<sup>2</sup>  
Wetted Perimeter    47.40    ft  
Hydraulic Radius    0.29    ft  
Top Width    46.80    ft  
Normal Depth    0.91    ft  
Critical Depth    1.00    ft

# East End Ave - half street capacity at ROW

## Results

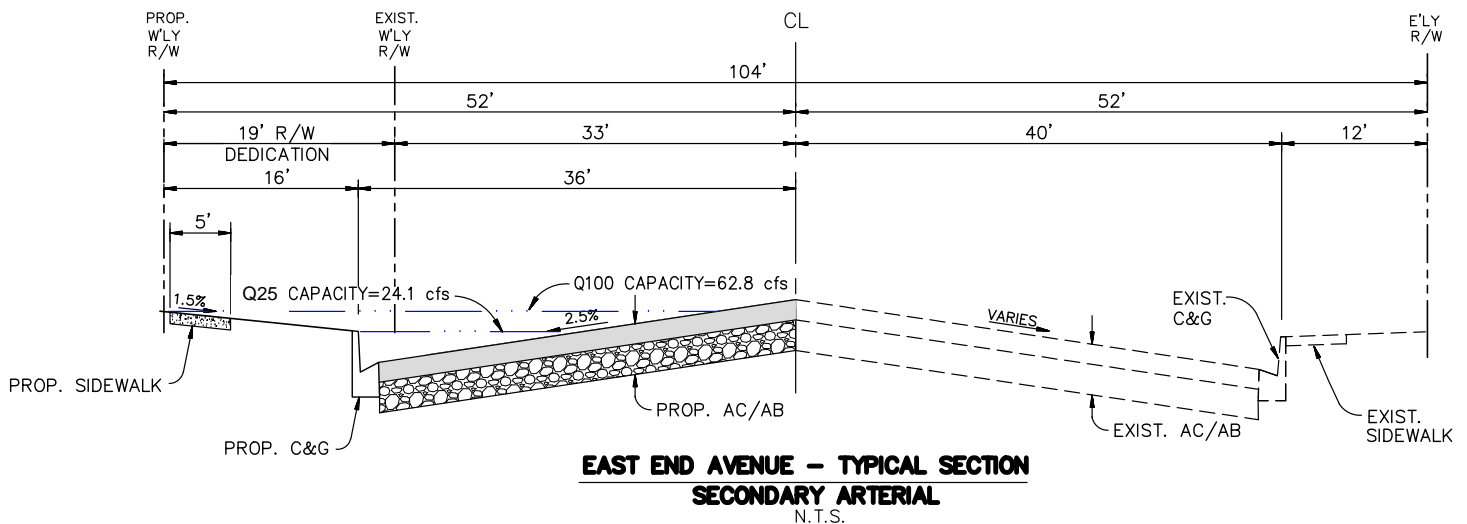
Critical Slope	0.00468	ft/ft
Velocity	4.52	ft/s
Velocity Head	0.32	ft
Specific Energy	1.23	ft
Froude Number	1.46	
Flow Type	Supercritical	

## GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

## GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.91	ft
Critical Depth	1.00	ft
Channel Slope	0.01070	ft/ft
Critical Slope	0.00468	ft/ft



# East End Ave - half street capacity at TC

## Project Description

Friction Method                  Manning Formula  
Solve For                          Discharge

## Input Data

Channel Slope                          0.01070    ft/ft  
Normal Depth                          0.67    ft  
Section Definitions

Station (ft)	Elevation (ft)
0+00 @ R/W	0.00
0+16 @ TC	-0.24
0+16 @ FL	-0.91
0+18 @ gutter lip	-0.72
0+52 @ C/L	0.13

## Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.00)	(0+52, 0.13)	0.015

## Options

Current Roughness Weighted Method                  Pavlovskii's Method  
Open Channel Weighting Method                  Pavlovskii's Method  
Closed Channel Weighting Method                  Pavlovskii's Method

## Results

Discharge    **24.13**    ft<sup>3</sup>/s  
Elevation Range                          -0.91 to 0.13 ft  
Flow Area    5.73    ft<sup>2</sup>  
Wetted Perimeter                          21.79    ft  
Hydraulic Radius                          0.26    ft  
Top Width    21.20    ft  
Normal Depth    0.67    ft  
Critical Depth    0.77    ft

# East End Ave - half street capacity at ROW

## Results

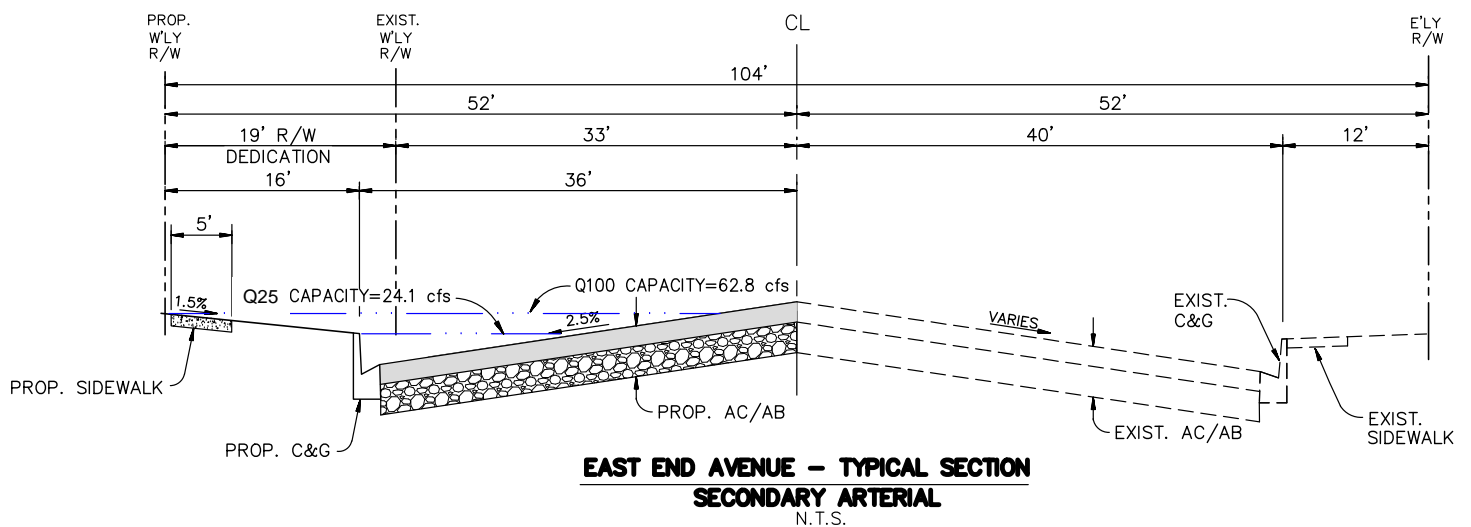
Critical Slope	0.00525	ft/ft
Velocity	4.21	ft/s
Velocity Head	0.28	ft
Specific Energy	0.95	ft
Froude Number	1.43	
Flow Type	Supercritical	

## GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

## GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.67	ft
Critical Depth	0.77	ft
Channel Slope	0.01070	ft/ft
Critical Slope	0.00525	ft/ft



# Philadelphia St. (west of East End) - half street capacity at ROW

**Project Description**

Friction Method	Manning Formula
Solve For	Discharge

**Input Data**

Channel Slope	0.00400	ft/ft
Normal Depth	0.88	ft

Section Definitions

Station (ft)	Elevation (ft)
0+00 @ R/W	0.00
0+16 @ TC	-0.21
0+16 @ FL	-0.88
0+18 @ gutter lip	-0.69
0+52 @ C/L	-0.18

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.00)	(0+52, -0.18)	0.015

**Options**

Current Roughness weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

**Results**

Discharge	55.14	ft <sup>3</sup> /s
Elevation Range	-0.88 to 0.00 ft	
Flow Area	18.02	ft <sup>2</sup>
Wetted Perimeter	52.77	ft
Hydraulic Radius	0.34	ft
Top Width	52.00	ft
Normal Depth	0.88	ft
Critical Depth	0.86	ft



# Philadelphia St. (west of East End) - half street capacity at ROW

## Results

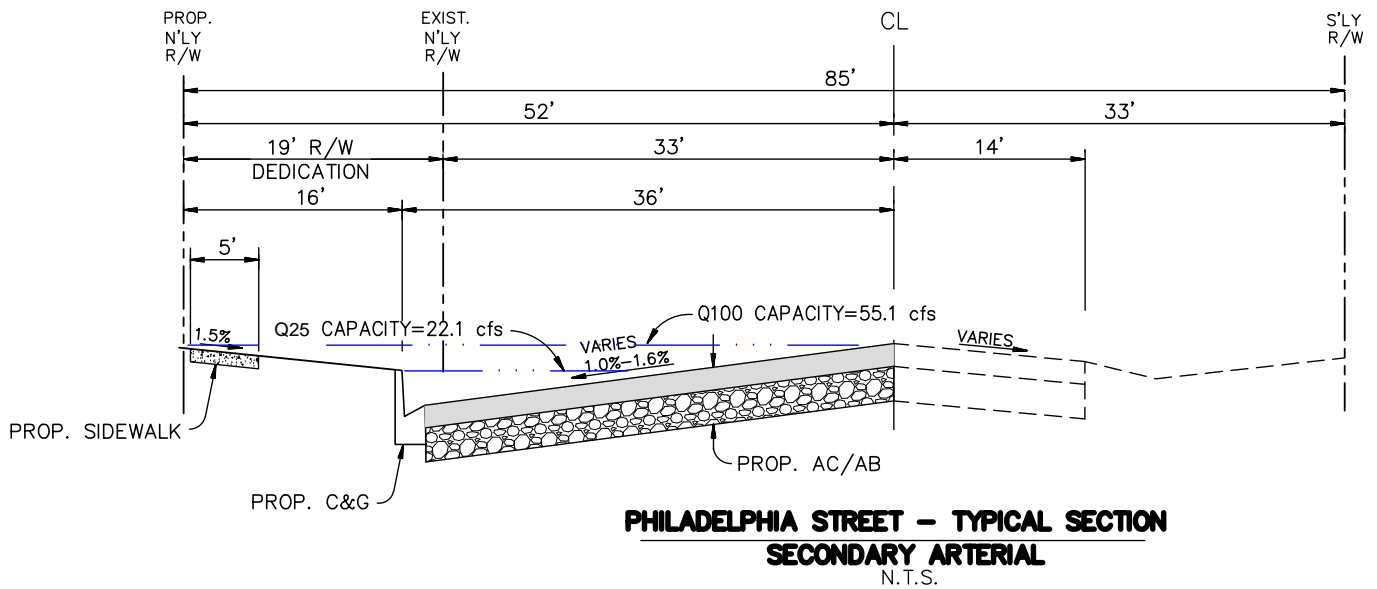
Critical Slope	0.00482	ft/ft
Velocity	3.06	ft/s
Velocity Head	0.15	ft
Specific Energy	1.03	ft
Froude Number	0.92	
Flow Type	Subcritical	

## GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

## GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.88	ft
Critical Depth	0.86	ft
Channel Slope	0.00400	ft/ft
Critical Slope	0.00482	ft/ft



# Philadelphia St. (west of East End) - half street capacity at TC

## Project Description

Friction Method	Manning Formula
Solve For	Discharge

## Input Data

Channel Slope	0.00400	ft/ft
Normal Depth	0.67	ft

Section Definitions

Station (ft)	Elevation (ft)
0+00 @ R/W	0.00
0+16 @ TC	-0.21
0+16 @ FL	-0.88
0+18 @ gutter lip	-0.69
0+52 @ C/L	-0.18

## Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.00)	(0+52, -0.18)	0.015

## Options

Current Roughness weighted Method	Pavlovskii's Method
Open Channel Weighting Method	Pavlovskii's Method
Closed Channel Weighting Method	Pavlovskii's Method

## Results

Discharge	22.16	ft <sup>3</sup> /s
Elevation Range	-0.88 to 0.00	ft
Flow Area	8.81	ft <sup>2</sup>
Wetted Perimeter	34.59	ft
Hydraulic Radius	0.25	ft
Top Width	34.00	ft
Normal Depth	0.67	ft
Critical Depth	0.64	ft

# Philadelphia St. (west of East End) - half street capacity at TC

## Results

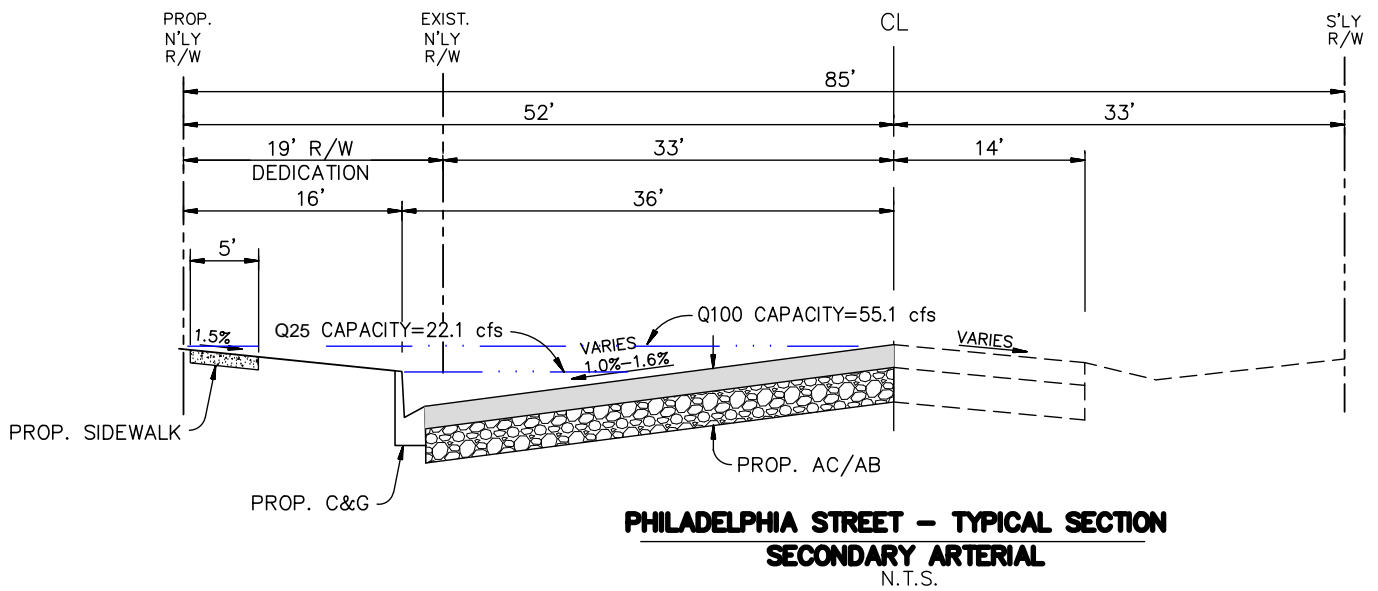
Critical Slope	0.00536	ft/ft
Velocity	2.52	ft/s
Velocity Head	0.10	ft
Specific Energy	0.77	ft
Froude Number	0.87	
Flow Type	Subcritical	

## GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

## GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.67	ft
Critical Depth	0.64	ft
Channel Slope	0.00400	ft/ft
Critical Slope	0.00536	ft/ft



# Philadelphia St. (east of East End) - half street capacity at ROW

**Project Description**

Friction Method                                  Manning Formula  
Solve For    Discharge

**Input Data**

Channel Slope    0.00320    ft/ft  
Normal Depth    0.88    ft  
Section Definitions

Station (ft)	Elevation (ft)
0+00 @ R/W	0.00
0+16 @ TC	-0.21
0+16 @ FL	-0.88
0+18 @ gutter lip	-0.69
0+52 @ C/L	-0.18

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.00)	(0+52, -0.18)	0.015

**Options**

Current Rounghness weignted Method                  Pavlovskii's Method  
Open Channel Weighting Method                  Pavlovskii's Method  
Closed Channel Weighting Method                  Pavlovskii's Method

**Results**

Discharge	49.31    ft³/s
Elevation Range	-0.88 to 0.00 ft
Flow Area	18.02    ft²
Wetted Perimeter	52.77    ft
Hydraulic Radius	0.34    ft
Top Width	52.00    ft
Normal Depth	0.88    ft
Critical Depth	0.83    ft

# Philadelphia St. (east of East End) - half street capacity at ROW

## Results

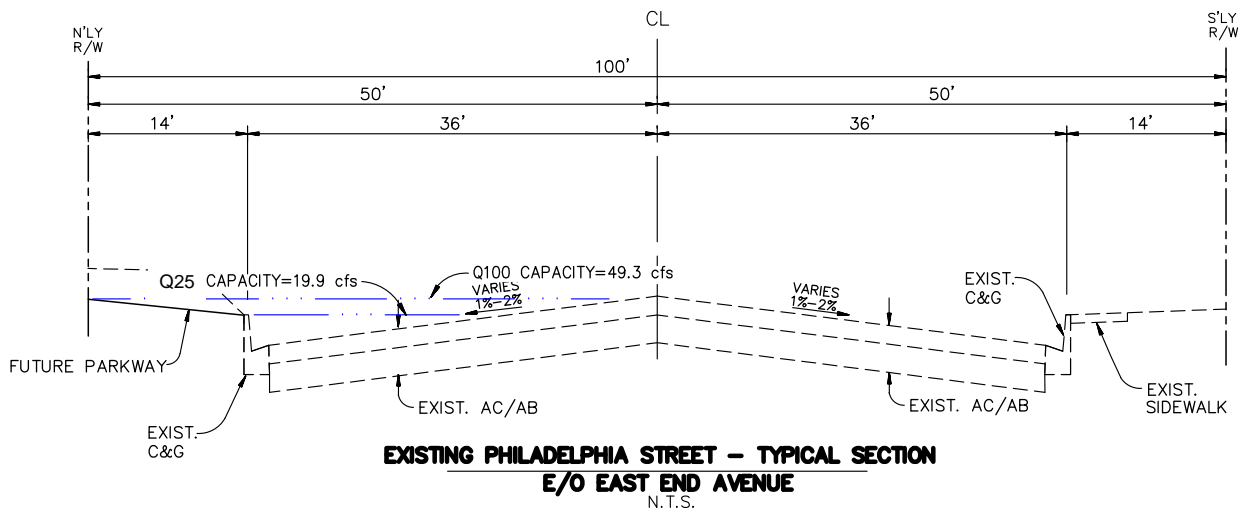
Critical Slope	0.00489	ft/ft
Velocity	2.74	ft/s
Velocity Head	0.12	ft
Specific Energy	1.00	ft
Froude Number	0.82	
Flow Type	Subcritical	

## GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

## GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.88	ft
Critical Depth	0.83	ft
Channel Slope	0.00320	ft/ft
Critical Slope	0.00489	ft/ft



# Philadelphia St. (east of East End) - half street capacity at TC

## Project Description

Friction Method                      Manning Formula  
 Solve For                              Discharge

## Input Data

Channel Slope                                  0.00320    ft/ft  
 Normal Depth                                  0.67    ft  
 Section Definitions

Station (ft)	Elevation (ft)
0+00    @ R/W	0.00
0+16    @ TC	-0.21
0+16    @ FL	-0.88
0+18    @ gutter lip	-0.69
0+52    @ C/L	-0.18

## Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00, 0.00)	(0+52, -0.18)	0.015

## Options

Current Roughness Weighted Method          Pavlovskii's Method  
 Open Channel Weighting Method            Pavlovskii's Method  
 Closed Channel Weighting Method          Pavlovskii's Method

## Results

Discharge    **19.82**    **ft<sup>3</sup>/s**  
 Elevation Range                                  -0.88 to 0.00 ft  
 Flow Area    8.81    ft<sup>2</sup>  
 Wetted Perimeter                                  34.59    ft  
 Hydraulic Radius                                  0.25    ft  
 Top Width    34.00    ft  
 Normal Depth    0.67    ft  
 Critical Depth    0.62    ft

