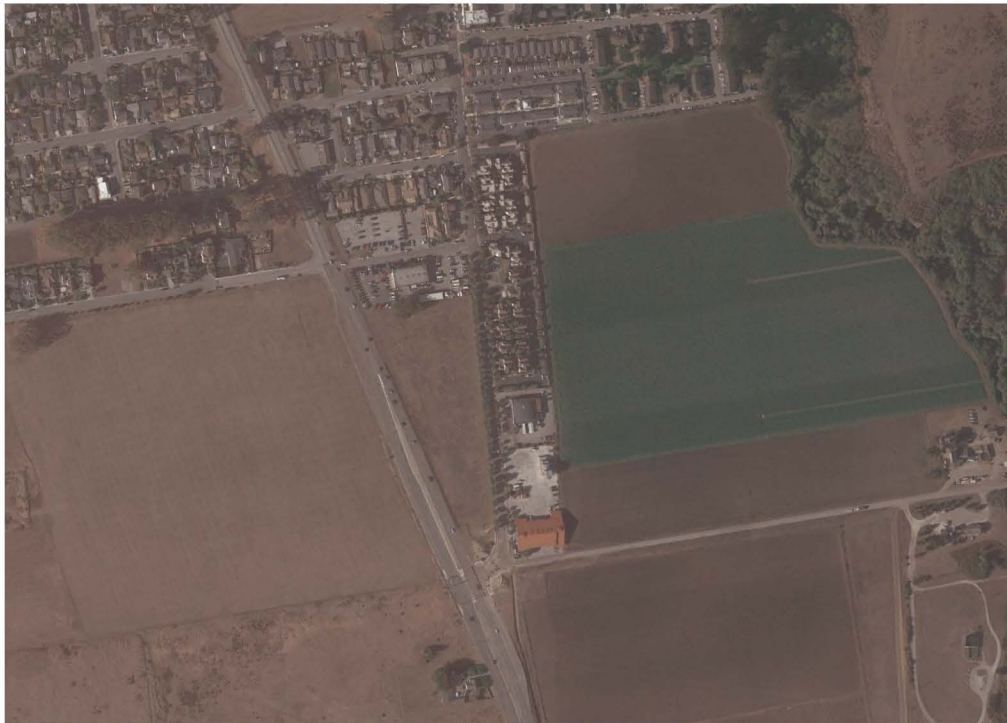


Appendix H: Traffic Impact Study

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Traffic Impact Study for the Hyatt Place Hotel



Prepared for the City of Half Moon Bay

Submitted by
W-Trans

July 13, 2020



**TRAFFIC ENGINEERING
TRANSPORTATION PLANNING**
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Executive Summary

The proposed project is a new 129-room hotel with 148 parking spaces to be located at the northeast corner of the intersection of State Route (SR) 1/South Main Street in Half Moon Bay, California. This project is expected to generate an average of 575 trips per day, including 44 trips during the weekday a.m. peak hour, 46 during the p.m. peak hour and 93 during the weekend midday peak hour.

This analysis addresses the potential impacts at eight study intersections. All study intersections are expected to continue operating acceptably under all conditions with and without the project, except for the signalized intersection at SR-1/North Main Street and the unsignalized intersection at SR-1/Seymour Street. The project's contribution to these intersections would not be considered an adverse impact.

The anticipated amount of vehicle traffic passing through the unsignalized intersection of SR-1/Seymour Street during the weekend peak hour under the Background plus Project and Cumulative Conditions would be insufficient to satisfy the peak hour volume warrant indicating potential need for a traffic signal, either with or without the proposed project.

Ten roadway segments along State Routes 1 and 92 within the study area were evaluated and determined to operate at acceptable levels of service, with or without the project, under all volumes evaluated.

The proposed project would have a less-than-significant transportation impact on vehicle miles traveled with the implementation of the recommended Transportation Demand Management Plan.

Pedestrian and bicycle facility connectivity would be improved by the project through provision of sidewalks along the street frontages, a Class II bike lane connecting South Main Street and Seymore Street, secure parking for 30 bikes, and a fleet of bikes owned by the hotel for their guests to use.

The sight distance at the project driveways along South Main Street were evaluated and deemed to be adequate since they are greater than the recommended minimum distance according to Caltrans *Highway Design Manual*. It is recommended that on-street parking be restricted for 15 feet on either side of the proposed project driveways on South Main Street and vegetation be trimmed to maintain adequate sight distance.

The proposed exit only driveway on Seymour Street would have inadequate sight lines between the driveway and SR-1. This is considered a significant safety impact. To improve the site access and reduce the project safety impact to a less-than-significant level, it is recommended that the driveway be eliminated, or a gate installed at the exit only driveway on Seymour Street and the driveway converted to an emergency vehicle access (EVA) drive only. An additional driveway access point on South Main Street could be accommodated if desired.

The proposed parking supply of 148 spaces exceeds both the City of Half Moon Bay parking requirements and the estimated demand based on standard rates published by the Institute of Transportation Engineers *Parking Generation Manual*.

Introduction

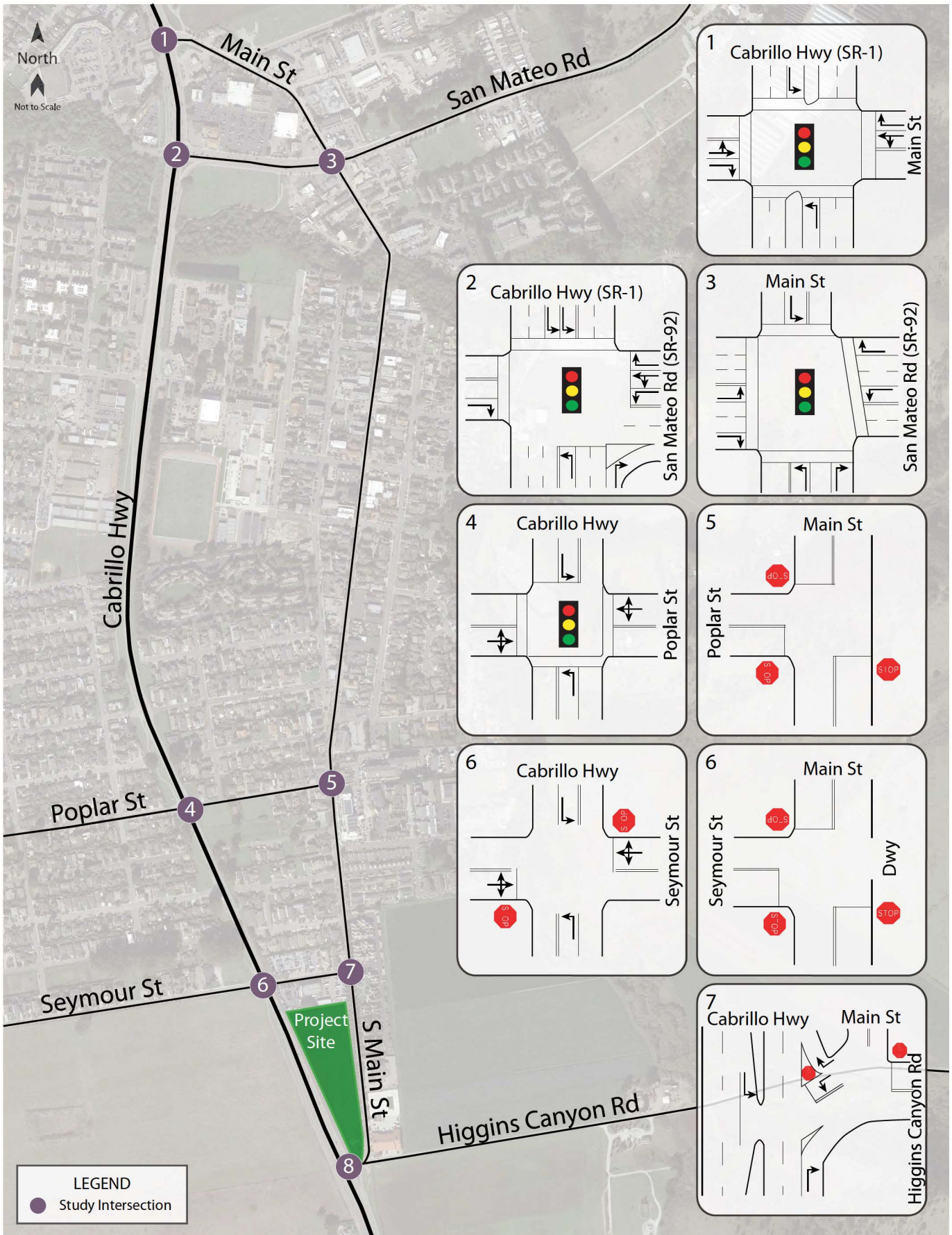
This report presents an analysis of the potential traffic impacts that would be associated with the proposed Hyatt Hotel project to be located at the northeast corner of State Route 1 and South Main Street in the City of Half Moon Bay. The traffic study was completed in accordance with the criteria established by the City of Half Moon Bay and County of San Mateo and is consistent with standard traffic engineering techniques.

Prelude

The purpose of a traffic impact study is to provide City staff and policy makers with data that they can use to make an informed decision regarding the potential traffic impacts of a proposed project, and any associated improvements that would be required in order to mitigate these impacts to a level of insignificance as defined by the City's General Plan or other policies. Vehicular traffic impacts are typically evaluated by determining the number of new trips that the proposed use would be expected to generate, distributing these trips to the surrounding street system based on existing travel patterns or anticipated travel patterns specific to the proposed project, then analyzing the impact the new traffic would be expected to have on critical intersections or roadway segments. Impacts relative to access for pedestrians, bicyclists, and to transit are also addressed.

Project Profile

The proposed project consists of construction a 129-room hotel on a vacant and undeveloped parcel. The project is located within the triangular area bounded by State Route 1, South Main Street and Seymour Street, as shown in Figure 1. The site plan is shown in Figure 2.



Traffic Impact Study for the Hyatt Place Hotel
Figure 1 – Study Area and Lane Configurations



Traffic Impact Study for the Hyatt Place Hotel Figure 2 – Site Plan



Transportation Setting

Operational Analysis

Study Area and Periods

A list of study intersections is provided below along with an indication as to whether the facility is included in the San Mateo County Congestion Management Program (CMP) network or not:

Intersections

1. State Route 1/North Main Street
2. State Route 1/State Route 92 (CMP)
3. Main Street/State Route 92 (CMP)
4. State Route 1/Poplar Street
5. Main Street/Poplar Street
6. State Route 1/Seymour Street
7. Main Street/Seymour Street
8. State Route 1/South Main Street

Roadway Segments:

1. State Route 1 from Linda Mar Boulevard to Frenchmans Creek Road (CMP)
2. State Route 1 from Frenchmans Creek Road to Miramontes Road (CMP)
3. State Route 92 from State Route 1 to I-280 (CMP)

Operating conditions during the weekday a.m. (7:00 – 9:00 a.m.), p.m. (4:00 – 6:00 p.m.) and Saturday midday (12:00 p.m. – 2:00 p.m.) peak periods were evaluated to capture the highest potential impacts for the proposed project as well as the highest volumes on the local transportation network. The morning peak (a.m. peak) hour reflects conditions during the home to work commute as well as the school morning drop-off period; the evening peak (p.m. peak) hour typically reflects the highest level of congestion during the homeward bound commute; and the Saturday midday peak represents the period of highest volumes occurring on a weekend attributable to recreational or leisure trips. Intersection counts are included in Appendix A. Conditions during the a.m., p.m. and Saturday midday peak hours were evaluated for the following scenarios:

1. **Existing Conditions.** Existing peak hour volume, lane geometry, and traffic control (e.g., signal timing, signal phasing, etc.)
2. **Existing plus Project Conditions.** Existing peak hour volumes plus net-new Project-generated trips estimated for the proposed hotel.
3. **Background Conditions.** (Existing + Near-Term Growth). Existing plus five years of traffic growth based on an interpolation between the base model and cumulative year model run using the growth projections from the Local Coastal Land Use Plan Update.
4. **Background plus Project Conditions.** (Existing + Near-Term Growth + Project). Background Condition volumes plus net-new Project-generated trips estimated for the proposed hotel.
5. **Cumulative Conditions.** Existing peak hour volumes plus anticipated forecasted growth for the year 2040 derived from the Local Coastal Land Use Plan Update.

6. **Cumulative plus Project Conditions.** Cumulative Year Condition volumes plus net-new Project-generated trips estimated for the proposed hotel.

Study Intersections

State Route 1 (SR-1)/North Main Street is a signalized intersection with protected left-turn phasing on all four approaches. Marked crosswalks and pedestrian signals are provided at each leg. This intersection is operated by the California Department of Transportation (Caltrans).

State Route 1 (SR-1)/State Route 92 (SR-92) is a signalized, four-legged intersection with protected left-turn phasing on all approaches. The intersection has a channelized right-turn lane on the south leg. Marked crosswalks and pedestrian signals are provided across the north and west legs only. This intersection is part of the County of San Mateo Congestion Management Program and is operated by Caltrans.

Main Street/State Route 92 (SR-92) is a signalized, four-legged intersection with protected left-turn phasing on all approaches. Marked crosswalks and pedestrian signals are provided across every approach. This intersection is part of the County of San Mateo Congestion Management Program and is operated by Caltrans.

State Route 1 (SR-1)/Poplar Street is a signalized, four-legged intersection with protected left-turn phasing on the northbound and southbound approaches and permissive left-turns for the Poplar Street approaches. Marked crosswalks and pedestrian signals are provided across the west, east and south legs only. This intersection is operated by the Caltrans.

Main Street/Poplar Street is an unsignalized all-way stop-controlled tee-intersection. Marked crosswalks are provided on the north and west legs.

State Route 1 (SR-1)/Seymour Street is a four-legged unsignalized side-street stop-controlled intersection. Marked crosswalks are not provided on any approach. This intersection is operated by the Caltrans.

Main Street/Seymour Street is an unsignalized all-way stop-controlled tee-intersection. Marked crosswalks are not provided on any approach.

State Route 1 (SR-1)/South Main Street/Higgins Canyon Road is an unsignalized, three-legged intersection. Marked crosswalks are not provided on any approach. This intersection is operated by the Caltrans.

The locations of the study intersections and the existing lane configurations and controls are shown in Figure 1.

Study Roadways

State Route 1 (SR-1) is a major north-south state highway that runs along most of the Pacific coastline of California. Through the project study area there are median left-turn lanes and one lane each for both the northbound and southbound directions. This portion of SR-1 is also known as the Cabrillo Highway. SR-1 facilitates major regional travel along California's coastline. The posted speed limit for SR-1 is 50 miles per hour (mph).

State Route 92 (SR-92) is a major east-west state highway that serves regional traffic between SR-1, I-280, the San Mateo Bridge and the City of Hayward. Within the study area, there is raised median with one or two through lanes in each direction.

Main Street is a north-south arterial roadway that primarily serves local City of Half Moon Bay traffic. This street has one travel lane in each direction with on-street parking. Adjacent land uses are mainly agricultural, public

facilities, commercial and residential. Main Street traverses the historic Main Street shopping district of Half Moon Bay. The posted speed limit is 25 mph.

Poplar Street is an east-west local street that provides access to the beach as well as local access for the residential areas surrounding SR-1 and Main Street. Poplar Street has one lane in each direction with residential land uses along both the north and south sides. The posted speed limit is 25 mph.

Seymour Street is an east-west local street that provides local access for the residential areas surrounding SR-1 and Main Street. Seymour Street has one lane in each direction. West of SR-1, Seymour Street has single family homes along the north side only. East of SR-1, the adjacent land uses are comprised mostly of commercial land uses. The posted speed limit is 25 mph.

Alternative Modes

Pedestrian Facilities

Pedestrian facilities in the study area include sidewalks, crosswalks, pedestrian signal phases, curb ramps, curb extensions, and various streetscape amenities such as lighting, benches, etc. In general, a network of sidewalks, crosswalks, pedestrian signals, and curb ramps provide access for pedestrians in the project vicinity, primarily along Main Street.

- **State Route 1 (SR-1)** – Pedestrian crosswalks are provided at the signalized intersections of SR-1 with SR-92, Kelly Avenue and Poplar Street. Sidewalks are not provided anywhere along SR-1 except at the intersections with SR-92 and Kelly Avenue. The intersection with Poplar Street has crosswalks but does not provide any conventional pedestrian amenities such as sidewalks or curb ramps.
- **State Route 92 (SR-92)** – Continuous sidewalk is provided along the north side of SR-92 between Main Street and SR-1, and along the south side of SR-92 for approximately 330 feet west of Main Street. Crosswalks are provided at the signalized intersections at SR-1 and Main Street.
- **Main Street** – Sidewalks are provided along both sides of Main Street with curb ramps and overhead lighting at intersections between SR-92 and Higgins Canyon Road. Crosswalks are also provided at the Main Street intersections with SR-92, Stone Pine Road, Mill Street, Kelly Street, Miramontes Street, and Correas Street. Between SR-1 and Seymour Street sidewalks are non-existent on the west side of Main Street, except for a 170-foot portion adjacent to the James Ford dealership parking lot.
- **Poplar Street** – Sidewalks are not provided along Poplar Street between SR-1 and Main Street. Pedestrians who wish to walk on Poplar Street either use the roadside shoulder or walk within the vehicle travel way.
- **Seymour Street** – Sidewalks are not provided along Seymour Street between SR-1 and Main Street. Pedestrians who wish to walk on Seymour Street either use the roadside shoulder or walk within the vehicle travel way.

Bicycle Facilities

The *Highway Design Manual*, California Department of Transportation (Caltrans), 2016, classifies bikeways into four categories:

- **Class I Multi-Use Path** – a completely separated right-of-way for the exclusive use of bicycles and pedestrians with cross flows of motorized traffic minimized.
- **Class II Bike Lane** – a striped and signed lane for one-way bike travel on a street or highway.
- **Class III Bike Route** – signing only for shared use with motor vehicles within the same travel lane on a street or highway.

- **Class IV Bikeway** – also known as a separated bikeway, a Class IV Bikeway is for the exclusive use of bicycles and includes a separation between the bikeway and the motor vehicle traffic lane. The separation may include, but is not limited to, grade separation, flexible posts, inflexible physical barriers, or on-street parking.

In the project area, bike facilities are provided as presented in Table 1, which shows a brief summary of the existing and planned bicycle facilities in the project vicinity, as contained in the *City of Half Moon Bay Bicycle & Pedestrian Master Plan, 2019*.

Status Facility	Class	Length (miles)	Begin Point	End Point
Existing				
California (Half Moon Bay) Coastal Trail	I	4.7	Seymour Bridge	Pillar Point Harbour Blvd
Naomi Patridge Trail	I	2.0	Purisima Way	Oak Ave
Pilarcitos Creek Trail	I	0.4	Oak Ave Park	State Route 92
State Route 1	I	1.2	Kelly Ave	Wavecrest Ave
Kelly Avenue Bike Lane	II	0.6	Balboa Blvd	State Route 1
Main Street Bike Lane	II	0.3	State Route 1	State Route 92
Miramontes Point Road Bike Lane	II	0.6	Coastal Trail	State Route 1
Kelly Avenue	III	0.3	State Route 1	Main St
Main Street	III	1.2	State Route 92	Higgins Canyon Rd
Mirada Road	III	0.3	Magellan Ave	Mirada Rd
Pilarcitos Avenue	III	0.3	Kelly Ave	Oak Ave
Planned				
State Route 1	I	6.0	Montara State Beach	Purisima Way
State Route 1	I	1.6	Wavecrest Rd	Dehoff Canyon Rd
State Route 92	I	1.0	Main Street	Eastern City Limit
Higgins Canyon Road	III	14.0	S. Main St	Purisima Creek Rd

Source: *City of Half Moon Bay Bicycle & Pedestrian Master Plan, Alta Planning & Design, 2019*

Transit Facilities

SamTrans provides multiple fixed route bus service in the City of Half Moon Bay. Routes 17 and 294 operates daily and Route 18 operates only on school days. All three routes have stops in Half Moon Bay primarily along SR-1 and Main Street.

Route 17 operates daily between Linda Mar Park & Ride in Pacifica and Miramontes Point Road along SR-1 in Half Moon Bay, with limited service to the town of Pescadero. Service is provided from 5:30 a.m. to 9:00 p.m. on weekdays and 5:00 a.m. to 8:00 p.m. on weekends. On weekdays, headways are around 1 hour, and on weekends, approximately 2 hours.

Route 18 operates on school days only and provides service between the town of Montara and the Moonridge Apartments in Half Moon Bay via SR-1 and Main Street. During the mornings, the northbound service departs

from the Moonridge Apartments at 7:27 a.m. and 8:22 a.m. while the southbound service departs from Montara at 7:09 a.m., 7:39 a.m., 8:04 a.m. and 8:43 a.m. In the afternoons, the northbound service departs at 3:48 p.m. and 4:19 p.m. while the southbound service departs at 3:28 p.m. and 3:58 p.m.

Route 294 operates daily from approximately 5:00 a.m. to 9:00 p.m. with headways ranging from 1 to 2 hours. Route 294 connects Half Moon Bay with the San Mateo Medical Center with stops along Main Street and SR-92.

Two bicycles can be carried on most SamTrans buses. Bike rack space is on a first come, first served basis. Additional bicycles are allowed on SamTrans buses at the discretion of the driver.

SamTrans also provides a door-to-door service for those who are unable to independently use the transit system due to a physical or mental disability. The SamTrans Paratransit service is designed to serve the needs of individuals with disabilities within San Mateo County.

On-Demand Transportation Services

On-demand private taxi services are available in Half Moon Bay 24 hours a day. Taxis can be used for trips within the local Planning Area and farther destinations, including nearby airports. Other ride-hailing applications are also available in Half Moon Bay and provide transportation throughout the Bay Area.

Capacity Analysis

Intersection Level of Service Methodologies

Level of Service (LOS) is used to rank traffic operation on various types of facilities based on traffic volumes and roadway capacity using a series of letter designations ranging from A to F. Generally, Level of Service A represents free flow conditions and Level of Service F represents forced flow or breakdown conditions. A unit of measure that indicates a level of delay generally accompanies the LOS designation.

In accordance with the City of Half Moon Bay evaluation standards the study intersections were analyzed using methodologies published in the *Highway Capacity Manual (HCM)*, Transportation Research Board, 2000 using the Synchro analysis software. This source contains methodologies for various types of intersection control, all of which are related to a measurement of delay in average number of seconds per vehicle.

The Levels of Service for the intersections with side-street stop controls, or those which are unsignalized and have one or two approaches stop controlled, were analyzed using the “Two-Way Stop-Controlled” intersection capacity method from the HCM. This methodology determines a level of service for each minor turning movement by estimating the level of average delay in seconds per vehicle. Results are presented for individual movements together with the weighted overall average delay for the intersection.

The study intersections with stop signs on all approaches were analyzed using the “All-Way Stop-Controlled” Intersection methodology from the HCM. This methodology evaluates delay for each approach based on turning movements, opposing and conflicting traffic volumes, and the number of lanes. Average vehicle delay is computed for the intersection as a whole and then related to a Level of Service.

The study intersections that are currently controlled by a traffic signal, or may be in the future, were evaluated using the signalized methodology from the HCM. This methodology is based on factors including traffic volumes, green time for each movement, phasing, whether or not the signals are coordinated, truck traffic, and pedestrian activity. Average stopped delay per vehicle in seconds is used as the basis for evaluation in this LOS methodology. For purposes of this study, delays were calculated using signal timing provided by the City of Half Moon Bay Staff.

The ranges of delay associated with the various levels of service are indicated in Table 2.

Table 2 – Intersection Level of Service Criteria

LOS	Two-Way Stop-Controlled	All-Way Stop-Controlled	Signalized
A	Delay of 0 to 10 seconds. Gaps in traffic are readily available for drivers exiting the minor street.	Delay of 0 to 10 seconds. Upon stopping, drivers are immediately able to proceed.	Delay of 0 to 10 seconds. Most vehicles arrive during the green phase, so do not stop at all.
B	Delay of 10 to 15 seconds. Gaps in traffic are somewhat less readily available than with LOS A, but no queuing occurs on the minor street.	Delay of 10 to 15 seconds. Drivers may wait for one or two vehicles to clear the intersection before proceeding from a stop.	Delay of 10 to 20 seconds. More vehicles stop than with LOS A, but many drivers still do not have to stop.
C	Delay of 15 to 25 seconds. Acceptable gaps in traffic are less frequent, and drivers may approach while another vehicle is already waiting to exit the side street.	Delay of 15 to 25 seconds. Drivers will enter a queue of one or two vehicles on the same approach and wait for vehicle to clear from one or more approaches prior to entering the intersection.	Delay of 20 to 35 seconds. The number of vehicles stopping is significant, although many still pass through without stopping.
D	Delay of 25 to 35 seconds. There are fewer acceptable gaps in traffic, and drivers may enter a queue of one or two vehicles on the side street.	Delay of 25 to 35 seconds. Queues of more than two vehicles are encountered on one or more approaches.	Delay of 35 to 55 seconds. The influence of congestion is noticeable, and most vehicles have to stop.
E	Delay of 35 to 50 seconds. Few acceptable gaps in traffic are available, and longer queues may form on the side street.	Delay of 35 to 50 seconds. Longer queues are encountered on more than one approach to the intersection.	Delay of 55 to 80 seconds. Most, if not all, vehicles must stop and drivers consider the delay excessive.
F	Delay of more than 50 seconds. Drivers may wait for long periods before there is an acceptable gap in traffic for exiting the side streets, creating long queues.	Delay of more than 50 seconds. Drivers enter long queues on all approaches.	Delay of more than 80 seconds. Vehicles may wait through more than one cycle to clear the intersection.

Reference: *Highway Capacity Manual*, Transportation Research Board, 2000

Roadway Segment Analysis

Freeway operations were evaluated using methods adopted by the City/County Association of Governments of San Mateo County (C/CAG) which uses the 2000 HCM volume-to-capacity (V/C) ratio methodology. For two-lane highways, the selected methodology, based on V/C ratios, accounts for the volume in both directions. The total volume is divided by the total bi-directional capacity of 2,800 vehicles per hour to establish the v/c ratio. The LOS criteria for multilane highways are based on calculating V/C ratios for each direction of travel. The capacity is estimated as the number of lanes multiplied by 2,200 vehicles per lane per hour. SR-92 between Main Street and I-280 is considered a two-lane highway with an 80 percent No-Passing Zone. The free-flow speed for SR-1 is 50 mph. The level of service descriptions and the maximum volume-to-capacity ratios for two-Lane and multilane highways are presented in Table 3.

Table 3 – Roadway Level of Service Criteria

LOS	Description	Two Lane Highways (for Rolling Terrain with 80% No-Passing Zone)	Multilane Highways (for 50 mph Free-Flow Speed)
A	Free flow operations with average operating speeds at, or above, the speed limit. Vehicles are unimpeded in their ability to maneuver.	0.04	0.30
B	Free flow operations with average operating speeds at the speed limit. Ability to maneuver is slightly restricted. Minor incidents cause some local deterioration in operations.	0.15	0.50
C	Stable operations with average operating speeds near the speed limit. Freedom to maneuver is noticeably restricted. Minor incidents cause substantial local deterioration in service.	0.30	0.70
D	Speeds begin to decline slightly with increasing flows. Freedom to maneuver is more noticeably restricted. Minor incidents create queuing.	0.46	0.84
E	Operations at capacity. Vehicle spacing causes little room to maneuver but speeds exceed 50 miles per hour (mph). Any disruption to the traffic stream can cause a wave of delay that propagates throughout the upstream traffic flow. Minor incidents cause serious breakdown of service with extensive queuing. Maneuverability is extremely limited.	0.90	1.00
F	Operations with breakdowns in vehicle flow. Volumes exceed capacity causing bottlenecks and queue formation.	Greater than 0.90	Greater than 1.00

Reference: C/CAG Congestion Management Plan, 2017

Regulatory Context

This section describes federal, State, regional, and local environmental laws and policies that are relevant to the California Environmental Quality Act (CEQA) review process for transportation and circulation. These policies provide a context for the impact discussion related to the proposed Plan’s consistency with the applicable regulatory conditions.

Federal Regulations

Americans with Disabilities Act

The Americans with Disabilities Act (ADA) of 1990 provides comprehensive rights and protections to individuals with disabilities. The goal of the ADA is to assure equality of opportunity, full participation, independent living, and economic self-sufficiency for people with disabilities. To implement this goal, the US Access Board, an independent Federal agency created in 1973 to ensure accessibility for people with disabilities, has created accessibility guidelines for public rights-of-way. While these guidelines have not been formally adopted, they have been widely followed by jurisdictions and agencies nationwide in the last decade. These guidelines, last revised in July 2011, address various issues, including roadway design practices, slope and terrain issues, and

pedestrian access to streets, sidewalks, curb ramps, street furnishings, pedestrian signals, parking, public transit, and other components of public rights-of-way. These guidelines would apply to proposed roadways in the study area.

State Regulations

California Department of Transportation

The California Department of Transportation (Caltrans) is the primary State agency responsible for transportation issues. One of its duties is the construction and maintenance of the State highway system. Caltrans approves the planning, design, and construction of improvements for all State-controlled facilities including State Route (SR) 1, SR-92, and the associated interchanges for these facilities in the study area. Caltrans has established standards for roadway traffic flow and developed procedures to determine if State-controlled facilities require improvements. For projects that may physically affect facilities under its administration, Caltrans requires encroachment permits before any construction work may be undertaken. For projects that would not physically affect facilities but may influence traffic flow and levels of service at such facilities, Caltrans may recommend measures to mitigate the traffic impacts of such projects.

The following Caltrans procedures and directives are relevant to the proposed Plan, particularly to State roadway facilities:

- **Level of Service Target.** Caltrans maintains a minimum level of service (LOS) at the transition between LOS C and LOS D for all its facilities. Where an existing facility is operating at less than the LOS C/D threshold, the existing measure of effectiveness should be maintained.
- **Caltrans Project Development Procedures Manual.** This manual outlines pertinent statutory requirements, planning policies, and implementing procedures regarding transportation facilities. It is continually and incrementally updated to reflect changes in policy and procedures. For example, the most recent revision incorporates the Complete Streets policy from Deputy Directive 64-R1, which is detailed below.
- **Caltrans Deputy Directive 64.** This directive requires Caltrans to consider the needs of non-motorized travelers, including pedestrians, bicyclists, and persons with disabilities, in all programming, planning, maintenance, construction, operations, and project development activities and products. This includes incorporation of the best available standards in all of Caltrans' practices.
- **Caltrans Deputy Directive 64-RI.** This directive requires Caltrans to provide for the needs of travelers of all ages and abilities in all planning, programming, design, construction, operations, and maintenance activities and products on the State highway system. Caltrans supports bicycle, pedestrian, and transit travel with a focus on "complete streets" that begins early in system planning and continues through project construction and maintenance and operations.
- **Caltrans Director's Policy 22.** This policy establishes support for balancing transportation needs with community goals. Caltrans seeks to involve and integrate community goals in the planning, design, construction, and maintenance and operations processes, including accommodating the needs of bicyclists and pedestrians.

California Senate Bill 743

Senate Bill (SB) 743 (Steinberg 2013) adds Public Resources Code Section 21099 to CEQA and changes the way that transportation impacts are analyzed under CEQA to better align local environmental review with statewide objectives to reduce greenhouse gas (GHG) emissions, encourage infill mixed-use development in designated priority development areas, reduce regional sprawl development, and reduce vehicle miles traveled (VMT) in California. SB 743 supports and complements the following:

- Assembly Bill 32 (AB 32), which requires statewide greenhouse gas reductions to 1990 levels by 2020, and continued reductions beyond 2020.

- SB 375 and California Air Resources Board established greenhouse gas reduction targets for metropolitan planning organizations to achieve in Regional Transportation Plans and Sustainable Community Strategies. Targets for the largest metropolitan planning organizations range from 13 percent to 16 percent reduction by 2035.
- SB 391 requires the California Transportation Plan to support an 80 percent reduction in GHGs below 1990 levels by 2050.
- Executive Order B-30-15, which sets a GHG emissions reduction target of 40 percent below 1990 levels by 2030, Executive Order S-3-05, which sets a GHG emissions reduction target of 80 percent below 1990 levels by 2050, and Executive Order B-16-12, which specifies a GHG emissions reduction target of 80 percent below 1990 levels by 2050 specifically for transportation.

In January 2019, the Natural Resources Agency finalized updates to the CEQA Guidelines including the incorporation of SB 743 modifications. These provisions will be effective beginning on July 1, 2020 and shall be applied to all qualifying development projects statewide. Additionally, the California Governor's Office of Planning and Research (OPR) in the publication *Transportation Impacts (SB 743) CEQA Guidelines Update and Technical Advisory*, 2018, provides guidance recommended criteria to evaluate Vehicle Miles Traveled.

Regional Regulations

Metropolitan Transportation Commission

The Metropolitan Transportation Commission (MTC) is the transportation planning, coordinating, and financing agency for the nine-county Bay Area, including San Mateo County. It also functions as the federally-mandated metropolitan planning organization (MPO) for the region. It is responsible for regularly updating the Regional Transportation Plan (RTP), a comprehensive blueprint for the development of mass transit, highway, airport, seaport, railroad, bicycle, and pedestrian facilities.

City/County Association of Governments of San Mateo County (C/CAG)

The City/County Association of Governments of San Mateo County (C/CAG) is a regional planning agency involved with various public services, including transportation. In this role, the CMA makes decisions on what local projects can utilize federal and State funding. The CMA prepares, adopts and updates the County's CMP, last updated in January 2018.

Bay Area Air Quality Management District

The Bay Area Air Quality Management District (BAAQMD) is the public agency tasked with regulating air pollution in the nine-county Bay Area, including San Mateo County. As a primary source of air pollution in the Bay Area region is from motor vehicles, air district regulations affect transportation planning in the Project Study Area. The BAAQMD's goals include reducing health disparities due to air pollution, achieving and maintaining air quality standards, and implementing exemplary regulatory programs and compliance with federal, State, and regional regulations.

Metropolitan Transportation Commission

The Metropolitan Transportation Commission (MTC) is the transportation planning, coordinating, and financing agency for the nine-county San Francisco Bay Area. The MTC functions as both the State-mandated regional transportation planning agency and the federally-mandated metropolitan planning organization (MPO) for the region. As such, it is responsible for regularly updating the Regional Transportation Plan, a comprehensive blueprint for the development of transportation facilities within the region. The Commission also screens requests from local agencies for State and federal grants for transportation projects to determine their compatibility with the Plan.

Local Regulations

Half Moon Bay General Plan

The City of Half Moon Bay's General Plan Circulation Element (adopted November 2013) provides a framework for development within the City. Policies and strategies that are pertinent to the transportation analysis for the proposed project are summarized below:

Policy 2-1: Provide acceptable Levels of Service by improving the road network and incorporating adopted traffic improvements. The City will support Level-of-Service (LOS) C as the desired Level-of-Service on Highway 1 and SR-92, except during the peak commuting and recreational periods when LOS E will be considered the minimum acceptable standard.

Policy 2-2: To the maximum extent practicable, limit future access along Highway 1 and SR-92 to signalized intersections located in accordance with adopted traffic improvements exercising flexibility to reflect changes in conditions and mobility needs over time. Access to existing properties will be modified and consolidated at these designated locations when possible. Additional signalization of the existing intersections along Highway 1 will be considered if warranted and necessary to provide safe and convenient access to and egress from established residential neighborhoods and commercial districts.

Policy 3-2: Promote the development of projects that incorporate all modes of transportation, accommodate all mode users and facilitate balanced mode share use within the context of the community and the roadway facility purpose.

Policy 4-2: Maximize pedestrian and bicycle safety, accessibility, connectivity, and education throughout Half Moon Bay to create neighborhoods where people choose to walk or ride between nearby destinations.

Policy 4-6: Require new developments to dedicate land as necessary to accommodate pedestrian infrastructure, including sidewalks as required by the adopted City Roadway Cross Sections.

Policy 4-8: Encourage pedestrian links between existing and future residential and commercial development.

Policy 7-1: Explore and support TDM programs that reduce the reliance of Half Moon Bay residents and visitors on use of the private automobile.

Traffic Operation Standards

Signalized Intersections

The City of Half Moon Bay has established criteria to determine the level of significance of traffic impacts based on standards set by the City's *General Plan Circulation Element*, *County of San Mateo Traffic Impact Study Requirements (2013)*, and the *San Mateo County Congestion Management Program (CMP), Appendix L: Traffic Impact Analysis Policy*.

For intersections in the CMP network, a project is considered to have an adverse impact if it causes one or more of the following:

1. For a CMP Intersection currently in compliance with the adopted LOS standard:
 - a. A project will be considered to have an adverse impact if the project will cause the CMP intersection to operate at a level of service that violates the standard adopted in the current Congestion Management Program (CMP).
 - b. A project will be considered to have an adverse impact if the cumulative analysis indicates that the combination of the proposed project and future cumulative traffic demand will result in the CMP

intersection to operate at a level of service that violates the standard adopted in the current Congestion Management Program (CMP) *and* the proposed project increases the average control delay at the intersection by four seconds or more.

- c. For a CMP Intersection currently not in compliance with the adopted LOS standard, a project is considered to have an adverse impact if the project will add any additional traffic to the CMP intersection that is currently not in compliance with its adopted level of service standard as established in the CMP.

The City's policy has established that LOS C is the desired level of service on SR-1 and SR-92, except during the peak two-hour commuting period and the peak recreational hour when LOS E is considered the minimum acceptable standard.

For local intersections, not on the CMP network, a traffic impact is considered to be adverse if the addition of project-generated traffic causes operation of an intersection along either SR-1 or SR-92 to deteriorate from an acceptable level of service (LOS E or better) to LOS F or increases the average control delay at the intersection by four seconds or more if the intersection was operating at LOS F without project-generated traffic added.

Unsignalized Intersections

The City of Half Moon Bay does not have a formally adopted minimum threshold for unsignalized intersections. For the purposes of this report, a traffic impact is considered to be adverse if all three of these conditions are met at an unsignalized intersection:

1. The addition of project-generated traffic causes operation of an unsignalized intersection to deteriorate from an acceptable level of service (LOS E or better) to LOS F;
2. The peak hour traffic warrant as defined in the *California Manual on Uniform Traffic Control Devices (CA-MUTCD)*, is satisfied; and
3. The project-generated traffic adds a minimum of ten vehicles to the critical movement (typically side street turning movements or mainline turning movements).

Roadway Segments

For freeway segments currently in compliance with the adopted LOS standard:

1. A project is considered to have an adverse impact if the project will cause the freeway segment to operate at a level of service that violates the standard adopted in the current Congestion Management Program (CMP).
2. A project will be considered to have an adverse impact if the cumulative analysis indicates that the combination of the proposed project and future cumulative traffic demand will result in the freeway segment to operate at a level of service that violates the standard adopted in the current Congestion Management Program (CMP) *and* the proposed project increases traffic demand on the freeway segment by an amount equal to one percent or more of the segment capacity, or causes the freeway segment volume-to-capacity (v/c) ratio to increase by one percent.

For freeway segments currently not in compliance with the adopted LOS standard:

1. A project is considered to have an adverse impact if the project will add traffic demand equal to one percent or more of the segment capacity or causes the freeway segment volume-to-capacity (v/c) ratio to increase by one percent if the freeway segment is currently not in compliance with the adopted LOS standard.

Existing Conditions

The Existing Conditions scenario provides an evaluation of current operation based on existing traffic volumes during the weekday a.m. and p.m. peak periods as well as weekend midday peak period. This condition does not

include project-generated traffic volumes. Traffic volume data representative of the typical weekday was collected on May 8, 2019, while local schools were in session. Since there are typically special events of varying sizes occurring every Saturday, counts for this period were conducted over two Saturdays (May 11, 2019 and June 1, 2019) and the larger of the two were applied in the analysis. These counts represent typical conditions as they were conducted on days with clear weather and reflect local, regional and visitor travel activity.

Intersection Levels of Service

Under existing conditions, all study intersections currently operate at acceptable levels of service during the weekday a.m., p.m., and weekend midday peak hours. This includes intersections operating at LOS E, which is considered the minimum acceptable standard during the peak two-hour commuting period and peak recreational hour. The existing traffic volumes are shown in Figure 3. A summary of the intersection level of service calculations is provided in Table 4, and a copy of the Level of Service calculations is provided in Appendix B.

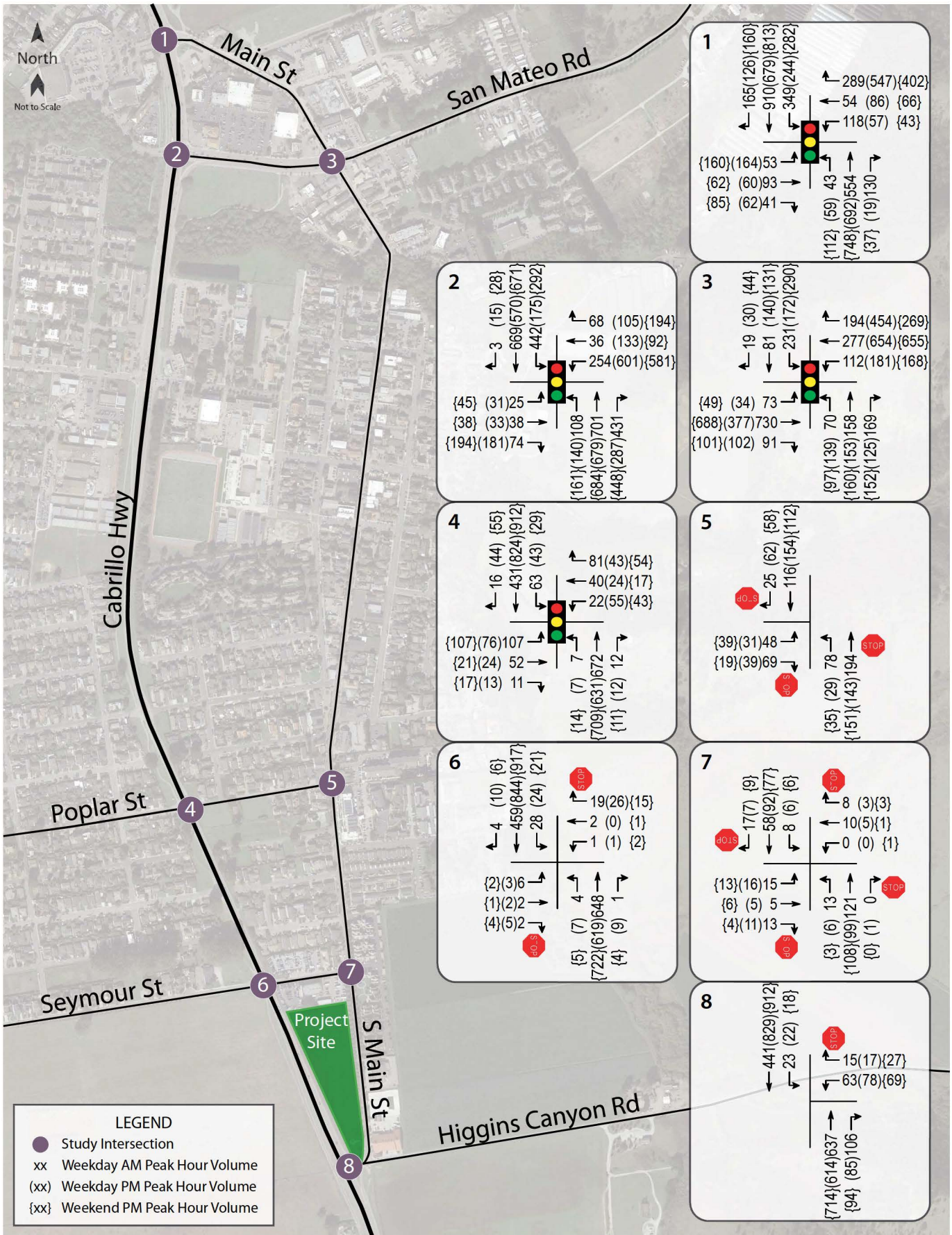
Table 4 – Existing Peak Hour Intersection Levels of Service

Study Intersection Approach	AM Peak		PM Peak		Weekend Peak	
	Delay	LOS	Delay	LOS	Delay	LOS
1. SR-1/N. Main St	37.1	D	39.4	D	43.4	D
2. SR-1/SR-92 (CMP)	41.8	D	37.4	D	31.2	C
3. Main St/SR-92 (CMP)	40.5	D	35.8	D	31.8	C
4. SR-1/Poplar St	31.4	C	20.1	C	22.5	C
5. Main St/Poplar St	4.3	A	2.2	A	2.3	A
6. SR-1/Seymour St	0.8	A	0.6	A	0.5	A
<i>Eastbound (Seymour St) Approach</i>	<i>27.1</i>	<i>D</i>	<i>33.6</i>	<i>D</i>	<i>39.1</i>	<i>E</i>
7. Main St/Seymour St	7.9	A	7.8	A	7.7	A
8. SR-1/S. Main St	1.5	A	1.9	A	2.0	A
<i>Westbound (S. Main St) Approach</i>	<i>21.7</i>	<i>C</i>	<i>31.1</i>	<i>D</i>	<i>36.8</i>	<i>E</i>

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*

Roadway Segments

Under Existing Conditions, all roadway segments currently operate within the acceptable LOS standard during all three peak hours evaluated. A summary of roadway segment LOS is provided in Table 5.



Traffic Impact Study for the Hyatt Place Hotel
Figure 3 – Existing Traffic Volumes



Table 5 – Existing Roadway Segment Analysis Summary

Study Segment	Peak Hour	Direction	Capacity (vph)	Existing Condition		
				Volume	V/C	LOS
A. SR-1 from Frenchmans Creek Rd to Grand Blvd	AM	NB	2,200	896	0.407	B
		SB	2,200	1,424	0.647	C
	PM	NB	2,200	1,403	0.638	C
		SB	2,200	1,049	0.477	B
	WKD	NB	2,200	1,310	0.595	C
		SB	2,200	1,255	0.570	C
B. SR-1 from Grand Blvd to N. Main St	AM	NB	4,400	896	0.204	A
		SB	4,400	1,424	0.324	B
	PM	NB	4,400	1,403	0.319	B
		SB	4,400	1,049	0.238	A
	WKD	NB	4,400	1,310	0.298	A
		SB	4,400	1,255	0.285	A
C. SR-1 from N. Main St to SR-92	AM	NB	4,400	794	0.180	A
		SB	4,400	1,114	0.253	A
	PM	NB	4,400	815	0.185	A
		SB	4,400	760	0.173	A
	WKD	NB	4,400	923	0.210	A
		SB	4,400	991	0.225	A
D. SR-1 from SR-92 to Kelly Ave	AM	NB	4,400	1,240	0.282	A
		SB	4,400	997	0.227	A
	PM	NB	4,400	1,106	0.251	A
		SB	4,400	1,352	0.307	B
	WKD	NB	4,400	1,293	0.294	A
		SB	4,400	1,446	0.329	B
E. SR-1 from Kelly Ave to Poplar St	AM	NB	2,200	860	0.391	B
		SB	2,200	510	0.232	A
	PM	NB	2,200	750	0.341	B
		SB	2,200	911	0.414	B
	WKD	NB	2,200	870	0.395	B
		SB	2,200	996	0.453	B
F. SR-1 from Poplar St to Seymour St	AM	NB	2,200	673	0.306	B
		SB	2,200	491	0.223	A
	PM	NB	2,200	648	0.295	A
		SB	2,200	878	0.399	B
	WKD	NB	2,200	739	0.336	B

Table 5 – Existing Roadway Segment Analysis Summary

Study Segment	Peak Hour	Direction	Capacity (vph)	Existing Condition		
				Volume	V/C	LOS
G. SR-1 from Seymour St to S. Main St	AM	SB	2,200	944	0.429	B
		NB	4,400	653	0.148	A
	PM	SB	4,400	462	0.105	A
		NB	4,400	635	0.144	A
	WKD	SB	4,400	850	0.193	A
		NB	4,400	731	0.166	A
H. SR-1 from S. Main St to Miramontes Point Rd	AM	SB	4,400	504	0.115	A
		NB	4,400	743	0.169	A
	PM	SB	4,400	907	0.206	A
		NB	4,400	699	0.159	A
	WKD	SB	4,400	981	0.223	A
		NB	4,400	808	0.184	A
I. SR-92 from SR-1 to Main St	AM	EB + WB	2,800	1,260	0.450	D
	PM	EB + WB	2,800	1,336	0.477	E
	WKD	EB + WB	2,800	1,634	0.584	E
J. SR-92 from Main St to I-280	AM	EB + WB	2,800	1,713	0.612	E
	PM	EB + WB	2,800	1,963	0.701	E
	WKD	EB +WB	2,800	2,222	0.794	E

Notes: SR-1 segments are assumed to be a “Level Multi-lane Highway” with 50-mph average speed. SR-92 segments are assumed to be a “Two-Lane Highway” with Rolling Hills and a 40-mph average speed.

Background Conditions

The background condition includes existing condition traffic plus the forecasted traffic demand due to local and regional growth for the near-term condition, defined to occur by the year 2024 (or existing condition plus five years).

Recent a.m. and p.m. peak hour traffic demand forecasts from the San Mateo County (C/CAG-VTA) Travel Demand Model produced for the Local Coastal Land Use Plan update were reviewed for changes in traffic demand along roadway segments within the study area. The year 2018 and 2040 growth forecasts (roadway segment link volumes) were used to derive an annual growth rate of 0.93-percent for the a.m. and 1.19-percent for the p.m. peak hours. Since a separate version of the San Mateo County Travel Demand Model for the weekend peak hour is not available, the p.m. peak hour growth rate was also used for the weekend peak hour as a reasonable substitute. These growth rates were applied to existing traffic volumes for the weekday a.m., p.m., and weekend peak hours to forecast the Background Condition future traffic demand. In general, changes in future traffic demands are reflected in these growth rates as they are derived from the county travel demand model that incorporates land use and future development assumptions across the region. Model forecast output sheets for the study area are included in Appendix C.

The City of Half Moon Bay is planning a capital improvement project which would enhance the safety and operations along SR-1 in the vicinity of the project. The improvements would be comprised of the signalization of the intersection of SR-1/South Main Street (including the addition of protected pedestrian crossings) and widening SR-1 from two to four lanes. These improvements are assumed to be completed by the year 2024 and as such are reflected in the background condition intersection analysis. Geometrics and controls at all remaining study intersections are assumed to be the same under background conditions as under the existing conditions.

Under the anticipated background conditions, all study intersections would be expected to continue operating at acceptable levels of service during the a.m., p.m., and weekend peak hours. These results are summarized in Table 6 and background condition traffic volumes are shown in Figure 4.

Table 6 – Background Peak Hour Intersection Levels of Service

Study Intersection Approach	AM Peak		PM Peak		Weekend Peak	
	Delay	LOS	Delay	LOS	Delay	LOS
1. SR-1/N. Main St	37.1	D	39.7	D	41.7	D
2. SR-1/SR-92 (CMP)	42.2	D	37.5	D	33.8	C
3. Main St/SR-92 (CMP)	40.9	D	36.1	D	36.6	D
4. SR-1/Poplar St	42.5	D	21.2	C	25.6	C
5. Main St/Poplar St	4.0	A	2.2	A	2.3	A
6. SR-1/Seymour St	0.9	A	0.8	A	0.7	A
<i>Eastbound (Seymour St) Approach</i>	<i>27.2</i>	<i>D</i>	<i>37.3</i>	<i>E</i>	<i>43.6</i>	<i>E</i>
7. Main St/Seymour St	7.7	A	7.7	A	7.7	A
8. SR-1/S. Main St	6.6	A	5.7	A	5.0	A

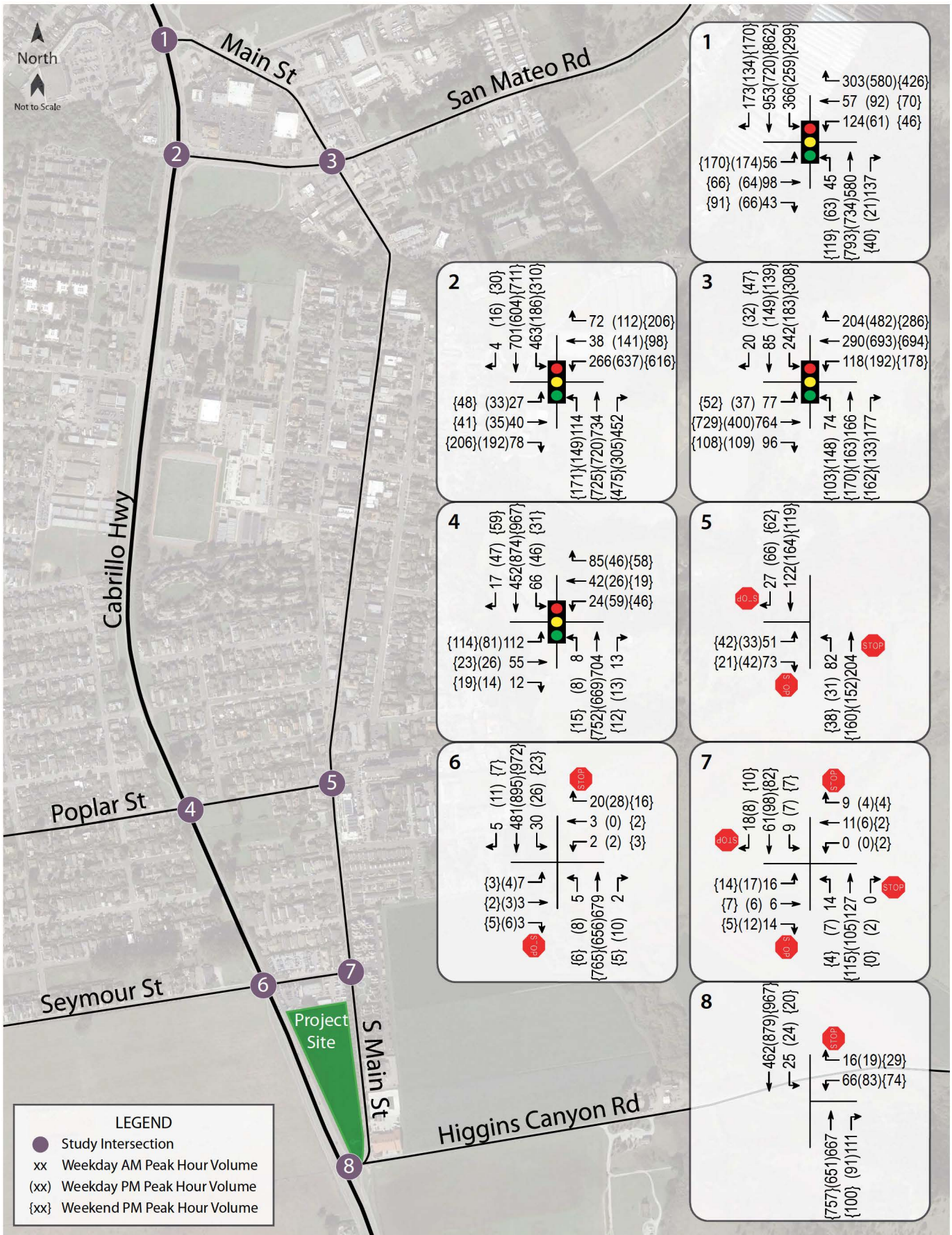
Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*

Cumulative Conditions

The cumulative condition is comprised of existing condition traffic plus the forecasted traffic demand due to local and regional growth for the long-term condition defined to occur by the year 2040 (or existing condition plus 21 years). Determination of the cumulative condition traffic demand volumes used the same annual growth rates to forecast the background condition volumes. Additionally, anticipated vehicle trips associated with key development projects along the coastal regional were added to the forecasted traffic volumes. A brief description of the development projects where trips were added is provided below:

- The Dunes at Half Moon Bay (212-Room Hotel, 15,060 square feet conference center, 177 RV parking spaces, 10 cabins and a retail store in Half Moon Bay)
- Cypress Point Affordable Housing Community Project (71 affordable housing units in Moss Beach)
- Harbor View Inn 15-room Expansion (51 Alhambra Avenue in El Granada)
- Main Street, Montara 3-story 22-room hotel (1390 Main Street in Montara)
- Harbor Village RV Park (50 space RV and 7 tent cabins at Capistrano/Hwy 1 in Princeton)

All study intersections are assumed to have the same geometry under cumulative conditions as under the background conditions. Under the anticipated cumulative condition volumes, the study intersections are expected to operate within acceptable service levels, except for the following locations and periods:



Traffic Impact Study for the Hyatt Place Hotel
 Figure 4 – Background Traffic Volumes

- SR-1/North Main Street would operate at LOS F during the weekend peak hour.
- SR-1/Seymour Street would operate acceptably with an overall LOS A during the p.m. peak hour and weekend peak hour, but with an LOS F at the eastbound (Seymour Street) approach for both peak hours.

Cumulative volumes are shown in Figure 5 and operating conditions are summarized in Table 7.

Table 7 – Cumulative Peak Hour Intersection Levels of Service						
Study Intersection Approach	AM Peak		PM Peak		Weekend Peak	
	Delay	LOS	Delay	LOS	Delay	LOS
1. SR-1/N. Main St	37.2	D	50.3	D	84.4	F
2. SR-1/SR-92 (CMP)	42.0	D	40.6	D	39.7	D
3. Main St/SR-92 (CMP)	40.9	D	38.9	D	41.6	D
4. SR-1/Poplar St	42.0	D	26.2	C	34.0	C
5. Main St/Poplar St	3.9	A	2.4	A	2.4	A
6. SR-1/Seymour St	1.1	A	1.0	A	1.0	A
<i>Eastbound (Seymour St) Approach</i>	<i>29.4</i>	<i>D</i>	<i>59.1</i>	<i>F</i>	<i>77.2</i>	<i>F</i>
7. Main St/Seymour St	7.8	A	7.9	A	7.8	A
8. SR-1/S. Main St	9.1	A	7.4	A	6.0	A

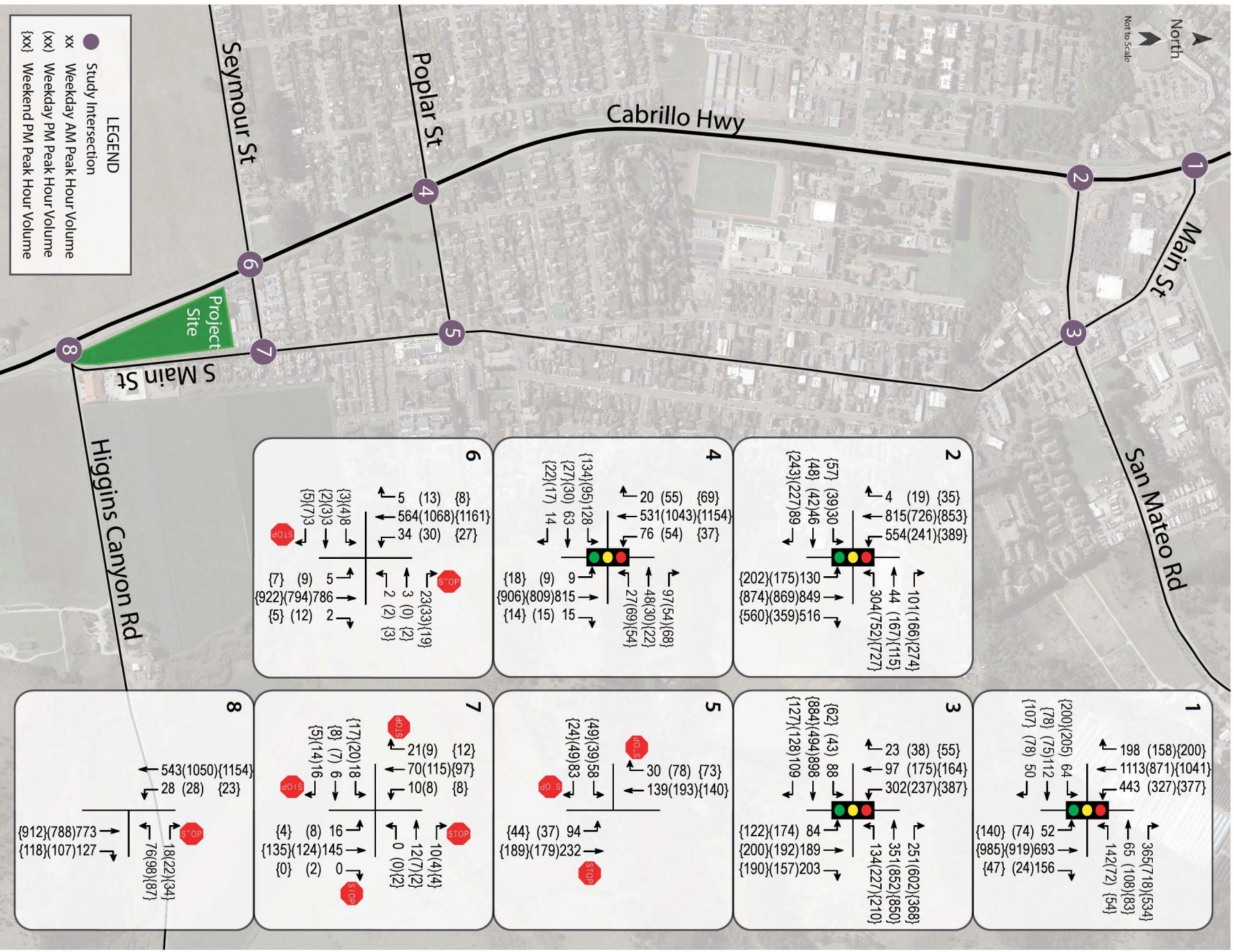
Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; **Bold** text = deficient operation; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*

Project Description

The proposed 129-room hotel would be located on the triangular shaped parcel roughly bounded by SR-1, South Main Street and Seymour Street in Half Moon Bay. The hotel would include 148 parking spaces and 90,784 square feet of hotel land use. The project also includes a Class I Bike Path and a series of adjacent pedestrian walking paths to be constructed within the open space between SR-1 and the main hotel building. The site is currently vacant and undeveloped. The proposed project site plan is shown in Figure 2.

Trip Generation

The project applicant intends to hire staff comprised mostly of Half Moon Bay residents. Doing so would potentially reduce the trip generation estimates as a portion of the staff would be able to walk or ride a bicycle to and from the hotel. Since the applicant cannot ensure that only Half Moon Bay residents would be hired, and to provide a conservative approach, the standard trip generation rates were applied with no trip reduction factor for employees within walking or biking distance.



Traffic Impact Study for the Hyatt Place Hotel
 Figure 5 – Cumulative (2040) Traffic Volumes

The anticipated trip generation for the proposed project was estimated using standard rates published by the Institute of Transportation Engineers (ITE) in *Trip Generation Manual*, 10th Edition, 2017 for “All Suites Hotel” (ITE LU #311)¹. The *Trip Generation Manual* does not specify a standard rate for “All Suites Hotel” during the weekend peak hour. Thus, the more conservative standard rate for “Hotel” (ITE LU #310) was used instead to estimate the trip potential for the weekend peak hour. The site is currently undeveloped and therefore not generating any trips. The project is not anticipated to generate any internal capture trip, pass-by trip credits or trip reductions resulting from nearby land use or transportation options.

The resulting expected trip generation potential for the proposed project is indicated in Table 8. The proposed project is expected to generate an average of 575 trips per day, including 44 trips during the a.m. peak hour, 46 during the p.m. peak hour and 93 during the weekend peak hour; these new trips represent the increase in traffic associated with the project.

Land Use	Units Rooms	Daily		AM Peak Hour ¹				PM Peak Hour ¹				Weekend Peak Hour ²			
		Rate	Trips	Rate	Trips	In	Out	Rate	Trips	In	Out	Rate	Trips	In	Out
Proposed															
All Suites Hotel	129	4.46	575	0.34	44	23	21	0.36	46	22	24	0.72	93	52	41
Total			575		44	23	21		46	22	24		93	52	41

Notes: ¹Standard Rates using the Peak Hour of Adjacent Street Traffic applied.

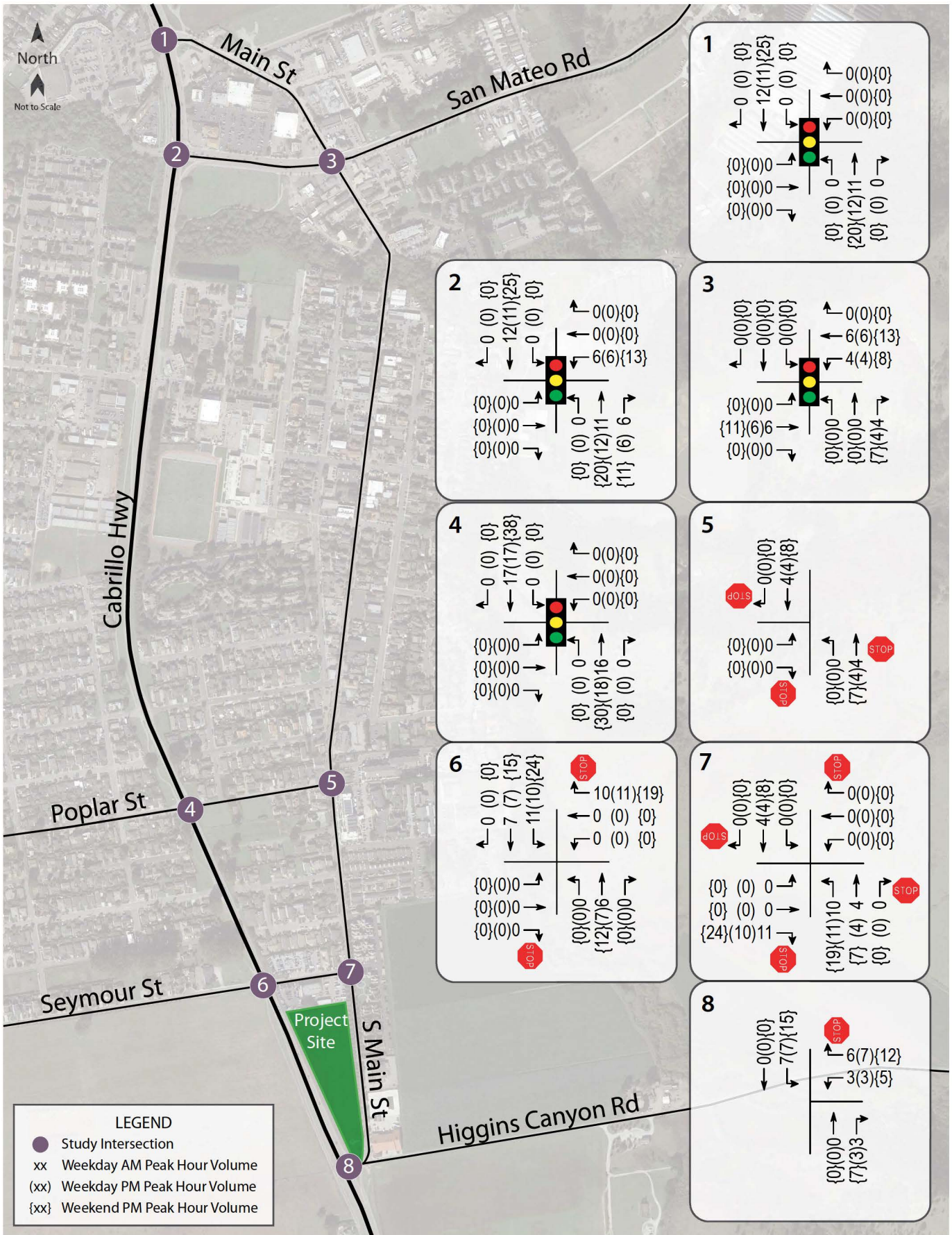
²Standard Rates using the Peak Hour of Generator applied since rates for Peak Hour of Adjacent Street Traffic are not available.

Trip Distribution

The San Mateo County (C/CAG-VTA) Travel Demand Model was used to estimate trip distribution patterns within the study area by comparing relative traffic on major roadways and then applying manual adjustments based on knowledge of the area and the application of professional judgment. The applied distribution assumptions and resulting trips are shown in Table 9 and Figure 6.

Route	Percent	Daily	AM Trips	PM Trips	Weekend Trips
To/From North via SR-1	48%	276	21	22	45
To/From East via SR-92	40%	230	18	18	37
To/From South via SR-1	12%	69	5	6	11
TOTAL	100%	575	44	46	93

¹ The ITE Trip Generation Manual describes an All Suites Hotel as a place of lodging that provides sleeping accommodations, a small restaurant and lounge, and small amounts of meeting space. Each suite includes a sitting room and separate bedroom; limited kitchen facilities are provided within the suite.



Traffic Impact Study for the Hyatt Place Hotel
Figure 6 – Project Traffic Volumes



Intersection Operation

Existing plus Project Conditions

Upon the addition of project-related traffic to the existing condition volumes, all study intersections would continue to operate at acceptable levels of service. These results are summarized in Table 10. Existing plus Project traffic volumes are shown in Figure 7.

Study Intersection Approach	Existing Condition						Existing + Project					
	AM Peak		PM Peak		Weekend Peak		AM Peak		PM Peak		Weekend Peak	
	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS
1. SR-1/N. Main St	37.1	D	39.4	D	43.4	D	37.2	D	39.4	D	38.1	D
2. SR-1/SR-92 (CMP)	41.8	D	37.4	D	31.2	C	41.7	D	37.4	D	35.7	D
3. Main St/SR-92 (CMP)	40.5	D	35.8	D	31.8	C	40.7	D	35.9	D	36.3	D
4. SR-1/Poplar St	31.4	C	20.1	C	22.5	C	41.1	D	20.5	C	25.6	C
5. Main St/Poplar St	4.3	A	2.2	A	2.3	A	4.3	A	2.2	A	2.3	A
6. SR-1/Seymour St	0.8	A	0.6	A	0.5	A	1.0	A	0.8	A	0.9	A
<i>EB (Seymour St) Approach</i>	<i>27.1</i>	<i>D</i>	<i>33.6</i>	<i>D</i>	<i>39.1</i>	<i>E</i>	<i>29.5</i>	<i>D</i>	<i>36.2</i>	<i>E</i>	<i>46.4</i>	<i>E</i>
7. Main St/Seymour St	7.9	A	7.8	A	7.7	A	8.0	A	7.9	A	8.0	A
8. SR-1/S. Main St	1.5	A	1.9	A	2.0	A	1.7	A	2.1	A	2.6	A
<i>WB (S. Main St) Approach</i>	<i>21.7</i>	<i>C</i>	<i>31.1</i>	<i>D</i>	<i>36.8</i>	<i>E</i>	<i>22.0</i>	<i>C</i>	<i>31.7</i>	<i>D</i>	<i>39.8</i>	<i>E</i>

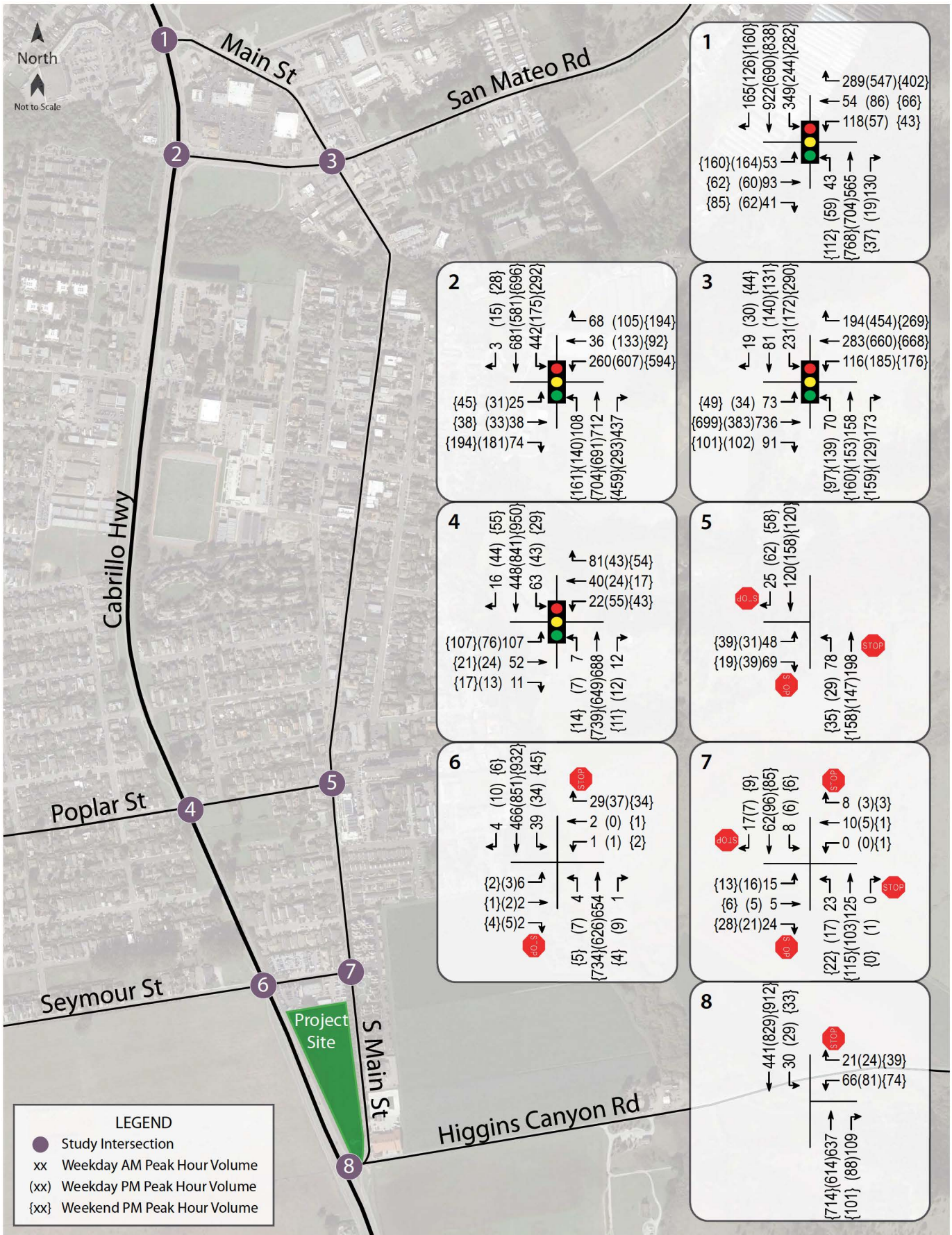
Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; CMP = Congestion Management Program; EB = Eastbound; WB = Westbound; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*

It should be noted that with the addition of project-related traffic volumes, average delay at the intersection of SR-1/SR-92 would decrease during the a.m. peak hour. While this is counter-intuitive, this occurs when trips are added to movements that are currently underutilized or have delays that are below the intersection average, resulting in a better balance between approaches and lower overall average delay. The conclusion could incorrectly be drawn that the project improves operation based on this data alone; however, it would be more appropriate to conclude that the project trips are expected to make use of excess capacity, so drivers would experience little, if any, change in conditions as a result of the project at these locations.

Finding – The study intersections are expected to continue operating within acceptable levels of service upon the addition of project-generated traffic.

Background plus Project Conditions

Upon the addition of project-related traffic to the background condition volumes, all the study intersections would continue to operate at acceptable levels of service, with the exception of SR-1/Seymour Street where operation would be expected to deteriorate from LOS E to F during the weekend peak hour. Since the peak hour volume warrant indicating potential need for a traffic signal would not be satisfied, the standards applied



Traffic Impact Study for the Hyatt Place Hotel
Figure 7 – Existing plus Project Traffic Volumes

this is not considered to be an adverse impact. These results are summarized in Table 11. Background plus Project traffic volumes are shown in Figure 8.

Table 11 – Background and Background plus Project Peak Hour Intersection Levels of Service

Study Intersection Approach	Background Condition						Background + Project					
	AM Peak		PM Peak		Weekend Peak		AM Peak		PM Peak		Weekend Peak	
	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS
1. SR-1/N. Main St	37.1	D	39.7	D	41.7	D	37.2	D	39.7	D	42.1	D
2. SR-1/SR-92 (CMP)	42.2	D	37.5	D	33.8	C	42.0	D	37.6	D	33.9	C
3. Main St/SR-92 (CMP)	40.9	D	36.1	D	36.6	D	40.9	D	36.2	D	36.8	D
4. SR-1/Poplar St	42.5	D	21.2	C	25.6	C	42.0	D	21.2	C	26.2	C
5. Main St/Poplar St	4.0	A	2.2	A	2.3	A	3.9	A	2.2	A	2.3	A
6. SR-1/Seymour St	0.9	A	0.8	A	0.7	A	1.1	A	0.9	A	1.1	A
<i>EB (Seymour St) Approach</i>	<i>27.2</i>	<i>D</i>	<i>37.3</i>	<i>E</i>	<i>43.6</i>	<i>E</i>	<i>29.4</i>	<i>D</i>	<i>40.3</i>	<i>E</i>	51.8	F
7. Main St/Seymour St	7.7	A	7.7	A	7.7	A	7.8	A	7.8	A	7.8	A
8. SR-1/S. Main St	6.6	A	5.7	A	5.0	A	9.1	A	8.5	A	9.5	A

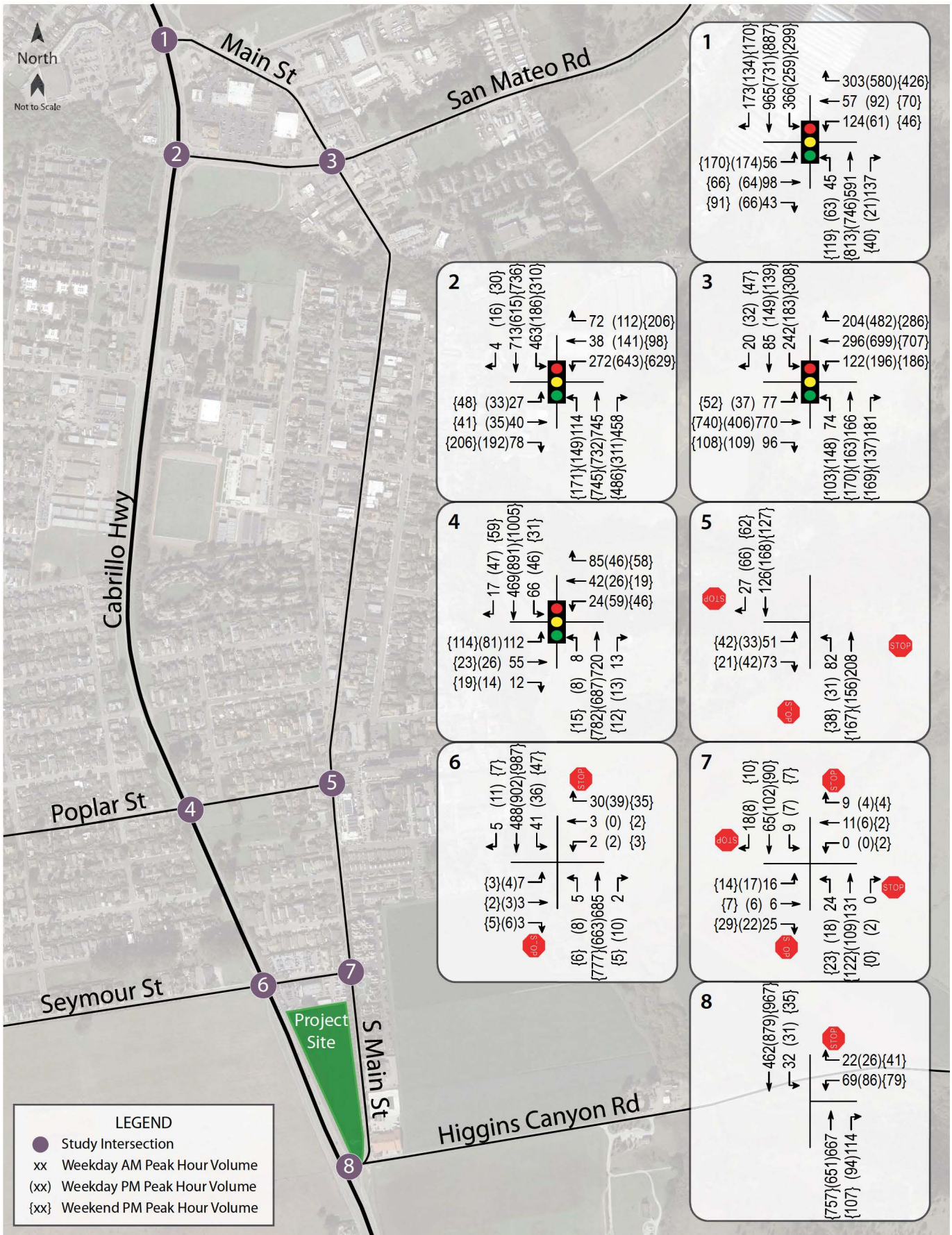
Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; CMP = Congestion Management Program; EB = Eastbound; WB = Westbound; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*; **Bold** text = deficient operation

It should be noted that with the addition of project-related traffic volumes, average delay at the intersections of SR-1/SR-92, SR-1/Poplar Street and Main Street/Polar Street would decrease during the a.m. peak hour. As noted previously, this condition reflects use of excess capacity and should not be interpreted as meaning that the project improves operation for other movements.

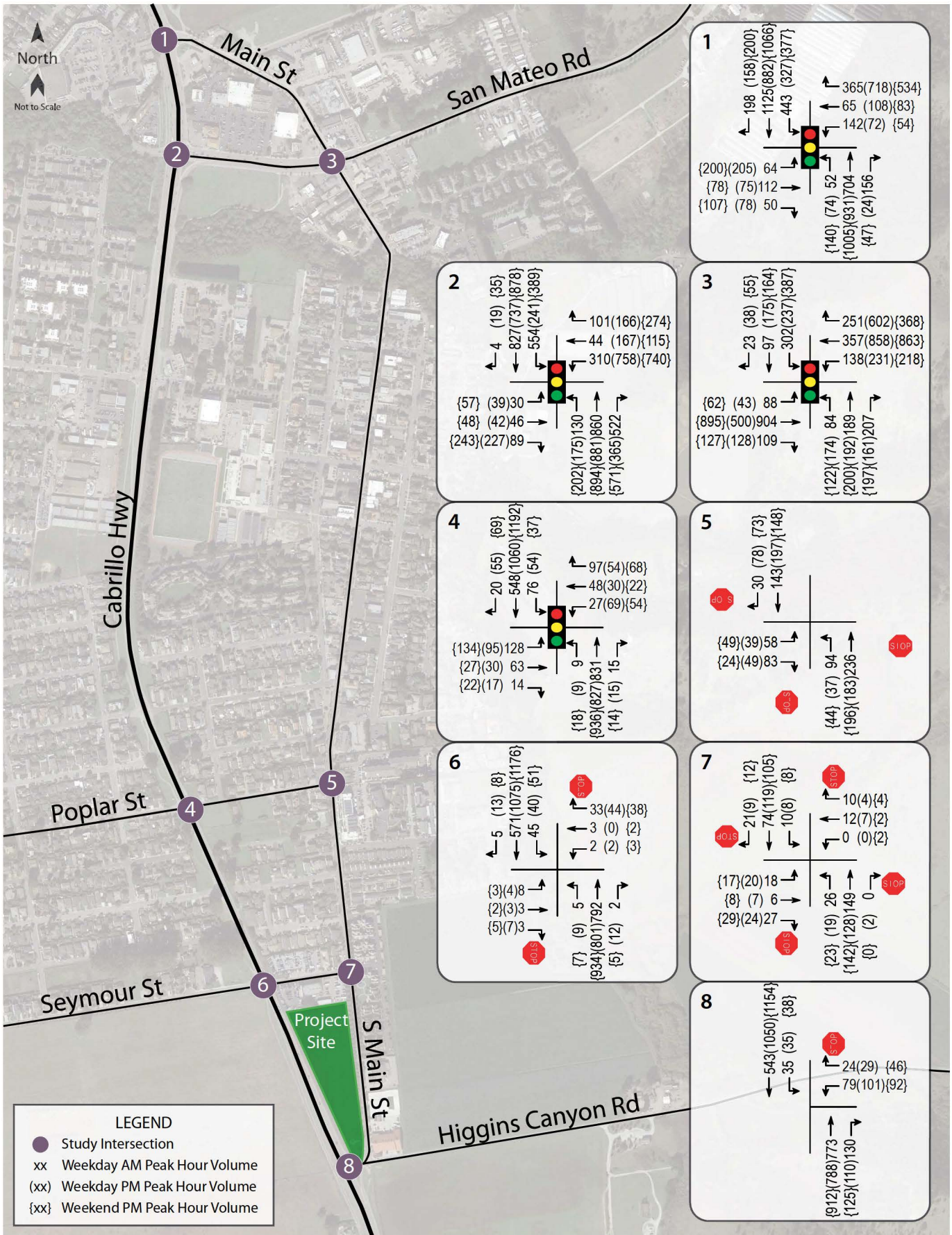
Finding – The study intersections are expected to continue operating at acceptable levels of service upon the addition of project-generated traffic, except at the intersection of SR-1/Seymour Street during the weekend peak hour, where the eastbound approach would have an average delay of 51.8 seconds per vehicle and operate at LOS F. However, the project would not result in an adverse impact at this intersection, since the volumes, even including project-related trips, would not satisfy the peak hour volume warrant for signalization.

Cumulative plus Project Conditions

Upon the addition of project-generated traffic to the anticipated cumulative condition volumes, all the study intersections would continue to operate at acceptable levels of service, except at the signalized intersection at SR-1/North Main Street which operates at LOS F during the weekend peak hour and unsignalized intersection of SR-1/Seymour Street which would operate at an overall LOS A during the p.m. and weekend peak hours, but with an LOS F at the eastbound (Seymour Street) approach. The Cumulative plus Project operating conditions are summarized in Table 12. Cumulative plus project traffic volumes are shown in Figure 9.



Traffic Impact Study for the Hyatt Place Hotel
Figure 8 – Background plus Project Traffic Volumes



Traffic Impact Study for the Hyatt Place Hotel
Figure 9 – Cumulative (2040) plus Project Traffic Volumes



Table 12 – Cumulative plus Project Peak Hour Intersection Levels of Service

Study Intersection Approach	Cumulative Condition						Cumulative + Project					
	AM Peak		PM Peak		Weekend Peak		AM Peak		PM Peak		Weekend Peak	
	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS	Delay	LOS
1. SR-1/N. Main St	37.2	D	50.3	D	84.4	F	59.9	E	51.0	D	87.9	F
2. SR-1/SR-92 (CMP)	42.0	D	40.6	D	39.7	D	37.4	D	41.0	D	40.4	D
3. Main St/SR-92 (CMP)	40.9	D	38.9	D	41.6	D	43.3	D	39.0	D	42.0	D
4. SR-1/Poplar St	42.0	D	26.2	C	34.0	C	48.7	D	26.6	C	35.1	D
5. Main St/Poplar St	3.9	A	2.4	A	2.4	A	4.2	A	2.3	A	2.4	A
6. SR-1/Seymour St	1.1	A	1.0	A	1.0	A	1.2	A	1.2	A	1.4	A
<i>EB (Seymour St) Approach</i>	<i>29.4</i>	<i>D</i>	59.1	F	77.2	F	<i>41.3</i>	<i>E</i>	65.0	F	96.6	F
7. Main St/Seymour St	7.8	A	7.9	A	7.8	A	8.0	A	8.0	A	8.0	A
8. SR-1/S. Main St	9.1	A	7.4	A	6.0	A	10.8	B	9.5	A	6.4	A

Notes: Delay is measured in average seconds per vehicle; LOS = Level of Service; CMP = Congestion Management Program; EB = Eastbound; WB = Westbound; Results for minor approaches to two-way stop-controlled intersections are indicated in *italics*; **Bold** text = deficient operation

The intersection of SR-1/North Main Street would operate at an unacceptable LOS F with or without the addition of project-generated vehicle trips during the weekend peak hour. The addition of project-generated trips would not increase the average control delay by more than four seconds. The project’s contribution to this intersection is not considered an adverse impact.

Under the p.m. and weekend peak hours, the stop-controlled Seymour Street approach at the intersection of SR-1/Seymour Street would operate at an unacceptable LOS F with or without the addition of project-generated vehicle trips. Also, under these conditions, the signalization peak hour volume warrant would not be satisfied. Therefore, the project’s contribution would not be considered an adverse impact at this intersection.

It should be noted that with the addition of project-related traffic volumes, average delay at the intersections of SR-1/SR-92 and Main Street/Poplar Street would decrease during the a.m. and p.m. peak hours, respectively. As noted previously, this condition reflects use of excess capacity and should not be interpreted as meaning that the project improves operation for other movements.

Finding – The study intersections are expected to continue operating at acceptable levels of service upon the addition of project-generated traffic, except at the intersections of SR-1/North Main Street during the weekend peak hour and SR-1/Seymour Street during the weekday p.m. and weekend peak hours. The project would not be considered an adverse impact at these intersections since the degradation of the average control delay at the signalized intersection of SR-1/North Main Street is less than four seconds and the unsignalized intersection at SR-1/Seymour Street would not satisfy the peak hour volume warrant for signalization.

Roadway Segment Analysis

Potential changes to the level of service of roadway segments near the project site were analyzed during the weekday a.m. and p.m. and weekend midday peak hours to determine if a significant amount of project traffic would be added to these roadway segments. Under Existing plus Project Conditions, all study roadway segments would continue to operate within the acceptable LOS standards during the three peak hours evaluated. A summary of roadway segment LOS is provided in Table 13.

Table 13 – Existing Plus Project Roadway Segment Analysis Summary

Study Segment	Peak Hour	Direction	Existing Condition			Existing plus Project				
			Volume	V/C	LOS	Added Trips	% of Capacity	Volume	V/C	LOS
A. SR-1 from Frenchmans Creek Rd to Grand Blvd	AM	NB	896	0.407	B	11	0.50%	907	0.412	B
		SB	1,424	0.647	C	12	0.55%	1,436	0.653	C
	PM	NB	1,403	0.638	C	12	0.55%	1,415	0.643	C
		SB	1,049	0.477	B	11	0.50%	1,060	0.482	B
	WKD	NB	1,310	0.595	C	20	0.91%	1,330	0.605	C
		SB	1,255	0.570	C	25	1.14%	1,280	0.582	C
B. SR-1 from Grand Blvd to N. Main St	AM	NB	896	0.204	A	11	0.25%	907	0.206	A
		SB	1,424	0.324	B	12	0.27%	1,436	0.326	B
	PM	NB	1,403	0.319	B	12	0.27%	1,415	0.322	B
		SB	1,049	0.238	A	11	0.25%	1,060	0.241	A
	WKD	NB	1,310	0.298	A	20	0.45%	1,330	0.302	B
		SB	1,255	0.285	A	25	0.57%	1,280	0.291	A
C. SR-1 from N. Main St to SR-92	AM	NB	794	0.180	A	11	0.25%	805	0.183	A
		SB	1,114	0.253	A	12	0.27%	1,126	0.256	A
	PM	NB	815	0.185	A	12	0.27%	827	0.188	A
		SB	760	0.173	A	11	0.25%	771	0.175	A
	WKD	NB	923	0.210	A	20	0.45%	943	0.214	A
		SB	991	0.225	A	25	0.57%	1,016	0.231	A
D. SR-1 from SR-92 to Kelly Ave	AM	NB	1,240	0.282	A	17	0.39%	1,257	0.286	A
		SB	997	0.227	A	18	0.41%	1,015	0.231	A
	PM	NB	1,106	0.251	A	18	0.41%	1,124	0.255	A
		SB	1,352	0.307	B	17	0.39%	1,369	0.311	B
	WKD	NB	1,293	0.294	A	31	0.70%	1,324	0.301	B
		SB	1,446	0.329	B	38	0.86%	1,484	0.337	B
E. SR-1 from Kelly Ave to Poplar St	AM	NB	860	0.391	B	17	0.77%	877	0.399	B
		SB	510	0.232	A	18	0.82%	528	0.240	A
	PM	NB	750	0.341	B	18	0.82%	768	0.349	B
		SB	911	0.414	B	17	0.77%	928	0.422	B
	WKD	NB	870	0.395	B	31	1.41%	901	0.410	B
		SB	996	0.453	B	38	1.73%	1,034	0.470	B

Table 13 – Existing Plus Project Roadway Segment Analysis Summary

Study Segment	Peak Hour	Direction	Existing Condition			Existing plus Project				
			Volume	V/C	LOS	Added Trips	% of Capacity	Volume	V/C	LOS
F. SR-1 from Poplar St to Seymour St	AM	NB	673	0.306	B	17	0.77%	690	0.314	B
		SB	491	0.223	A	18	0.82%	509	0.231	A
	PM	NB	648	0.295	A	18	0.82%	666	0.303	B
		SB	878	0.399	B	17	0.77%	895	0.407	B
	WKD	NB	739	0.336	B	31	1.41%	770	0.350	B
		SB	944	0.429	B	38	1.73%	982	0.446	B
G. SR-1 from Seymour St to S. Main St	AM	NB	653	0.148	A	6	0.14%	659	0.150	A
		SB	462	0.105	A	7	0.16%	469	0.107	A
	PM	NB	635	0.144	A	7	0.16%	642	0.146	A
		SB	850	0.193	A	7	0.16%	857	0.195	A
	WKD	NB	731	0.166	A	12	0.27%	743	0.169	A
		SB	923	0.210	A	15	0.34%	938	0.213	A
H. SR-1 from S. Main St to Miramontes Point Rd	AM	NB	743	0.169	A	3	0.07%	746	0.170	A
		SB	504	0.115	A	3	0.07%	507	0.115	A
	PM	NB	699	0.159	A	3	0.07%	702	0.160	A
		SB	907	0.206	A	3	0.07%	910	0.207	A
	WKD	NB	808	0.184	A	7	0.16%	815	0.185	A
		SB	981	0.223	A	5	0.11%	986	0.224	A
I. SR-92 from SR-1 to Main St	AM	EB +WB	1,260	0.450	D	12	0.43%	1,272	0.454	D
	PM	EB +WB	1,336	0.477	E	12	0.43%	1,348	0.481	E
	WKD	EB +WB	1,634	0.584	E	24	0.86%	1,658	0.592	E
J. SR-92 from Main St to I-280	AM	EB +WB	1,713	0.612	E	20	0.71%	1,733	0.619	E
	PM	EB +WB	1,963	0.701	E	20	0.71%	1,983	0.708	E
	WKD	EB +WB	2,222	0.794	E	39	1.39%	2,261	0.808	E

Notes: V/C = Volume-to-Capacity Ratio; SR-1 segments are assumed to be a “Level Multi-lane Highway” with 50 mph average speed; SR-92 segments are assumed to be a “Two-Lane Highway” with Rolling Hills and a 40-mph average speed. Source: W-Trans, 2020

Finding – The study roadway segments are expected to continue operating at acceptable levels of service upon the addition of project-generated traffic to Existing volumes.

Vehicle Miles Traveled

Consideration was given to the project’s potential generation of Vehicle Miles Traveled (VMT). Because the City of Half Moon Bay has not yet adopted a standard of significance for evaluating VMT, guidance provided by the California Governor’s Office of Planning and Research (OPR) in the publication *Transportation Impacts (SB 743) CEQA Guidelines Update and Technical Advisory*, 2018, was used.