# Philadelphia St. (east of East End) - half street capacity at TC

## Results

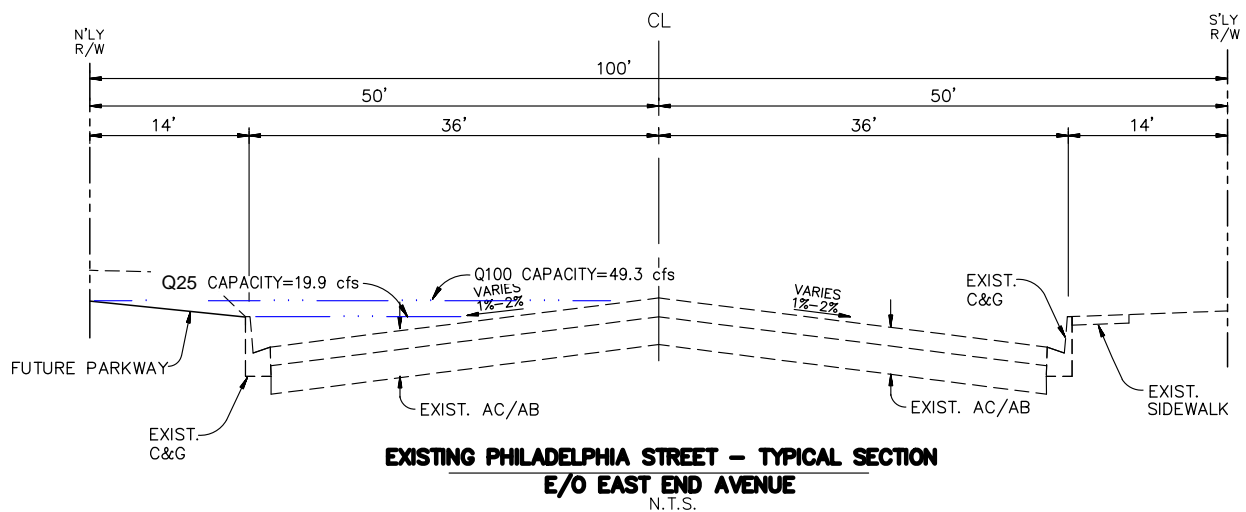
Critical Slope	0.00544	ft/ft
Velocity	2.25	ft/s
Velocity Head	0.08	ft
Specific Energy	0.75	ft
Froude Number	0.78	
Flow Type	Subcritical	

## GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

## GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.67	ft
Critical Depth	0.62	ft
Channel Slope	0.00320	ft/ft
Critical Slope	0.00544	ft/ft







PAMA East End Ave and Philadelphia  
 33" Storm Drain  
 RSK 08/13/21

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Prs/Pip	Wth
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type	Ch
87.000	775.400	6.900	782.300	56.64	9.54	1.41	783.71	.00	2.44	.00	2.750	.000	.00	1	.0
38.583	.0966					.0115	.44	6.90	.00	1.11	.013	.00	.00	PIPE	
125.583	779.126	3.817	782.943	56.64	9.54	1.41	784.35	.00	2.44	.00	2.750	.000	.00	1	.0
HYDRAULIC JUMP															
125.583	779.126	1.542	780.667	56.64	16.52	4.24	784.91	.00	2.44	2.73	2.750	.000	.00	1	.0
.752	.0966					.0310	.02	1.54	2.60	1.11	.013	.00	.00	PIPE	
126.335	779.198	1.553	780.751	56.64	16.37	4.16	784.91	.00	2.44	2.73	2.750	.000	.00	1	.0
4.677	.0966					.0289	.14	1.55	2.56	1.11	.013	.00	.00	PIPE	
131.012	779.650	1.615	781.265	56.64	15.61	3.78	785.05	.00	2.44	2.71	2.750	.000	.00	1	.0
3.916	.0966					.0256	.10	1.62	2.38	1.11	.013	.00	.00	PIPE	
134.928	780.028	1.681	781.709	56.64	14.89	3.44	785.15	.00	2.44	2.68	2.750	.000	.00	1	.0
3.284	.0966					.0226	.07	1.68	2.20	1.11	.013	.00	.00	PIPE	
138.212	780.345	1.751	782.096	56.64	14.19	3.13	785.22	.00	2.44	2.65	2.750	.000	.00	1	.0
2.750	.0966					.0201	.06	1.75	2.04	1.11	.013	.00	.00	PIPE	
140.962	780.611	1.825	782.436	56.64	13.53	2.84	785.28	.00	2.44	2.60	2.750	.000	.00	1	.0
2.281	.0966					.0179	.04	1.83	1.88	1.11	.013	.00	.00	PIPE	
143.243	780.831	1.904	782.735	56.64	12.90	2.58	785.32	.00	2.44	2.54	2.750	.000	.00	1	.0
1.848	.0966					.0159	.03	1.90	1.73	1.11	.013	.00	.00	PIPE	

WATER SURFACE PROFILE LISTING

Date: 8-16-2021 Time:11: 1: 0

PAMA East End Ave and Philadelphia  
33" Storm Drain  
RSK 08/13/21

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Prs/Pip	Wth
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type	Ch
145.090	781.009	1.990	782.999	56.64	12.30	2.35	785.35	.00	2.44	2.46	2.750	.000	.00	1	.0
	1.465	.0966				.0142	.02	1.99	1.58	1.11	.013	.00	.00	PIPE	
146.555	781.151	2.083	783.234	56.64	11.73	2.14	785.37	.00	2.44	2.36	2.750	.000	.00	1	.0
	1.089	.0966				.0128	.01	2.08	1.44	1.11	.013	.00	.00	PIPE	
147.644	781.256	2.186	783.442	56.64	11.18	1.94	785.38	.00	2.44	2.22	2.750	.000	.00	1	.0
	.713	.0966				.0116	.01	2.19	1.30	1.11	.013	.00	.00	PIPE	
148.357	781.325	2.302	783.627	56.64	10.66	1.77	785.39	.00	2.44	2.03	2.750	.000	.00	1	.0
	.263	.0966				.0106	.00	2.30	1.16	1.11	.013	.00	.00	PIPE	
148.620	781.350	2.441	783.791	56.64	10.16	1.60	785.39	.00	2.44	1.74	2.750	.000	.00	1	.0
	85.456	.0096				.0101	.86	2.44	1.00	2.75	.013	.00	.00	PIPE	
234.076	782.173	2.626	784.799	56.64	9.69	1.46	786.26	.00	2.44	1.14	2.750	.000	.00	1	.0
	98.495	.0096				.0104	1.03	2.63	.75	2.75	.013	.00	.00	PIPE	
332.571	783.122	2.750	785.872	56.64	9.54	1.41	787.28	.00	2.44	.00	2.750	.000	.00	1	.0
	97.429	.0096				.0112	1.09	2.75	.00	2.75	.013	.00	.00	PIPE	
430.000	784.060	2.929	786.989	56.64	9.54	1.41	788.40	.00	2.44	.00	2.750	.000	.00	1	.0
JUNCT STR	.0200					.0109	.02	2.93	.00		.013	.00	.00	PIPE	
432.000	784.100	3.168	787.268	54.00	9.09	1.28	788.55	.00	2.40	.00	2.750	.000	.00	1	.0
	295.120	.0103				.0104	3.08	3.17	.00	2.27	.013	.00	.00	PIPE	

WATER SURFACE PROFILE LISTING

Date: 8-16-2021 Time:11: 1: 0

PAMA East End Ave and Philadelphia  
33" Storm Drain  
RSK 08/13/21

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	ZL	No Prs/Pip	Wth
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type	Ch
727.120	787.130	3.215	790.345	54.00	9.09	1.28	791.63	.00	2.40	.00	2.750	.000	.00	1	.0
JUNCT STR	.0100					.0087	.03	3.21	.00		.013	.00	.00	PIPE	
731.120	787.170	4.072	791.242	44.00	7.41	.85	792.09	.00	2.20	.00	2.750	.000	.00	1	.0
66.000	.0095					.0069	.46	4.07	.00	1.95	.013	.00	.00	PIPE	
797.120	787.800	3.899	791.699	44.00	7.41	.85	792.55	.00	2.20	.00	2.750	.000	.00	1	.0
JUNCT STR	.0100					.0053	.02	3.90	.00		.013	.00	.00	PIPE	
801.120	787.840	4.683	792.523	32.00	5.39	.45	792.97	.00	1.88	.00	2.750	.000	.00	1	.0
328.921	.0095					.0036	1.19	4.68	.00	1.57	.013	.00	.00	PIPE	
1130.041	790.977	2.750	793.727	32.00	5.39	.45	794.18	.00	1.88	.00	2.750	.000	.00	1	.0
34.036	.0095					.0034	.12	2.75	.00	1.57	.013	.00	.00	PIPE	
1164.077	791.302	2.495	793.797	32.00	5.65	.50	794.29	.00	1.88	1.59	2.750	.000	.00	1	.0
15.816	.0095					.0033	.05	2.50	.53	1.57	.013	.00	.00	PIPE	
1179.893	791.453	2.347	793.800	32.00	5.93	.55	794.35	.00	1.88	1.94	2.750	.000	.00	1	.0
9.588	.0095					.0036	.03	2.35	.63	1.57	.013	.00	.00	PIPE	
1189.481	791.544	2.246	793.791	32.00	6.16	.59	794.38	.00	1.88	2.13	2.750	.000	.00	1	.0
HYDRAULIC JUMP															
1189.481	791.544	1.566	793.111	32.00	9.16	1.30	794.41	.00	1.88	2.72	2.750	.000	.00	1	.0
22.545	.0095					.0095	.22	1.57	1.42	1.57	.013	.00	.00	PIPE	