To estimate the average distance traveled per employee, commuting to work data available from the US Census (2017) for the City of Half Moon Bay was used. This data summarizes the “home to work” distance traveled within the study area and does not include nuances like short distance midday trips, shopping-related trips or chained trips between the workplace and home. City Staff estimates that the average distance traveled between the project site and the two nearest commercial airports is 29.0 miles. (The distances to San Francisco Airport (SFO) and the San Jose Airport (SJC) are 38 miles and 20 miles, respectively.) The City of Half Moon Bay is approximately 4 miles long and this distance was assumed to be the average distance traveled for a local guest trip.

The unmitigated project condition was estimated by separating the total number of daily trips into three trip categories; employee trips, guest trip to/from the airport and local guest trips. The number of trips for each category was then multiplied by the average distance traveled for each trip category. A summary of the unmitigated VMT findings for this project is provided in Table 14.

Table 14 – Unmitigated Vehicle Miles Traveled Summary			
Trip Type	No. Daily Trips	Avg. Distance (mi)	VMT¹
Employees	48	18.9	907
Guests Trips (Airport)	79 ²	29.0	2,304
Guests Trips (Local)	448	4.0	1,790
Total	575		5,002

Note: 1) VMT estimates provided are subject to rounding error.
 2) Guest trips were estimated considering the peak room occupancy, number of rooms, and average length of stay

Standards of Significance

The OPR *Technical Advisory* includes suggested VMT significance thresholds for residential, employment, and retail uses but does not address hotel or other visitor-based land uses. The Technical Advisory indicates that lead agencies may develop their own thresholds for other land use types. For the purposes of this study, the City of Half Moon Bay Staff has defined that a project, with the implementation of Transportation Demand Management (TDM) measures, which generates 15 (or more) percent less than the project unmitigated VMT would indicate a less-than-significant impact.

Recommended TDM Program

Transportation Demand Management (TDM) measures aim to reduce single-occupancy vehicle trips, parking demand, and total VMT through use of alternative modes of transportation and more efficiently planned trips. The following section describes the proposed guest and employee TDM program.

Guest TDM Programs

Airport/Coastal Shuttle

The hotel should offer a free shuttle service to both San Francisco and San Jose airports to encourage guests to stay without renting a vehicle. Shuttles should operate frequently enough to provide guests with timely service while maximizing the potential for ridesharing. In addition, the shuttle should also stop at appropriate at tourist destinations and beaches along the coast so that guests can make short-distance trips without a car.

Parking Price Incentive

Many hotels in more remote coastal locations offer parking to be included in the cost of a room and by doing so, inadvertently encourage guests to bring cars and generate more congestion. As an alternative, the hotel should offer, and advertise, reduced room rates for those who do not arrive in a private vehicle. As an initial step, the hotel can offer a reduced rate of \$10 per night weekdays and \$20 on weekends and holidays, and adjust the price as necessary to manage parking demand.

Bike Share Program

A bike share program operates by having the hotel provide bicycles for guest use. By covering the access costs to the bike share program, the hotel provides guests with a non-auto mode option for exploring Half Moon Bay, enabling guests to feel more comfortable taking a shuttle to the hotel, knowing that they will have a way to get around once they arrive. In addition, the hotel should provide guests with bicycle helmets and locks free of charge to further encourage the use of bicycles.

Transportation Information

Providing guests with information regarding transportation options to the hotel can help encourage guests to consider non-auto or rideshare options. This information should be emailed or mailed to guests as part of their registration confirmation process providing guests with the information early on to assist in their logistics planning for arrival to the hotel. Information regarding the availability of shuttle service to the hotel and lower room rates for guests without cars should be highlighted. In addition, an on-site transportation board including bicycle maps, trails, transit routes and schedules, and contact numbers for taxi and town car services should be included in the reception area to assist guests.

Employee TDM Programs

Bicycle Parking

The hotel should provide secure storage where employees will be able securely store their bicycles while at work. Providing secure long-term parking for employees is a critical component of encouraging employees to bike to work as the lack of secure parking is often cited by employees as a deterrent. In addition, the hotel should provide hotel-maintained racks outside for visitors or other short-term users.

Parking Pricing and Cash-Out

As noted above, many hotels offer free parking for guests and the same is often given as a fringe benefit to employees. This serves as a strong disincentive for employees to not drive to work. Instead, the hotel should both price parking for employees on a daily basis and offer a “cash-out” to those who don’t drive to work. Under a parking cash-out program, an employer offers the cash value of the parking subsidy to any employee who does not drive to work. Offering employees the option of a “cash out” incentive to use an alternative mode of transportation (transit, bike, walk, or carpool to work) will help to reduce vehicle commute trips and emissions. This analysis assumes an initial parking price of \$7 per day.

In addition to pricing parking for employees (and guests), the hotel should work actively with the community to ensure parking demand does not “spillover” onto nearby streets. This can be accomplished either by educating and monitoring guests and employees or simply creating an on-street permit area around the hotel with parking prioritized for residents.

Ridematching

The greatest barrier to workplace carpooling is often simply being able to identify and travel with other nearby employees. Fortunately, there are services that can assist in pairing employees within the same organization or across organizations. The most basic publicly available service is 511.org’s free ridematching service that is also

offered through commute.org. As an alternative, the hotel may wish to set up a basic internal ridematching program among employees to facilitate carpooling.

Priority Parking

An easy way of promoting ridesharing is to designate priority employee parking spaces for carpools. The cost of this improvement is limited to the paint or sign used and can help market ridesharing as a priority in the organization.

Guaranteed Ride Home Program

Guaranteed Ride Home (GRH) is a program that provides a “back-up” ride to employees who carpool, use transit, bike/walk, or use other alternatives as their commute mode; in San Mateo County, it is provided through commute.org. If an employee who carpools to work, so does not have their own vehicle, needs to leave work for an emergency, such as a sick child or other unexpected need, they will be redeemed for the cost of taxi ride to get them home. This is an important supportive measure to encourage employees not to drive alone to work and often goes as a welcome, but unused benefit.

Transportation Coordinator

The presence of a staff person dedicated part-time to overseeing and managing the TDM program will be helpful in ensuring the ongoing success of these programs. This would not be a distinct position, but instead would be a role that is integrated into the on-site manager. The duties can include:

- Managing the shuttle program
- Create and distribute employee transportation information welcome packets
- Maintain and update a bulletin board or other physical source of transportation information
- Distribute local bicycle and walking maps
- Monitor bicycle facilities
- Administer the parking and cash-out program
- Oversee and manage the Guaranteed Ride Home program
- Promote the ride-matching program

Welcome Packet for New Employees

New employees should be provided with a welcome packet containing relevant transportation information. The packet could include material regarding ride-matching services, the guaranteed ride home program, the cash-out program as well as resources for those walking or biking to work.

Monitor Performance

It is important to continually monitor the performance of a TDM program and adjust measures as necessary to ensure its success. The hotel should conduct mode split and VMT surveys each year to both make adjustments and use as marketing material. Guest and employee satisfaction surveys are also an effective way of ensuring a quality TDM program.

TDM Program Impact Analysis

The suite of TDM measures outlined above will have a profound impact on reducing both guest and employee vehicle trips and VMT. The expected VMT reductions associated with the various TDM measures were estimated based on information published in the California Air Pollution Officers Association (CAPCOA) report *Quantifying Greenhouse Gas Mitigation Measures*, CAPCOA, 2010, the most utilized current resource to measure VMT reductions. As Table 15 shows, overall hotel VMT is expected to be reduced by 15.4% using this suite of TDM strategies.

Table 15 – Estimated Vehicle Miles Traveled Reductions

Trip Type	No. Daily Trips	Avg. Distance (mi)	Total VMT¹	VMT¹ Reduction	Mitigated VMT¹	Percent Reduction
Employees	48	18.9	907	127	780	14.0%
Guests Trips (Airport)	79 ²	29.0	2,304	378	1,926	16.4%
Guests Trips (Local)	448	4.0	1,790	267	1,523	14.9%
Total	575		5,002	772	4,230	15.4%

Note: 1) VMT estimates provided are subject to rounding error.
 2) Guest trips were estimated considering the peak room occupancy, number of rooms, and average length of stay

Finding – The TDM program results in a 15.4 percent VMT reduction, resulting in a *less-than-significant* VMT impact.

Recommendation – The project should implement the TDM measures identified in this report to reduce its VMT by 15.4 percent below unmitigated project conditions.

Signal Warrant Analysis

A traffic signal warrant analysis was conducted to determine the potential need for a traffic signal at each unsignalized study intersection that is projected to operate at LOS E or F. Chapter 4C of the *California Manual on Uniform Traffic Control Devices (CA-MUTCD)* provides guidance on when a traffic signal should be considered. For the purposes of this study, only Warrant 3 (Peak Hour) was considered.

Warrant 3 is satisfied when an engineering study finds that finds that the criteria in either of the following two categories are met:

- A. If all three of the following conditions exist for the same one hour (any four consecutive 15-minute periods) of an average day:
 1. The total stopped time delay experienced by the traffic on one minor-street approach (one direction only) controlled by a STOP sign equals or exceeds: four vehicle-hours for a one-lane approach; or five vehicle-hours for a two-lane approach, and
 2. The volume on the same minor-street approach (one direction only) equals or exceeds 100 vehicles per hour for one moving lane of traffic or 150 vehicles per hour for two moving lanes, and
 3. The total entering volume serviced during the hour equals or exceeds 650 vehicles per hour for intersections with three approaches or 800 vehicles per hour for intersections with four or more approaches.

- B. The plotted point representing the vehicles per hour on the major street (total of both approaches) and the corresponding vehicles per hour on the higher-volume minor-street approach (one direction only) for one hour (any four consecutive 15-minute periods) of an average day falls above the applicable curve in Figure 4C-3 for the existing combination of approach lanes.

The peak hour warrant would not be satisfied at the intersection of SR-1/Seymour Street for any of the scenarios analyzed in this study. It should be noted that the satisfaction of a traffic signal warrant or warrants does not require the installation of a traffic control signal, as other factors (warrants) should also be considered. Warrant 3 worksheets are included in Appendix D.

Findings – The intersection of SR-1/Seymour Street is projected to operate at LOS F during the weekend peak hour under Background plus Project conditions, and under Cumulative Conditions with or without project-generated trips during the weekday p.m. and weekend peak hours. The evaluation confirmed that volumes at the intersection of SR-1/Seymour Street would be insufficient to satisfy Warrant 3 under any of these scenarios. Thus, the project would not result in an adverse impact at this intersection.

Vehicular Access and Circulation

Vehicular Access

Internal Circulation

On-site circulation was evaluated to determine if the layout would provide adequate circulation for vehicles and pedestrians. Based on a review of the site plan (dated January 29, 2019), the internal roadways are expected to provide acceptable circulation for motorized vehicles. This site plan also indicates clearly marked paths for pedestrians between the building entrances, the parking lot, and sidewalks along South Main Street and Seymour Street.

Site development standards published by the *Coastside Fire Protection District* stipulate that all new emergency access roads shall have 15.5 feet of vertical clearance and an unobstructed minimum width of 20 feet. Where hydrants are located, the road shall be a minimum of 26 feet wide for a length of 20 feet on each side of the hydrant (40 feet total length). A detailed review of the site plan for compliance with Coastside Fire Protection District standards was not conducted as the site plan does not include the level of detail necessary. It is recommended that representatives from the Coastside Fire Protection District review the detailed construction plans as they become available.

Site Access

Vehicle access to the project site would be accomplished via three driveways: two driveways on South Main Street and one driveway on Seymour Street. The driveways on South Main Street as proposed would be full-access and allow all vehicle movements. The driveway on Seymour Street would be limited to right-turn exit movements only. The southernmost driveway on South Main Street is intended as a service access for deliveries and other operational needs of the hotel. All hotel guests are expected to use the main (northern) driveway on South Main Street as the primary access point for the project.

Project Driveway Sight Distances

Sight distances along South Main Street and Seymour Street at each project driveway were evaluated based on sight distance criteria contained in the *Highway Design Manual* published by Caltrans. The recommended sight distances for minor street approaches that are either a private road or a driveway are based on stopping sight distance associated with the approach travel speeds on the public street. Additionally, the stopping sight distance needed for a following driver to stop if there is a vehicle waiting to turn into a side street or driveway is evaluated based on the stopping sight distance criterion and the approach speed on the major street.

Sight distance at each proposed driveway was field measured. Based on a design speed of 25 mph, the minimum stopping sight distance needed is 150 feet.

The distance between SR-1 and the exit only project driveway on Seymour Street is 100 feet, which is less than the minimum required sight distance for a 25-mph facility. A driver exiting the project site from the Seymour Street driveway would not be able to see an approaching vehicle from northbound SR-1 turning onto eastbound Seymour Street. Additionally, due to the position of the driveway relative to SR-1, a driver exiting from the Seymour Street driveway would be required to turn and look nearly 180 degrees over their left shoulder to gain the line of sight to properly view an inbound northbound right-turning vehicle from SR-1. The inadequate sight distance at the Seymour Street Driveway is considered a significant project impact.

The available sight distances at each driveway along South Main Street would exceed 150 feet in both directions, which would be adequate for the anticipated travel speeds. To maintain this sight distance, it is noted that any vegetation near the project's driveways should be trimmed to an appropriate height of less than three feet and trees trimmed so that nothing hangs below a height of seven feet from the surface of the roadway. Additionally, it is recommended that on-street parking be restricted for 15 feet on either side of the two project driveways on South Main Street.

Finding – Sight distances at each driveway exit would be hindered by the presence of on-street parking and vegetation along South Main Street. The proposed exit only access on Seymour Street would have an inadequate sight distance toward SR-1, which is considered a significant project impact.

Mitigations – To achieve a minimum sight distance of 150 feet at each driveway access point, it is recommended that on-street parking be restricted for 15 feet on either side of each driveway. Also, it is recommended that vegetation along the project frontage on South Main Street be trimmed.

To reduce the project safety impact to a less-than-significant level, it is recommended that the Seymour Street egress should be removed from the project plans or converted to an emergency-vehicle-only access. Additionally, the following optional improvements should be considered as potential site improvements:

1. Include a gate at the Seymour Street egress to prevent daily use. The gate should be maintained so that opening the gate during an emergency evacuation condition is possible.
2. Modify the site plan to include an additional driveway access on South Main Street at the northern end of the parking lot located approximately 260 feet south of the Main Street/Seymour Street intersection.

Alternative Modes

Given the proximity to nearby residences, the historic Main Street shopping district and Poplar Beach relative to the hotel site, it is reasonable to assume that some hotel guests and employees would walk, bicycle, and/or use transit to reach the hotel.

Pedestrian Facilities

Project Site – The project would build new sidewalks on its frontage with Main Street and a new pedestrian walking path with benches along SR-1 between Main Street and Seymour Street. The project also includes a pedestrian walking path which would be located in between SR-1 and the hotel buildings. The walking path would be generally parallel with SR-1 and connect South Main Street with Seymour Street. The addition of the proposed sidewalk and walking paths would fill in areas of discontinuous sidewalks and complete walking connectivity throughout the immediate neighborhood.

Finding – Pedestrian facilities serving the project site would be adequate.

Bicycle Facilities

The project includes a Class I bike path which would be located between SR-1 and the hotel buildings. The bicycle path would be generally parallel with SR-1 and connect South Main Street with Seymour Street.

Finding – Existing and proposed bicycle facilities and shared use of minor streets would provide adequate access for bicyclists.

Bicycle Storage

The *City of Half Moon Bay Municipal Code 18.36.070 Bicycle Parking* states that short-term bicycle parking shall be provided to serve guests and other visitors. The number of short-term bicycle parking spaces shall be at a ratio of one bicycle parking space per ten off-street parking spaces with a minimum of four bicycle parking spaces per establishment. Given the proposed supply of 148 spaces, the project should have at least fifteen bicycle parking spaces.

The project will include bicycle racks located near the main entrance to the hotel lobby as well as bicycle lockers on-site with a combined maximum capacity for short-term bicycle parking of approximately 30 bicycles. The hotel is also proposing to include a rental or bike check out service providing up to 20 bicycles which would be available for use by hotel guests. It is also noteworthy to mention that bicycles can also be rented at Half Moon Bay Bike Works which is located approximately 4,800 feet from the project on Kelly Avenue.

Finding – Bicycle storage facilities will provide storage for more than fifteen bicycles and would therefore satisfy City Code requirements.

Transit

Existing transit routes were reviewed and found to be adequate to accommodate project-generated transit trips. Existing stops are within an acceptable walking distance (one-quarter mile) of the site.

Finding – Transit facilities serving the project site are adequate.

Parking

The proposed project’s off-street parking supply was analyzed to determine whether it would be sufficient to meet anticipated parking demand. The project includes 148 parking stalls located in a surface parking lot. These spaces are not anticipated to be shared with adjacent land uses. The parking supply was compared to two separate resources; the City Municipal Code and published ITE parking demand rates.

Parking supply requirements are stipulated in the *City of Half Moon Bay Municipal Code, Chapter 18.36.040 Off-street parking facilities*; for “Hotels, motels and motor lodges”. The City requirement states that one space should be provided per guest bedroom plus one space per employee. The proposed project is comprised of 129 rooms (with one bedroom each) and seventeen employees. The City’s parking requirement for this project is 146 spaces.

Parking demand for the proposed project was estimated using standard rates published by ITE in *Parking Generation, 5th Edition, 2019*. The parking demand of the project was estimated using the published 85th-percentile rates for Hotel (ITE LU #310) in a general suburban setting.

The project is proposing to provide 148 spaces, which is greater than either the City requirement (146 spaces) or the projected parking demand (128 spaces). The proposed parking supply, expected demand, and City parking Code requirements are summarized in Table 16.

Land Use	Units (No. of Rooms)	Supply (spaces)	ITE Parking Generation		City Requirements	
			Rate ¹	Est. Parking Demand	Rate ²	Spaces Required
Hotel	129	148	0.99	128	One space for each guest bedroom, plus one space per employee.	146

Notes: ¹ *Parking Generation 5th Edition*, Institute of Transportation Engineers, 2019
² Chapter 18,35,040 Off-street parking facilities, *Half Moon Bay Municipal Code*

Requirements stipulated by the Federal Accessibility Guidelines state that a minimum number of stalls must be categorized as accessible stalls for disabled persons. To satisfy this requirement, at least five stalls for disabled persons must be provided. The site plan shows six of the 148 spaces designated as accessible spaces. Thus, the project would comply with these Federal Accessibility Guidelines.

Finding – The project would provide an adequate number of parking spaces to accommodate the anticipated demand per ITE rates, and to satisfy the City parking Code requirements. Also, the number of accessible stalls would satisfy applicable requirements.

Conclusions and Recommendations

Conclusions

- The proposed project is expected to generate an average of 575 trips per day, including 44 trips during the weekday a.m. peak hour, 46 during the p.m. peak hour and 93 during the weekend midday peak hour.
- All study intersections are expected to continue operating acceptably under all conditions with and without the project, except for the signalized intersection at SR-1/North Main Street and the unsignalized intersection at SR-1/Seymour Street. However, the proposed project would not be considered an adverse impact at each of these intersections.
- The anticipated amount of vehicle traffic passing through the unsignalized intersection of SR-1/Seymour Street during the weekend peak hour under Background plus Project and Cumulative Conditions, would not satisfy the peak hour volume warrant indicating potential need for a traffic signal, either with or without the proposed project.
- State Routes 1 and 92 within the study area are anticipated to operate at acceptable levels of service with or without the project, under all volume scenarios evaluated.
- The proposed project would have a less-than-significant transportation impact on vehicle miles traveled with the implementation of the recommended Transportation Demand Management Plan.
- Pedestrian, bicycle, and transit facilities would be adequate to serve the project as proposed.
- Sight lines at the project driveways along South Main Street are adequate. The proposed exit only driveway on Seymour Street would have an inadequate sight distance between the driveway and SR-1.
- The proposed parking supply of 148 spaces exceeds both the City parking requirements and the estimated parking demand based on standard rates.

Recommendations

- The project should implement the recommended Transportation Demand Management Plan measures to reduce its VMT by more than 15 percent below unmitigated project conditions.
- To achieve a minimum sight distance of 150 feet at each driveway access point, it is recommended that parking be prohibited for 15 feet on either side of each driveway. Further, to maintain adequate sight lines, vegetation along the project frontage on South Main Street should be trimmed to ensure that all landscaping lies below three feet in height of above seven feet.
- To improve the site access and reduce the project safety impact to a less-than-significant level, it is recommended that the exit only driveway at Seymour Street either be eliminated or converted to an EVA. If an additional site access driveway is desired, the site plan should be modified to include another driveway on South Main Street at the northern end of the parking lot, approximately 260 feet south of the Main Street/Seymour Street intersection.

Study Participants and References

Study Participants

Principal in Charge	Mark E. Spencer, PE
Project Manager/Traffic Engineer	Kenny B. Jeong, PE
Assistant Engineer	Allison Woodworth, EIT
Graphics	Hannah Yung-Boxdell
Editing/Formatting	Hannah Yung-Boxdell
Report Review	Dalene J. Whitlock, PE, PTOE

References

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- Trip Generation Manual*, 10th Edition, Institute of Transportation Engineers, 2017

HMB003





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Appendix A

Traffic Count Data





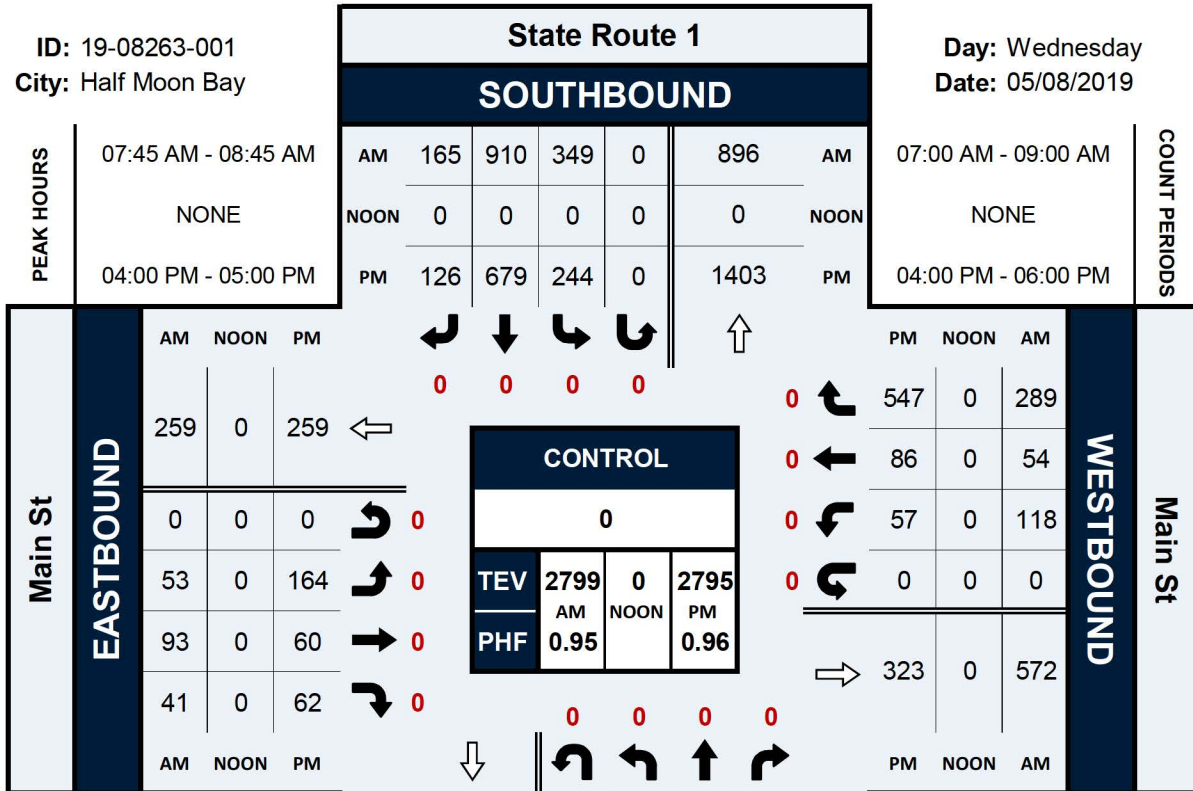
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State Route 1 & Main St

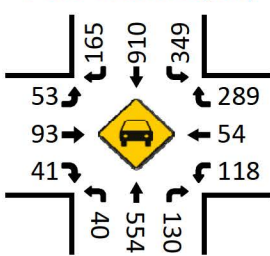
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City: Half Moon Bay

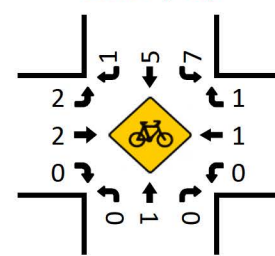
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Date: 05/08/2019



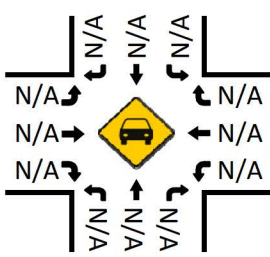
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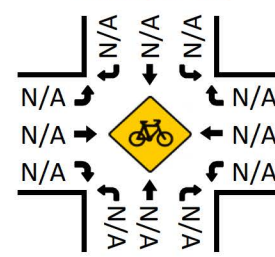
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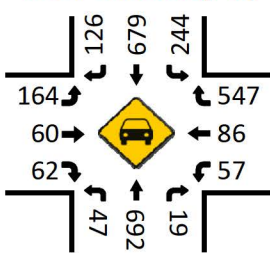
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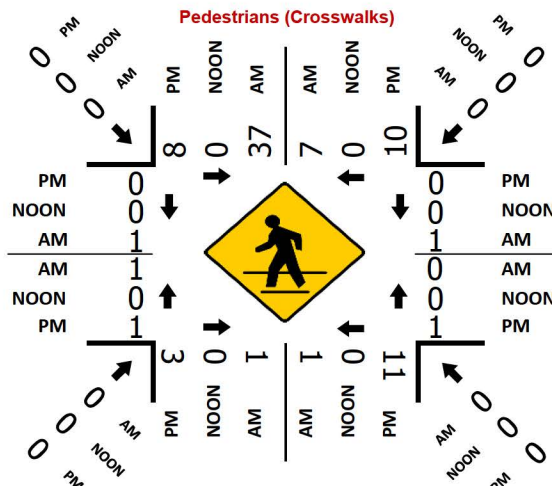
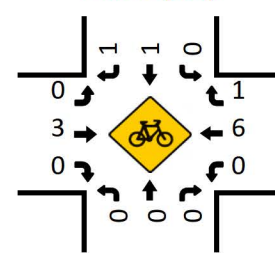
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Total Vehicles (PM)



Bikes (PM)

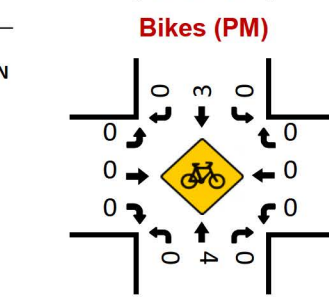
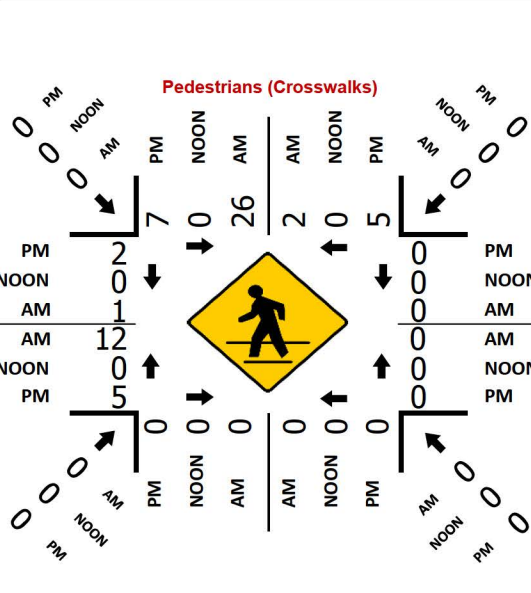
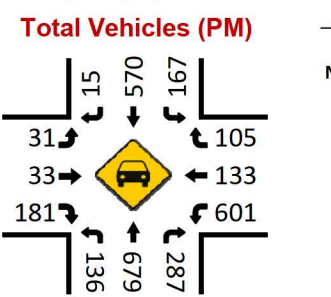
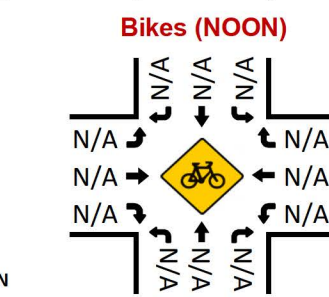
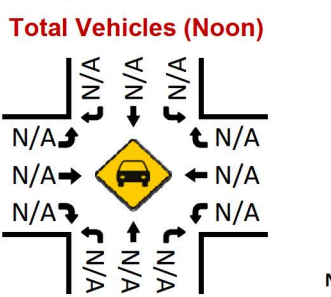
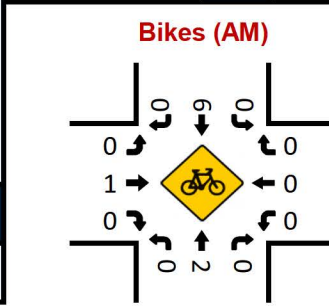
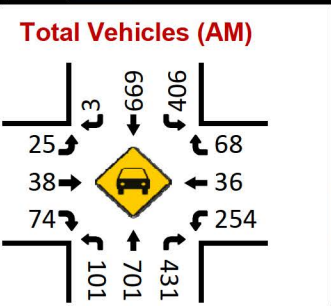
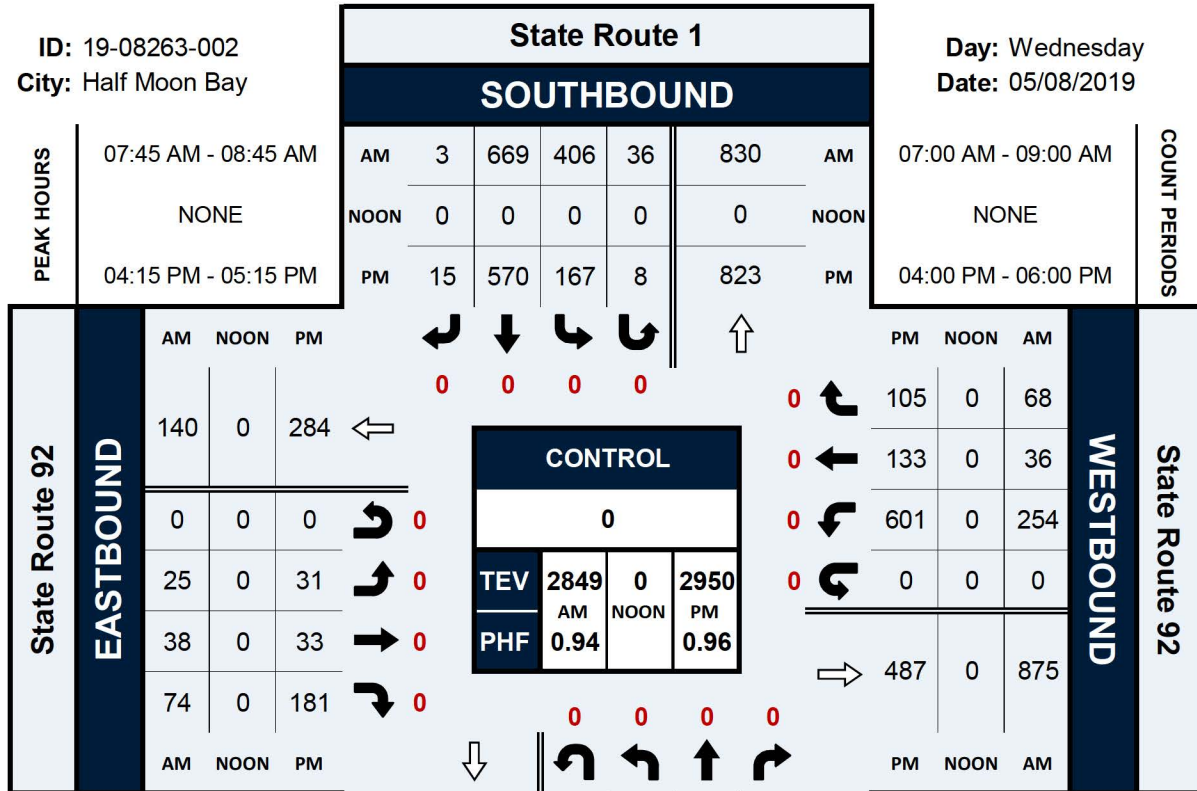


State Route 1 & State Route 92

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City: Half Moon Bay

Day: Wednesday
Date: 05/08/2019

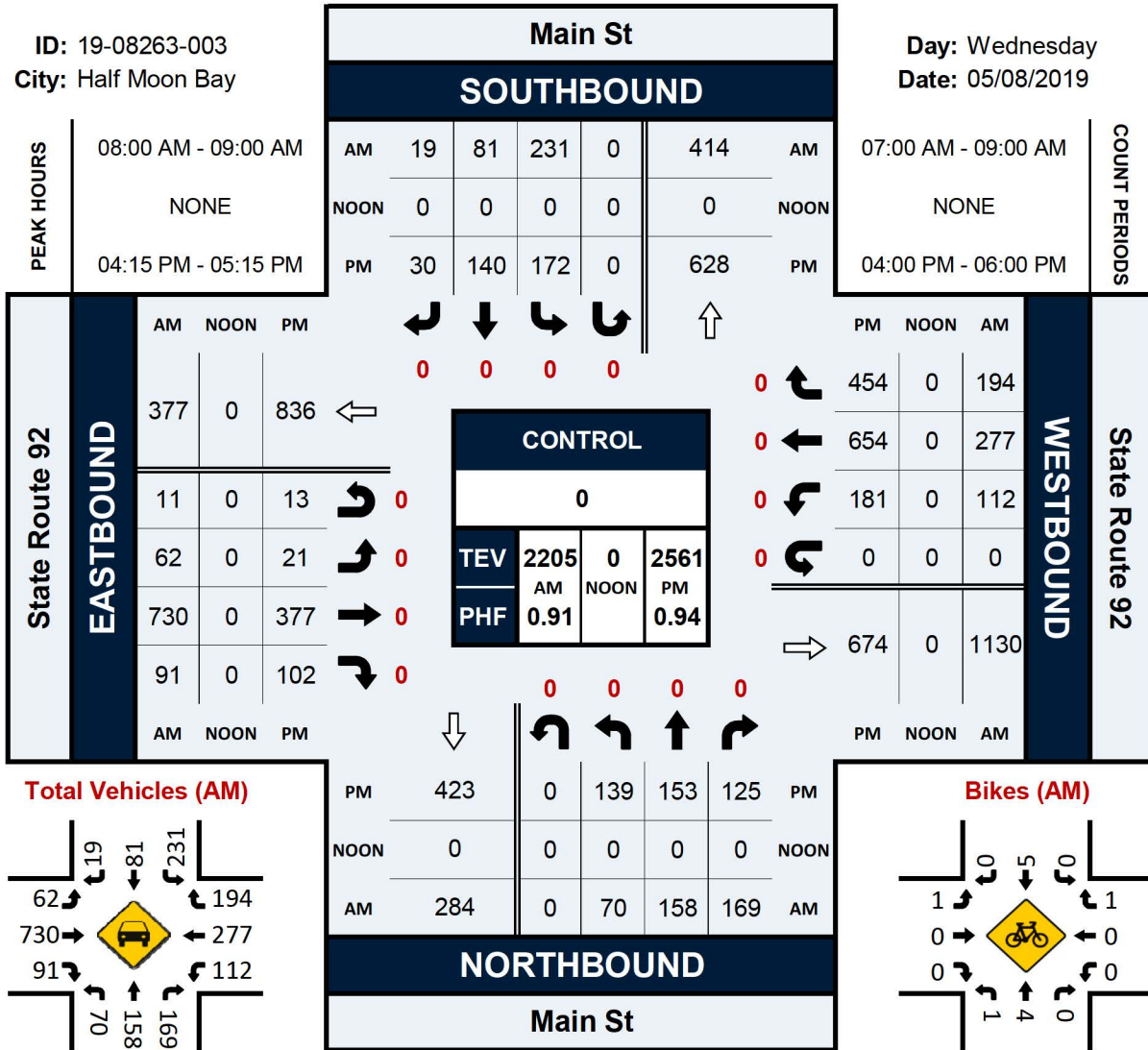


Main St & State Route 92

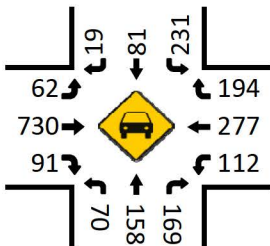
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City: Half Moon Bay

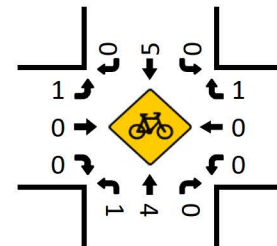
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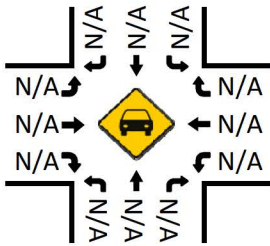
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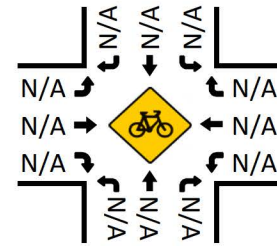
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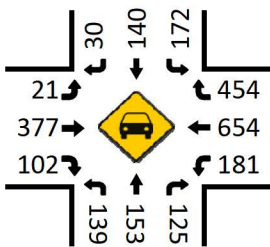
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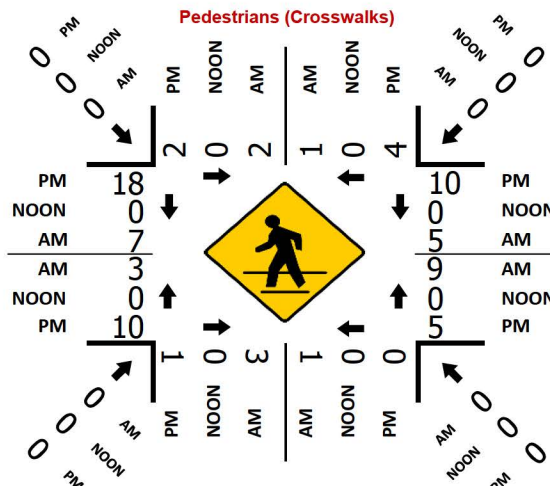
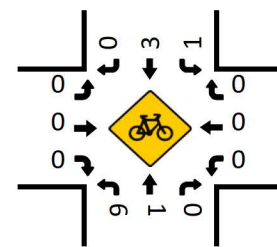
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Total Vehicles (PM)



Bikes (PM)

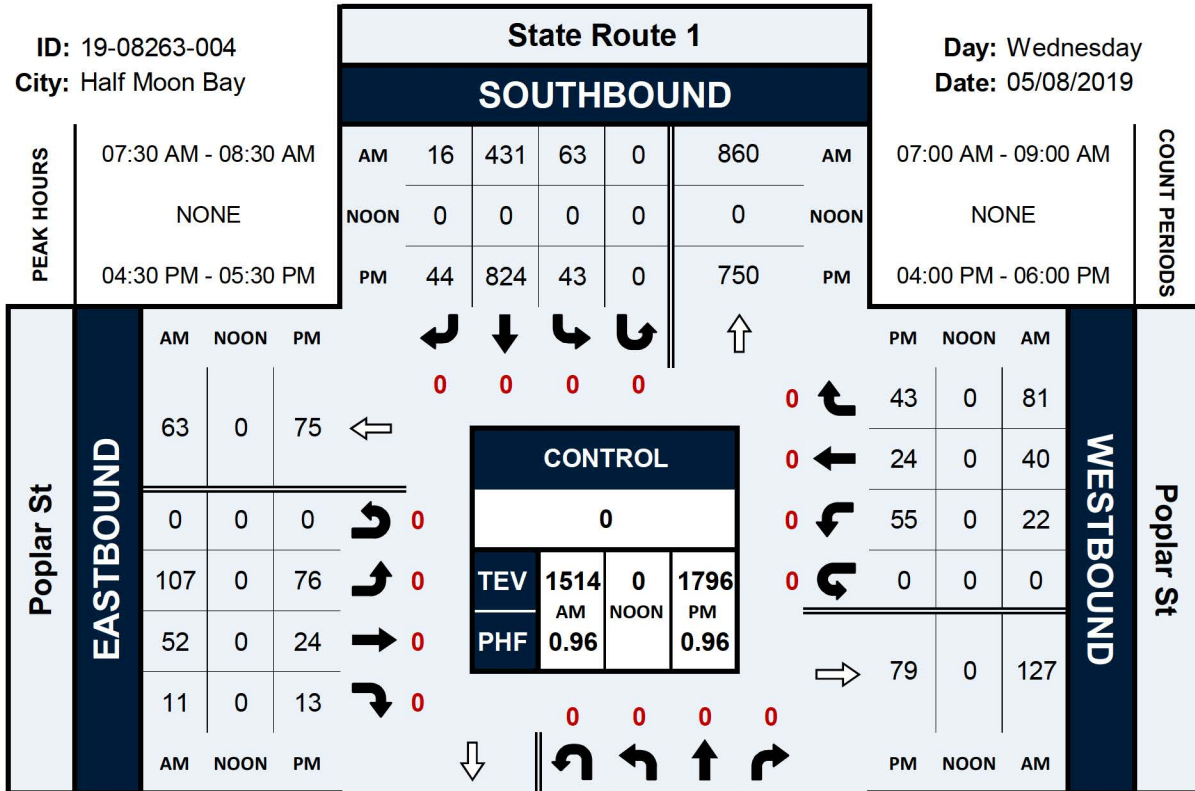


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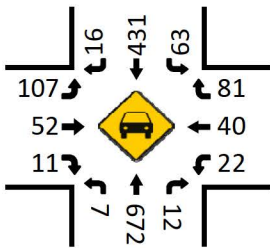
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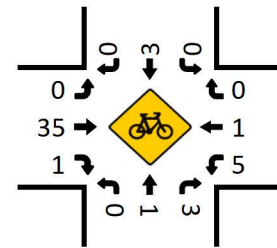
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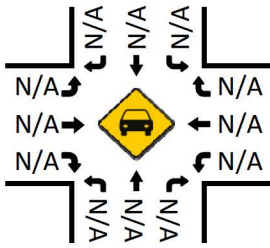
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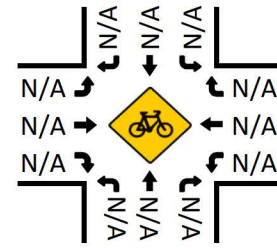
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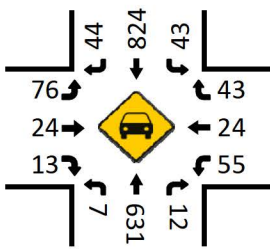
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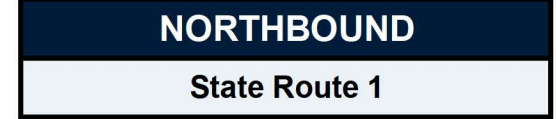
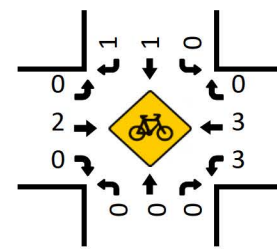
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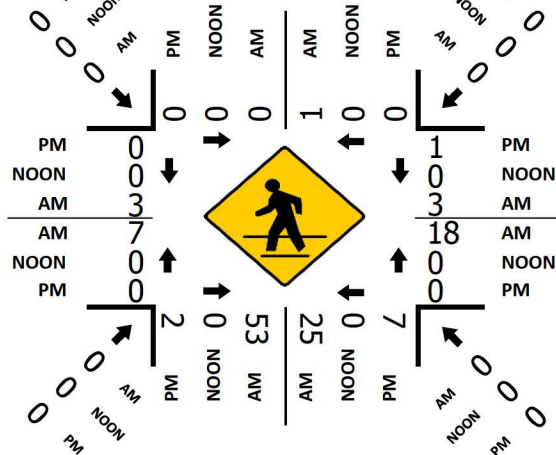
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Bikes (PM)



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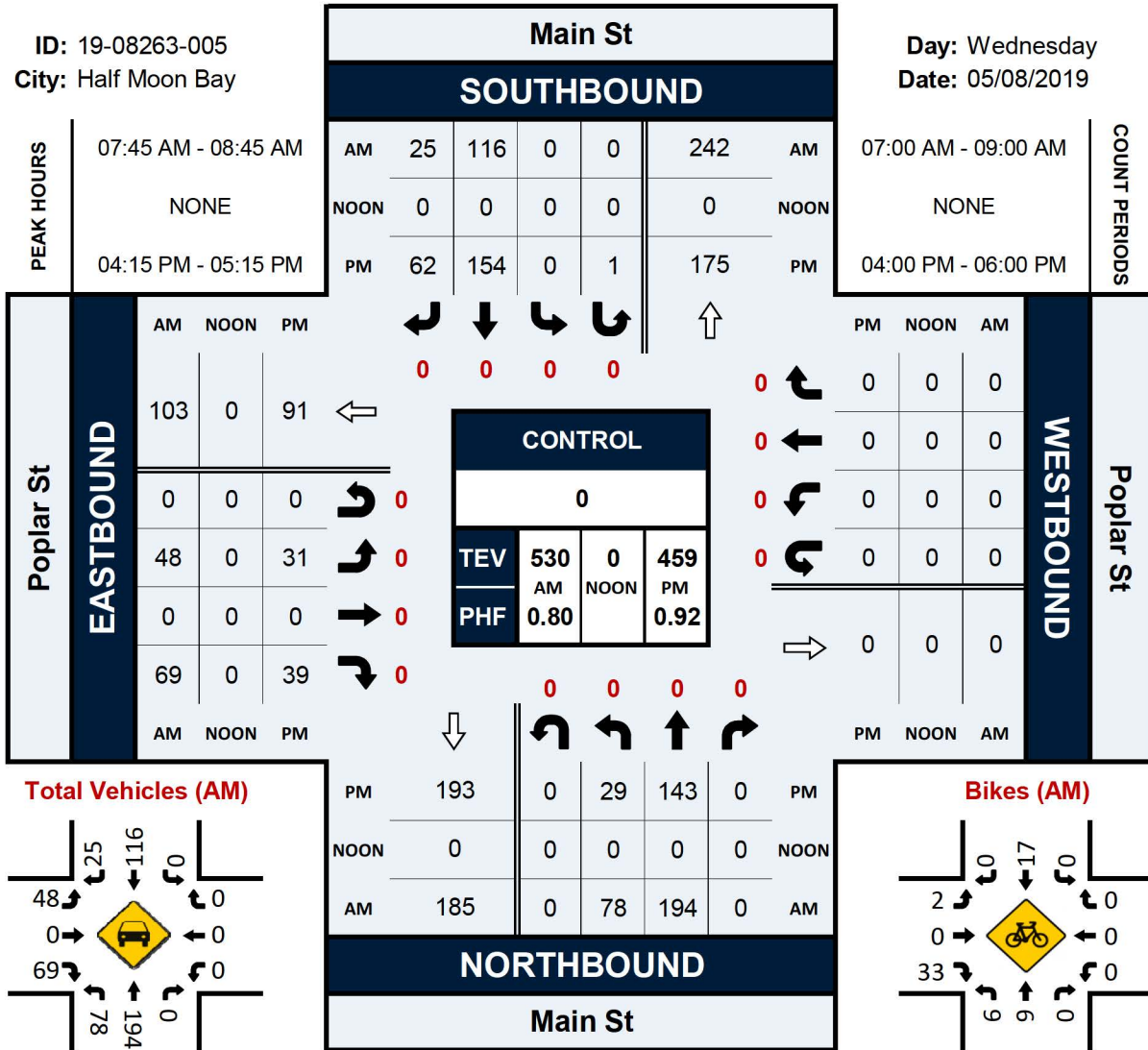


Main St & Poplar St

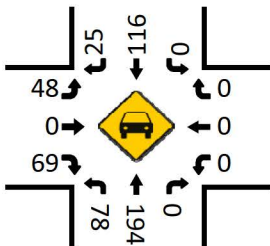
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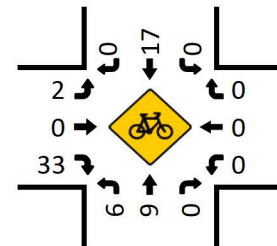
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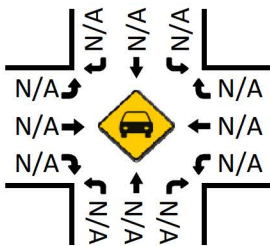
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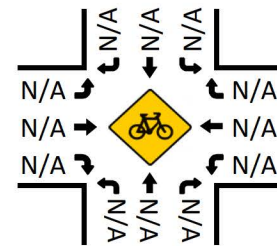
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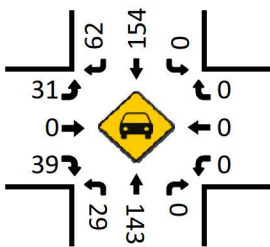
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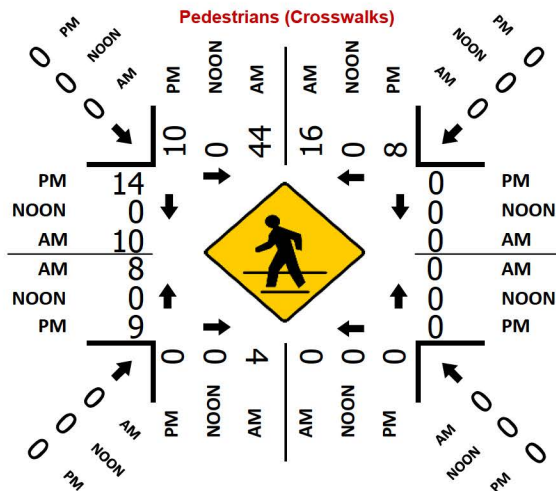
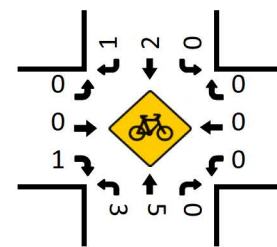
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Bikes (PM)

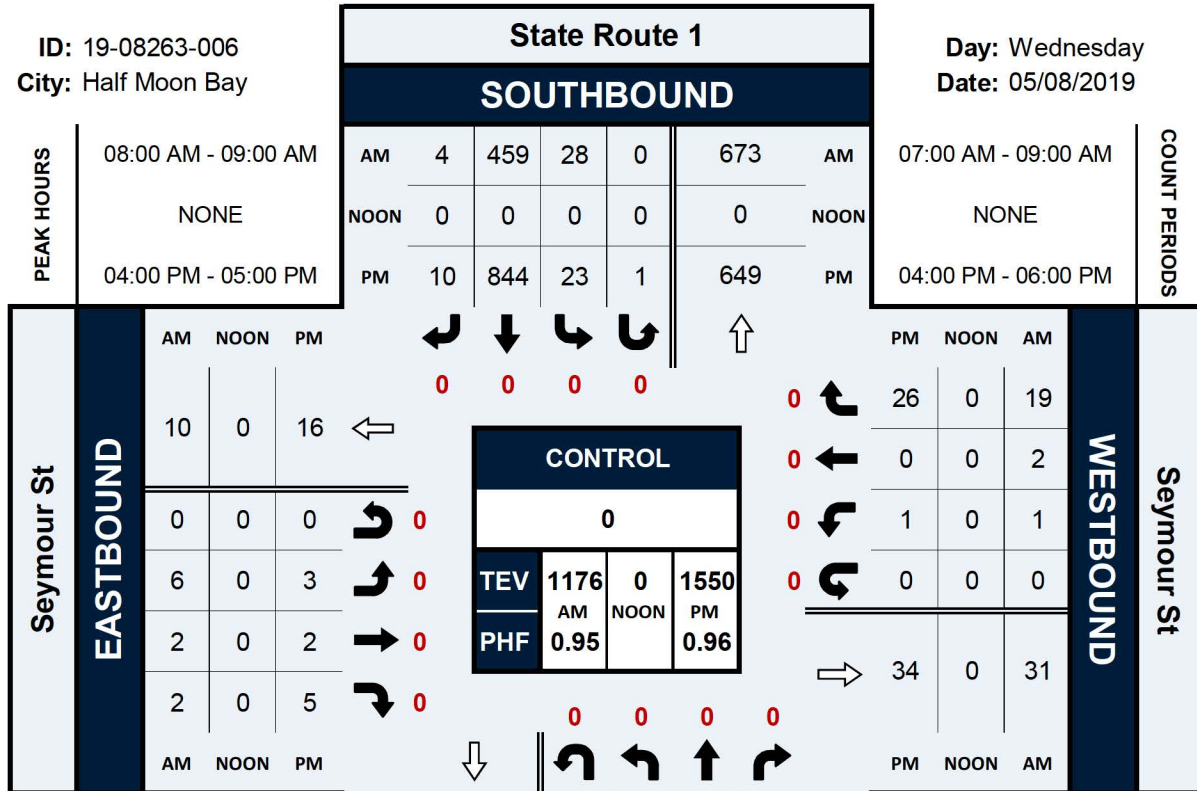


State Route 1 & Seymour St

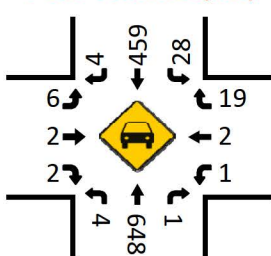
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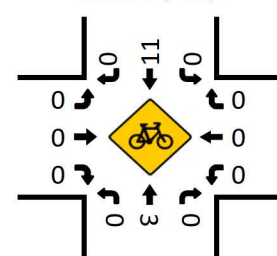
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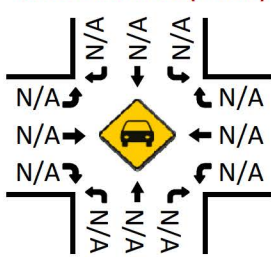
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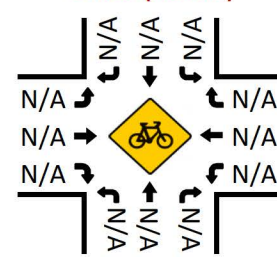
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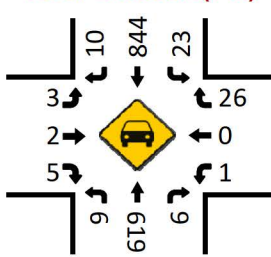
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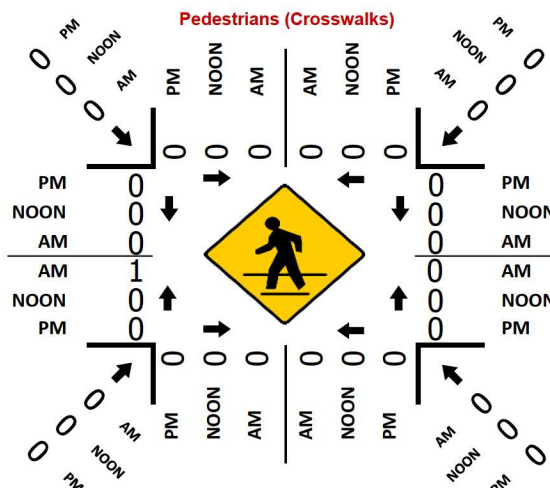
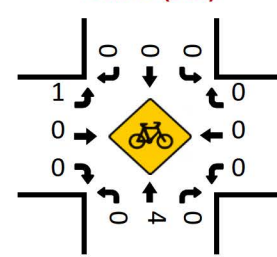
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Total Vehicles (PM)



Bikes (PM)

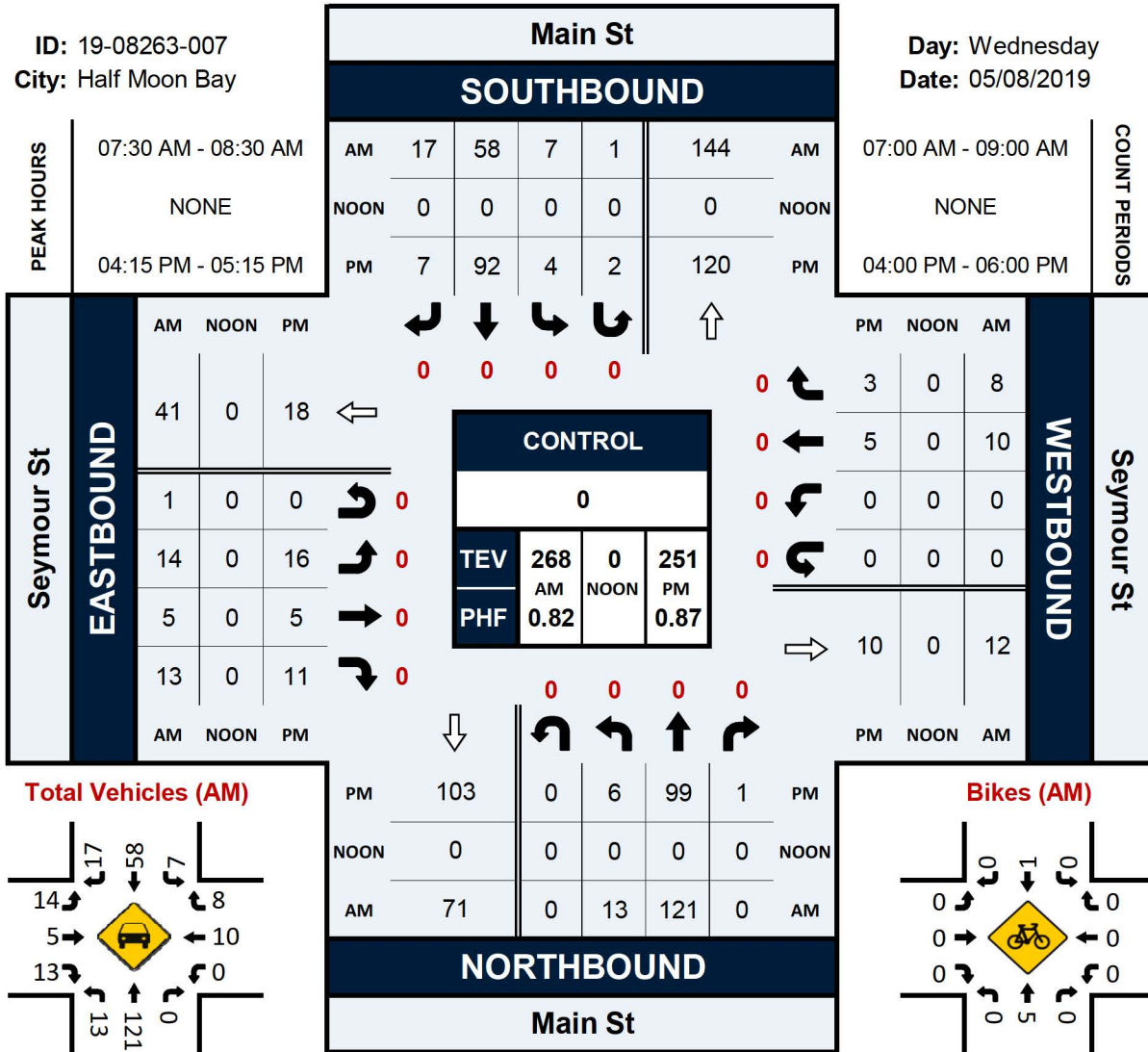


Main St & Seymour St

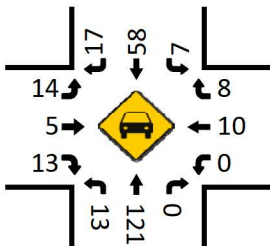
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City: Half Moon Bay

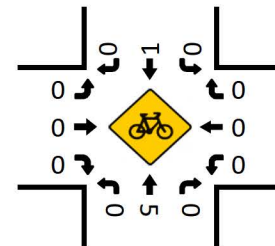
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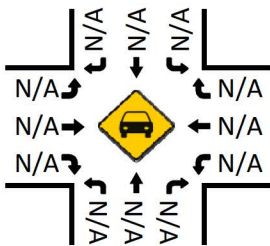
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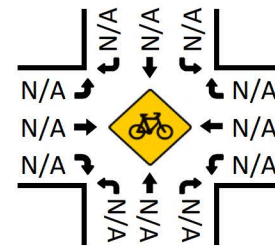
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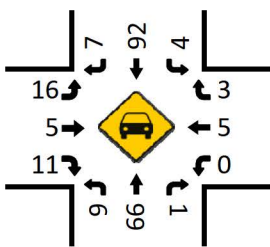
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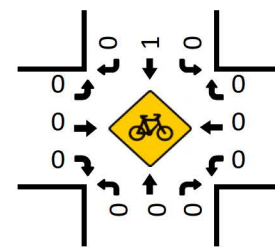
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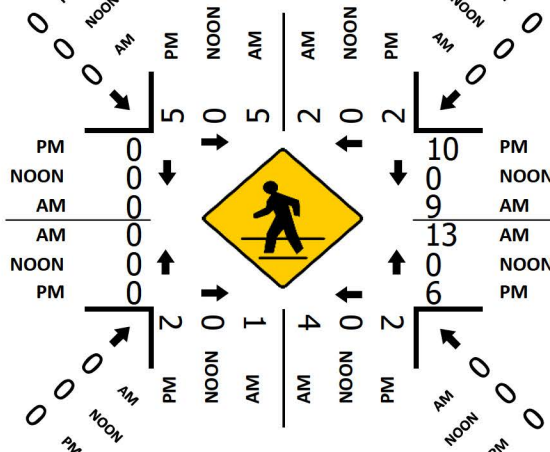
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

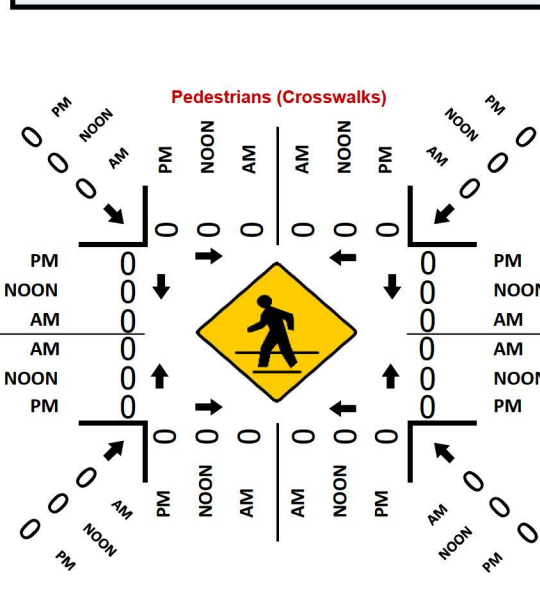
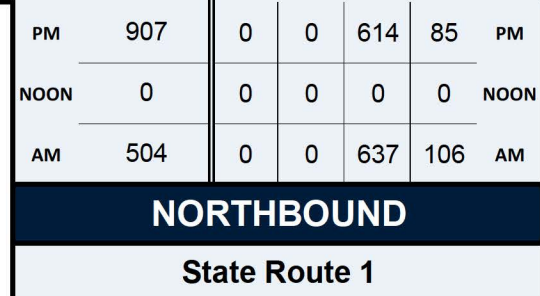
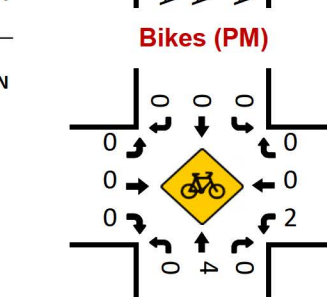
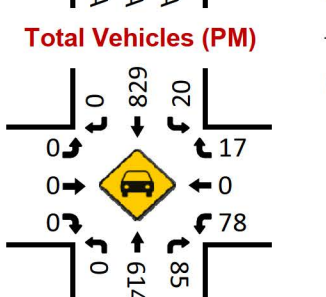
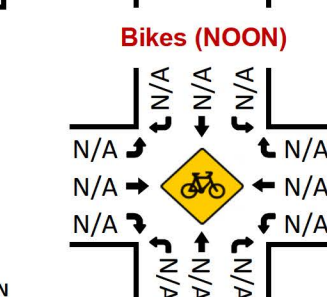
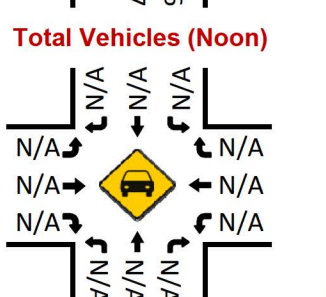
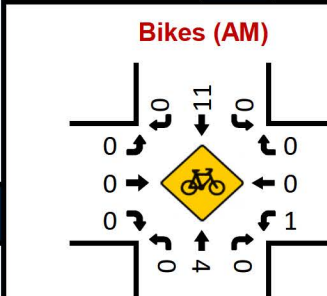
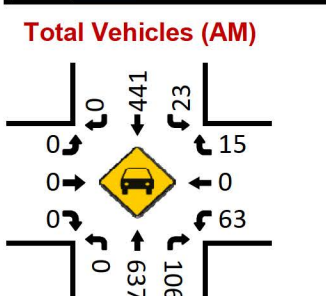
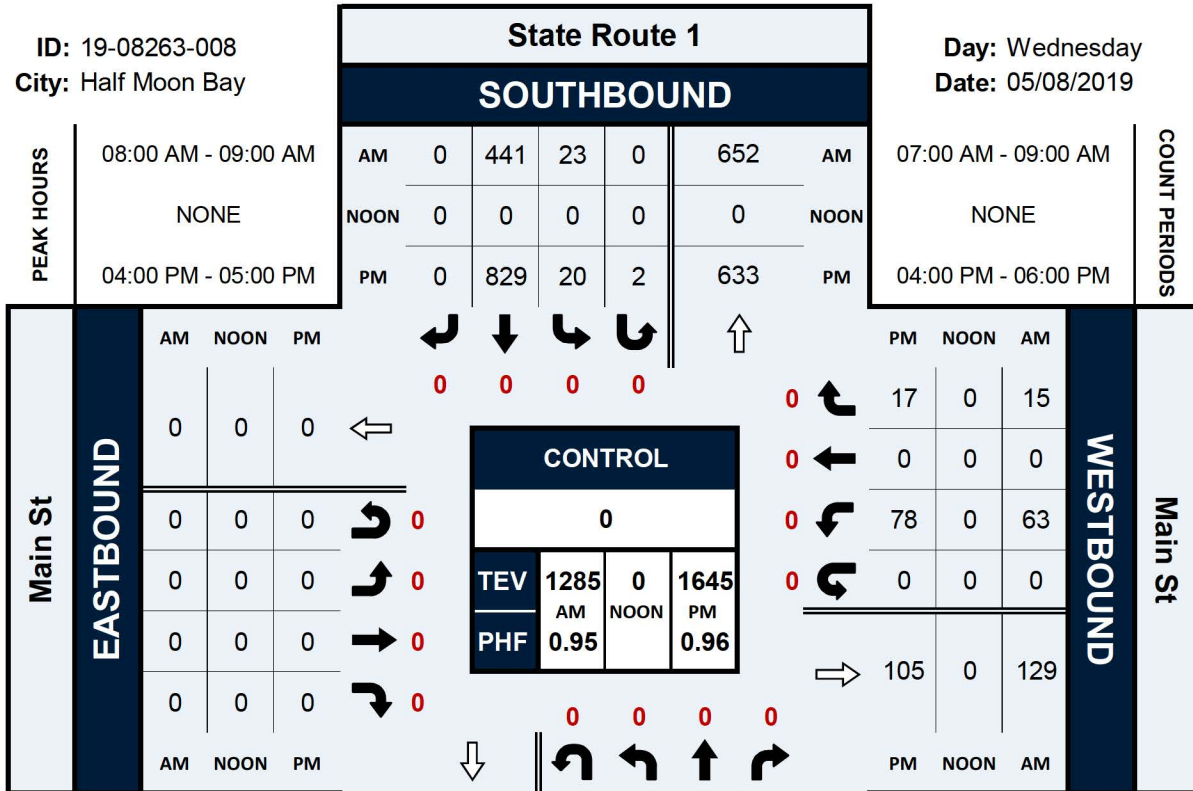


State Route 1 & Main St

Peak Hour Turning Movement Count

ID: 19-08263-008
City: Half Moon Bay

Day: Wednesday
Date: 05/08/2019

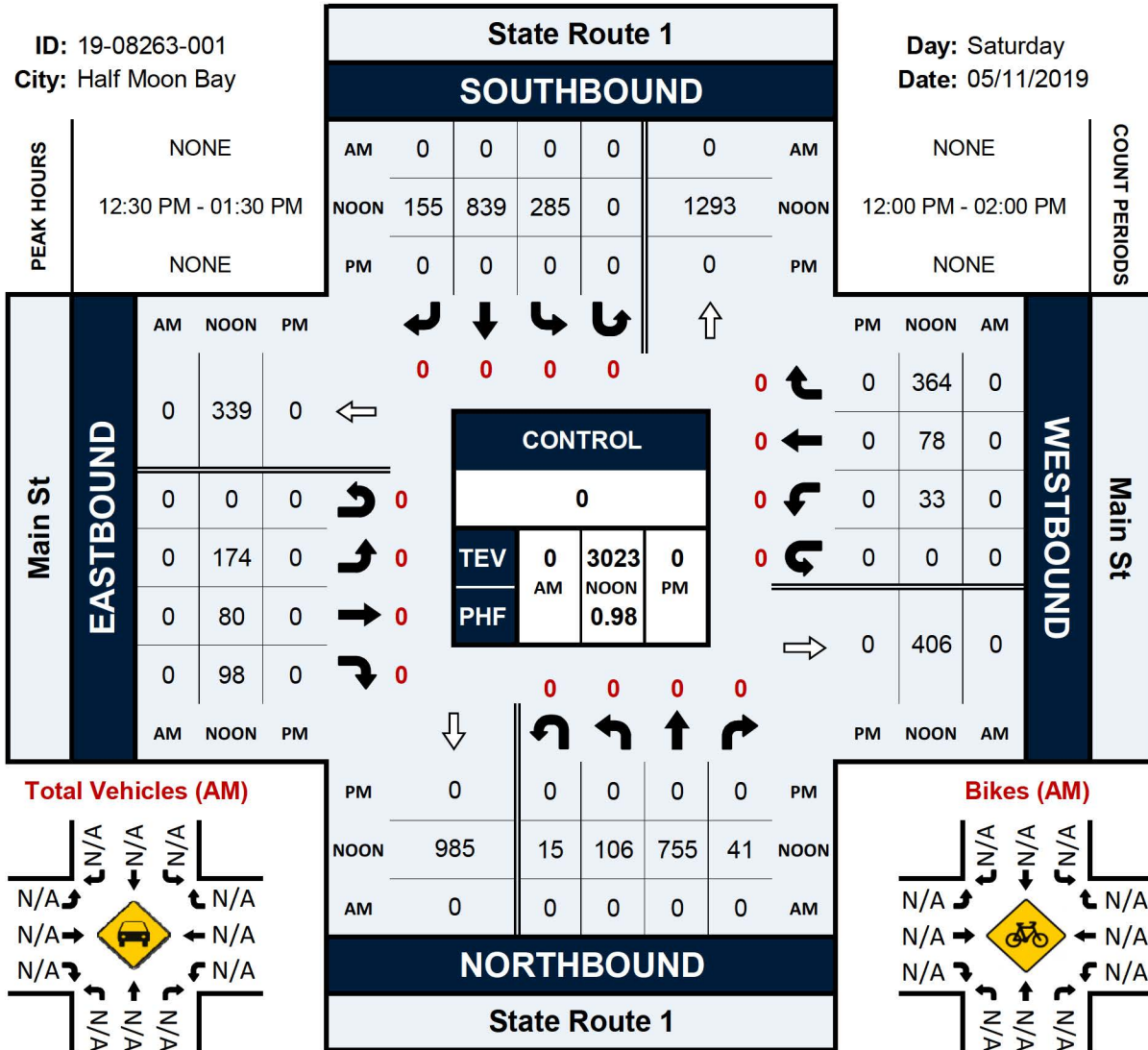


State Route 1 & Main St

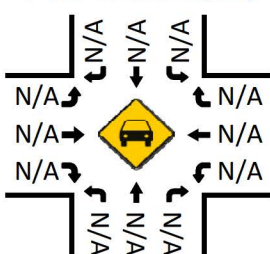
Peak Hour Turning Movement Count

ID: 19-08263-001
City: Half Moon Bay

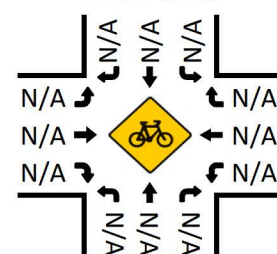
Day: Saturday
Date: 05/11/2019



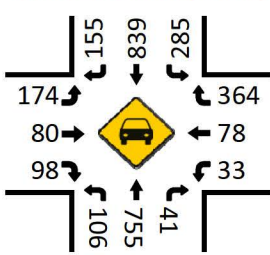
Total Vehicles (AM)



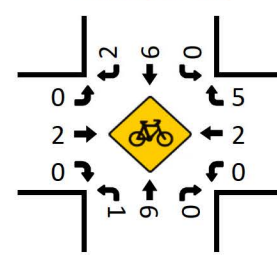
Bikes (AM)



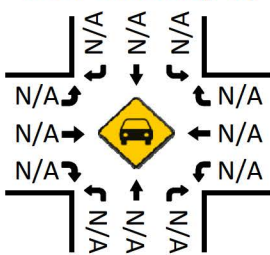
Total Vehicles (Noon)



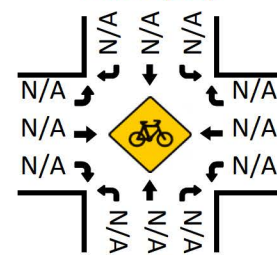
Bikes (NOON)



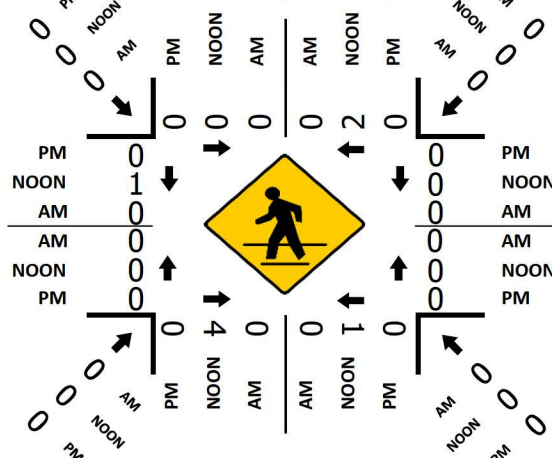
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

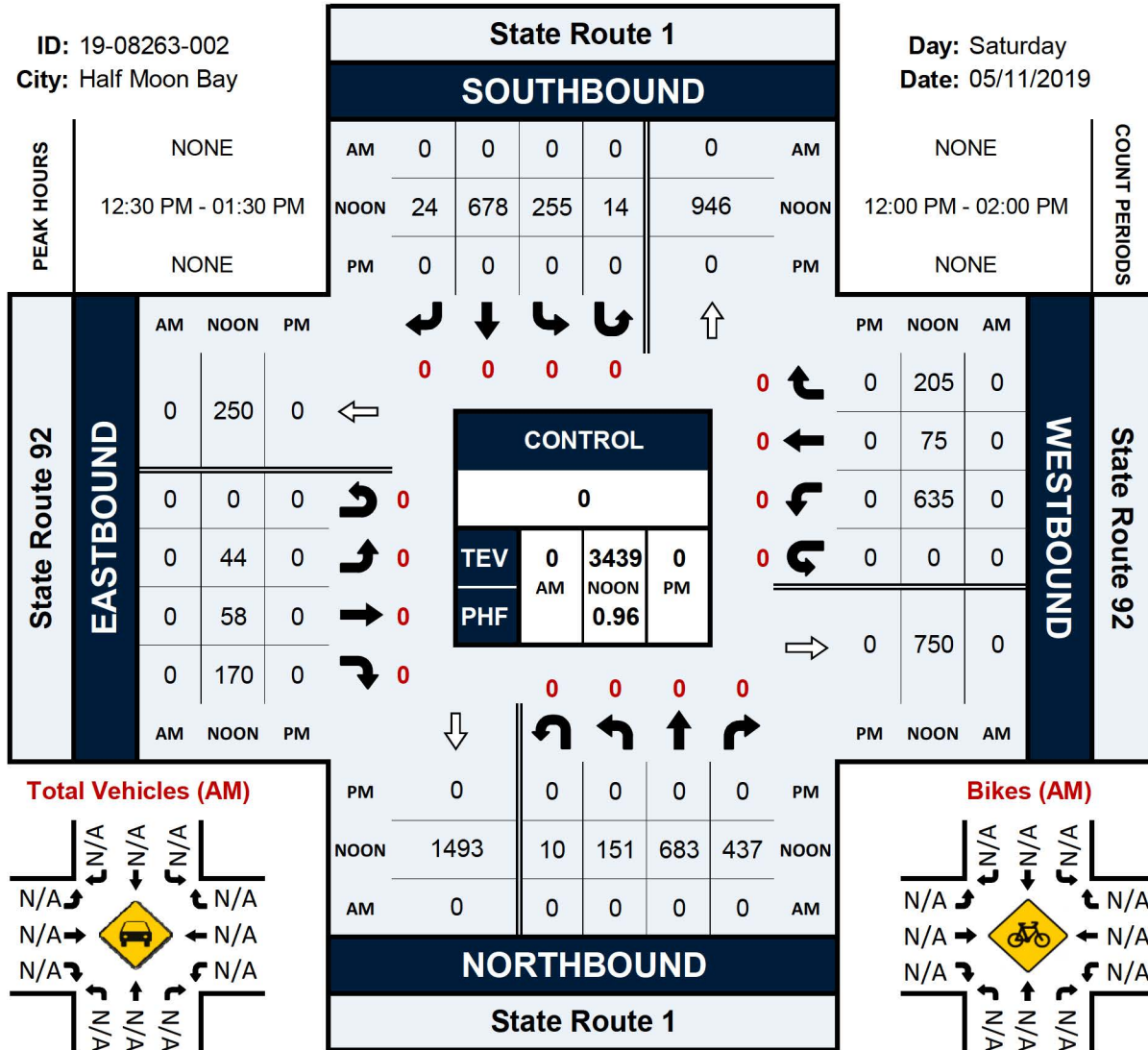


State Route 1 & State Route 92

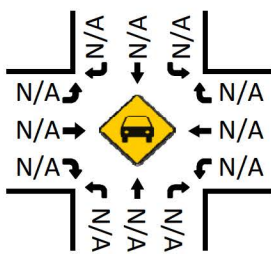
Peak Hour Turning Movement Count

ID: 19-08263-002
City: Half Moon Bay

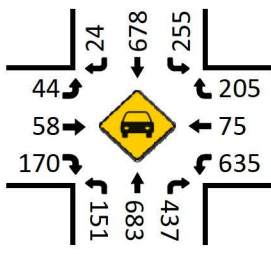
Day: Saturday
Date: 05/11/2019



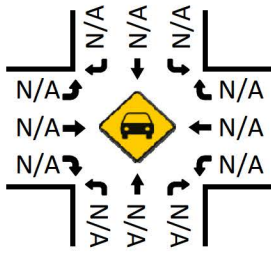
Total Vehicles (AM)



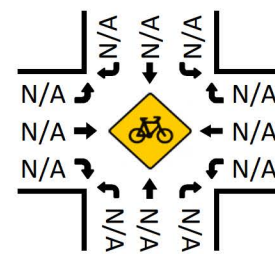
Total Vehicles (Noon)



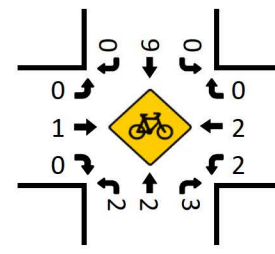
Total Vehicles (PM)



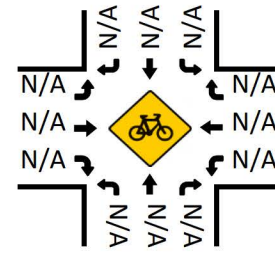
Bikes (AM)



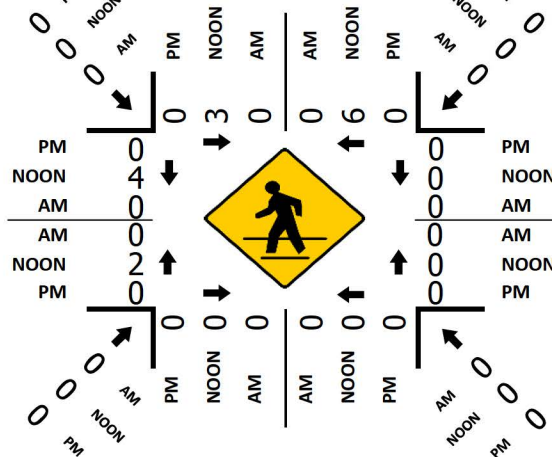
Bikes (NOON)



Bikes (PM)



Pedestrians (Crosswalks)

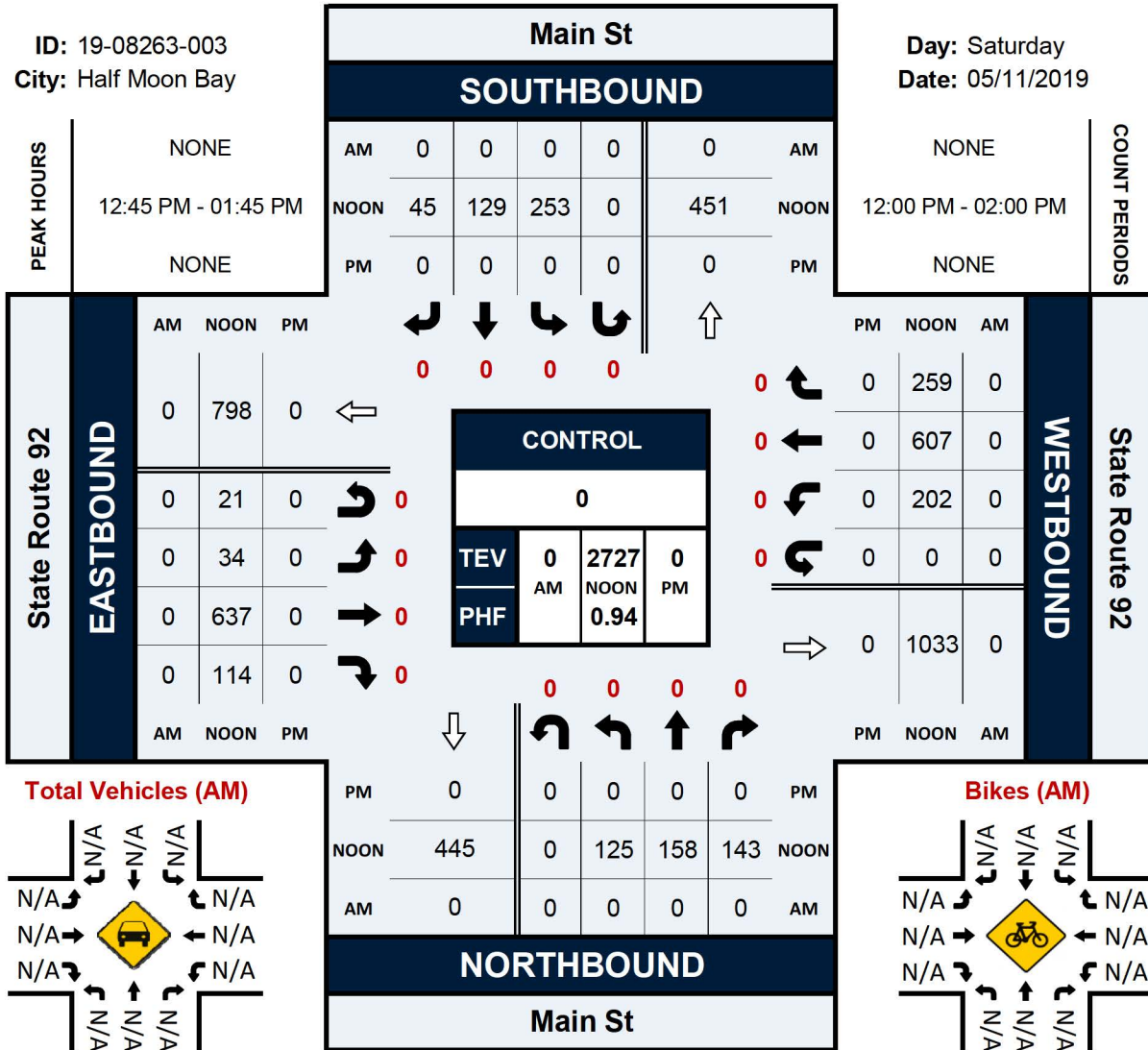


Main St & State Route 92

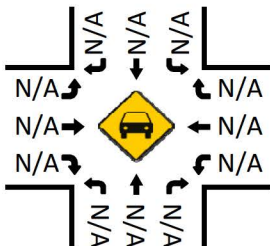
Peak Hour Turning Movement Count

ID: 19-08263-003
City: Half Moon Bay

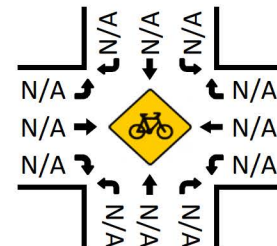
Day: Saturday
Date: 05/11/2019



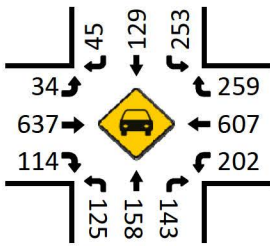
Total Vehicles (AM)



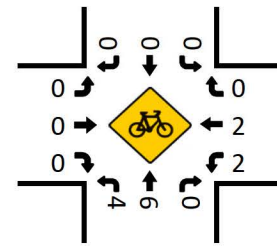
Bikes (AM)



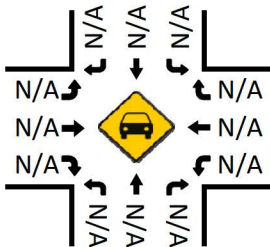
Total Vehicles (Noon)



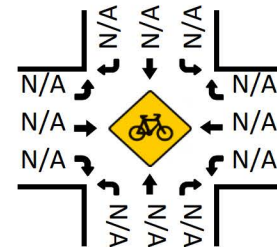
Bikes (NOON)



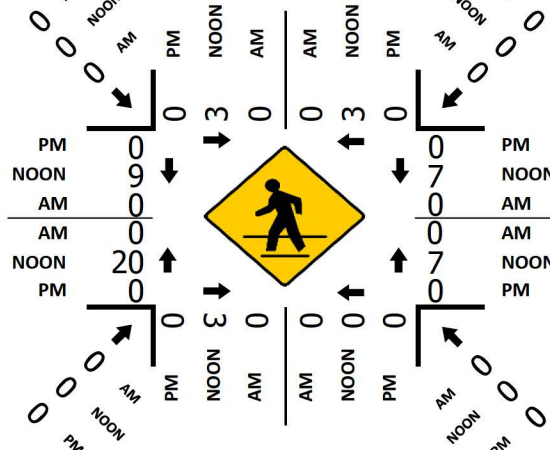
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

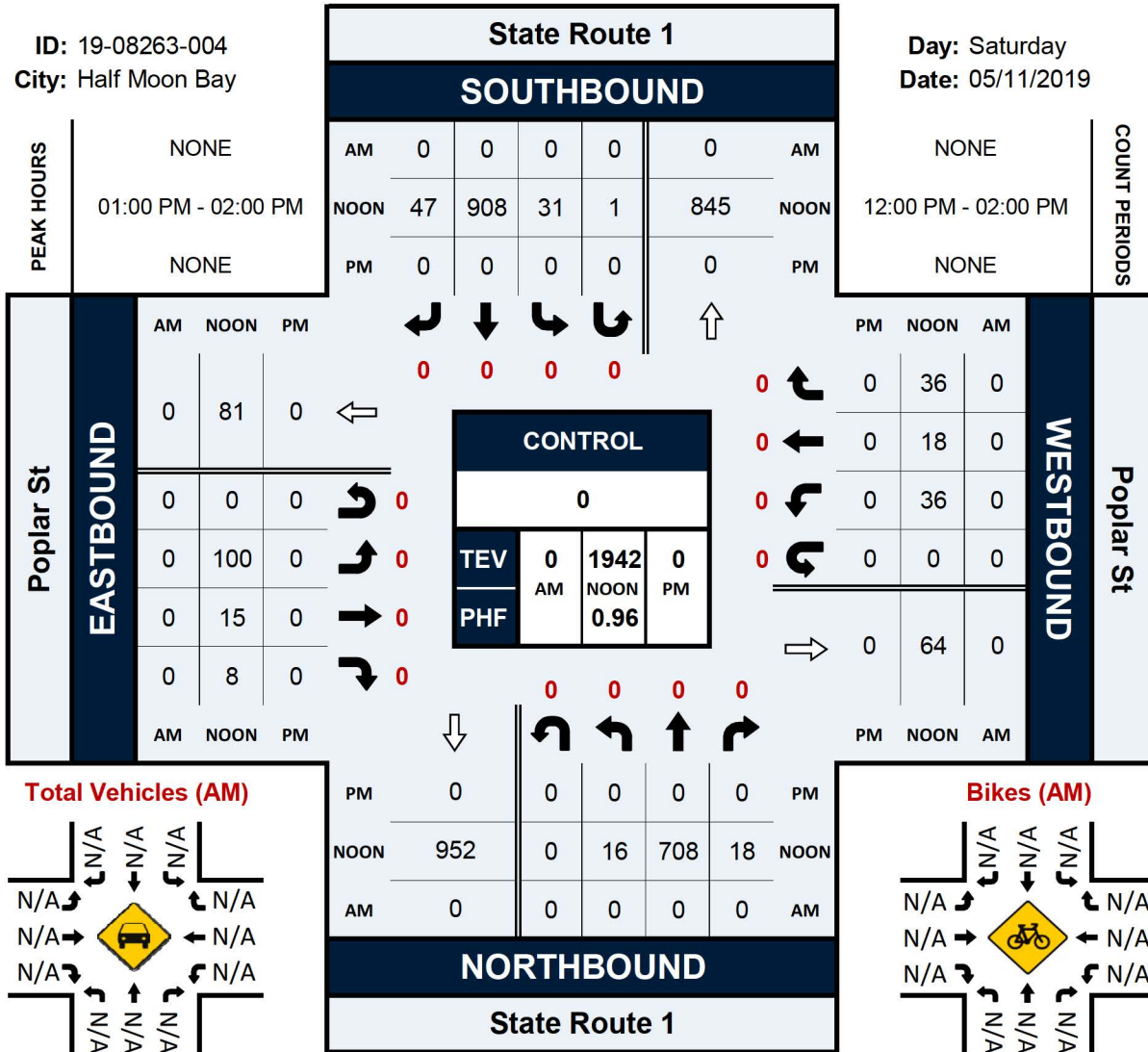


State Route 1 & Poplar St

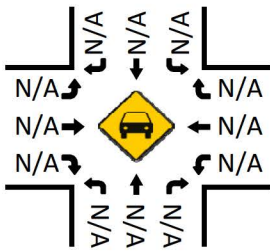
Peak Hour Turning Movement Count

ID: 19-08263-004
City: Half Moon Bay

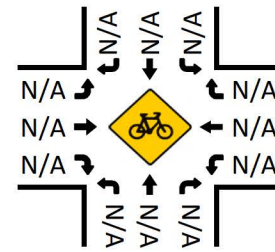
Day: Saturday
Date: 05/11/2019



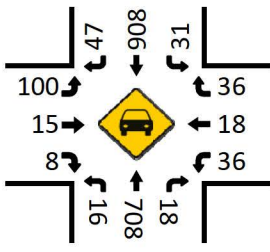
Total Vehicles (AM)



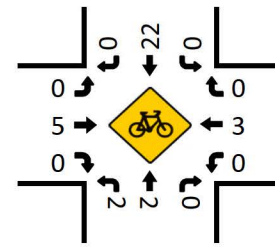
Bikes (AM)



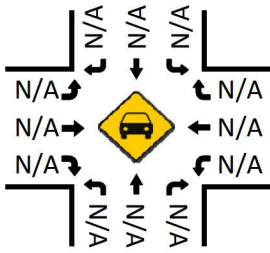
Total Vehicles (Noon)



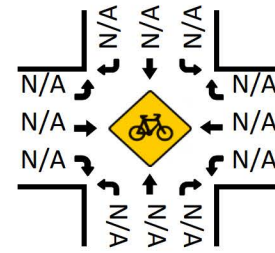
Bikes (NOON)



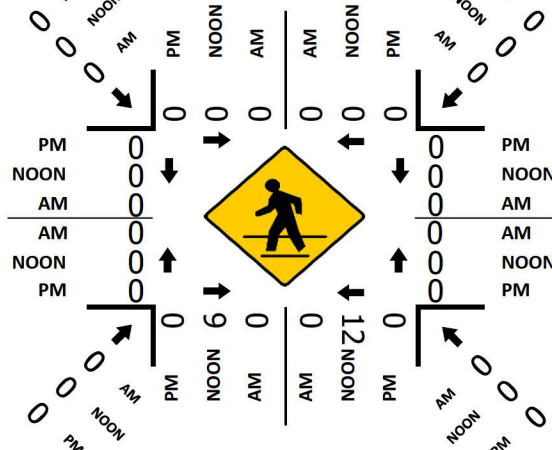
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