WATER SURFACE PROFILE LISTING

Date: 8-16-2021 Time:11: 1: 0

PAMA East End Ave and Philadelphia  
33" Storm Drain  
RSK 08/13/21

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*****
| Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height/ | Base Wt | | No Wth
Station | Elev | (FT) | Elev | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
-|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|-
L/Elem |Ch Slope | | | | | | | | | | | | | | ZR | Type Ch
*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****|*****
| | | | | | | | | | | | | | | | |
1212.026 | 791.759 | 1.566 | 793.326 | 32.00 | 9.16 | 1.30 | 794.63 | .00 | 1.88 | 2.72 | 2.750 | .000 | .00 | 1 | .0
-|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|-
103.884 | .0095 | | | | | | | | | | | | | | .00 | .00 | PIPE
| | | | | | | | | | | | | | | | |
1315.910 | 792.750 | 1.597 | 794.347 | 32.00 | 8.94 | 1.24 | 795.59 | .00 | 1.88 | 2.71 | 2.750 | .000 | .00 | 1 | .0
-|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|-
45.003 | .0095 | | | | | | | | | | | | | | .00 | .00 | PIPE
| | | | | | | | | | | | | | | | |
1360.913 | 793.180 | 1.661 | 794.841 | 32.00 | 8.53 | 1.13 | 795.97 | .00 | 1.88 | 2.69 | 2.750 | .000 | .00 | 1 | .0
-|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|-
16.357 | .0095 | | | | | | | | | | | | | | .00 | .00 | PIPE
| | | | | | | | | | | | | | | | |
1377.270 | 793.336 | 1.730 | 795.066 | 32.00 | 8.13 | 1.03 | 796.09 | .00 | 1.88 | 2.66 | 2.750 | .000 | .00 | 1 | .0
-|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|-
6.997 | .0095 | | | | | | | | | | | | | | .00 | .00 | PIPE
| | | | | | | | | | | | | | | | |
1384.267 | 793.402 | 1.803 | 795.205 | 32.00 | 7.75 | .93 | 796.14 | .00 | 1.88 | 2.61 | 2.750 | .000 | .00 | 1 | .0
-|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|-
1.863 | .0095 | | | | | | | | | | | | | | .00 | .00 | PIPE
| | | | | | | | | | | | | | | | |
1386.130 | 793.420 | 1.882 | 795.302 | 32.00 | 7.39 | .85 | 796.15 | .00 | 1.88 | 2.56 | 2.750 | .000 | .00 | 1 | .0
-|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|- -|-

```

Attachment 4 – Hydrology: AES (Rational Method)

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION)  
(c) Copyright 1983-2014 Advanced Engineering Software (aes)  
Ver. 21.0 Release Date: 06/01/2014 License ID 1202

Analysis prepared by:

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2603 Main Street, Irvine CA. 92614  
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949-988-5815

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* PAMA INDUSTRIAL - PHILADELPHIA ST AT EAST END AVE \*  
\* RATIONAL METHOD 10 YEAR STORM EVENT \*  
\* RYAN KIM HC 08/12/21 \*  
\*\*\*\*\*

FILE NAME: PAMA10\_A.DAT  
TIME/DATE OF STUDY: 10:45 08/12/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL\*

SLOPE OF INTENSITY DURATION CURVE(LOG(I;IN/HR) vs. LOG(Tc;MIN)) = 0.6000  
USER SPECIFIED 1-HOUR INTENSITY(INCH/HOUR) = 0.9490

\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	41.0	34.0	0.025/0.025/ ---	0.67	2.00	0.0313	0.167	0.0130
2	30.0	23.0	0.020/0.020/ ---	0.50	1.50	0.0313	0.125	0.0130

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.67 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 736.00  
ELEVATION DATA: UPSTREAM(FEET) = 840.00 DOWNSTREAM(FEET) = 837.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 12.811

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.397

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
"2 DWELLINGS/ACRE"	A	1.53	0.98	0.700	32	18.46
COMMERCIAL	A	0.60	0.98	0.100	32	12.81

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.97  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.531  
SUBAREA RUNOFF(CFS) = 3.60  
TOTAL AREA(ACRES) = 2.13 PEAK FLOW RATE(CFS) = 3.60

\*\*\*\*\*

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 837.00 DOWNSTREAM ELEVATION(FEET) = 822.00

STREET LENGTH(FEET) = 1519.00 CURB HEIGHT(INCHES) = 8.0

STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.025

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.89

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.41

HALFSTREET FLOOD WIDTH(FEET) = 10.57

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.10

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.28

STREET FLOW TRAVEL TIME(MIN.) = 8.15 Tc(MIN.) = 20.96

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.783

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	1.70	0.98	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 2.58

EFFECTIVE AREA(ACRES) = 3.83 AREA-AVERAGED Fm(INCH/HR) = 0.33

AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.34

TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 5.01

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 10.65

FLOW VELOCITY(FEET/SEC.) = 3.14 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.30

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 2255.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 822.00 DOWNSTREAM ELEVATION(FEET) = 805.00
STREET LENGTH(FEET) = 1469.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.025
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.28
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.43
HALFSTREET FLOOD WIDTH(FEET) = 11.41
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.48
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.51
STREET FLOW TRAVEL TIME(MIN.) = 7.04 Tc(MIN.) = 28.00
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.499

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 2.02 0.98 0.100 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.97
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.02 SUBAREA RUNOFF(CFS) = 2.55
EFFECTIVE AREA(ACRES) = 5.85 AREA-AVERAGED Fm(INCH/HR) = 0.25
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.26
TOTAL AREA(ACRES) = 5.9 PEAK FLOW RATE(CFS) = 6.57

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 11.56
FLOW VELOCITY(FEET/SEC.) = 3.55 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.55
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 3724.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 805.00 DOWNSTREAM ELEVATION(FEET) = 799.00
STREET LENGTH(FEET) = 510.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.025
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.99
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.44
HALFSTREET FLOOD WIDTH(FEET) = 11.86
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.60
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.60
STREET FLOW TRAVEL TIME(MIN.) = 2.36 Tc(MIN.) = 30.36
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.428



SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.69	0.98	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.69 SUBAREA RUNOFF(CFS) = 0.83  
EFFECTIVE AREA(ACRES) = 6.54 AREA-AVERAGED Fm(INCH/HR) = 0.23  
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.24  
TOTAL AREA(ACRES) = 6.5 PEAK FLOW RATE(CFS) = 7.03

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 11.86  
FLOW VELOCITY(FEET/SEC.) = 3.62 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.61  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 4234.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 799.00 DOWNSTREAM ELEVATION(FEET) = 792.00  
STREET LENGTH(FEET) = 650.00 CURB HEIGHT(INCHES) = 8.0  
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.025  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.53  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.46  
HALFSTREET FLOOD WIDTH(FEET) = 12.47  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.54  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.63  
STREET FLOW TRAVEL TIME(MIN.) = 3.06 Tc(MIN.) = 33.42  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.348

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.89	0.98	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.89 SUBAREA RUNOFF(CFS) = 1.00  
EFFECTIVE AREA(ACRES) = 7.43 AREA-AVERAGED Fm(INCH/HR) = 0.22  
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.22  
TOTAL AREA(ACRES) = 7.4 PEAK FLOW RATE(CFS) = 7.56

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.46 HALFSTREET FLOOD WIDTH(FEET) = 12.47  
FLOW VELOCITY(FEET/SEC.) = 3.56 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.64  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 4884.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

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=====
MAINLINE Tc(MIN.) = 33.42
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.348
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap        SCS
LAND USE                GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"2 DWELLINGS/ACRE"      A        5.29      0.98      0.700     32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700
SUBAREA AREA(ACRES) = 5.29      SUBAREA RUNOFF(CFS) = 3.17
EFFECTIVE AREA(ACRES) = 12.72   AREA-AVERAGED Fm(INCH/HR) = 0.41
AREA-AVERAGED Fp(INCH/HR) = 0.98  AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 12.7      PEAK FLOW RATE(CFS) = 10.73

*****
FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====
*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 694.00
ELEVATION DATA: UPSTREAM(FEET) = 818.00  DOWNSTREAM(FEET) = 810.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 14.644
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.212
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap        SCS  Tc
LAND USE                GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"2 DWELLINGS/ACRE"      A        8.96      0.98      0.700     32  14.64
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700
SUBAREA RUNOFF(CFS) = 12.33
TOTAL AREA(ACRES) = 8.96   PEAK FLOW RATE(CFS) = 12.33

*****
FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 810.00  DOWNSTREAM ELEVATION(FEET) = 803.00
STREET LENGTH(FEET) = 872.00  CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 23.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 21.09

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STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.48  
 HALFSTREET FLOOD WIDTH(FEET) = 17.67  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.25  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.56  
 STREET FLOW TRAVEL TIME(MIN.) = 4.47 Tc(MIN.) = 19.11  
 \* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.885  
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "2 DWELLINGS/ACRE"	A	16.10	0.98	0.700	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700  
 SUBAREA AREA(ACRES) = 16.10 SUBAREA RUNOFF(CFS) = 17.43  
 EFFECTIVE AREA(ACRES) = 25.06 AREA-AVERAGED Fm(INCH/HR) = 0.68  
 AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.70  
 TOTAL AREA(ACRES) = 25.1 PEAK FLOW RATE(CFS) = 27.13

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.52 HALFSTREET FLOOD WIDTH(FEET) = 19.51  
 FLOW VELOCITY(FEET/SEC.) = 3.46 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.79  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 1566.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 2 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 803.00 DOWNSTREAM ELEVATION(FEET) = 800.00  
 STREET LENGTH(FEET) = 570.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 23.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 31.16  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 NOTE: STREET FLOW EXCEEDS TOP OF CURB.  
 THE FOLLOWING STREET FLOW RESULTS ARE BASED ON THE ASSUMPTION  
 THAT NEGLIBLE FLOW OCCURS OUTSIDE OF THE STREET CHANNEL.  
 THAT IS, ALL FLOW ALONG THE PARKWAY, ETC., IS NEGLECTED.

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "2 DWELLINGS/ACRE"	A	8.61	0.98	0.700	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700  
 SUBAREA AREA(ACRES) = 8.61 SUBAREA RUNOFF(CFS) = 8.05

EFFECTIVE AREA(ACRES) = 33.67 AREA-AVERAGED Fm(INCH/HR) = 0.68  
 AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.70  
 TOTAL AREA(ACRES) = 33.7 PEAK FLOW RATE(CFS) = 31.50

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.57 HALFSTREET FLOOD WIDTH(FEET) = 22.40  
 FLOW VELOCITY(FEET/SEC.) = 3.07 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.76  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 2136.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 303.00 TO NODE 106.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 793.40 DOWNSTREAM(FEET) = 787.82  
 FLOW LENGTH(FEET) = 673.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.35  
 ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 31.50  
 PIPE TRAVEL TIME(MIN.) = 1.34 Tc(MIN.) = 23.57  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 106.00 = 2809.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	31.50	23.57	1.662	0.98( 0.68)	0.70	33.7	300.00

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 106.00 = 2809.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	10.73	33.42	1.348	0.98( 0.41)	0.42	12.7	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 106.00 = 4884.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	41.60	23.57	1.662	0.98( 0.63)	0.64	42.6	300.00
2	32.13	33.42	1.348	0.97( 0.61)	0.62	46.4	100.00
TOTAL AREA(ACRES) =		46.4					

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 41.60 Tc(MIN.) = 23.572  
 EFFECTIVE AREA(ACRES) = 42.64 AREA-AVERAGED Fm(INCH/HR) = 0.63  
 AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.64  
 TOTAL AREA(ACRES) = 46.4  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 106.00 = 4884.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 12  
 -----

>>>>CLEAR MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	787.82	DOWNSTREAM(FEET) =	787.15
FLOW LENGTH(FEET) =	70.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 33.0 INCH PIPE IS	22.8 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	9.48		
ESTIMATED PIPE DIAMETER(INCH) =	33.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	41.60		
PIPE TRAVEL TIME(MIN.) =	0.12	Tc(MIN.) =	23.69
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 =	4954.00 FEET.		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) =	1000.00		
ELEVATION DATA: UPSTREAM(FEET) =	822.00	DOWNSTREAM(FEET) =	810.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.669

\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.535

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	1.24	0.98	0.100	32	11.67

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA RUNOFF(CFS) = 2.72

TOTAL AREA(ACRES) = 1.24 PEAK FLOW RATE(CFS) = 2.72

\*\*\*\*\*  
FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	810.00	DOWNSTREAM ELEVATION(FEET) =	798.00
STREET LENGTH(FEET) =	1000.00	CURB HEIGHT(INCHES) =	8.0
STREET HALFWIDTH(FEET) =	41.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.025

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.48

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.43  
HALFSTREET FLOOD WIDTH(FEET) = 11.41  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.59  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.56  
STREET FLOW TRAVEL TIME(MIN.) = 4.64 Tc(MIN.) = 16.31  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.073  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	4.21	0.98	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 4.21 SUBAREA RUNOFF(CFS) = 7.49  
EFFECTIVE AREA(ACRES) = 5.45 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 5.4 PEAK FLOW RATE(CFS) = 9.69

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 13.54  
FLOW VELOCITY(FEET/SEC.) = 3.92 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.91  
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 2000.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 798.00 DOWNSTREAM ELEVATION(FEET) = 794.00  
STREET LENGTH(FEET) = 550.00 CURB HEIGHT(INCHES) = 8.0  
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.025  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.53  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.54  
HALFSTREET FLOOD WIDTH(FEET) = 15.52  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.30  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.77  
STREET FLOW TRAVEL TIME(MIN.) = 2.78 Tc(MIN.) = 19.09  
\* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.887  
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	1.04	0.98	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 1.04 SUBAREA RUNOFF(CFS) = 1.67  
EFFECTIVE AREA(ACRES) = 6.49 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 6.5 PEAK FLOW RATE(CFS) = 10.45

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.53 HALFSTREET FLOOD WIDTH(FEET) = 15.44

FLOW VELOCITY(FEET/SEC.) = 3.31 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.77  
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 203.00 = 2550.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 203.00 TO NODE 107.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\*\*\*\*  
\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	10.45	19.09	1.887	0.98( 0.10)	0.10	6.5	200.00

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 107.00 = 2550.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	41.60	23.69	1.657	0.98( 0.63)	0.64	42.6	300.00
2	32.13	33.55	1.345	0.97( 0.61)	0.62	46.4	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 4954.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	51.42	19.09	1.887	0.98( 0.54)	0.56	40.8	200.00
2	50.71	23.69	1.657	0.97( 0.56)	0.57	49.1	300.00
3	39.41	33.55	1.345	0.98( 0.55)	0.56	52.9	100.00

TOTAL AREA(ACRES) = 52.9

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 51.42 Tc(MIN.) = 19.090  
EFFECTIVE AREA(ACRES) = 40.85 AREA-AVERAGED Fm(INCH/HR) = 0.54  
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.56  
TOTAL AREA(ACRES) = 52.9  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 4954.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 787.15 DOWNSTREAM(FEET) = 784.90  
FLOW LENGTH(FEET) = 315.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.83  
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 51.42  
PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 19.68  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 5269.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
MAINLINE Tc(MIN.) = 19.68
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 1.852
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/   SCS SOIL   AREA      Fp        Ap      SCS
LAND USE            GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
COMMERCIAL          A        3.60     0.98     0.100    32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 3.60      SUBAREA RUNOFF(CFS) = 5.69
EFFECTIVE AREA(ACRES) = 44.45   AREA-AVERAGED Fm(INCH/HR) = 0.51
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.52
TOTAL AREA(ACRES) = 56.5      PEAK FLOW RATE(CFS) = 53.87