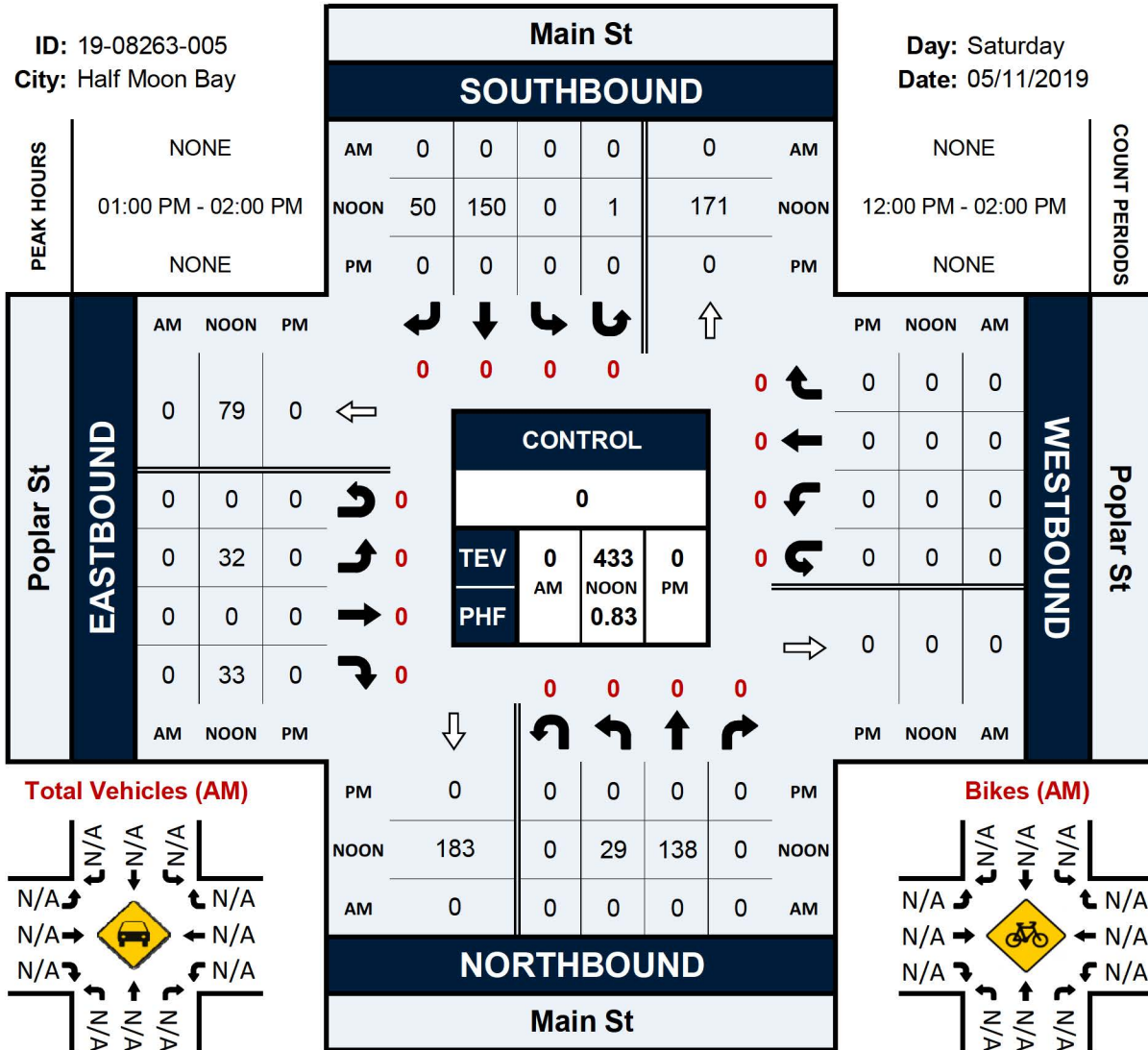


Main St & Poplar St

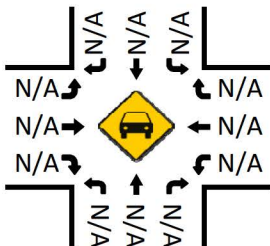
Peak Hour Turning Movement Count

ID: 19-08263-005
City: Half Moon Bay

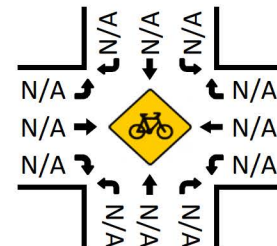
Day: Saturday
Date: 05/11/2019



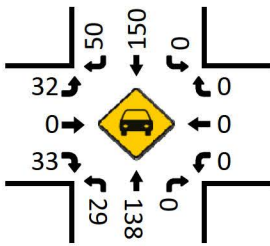
Total Vehicles (AM)



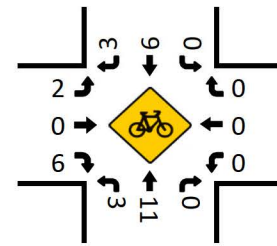
Bikes (AM)



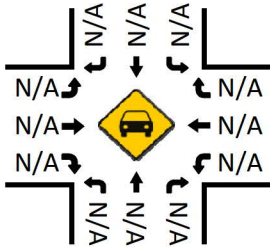
Total Vehicles (Noon)



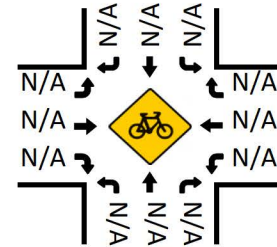
Bikes (NOON)



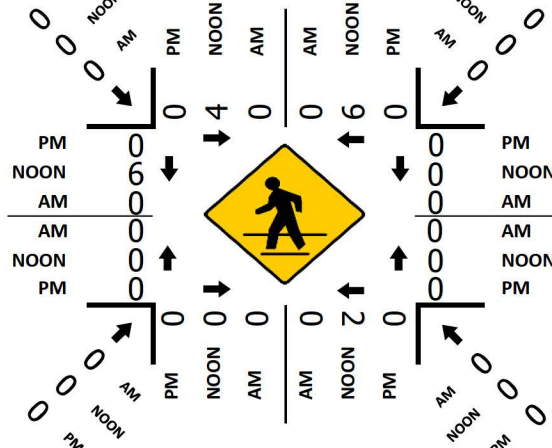
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

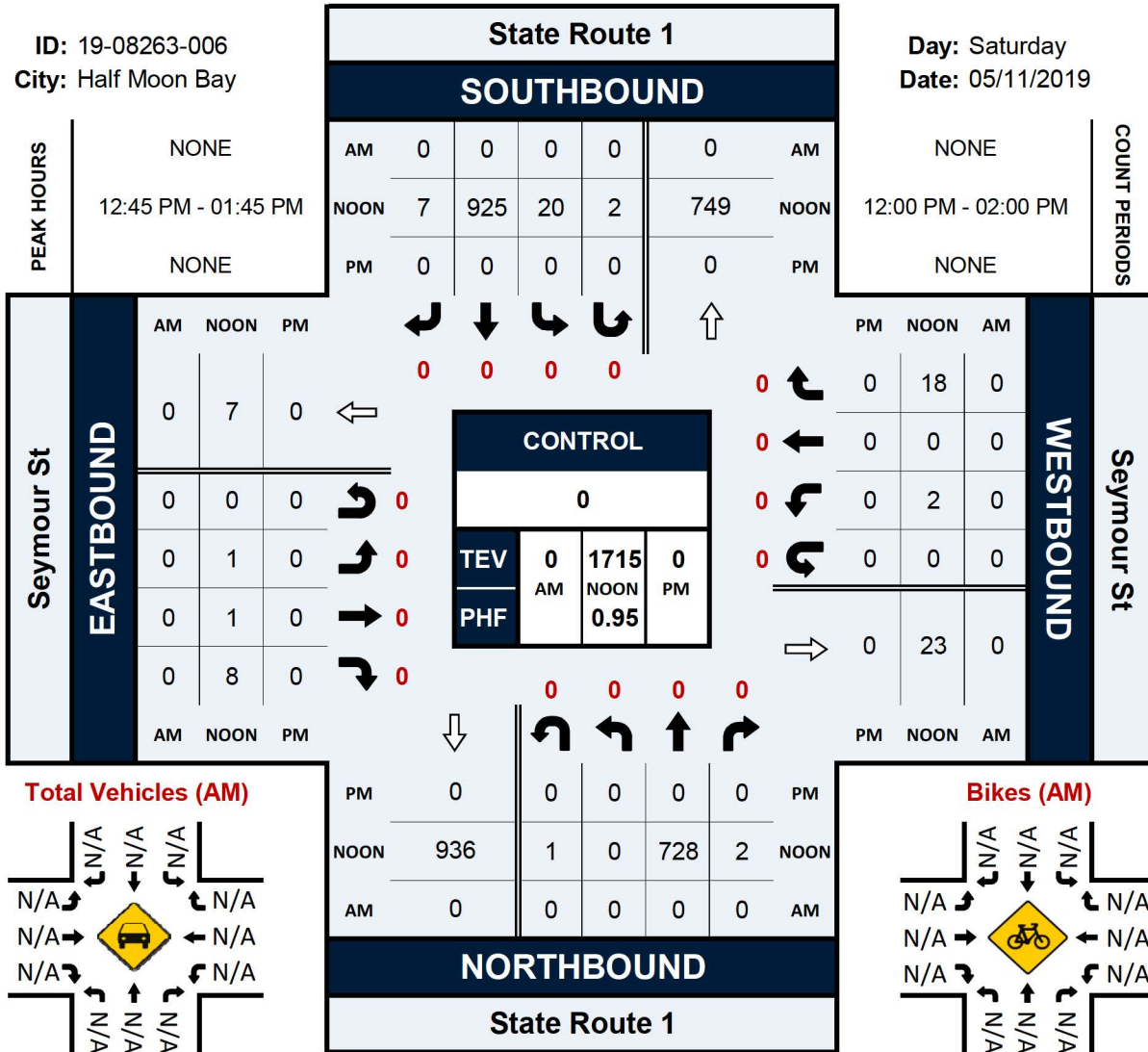


State Route 1 & Seymour St

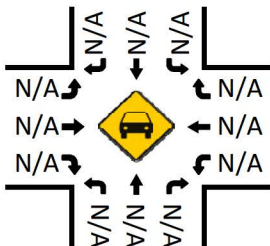
Peak Hour Turning Movement Count

ID: 19-08263-006
City: Half Moon Bay

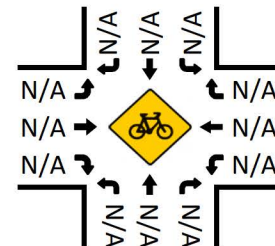
Day: Saturday
Date: 05/11/2019



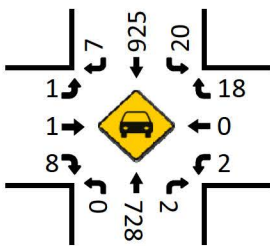
Total Vehicles (AM)



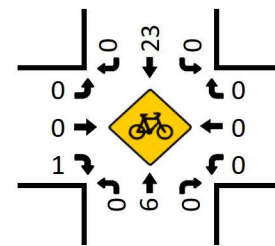
Bikes (AM)



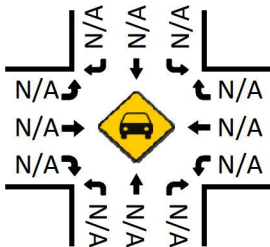
Total Vehicles (Noon)



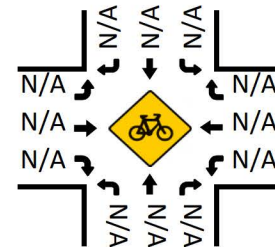
Bikes (NOON)



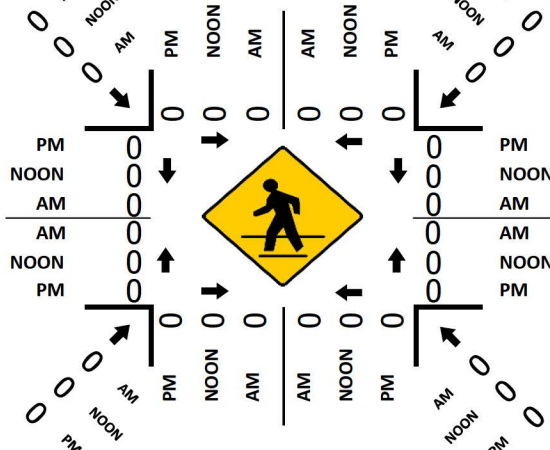
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

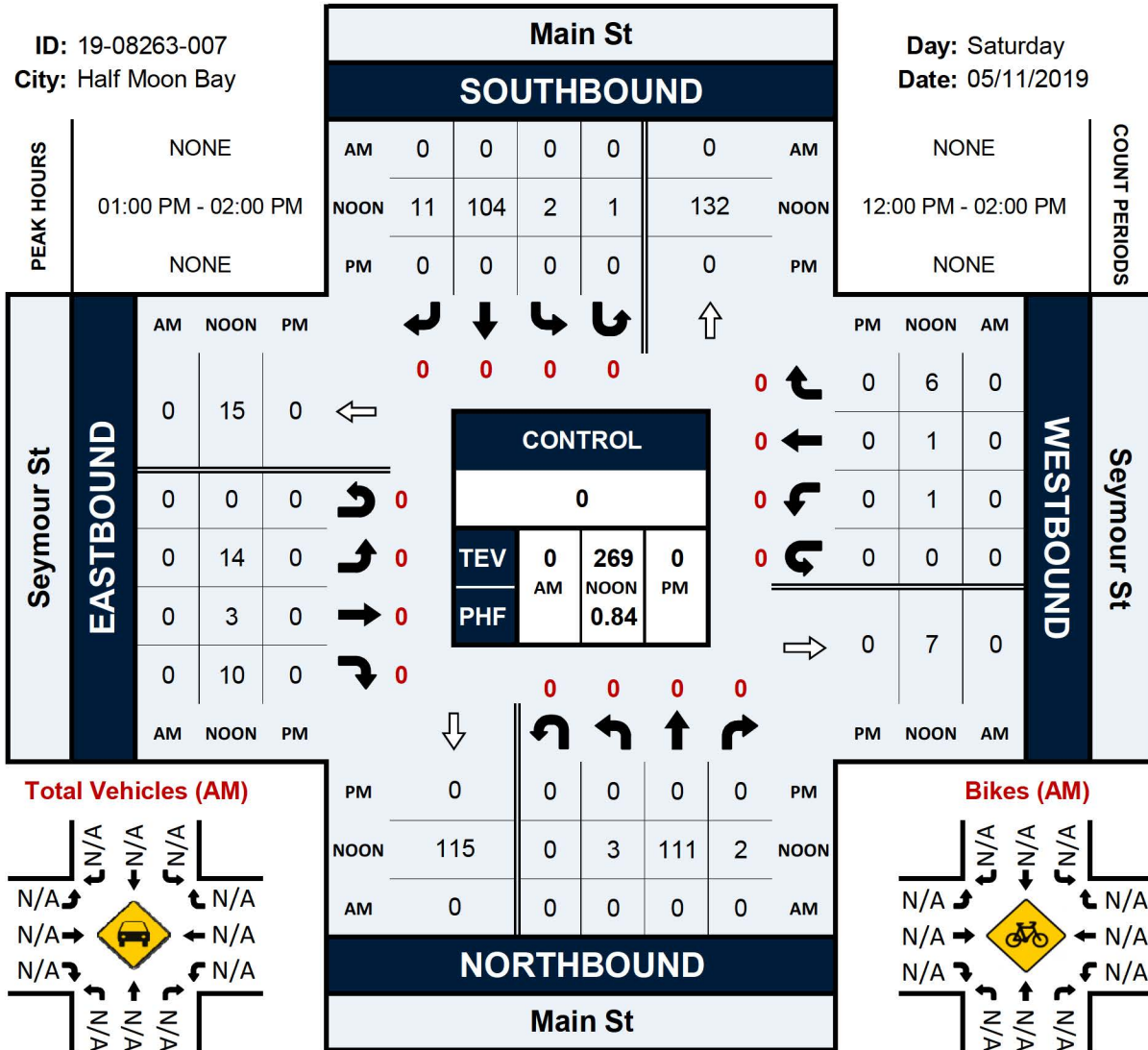


Main St & Seymour St

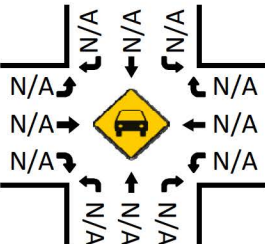
Peak Hour Turning Movement Count

ID: 19-08263-007
City: Half Moon Bay

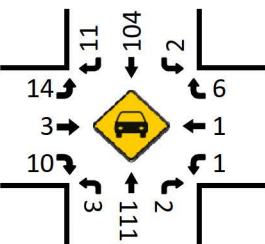
Day: Saturday
Date: 05/11/2019



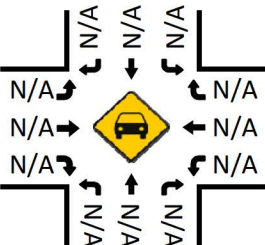
Total Vehicles (AM)



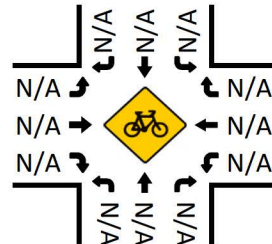
Total Vehicles (Noon)



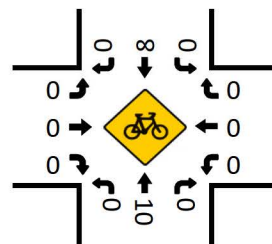
Total Vehicles (PM)



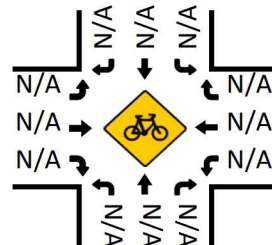
Bikes (AM)



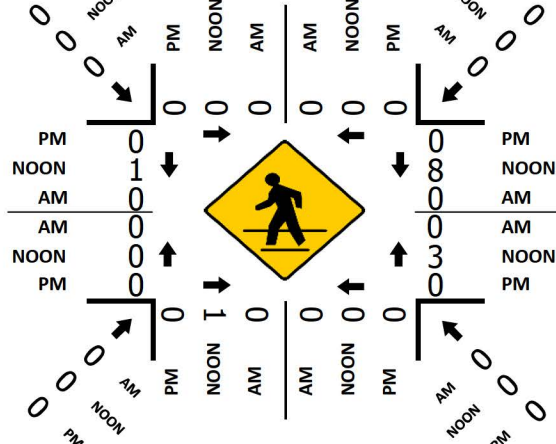
Bikes (NOON)



Bikes (PM)



Pedestrians (Crosswalks)

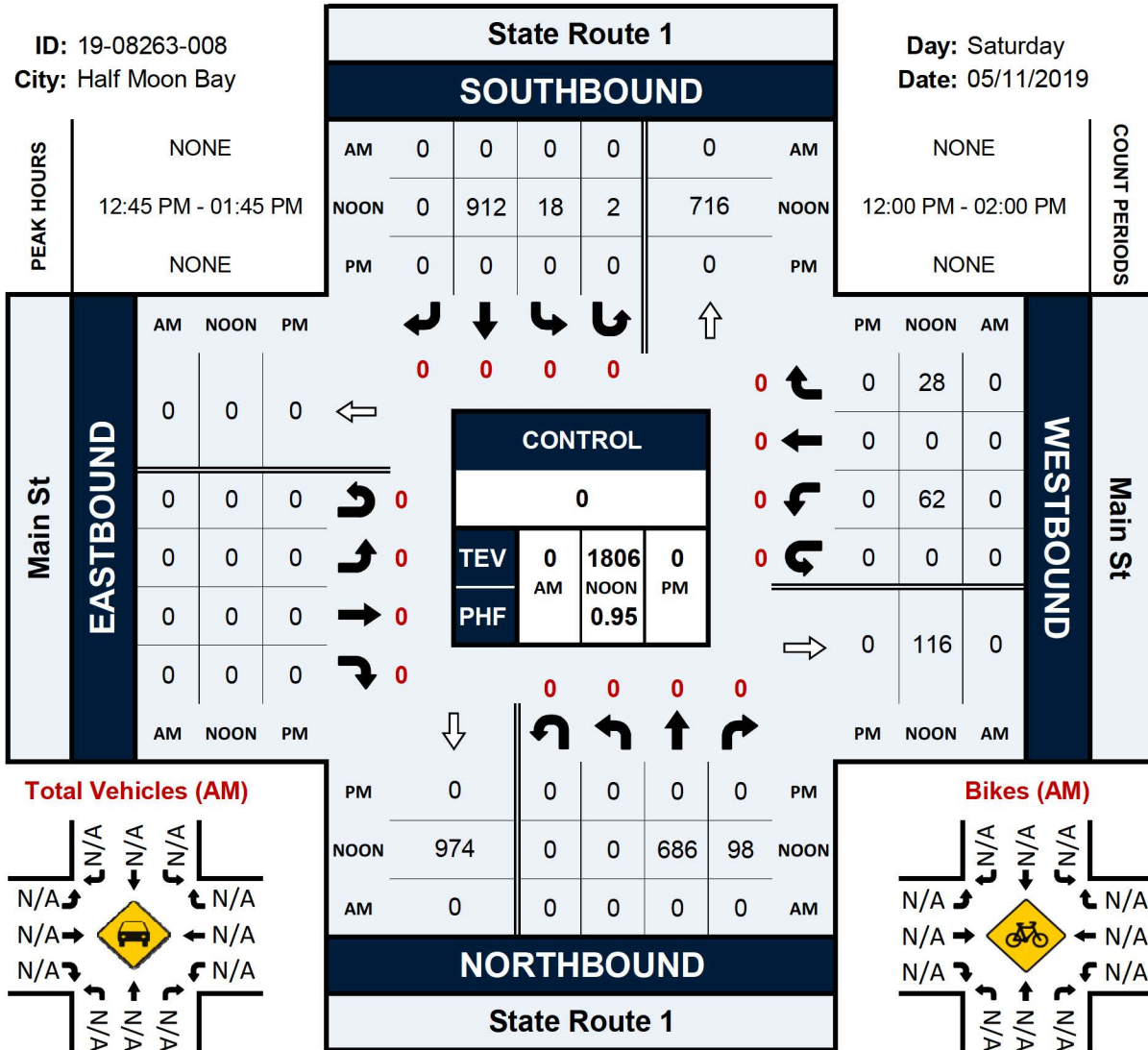


State Route 1 & Main St

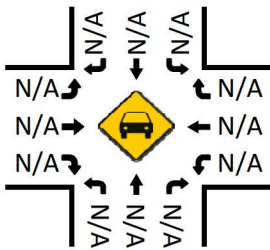
Peak Hour Turning Movement Count

ID: 19-08263-008
City: Half Moon Bay

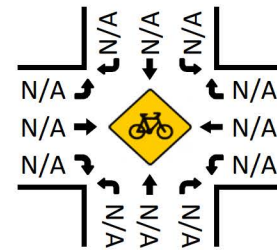
Day: Saturday
Date: 05/11/2019



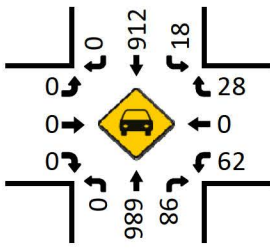
Total Vehicles (AM)



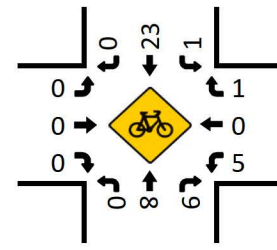
Bikes (AM)



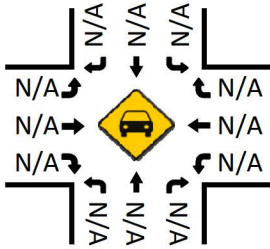
Total Vehicles (Noon)



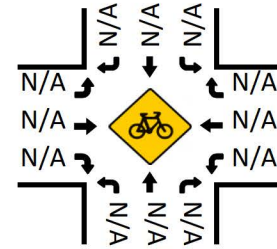
Bikes (NOON)



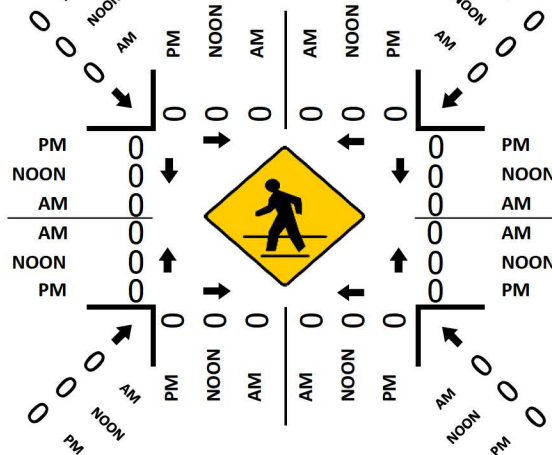
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

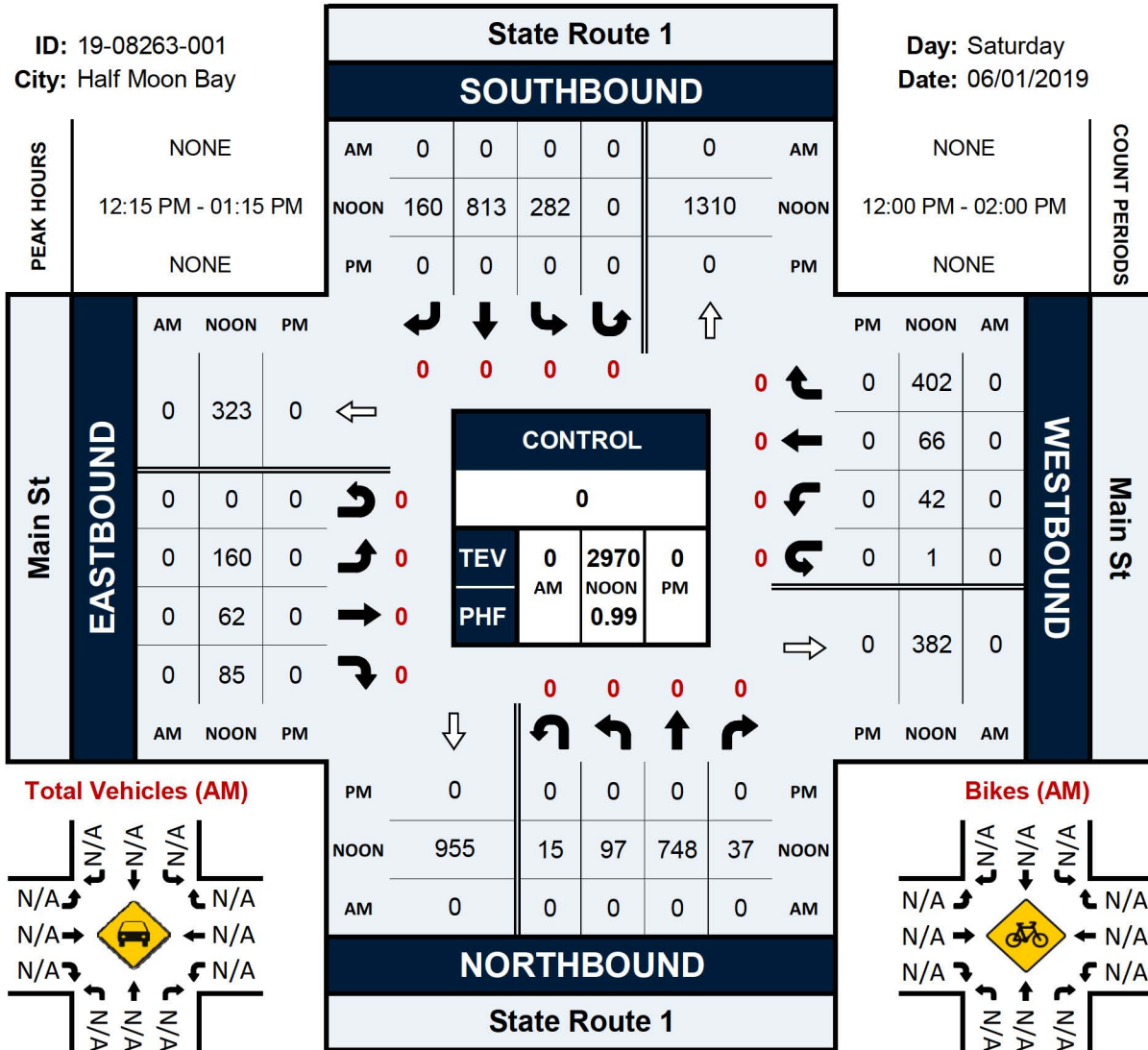


State Route 1 & Main St

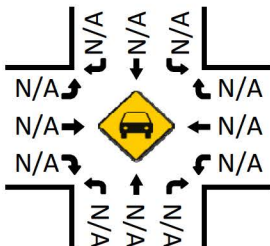
Peak Hour Turning Movement Count

ID: 19-08263-001
City: Half Moon Bay

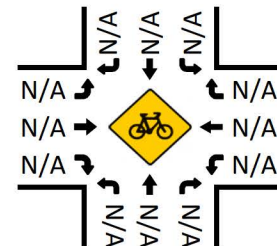
Day: Saturday
Date: 06/01/2019



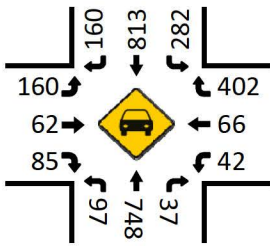
Total Vehicles (AM)



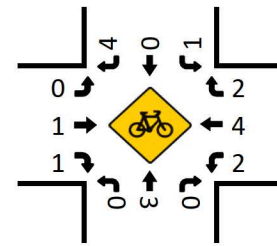
Bikes (AM)



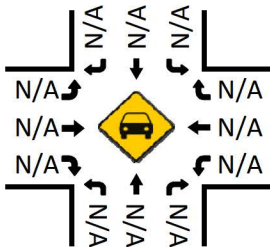
Total Vehicles (Noon)



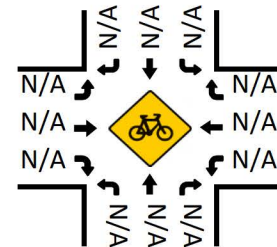
Bikes (NOON)



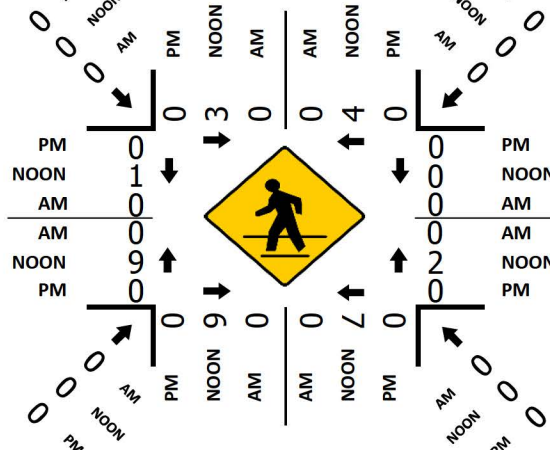
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

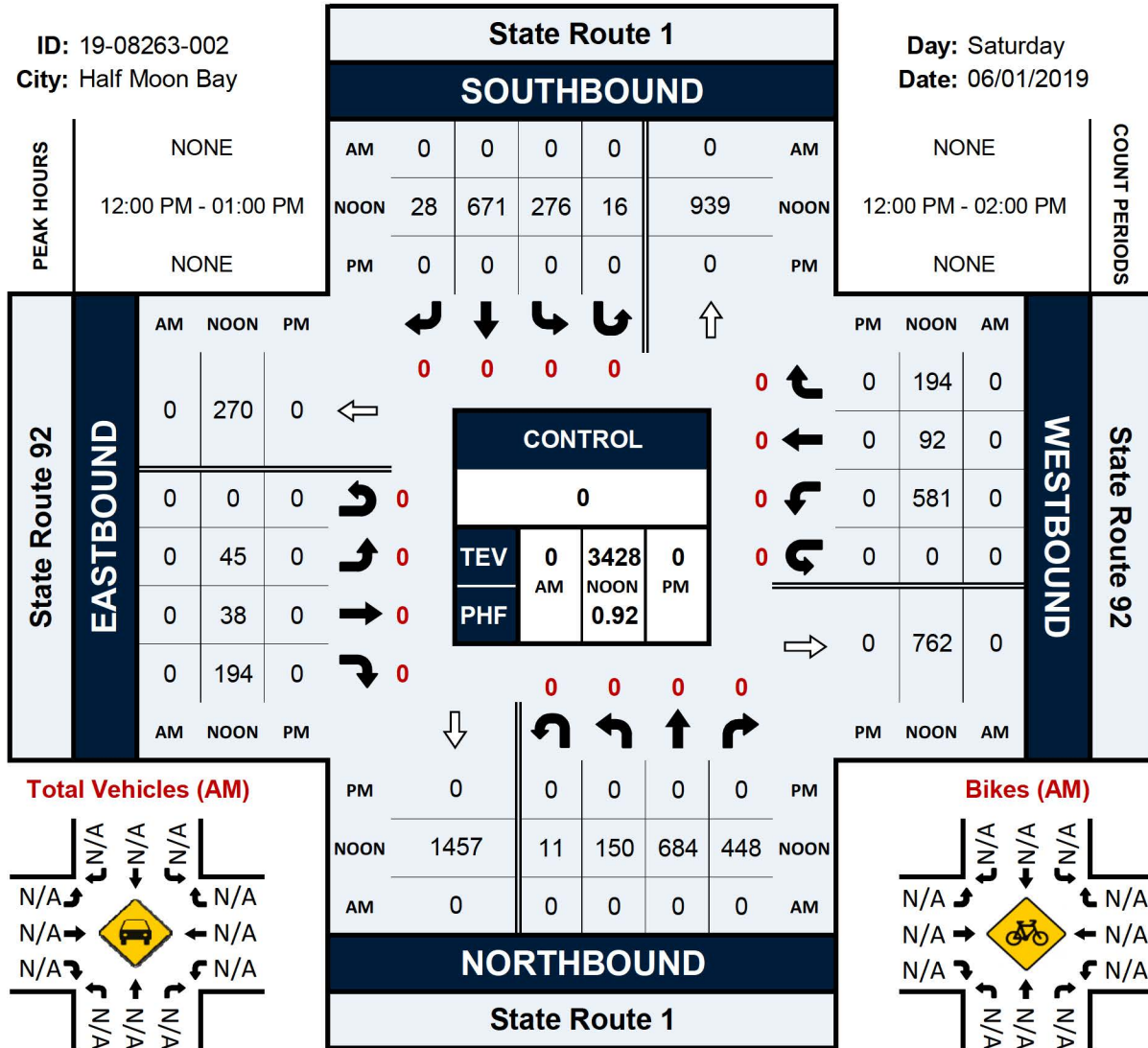


State Route 1 & State Route 92

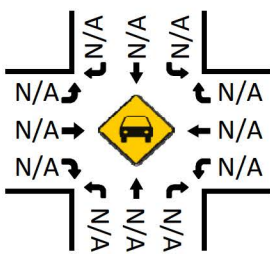
Peak Hour Turning Movement Count

ID: 19-08263-002
City: Half Moon Bay

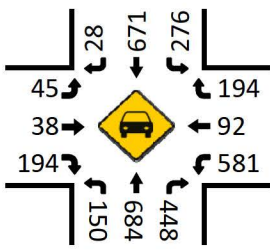
Day: Saturday
Date: 06/01/2019



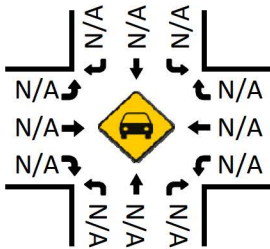
Total Vehicles (AM)



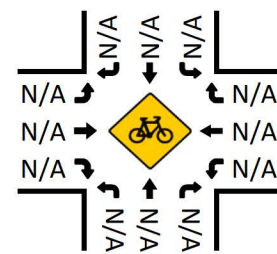
Total Vehicles (Noon)



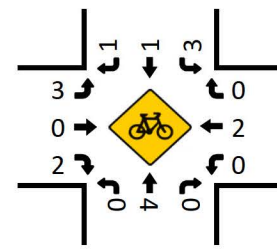
Total Vehicles (PM)



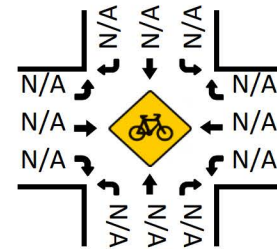
Bikes (AM)



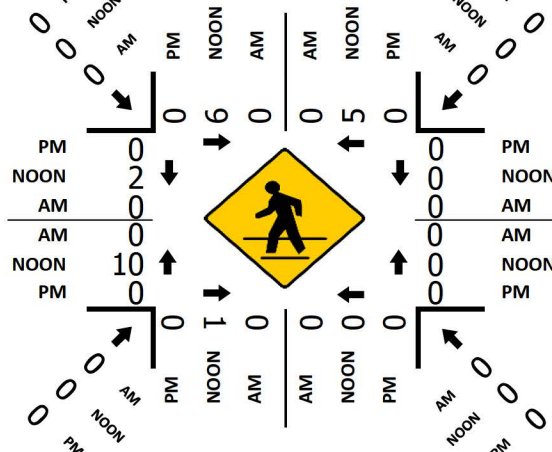
Bikes (NOON)



Bikes (PM)



Pedestrians (Crosswalks)

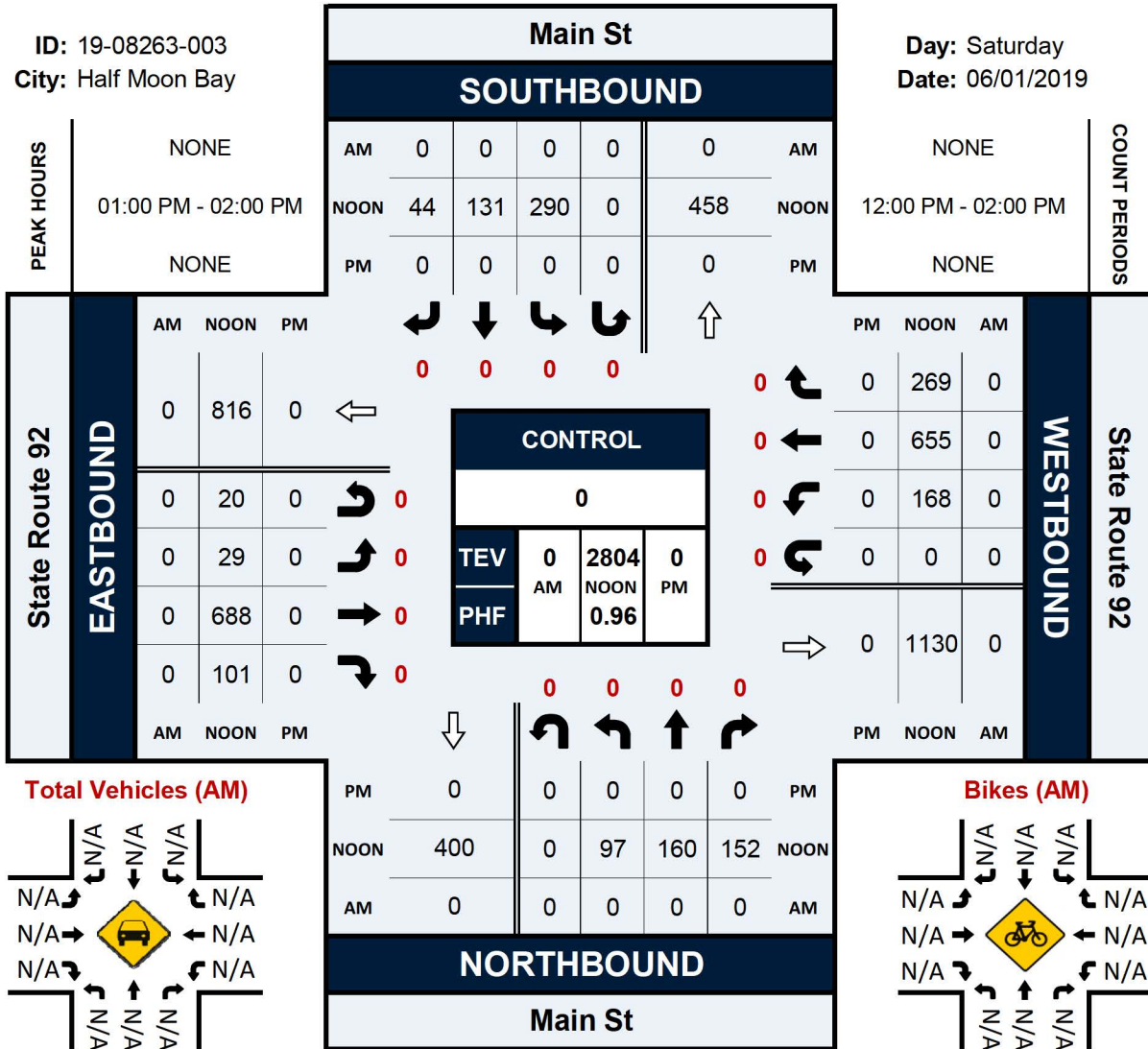


Main St & State Route 92

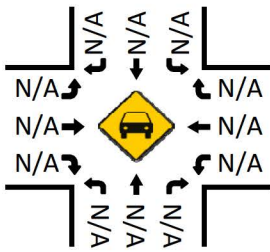
Peak Hour Turning Movement Count

ID: 19-08263-003
City: Half Moon Bay

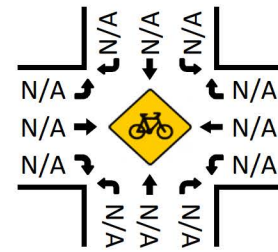
Day: Saturday
Date: 06/01/2019



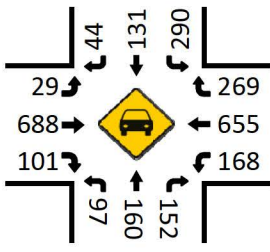
Total Vehicles (AM)



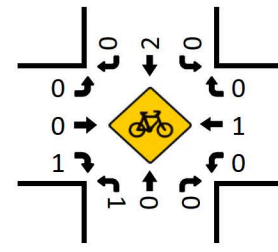
Bikes (AM)



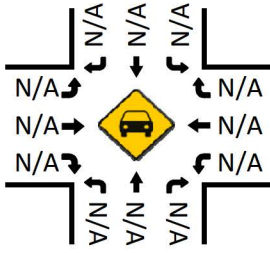
Total Vehicles (Noon)



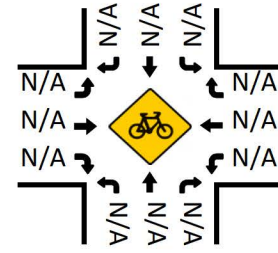
Bikes (NOON)



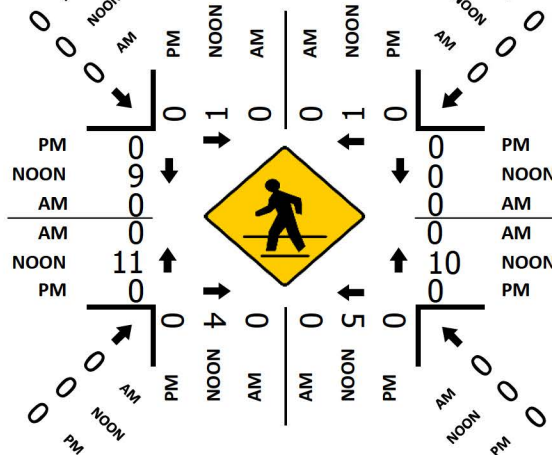
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

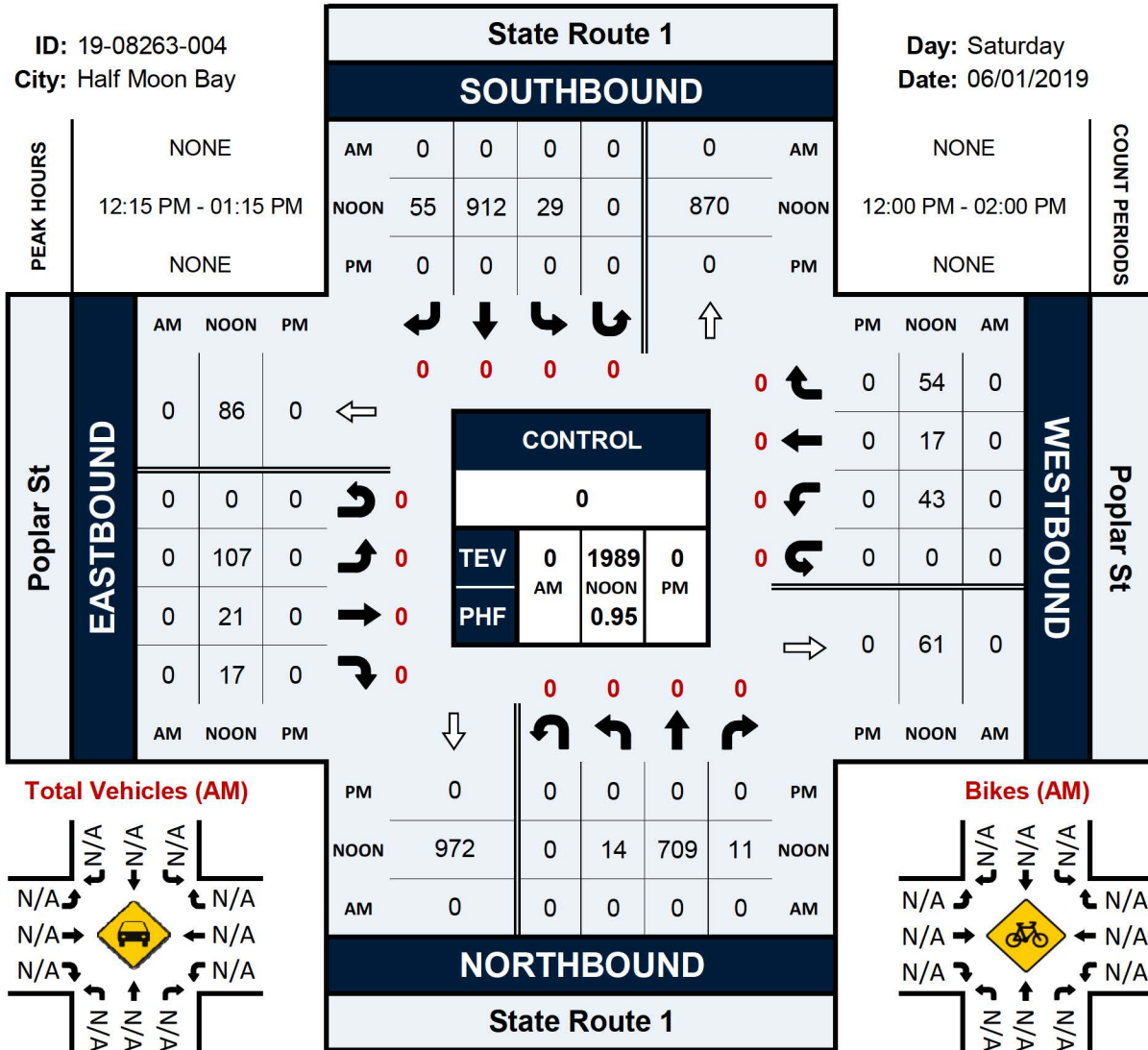


State Route 1 & Poplar St

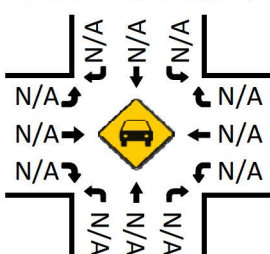
Peak Hour Turning Movement Count

ID: 19-08263-004
City: Half Moon Bay

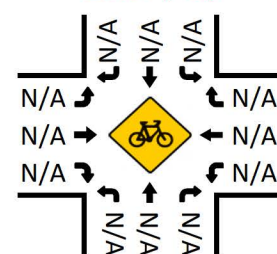
Day: Saturday
Date: 06/01/2019



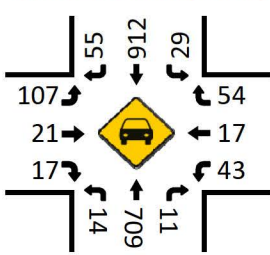
Total Vehicles (AM)



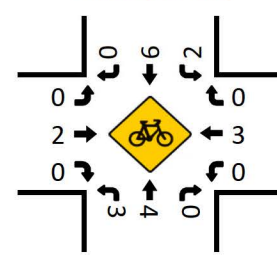
Bikes (AM)



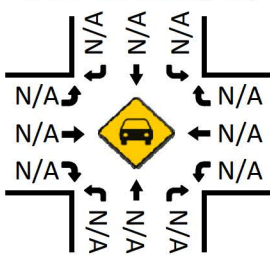
Total Vehicles (Noon)



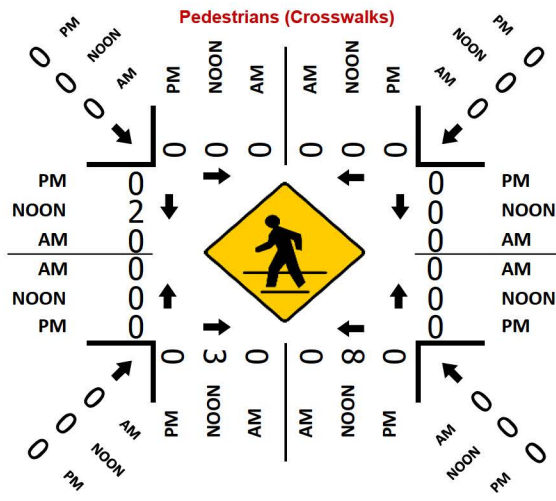
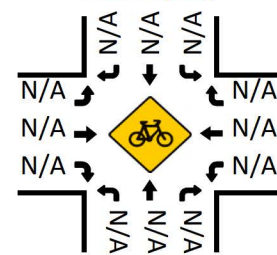
Bikes (NOON)



Total Vehicles (PM)



Bikes (PM)

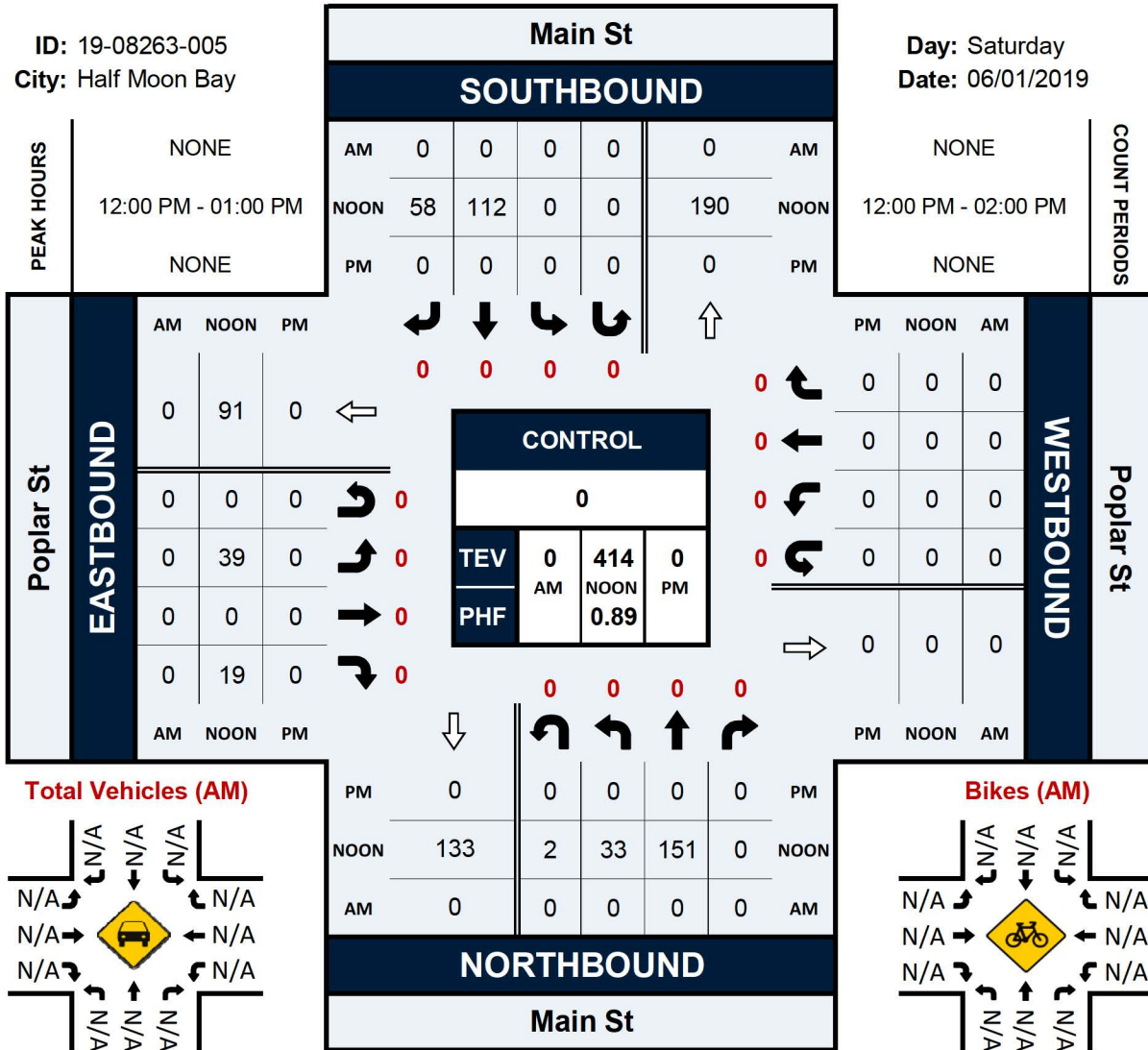


Main St & Poplar St

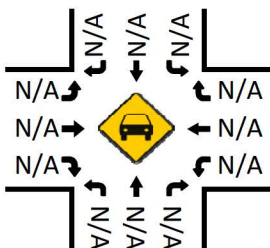
Peak Hour Turning Movement Count

ID: 19-08263-005
City: Half Moon Bay

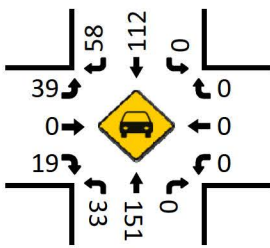
Day: Saturday
Date: 06/01/2019



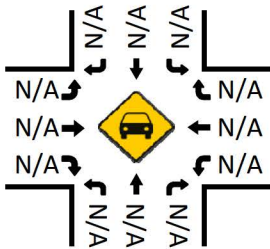
Total Vehicles (AM)



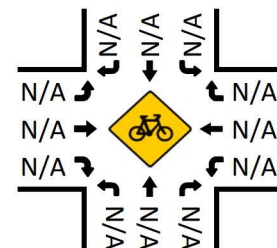
Total Vehicles (Noon)



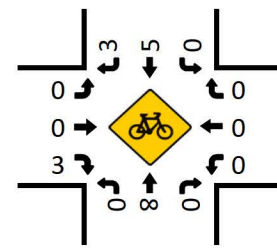
Total Vehicles (PM)



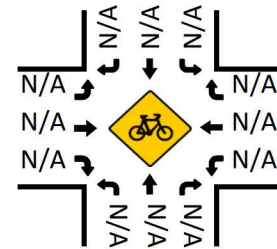
Bikes (AM)



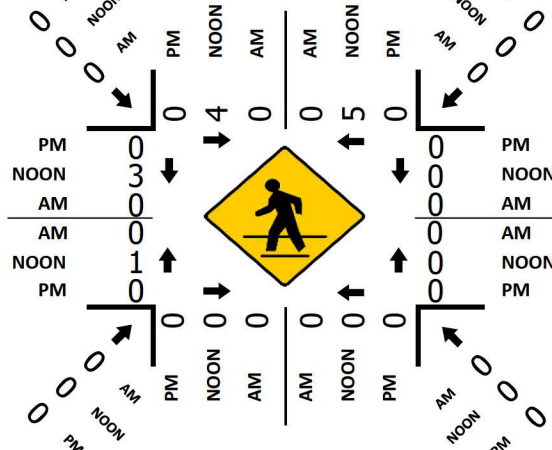
Bikes (NOON)



Bikes (PM)



Pedestrians (Crosswalks)

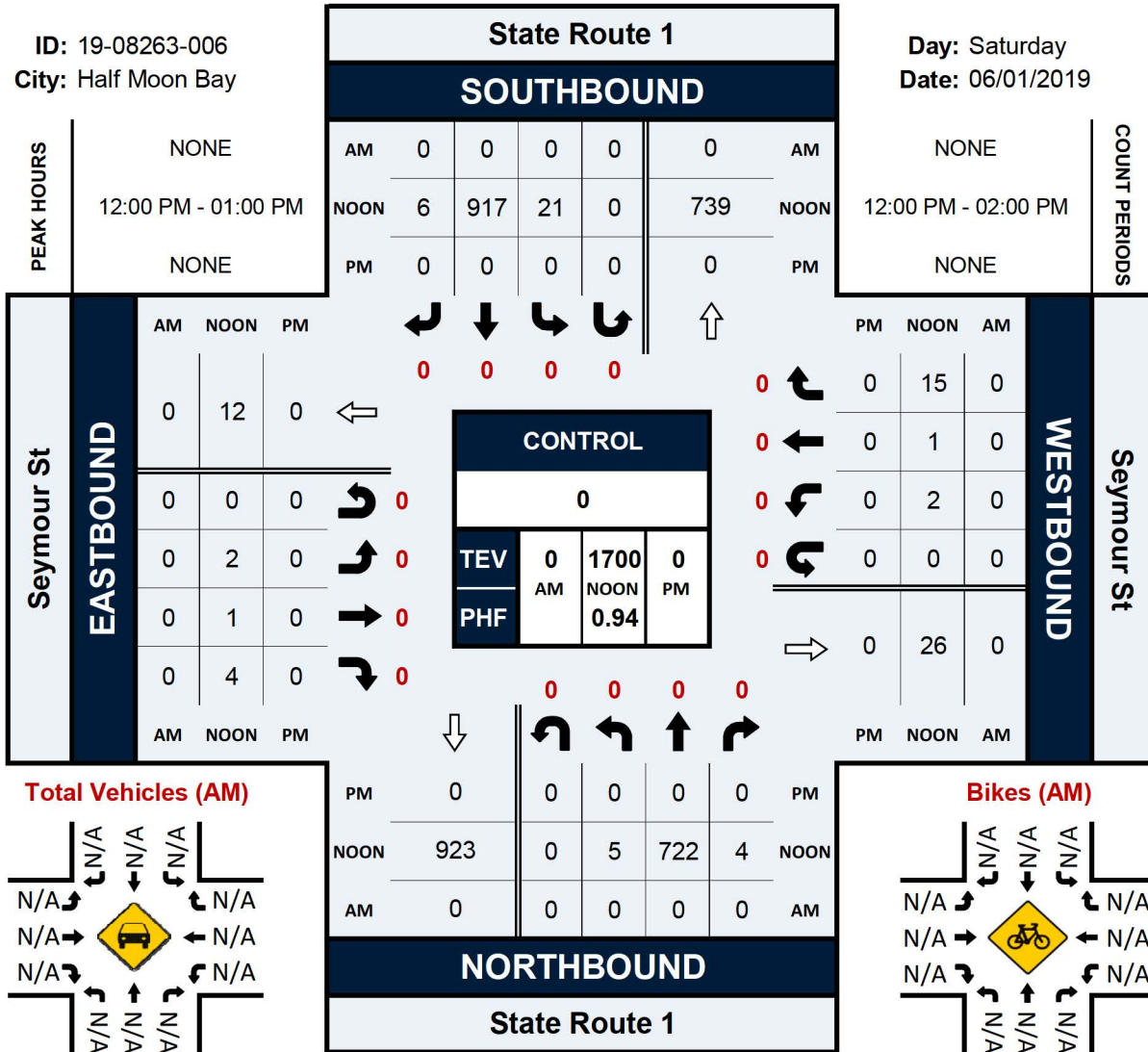


State Route 1 & Seymour St

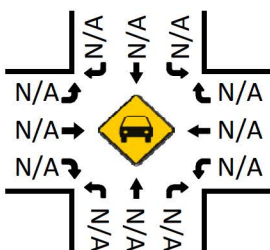
Peak Hour Turning Movement Count

ID: 19-08263-006
City: Half Moon Bay

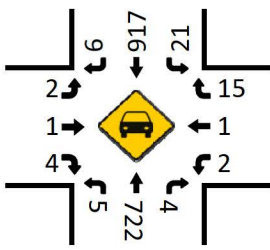
Day: Saturday
Date: 06/01/2019



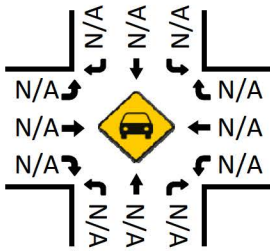
Total Vehicles (AM)



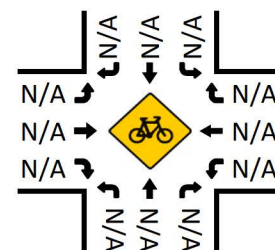
Total Vehicles (Noon)



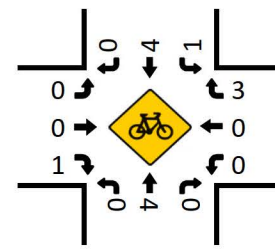
Total Vehicles (PM)



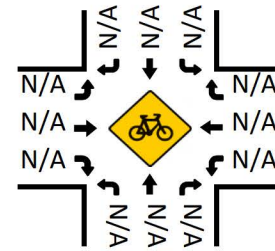
Bikes (AM)



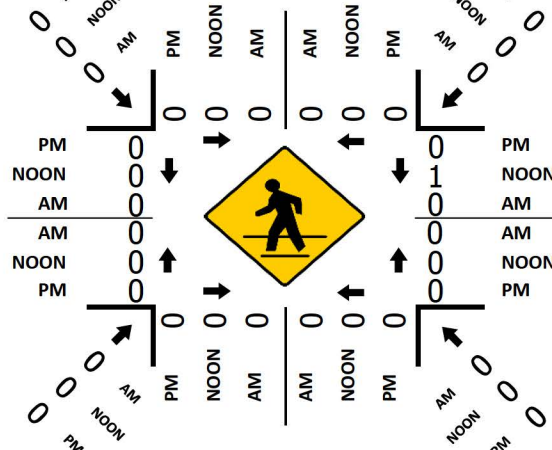
Bikes (NOON)



Bikes (PM)



Pedestrians (Crosswalks)

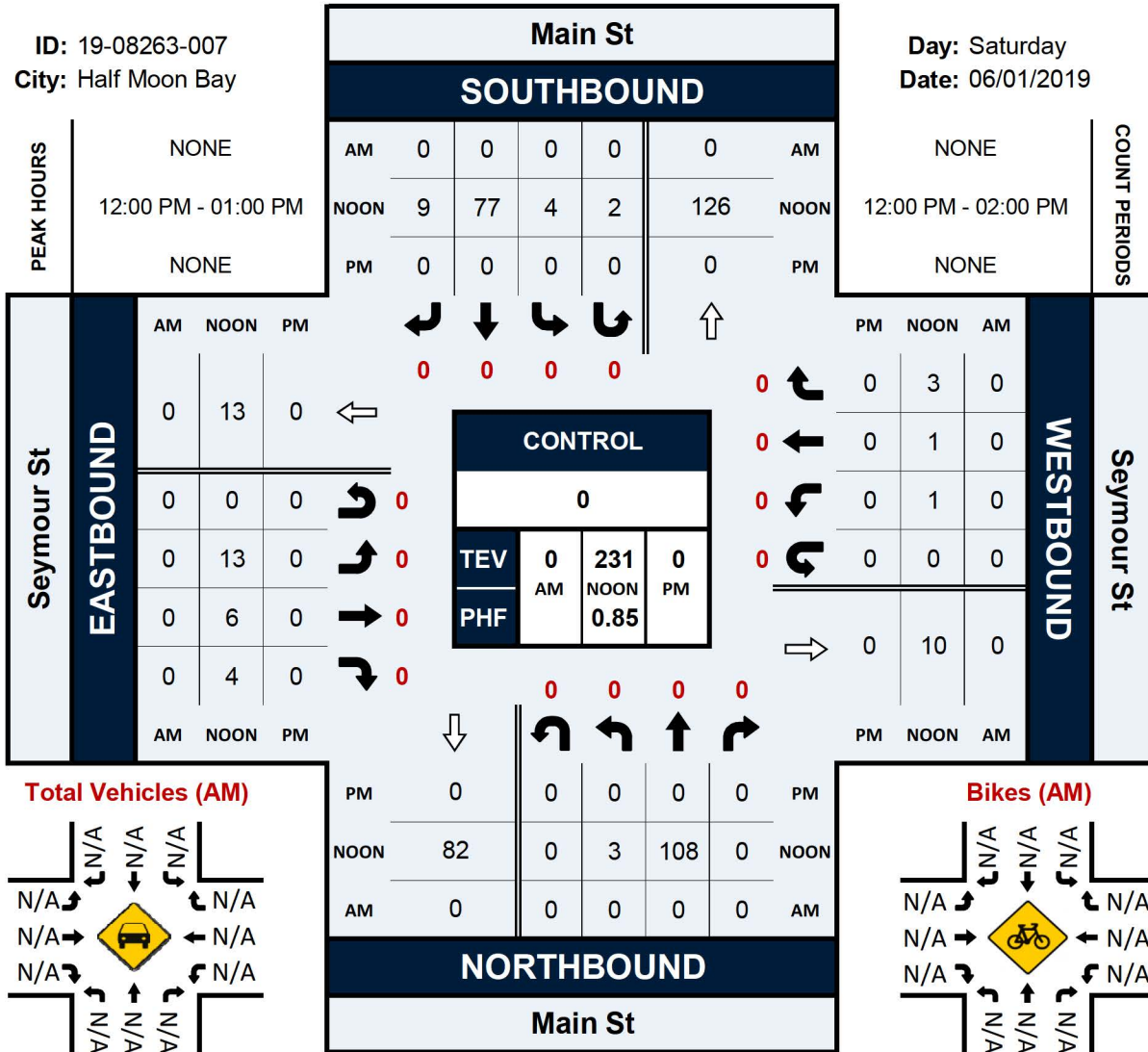


Main St & Seymour St

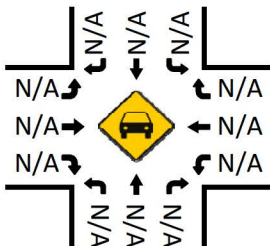
Peak Hour Turning Movement Count

ID: 19-08263-007
City: Half Moon Bay

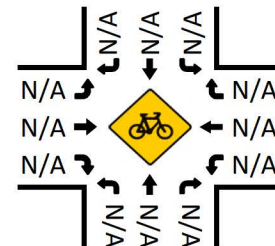
Day: Saturday
Date: 06/01/2019



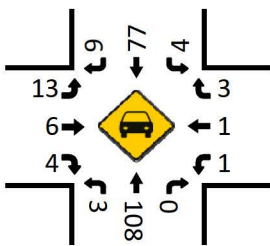
Total Vehicles (AM)



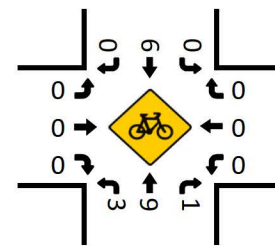
Bikes (AM)



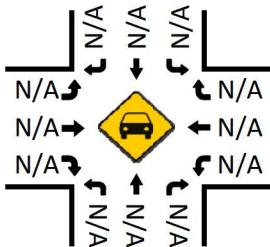
Total Vehicles (Noon)



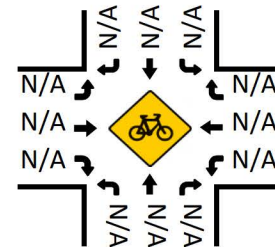
Bikes (NOON)



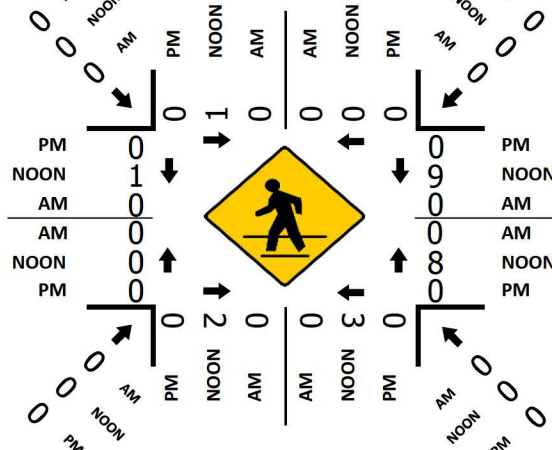
Total Vehicles (PM)



Bikes (PM)



Pedestrians (Crosswalks)

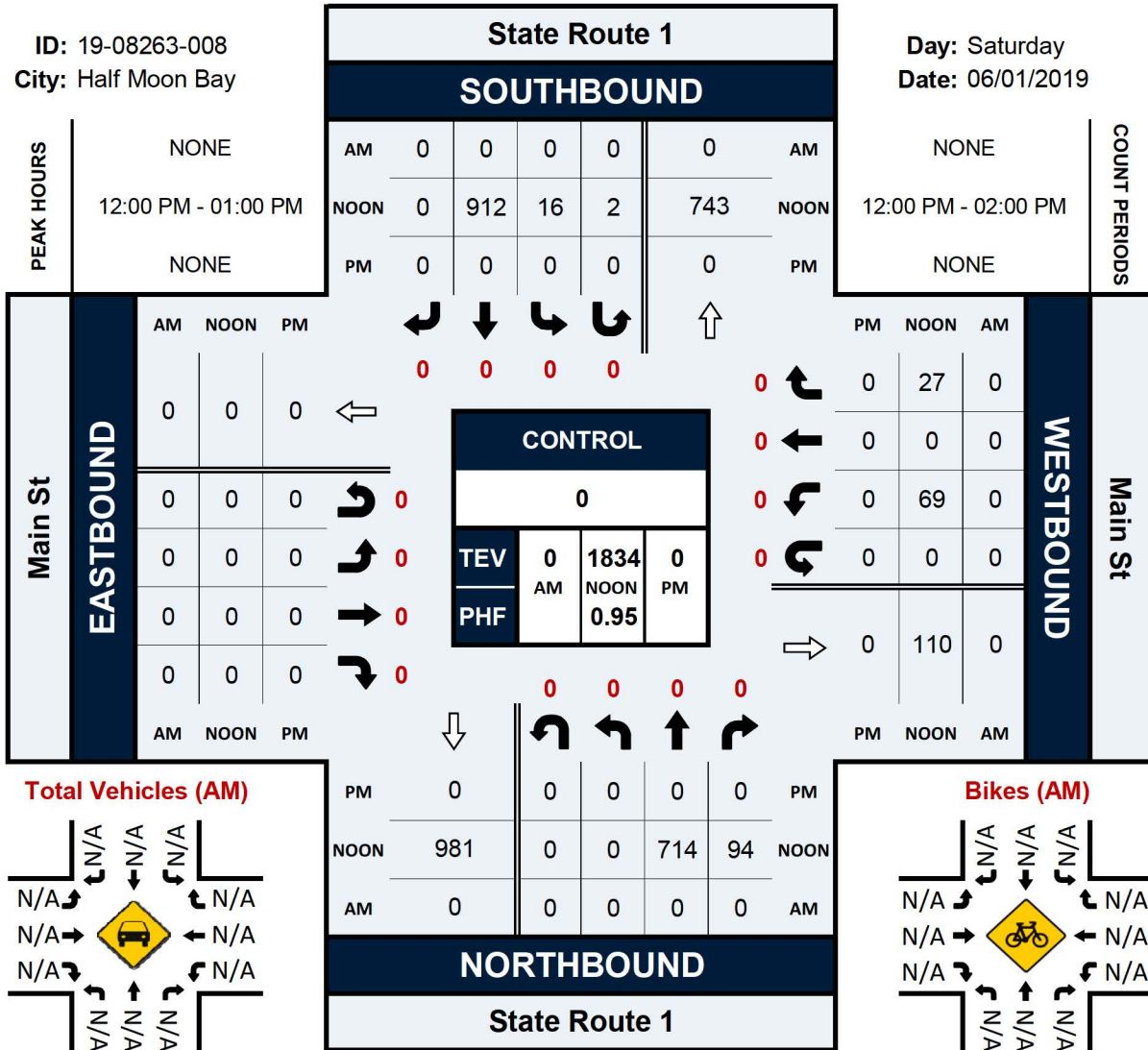


State Route 1 & Main St

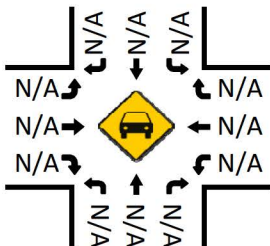
Peak Hour Turning Movement Count

ID: 19-08263-008
City: Half Moon Bay

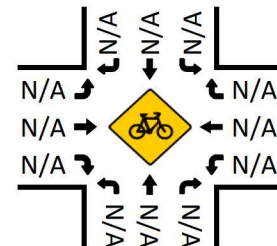
Day: Saturday
Date: 06/01/2019



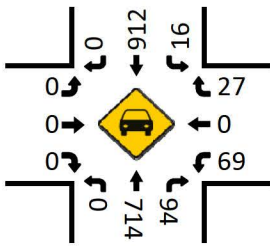
Total Vehicles (AM)



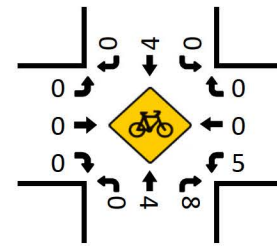
Bikes (AM)



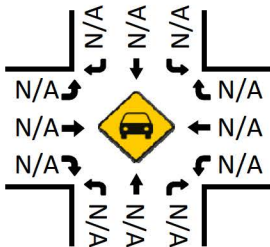
Total Vehicles (Noon)



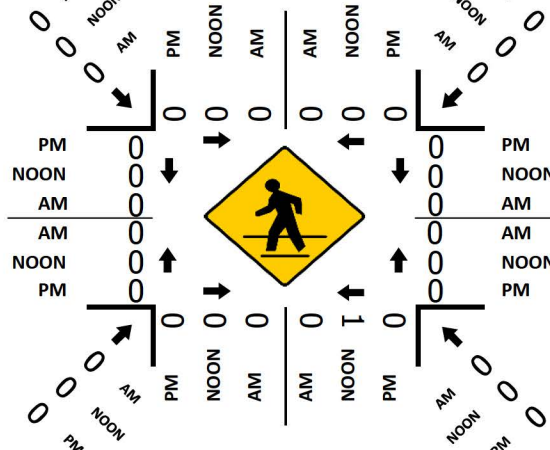
Bikes (NOON)



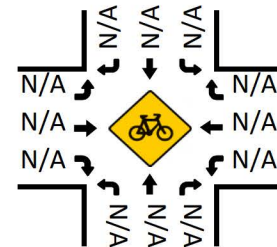
Total Vehicles (PM)



Pedestrians (Crosswalks)



Bikes (PM)



Appendix B

Intersection Level of Service Calculations





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HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

06/14/2019

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	48	69	78	194	116	25
Future Volume (Veh/h)	48	69	78	194	116	25
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	0.80	0.80	0.80	0.80	0.80	0.80
Hourly flow rate (vph)	60	86	98	243	145	31
Pedestrians	15		7		6	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		1	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	620	182	191			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	620	182	191			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	85	90	93			
cM capacity (veh/h)	412	844	1365			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	146	341	176			
Volume Left	60	98	0			
Volume Right	86	0	31			
eSH	590	1365	1700			
Volume to Capacity	0.25	0.07	0.10			
Queue Length 95th (ft)	24	6	0			
Control Delay (s)	13.1	2.7	0.0			
Lane LOS	B	A				
Approach Delay (s)	13.1	2.7	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			4.3			
Intersection Capacity Utilization			43.1%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

06/14/2019

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↕	↕		↕	↕	
Traffic Volume (veh/h)	6	2	2	1	2	19	4	648	1	28	459	4
Future Volume (Veh/h)	6	2	2	1	2	19	4	648	1	28	459	4
Sign Control	Stop		Stop		Free		Free		Free		Free	
Grade	0%		0%		0%		0%		0%		0%	
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Hourly flow rate (vph)	6	2	2	1	2	20	4	675	1	29	478	4
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)	1190											
pX, platoon unblocked												
vC, conflicting volume	1242	1222	480	1222	1224	676	482			676		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1242	1222	480	1222	1224	676	482			676		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	96	99	100	99	99	96	100			97		
cM capacity (veh/h)	140	173	586	150	173	454	1081			915		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	10	23	4	676	29	482						
Volume Left	6	1	4	0	29	0						
Volume Right	2	20	0	1	0	4						
eSH	173	369	1081	1700	915	1700						
Volume to Capacity	0.06	0.06	0.00	0.40	0.03	0.28						
Queue Length 95th (ft)	5	5	0	0	2	0						
Control Delay (s)	27.1	15.4	8.3	0.0	9.1	0.0						
Lane LOS	D	C	A		A							
Approach Delay (s)	27.1	15.4	0.0	0.5								
Approach LOS	D	C										
Intersection Summary												
Average Delay			0.8									
Intersection Capacity Utilization			44.2%	ICU Level of Service	A							
Analysis Period (min)			15									

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

06/14/2019

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↔			↔		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	15	5	13	0	10	8	13	121	0	8	58	17
Future Volume (vph)	15	5	13	0	10	8	13	121	0	8	58	17
Peak Hour Factor	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82
Hourly flow rate (vph)	18	6	16	0	12	10	16	148	0	10	71	21
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	40	22	164	102								
Volume Left (vph)	18	0	16	10								
Volume Right (vph)	16	10	0	21								
Hadj (s)	-0.12	-0.24	0.05	-0.07								
Departure Headway (s)	4.4	4.3	4.2	4.1								
Degree Utilization, x	0.05	0.03	0.19	0.12								
Capacity (veh/h)	769	775	835	849								
Control Delay (s)	7.6	7.4	8.2	7.7								
Approach Delay (s)	7.6	7.4	8.2	7.7								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay				7.9								
Level of Service				A								
Intersection Capacity Utilization			27.2%	ICU Level of Service				A				
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

8: SR 1 & Higgins Canyon Rd

06/14/2019

Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	↔	↔	↕	↕	↔	↔		
Traffic Volume (veh/h)	63	15	637	106	23	441		
Future Volume (Veh/h)	63	15	637	106	23	441		
Sign Control	Stop		Free		Free			
Grade	0%		0%		0%			
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95		
Hourly flow rate (vph)	66	16	671	112	24	464		
Pedestrians								
Lane Width (ft)								
Walking Speed (ft/s)								
Percent Blockage								
Right turn flare (veh)								
Median type			None			None		
Median storage (veh)								
Upstream signal (ft)								
pX, platoon unblocked								
vC, conflicting volume	951	336			671			
vC1, stage 1 conf vol								
vC2, stage 2 conf vol								
vCu, unblocked vol	951	336			671			
tC, single (s)	6.8	6.9			4.1			
tC, 2 stage (s)								
tF (s)	3.5	3.3			2.2			
pD queue free %	74	98			97			
cM capacity (veh/h)	251	660			915			
Direction, Lane #	WB 1	WB 2	NB 1	NB 2	NB 3	SB 1	SB 2	SB 3
Volume Total	66	16	336	336	112	24	232	232
Volume Left	66	0	0	0	0	24	0	0
Volume Right	0	16	0	0	112	0	0	0
sSH	251	660	1700	1700	1700	915	1700	1700
Volume to Capacity	0.26	0.02	0.20	0.20	0.07	0.03	0.14	0.14
Queue Length 95th (ft)	26	2	0	0	0	2	0	0
Control Delay (s)	24.4	10.6	0.0	0.0	0.0	9.0	0.0	0.0
Lane LOS	C	B				A		
Approach Delay (s)	21.7		0.0			0.4		
Approach LOS	C							
Intersection Summary								
Average Delay			1.5					
Intersection Capacity Utilization			29.3%	ICU Level of Service				A
Analysis Period (min)			15					

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

06/14/2019

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	31	39	29	143	154	62
Future Volume (Veh/h)	31	39	29	143	154	62
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	34	42	32	155	167	67
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	430	218	243			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	430	218	243			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
pD queue free %	94	95	98			
cM capacity (veh/h)	562	811	1313			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	76	187	234			
Volume Left	34	32	0			
Volume Right	42	0	67			
eSH	677	1313	1700			
Volume to Capacity	0.11	0.02	0.14			
Queue Length 95th (ft)	9	2	0			
Control Delay (s)	11.0	1.5	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.0	1.5	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.2			
Intersection Capacity Utilization			38.2%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

06/14/2019

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↕	↕		↕	↕	
Traffic Volume (veh/h)	3	2	5	1	0	26	7	619	9	24	844	10
Future Volume (Veh/h)	3	2	5	1	0	26	7	619	9	24	844	10
Sign Control	Stop		Stop		Stop		Free		Free		Free	
Grade	0%		0%		0%		0%		0%		0%	
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Hourly flow rate (vph)	3	2	5	1	0	27	7	645	9	25	879	10
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)									1190			
pX, platoon unblocked												
vC, conflicting volume	1620	1602	885	1600	1602	650	889			654		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1620	1602	885	1600	1602	650	889			654		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
pD queue free %	96	98	99	99	100	94	99			97		
cM capacity (veh/h)	76	102	344	81	102	469	762			933		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	10	28	7	654	25	889						
Volume Left	3	1	7	0	25	0						
Volume Right	5	27	0	9	0	10						
eSH	136	401	762	1700	933	1700						
Volume to Capacity	0.07	0.07	0.01	0.38	0.03	0.52						
Queue Length 95th (ft)	6	6	1	0	2	0						
Control Delay (s)	33.6	14.7	9.8	0.0	9.0	0.0						
Lane LOS	D	B	A		A							
Approach Delay (s)	33.6	14.7	0.1	0.2								
Approach LOS	D	B										
Intersection Summary												
Average Delay			0.6									
Intersection Capacity Utilization			55.4%		ICU Level of Service	B						
Analysis Period (min)			15									

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

06/14/2019

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↔			↔		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	16	5	11	0	5	3	6	99	1	6	92	7
Future Volume (vph)	16	5	11	0	5	3	6	99	1	6	92	7
Peak Hour Factor	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87
Hourly flow rate (vph)	18	6	13	0	6	3	7	114	1	7	106	8
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	37	9	122	121								
Volume Left (vph)	18	0	7	7								
Volume Right (vph)	13	3	1	8								
Hadj (s)	-0.08	-0.17	0.04	0.01								
Departure Headway (s)	4.4	4.3	4.2	4.1								
Degree Utilization, x	0.04	0.01	0.14	0.14								
Capacity (veh/h)	779	775	842	855								
Control Delay (s)	7.6	7.4	7.8	7.8								
Approach Delay (s)	7.6	7.4	7.8	7.8								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay				7.8								
Level of Service				A								
Intersection Capacity Utilization			26.5%	ICU Level of Service				A				
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

8: SR 1 & Higgins Canyon Rd

06/14/2019

Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	↔	↔	↕	↕	↔	↔		
Traffic Volume (veh/h)	78	17	614	85	22	829		
Future Volume (Veh/h)	78	17	614	85	22	829		
Sign Control	Stop		Free			Free		
Grade	0%		0%			0%		
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96		
Hourly flow rate (vph)	81	18	640	89	23	864		
Pedestrians								
Lane Width (ft)								
Walking Speed (ft/s)								
Percent Blockage								
Right turn flare (veh)								
Median type			None			None		
Median storage (veh)								
Upstream signal (ft)								
pX, platoon unblocked								
vC, conflicting volume	1118	320			640			
vC1, stage 1 conf vol								
vC2, stage 2 conf vol								
vCu, unblocked vol	1118	320			640			
tC, single (s)	6.8	6.9			4.1			
tC, 2 stage (s)								
tF (s)	3.5	3.3			2.2			
pD queue free %	59	97			98			
cM capacity (veh/h)	196	676			940			
Direction, Lane #	WB 1	WB 2	NB 1	NB 2	NB 3	SB 1	SB 2	SB 3
Volume Total	81	18	320	320	89	23	432	432
Volume Left	81	0	0	0	0	23	0	0
Volume Right	0	18	0	0	89	0	0	0
sSH	196	676	1700	1700	1700	940	1700	1700
Volume to Capacity	0.41	0.03	0.19	0.19	0.05	0.02	0.25	0.25
Queue Length 95th (ft)	47	2	0	0	0	2	0	0
Control Delay (s)	35.7	10.5	0.0	0.0	0.0	8.9	0.0	0.0
Lane LOS	E	B				A		
Approach Delay (s)	31.1		0.0			0.2		
Approach LOS	D							
Intersection Summary								
Average Delay			1.9					
Intersection Capacity Utilization			33.9%	ICU Level of Service				A
Analysis Period (min)			15					

HCM Signalized Intersection Capacity Analysis

1: SR 1 & Main St

06/14/2019



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	160	62	85	43	66	402	112	748	37	282	813	160
Future Volume (vph)	160	62	85	43	66	402	112	748	37	282	813	160
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0		4.7	3.5	3.5	3.5	5.5		3.5	5.5	
Lane Util. Factor	1.00	1.00		1.00	1.00	0.95	1.00	0.95		1.00	0.95	
Frbp, ped/bikes	1.00	0.98		1.00	0.99	1.00	1.00	1.00		1.00	0.99	
Fipb, ped/bikes	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	
Frt	1.00	0.85		1.00	0.85	1.00	0.99	1.00		1.00	0.98	
Flt Protected	0.97	1.00		0.98	1.00	0.95	1.00	0.95		1.00	1.00	
Satd. Flow (prot)	1806	1553		1849	1586	1805	3540	1770		3433		
Flt Permitted	0.97	1.00		0.98	1.00	0.95	1.00	0.95		1.00	1.00	
Satd. Flow (perm)	1806	1553		1849	1586	1805	3540	1770		3433		
Peak-hour factor, PHF	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99
Adj. Flow (vph)	162	63	86	43	67	406	113	756	37	285	821	162
RTOR Reduction (vph)	0	0	71	0	0	194	0	2	0	0	8	0
Lane Group Flow (vph)	0	225	15	0	110	212	113	791	0	285	975	0
Confl. Peds. (#/hr)	9		7	7		9	6		3	3		6
Confl. Bikes (#/hr)								1				
Heavy Vehicles (%)	1%	3%	2%	2%	0%	1%	0%	1%	4%	2%	2%	2%
Turn Type	Split	NA	Perm	Split	NA	pm+ov	Prot	NA		Prot	NA	
Protected Phases	3	3		4	4	5	1	6		5	2	
Permitted Phases			3			4						
Actuated Green, G (s)	24.2	24.2		21.0	56.2	8.5	37.9	35.2		64.6		
Effective Green, g (s)	24.2	24.2		21.0	56.2	8.5	37.9	35.2		64.6		
Actuated g/C Ratio	0.18	0.18		0.15	0.41	0.06	0.28	0.26		0.47		
Clearance Time (s)	4.0	4.0		4.7	3.5	3.5	5.5	3.5		5.5		
Vehicle Extension (s)	3.0	3.0		2.0	2.0	2.0	2.0	2.0		2.0		
Lane Grp Cap (vph)	321	276		285	655	112	986	458		1630		
v/s Ratio Prot	c0.12			c0.06	0.08	c0.06	c0.22	c0.16		0.28		
v/s Ratio Perm		0.01			0.05							
v/c Ratio	0.70	0.06		0.39	0.32	1.01	0.80	0.62		0.60		
Uniform Delay, d1	52.5	46.4		51.7	27.0	63.8	45.6	44.5		26.2		
Progression Factor	1.00	1.00		1.08	2.42	0.66	0.57	1.00		1.00		
Incremental Delay, d2	6.8	0.1		0.3	0.1	82.6	6.2	1.9		1.6		
Delay (s)	59.3	46.5		56.3	65.4	124.9	32.2	46.4		27.8		
Level of Service	E	D		E	E	F	C	D		C		
Approach Delay (s)	55.7			63.5			43.8			32.0		
Approach LOS	E			E			D			C		

Intersection Summary			
HCM 2000 Control Delay	43.4	HCM 2000 Level of Service	D
HCM 2000 Volume to Capacity ratio	0.66		
Actuated Cycle Length (s)	136.0	Sum of lost time (s)	17.7
Intersection Capacity Utilization	77.6%	ICU Level of Service	D
Analysis Period (min)	15		
c Critical Lane Group			

HCM Signalized Intersection Capacity Analysis

2: SR 1 & SR 92

06/14/2019



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	45	38	194	581	92	194	161	684	448	292	671	28
Future Volume (vph)	45	38	194	581	92	194	161	684	448	292	671	28
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.1	4.1	4.6	4.6	4.6	3.5	5.5	5.5	3.5	5.5		
Lane Util. Factor	1.00	1.00	0.95	0.95	1.00	1.00	0.95	1.00	0.97	0.95		
Frbp, ped/bikes	1.00	0.98	1.00	1.00	0.98	1.00	1.00	1.00	1.00	1.00		
Fipb, ped/bikes	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		
Frt	1.00	0.85	1.00	1.00	0.85	1.00	1.00	0.85	1.00	0.99		
Flt Protected	0.97	1.00	0.95	0.96	1.00	0.95	1.00	1.00	0.95	1.00		
Satd. Flow (prot)	1850	1574	1681	1717	1535	1787	3539	1583	3467	3524		
Flt Permitted	0.97	1.00	0.95	0.96	1.00	0.95	1.00	1.00	0.95	1.00		
Satd. Flow (perm)	1850	1574	1681	1717	1535	1787	3539	1583	3467	3524		
Peak-hour factor, PHF	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92	0.92
Adj. Flow (vph)	49	41	211	632	100	211	175	743	487	317	729	30
RTOR Reduction (vph)	0	0	184	0	0	156	0	0	295	0	2	0
Lane Group Flow (vph)	0	90	27	367	365	55	175	743	192	317	757	0
Confl. Peds. (#/hr)	10		1	1	10	7						7
Heavy Vehicles (%)	0%	0%	1%	2%	0%	3%	1%	2%	2%	1%	1%	18%
Turn Type	Split	NA	Perm	Split	NA	Perm	Prot	NA	Perm	Prot	NA	
Protected Phases	3	3		4	4	4	1	6		5	2	
Permitted Phases			3			4						
Actuated Green, G (s)	11.9	11.9	35.7	35.7	35.7	19.4	53.5	53.5	17.2	51.3		
Effective Green, g (s)	11.9	11.9	35.7	35.7	35.7	19.4	53.5	53.5	17.2	51.3		
Actuated g/C Ratio	0.09	0.09	0.26	0.26	0.26	0.14	0.39	0.39	0.13	0.38		
Clearance Time (s)	4.1	4.1	4.6	4.6	4.6	3.5	5.5	5.5	3.5	5.5		
Vehicle Extension (s)	2.0	2.0	2.0	2.0	2.0	2.0	3.0	3.0	3.0	3.0		
Lane Grp Cap (vph)	161	137	441	450	402	254	1392	622	438	1329		
v/s Ratio Prot	c0.05		c0.22	0.21		c0.10	0.21		c0.09	c0.21		
v/s Ratio Perm		0.02			0.04			0.12				
v/c Ratio	0.56	0.19	0.83	0.81	0.14	0.69	0.53	0.31	0.72	0.57		
Uniform Delay, d1	59.5	57.6	47.3	47.0	38.4	55.4	31.7	28.5	57.1	33.6		
Progression Factor	1.00	1.00	0.68	0.68	0.34	1.25	0.62	0.33	0.75	0.54		
Incremental Delay, d2	2.4	0.3	11.7	9.7	0.1	5.7	1.4	1.2	5.2	1.6		
Delay (s)	61.9	57.9	43.8	41.7	13.1	74.9	21.0	10.5	48.3	19.9		
Level of Service	E	E	D	D	B	E	C	B	D	B		
Approach Delay (s)	59.1			36.1			24.1			28.3		
Approach LOS	E			D			C			C		

Intersection Summary			
HCM 2000 Control Delay	31.2	HCM 2000 Level of Service	C
HCM 2000 Volume to Capacity ratio	0.69		
Actuated Cycle Length (s)	136.0	Sum of lost time (s)	17.7
Intersection Capacity Utilization	68.6%	ICU Level of Service	C
Analysis Period (min)	15		
c Critical Lane Group			

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

06/14/2019

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	39	19	35	151	112	58
Future Volume (Veh/h)	39	19	35	151	112	58
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	0.89	0.89	0.89	0.89	0.89	0.89
Hourly flow rate (vph)	44	21	39	170	126	65
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	418	176	200			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	418	176	200			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
pD queue free %	92	98	97			
cM capacity (veh/h)	570	855	1362			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	65	209	191			
Volume Left	44	39	0			
Volume Right	21	0	65			
eSH	639	1362	1700			
Volume to Capacity	0.10	0.03	0.11			
Queue Length 95th (ft)	8	2	0			
Control Delay (s)	11.3	1.6	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.3	1.6	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.3			
Intersection Capacity Utilization			36.4%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

06/14/2019

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↕	↕		↕	↕	
Traffic Volume (veh/h)	2	1	4	2	1	15	5	722	4	21	917	6
Future Volume (Veh/h)	2	1	4	2	1	15	5	722	4	21	917	6
Sign Control	Stop		Stop		Free		Free		Free		Free	
Grade	0%		0%		0%		0%		0%		0%	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Hourly flow rate (vph)	2	1	4	2	1	16	5	768	4	22	976	6
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)	1190											
pX, platoon unblocked												
vC, conflicting volume	1818	1805	980	1806	1806	770	982			772		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1818	1805	980	1806	1806	770	982			772		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
pD queue free %	96	99	99	97	99	96	99			97		
cM capacity (veh/h)	56	77	303	58	77	401	703			843		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	7	19	5	772	22	982						
Volume Left	2	2	5	0	22	0						
Volume Right	4	16	0	4	0	6						
eSH	113	218	703	1700	843	1700						
Volume to Capacity	0.06	0.09	0.01	0.45	0.03	0.58						
Queue Length 95th (ft)	5	7	1	0	2	0						
Control Delay (s)	39.1	23.1	10.2	0.0	9.4	0.0						
Lane LOS	E	C	B		A							
Approach Delay (s)	39.1	23.1	0.1	0.2								
Approach LOS	E	C										
Intersection Summary												
Average Delay			0.5									
Intersection Capacity Utilization			59.0%	ICU Level of Service	B							
Analysis Period (min)			15									

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

06/14/2019

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↔			↔		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	13	6	4	1	1	3	3	108	0	6	77	9
Future Volume (vph)	13	6	4	1	1	3	3	108	0	6	77	9
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85
Hourly flow rate (vph)	15	7	5	1	1	4	4	127	0	7	91	11
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	27	6	131	109								
Volume Left (vph)	15	1	4	7								
Volume Right (vph)	5	4	0	11								
Hadj (s)	0.03	-0.33	0.04	-0.01								
Departure Headway (s)	4.5	4.1	4.1	4.1								
Degree Utilization, x	0.03	0.01	0.15	0.12								
Capacity (veh/h)	763	820	853	865								
Control Delay (s)	7.6	7.1	7.8	7.7								
Approach Delay (s)	7.6	7.1	7.8	7.7								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay				7.7								
Level of Service				A								
Intersection Capacity Utilization			23.7%	ICU Level of Service				A				
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

8: SR 1 & Higgins Canyon Rd

06/14/2019

Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	↔	↔	↕	↕	↔	↔		
Traffic Volume (veh/h)	69	27	714	94	18	912		
Future Volume (Veh/h)	69	27	714	94	18	912		
Sign Control	Stop		Free		Free			
Grade	0%		0%		0%			
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95		
Hourly flow rate (vph)	73	28	752	99	19	960		
Pedestrians								
Lane Width (ft)								
Walking Speed (ft/s)								
Percent Blockage								
Right turn flare (veh)								
Median type			None			None		
Median storage (veh)								
Upstream signal (ft)								
pX, platoon unblocked								
vC, conflicting volume	1270	376			752			
vC1, stage 1 conf vol								
vC2, stage 2 conf vol								
vCu, unblocked vol	1270	376			752			
tC, single (s)	6.8	6.9			4.1			
tC, 2 stage (s)								
tF (s)	3.5	3.3			2.2			
p0 queue free %	53	95			98			
cM capacity (veh/h)	156	622			853			
Direction, Lane #	WB 1	WB 2	NB 1	NB 2	NB 3	SB 1	SB 2	SB 3
Volume Total	73	28	376	376	99	19	480	480
Volume Left	73	0	0	0	0	19	0	0
Volume Right	0	28	0	0	99	0	0	0
sSH	156	622	1700	1700	1700	853	1700	1700
Volume to Capacity	0.47	0.05	0.22	0.22	0.06	0.02	0.28	0.28
Queue Length 95th (ft)	54	4	0	0	0	2	0	0
Control Delay (s)	46.7	11.1	0.0	0.0	0.0	9.3	0.0	0.0
Lane LOS	E	B				A		
Approach Delay (s)	36.8		0.0			0.2		
Approach LOS	E							
Intersection Summary								
Average Delay			2.0					
Intersection Capacity Utilization			35.7%	ICU Level of Service				A
Analysis Period (min)			15					