```

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 109.00 IS CODE = 31

```

-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 784.90 DOWNSTREAM(FEET) = 775.00
FLOW LENGTH(FEET) = 332.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 30.0 INCH PIPE IS 19.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.55
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 53.87
PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 20.04
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 109.00 = 5601.00 FEET.

```

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-----
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 56.5 TC(MIN.) = 20.04
EFFECTIVE AREA(ACRES) = 44.45 AREA-AVERAGED Fm(INCH/HR)= 0.51
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.519
PEAK FLOW RATE(CFS) = 53.87

```

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	53.87	20.04	1.832	0.98( 0.51)	0.52	44.4	200.00
2	52.60	24.65	1.618	0.97( 0.52)	0.54	52.7	300.00
3	41.33	34.56	1.321	0.98( 0.52)	0.53	56.5	100.00

END OF RATIONAL METHOD ANALYSIS





\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION)  
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Ver. 21.0 Release Date: 06/01/2014 License ID 1202

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* PAMA EAST END AVE PHILADELPHIA ST \*  
\* RATIONAL METHOD 25 YEAR STORM EVENT \*  
\* RYAN KIM HC 08/09/21 \*  
\*\*\*\*\*

FILE NAME: PAMA25\_A.DAT  
TIME/DATE OF STUDY: 01:05 08/09/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL\*

SLOPE OF INTENSITY DURATION CURVE(LOG(I;IN/HR) vs. LOG(Tc;MIN)) = 0.6000  
USER SPECIFIED 1-HOUR INTENSITY(INCH/HOUR) = 1.1700

\*ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	41.0	34.0	0.025/0.025/ ---	0.67	2.00	0.0313	0.167	0.0130
2	30.0	23.0	0.020/0.020/ ---	0.50	1.50	0.0313	0.125	0.0130

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.67 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 736.00  
ELEVATION DATA: UPSTREAM(FEET) = 840.00 DOWNSTREAM(FEET) = 837.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 12.811

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.955

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
"2 DWELLINGS/ACRE"	A	1.53	0.98	0.700	32	18.46
COMMERCIAL	A	0.60	0.98	0.100	32	12.81

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.97  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.531  
SUBAREA RUNOFF(CFS) = 4.67  
TOTAL AREA(ACRES) = 2.13 PEAK FLOW RATE(CFS) = 4.67

\*\*\*\*\*

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 837.00 DOWNSTREAM ELEVATION(FEET) = 822.00

STREET LENGTH(FEET) = 1519.00 CURB HEIGHT(INCHES) = 8.0

STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.025

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.31

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.44

HALFSTREET FLOOD WIDTH(FEET) = 11.79

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.29

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.46

STREET FLOW TRAVEL TIME(MIN.) = 7.69 Tc(MIN.) = 20.50

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.228

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	1.70	0.98	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 3.26

EFFECTIVE AREA(ACRES) = 3.83 AREA-AVERAGED Fm(INCH/HR) = 0.33

AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.34

TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 6.54

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.45 HALFSTREET FLOOD WIDTH(FEET) = 11.94

FLOW VELOCITY(FEET/SEC.) = 3.33 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.49

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 2255.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 822.00 DOWNSTREAM ELEVATION(FEET) = 805.00
STREET LENGTH(FEET) = 1469.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.025
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.16
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.47
HALFSTREET FLOOD WIDTH(FEET) = 12.70
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.72
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.73
STREET FLOW TRAVEL TIME(MIN.) = 6.59 Tc(MIN.) = 27.09
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 1.885

SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 2.02 0.98 0.100 32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.97
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.02 SUBAREA RUNOFF(CFS) = 3.25
EFFECTIVE AREA(ACRES) = 5.85 AREA-AVERAGED Fm(INCH/HR) = 0.25
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.26
TOTAL AREA(ACRES) = 5.9 PEAK FLOW RATE(CFS) = 8.61

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 13.01
FLOW VELOCITY(FEET/SEC.) = 3.75 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.78
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 3724.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 805.00 DOWNSTREAM ELEVATION(FEET) = 799.00
STREET LENGTH(FEET) = 510.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.025
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.14
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.48
HALFSTREET FLOOD WIDTH(FEET) = 13.24
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.86
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.85
STREET FLOW TRAVEL TIME(MIN.) = 2.20 Tc(MIN.) = 29.29
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 1.799

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.69	0.98	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.69      SUBAREA RUNOFF(CFS) = 1.06  
EFFECTIVE AREA(ACRES) = 6.54      AREA-AVERAGED Fm(INCH/HR) = 0.23  
AREA-AVERAGED Fp(INCH/HR) = 0.98      AREA-AVERAGED Ap = 0.24  
TOTAL AREA(ACRES) = 6.5      PEAK FLOW RATE(CFS) = 9.21

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.48      HALFSTREET FLOOD WIDTH(FEET) = 13.31  
FLOW VELOCITY(FEET/SEC.) = 3.85      DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.85  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 4234.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 799.00      DOWNSTREAM ELEVATION(FEET) = 792.00  
STREET LENGTH(FEET) = 650.00      CURB HEIGHT(INCHES) = 8.0  
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.025  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.85

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.50  
HALFSTREET FLOOD WIDTH(FEET) = 13.92  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.79  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.88  
STREET FLOW TRAVEL TIME(MIN.) = 2.86      Tc(MIN.) = 32.16  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 1.701

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.89	0.98	0.100	32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.89      SUBAREA RUNOFF(CFS) = 1.28  
EFFECTIVE AREA(ACRES) = 7.43      AREA-AVERAGED Fm(INCH/HR) = 0.22  
AREA-AVERAGED Fp(INCH/HR) = 0.98      AREA-AVERAGED Ap = 0.22  
TOTAL AREA(ACRES) = 7.4      PEAK FLOW RATE(CFS) = 9.92

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.50      HALFSTREET FLOOD WIDTH(FEET) = 14.00  
FLOW VELOCITY(FEET/SEC.) = 3.77      DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.88  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 4884.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

```

=====
MAINLINE Tc(MIN.) = 32.16
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 1.701
SUBAREA LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap      SCS
LAND USE                GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"2 DWELLINGS/ACRE"      A        5.29      0.98      0.700    32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700
SUBAREA AREA(ACRES) = 5.29      SUBAREA RUNOFF(CFS) = 4.85
EFFECTIVE AREA(ACRES) = 12.72   AREA-AVERAGED Fm(INCH/HR) = 0.41
AREA-AVERAGED Fp(INCH/HR) = 0.98  AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 12.7      PEAK FLOW RATE(CFS) = 14.77

*****
FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====
*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 694.00
ELEVATION DATA: UPSTREAM(FEET) = 818.00 DOWNSTREAM(FEET) = 810.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 14.644
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.727
SUBAREA Tc AND LOSS RATE DATA(AMC II):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap      SCS  Tc
LAND USE                GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"2 DWELLINGS/ACRE"      A        8.96      0.98      0.700    32  14.64
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700
SUBAREA RUNOFF(CFS) = 16.49
TOTAL AREA(ACRES) = 8.96   PEAK FLOW RATE(CFS) = 16.49

*****
FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 810.00 DOWNSTREAM ELEVATION(FEET) = 803.00
STREET LENGTH(FEET) = 872.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 23.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 28.60

```

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

NOTE: STREET FLOW EXCEEDS TOP OF CURB.

THE FOLLOWING STREET FLOW RESULTS ARE BASED ON THE ASSUMPTION THAT NEGLIBLE FLOW OCCURS OUTSIDE OF THE STREET CHANNEL.

THAT IS, ALL FLOW ALONG THE PARKWAY, ETC., IS NEGLECTED.

STREET FLOW DEPTH(FEET) = 0.52

HALFSTREET FLOOD WIDTH(FEET) = 19.90

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.51

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.84

STREET FLOW TRAVEL TIME(MIN.) = 4.14 Tc(MIN.) = 18.79

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.348

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
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RESIDENTIAL

"2 DWELLINGS/ACRE" A 16.10 0.98 0.700 32

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700

SUBAREA AREA(ACRES) = 16.10 SUBAREA RUNOFF(CFS) = 24.14

EFFECTIVE AREA(ACRES) = 25.06 AREA-AVERAGED Fm(INCH/HR) = 0.68

AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.70

TOTAL AREA(ACRES) = 25.1 PEAK FLOW RATE(CFS) = 37.57

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.57 HALFSTREET FLOOD WIDTH(FEET) = 22.12

FLOW VELOCITY(FEET/SEC.) = 3.75 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.13

\*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,

AND L = 872.0 FT WITH ELEVATION-DROP = 7.0 FT, IS 25.9 CFS,

WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 302.00

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 1566.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 2 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 803.00 DOWNSTREAM ELEVATION(FEET) = 800.00

STREET LENGTH(FEET) = 570.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 23.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 43.29

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

NOTE: STREET FLOW EXCEEDS TOP OF CURB.

THE FOLLOWING STREET FLOW RESULTS ARE BASED ON THE ASSUMPTION THAT NEGLIBLE FLOW OCCURS OUTSIDE OF THE STREET CHANNEL.

THAT IS, ALL FLOW ALONG THE PARKWAY, ETC., IS NEGLECTED.

STREET FLOW DEPTH(FEET) = 0.63

HALFSTREET FLOOD WIDTH(FEET) = 25.35

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.31

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.09

STREET FLOW TRAVEL TIME(MIN.) = 2.87 Tc(MIN.) = 21.66

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.156

SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "2 DWELLINGS/ACRE"	A	8.61	0.98	0.700	32
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700					
SUBAREA AREA(ACRES) =		8.61	SUBAREA RUNOFF(CFS) =		11.42
EFFECTIVE AREA(ACRES) =		33.67	AREA-AVERAGED Fm(INCH/HR) =		0.68
AREA-AVERAGED Fp(INCH/HR) =		0.98	AREA-AVERAGED Ap =		0.70
TOTAL AREA(ACRES) =		33.7	PEAK FLOW RATE(CFS) =		44.65

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.64 HALFSTREET FLOOD WIDTH(FEET) = 25.63  
 FLOW VELOCITY(FEET/SEC.) = 3.34 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.13  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 2136.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 303.00 TO NODE 106.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 793.40 DOWNSTREAM(FEET) = 787.82  
 FLOW LENGTH(FEET) = 673.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.99  
 ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 44.65  
 PIPE TRAVEL TIME(MIN.) = 1.25 Tc(MIN.) = 22.91  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 106.00 = 2809.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	44.65	22.91	2.085	0.98( 0.68)	0.70	33.7	300.00
LONGEST FLOWPATH FROM NODE 300.00 TO NODE 106.00 = 2809.00 FEET.							

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	14.77	32.16	1.701	0.98( 0.41)	0.42	12.7	100.00
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 106.00 = 4884.00 FEET.							

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	58.31	22.91	2.085	0.98( 0.62)	0.64	42.7	300.00
2	47.20	32.16	1.701	0.97( 0.61)	0.62	46.4	100.00
TOTAL AREA(ACRES) = 46.4							

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 58.31 Tc(MIN.) = 22.908  
 EFFECTIVE AREA(ACRES) = 42.73 AREA-AVERAGED Fm(INCH/HR) = 0.62  
 AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.64  
 TOTAL AREA(ACRES) = 46.4

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 106.00 = 4884.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 787.82 DOWNSTREAM(FEET) = 787.15

FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.1 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 10.20

ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 58.31

PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 23.02

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 4954.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 1000.00

ELEVATION DATA: UPSTREAM(FEET) = 822.00 DOWNSTREAM(FEET) = 810.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.669

\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.125

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	1.24	0.98	0.100	32	11.67

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA RUNOFF(CFS) = 3.38

TOTAL AREA(ACRES) = 1.24 PEAK FLOW RATE(CFS) = 3.38

\*\*\*\*\*

FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 810.00 DOWNSTREAM ELEVATION(FEET) = 798.00

STREET LENGTH(FEET) = 1000.00 CURB HEIGHT(INCHES) = 8.0

STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00



INSIDE STREET CROSSFALL(DECIMAL) = 0.025  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.10  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.46  
HALFSTREET FLOOD WIDTH(FEET) = 12.55  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.77  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.74  
STREET FLOW TRAVEL TIME(MIN.) = 4.42 Tc(MIN.) = 16.09  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.577  
SUBAREA LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
COMMERCIAL A 4.21 0.98 0.100 32  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 4.21 SUBAREA RUNOFF(CFS) = 9.40  
EFFECTIVE AREA(ACRES) = 5.45 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 5.4 PEAK FLOW RATE(CFS) = 12.16

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.52 HALFSTREET FLOOD WIDTH(FEET) = 14.83  
FLOW VELOCITY(FEET/SEC.) = 4.15 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.15  
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 2000.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 798.00 DOWNSTREAM ELEVATION(FEET) = 794.00  
STREET LENGTH(FEET) = 550.00 CURB HEIGHT(INCHES) = 8.0  
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.025  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.22  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.57  
HALFSTREET FLOOD WIDTH(FEET) = 16.97  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.50  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.00  
STREET FLOW TRAVEL TIME(MIN.) = 2.62 Tc(MIN.) = 18.71  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.354  
SUBAREA LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
COMMERCIAL A 1.04 0.98 0.100 32  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 1.04 SUBAREA RUNOFF(CFS) = 2.11  
EFFECTIVE AREA(ACRES) = 6.49 AREA-AVERAGED Fm(INCH/HR) = 0.10  
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 6.5 PEAK FLOW RATE(CFS) = 13.18

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.57 HALFSTREET FLOOD WIDTH(FEET) = 16.97  
FLOW VELOCITY(FEET/SEC.) = 3.49 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.00  
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 203.00 = 2550.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 203.00 TO NODE 107.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	13.18	18.71	2.354	0.98( 0.10)	0.10	6.5	200.00

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 107.00 = 2550.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	58.31	23.02	2.079	0.98( 0.62)	0.64	42.7	300.00
2	47.20	32.28	1.697	0.97( 0.61)	0.62	46.4	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 4954.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	69.54	18.71	2.354	0.97( 0.54)	0.56	41.2	200.00
2	69.88	23.02	2.079	0.98( 0.56)	0.57	49.2	300.00
3	56.54	32.28	1.697	0.98( 0.55)	0.56	52.9	100.00

TOTAL AREA(ACRES) = 52.9

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 69.88 Tc(MIN.) = 23.022  
EFFECTIVE AREA(ACRES) = 49.22 AREA-AVERAGED Fm(INCH/HR) = 0.56  
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.57  
TOTAL AREA(ACRES) = 52.9  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 4954.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 787.15 DOWNSTREAM(FEET) = 784.90  
FLOW LENGTH(FEET) = 315.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 42.0 INCH PIPE IS 29.6 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.66  
ESTIMATED PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 69.88  
PIPE TRAVEL TIME(MIN.) = 0.54 Tc(MIN.) = 23.57  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 5269.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 23.57  
\* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.050  
SUBAREA LOSS RATE DATA(AMC II):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
COMMERCIAL A 3.60 0.98 0.100 32  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.98  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 3.60 SUBAREA RUNOFF(CFS) = 6.33  
EFFECTIVE AREA(ACRES) = 52.82 AREA-AVERAGED Fm(INCH/HR) = 0.52  
AREA-AVERAGED Fp(INCH/HR) = 0.98 AREA-AVERAGED Ap = 0.54  