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	51	73	82	204	122	27
Future Volume (Veh/h)	51	73	82	204	122	27
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	51	73	82	204	122	27
Pedestrians	15		7		6	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		1	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	524	158	164			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	524	158	164			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	89	92	94			
cM capacity (veh/h)	475	872	1397			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	124	286	149			
Volume Left	51	82	0			
Volume Right	73	0	27			
eSH	649	1397	1700			
Volume to Capacity	0.19	0.06	0.09			
Queue Length 95th (ft)	18	5	0			
Control Delay (s)	11.9	2.6	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.9	2.6	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			4.0			
Intersection Capacity Utilization			44.5%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↕	↕		↕	↕	
Traffic Volume (veh/h)	7	3	3	2	3	20	5	679	2	30	481	5
Future Volume (Veh/h)	7	3	3	2	3	20	5	679	2	30	481	5
Sign Control	Stop			Stop			Free			Free		
Grade	0%			0%			0%			0%		
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	7	3	3	2	3	20	5	679	2	30	481	5
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type							None			None		
Median storage (veh)												
Upstream signal (ft)							1268			1190		
pX, platoon unblocked												
vC, conflicting volume	1254	1234	484	1236	1236	680	486				681	
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1254	1234	484	1236	1236	680	486				681	
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1				4.1	
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2				2.2	
p0 queue free %	95	98	99	99	98	96	100				97	
cM capacity (veh/h)	136	170	583	146	170	451	1077				912	
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	13	25	5	681	30	486						
Volume Left	7	2	5	0	30	0						
Volume Right	3	20	0	2	0	5						
eSH	175	330	1077	1700	912	1700						
Volume to Capacity	0.07	0.08	0.00	0.40	0.03	0.29						
Queue Length 95th (ft)	6	6	0	0	3	0						
Control Delay (s)	27.2	16.8	8.4	0.0	9.1	0.0						
Lane LOS	D	C	A		A							
Approach Delay (s)	27.2	16.8	0.1	0.5								
Approach LOS	D	C										
Intersection Summary												
Average Delay				0.9								
Intersection Capacity Utilization				45.9%			ICU Level of Service	A				
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop											
Traffic Volume (vph)	16	6	14	0	11	9	14	127	0	9	61	18
Future Volume (vph)	16	6	14	0	11	9	14	127	0	9	61	18
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	16	6	14	0	11	9	14	127	0	9	61	18
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	36	20	141	88								
Volume Left (vph)	16	0	14	9								
Volume Right (vph)	14	9	0	18								
Hadj (s)	-0.11	-0.24	0.05	-0.07								
Departure Headway (s)	4.3	4.2	4.2	4.1								
Degree Utilization, x	0.04	0.02	0.16	0.10								
Capacity (veh/h)	789	796	842	858								
Control Delay (s)	7.5	7.3	8.0	7.6								
Approach Delay (s)	7.5	7.3	8.0	7.6								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay	7.7											
Level of Service	A											
Intersection Capacity Utilization	27.5%		ICU Level of Service				A					
Analysis Period (min)	15											

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↔	↔	↕	↕	↔	↔
Traffic Volume (vph)	66	16	667	111	25	462
Future Volume (vph)	66	16	667	111	25	462
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	66	16	667	111	25	462
RTOR Reduction (vph)	0	15	0	38	0	0
Lane Group Flow (vph)	66	1	667	73	25	462
Turn Type	Prot	Perm	NA	Prot	Prot	NA
Protected Phases	8		2	2	1	6
Permitted Phases	8					
Actuated Green, G (s)	4.8	4.8	34.2	34.2	0.9	39.1
Effective Green, g (s)	4.8	4.8	34.2	34.2	0.9	39.1
Actuated g/C Ratio	0.09	0.09	0.66	0.66	0.02	0.75
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	163	146	2332	1043	30	2666
v/s Ratio Prot	c0.04		c0.19	0.05	c0.01	0.13
v/s Ratio Perm	0.00					
v/c Ratio	0.40	0.01	0.29	0.07	0.83	0.17
Uniform Delay, d1	22.2	21.4	3.7	3.2	25.4	1.8
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.6	0.0	0.3	0.1	95.9	0.1
Delay (s)	23.8	21.4	4.0	3.3	121.3	2.0
Level of Service	C	C	A	A	F	A
Approach Delay (s)	23.4		3.9			8.1
Approach LOS	C		A			A
Intersection Summary						
HCM 2000 Control Delay	6.6		HCM 2000 Level of Service		A	
HCM 2000 Volume to Capacity ratio	0.31					
Actuated Cycle Length (s)	51.9		Sum of lost time (s)		12.0	
Intersection Capacity Utilization	31.1%		ICU Level of Service		A	
Analysis Period (min)	15					
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	33	42	31	152	164	66
Future Volume (Veh/h)	33	42	31	152	164	66
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	33	42	31	152	164	66
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	422	214	239			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	422	214	239			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	94	95	98			
cM capacity (veh/h)	569	814	1318			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	75	183	230			
Volume Left	33	31	0			
Volume Right	42	0	66			
eSH	685	1318	1700			
Volume to Capacity	0.11	0.02	0.14			
Queue Length 95th (ft)	9	2	0			
Control Delay (s)	10.9	1.5	0.0			
Lane LOS	B	A				
Approach Delay (s)	10.9	1.5	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.2			
Intersection Capacity Utilization			39.6%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↕		↕			
Traffic Volume (veh/h)	4	3	6	2	0	28	8	656	10	26	895	11
Future Volume (Veh/h)	4	3	6	2	0	28	8	656	10	26	895	11
Sign Control	Stop			Stop			Free		Free			
Grade	0%			0%			0%		0%			
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	4	3	6	2	0	28	8	656	10	26	895	11
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)							1268		1190			
pX, platoon unblocked												
vC, conflicting volume	1652	1634	902	1632	1635	661	906			666		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1652	1634	902	1632	1635	661	906			666		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	94	97	98	97	100	94	99			97		
cM capacity (veh/h)	72	97	336	75	97	462	751			923		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	13	30	8	666	26	906						
Volume Left	4	2	8	0	26	0						
Volume Right	6	28	0	10	0	11						
eSH	124	345	751	1700	923	1700						
Volume to Capacity	0.10	0.09	0.01	0.39	0.03	0.53						
Queue Length 95th (ft)	9	7	1	0	2	0						
Control Delay (s)	37.3	16.4	9.8	0.0	9.0	0.0						
Lane LOS	E	C	A		A							
Approach Delay (s)	37.3	16.4	0.1	0.3								
Approach LOS	E	C										
Intersection Summary												
Average Delay				0.8								
Intersection Capacity Utilization				58.1%			ICU Level of Service	B				
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	17	6	12	0	6	4	7	105	2	7	98	8
Future Volume (vph)	17	6	12	0	6	4	7	105	2	7	98	8
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	17	6	12	0	6	4	7	105	2	7	98	8
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	35	10	114	113								
Volume Left (vph)	17	0	7	7								
Volume Right (vph)	12	4	2	8								
Hadj (s)	-0.07	-0.21	0.04	0.00								
Departure Headway (s)	4.3	4.2	4.1	4.1								
Degree Utilization, x	0.04	0.01	0.13	0.13								
Capacity (veh/h)	787	802	845	858								
Control Delay (s)	7.5	7.3	7.8	7.7								
Approach Delay (s)	7.5	7.3	7.8	7.7								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay				7.7								
Level of Service				A								
Intersection Capacity Utilization				26.9%	ICU Level of Service							A
Analysis Period (min)				15								

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↔	↔	↕	↕	↔	↔
Traffic Volume (vph)	83	19	651	91	24	879
Future Volume (vph)	83	19	651	91	24	879
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	83	19	651	91	24	879
RTOR Reduction (vph)	0	17	0	32	0	0
Lane Group Flow (vph)	83	2	651	59	24	879
Turn Type	Prot	Perm	NA	Prot	Prot	NA
Protected Phases	8		2	2	1	6
Permitted Phases	8					
Actuated Green, G (s)	5.1	5.1	33.2	33.2	0.9	38.1
Effective Green, g (s)	5.1	5.1	33.2	33.2	0.9	38.1
Actuated g/C Ratio	0.10	0.10	0.65	0.65	0.02	0.74
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	176	157	2294	1026	31	2633
v/s Ratio Prot	c0.05		0.18	0.04	0.01	c0.25
v/s Ratio Perm	0.00					
v/c Ratio	0.47	0.01	0.28	0.06	0.77	0.33
Uniform Delay, d1	21.8	20.8	3.9	3.3	25.0	2.2
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	2.0	0.0	0.3	0.1	73.6	0.3
Delay (s)	23.8	20.8	4.2	3.4	98.7	2.6
Level of Service	C	C	A	A	F	A
Approach Delay (s)	23.2		4.1			5.1
Approach LOS	C		A			A
Intersection Summary						
HCM 2000 Control Delay			5.7	HCM 2000 Level of Service		A
HCM 2000 Volume to Capacity ratio			0.39			
Actuated Cycle Length (s)			51.2	Sum of lost time (s)	12.0	
Intersection Capacity Utilization			35.6%	ICU Level of Service	A	
Analysis Period (min)			15			
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	42	21	38	160	119	62
Future Volume (Veh/h)	42	21	38	160	119	62
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	42	21	38	160	119	62
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	397	167	190			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	397	167	190			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	93	98	97			
cM capacity (veh/h)	586	865	1373			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	63	198	181			
Volume Left	42	38	0			
Volume Right	21	0	62			
eSH	657	1373	1700			
Volume to Capacity	0.10	0.03	0.11			
Queue Length 95th (ft)	8	2	0			
Control Delay (s)	11.1	1.7	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.1	1.7	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.3			
Intersection Capacity Utilization			37.8%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↕			↕		
Traffic Volume (veh/h)	3	2	5	3	2	16	6	765	5	23	972	7
Future Volume (Veh/h)	3	2	5	3	2	16	6	765	5	23	972	7
Sign Control	Stop			Stop			Free		Free			
Grade	0%			0%			0%		0%			
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	3	2	5	3	2	16	6	765	5	23	972	7
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)							1267		1190			
pX, platoon unblocked												
vC, conflicting volume	1816	1804	976	1804	1804	768	979			770		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1816	1804	976	1804	1804	768	979			770		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	95	97	98	95	97	96	99			97		
cM capacity (veh/h)	55	77	304	58	76	402	705			844		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	10	21	6	770	23	979						
Volume Left	3	3	6	0	23	0						
Volume Right	5	16	0	5	0	7						
eSH	103	178	705	1700	844	1700						
Volume to Capacity	0.10	0.12	0.01	0.45	0.03	0.58						
Queue Length 95th (ft)	8	10	1	0	2	0						
Control Delay (s)	43.6	27.9	10.2	0.0	9.4	0.0						
Lane LOS	E	D	B	A								
Approach Delay (s)	43.6	27.9	0.1	0.2								
Approach LOS	E	D										
Intersection Summary												
Average Delay				0.7								
Intersection Capacity Utilization				61.9%			ICU Level of Service	B				
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	14	7	5	2	2	4	4	115	0	7	82	10
Future Volume (vph)	14	7	5	2	2	4	4	115	0	7	82	10
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	14	7	5	2	2	4	4	115	0	7	82	10
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	26	8	119	99								
Volume Left (vph)	14	2	4	7								
Volume Right (vph)	5	4	0	10								
Hadj (s)	0.03	-0.22	0.04	-0.01								
Departure Headway (s)	4.4	4.2	4.1	4.1								
Degree Utilization, x	0.03	0.01	0.14	0.11								
Capacity (veh/h)	775	812	855	867								
Control Delay (s)	7.6	7.2	7.8	7.6								
Approach Delay (s)	7.6	7.2	7.8	7.6								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay	7.7											
Level of Service	A											
Intersection Capacity Utilization	23.9%			ICU Level of Service	A							
Analysis Period (min)	15											

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↕	↕	↕	↕	↕	↕
Traffic Volume (vph)	74	29	757	100	20	967
Future Volume (vph)	74	29	757	100	20	967
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	74	29	757	100	20	967
RTOR Reduction (vph)	0	26	0	35	0	0
Lane Group Flow (vph)	74	3	757	65	20	967
Turn Type	Prot	Perm	NA	Perm	Prot	NA
Protected Phases	8		2		1	6
Permitted Phases		8		2		
Actuated Green, G (s)	5.0	5.0	33.2	33.2	0.9	38.1
Effective Green, g (s)	5.0	5.0	33.2	33.2	0.9	38.1
Actuated g/C Ratio	0.10	0.10	0.65	0.65	0.02	0.75
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	173	154	2299	1028	31	2638
v/s Ratio Prot	c0.04		0.21		0.01	c0.27
v/s Ratio Perm		0.00		0.04		
v/c Ratio	0.43	0.02	0.33	0.06	0.65	0.37
Uniform Delay, d1	21.7	20.8	4.0	3.3	24.9	2.3
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.7	0.0	0.4	0.1	37.9	0.4
Delay (s)	23.4	20.9	4.4	3.4	62.8	2.7
Level of Service	C	C	A	A	E	A
Approach Delay (s)	22.7		4.3			3.9
Approach LOS	C		A			A
Intersection Summary						
HCM 2000 Control Delay	5.0		HCM 2000 Level of Service		A	
HCM 2000 Volume to Capacity ratio	0.41					
Actuated Cycle Length (s)	51.1		Sum of lost time (s)		12.0	
Intersection Capacity Utilization	37.5%		ICU Level of Service		A	
Analysis Period (min)	15					
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	51	73	82	208	126	27
Future Volume (Veh/h)	51	73	82	208	126	27
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	51	73	82	208	126	27
Pedestrians	15		7		6	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		1	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	532	162	168			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	532	162	168			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	89	92	94			
cM capacity (veh/h)	470	867	1392			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	124	290	153			
Volume Left	51	82	0			
Volume Right	73	0	27			
eSH	643	1392	1700			
Volume to Capacity	0.19	0.06	0.09			
Queue Length 95th (ft)	18	5	0			
Control Delay (s)	11.9	2.6	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.9	2.6	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			3.9			
Intersection Capacity Utilization			44.8%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↕	↕		↕	↕	
Traffic Volume (veh/h)	7	3	3	2	3	30	5	685	2	41	488	5
Future Volume (Veh/h)	7	3	3	2	3	30	5	685	2	41	488	5
Sign Control	Stop			Stop			Free			Free		
Grade	0%			0%			0%			0%		
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	7	3	3	2	3	30	5	685	2	41	488	5
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type							None			None		
Median storage (veh)												
Upstream signal (ft)							1268			1190		
pX, platoon unblocked												
vC, conflicting volume	1299	1270	490	1270	1271	686	493				687	
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1299	1270	490	1270	1271	686	493				687	
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1				4.1	
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2				2.2	
p0 queue free %	94	98	99	99	98	93	100				95	
cM capacity (veh/h)	122	160	578	137	159	447	1071				907	
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	13	35	5	687	41	493						
Volume Left	7	2	5	0	41	0						
Volume Right	3	30	0	2	0	5						
eSH	160	348	1071	1700	907	1700						
Volume to Capacity	0.08	0.10	0.00	0.40	0.05	0.29						
Queue Length 95th (ft)	7	8	0	0	4	0						
Control Delay (s)	29.4	16.5	8.4	0.0	9.2	0.0						
Lane LOS	D	C	A		A							
Approach Delay (s)	29.4	16.5	0.1	0.7								
Approach LOS	D	C										
Intersection Summary												
Average Delay				1.1								
Intersection Capacity Utilization				46.2%	ICU Level of Service	A						
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↔			↔		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	16	6	25	0	11	9	24	131	0	9	65	18
Future Volume (vph)	16	6	25	0	11	9	24	131	0	9	65	18
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	16	6	25	0	11	9	24	131	0	9	65	18
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	47	20	155	92								
Volume Left (vph)	16	0	24	9								
Volume Right (vph)	25	9	0	18								
Hadj (s)	-0.22	-0.24	0.06	-0.06								
Departure Headway (s)	4.2	4.3	4.2	4.1								
Degree Utilization, x	0.06	0.02	0.18	0.11								
Capacity (veh/h)	798	783	832	847								
Control Delay (s)	7.5	7.4	8.1	7.6								
Approach Delay (s)	7.5	7.4	8.1	7.6								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay				7.8								
Level of Service				A								
Intersection Capacity Utilization				29.3%	ICU Level of Service							A
Analysis Period (min)				15								

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↔	↔	↕	↕	↔	↔
Traffic Volume (vph)	69	22	667	114	32	462
Future Volume (vph)	69	22	667	114	32	462
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	69	22	667	114	32	462
RTOR Reduction (vph)	0	20	0	39	0	0
Lane Group Flow (vph)	69	2	667	75	32	462
Turn Type	Prot	Perm	NA	Prot	Prot	NA
Protected Phases	8		2	2	1	6
Permitted Phases	8					
Actuated Green, G (s)	4.8	4.8	33.4	33.4	0.9	38.3
Effective Green, g (s)	4.8	4.8	33.4	33.4	0.9	38.3
Actuated g/C Ratio	0.09	0.09	0.65	0.65	0.02	0.75
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	166	148	2313	1034	31	2652
v/s Ratio Prot	c0.04		c0.19	0.05	c0.02	0.13
v/s Ratio Perm	0.00					
v/c Ratio	0.42	0.01	0.29	0.07	1.03	0.17
Uniform Delay, d1	21.8	21.0	3.8	3.2	25.1	1.8
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.7	0.0	0.3	0.1	171.6	0.1
Delay (s)	23.5	21.0	4.1	3.4	196.7	2.0
Level of Service	C	C	A	A	F	A
Approach Delay (s)	22.9		4.0			14.6
Approach LOS	C		A			B
Intersection Summary						
HCM 2000 Control Delay			9.1	HCM 2000 Level of Service		A
HCM 2000 Volume to Capacity ratio			0.32			
Actuated Cycle Length (s)			51.1	Sum of lost time (s)	12.0	
Intersection Capacity Utilization			35.6%	ICU Level of Service	A	
Analysis Period (min)			15			
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	39	49	37	179	193	78
Future Volume (Veh/h)	39	49	37	179	193	78
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	39	49	37	179	193	78
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	496	249	280			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	496	249	280			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	92	94	97			
cM capacity (veh/h)	513	779	1273			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	88	216	271			
Volume Left	39	37	0			
Volume Right	49	0	78			
cSH	633	1273	1700			
Volume to Capacity	0.14	0.03	0.16			
Queue Length 95th (ft)	12	2	0			
Control Delay (s)	11.6	1.6	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.6	1.6	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.4			
Intersection Capacity Utilization			44.1%	ICU Level of Service		A
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		↔			↔		↕	↕		↕	↕		
Traffic Volume (veh/h)	4	3	7	2	0	33	9	794	12	30	1068	13	
Future Volume (Veh/h)	4	3	7	2	0	33	9	794	12	30	1068	13	
Sign Control	Stop			Stop			Free			Free			
Grade	0%			0%			0%			0%			
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Hourly flow rate (vph)	4	3	7	2	0	33	9	794	12	30	1068	13	
Pedestrians							1						
Lane Width (ft)							12.0						
Walking Speed (ft/s)							4.0						
Percent Blockage							0						
Right turn flare (veh)													
Median type							None			None			
Median storage (veh)													
Upstream signal (ft)							1268			1190			
pX, platoon unblocked													
vC, conflicting volume	1980	1958	1076	1956	1959	800	1081	806					
vC1, stage 1 conf vol													
vC2, stage 2 conf vol													
vCu, unblocked vol	1980	1958	1076	1956	1959	800	1081	806					
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1	4.1					
tC, 2 stage (s)													
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2	2.2					
p0 queue free %	90	95	97	95	100	91	99	96					
cM capacity (veh/h)	41	60	266	43	60	385	645	819					
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2							
Volume Total	14	35	9	806	30	1081							
Volume Left	4	2	9	0	30	0							
Volume Right	7	33	0	12	0	13							
cSH	80	265	645	1700	819	1700							
Volume to Capacity	0.17	0.13	0.01	0.47	0.04	0.64							
Queue Length 95th (ft)	15	11	1	0	3	0							
Control Delay (s)	59.1	20.6	10.7	0.0	9.6	0.0							
Lane LOS	F	C	B	A									
Approach Delay (s)	59.1	20.6	0.1	0.3									
Approach LOS	F	C											
Intersection Summary													
Average Delay				1.0									
Intersection Capacity Utilization				67.3%	ICU Level of Service				C				
Analysis Period (min)				15									

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	20	7	14	0	7	4	8	124	2	8	115	9
Future Volume (vph)	20	7	14	0	7	4	8	124	2	8	115	9
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	20	7	14	0	7	4	8	124	2	8	115	9
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	41	11	134	132								
Volume Left (vph)	20	0	8	8								
Volume Right (vph)	14	4	2	9								
Hadj (s)	-0.07	-0.18	0.04	0.01								
Departure Headway (s)	4.4	4.3	4.2	4.2								
Degree Utilization, x	0.05	0.01	0.16	0.15								
Capacity (veh/h)	756	765	836	848								
Control Delay (s)	7.7	7.4	8.0	7.9								
Approach Delay (s)	7.7	7.4	8.0	7.9								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay				7.9								
Level of Service				A								
Intersection Capacity Utilization			27.6%	ICU Level of Service			A					
Analysis Period (min)				15								

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↕	↕	↕	↕	↕	↕
Traffic Volume (vph)	98	22	788	107	28	1050
Future Volume (vph)	98	22	788	107	28	1050
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Fr	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	98	22	788	107	28	1050
RTOR Reduction (vph)	0	20	0	39	0	0
Lane Group Flow (vph)	98	2	788	68	28	1050
Turn Type	Prot	Perm	NA	Prot	Prot	NA
Protected Phases	8		2	2	1	6
Permitted Phases	8					
Actuated Green, G (s)	5.4	5.4	32.3	32.3	0.8	37.1
Effective Green, g (s)	5.4	5.4	32.3	32.3	0.8	37.1
Actuated g/C Ratio	0.11	0.11	0.64	0.64	0.02	0.73
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	189	169	2263	1012	28	2599
v/s Ratio Prot	c0.06		0.22	0.04	0.02	c0.30
v/s Ratio Perm	0.00					
v/c Ratio	0.52	0.01	0.35	0.07	1.00	0.40
Uniform Delay, d1	21.3	20.2	4.2	3.4	24.9	2.5
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	2.4	0.0	0.4	0.1	170.1	0.5
Delay (s)	23.7	20.2	4.6	3.6	194.9	3.0
Level of Service	C	C	A	A	F	A
Approach Delay (s)	23.1		4.5			8.0
Approach LOS	C		A			A
Intersection Summary						
HCM 2000 Control Delay			7.4	HCM 2000 Level of Service	A	
HCM 2000 Volume to Capacity ratio			0.46			
Actuated Cycle Length (s)			50.5	Sum of lost time (s)	12.0	
Intersection Capacity Utilization			41.1%	ICU Level of Service	A	
Analysis Period (min)			15			

c Critical Lane Group

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	49	24	44	189	140	73
Future Volume (Veh/h)	49	24	44	189	140	73
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	49	24	44	189	140	73
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	464	194	222			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	464	194	222			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	91	97	97			
cM capacity (veh/h)	533	836	1337			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	73	233	213			
Volume Left	49	44	0			
Volume Right	24	0	73			
eSH	605	1337	1700			
Volume to Capacity	0.12	0.03	0.13			
Queue Length 95th (ft)	10	3	0			
Control Delay (s)	11.8	1.7	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.8	1.7	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.4			
Intersection Capacity Utilization			41.4%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↕			↕		
Traffic Volume (veh/h)	3	2	5	3	2	19	7	922	5	27	1161	8
Future Volume (Veh/h)	3	2	5	3	2	19	7	922	5	27	1161	8
Sign Control	Stop			Stop			Free		Free			
Grade	0%			0%			0%		0%			
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	3	2	5	3	2	19	7	922	5	27	1161	8
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)							1267		1190			
pX, platoon unblocked												
vC, conflicting volume	2175	2160	1166	2160	2162	924	1169			927		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	2175	2160	1166	2160	2162	924	1169			927		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	90	96	98	90	96	94	99			96		
cM capacity (veh/h)	29	45	236	31	45	326	598			737		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	10	24	7	927	27	1169						
Volume Left	3	3	7	0	27	0						
Volume Right	5	19	0	5	0	8						
eSH	60	121	598	1700	737	1700						
Volume to Capacity	0.17	0.20	0.01	0.55	0.04	0.69						
Queue Length 95th (ft)	14	18	1	0	3	0						
Control Delay (s)	77.2	42.1	11.1	0.0	10.1	0.0						
Lane LOS	F	E	B	B								
Approach Delay (s)	77.2	42.1	0.1	0.2								
Approach LOS	F	E										
Intersection Summary												
Average Delay				1.0								
Intersection Capacity Utilization				71.9%	ICU Level of Service	C						
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	17	8	5	2	2	4	4	135	0	8	97	12
Future Volume (vph)	17	8	5	2	2	4	4	135	0	8	97	12
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	17	8	5	2	2	4	4	135	0	8	97	12
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	30	8	139	117								
Volume Left (vph)	17	2	4	8								
Volume Right (vph)	5	4	0	12								
Hadj (s)	0.05	-0.22	0.04	-0.01								
Departure Headway (s)	4.5	4.3	4.1	4.1								
Degree Utilization, x	0.04	0.01	0.16	0.13								
Capacity (veh/h)	752	779	848	860								
Control Delay (s)	7.7	7.3	7.9	7.7								
Approach Delay (s)	7.7	7.3	7.9	7.7								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay				7.8								
Level of Service				A								
Intersection Capacity Utilization				24.3%	ICU Level of Service							A
Analysis Period (min)				15								

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↔	↔	↕	↕	↔	↔
Traffic Volume (vph)	87	34	912	118	23	1154
Future Volume (vph)	87	34	912	118	23	1154
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	87	34	912	118	23	1154
RTOR Reduction (vph)	0	30	0	42	0	0
Lane Group Flow (vph)	87	4	912	76	23	1154
Turn Type	Prot	Perm	NA	Perm	Prot	NA
Protected Phases	8		2		1	6
Permitted Phases		8		2		
Actuated Green, G (s)	5.2	5.2	32.4	32.4	0.8	37.2
Effective Green, g (s)	5.2	5.2	32.4	32.4	0.8	37.2
Actuated g/C Ratio	0.10	0.10	0.64	0.64	0.02	0.74
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	182	163	2275	1017	28	2612
v/s Ratio Prot	c0.05		0.26		0.01	c0.33
v/s Ratio Perm		0.00		0.05		
v/c Ratio	0.48	0.02	0.40	0.07	0.82	0.44
Uniform Delay, d1	21.3	20.3	4.3	3.4	24.7	2.6
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	2.0	0.1	0.5	0.1	96.0	0.5
Delay (s)	23.3	20.4	4.9	3.5	120.7	3.1
Level of Service	C	C	A	A	F	A
Approach Delay (s)	22.5		4.7			5.4
Approach LOS	C		A			A
Intersection Summary						
HCM 2000 Control Delay			6.0	HCM 2000 Level of Service		A
HCM 2000 Volume to Capacity ratio			0.49			
Actuated Cycle Length (s)			50.4	Sum of lost time (s)	12.0	
Intersection Capacity Utilization			43.4%	ICU Level of Service	A	
Analysis Period (min)			15			
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis

5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔		↕		↕	
Traffic Volume (veh/h)	48	69	78	198	120	25
Future Volume (Veh/h)	48	69	78	198	120	25
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	0.80	0.80	0.80	0.80	0.80	0.80
Hourly flow rate (vph)	60	86	98	248	150	31
Pedestrians	15		7		6	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		1	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	630	188	196			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	630	188	196			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	85	90	93			
cM capacity (veh/h)	406	839	1360			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	146	346	181			
Volume Left	60	98	0			
Volume Right	86	0	31			
eSH	583	1360	1700			
Volume to Capacity	0.25	0.07	0.11			
Queue Length 95th (ft)	25	6	0			
Control Delay (s)	13.2	2.7	0.0			
Lane LOS	B	A				
Approach Delay (s)	13.2	2.7	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			4.3			
Intersection Capacity Utilization			43.5%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis

6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔		↔		↔		↕		↕		↕	
Traffic Volume (veh/h)	6	2	2	1	2	29	4	654	1	39	466	4
Future Volume (Veh/h)	6	2	2	1	2	29	4	654	1	39	466	4
Sign Control	Stop			Stop			Free		Free			
Grade	0%			0%			0%		0%			
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Hourly flow rate (vph)	6	2	2	1	2	30	4	681	1	41	485	4
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type							None			None		
Median storage (veh)												
Upstream signal (ft)	1190											
pX, platoon unblocked												
vC, conflicting volume	1289	1259	487	1260	1260	682	489	682				
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1289	1259	487	1260	1260	682	489	682				
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1	4.1				
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2	2.2				
p0 queue free %	95	99	100	99	99	93	100	95				
cM capacity (veh/h)	125	162	581	140	162	450	1074	911				
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	10	33	4	682	41	489						
Volume Left	6	1	4	0	41	0						
Volume Right	2	30	0	1	0	4						
eSH	157	383	1074	1700	911	1700						
Volume to Capacity	0.06	0.09	0.00	0.40	0.05	0.29						
Queue Length 95th (ft)	5	7	0	0	4	0						
Control Delay (s)	29.5	15.3	8.4	0.0	9.1	0.0						
Lane LOS	D	C	A		A							
Approach Delay (s)	29.5	15.3	0.0	0.7								
Approach LOS	D	C										
Intersection Summary												
Average Delay				1.0								
Intersection Capacity Utilization				44.8%	ICU Level of Service	A						
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	15	5	24	0	10	8	23	125	0	8	62	17
Future Volume (vph)	15	5	24	0	10	8	23	125	0	8	62	17
Peak Hour Factor	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82	0.82
Hourly flow rate (vph)	18	6	29	0	12	10	28	152	0	10	76	21
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	53	22	180	107								
Volume Left (vph)	18	0	28	10								
Volume Right (vph)	29	10	0	21								
Hadj (s)	-0.23	-0.24	0.07	-0.07								
Departure Headway (s)	4.3	4.4	4.2	4.2								
Degree Utilization, x	0.06	0.03	0.21	0.12								
Capacity (veh/h)	767	760	824	836								
Control Delay (s)	7.6	7.5	8.4	7.8								
Approach Delay (s)	7.6	7.5	8.4	7.8								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay	8.0											
Level of Service	A											
Intersection Capacity Utilization	29.1%		ICU Level of Service	A								
Analysis Period (min)	15											

HCM Unsignalized Intersection Capacity Analysis

8: SR 1 & Higgins Canyon Rd

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	↕	↕	↕	↕	↕	↕		
Traffic Volume (veh/h)	66	21	637	109	30	441		
Future Volume (Veh/h)	66	21	637	109	30	441		
Sign Control	Stop		Free		Free			
Grade	0%		0%		0%			
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95		
Hourly flow rate (vph)	69	22	671	115	32	464		
Pedestrians								
Lane Width (ft)								
Walking Speed (ft/s)								
Percent Blockage								
Right turn flare (veh)								
Median type	None		None					
Median storage (veh)								
Upstream signal (ft)								
pX, platoon unblocked								
vC, conflicting volume	967	336			671			
vC1, stage 1 conf vol								
vC2, stage 2 conf vol								
vCu, unblocked vol	967	336			671			
tC, single (s)	6.8	6.9			4.1			
tC, 2 stage (s)								
tF (s)	3.5	3.3			2.2			
p0 queue free %	72	97			97			
cM capacity (veh/h)	243	660			915			
Direction, Lane #	WB 1	WB 2	NB 1	NB 2	NB 3	SB 1	SB 2	SB 3
Volume Total	69	22	336	336	115	32	232	232
Volume Left	69	0	0	0	0	32	0	0
Volume Right	0	22	0	0	115	0	0	0
sSH	243	660	1700	1700	1700	915	1700	1700
Volume to Capacity	0.28	0.03	0.20	0.20	0.07	0.03	0.14	0.14
Queue Length 95th (ft)	28	3	0	0	0	3	0	0
Control Delay (s)	25.6	10.6	0.0	0.0	0.0	9.1	0.0	0.0
Lane LOS	D	B				A		
Approach Delay (s)	22.0		0.0			0.6		
Approach LOS	C							
Intersection Summary								
Average Delay	1.7							
Intersection Capacity Utilization	34.6%		ICU Level of Service	A				
Analysis Period (min)	15							

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	31	39	29	147	158	62
Future Volume (Veh/h)	31	39	29	147	158	62
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	0.92	0.92	0.92	0.92	0.92	0.92
Hourly flow rate (vph)	34	42	32	160	172	67
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	440	222	248			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	440	222	248			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	94	95	98			
cM capacity (veh/h)	555	805	1308			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	76	192	239			
Volume Left	34	32	0			
Volume Right	42	0	67			
eSH	670	1308	1700			
Volume to Capacity	0.11	0.02	0.14			
Queue Length 95th (ft)	10	2	0			
Control Delay (s)	11.1	1.5	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.1	1.5	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.2			
Intersection Capacity Utilization			38.6%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↕	↕		↕	↕	
Traffic Volume (veh/h)	3	2	5	1	0	37	7	626	9	34	851	10
Future Volume (Veh/h)	3	2	5	1	0	37	7	626	9	34	851	10
Sign Control	Stop		Stop		Stop		Free		Free		Free	
Grade	0%		0%		0%		0%		0%		0%	
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
Hourly flow rate (vph)	3	2	5	1	0	39	7	652	9	35	886	10
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)	1190											
pX, platoon unblocked												
vC, conflicting volume	1666	1636	892	1634	1636	656	896			661		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1666	1636	892	1634	1636	656	896			661		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	96	98	99	99	100	92	99			96		
cM capacity (veh/h)	68	96	340	76	96	465	757			927		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	10	40	7	661	35	896						
Volume Left	3	1	7	0	35	0						
Volume Right	5	39	0	9	0	10						
eSH	125	412	757	1700	927	1700						
Volume to Capacity	0.08	0.10	0.01	0.39	0.04	0.53						
Queue Length 95th (ft)	6	8	1	0	3	0						
Control Delay (s)	36.2	14.7	9.8	0.0	9.0	0.0						
Lane LOS	E	B	A		A							
Approach Delay (s)	36.2	14.7	0.1	0.3								
Approach LOS	E	B										
Intersection Summary												
Average Delay			0.8									
Intersection Capacity Utilization			55.7%	ICU Level of Service	B							
Analysis Period (min)			15									

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	16	5	21	0	5	3	17	103	1	6	96	7
Future Volume (vph)	16	5	21	0	5	3	17	103	1	6	96	7
Peak Hour Factor	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87
Hourly flow rate (vph)	18	6	24	0	6	3	20	118	1	7	110	8
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	48	9	139	125								
Volume Left (vph)	18	0	20	7								
Volume Right (vph)	24	3	1	8								
Hadj (s)	-0.19	-0.17	0.06	0.01								
Departure Headway (s)	4.3	4.4	4.2	4.2								
Degree Utilization, x	0.06	0.01	0.16	0.15								
Capacity (veh/h)	787	761	831	843								
Control Delay (s)	7.6	7.4	8.0	7.9								
Approach Delay (s)	7.6	7.4	8.0	7.9								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay	7.9											
Level of Service	A											
Intersection Capacity Utilization	28.5%		ICU Level of Service	A								
Analysis Period (min)	15											

HCM Unsignalized Intersection Capacity Analysis

8: SR 1 & Higgins Canyon Rd

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT			
Lane Configurations	↕	↕	↕	↕	↕	↕			
Traffic Volume (veh/h)	81	24	614	88	29	829			
Future Volume (Veh/h)	81	24	614	88	29	829			
Sign Control	Stop		Free		Free				
Grade	0%		0%		0%				
Peak Hour Factor	0.96	0.96	0.96	0.96	0.96	0.96			
Hourly flow rate (vph)	84	25	640	92	30	864			
Pedestrians									
Lane Width (ft)									
Walking Speed (ft/s)									
Percent Blockage									
Right turn flare (veh)									
Median type	None		None						
Median storage (veh)									
Upstream signal (ft)									
pX, platoon unblocked									
vC, conflicting volume	1132	320			640				
vC1, stage 1 conf vol									
vC2, stage 2 conf vol									
vCu, unblocked vol	1132	320			640				
tC, single (s)	6.8	6.9			4.1				
tC, 2 stage (s)									
tF (s)	3.5	3.3			2.2				
p0 queue free %	56	96			97				
cM capacity (veh/h)	191	676			940				
Direction, Lane #	WB 1	WB 2	NB 1	NB 2	NB 3	SB 1	SB 2	SB 3	
Volume Total	84	25	320	320	92	30	432	432	
Volume Left	84	0	0	0	0	30	0	0	
Volume Right	0	25	0	0	92	0	0	0	
sSH	191	676	1700	1700	1700	940	1700	1700	
Volume to Capacity	0.44	0.04	0.19	0.19	0.05	0.03	0.25	0.25	
Queue Length 95th (ft)	51	3	0	0	0	2	0	0	
Control Delay (s)	38.0	10.5	0.0	0.0	0.0	9.0	0.0	0.0	
Lane LOS	E	B				A			
Approach Delay (s)	31.7		0.0			0.3			
Approach LOS	D								
Intersection Summary									
Average Delay	2.1								
Intersection Capacity Utilization	34.8%		ICU Level of Service	A					
Analysis Period (min)	15								

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	39	19	35	158	120	58
Future Volume (Veh/h)	39	19	35	158	120	58
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	0.89	0.89	0.89	0.89	0.89	0.89
Hourly flow rate (vph)	44	21	39	178	135	65
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	434	184	209			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	434	184	209			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	92	98	97			
cM capacity (veh/h)	557	846	1352			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	65	217	200			
Volume Left	44	39	0			
Volume Right	21	0	65			
eSH	626	1352	1700			
Volume to Capacity	0.10	0.03	0.12			
Queue Length 95th (ft)	9	2	0			
Control Delay (s)	11.4	1.6	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.4	1.6	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.3			
Intersection Capacity Utilization			37.1%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↕	↕		↕	↕	
Traffic Volume (veh/h)	2	1	4	2	1	34	5	734	4	45	932	6
Future Volume (Veh/h)	2	1	4	2	1	34	5	734	4	45	932	6
Sign Control	Stop		Stop		Free		Free		Free		Free	
Grade	0%		0%		0%		0%		0%		0%	
Peak Hour Factor	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
Hourly flow rate (vph)	2	1	4	2	1	36	5	781	4	48	991	6
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)									1190			
pX, platoon unblocked												
vC, conflicting volume	1918	1885	995	1886	1886	783	997			785		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1918	1885	995	1886	1886	783	997			785		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	95	98	99	96	98	91	99			94		
cM capacity (veh/h)	44	66	297	50	66	394	694			834		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	7	39	5	785	48	997						
Volume Left	2	2	5	0	48	0						
Volume Right	4	36	0	4	0	6						
eSH	94	266	694	1700	834	1700						
Volume to Capacity	0.07	0.15	0.01	0.46	0.06	0.59						
Queue Length 95th (ft)	6	13	1	0	5	0						
Control Delay (s)	46.4	20.9	10.2	0.0	9.6	0.0						
Lane LOS	E	C	B		A							
Approach Delay (s)	46.4	20.9	0.1		0.4							
Approach LOS	E	C										
Intersection Summary												
Average Delay				0.9								
Intersection Capacity Utilization				59.7%	ICU Level of Service	B						
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↔			↔		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	13	6	28	1	1	3	22	115	0	6	85	9
Future Volume (vph)	13	6	28	1	1	3	22	115	0	6	85	9
Peak Hour Factor	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85	0.85
Hourly flow rate (vph)	15	7	33	1	1	4	26	135	0	7	100	11
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	55	6	161	118								
Volume Left (vph)	15	1	26	7								
Volume Right (vph)	33	4	0	11								
Hadj (s)	-0.27	-0.33	0.07	-0.01								
Departure Headway (s)	4.2	4.2	4.2	4.2								
Degree Utilization, x	0.06	0.01	0.19	0.14								
Capacity (veh/h)	784	779	830	839								
Control Delay (s)	7.5	7.3	8.2	7.9								
Approach Delay (s)	7.5	7.3	8.2	7.9								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay	8.0											
Level of Service	A											
Intersection Capacity Utilization	26.0%		ICU Level of Service		A							
Analysis Period (min)	15											

HCM Unsignalized Intersection Capacity Analysis

8: SR 1 & Higgins Canyon Rd

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	↔	↔	↕	↕	↔	↔		
Traffic Volume (veh/h)	74	39	714	101	33	912		
Future Volume (Veh/h)	74	39	714	101	33	912		
Sign Control	Stop		Free		Free			
Grade	0%		0%		0%			
Peak Hour Factor	0.95	0.95	0.95	0.95	0.95	0.95		
Hourly flow rate (vph)	78	41	752	106	35	960		
Pedestrians								
Lane Width (ft)								
Walking Speed (ft/s)								
Percent Blockage								
Right turn flare (veh)								
Median type			None			None		
Median storage (veh)								
Upstream signal (ft)								
pX, platoon unblocked								
vC, conflicting volume	1302	376			752			
vC1, stage 1 conf vol								
vC2, stage 2 conf vol								
vCu, unblocked vol	1302	376			752			
tC, single (s)	6.8	6.9			4.1			
tC, 2 stage (s)								
tF (s)	3.5	3.3			2.2			
pD queue free %	47	93			96			
cM capacity (veh/h)	146	622			853			
Direction, Lane #	WB 1	WB 2	NB 1	NB 2	NB 3	SB 1	SB 2	SB 3
Volume Total	78	41	376	376	106	35	480	480
Volume Left	78	0	0	0	0	35	0	0
Volume Right	0	41	0	0	106	0	0	0
sSH	146	622	1700	1700	1700	853	1700	1700
Volume to Capacity	0.53	0.07	0.22	0.22	0.06	0.04	0.28	0.28
Queue Length 95th (ft)	66	5	0	0	0	3	0	0
Control Delay (s)	54.8	11.2	0.0	0.0	0.0	9.4	0.0	0.0
Lane LOS	F	B				A		
Approach Delay (s)	39.8		0.0			0.3		
Approach LOS	E							
Intersection Summary								
Average Delay	2.6							
Intersection Capacity Utilization	37.2%		ICU Level of Service		A			
Analysis Period (min)	15							

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	51	73	82	208	126	27
Future Volume (Veh/h)	51	73	82	208	126	27
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	51	73	82	208	126	27
Pedestrians	15		7		6	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		1	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	532	162	168			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	532	162	168			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	89	92	94			
cM capacity (veh/h)	470	867	1392			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	124	290	153			
Volume Left	51	82	0			
Volume Right	73	0	27			
eSH	643	1392	1700			
Volume to Capacity	0.19	0.06	0.09			
Queue Length 95th (ft)	18	5	0			
Control Delay (s)	11.9	2.6	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.9	2.6	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			3.9			
Intersection Capacity Utilization			44.8%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St


05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations		↔			↔		↕	↕		↕	↕		
Traffic Volume (veh/h)	7	3	3	2	3	30	5	685	2	41	488	5	
Future Volume (Veh/h)	7	3	3	2	3	30	5	685	2	41	488	5	
Sign Control	Stop			Stop			Free			Free			
Grade	0%			0%			0%			0%			
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Hourly flow rate (vph)	7	3	3	2	3	30	5	685	2	41	488	5	
Pedestrians													
Lane Width (ft)													
Walking Speed (ft/s)													
Percent Blockage													
Right turn flare (veh)													
Median type							None			None			
Median storage (veh)													
Upstream signal (ft)							1268			1190			
pX, platoon unblocked													
vC, conflicting volume	1299	1270	490	1270	1271	686	493						687
vC1, stage 1 conf vol													
vC2, stage 2 conf vol													
vCu, unblocked vol	1299	1270	490	1270	1271	686	493						687
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1						4.1
tC, 2 stage (s)													
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2						2.2
p0 queue free %	94	98	99	99	98	93	100						95
cM capacity (veh/h)	122	160	578	137	159	447	1071						907
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2							
Volume Total	13	35	5	687	41	493							
Volume Left	7	2	5	0	41	0							
Volume Right	3	30	0	2	0	5							
eSH	160	348	1071	1700	907	1700							
Volume to Capacity	0.08	0.10	0.00	0.40	0.05	0.29							
Queue Length 95th (ft)	7	8	0	0	4	0							
Control Delay (s)	29.4	16.5	8.4	0.0	9.2	0.0							
Lane LOS	D	C	A		A								
Approach Delay (s)	29.4	16.5	0.1	0.7									
Approach LOS	D	C											
Intersection Summary													
Average Delay				1.1									
Intersection Capacity Utilization				46.2%	ICU Level of Service	A							
Analysis Period (min)				15									

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020




Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	16	6	25	0	11	9	24	131	0	9	65	18
Future Volume (vph)	16	6	25	0	11	9	24	131	0	9	65	18
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	16	6	25	0	11	9	24	131	0	9	65	18
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	47	20	155	92								
Volume Left (vph)	16	0	24	9								
Volume Right (vph)	25	9	0	18								
Hadj (s)	-0.22	-0.24	0.06	-0.06								
Departure Headway (s)	4.2	4.3	4.2	4.1								
Degree Utilization, x	0.06	0.02	0.18	0.11								
Capacity (veh/h)	798	783	832	847								
Control Delay (s)	7.5	7.4	8.1	7.6								
Approach Delay (s)	7.5	7.4	8.1	7.6								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay	7.8											
Level of Service	A											
Intersection Capacity Utilization	29.3%		ICU Level of Service		A							
Analysis Period (min)	15											

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020



Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↔	↔	↕	↕	↔	↔
Traffic Volume (vph)	69	22	667	114	32	462
Future Volume (vph)	69	22	667	114	32	462
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Fr	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	69	22	667	114	32	462
RTOR Reduction (vph)	0	20	0	39	0	0
Lane Group Flow (vph)	69	2	667	75	32	462
Turn Type	Prot	Perm	NA	Prot	Prot	NA
Protected Phases	8		2	2	1	6
Permitted Phases	8					
Actuated Green, G (s)	4.8	4.8	33.4	33.4	0.9	38.3
Effective Green, g (s)	4.8	4.8	33.4	33.4	0.9	38.3
Actuated g/C Ratio	0.09	0.09	0.65	0.65	0.02	0.75
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	166	148	2313	1034	31	2652
v/s Ratio Prot	c0.04		c0.19	0.05	c0.02	0.13
v/s Ratio Perm	0.00					
v/c Ratio	0.42	0.01	0.29	0.07	1.03	0.17
Uniform Delay, d1	21.8	21.0	3.8	3.2	25.1	1.8
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.7	0.0	0.3	0.1	171.6	0.1
Delay (s)	23.5	21.0	4.1	3.4	196.7	2.0
Level of Service	C	C	A	A	F	A
Approach Delay (s)	22.9		4.0			14.6
Approach LOS	C		A			B
Intersection Summary						
HCM 2000 Control Delay	9.1		HCM 2000 Level of Service		A	
HCM 2000 Volume to Capacity ratio	0.32					
Actuated Cycle Length (s)	51.1		Sum of lost time (s)		12.0	
Intersection Capacity Utilization	35.6%		ICU Level of Service		A	
Analysis Period (min)	15					
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	33	42	31	156	168	66
Future Volume (Veh/h)	33	42	31	156	168	66
Sign Control	Stop			Free		Free
Grade	0%			0%		0%
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	33	42	31	156	168	66
Pedestrians	9			8		2
Lane Width (ft)	12.0			12.0		12.0
Walking Speed (ft/s)	4.0			4.0		4.0
Percent Blockage	1			1		0
Right turn flare (veh)						
Median type				None		None
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	430	218	243			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	430	218	243			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	94	95	98			
cM capacity (veh/h)	563	810	1313			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	75	187	234			
Volume Left	33	31	0			
Volume Right	42	0	66			
eSH	679	1313	1700			
Volume to Capacity	0.11	0.02	0.14			
Queue Length 95th (ft)	9	2	0			
Control Delay (s)	11.0	1.5	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.0	1.5	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.2			
Intersection Capacity Utilization			40.0%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↕			↕		
Traffic Volume (veh/h)	4	3	6	2	0	39	8	663	10	36	902	11
Future Volume (Veh/h)	4	3	6	2	0	39	8	663	10	36	902	11
Sign Control	Stop			Stop			Free		Free			
Grade	0%			0%			0%		0%			
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	4	3	6	2	0	39	8	663	10	36	902	11
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)							1268		1190			
pX, platoon unblocked												
vC, conflicting volume	1698	1668	908	1666	1669	668	913	673				
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1698	1668	908	1666	1669	668	913	673				
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1	4.1				
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2	2.2				
p0 queue free %	94	97	98	97	100	91	99	96				
cM capacity (veh/h)	64	91	333	71	91	458	746	918				
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	13	41	8	673	36	913						
Volume Left	4	2	8	0	36	0						
Volume Right	6	39	0	10	0	11						
eSH	115	362	746	1700	918	1700						
Volume to Capacity	0.11	0.11	0.01	0.40	0.04	0.54						
Queue Length 95th (ft)	9	10	1	0	3	0						
Control Delay (s)	40.3	16.2	9.9	0.0	9.1	0.0						
Lane LOS	E	C	A		A							
Approach Delay (s)	40.3	16.2	0.1	0.3								
Approach LOS	E	C										
Intersection Summary												
Average Delay					0.9							
Intersection Capacity Utilization					58.5%		ICU Level of Service	B				
Analysis Period (min)					15							

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	17	6	22	0	6	4	18	109	2	7	102	8
Future Volume (vph)	17	6	22	0	6	4	18	109	2	7	102	8
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	17	6	22	0	6	4	18	109	2	7	102	8
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	45	10	129	117								
Volume Left (vph)	17	0	18	7								
Volume Right (vph)	22	4	2	8								
Hadj (s)	-0.18	-0.21	0.05	0.00								
Departure Headway (s)	4.3	4.3	4.2	4.2								
Degree Utilization, x	0.05	0.01	0.15	0.14								
Capacity (veh/h)	795	778	835	847								
Control Delay (s)	7.5	7.3	7.9	7.8								
Approach Delay (s)	7.5	7.3	7.9	7.8								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay				7.8								
Level of Service				A								
Intersection Capacity Utilization				28.8%	ICU Level of Service							A
Analysis Period (min)				15								

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↕	↕	↕	↕	↕	↕
Traffic Volume (vph)	86	26	651	94	31	879
Future Volume (vph)	86	26	651	94	31	879
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	86	26	651	94	31	879
RTOR Reduction (vph)	0	23	0	34	0	0
Lane Group Flow (vph)	86	3	651	60	31	879
Turn Type	Prot	Perm	NA	Prot	Prot	NA
Protected Phases	8		2	2	1	6
Permitted Phases	8					
Actuated Green, G (s)	5.2	5.2	32.5	32.5	0.8	37.3
Effective Green, g (s)	5.2	5.2	32.5	32.5	0.8	37.3
Actuated g/C Ratio	0.10	0.10	0.64	0.64	0.02	0.74
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	182	163	2277	1018	28	2613
v/s Ratio Prot	c0.05		0.18	0.04	c0.02	c0.25
v/s Ratio Perm	0.00					
v/c Ratio	0.47	0.02	0.29	0.06	1.11	0.34
Uniform Delay, d1	21.4	20.4	3.9	3.3	24.9	2.3
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.9	0.0	0.3	0.1	204.7	0.3
Delay (s)	23.3	20.4	4.2	3.4	229.5	2.6
Level of Service	C	C	A	A	F	A
Approach Delay (s)	22.6		4.1			10.4
Approach LOS	C		A			B
Intersection Summary						
HCM 2000 Control Delay			8.5	HCM 2000 Level of Service		A
HCM 2000 Volume to Capacity ratio			0.39			
Actuated Cycle Length (s)			50.5	Sum of lost time (s)	12.0	
Intersection Capacity Utilization			36.1%	ICU Level of Service	A	
Analysis Period (min)			15			
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↑	↑	
Traffic Volume (veh/h)	42	21	38	167	127	62
Future Volume (Veh/h)	42	21	38	167	127	62
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	42	21	38	167	127	62
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	412	175	198			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	412	175	198			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	93	98	97			
cM capacity (veh/h)	574	856	1364			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	63	205	189			
Volume Left	42	38	0			
Volume Right	21	0	62			
eSH	645	1364	1700			
Volume to Capacity	0.10	0.03	0.11			
Queue Length 95th (ft)	8	2	0			
Control Delay (s)	11.2	1.6	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.2	1.6	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.3			
Intersection Capacity Utilization	38.4%		ICU Level of Service	A		
Analysis Period (min)	15					

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↑	↑		↑	↑	
Traffic Volume (veh/h)	3	2	5	3	2	35	6	777	5	47	987	7
Future Volume (Veh/h)	3	2	5	3	2	35	6	777	5	47	987	7
Sign Control	Stop			Stop			Free		Free			
Grade	0%			0%			0%		0%			
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	3	2	5	3	2	35	6	777	5	47	987	7
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)							1267		1190			
pX, platoon unblocked												
vC, conflicting volume	1910	1878	992	1880	1880	780	994			782		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1910	1878	992	1880	1880	780	994			782		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	93	97	98	94	97	91	99			94		
cM capacity (veh/h)	44	67	298	50	67	396	696			836		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	10	40	6	782	47	994						
Volume Left	3	3	6	0	47	0						
Volume Right	5	35	0	5	0	7						
eSH	87	223	696	1700	836	1700						
Volume to Capacity	0.12	0.18	0.01	0.46	0.06	0.58						
Queue Length 95th (ft)	9	16	1	0	4	0						
Control Delay (s)	51.8	24.6	10.2	0.0	9.6	0.0						
Lane LOS	F	C	B	A								
Approach Delay (s)	51.8	24.6	0.1	0.4								
Approach LOS	F	C										
Intersection Summary												
Average Delay				1.1								
Intersection Capacity Utilization	62.7%			ICU Level of Service		B						
Analysis Period (min)	15											

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	14	7	29	2	2	4	23	122	0	7	90	10
Future Volume (vph)	14	7	29	2	2	4	23	122	0	7	90	10
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	14	7	29	2	2	4	23	122	0	7	90	10
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	50	8	145	107								
Volume Left (vph)	14	2	23	7								
Volume Right (vph)	29	4	0	10								
Hadj (s)	-0.26	-0.22	0.07	-0.01								
Departure Headway (s)	4.2	4.3	4.2	4.2								
Degree Utilization, x	0.06	0.01	0.17	0.12								
Capacity (veh/h)	806	775	834	845								
Control Delay (s)	7.5	7.3	8.1	7.8								
Approach Delay (s)	7.5	7.3	8.1	7.8								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay	7.8											
Level of Service	A											
Intersection Capacity Utilization	26.3%		ICU Level of Service		A							
Analysis Period (min)	15											

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↕	↕	↕	↕	↕	↕
Traffic Volume (vph)	79	41	757	107	35	967
Future Volume (vph)	79	41	757	107	35	967
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	79	41	757	107	35	967
RTOR Reduction (vph)	0	37	0	38	0	0
Lane Group Flow (vph)	79	4	757	69	35	967
Turn Type	Prot	Perm	NA	Perm	Prot	NA
Protected Phases	8		2		1	6
Permitted Phases		8		2		
Actuated Green, G (s)	5.0	5.0	32.1	32.1	0.8	36.9
Effective Green, g (s)	5.0	5.0	32.1	32.1	0.8	36.9
Actuated g/C Ratio	0.10	0.10	0.64	0.64	0.02	0.74
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	177	158	2276	1018	28	2617
v/s Ratio Prot	c0.04		0.21		c0.02	c0.27
v/s Ratio Perm		0.00		0.04		
v/c Ratio	0.45	0.03	0.33	0.07	1.25	0.37
Uniform Delay, d1	21.1	20.3	4.0	3.3	24.6	2.3
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.8	0.1	0.4	0.1	254.6	0.4
Delay (s)	22.9	20.3	4.4	3.4	279.1	2.7
Level of Service	C	C	A	A	F	A
Approach Delay (s)	22.0		4.3			12.4
Approach LOS	C		A			B
Intersection Summary						
HCM 2000 Control Delay	9.5		HCM 2000 Level of Service		A	
HCM 2000 Volume to Capacity ratio	0.42					
Actuated Cycle Length (s)	49.9		Sum of lost time (s)		12.0	
Intersection Capacity Utilization	38.6%		ICU Level of Service		A	
Analysis Period (min)	15					
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	58	83	94	236	143	30
Future Volume (Veh/h)	58	83	94	236	143	30
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	58	83	94	236	143	30
Pedestrians	15		7		6	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		1	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	603	180	188			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	603	180	188			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	86	90	93			
cM capacity (veh/h)	423	847	1369			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	141	330	173			
Volume Left	58	94	0			
Volume Right	83	0	30			
eSH	600	1369	1700			
Volume to Capacity	0.24	0.07	0.10			
Queue Length 95th (ft)	23	6	0			
Control Delay (s)	12.8	2.7	0.0			
Lane LOS	B	A				
Approach Delay (s)	12.8	2.7	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			4.2			
Intersection Capacity Utilization			48.4%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↕	↕		↕	↕	
Traffic Volume (veh/h)	8	3	3	2	3	33	5	792	2	45	571	5
Future Volume (Veh/h)	8	3	3	2	3	33	5	792	2	45	571	5
Sign Control	Stop			Stop			Free			Free		
Grade	0%			0%			0%			0%		
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	8	3	3	2	3	33	5	792	2	45	571	5
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type							None			None		
Median storage (veh)												
Upstream signal (ft)							1268			1190		
pX, platoon unblocked												
vC, conflicting volume	1500	1468	574	1468	1469	793	576				794	
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	1500	1468	574	1468	1469	793	576				794	
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1				4.1	
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2				2.2	
p0 queue free %	91	98	99	98	97	92	99				95	
cM capacity (veh/h)	86	120	519	98	120	389	997				827	
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	14	38	5	794	45	576						
Volume Left	8	2	5	0	45	0						
Volume Right	3	33	0	2	0	5						
eSH	113	292	997	1700	827	1700						
Volume to Capacity	0.12	0.13	0.01	0.47	0.05	0.34						
Queue Length 95th (ft)	10	11	0	0	4	0						
Control Delay (s)	41.3	19.2	8.6	0.0	9.6	0.0						
Lane LOS	E	C	A		A							
Approach Delay (s)	41.3	19.2	0.1	0.7								
Approach LOS	E	C										
Intersection Summary												
Average Delay						1.2						
Intersection Capacity Utilization						52.5%	ICU Level of Service	A				
Analysis Period (min)						15						

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	18	6	27	0	12	10	26	149	0	10	74	21
Future Volume (vph)	18	6	27	0	12	10	26	149	0	10	74	21
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	18	6	27	0	12	10	26	149	0	10	74	21
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	51	22	175	105								
Volume Left (vph)	18	0	26	10								
Volume Right (vph)	27	10	0	21								
Hadj (s)	-0.21	-0.24	0.06	-0.07								
Departure Headway (s)	4.3	4.3	4.2	4.2								
Degree Utilization, x	0.06	0.03	0.21	0.12								
Capacity (veh/h)	768	764	826	838								
Control Delay (s)	7.6	7.5	8.3	7.8								
Approach Delay (s)	7.6	7.5	8.3	7.8								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay	8.0											
Level of Service	A											
Intersection Capacity Utilization	30.7%		ICU Level of Service		A							
Analysis Period (min)	15											

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↕	↕	↕	↕	↕	↕
Traffic Volume (vph)	79	24	773	130	35	543
Future Volume (vph)	79	24	773	130	35	543
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	79	24	773	130	35	543
RTOR Reduction (vph)	0	22	0	46	0	0
Lane Group Flow (vph)	79	2	773	84	35	543
Turn Type	Prot	Perm	NA	Prot	Prot	NA
Protected Phases	8		2	2	1	6
Permitted Phases	8					
Actuated Green, G (s)	5.0	5.0	32.7	32.7	0.8	37.5
Effective Green, g (s)	5.0	5.0	32.7	32.7	0.8	37.5
Actuated g/C Ratio	0.10	0.10	0.65	0.65	0.02	0.74
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	175	156	2291	1025	28	2627
v/s Ratio Prot	c0.04		c0.22	0.05	c0.02	0.15
v/s Ratio Perm	0.00					
v/c Ratio	0.45	0.02	0.34	0.08	1.25	0.21
Uniform Delay, d1	21.5	20.5	4.0	3.3	24.9	2.0
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.8	0.0	0.4	0.2	254.6	0.2
Delay (s)	23.3	20.6	4.4	3.5	279.4	2.2
Level of Service	C	C	A	A	F	A
Approach Delay (s)	22.7		4.3			18.9
Approach LOS	C		A			B
Intersection Summary						
HCM 2000 Control Delay	10.8		HCM 2000 Level of Service		B	
HCM 2000 Volume to Capacity ratio	0.37					
Actuated Cycle Length (s)	50.5		Sum of lost time (s)		12.0	
Intersection Capacity Utilization	39.1%		ICU Level of Service		A	
Analysis Period (min)	15					
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	39	49	37	183	197	78
Future Volume (Veh/h)	39	49	37	183	197	78
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	39	49	37	183	197	78
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	504	253	284			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	504	253	284			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
p0 queue free %	92	94	97			
cM capacity (veh/h)	507	775	1269			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	88	220	275			
Volume Left	39	37	0			
Volume Right	49	0	78			
cSH	628	1269	1700			
Volume to Capacity	0.14	0.03	0.16			
Queue Length 95th (ft)	12	2	0			
Control Delay (s)	11.7	1.5	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.7	1.5	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.3			
Intersection Capacity Utilization			44.5%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔		↕	↕		↕	↕	
Traffic Volume (veh/h)	4	3	7	2	0	44	9	801	12	40	1075	13
Future Volume (Veh/h)	4	3	7	2	0	44	9	801	12	40	1075	13
Sign Control	Stop			Stop			Free			Free		
Grade	0%			0%			0%			0%		
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	4	3	7	2	0	44	9	801	12	40	1075	13
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None			None		
Median storage (veh)												
Upstream signal (ft)							1268			1190		
pX, platoon unblocked												
vC, conflicting volume	2024	1992	1082	1990	1993	807	1088				813	
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	2024	1992	1082	1990	1993	807	1088				813	
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1				4.1	
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2				2.2	
p0 queue free %	89	95	97	95	100	88	99				95	
cM capacity (veh/h)	36	57	264	40	57	381	641				814	
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	14	46	9	813	40	1088						
Volume Left	4	2	9	0	40	0						
Volume Right	7	44	0	12	0	13						
cSH	74	279	641	1700	814	1700						
Volume to Capacity	0.19	0.16	0.01	0.48	0.05	0.64						
Queue Length 95th (ft)	16	15	1	0	4	0						
Control Delay (s)	65.0	20.4	10.7	0.0	9.7	0.0						
Lane LOS	F	C	B	A								
Approach Delay (s)	65.0	20.4	0.1	0.3								
Approach LOS	F	C										
Intersection Summary												
Average Delay				1.2								
Intersection Capacity Utilization				67.7%			ICU Level of Service	C				
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	20	7	24	0	7	4	19	128	2	8	119	9
Future Volume (vph)	20	7	24	0	7	4	19	128	2	8	119	9
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	20	7	24	0	7	4	19	128	2	8	119	9
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	51	11	149	136								
Volume Left (vph)	20	0	19	8								
Volume Right (vph)	24	4	2	9								
Hadj (s)	-0.17	-0.18	0.05	0.01								
Departure Headway (s)	4.4	4.4	4.2	4.2								
Degree Utilization, x	0.06	0.01	0.18	0.16								
Capacity (veh/h)	762	752	827	838								
Control Delay (s)	7.7	7.5	8.1	8.0								
Approach Delay (s)	7.7	7.5	8.1	8.0								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay				8.0								
Level of Service				A								
Intersection Capacity Utilization			29.6%	ICU Level of Service			A					
Analysis Period (min)				15								

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↕	↕	↕	↕	↕	↕
Traffic Volume (vph)	101	29	788	110	35	1050
Future Volume (vph)	101	29	788	110	35	1050
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	101	29	788	110	35	1050
RTOR Reduction (vph)	0	26	0	40	0	0
Lane Group Flow (vph)	101	3	788	70	35	1050
Turn Type	Prot	Perm	NA	Prot	Prot	NA
Protected Phases	8		2	2	1	6
Permitted Phases	8					
Actuated Green, G (s)	5.4	5.4	31.8	31.8	0.8	36.6
Effective Green, g (s)	5.4	5.4	31.8	31.8	0.8	36.6
Actuated g/C Ratio	0.11	0.11	0.64	0.64	0.02	0.73
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	191	170	2250	1006	28	2590
v/s Ratio Prot	c0.06		0.22	0.04	c0.02	c0.30
v/s Ratio Perm	0.00					
v/c Ratio	0.53	0.02	0.35	0.07	1.25	0.41
Uniform Delay, d1	21.1	19.9	4.3	3.5	24.6	2.6
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	2.6	0.0	0.4	0.1	254.6	0.5
Delay (s)	23.7	20.0	4.7	3.6	279.2	3.0
Level of Service	C	B	A	A	F	A
Approach Delay (s)	22.9		4.6			11.9
Approach LOS	C		A			B
Intersection Summary						
HCM 2000 Control Delay			9.5	HCM 2000 Level of Service	A	
HCM 2000 Volume to Capacity ratio			0.47			
Actuated Cycle Length (s)			50.0	Sum of lost time (s)	12.0	
Intersection Capacity Utilization			41.3%	ICU Level of Service	A	
Analysis Period (min)			15			
c Critical Lane Group						

HCM Unsignalized Intersection Capacity Analysis
5: Main St & Poplar St

05/01/2020

Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↔			↕	↕	
Traffic Volume (veh/h)	49	24	44	196	148	73
Future Volume (Veh/h)	49	24	44	196	148	73
Sign Control	Stop		Free		Free	
Grade	0%		0%		0%	
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	49	24	44	196	148	73
Pedestrians	9		8		2	
Lane Width (ft)	12.0		12.0		12.0	
Walking Speed (ft/s)	4.0		4.0		4.0	
Percent Blockage	1		1		0	
Right turn flare (veh)						
Median type			None		None	
Median storage (veh)						
Upstream signal (ft)						
pX, platoon unblocked						
vC, conflicting volume	480	202	230			
vC1, stage 1 conf vol						
vC2, stage 2 conf vol						
vCu, unblocked vol	480	202	230			
tC, single (s)	6.4	6.2	4.1			
tC, 2 stage (s)						
tF (s)	3.5	3.3	2.2			
pD queue free %	91	97	97			
cM capacity (veh/h)	522	827	1328			
Direction, Lane #	EB 1	NB 1	SB 1			
Volume Total	73	240	221			
Volume Left	49	44	0			
Volume Right	24	0	73			
eSH	594	1328	1700			
Volume to Capacity	0.12	0.03	0.13			
Queue Length 95th (ft)	10	3	0			
Control Delay (s)	11.9	1.7	0.0			
Lane LOS	B	A				
Approach Delay (s)	11.9	1.7	0.0			
Approach LOS	B					
Intersection Summary						
Average Delay			2.4			
Intersection Capacity Utilization			42.0%	ICU Level of Service	A	
Analysis Period (min)			15			

HCM Unsignalized Intersection Capacity Analysis
6: SR 1 & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↔			↔			↕			↕		
Traffic Volume (veh/h)	3	2	5	3	2	38	7	934	5	51	1176	8
Future Volume (Veh/h)	3	2	5	3	2	38	7	934	5	51	1176	8
Sign Control	Stop			Stop			Free		Free			
Grade	0%			0%			0%		0%			
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	3	2	5	3	2	38	7	934	5	51	1176	8
Pedestrians							1					
Lane Width (ft)							12.0					
Walking Speed (ft/s)							4.0					
Percent Blockage							0					
Right turn flare (veh)												
Median type							None		None			
Median storage (veh)												
Upstream signal (ft)							1267		1190			
pX, platoon unblocked												
vC, conflicting volume	2269	2235	1181	2236	2236	936	1184	939				
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	2269	2235	1181	2236	2236	936	1184	939				
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1	4.1				
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2	2.2				
pD queue free %	87	95	98	89	95	88	99	93				
cM capacity (veh/h)	23	39	231	27	39	321	590	730				
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	10	43	7	939	51	1184						
Volume Left	3	3	7	0	51	0						
Volume Right	5	38	0	5	0	8						
eSH	49	152	590	1700	730	1700						
Volume to Capacity	0.20	0.28	0.01	0.55	0.07	0.70						
Queue Length 95th (ft)	17	27	1	0	6	0						
Control Delay (s)	96.6	37.6	11.2	0.0	10.3	0.0						
Lane LOS	F	E	B	B								
Approach Delay (s)	96.6	37.6	0.1	0.4								
Approach LOS	F	E										
Intersection Summary												
Average Delay				1.4								
Intersection Capacity Utilization				72.7%	ICU Level of Service	C						
Analysis Period (min)				15								

HCM Unsignalized Intersection Capacity Analysis

7: Main St & Seymour St

05/01/2020

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↕			↕			↕			↕		
Sign Control	Stop			Stop			Stop			Stop		
Traffic Volume (vph)	17	8	29	2	2	4	23	142	0	8	105	12
Future Volume (vph)	17	8	29	2	2	4	23	142	0	8	105	12
Peak Hour Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Hourly flow rate (vph)	17	8	29	2	2	4	23	142	0	8	105	12
Direction, Lane #	EB 1	WB 1	NB 1	SB 1								
Volume Total (vph)	54	8	165	125								
Volume Left (vph)	17	2	23	8								
Volume Right (vph)	29	4	0	12								
Hadj (s)	-0.23	-0.22	0.06	-0.01								
Departure Headway (s)	4.3	4.4	4.2	4.2								
Degree Utilization, x	0.06	0.01	0.19	0.15								
Capacity (veh/h)	770	753	828	837								
Control Delay (s)	7.6	7.4	8.2	7.9								
Approach Delay (s)	7.6	7.4	8.2	7.9								
Approach LOS	A	A	A	A								
Intersection Summary												
Delay	8.0											
Level of Service	A											
Intersection Capacity Utilization	27.4%		ICU Level of Service		A							
Analysis Period (min)	15											

HCM Signalized Intersection Capacity Analysis

8: SR 1 & Main St

05/01/2020

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	↕	↕	↕	↕	↕	↕
Traffic Volume (vph)	92	46	912	125	38	1154
Future Volume (vph)	92	46	912	125	38	1154
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Util. Factor	1.00	1.00	0.95	1.00	1.00	0.95
Frt	1.00	0.85	1.00	0.85	1.00	1.00
Fit Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1770	1583	3539	1583	1770	3539
Fit Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1770	1583	3539	1583	1770	3539
Peak-hour factor, PHF	1.00	1.00	1.00	1.00	1.00	1.00
Adj. Flow (vph)	92	46	912	125	38	1154
RTOR Reduction (vph)	0	40	0	51	0	0
Lane Group Flow (vph)	92	6	912	74	38	1154
Turn Type	Prot	Perm	NA	Perm	Prot	NA
Protected Phases	8		2		1	6
Permitted Phases		8		2		
Actuated Green, G (s)	6.6	6.6	29.5	29.5	1.7	35.2
Effective Green, g (s)	6.6	6.6	29.5	29.5	1.7	35.2
Actuated g/C Ratio	0.13	0.13	0.59	0.59	0.03	0.71
Clearance Time (s)	4.0	4.0	4.0	4.0	4.0	4.0
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0
Lane Grp Cap (vph)	234	209	2096	937	60	2501
v/s Ratio Prot	c0.05		0.26		0.02	c0.33
v/s Ratio Perm		0.00		0.05		
v/c Ratio	0.39	0.03	0.44	0.08	0.63	0.46
Uniform Delay, d1	19.8	18.8	5.6	4.3	23.7	3.2
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	1.1	0.1	0.7	0.2	19.8	0.6
Delay (s)	20.9	18.9	6.2	4.5	43.5	3.8
Level of Service	C	B	A	A	D	A
Approach Delay (s)	20.2		6.0			5.1
Approach LOS	C		A			A
Intersection Summary						
HCM 2000 Control Delay	6.4		HCM 2000 Level of Service		A	
HCM 2000 Volume to Capacity ratio	0.50					
Actuated Cycle Length (s)	49.8		Sum of lost time (s)		12.0	
Intersection Capacity Utilization	43.7%		ICU Level of Service		A	
Analysis Period (min)	15					
c Critical Lane Group						

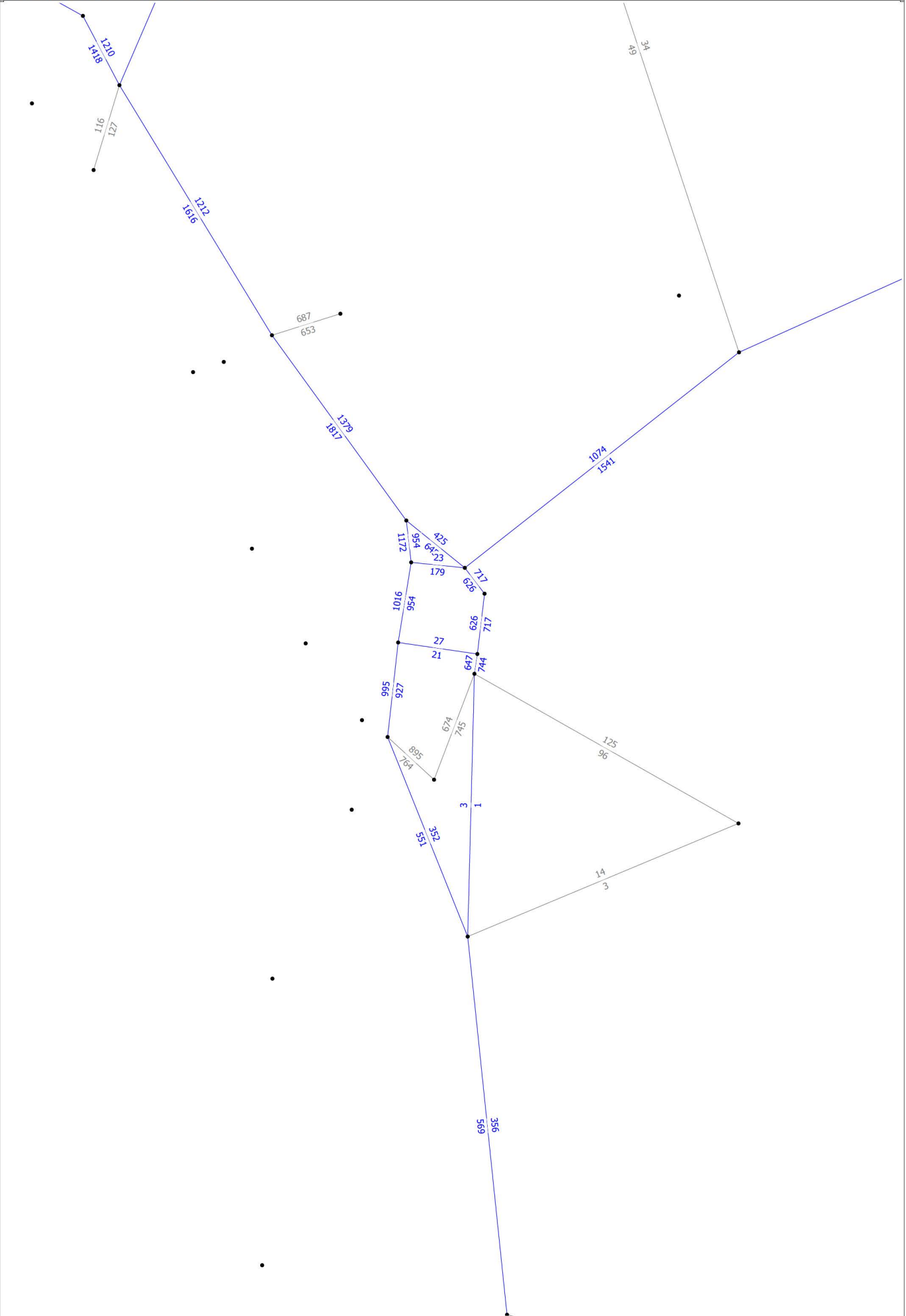
Appendix C

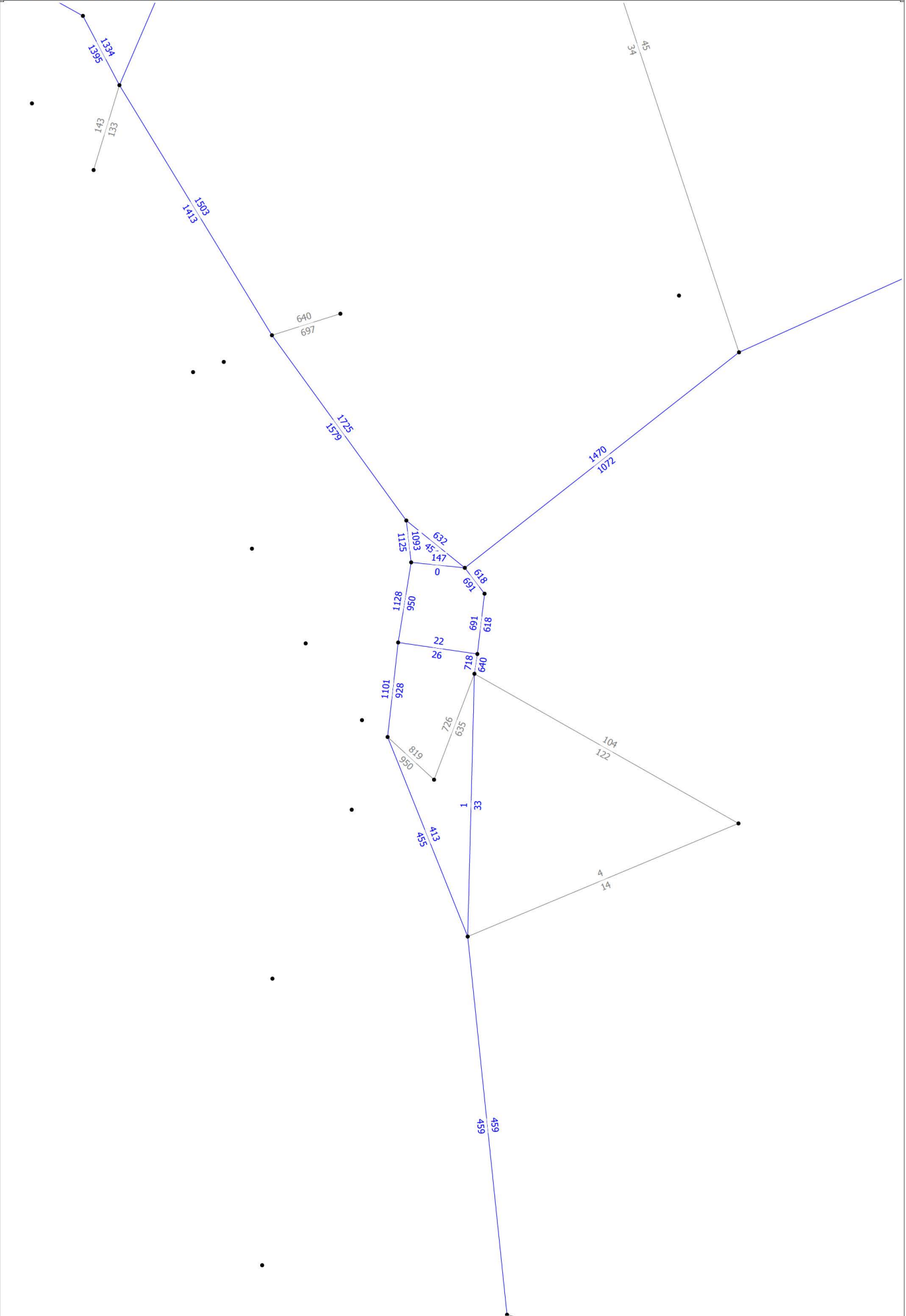
San Mateo County Travel Demand Model Forecasted Link Volume Plots

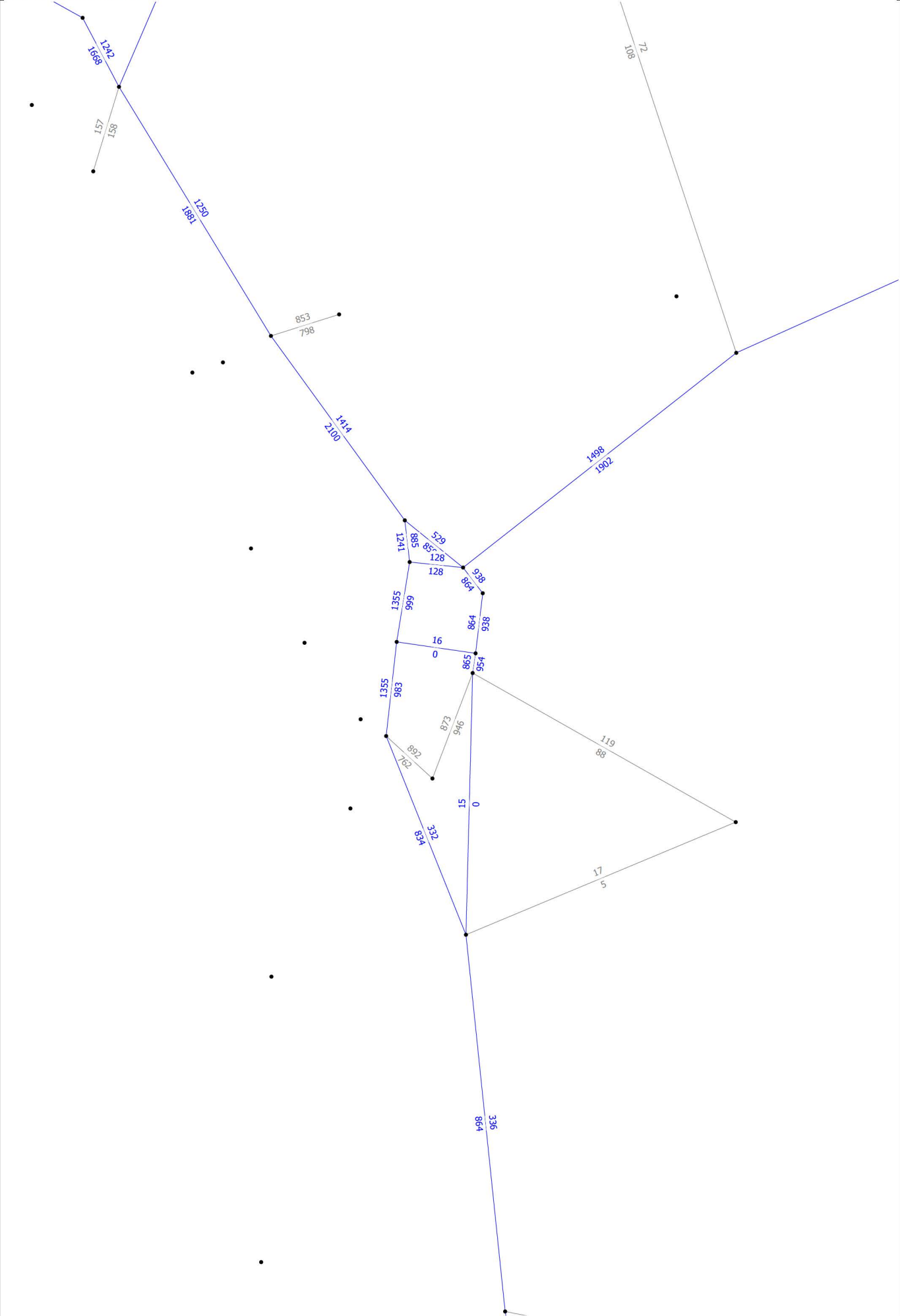


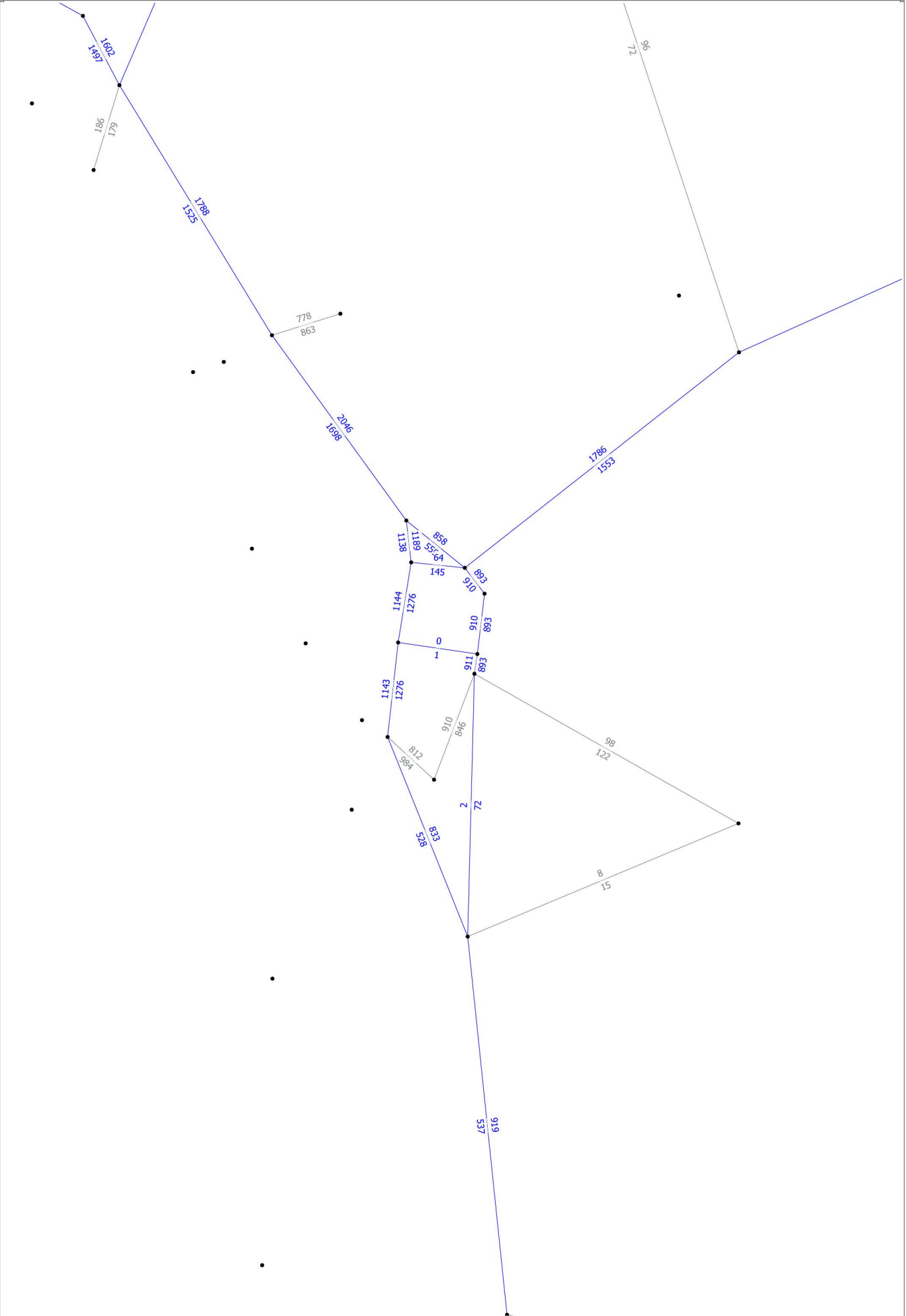


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Appendix D

Peak Hour Volume Warrant Worksheets





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Warrant 3: Peak-Hour Volumes and Delay

SR 1 & Seymour Street
Half Moon Bay

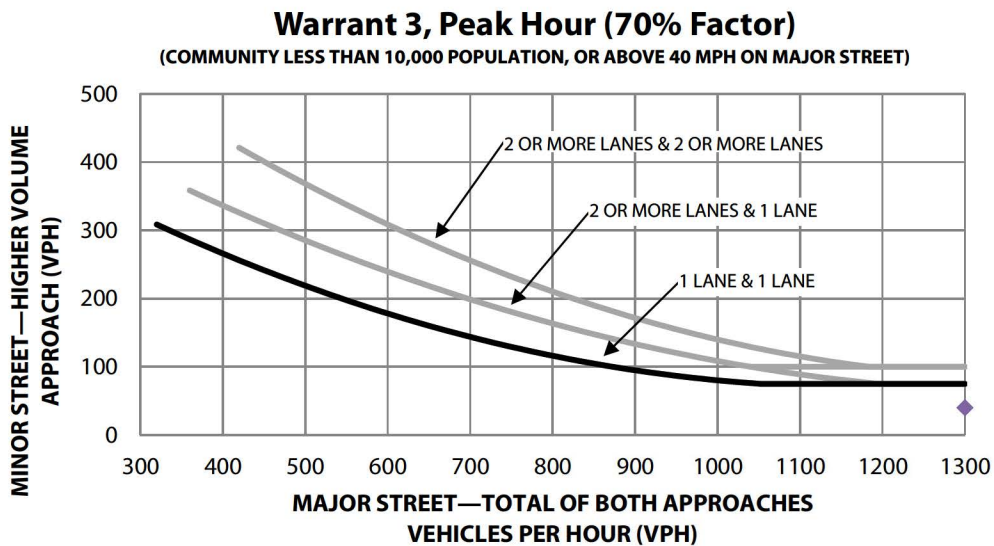
Project Name: Hyatt Place TIA

Intersection: 6

	<u>Major Street</u>	<u>Minor Street</u>
Street Name	SR 1	Seymour Street
Direction	N-S	E-W
Number of Lanes	1	1
Approach Speed	50	25

Population less than 10,000? No
Date of Count: Tuesday, June 19, 2018
Scenario: Background + Project Weekend

Warrant 3 Met?: Met when either Condition A or B is met	No
Condition A: Met when conditions A1, A2, and A3 are met	Not Met
Condition A1 The total delay experienced by traffic on one minor street approach (one direction only) controlled by a STOP sign equals or exceeds four vehicle-hours for a one lane approach, or five vehicle-hours for a two-lane approach Minor Approach Delay: 0.27 vehicle-hours	Not Met
Condition A2 The volume on the same minor street approach (one direction only) equals or exceeds 100 vph for one moving lane of traffic of 150 vph for two moving lanes Minor Approach Volume: 40 vph	Not Met
Condition A3 The total entering volume serviced during the hour equals or exceeds 800 vph for intersections with four or more approaches or 650 vph for intersections with three approaches Total Entering Volume: 1879 vph	Met
Condition B The plotted point falls above the curve	Not Met



Warrant 3: Peak-Hour Volumes and Delay

SR 1 & Seymour Street
Half Moon Bay

Project Name: Hyatt Place TIA

Intersection: 6

	<u>Major Street</u>	<u>Minor Street</u>
Street Name	SR 1	Seymour Street
Direction	N-S	E-W
Number of Lanes	1	1
Approach Speed	50	25

Population less than 10,000? No
Date of Count: Tuesday, June 19, 2018
Scenario: 2040 + Project PM

Warrant 3 Met?: Met when either Condition A or B is met

Condition A: Met when conditions A1, A2, and A3 are met

Condition A1

The total delay experienced by traffic on one minor street approach (one direction only) controlled by a STOP sign equals or exceeds four vehicle-hours for a one lane approach, or five vehicle-hours for a two-lane approach

Minor Approach Delay: 0.26 vehicle-hours

Condition A2

The volume on the same minor street approach (one direction only) equals or exceeds 100 vph for one moving lane of traffic or 150 vph for two moving lanes

Minor Approach Volume: 46 vph

Condition A3

The total entering volume serviced during the hour equals or exceeds 800 vph for intersections with four or more approaches or 650 vph for intersections with three approaches

Total Entering Volume: 2010 vph

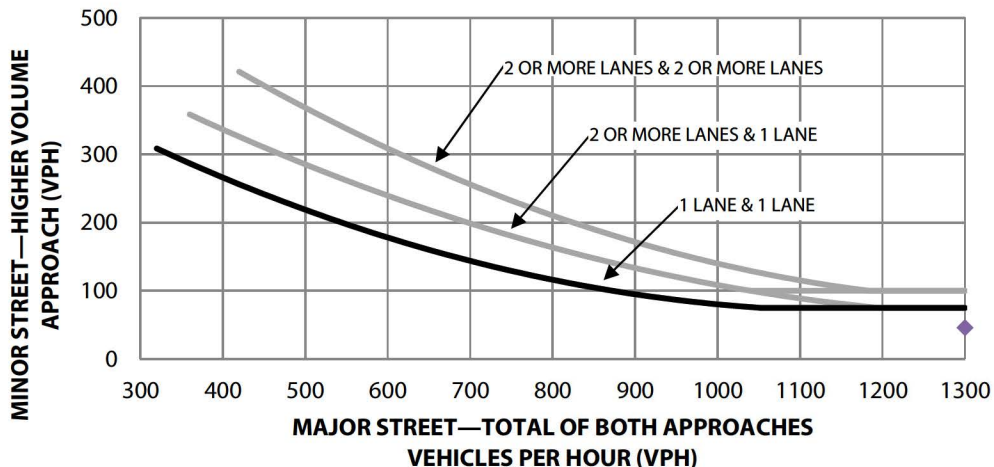
Condition B

The plotted point falls above the curve

No
Not Met
Not Met
Not Met
Met
Not Met

Warrant 3, Peak Hour (70% Factor)

(COMMUNITY LESS THAN 10,000 POPULATION, OR ABOVE 40 MPH ON MAJOR STREET)



Warrant 3: Peak-Hour Volumes and Delay

SR 1 & Seymour Street
Half Moon Bay

Project Name: Hyatt Place TIA

Intersection: 6

	<u>Major Street</u>	<u>Minor Street</u>
Street Name	SR 1	Seymour Street
Direction	N-S	E-W
Number of Lanes	1	1
Approach Speed	50	25

Population less than 10,000? No
Date of Count: Tuesday, June 19, 2018
Scenario: 2040 + Project SAT

Warrant 3 Met?: Met when either Condition A or B is met	No
Condition A: Met when conditions A1, A2, and A3 are met	Not Met
Condition A1 The total delay experienced by traffic on one minor street approach (one direction only) controlled by a STOP sign equals or exceeds four vehicle-hours for a one lane approach, or five vehicle-hours for a two-lane approach Minor Approach Delay: 0.45 vehicle-hours	Not Met
Condition A2 The volume on the same minor street approach (one direction only) equals or exceeds 100 vph for one moving lane of traffic of 150 vph for two moving lanes Minor Approach Volume: 43 vph	Not Met
Condition A3 The total entering volume serviced during the hour equals or exceeds 800 vph for intersections with four or more approaches or 650 vph for intersections with three approaches Total Entering Volume: 2234 vph	Met
Condition B The plotted point falls above the curve	Not Met