TOTAL AREA(ACRES) = 56.5 PEAK FLOW RATE(CFS) = 72.52

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	72.92	19.25	2.314	0.97( 0.51)	0.52	44.8	200.00
2	72.52	23.57	2.050	0.98( 0.52)	0.54	52.8	300.00
3	59.09	32.85	1.679	0.98( 0.52)	0.53	56.5	100.00

NEW PEAK FLOW DATA ARE:

PEAK FLOW RATE(CFS) = 72.92 Tc(MIN.) = 19.25  
AREA-AVERAGED Fm(INCH/HR) = 0.51 AREA-AVERAGED Fp(INCH/HR) = 0.97  
AREA-AVERAGED Ap = 0.52 EFFECTIVE AREA(ACRES) = 44.82

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 109.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 784.90 DOWNSTREAM(FEET) = 775.00  
FLOW LENGTH(FEET) = 332.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 33.0 INCH PIPE IS 22.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 16.72  
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 72.92  
PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 19.58  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 109.00 = 5601.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 56.5 TC(MIN.) = 19.58  
EFFECTIVE AREA(ACRES) = 44.82 AREA-AVERAGED Fm(INCH/HR) = 0.51  
AREA-AVERAGED Fp(INCH/HR) = 0.97 AREA-AVERAGED Ap = 0.519  
PEAK FLOW RATE(CFS) = 72.92

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	72.92	19.58	2.291	0.97( 0.51)	0.52	44.8	200.00
2	72.52	23.90	2.033	0.98( 0.52)	0.54	52.8	300.00
3	59.09	33.20	1.669	0.98( 0.52)	0.53	56.5	100.00

=====

=====  
END OF RATIONAL METHOD ANALYSIS



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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
(Reference: 1986 SAN BERNARDINO CO. HYDROLOGY CRITERION)  
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Ver. 21.0 Release Date: 06/01/2014 License ID 1202

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* PAMA EAST END AVE PHILADELPHIA ST \*  
\* RATIONAL METHOD 100 YEAR STORM EVENT \*  
\* RYAN KIM HC 08/12/21 \*  
\*\*\*\*\*

FILE NAME: PAMAH\_A.DAT  
TIME/DATE OF STUDY: 10:49 08/12/2021

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--\*TIME-OF-CONCENTRATION MODEL\*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 12.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
\*USER-DEFINED LOGARITHMIC INTERPOLATION USED FOR RAINFALL\*

SLOPE OF INTENSITY DURATION CURVE(LOG(I;IN/HR) vs. LOG(Tc;MIN)) = 0.6000  
USER SPECIFIED 1-HOUR INTENSITY(INCH/HOUR) = 1.5400

\*ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD\*

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	FACTOR (n)
1	41.0	34.0	0.025/0.025/ ---	0.67	2.00	0.0313	0.167	0.0130
2	30.0	23.0	0.020/0.020/ ---	0.50	1.50	0.0313	0.125	0.0130

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.67 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

\*\*\*\*\*

FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 736.00  
ELEVATION DATA: UPSTREAM(FEET) = 840.00 DOWNSTREAM(FEET) = 837.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 12.811

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.889

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
"2 DWELLINGS/ACRE"	A	1.53	0.74	0.700	52	18.46
COMMERCIAL	A	0.60	0.74	0.100	52	12.81

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.531  
SUBAREA RUNOFF(CFS) = 6.70  
TOTAL AREA(ACRES) = 2.13 PEAK FLOW RATE(CFS) = 6.70

\*\*\*\*\*

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 837.00 DOWNSTREAM ELEVATION(FEET) = 822.00

STREET LENGTH(FEET) = 1519.00 CURB HEIGHT(INCHES) = 8.0

STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.025

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.93

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.49

HALFSTREET FLOOD WIDTH(FEET) = 13.62

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.58

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.75

STREET FLOW TRAVEL TIME(MIN.) = 7.08 Tc(MIN.) = 19.89

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.987

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	1.70	0.74	0.100	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100

SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 4.46

EFFECTIVE AREA(ACRES) = 3.83 AREA-AVERAGED Fm(INCH/HR) = 0.25

AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.34

TOTAL AREA(ACRES) = 3.8 PEAK FLOW RATE(CFS) = 9.43

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.50 HALFSTREET FLOOD WIDTH(FEET) = 13.92

FLOW VELOCITY(FEET/SEC.) = 3.62 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.80

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 102.00 = 2255.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 103.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 822.00 DOWNSTREAM ELEVATION(FEET) = 805.00
STREET LENGTH(FEET) = 1469.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.025
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.68
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.52
HALFSTREET FLOOD WIDTH(FEET) = 14.68
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.06
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.09
STREET FLOW TRAVEL TIME(MIN.) = 6.03 Tc(MIN.) = 25.91
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.549

SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
COMMERCIAL A 2.02 0.74 0.100 52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA AREA(ACRES) = 2.02 SUBAREA RUNOFF(CFS) = 4.50
EFFECTIVE AREA(ACRES) = 5.85 AREA-AVERAGED Fm(INCH/HR) = 0.19
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.26
TOTAL AREA(ACRES) = 5.9 PEAK FLOW RATE(CFS) = 12.41

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.52 HALFSTREET FLOOD WIDTH(FEET) = 15.06
FLOW VELOCITY(FEET/SEC.) = 4.12 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.16
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 103.00 = 3724.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====
UPSTREAM ELEVATION(FEET) = 805.00 DOWNSTREAM ELEVATION(FEET) = 799.00
STREET LENGTH(FEET) = 510.00 CURB HEIGHT(INCHES) = 8.0
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.025
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.15
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.53
HALFSTREET FLOOD WIDTH(FEET) = 15.37
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.20
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.24
STREET FLOW TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 27.94
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.436

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.69	0.74	0.100	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.69 SUBAREA RUNOFF(CFS) = 1.47  
EFFECTIVE AREA(ACRES) = 6.54 AREA-AVERAGED Fm(INCH/HR) = 0.18  
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.24  
TOTAL AREA(ACRES) = 6.5 PEAK FLOW RATE(CFS) = 13.29

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.53 HALFSTREET FLOOD WIDTH(FEET) = 15.44  
FLOW VELOCITY(FEET/SEC.) = 4.20 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.25  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 104.00 = 4234.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 799.00 DOWNSTREAM ELEVATION(FEET) = 792.00  
STREET LENGTH(FEET) = 650.00 CURB HEIGHT(INCHES) = 8.0  
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.025  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 14.18  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.55  
HALFSTREET FLOOD WIDTH(FEET) = 16.13  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.13  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.28  
STREET FLOW TRAVEL TIME(MIN.) = 2.62 Tc(MIN.) = 30.56  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.308

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.89	0.74	0.100	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 0.89 SUBAREA RUNOFF(CFS) = 1.79  
EFFECTIVE AREA(ACRES) = 7.43 AREA-AVERAGED Fm(INCH/HR) = 0.17  
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.22  
TOTAL AREA(ACRES) = 7.4 PEAK FLOW RATE(CFS) = 14.33

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.55 HALFSTREET FLOOD WIDTH(FEET) = 16.21  
FLOW VELOCITY(FEET/SEC.) = 4.14 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.29  
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 4884.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<



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=====
MAINLINE Tc(MIN.) = 30.56
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.308
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap        SCS
LAND USE              GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"2 DWELLINGS/ACRE"    A        5.29      0.74      0.700     52
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700
SUBAREA AREA(ACRES) = 5.29      SUBAREA RUNOFF(CFS) = 8.52
EFFECTIVE AREA(ACRES) = 12.72   AREA-AVERAGED Fm(INCH/HR) = 0.31
AREA-AVERAGED Fp(INCH/HR) = 0.74  AREA-AVERAGED Ap = 0.42
TOTAL AREA(ACRES) = 12.7      PEAK FLOW RATE(CFS) = 22.84

*****
FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====
*****
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 694.00
ELEVATION DATA: UPSTREAM(FEET) = 818.00 DOWNSTREAM(FEET) = 810.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 14.644
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.589
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap        SCS  Tc
LAND USE              GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"2 DWELLINGS/ACRE"    A        8.96      0.74      0.700     52  14.64
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700
SUBAREA RUNOFF(CFS) = 24.76
TOTAL AREA(ACRES) = 8.96   PEAK FLOW RATE(CFS) = 24.76

*****
FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 2 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 810.00 DOWNSTREAM ELEVATION(FEET) = 803.00
STREET LENGTH(FEET) = 872.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 23.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 43.73

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STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

NOTE: STREET FLOW EXCEEDS TOP OF CURB.

THE FOLLOWING STREET FLOW RESULTS ARE BASED ON THE ASSUMPTION THAT NEGLIBLE FLOW OCCURS OUTSIDE OF THE STREET CHANNEL.

THAT IS, ALL FLOW ALONG THE PARKWAY, ETC., IS NEGLECTED.

STREET FLOW DEPTH(FEET) = 0.60

HALFSTREET FLOOD WIDTH(FEET) = 23.46

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.89

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.32

STREET FLOW TRAVEL TIME(MIN.) = 3.74 Tc(MIN.) = 18.38

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.132

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
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RESIDENTIAL

"2 DWELLINGS/ACRE" A 16.10 0.74 0.700 52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700

SUBAREA AREA(ACRES) = 16.10 SUBAREA RUNOFF(CFS) = 37.85

EFFECTIVE AREA(ACRES) = 25.06 AREA-AVERAGED Fm(INCH/HR) = 0.52

AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.70

TOTAL AREA(ACRES) = 25.1 PEAK FLOW RATE(CFS) = 58.92

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.65 HALFSTREET FLOOD WIDTH(FEET) = 26.30

FLOW VELOCITY(FEET/SEC.) = 4.19 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.73

\*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,

AND L = 872.0 FT WITH ELEVATION-DROP = 7.0 FT, IS 39.6 CFS,

WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 302.00

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 1566.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 302.00 TO NODE 303.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 2 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 803.00 DOWNSTREAM ELEVATION(FEET) = 800.00

STREET LENGTH(FEET) = 570.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 23.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 68.13

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

NOTE: STREET FLOW EXCEEDS TOP OF CURB.

THE FOLLOWING STREET FLOW RESULTS ARE BASED ON THE ASSUMPTION THAT NEGLIBLE FLOW OCCURS OUTSIDE OF THE STREET CHANNEL.

THAT IS, ALL FLOW ALONG THE PARKWAY, ETC., IS NEGLECTED.

STREET FLOW DEPTH(FEET) = 0.73

HALFSTREET FLOOD WIDTH(FEET) = 30.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.71

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.70

STREET FLOW TRAVEL TIME(MIN.) = 2.56 Tc(MIN.) = 20.94

\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.896

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "2 DWELLINGS/ACRE"	A	8.61	0.74	0.700	52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.700  
 SUBAREA AREA(ACRES) = 8.61 SUBAREA RUNOFF(CFS) = 18.42  
 EFFECTIVE AREA(ACRES) = 33.67 AREA-AVERAGED Fm(INCH/HR) = 0.52  
 AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.70  
 TOTAL AREA(ACRES) = 33.7 PEAK FLOW RATE(CFS) = 72.03

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.74 HALFSTREET FLOOD WIDTH(FEET) = 30.00  
 FLOW VELOCITY(FEET/SEC.) = 3.80 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.81  
 \*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,  
 AND L = 570.0 FT WITH ELEVATION-DROP = 3.0 FT, IS 22.5 CFS,  
 WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 303.00  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 303.00 = 2136.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 303.00 TO NODE 106.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 793.40 DOWNSTREAM(FEET) = 787.82  
 FLOW LENGTH(FEET) = 673.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 39.0 INCH PIPE IS 31.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.07  
 ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 72.03  
 PIPE TRAVEL TIME(MIN.) = 1.11 Tc(MIN.) = 22.05  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 106.00 = 2809.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	72.03	22.05	2.808	0.74( 0.52)	0.70	33.7	300.00

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 106.00 = 2809.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	22.84	30.56	2.308	0.74( 0.31)	0.42	12.7	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 106.00 = 4884.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	92.63	22.05	2.808	0.74( 0.48)	0.64	42.8	300.00
2	79.16	30.56	2.308	0.74( 0.46)	0.62	46.4	100.00

TOTAL AREA(ACRES) = 46.4

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 92.63 Tc(MIN.) = 22.053  
 EFFECTIVE AREA(ACRES) = 42.85 AREA-AVERAGED Fm(INCH/HR) = 0.48  
 AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.64  
 TOTAL AREA(ACRES) = 46.4  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 106.00 = 4884.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 106.00 TO NODE 106.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 106.00 TO NODE 107.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 787.82 DOWNSTREAM(FEET) = 787.15  
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 42.0 INCH PIPE IS 33.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 11.36  
 ESTIMATED PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 92.63  
 PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 22.16  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 4954.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 1000.00  
 ELEVATION DATA: UPSTREAM(FEET) = 822.00 DOWNSTREAM(FEET) = 810.00

Tc = K\*[(LENGTH\*\* 3.00)/(ELEVATION CHANGE)]\*\*0.20  
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.669  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.113  
 SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	A	1.24	0.74	0.100	52	11.67

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA RUNOFF(CFS) = 4.51  
 TOTAL AREA(ACRES) = 1.24 PEAK FLOW RATE(CFS) = 4.51

\*\*\*\*\*

FLOW PROCESS FROM NODE 201.00 TO NODE 202.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 810.00 DOWNSTREAM ELEVATION(FEET) = 798.00

STREET LENGTH(FEET) = 1000.00 CURB HEIGHT(INCHES) = 8.0  
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.025  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.89  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.50  
HALFSTREET FLOOD WIDTH(FEET) = 14.23  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.02  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.03  
STREET FLOW TRAVEL TIME(MIN.) = 4.15 Tc(MIN.) = 15.81  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.428  
SUBAREA LOSS RATE DATA(AMC III):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
COMMERCIAL A 4.21 0.74 0.100 52  
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74  
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
SUBAREA AREA(ACRES) = 4.21 SUBAREA RUNOFF(CFS) = 12.71  
EFFECTIVE AREA(ACRES) = 5.45 AREA-AVERAGED Fm(INCH/HR) = 0.07  
AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.10  
TOTAL AREA(ACRES) = 5.4 PEAK FLOW RATE(CFS) = 16.45

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.57 HALFSTREET FLOOD WIDTH(FEET) = 16.74  
FLOW VELOCITY(FEET/SEC.) = 4.47 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.53  
LONGEST FLOWPATH FROM NODE 200.00 TO NODE 202.00 = 2000.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 798.00 DOWNSTREAM ELEVATION(FEET) = 794.00  
STREET LENGTH(FEET) = 550.00 CURB HEIGHT(INCHES) = 8.0  
STREET HALFWIDTH(FEET) = 41.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 34.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.025  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.025

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0130

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.89  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.63  
HALFSTREET FLOOD WIDTH(FEET) = 19.10  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.77  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.36  
STREET FLOW TRAVEL TIME(MIN.) = 2.43 Tc(MIN.) = 18.24  
\* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.146  
SUBAREA LOSS RATE DATA(AMC III):  
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS

LAND USE                    GROUP    (ACRES)   (INCH/HR)   (DECIMAL)   CN  
 COMMERCIAL                    A            1.04        0.74        0.100       52  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 1.04        SUBAREA RUNOFF(CFS) = 2.88  
 EFFECTIVE AREA(ACRES) = 6.49        AREA-AVERAGED Fm(INCH/HR) = 0.07  
 AREA-AVERAGED Fp(INCH/HR) = 0.74    AREA-AVERAGED Ap = 0.10  
 TOTAL AREA(ACRES) = 6.5            PEAK FLOW RATE(CFS) = 17.94

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.63    HALFSTREET FLOOD WIDTH(FEET) = 19.18  
 FLOW VELOCITY(FEET/SEC.) = 3.76    DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.36  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 203.00 = 2550.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 203.00 TO NODE 107.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	17.94	18.24	3.146	0.74( 0.07)	0.10	6.5	200.00

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 107.00 = 2550.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	92.63	22.16	2.800	0.74( 0.48)	0.64	42.8	300.00
2	79.16	30.66	2.304	0.74( 0.46)	0.62	46.4	100.00

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 4954.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	105.58	18.24	3.146	0.74( 0.41)	0.56	41.8	200.00
2	108.55	22.16	2.800	0.74( 0.42)	0.57	49.3	300.00
3	92.18	30.66	2.304	0.74( 0.42)	0.56	52.9	100.00

TOTAL AREA(ACRES) = 52.9

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 108.55    Tc(MIN.) = 22.156  
 EFFECTIVE AREA(ACRES) = 49.34    AREA-AVERAGED Fm(INCH/HR) = 0.42  
 AREA-AVERAGED Fp(INCH/HR) = 0.74    AREA-AVERAGED Ap = 0.57  
 TOTAL AREA(ACRES) = 52.9  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 107.00 = 4954.00 FEET.

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FLOW PROCESS FROM NODE 107.00 TO NODE 107.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

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FLOW PROCESS FROM NODE 107.00 TO NODE 108.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 787.15    DOWNSTREAM(FEET) = 784.90

FLOW LENGTH(FEET) = 315.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 48.0 INCH PIPE IS 36.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.68  
 ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 108.55  
 PIPE TRAVEL TIME(MIN.) = 0.49 Tc(MIN.) = 22.65  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 108.00 = 5269.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 108.00 TO NODE 108.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 22.65  
 \* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 2.763  
 SUBAREA LOSS RATE DATA(AMC III):  
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS  
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN  
 COMMERCIAL A 3.60 0.74 0.100 52  
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.74  
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100  
 SUBAREA AREA(ACRES) = 3.60 SUBAREA RUNOFF(CFS) = 8.71  
 EFFECTIVE AREA(ACRES) = 52.94 AREA-AVERAGED Fm(INCH/HR) = 0.40  
 AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.54  
 TOTAL AREA(ACRES) = 56.5 PEAK FLOW RATE(CFS) = 112.65

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FLOW PROCESS FROM NODE 108.00 TO NODE 109.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 784.90 DOWNSTREAM(FEET) = 775.00  
 FLOW LENGTH(FEET) = 332.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 39.0 INCH PIPE IS 26.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 18.65  
 ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 112.65  
 PIPE TRAVEL TIME(MIN.) = 0.30 Tc(MIN.) = 22.94  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 109.00 = 5601.00 FEET.

END OF STUDY SUMMARY:  
 TOTAL AREA(ACRES) = 56.5 TC(MIN.) = 22.94  
 EFFECTIVE AREA(ACRES) = 52.94 AREA-AVERAGED Fm(INCH/HR)= 0.40  
 AREA-AVERAGED Fp(INCH/HR) = 0.74 AREA-AVERAGED Ap = 0.537  
 PEAK FLOW RATE(CFS) = 112.65

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	110.66	19.04	3.066	0.74( 0.39)	0.52	45.4	200.00
2	112.65	22.94	2.742	0.74( 0.40)	0.54	52.9	300.00
3	95.95	31.49	2.267	0.74( 0.39)	0.53	56.5	100.00

END OF RATIONAL METHOD ANALYSIS

